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No. 385 App 76

No. Six App 76 7/17/30 N.H.

	Scimitar st.	Klauber to Bach	1-29
X	Attix	" " Radio Dr.	30-33
X	Orange	Winnet to Paradise	34-62
X	Paradise	Radio Dr. to Mariposa	63-68
X	Winnet	Scimitar - Orange	69-76

SCIMITAR STX Sec 6
Klauber to Bach.

12-23-27
miller

BM. 12.60 443.44 430.84 Pipe SW cor
Scimitar
+Klauber

Point A on Plat Book 1214-P.5 = E.C. Curve + white Klauber
white Klauber at P.C. 6.2 437.2

This portion of Curve $\Delta 30-38'$ divided into 4 parts

#B

N. line Scimitar at B. 11.4 432.0

3.8 S.E. on Rad. Line = N. Line Klauber 11.8 431.6

#C

N. line Scimitar at C 13.0 430.4

13. S.E. on Radial Line = W. Line Klauber 16.0 427.4

#D

N. Scimitar at D 9.4 434.0

7 S.E. on Radial Line 11.1 432.3

11 S.E. " " 14.3 429.1

81 S.E. " " = W. Line Klauber 16.0 427.4

E. on Radial Line from SW. Cor Scimitar + Klauber
Regular Section from E West

S 12.6 430.8 Scimitar

ch 11.2 432.2

114 9.7 433.7

C 9.5 433.9

114 10.1 433.3

+2 6.7 436.7

ch 5.2 438.2

N 2.9 440.5

T.P. 6.57 448.76 1.25 442.19

$L = 47.59'$
 $\Delta = 6.49'$

From Sec #E. W. to E.C. This portion of Curve $\Delta 68-10'$
Divided into 10 parts $\Delta 6-49'$

448.76

Sec #1 $\Delta 6-49'$

N 2.8 446.0

ch 5.8 443.0

114 7.3 444.5

+5 11.1 437.7

C 11.0 437.7 ✓

114 10.0 438.8 ✓

+5 12.4 436.4

ch 13.3 435.5

S 14.7 434.1

$L = 47.59'$
 $\Delta = 6.49'$

Sec #2 $\Delta 13-38'$

S 15.4 433.4

ch 13.0 435.8

+5 12.8 436.0

114 9.7 439.1

C 7.9 438.9 ✓

+4 10.1 438.7

+8 6.9 441.9

114 6.4 442.4

ch 4.0 444.8

N 2.1 446.7

$L = 47.59'$
 $\Delta = 6.49'$

Sec #3 $\Delta 20-27'$

N 1.9 446.9

ch 4.7 444.1

114 7.6 441.1

+5 11.8 437.0

C 11.6 437.2 ✓

$L = 47.6'$
 $\Delta = 10.54'$

448.76

14	11.8	4370 ✓
+5	14.6	4342
d	15.5	4333
S	18.0	4308
Sub station $\Delta 21^{\circ}-07'-54''$		
S	21.5	427.3 <small>under House House 4.7 in St.</small>
+8	21.2	427.6
d	15.5	433.3
+5	14.6	434.2
14	11.8	4370
c	11.6	4372 ✓
+5	11.4	4373
14	7.6	4412
d	4.7	4441
N	1.9	4469
T.P.	2.37	444.98 ✓
Sub station $\Delta 25^{\circ}-54'-12''$		
N	0.8	4442
d	3.3	4417
14	5.9	4391
+2	6.7	4383
+4	9.4	4356
c	9.3	4357 ✓
14	9.5	4357
+5	12.1	4329
+8	12.7	4323

 $\phi L = 33.31'$
 $\Delta = 4^{\circ} 46' 18''$
 $\phi L = 9.52'$
 $\Delta = 1^{\circ} 21' 48''$

444.98

Scimitar 2

d	17.3	4227
11-House		4268
S	18.2	<small>under House</small>
Sec # $\Delta 27^{\circ}-16'$		
S	17.0	4280
d	13.6	4314
+5	13.1	4317
14	9.4	4356
c	9.7	4353 ✓
+6	9.8	4352
+8	7.0	4380
14	6.4	4386
d	4.0	4410
N	1.1	4439
Sec # $\Delta 34^{\circ}-05'$		
N	3.4	4416
d	6.1	4389
14	8.1	4369
+4	10.8	4342
c	10.6	4344 ✓
14	10.4	4346
+4	12.8	4322
d	13.8	4312
S	15.6	4294

 $\phi L = 47.59'$
 $\Delta = 6^{\circ} 49'$
 $\phi L = 47.59'$
 $\Delta = 6^{\circ} 49'$

444.98

Sec #6

 $\Delta = 40^{\circ} 54'$

17.2

427 8

S

cb

14.5

430 5

1/4

12.8

432 2

+3

10.8

434 2

C

11.0

434 0 ✓

+6

11.0

434 0

1/4

8.7

436 3

cb

6.3

438 7

N

3.5

441 5

 $\Phi L = 61.55'$ $\Delta = 8^{\circ} 49'$

Sec #7

 $\Delta = 49^{\circ} 43'$

2.7

442 3

N

cb

5.2

439 8

1/4

8.5

436 5

+2

10.4

434 6

C

9.9

435 1 ✓

1/4

9.4

435 6

+3

12.4

432 6

cb

14.2

430 8

S

16.1

428 9

 $\Phi L = 33.63'$ $\Delta = 4^{\circ} 49'$

Sec #8

 $\Delta = 54^{\circ} 32'$

17.0

428 0

S

cb

14.7

430 3

+5

13.4

431 6

1/4

10.6

434 4

+2

9.6

435 4

C

9.8

435 2 ✓

 $\Phi L = 38.07'$ $\Delta = 5^{\circ} 27' 12''$

444.98

similar

3

1/4

9.8

432 2

+6

6.3

435 7

cb

5.7

439 3

N

2.1

442 9

sub station

 $\Delta = 59^{\circ} 59' - 12''$

3.4

441 6

N

cb

6.4

438 6

+5

7.1

437 9

+6

10.2

434 8

1/4

10.1

434 9

C

10.0

475 0 ✓

+5

7.9

434 1

1/4

12.8

432 2

cb

14.6

430 4

S

16.3

428 7

 $\Phi L = 9.52'$ $\Delta = 1^{\circ} 21' 48''$

Sec #9

 $\Delta = 61^{\circ} 21'$

22.0

423 0

S

+1

15.0

430 0

cb

14.6

430 4

1/4

12.0

433 0

+5

10.0

435 0

C

10.2

434 8 ✓

1/4

10.4

434 6

+4

10.5

434 5

cb

7.0

438 0

N

3.4

441 6

 $\Phi L = 47.59'$ $\Delta = 6^{\circ} 40' 02''$

444.98
 T.P. 2.81 444.03 3.76 441.22

Sec # 10 - P.R.C. curve # $\Delta 58^{\circ}36'$ $\phi.R. 300.0$ divided 8 Parts

N	$\phi R = 300$	1.7	4412 3
cb		4.8	439 2
+6		10.4	433 6
"4		10.1	433 9
c		10.0	4340 ✓
+2		10.0	4340 ✓
"4		14.8	429 2
cb		18.5	425 5
+3		23.6	420 4
S		23.1	420 9
Sec # $\Delta 7^{\circ}19'30''$			
S		22.8	421 2
+8		23.0	421 0
cb		21.0	423 0
+6		19.9	424 1
"4		17.0	427 0
+7		11.0	433 0
c		11.0	433 0 ✓
"4		11.2	432 8
+3		11.5	432 5
+7		9.9	434 1
cb		8.0	436 0
N		3.8	440 2

$\phi L = 38.35'$
 $\Delta = 7^{\circ}19'30''$

$\phi L = 38.35'$
 $\Delta = 7^{\circ}19'30''$

444.03
 Sec # 2 $\Delta 14^{\circ}39'$

N		1.7	442 3
cb		5.7	438 3
"4		8.7	435 3
+2		12.3	431 7
c		12.0	4320 ✓
+6		12.2	431 8
"4		14.5	429 5
+4		16.6	427 4
+8		17.2	426 8
cb		19.5	424 5
S		20.1	423 9
Sec # $\Delta 21^{\circ}58'30''$			
S		18.4	425 6
cb		15.8	428 2
"4		14.2	429 8
+1		12.6	431 4
c		13.1	430 9 ✓
+4		13.0	431 0
+8		8.8	435 2
"4		8.3	435 7
cb		5.5	438 5
N		2.6	441 4

$\phi L = 38.35'$
 $\Delta = 7^{\circ}19'30''$

$\phi L = 10.18'$
 $\Delta = 3^{\circ}30'45''$

Sub station $\Delta = 25^{\circ}38'15''$

N		4.1	439 9
cb		6.4	437 6 ✓
"4		8.8	435 2

scimitar 4

444.03 substation (con)

tl	13.5	430.5
c	14.0	430.0
"4	14.0	430.0
cl	16.1	427.9
S	18.4	425.6
sec #4 $\Delta 29^{\circ}-18'$		
S	21.6	422.4
cl	19.0	425.0
+7	16.5	428.5
"4	14.6	429.4
c	15.2	429.8
+5	15.0	429.0
"4	9.3	424.7
cl	7.1	436.9
N	5.5	428.5
sec #5 $\Delta 36^{\circ}-37'-30''$		
N	8.3	425.7
cl	10.8	433.2
"4	16.0	428.0
+3	16.6	427.4
c	16.6	427.4
+5	16.8	427.2
"4	18.8	425.2
cl	23.4	420.6
S	25.7	418.3

444.03 semitar
Sub Station $\Delta 40^{\circ}-17'-15''$

S	26.2	417.8
cl	23.7	420.3
"4	19.0	425.0
+3	17.4	426.6
c	17.3	426.7
+6	17.5	426.5
"4	15.3	428.7
cl	12.0	432.0
+8	10.0	434.0
N	8.0	436.0
sec #6 $\Delta 43^{\circ}-57'$		
N	8.2	435.8
+3	10.0	434.0
cl	11.4	432.6
"4	14.0	430.0
+5	18.0	426.0
c	17.6	426.4
"4	17.4	426.6
+3	19.7	424.3
cl	22.0	422.0
S	25.0	419.0
T.P. 0.73	433.64	11.12
sec #7 $\Delta 51^{\circ}-16'-30''$		
S	13.0	420.6
cl	10.8	422.8
"4	8.3	425.3

see #7 (cont)

C	8.5	425.1
+4	8.7	424.9
"4	4.7	428.9
cl	2.6	431.0
+6	11.4	432.2
N	0.0	433.6

see #8 = P.R.C. Curve 10 divided 4 Parts from this P.R.C. to

Radial line from S.E. Cor Semitar + Mcensts.
R=180

N	3.8	429.8
cl	5.5	428.1
+8	6.8	426.8
"4	8.2	425.4
+2	10.8	422.8
C	9.8	423.8
"4	9.4	424.2
cl	12.0	421.6
S	14.0	419.6

see #7 $\Delta 10^{\circ} 58' 30''$

S	14.9	418.7
cl	13.6	420.0
"4	11.9	421.7
+2	10.9	422.7
C	10.9	422.7
"4	11.9	421.7
+2	11.9	421.7
+8	8.0	425.6

cl	7.7	425.9
N	6.2	427.4

see #2 $\Delta 21^{\circ} 57'$

N	8.5	425.1
cl	9.5	424.1
+6	10.5	423.1
"4	13.3	420.3

 $\Delta L = 34.48'$
 $\Delta = 10^{\circ} 58' 30''$

C	12.4	421.2
+7	12.1	421.5
"4	13.2	420.4
+3	14.7	418.9
cl	15.2	418.4
S	17.0	416.6

see #3 $\Delta 32^{\circ} 55' 30''$

S	19.6	414.0
cl	18.0	415.6
"4	16.2	417.4
+4	14.9	419.7
C	15.0	418.6
"4	16.0	417.6
+5	12.0	421.6
cl	11.5	422.1
N	10.3	423.3

 $\Delta L = 17.24'$
 $\Delta = 52^{\circ} 29' 15''$

T.P.	1.65	422.89	12.40	421.24
------	------	--------	-------	--------

Substation $\Delta 38^{\circ}24'45''$

N	2.0	420.9
cl	3.8	419.1
+6	4.8	418.1
+7	6.1	416.8
-14	6.1	416.8
C	5.7	417.2
14 ⁺	6.0	416.9
cl	8.3	414.6
S	10.2	412.7

 $\Delta L = 17.24'$ $\Delta = 50^{\circ}28'15''$ Sec H $\Delta 43^{\circ}54'$ - Radial Line from S.E. Cor Wren to Scimitar

S	12.6	410.3
cl	10.8	412.1
14	9.0	413.9
+6	7.3	415.6
C	7.1	415.8
+4	7.5	415.4
+3	7.5	415.3
+7	4.2	418.7
cl	3.4	419.5
N	1.4	421.5

 $\Delta L = 23.12'$ $\Delta = 7^{\circ}21'29''$ on Radial Line of Wren $\Delta = 51^{\circ}15'29''$

N	2.3	420.6
cl	4.4	418.5
+5	9.1	413.8
14	8.7	414.2
C	8.6	414.3

 $\Delta L = 23.12'$ $\Delta = 7^{\circ}21'31''$

+5	8.1	414.8
14	9.9	413.0
cl	13.0	409.9
S	13.1	409.8

 $\Delta 58^{\circ}37'$ Radial Line from S.W. Cor Scimitar to Wren

S	17.5	405.4
cl	16.1	406.8
14	13.1	409.8
+6	10.3	412.6
C	10.6	412.3
14	10.5	412.4
+5	11.1	411.8
cl	6.6	416.3
N	4.5	418.4

 $\Delta L = 31.25'$ $\Delta = 9^{\circ}57'$ $\Delta 68^{\circ}34'$ - P.R. C. Bet Curve # 1049

N	5.3	417.6
cl	8.6	414.3
14	12.8	410.1
C	12.9	410.0
T.P.	6.97	417.48
	12.38	410.51
+5	7.0	410.5
14	9.3	408.2
cl	13.3	404.2
S	15.8	401.7

 $\Delta L = 26.81'$ $\Delta = 5^{\circ}41'24''$

417.48
Curve #9 divided into 5 parts $\Delta 5^{\circ} 41' 24''$
Sec #4 $\Delta 5^{\circ} 41' 24''$

N	S	17.0	400.5
cl	cl	14.3	403.2
+6	+3	12.9	404.6
+7	"4	8.8	408.7
-14	2	9.0	408.5
	+4	9.1	408.4
C	"4	6.5	411.0
14	cl	3.2	414.3
cl	N	1.0	416.5
S			
S	N	10.5	418.0
cl	cl	2.2	415.3
14	"4	5.2	412.3
+6	+2	5.5	412.0
C	+7	10.5	407.0
14	C	10.1	407.4
+2	"4	10.0	407.5
+3	+3	10.3	407.2
cl	cl	14.7	402.8
S	S	17.4	400.1
S		17.6	399.9
cl	cl	15.0	402.5
+5	+5	11.6	405.9
"4	"4	11.2	406.3
C	C	11.4	406.1

$L = 26.81$
 $\Delta = 5^{\circ} 41' 24''$

$L = 26.81$
 $\Delta = 5^{\circ} 41' 24''$

$L = 26.82$
 $\Delta = 5^{\circ} 41' 24''$

Sec #2 $\Delta 11^{\circ} 22' 44''$

Sec #3 $\Delta 17^{\circ} 04' 12''$

Seimitar

417.48

+2	11.4	406.1
+4	8.6	408.9
"4	7.5	410.0
cl	5.3	412.2
N	2.2	415.3
N	2.8	414.7
cl	5.3	412.2
"4	7.5	410.0
+5	8.7	408.8
+8	12.9	404.6
C	12.9	404.6
14	12.4	405.1
+5	12.7	404.8
cl	15.2	402.3
S	17.4	400.1
S	18.3	399.2
cl	16.5	401.0
+5	13.5	404.0
"4	13.3	404.2
2	14.0	403.5
+3	14.5	403.0
+6	9.4	408.1
"4	9.0	408.5
cl	6.8	410.7
N	4.9	412.6

Sec #4 $\Delta 22^{\circ} 45' 36''$

$L = 26.82$
 $\Delta = 5^{\circ} 41' 24''$

$L = 26.54$

Sec #5 $\Delta 28^{\circ} 27' = P.R.C. \text{ Bet Curves } 84.9$

417.44
 CURVE #8 Δ 45°-04' divided into 8 Parts Δ 5°-38'
 Sec #1 Δ 5°-38'

407.34

Scimitar

OK

$R=270'$

$L=26.54'$
 $\Delta=5^{\circ}38'$

Sec #2 $\Delta=11^{\circ}16'$

$L=26.54'$
 $\Delta=5^{\circ}38'$

Sec #3 $\Delta=16.54'$

$L=26.54'$
 $\Delta=5^{\circ}38'$

N	6.7	410.8
cb	8.8	408.7
1/4	11.4	406.1
+5	15.4	402.1
c	14.8	402.7
1/4	14.9	402.6
+4	12.0	400.5
cb	18.0	399.5
S	20.6	396.9
Sec #2 $\Delta=11^{\circ}16'$		
S	21.1	396.4
cb	19.3	398.2
+7	18.2	399.3
1/4	15.5	402.0
c	16.0	401.5
+7	17.4	400.1
1/4	12.1	405.4
cb	10.0	407.5
N	7.2	410.3
Sec #3 $\Delta=16.54'$		
N	9.7	407.8
cb	12.0	405.5
T.P.	2.18	405.16
1/4	3.2	404.1
+3	7.7	399.6
c	6.9	408.6

1/4	6.1	401.2
+3	8.0	399.3
cb	9.2	398.1
S	11.5	395.9
Sec #4 $\Delta=22^{\circ}32'$		
S	13.8	393.5
cb	11.7	395.6
1/4	10.5	396.9
+3	8.0	399.3
c	8.3	399.0
1/4	9.3	398.0
+5	3.7	403.6
cb	2.3	405.0
N	0.0	407.3
Sec #5 $\Delta=28^{\circ}10'$		
N	2.0	406.3
cb	4.8	402.5
+8	8.7	398.6
1/4	10.4	396.9
c	9.6	397.7
+8	9.2	398.1
1/4	10.6	396.7
cb	12.0	395.3
S	14.0	393.3

407.34
Sec #6 $\Delta 33^{\circ} 48'$

S	15.7	391.6
cl	14.0	393.3
"4	12.3	395.0
+3	10.3	397.0
e	10.6	396.7
+8	11.3	396.8
"4	7.7	399.6
cl	5.6	401.7
N	3.5	403.8

L = 26.55'

Sec #7 $\Delta 39^{\circ} 26'$

N	3.8	403.5
cl	5.4	401.9
"4	7.4	399.9
+5	12.0	395.3
e	11.7	395.6
"4	11.5	395.8
+2	13.0	394.3
cl	14.7	392.6
S	17.0	390.3

L = 26.55'

Sec #8 $\Delta 45^{\circ} 04' = P.R.C. \text{ Bet Curves } \# 847$

S	18.5	388.8
cl	15.6	391.7
+8	13.9	393.4
"4	12.8	394.5
e	12.5	394.8
+5	12.7	394.6

L = 36.79'

$\Delta = 10^{\circ} 02' 15''$

407.34

Seimitar

10

"4	9.6	397.7
cl	6.7	400.6
N	4.7	402.6

Portion of Curve #7 Bet above P.R.C. & Radial Line from N.E. Cor.

Winnett & Seimitar $\Delta 40^{\circ} 09'$ & R 210 divided into 4 parts

Sec # $\Delta 10^{\circ} 02' 15''$

N	5.7	401.6
cl	8.6	398.7
"4	10.6	396.7
+3	11.1	396.2
+6	14.3	393.0
e	14.2	393.1
"4	14.3	393.0
+4	14.2	393.1
+7	16.4	390.9
cl	17.1	390.2
S	19.4	387.9

L = 36.79'

$\Delta = 10^{\circ} 02' 15''$

Sec #2 $\Delta 20^{\circ} 04' 30''$

S	20.5	386.8
cl	18.3	389.0
+5	15.8	391.5
"4	16.0	391.3
e	16.1	391.2
+2	16.5	390.8
+5	12.8	394.5
"4	12.2	395.1

L = 36.79'

$\Delta = 10^{\circ} 02' 15''$

407.34
see 2. con

cb		10.6	396.7
N		8.8	398.5
	see #3	$\Delta 30^\circ 04' - 45'$	
N		11.6	395.7
cb		13.1	394.2
T.P.	1.42	396.47	12.29 395.05
"4		4.2	392.3
+7		5.2	391.3
e		6.5	390.0
"4		6.7	389.8
+5		6.7	389.8
+8		8.5	388.0
cb		8.8	387.7
5		10.0	386.5
	see #4	$\Delta 40^\circ 09' =$ Radial Line from N.E. Cor. Winnetka Scimitar	
5		11.3	385.2
cb		9.7	386.8
+2		9.5	387.0
+5		7.0	389.5
"4		7.0	389.5
e		6.9	389.5
+5		6.7	389.8
"4		4.9	391.6
cb		4.0	392.5
N		3.0	393.5

$\Delta L = 36.70'$
 $\Delta 40^\circ 02' 15''$

$\Delta L = 26.76'$
 $\Delta = 70' 18''$

396.47
 $\Delta 47^\circ 27' =$ Winnet on Radial Line

N.		4.1	392.4
cb		5.9	390.6
"4		6.6	389.9
e		7.1	389.4
"4		7.3	389.2
+4		7.2	389.3
cb		10.2	386.3
5		11.9	384.6
		$\Delta 54^\circ 45' =$ Radial Line from N.W. Cor. Winnetka Scimitar	
5		11.9	384.6
cb		10.1	386.4
+3		9.8	386.7
+7		7.4	389.1
"4		7.6	388.9
e		7.4	389.1
"4		6.6	389.9
cb		5.4	391.1
N		3.6	392.9
T.P. on B.M.		3.35	393.12 + Winnetka

Curve #6 from W. Line of Winnet to P.T.
 $\Delta 82^\circ 58'$ divided into 10 parts.
 Sec #1, AB-18 All sections on Radial Line
 429 397.41 393.12

$\Delta C = 210$

N		A.1	393.3
+2		4.3	393.1
cb		6.6	390.8
"4		7.9	389.5

$\Delta L = 26.76'$
 $\Delta 47^\circ 27'$

$\Delta L = 28' 58.60''$

$\Delta L = 24.08'$
 $\Delta 82^\circ 58'$

397.41

Sec #1 (Cont.)

KR=210

 $\phi L = 30.42'$ $\Delta = 8^{\circ}18'$

C	8.3	389.1
1/4	5.6	388.8
+3	5.6	388.8
Cl	10.4	387.0
S	12.2	385.2

Sec #2 $\Delta 16^{\circ}36'$ $\phi L = 30.42'$ $\Delta = 8^{\circ}18'$

S	11.5	385.9
Cl	9.7	387.7
+7	8.1	389.3
1/4	8.1	389.3
C	8.0	389.4
+5	8.0	389.4
1/4	6.6	390.8
Cl	5.1	392.0
+8	4.2	393.2
N	3.3	394.1

Sec #3 $\Delta 24^{\circ}54'$ $\phi L = 30.42'$ $\Delta = 8^{\circ}18'$

N	2.6	394.8
Cl	3.7	393.7
1/4	5.6	391.8
+5	7.4	390.0
C	7.5	389.9
1/4	7.4	390.0
+2	7.3	390.1
+5	9.0	388.4
Cl	7.3	388.1
S	10.4	387.0

Scimitar

12

397.41

Sec #4 $\Delta 33^{\circ}12'$ $\phi L = 30.36'$ $\Delta = 8^{\circ}17'$

S	9.6	386.8
Cl	7.5	389.9
+5	7.1	390.3
+5	5.3	392.1
1/4	5.4	392.0
C	5.3	392.1
+5	5.5	391.9
1/4	3.7	393.7
Cl	2.2	395.2
N	1.2	396.2

Sec #5 $\Delta 41^{\circ}29'$ $\phi L = 30.42'$ $\Delta = 8^{\circ}18'$

N	0.0	397.4
Cl	0.4	397.0
1/4	2.8	394.6
C	3.3	394.2
1/4	3.1	394.3
+2	3.0	394.4
+5	4.6	392.8
Cl	5.0	392.4
S	7.1	390.3

Sec #6 $\Delta 49^{\circ}47'$ $\phi L = 30.42'$ $\Delta = 8^{\circ}18'$

S	4.9	392.5
Cl	3.0	394.4
+5	2.7	394.7
+8	1.5	395.9
1/4	1.4	396.0
C	1.5	395.9

397.41
Sec #6 Cont.

1/4		0.1	397.3
T.P.	11.09	408.04	0.46 396.95
Ch		8.5	399.5
N		7.6	400.4
Sec #7 $\Delta 58^{\circ} 05'$			
N		5.6	402.4
Ch		6.1	401.9
+7		8.9	399.1
1/4		9.2	398.8
C		10.0	398.0
1/4		10.4	397.6
Ch		12.0	396.0
3		13.6	394.4
Sec #8 $\Delta 66^{\circ} 23'$			
5		11.7	396.2
+3		10.4	397.6
Ch		9.7	398.3
1/4		8.5	399.5
C		7.9	400.1
1/4		6.9	401.1
Ch		5.1	402.6
N		3.9	404.1
Sec #9 $\Delta 74^{\circ} 41'$			
N		2.1	405.9
+4		2.3	405.7
+6		3.6	404.4
Ch		4.1	403.9

$\phi L = 30.42'$
 $\Delta 8^{\circ} 18'$
 $\phi L = 30.42'$
 $\Delta 8^{\circ} 18'$

108.04
Sec #9 Cont.

similar

13

1/4		3.0	4030
C		6.7	4013
1/4		7.0	4010
+6		6.8	4012
Ch		8.3	3997
+5		9.5	3985
5		10.1	3979
Sec #10 P.T. $\Delta 82^{\circ} 58'$			
5		7.7	3983
Ch		7.6	4004
+5		5.5	4035
1/4		6.0	4020
C		5.6	4024
1/4		4.3	4037
Ch		3.2	4048
+5		2.3	4057
+7		1.0	4070
N		0.9	4071

$\phi L = 30.36'$
 $\Delta 8^{\circ} 19'$

T.P. on hub N.W. P.T.

0.94

407.10 Elev. hub

X-section of Tangent between Curve #6 + #5 beginning at N. end of tangent.

0100

5.15

415.28

40710

W		8.2	
+3		8.3	same as above
+5		9.6	
Ch		10.5	

415.28
0+00 Cont

1/4	11.6	
C	12.9	
1/4	13.0	
+5	12.8	
Ch	14.9	
E	17.0	

same as E.C.

0+25 S

E	15.6	399.7
Ch	13.5	401.5
+5	11.8	403.5
1/4	12.4	402.9
C	11.6	403.7
1/4	10.5	404.8
Ch	9.2	406.1
W	8.2	407.1

0+30 S

W	6.6	408.7
+5	7.3	408.0
+8	9.0	406.3
Ch	9.3	406.0
1/4	10.4	404.9
C	11.4	403.9
1/4	12.0	403.3
+5	11.8	403.5
Ch	13.8	401.5
E	16.0	398.7

415.28

semitar

14

0+50 S

E	15.3	4000
Ch	13.6	4017
+6	11.3	4040
1/4	11.2	4041
C	10.9	4044
1/4	10.0	4053
+3	8.2	4071
Ch	7.1	4082
W	5.5	4098

0+70 S

W	4.0	4113 ✓
Ch	5.9	4094
1/4	7.6	4077
+6	10.4	4049
C	10.5	4048
1/4	10.3	4050
+2	10.3	4050
+6	11.9	4034
Ch	13.0	4023
E	15.1	4002

1+00 S

E	14.3	4010
Ch	11.9	4034
1/4	9.0	4063
C	9.5	4058

1+00 Cont.
415.28

+A	9.9	405.4
1/4	6.0	409.3
Cl.	4.0	411.3
W	2.8	412.6

1+30.5

W	0.6	414.7
Cl.	2.1	413.2
1/4	3.5	411.8
+5	8.5	406.8
C	8.3	407.0
1/4	8.0	407.3
+3	9.7	405.6
Cl.	11.8	403.5
E	14.0	401.3

1+70.5

E	14.0	401.3
Cl.	11.0	404.3
+A	10.1	405.2
1/4	6.6	408.7
C	6.4	408.9
+5	6.8	408.5
1/4	2.7	412.6
T.P	8.68	422.95
Cl.	7.5	415.5
W	4.8	418.2

422.95

semitar

15

2+10.5

W	2.6	420.4
Cl.	4.9	418.1
1/4	8.2	414.8
+6	12.2	410.8
C	12.1	410.9
1/4	12.1	410.9
+5	15.1	407.9
Cl.	16.2	406.8
E	19.1	403.9

2+25.5

E	18.5	404.5
Cl.	15.0	408.0
+5	14.0	409.0
1/4	11.3	411.7
C	11.2	411.8
+A	11.4	411.6
+7	7.0	416.0
1/4	6.3	416.7
Cl.	4.7	418.3
W	2.8	420.2

2+45.5

W	0.7	422.3
Cl.	3.7	419.3
1/4	6.4	416.6
+A	7.6	415.4
+7	10.3	412.7

422.95

2+45 Cont. 5

C	10.4	412.6
1/4	10.7	412.3
+3	10.8	412.2
+5	13.2	409.8
Ch	14.8	408.2
E	17.5	405.5

2+80 S

E	14.3	408.7
Ch	11.0	412.0
+3	10.6	413.4
+8	8.2	414.8
1/4	8.4	414.6
C	8.5	414.5
+3	8.7	414.3
+7	4.9	418.1
1/4	4.0	419.0
Ch	1.3	421.7
W	0.0	420.0

T.P. 11.24 430.44 3.75 419.20

3+00 S

W	5.5	424.9
Ch	7.6	422.9
1/4	10.2	420.2
+2	10.8	419.2
+6	14.4	416.0
C	14.4	416.0

430.44

Scimitar

16

3+00 Cont. 5

1/4	14.5	415.9
+2	14.5	415.9
+7	17.9	412.5
Ch	17.9	412.5
E	20.7	409.7
3+35 S		410.3

E	20.1	
Ch	18.3	412.1
1/4	12.5	417.5
C	12.2	418.2
+4	12.3	418.1
+7	8.3	422.1
1/4	7.8	422.6
Ch	6.2	424.2
W	4.3	426.1

3+55 S

W	2.4	428.0
Ch	5.0	425.4
1/4	8.0	422.4
+6	9.3	421.1
+7	11.6	418.8
C	11.7	418.7
1/4	11.6	418.8
Ch	16.2	414.2
F	19.3	411.1

130.44

3+75 S

411.4

E	19.0	
Ch	15.6	410.8
1/4	10.9	419.5
C	10.9	419.5
+8	10.6	419.8
1/4	8.0	422.4
Ch	4.5	425.9
W	2.7	427.7

4+00 S

W	4.2	426.2
Ch	6.4	426.0
+8	7.9	422.5
1/4	9.2	421.2
C	9.6	420.8
1/4	9.6	420.8
Ch	14.2	416.2
E	17.5	412.9

4+30 S

F	17.0	413.4
Ch	14.0	416.4
+5	12.6	417.8
1/4	9.2	421.2
C	8.7	421.7
1/4	8.7	421.7
+5	4.3	426.1

430.44

4+30 Cont. S

semitar

17

Ch	2.9	427.5
W	0.6	429.8

4+55 S

W	0.2	430.2
Ch	2.5	427.9
1/4	4.8	425.6
+6	8.2	422.2
C	8.1	422.3
1/4	8.3	422.1
+5	11.6	419.8
Ch	13.2	417.2
E	15.3	415.1

5+00 S

E	13.3	417.1
Ch	11.2	419.2
+2	10.8	419.6
1/4	6.9	423.5
+2	5.5	424.9
C	5.7	424.7
+6	6.2	424.2
1/4	3.5	426.9
Ch	0.5	429.9
T.P.	6.23	435.55 ✓
W	3.7	431.9

435.55

5+23325 S = Curve #5
End of Tangent P.O. #5 Curve

W	1.7	433.9
CL	4.2	431.4
1/4	6.2	429.4
+2	9.8	425.8
C	9.2	426.4
+6	8.4	427.2
1/4	11.0	424.6
CL	13.6	422.0
E	16.8	418.8
T.P.	2.92	437.25
	1.22	434.33

P.O. Curve #5

Sec #1 $\Delta 16^{\circ} 51' 50''$

E	15.5	421.8
CL	13.1	423.9
1/4	11.6	425.7
+4	9.0	428.3
C	9.3	428.0
1/4	9.6	427.7
+2	7.0	430.3
CL	5.4	421.9
W	3.7	423.6

Sec #2 $\Delta 33^{\circ} 43' 10''$

W	3.1	434.2
CL	4.5	432.8
+8	5.3	432.0
1/4	5.2	429.1

137.25
Sec #2 Cont

semitar

18

C	7.8	429.5
1/4	7.4	429.9
CL	9.0	428.3
E	10.4	426.9
E	9.4	427.9
CL	8.6	428.7
1/4	7.0	430.3
C	7.1	430.2
1/4	7.1	430.2
+2	7.0	430.3
+5	4.1	433.2
CL	3.1	434.2
W	1.5	435.8

Sec #3 $\Delta 50^{\circ} 35' 30''$

W	1.8	435.5
CL	3.4	433.9
+6	7.7	429.6
1/4	7.8	429.5
C	7.5	429.8
+5	7.7	429.6
1/4	8.5	428.8
CL	10.3	427.0
E	12.0	425.3

437.25
Sec #5 $\Delta 84^\circ-19'-10''$

S	16.1	421.2
Ch	13.3	424.0
1/4	11.7	426.6
+5	9.2	428.1
C	9.2	428.1
1/4	9.5	427.8
+3	9.4	427.9
+6	6.3	431.0
Ch	4.9	432.4
N	2.8	434.5

$L = 29.43'$
 $\Delta = 16^\circ 51' 58''$

Sec #6 $\Delta 101^\circ-11''$ P.C.C.

N	2.9	434.4
Ch	5.1	431.9
1/4	8.2	429.1
+3	10.8	426.5
C	10.6	426.7
1/4	10.9	426.4
+5	13.5	423.8
Ch	14.3	423.0
S	17.7	419.6

$L = 26.01'$
 $\Delta = 90^\circ 19''$

Sec #7 $\Delta 9^\circ-19''$ Curve #7

S	17.6	419.7
Ch	15.0	422.3
+5	11.9	425.4
1/4	11.7	425.6
C	11.7	425.6

$R = 160'$
 $L = 26.01'$
 $\Delta = 90^\circ 19''$

437.25
Sec #1 Cont.

semitar 19

+2	11.7	435.6
+7	8.2	429.1
1/4	6.9	430.4
Ch	4.5	432.8
N	2.3	435.0

Sec #2 $\Delta 18^\circ-38''$

N	3.6	433.7
Ch	6.6	420.7
1/4	9.5	427.8
C	12.3	425.0
1/4	12.5	424.8
+5	12.7	424.6
Ch	16.0	421.3
S	18.2	419.1

$L = 26.02'$
 $\Delta = 90^\circ 19''$

Sec #3 $\Delta 27^\circ-57''$

S	18.7	418.6
Ch	16.3	421.0
+2	16.3	421.0
+8	13.1	424.2
1/4	13.1	424.2
C	12.6	424.7
1/4	9.9	427.4
Ch	7.0	430.3
N	4.6	432.7

$L = 26.02'$
 $\Delta = 90^\circ 19''$

Sec #4 $\Delta 37^\circ-16''$

N	3.6	433.7
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437.25
Sec #4 Cont.

Ch	6.0	421.3
1/4	9.1	428.2
+7	12.0	425.3
C	11.9	425.4
1/4	12.3	425.0
+2	12.7	424.6
Ch	17.2	420.1
S	20.1	417.2
Sec #5 $\Delta 46^{\circ} 35'$		
S	20.0	417.3
Ch	16.2	411.1
1/4	11.3	426.0
C	10.8	426.5
+9	11.0	426.3
+5	7.2	430.1
1/4	6.8	430.5
Ch	5.1	432.7
N	2.6	434.7
Sec #6 $\Delta 55^{\circ} 34'$ P.R.C.		
N	1.8	435.5
Ch	4.1	433.2
1/4	6.8	430.5
+1	10.6	428.7
C	10.3	427.0
+8	10.4	426.9
1/4	12.2	424.5

$L = 26.02'$
 $\Delta = 8^{\circ} 19'$

$L = 26.02'$
 $\Delta = 9^{\circ} 19'$

Sec #6 $\Delta 55^{\circ} 34'$ P.R.C.

437.25
Sec #6 Cont.

Ch	15.0	422.3
S	17.6	419.7
T.P.	9.96	436.65
Curve #3 - Sec #1 $\Delta 10^{\circ} 21'$		
S	16.2	420.5
Ch	14.2	422.5
1/4	12.4	424.3
+5	9.6	427.1
C	9.7	427.0
+8	10.1	426.6
1/4	6.8	429.9
Ch	3.6	433.1
N	1.0	435.7
Sec #2 $\Delta 20^{\circ} 42'$		
N	1.2	435.5
Ch	3.9	432.8
1/4	7.1	429.6
+2	10.6	426.1
C	10.5	426.2
+6	10.3	426.4
1/4	13.2	423.5
Ch	14.3	422.4
S	17.3	419.4
Sec #3 $\Delta 31^{\circ} 03'$		
S	18.6	418.1
Ch	16.0	420.7

$L = 27.10'$
 $\Delta = 10^{\circ} 21'$

$L = 27.10'$
 $\Delta = 10^{\circ} 21'$

$L = 27.10'$
 $\Delta = 10^{\circ} 21'$

scimitar

20

436.65
Sec #3 Cont.

+5	14.9	421.8
1/4	11.2	425.5
C	11.3	426.4
+7	11.9	424.8
1/4	8.5	428.2
Ch	5.4	421.3
N	2.5	434.2

Sec #4 A 41-24

N	3.7	433.0
Ch	6.9	429.8
1/4	9.9	426.8
+2	13.2	423.5
C	12.6	424.1
+6	11.9	424.8
1/4	14.8	421.9
Ch	17.0	419.7
S	20.4	416.3

Sec #5 A 51-45

S	22.9	413.8
Ch	19.3	417.4
+5	18.2	418.5
1/4	16.0	420.7
+3	14.1	422.6
C	14.2	422.5
+7	15.0	421.7
1/4	11.3	425.4

436.65
Sec #5 Cont = 0+00

semitar

21

Ch	9.1	427.6
N	6.1	430.6
T.P. 441	428.48	12.58
	0+35 W	

N	0.1	428.4
Ch	2.1	426.4
1/4	5.0	423.5
+3	7.8	420.7

C	8.5	420.0
+8	8.9	419.6
1/4	10.7	417.8
+4	12.6	415.9
Ch	13.3	415.2
S	16.5	412.0

0+65 W

S	19.0	409.5
Ch	15.8	412.7
S	14.7	413.8
1/4	10.8	417.7

C	10.6	417.9
+6	11.0	417.5
1/4	7.4	421.1
Ch	4.5	424.0
N	1.6	426.9

0+90 W

N	2.5	426.0
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428.48
0+90 cont. W

Ch	4.6	423.9
1/4	7.3	421.2
+3	8.1	420.4
+5	12.8	415.7
C	12.2	416.3
1/4	13.0	415.5
+A	16.2	412.3
Ch	17.5	411.0
S	20.0	408.5

1+05 W

S	21.0	407.5
+6	19.2	409.3
Ch	17.6	410.9
+7	16.3	412.2
1/4	13.9	414.6
C	13.6	414.9
+5	13.7	414.8
+8	10.1	418.4
1/4	9.2	419.3
Ch	6.1	422.1
N	4.2	424.3

1+40 W

N	7.1	421.4
Ch	9.7	418.8
1/4	12.6	415.9
T.P.	1.50	417.33
	12.65	415.83

417.33
1+40 cont. W.

+2	2.0	415.3
+5	4.9	412.4
C	4.9	412.7
1/4	5.7	411.6
+3	7.9	409.4
Ch	8.8	408.5
S	11.6	405.7

1+75 W

S	13.9	403.4
Ch	11.3	406.0
+8	9.3	408.0
1/4	7.6	409.7
C	7.1	409.9
+5	7.6	409.7
+8	5.2	412.1
1/4	4.5	412.8
Ch	2.1	414.9
N	0.5	416.8

2+00 W

N	1.7	415.6
Ch	3.8	413.5
1/4	6.0	411.3
+2	6.1	410.9
+A	8.5	408.8
C	8.6	408.7
1/4	9.1	408.2

Scimitar

22

417.33

2+00 cont

+5	11.5	405.8
cb	12.3	405.0
S	13.3	404.0
2+25 W		
S	13.7	403.6
cb	12.9	404.9
+5	11.8	405.5
1/4	9.7	407.6
C	9.5	407.8
+5	10.0	407.3
+8	7.1	410.2
1/4	6.7	410.6
cb	5.0	412.3
N	2.7	414.6
2+55 W		
N	3.5	413.8
cb	5.5	411.8
1/4	7.7	409.6
+5	8.5	408.8
+6	10.7	406.6
C	10.5	406.8
1/4	10.4	406.9
+2	10.4	406.9
+5	12.0	405.3
cb	12.7	404.6
S	15.0	402.3

417.33

semitar

23

2+95 W

S	15.3	402.0	
cb	14.3	403.0	
+5	14.1	403.2	
+8	12.8	404.5	
1/4	12.7	404.6	
C	12.6	404.7	
+5	13.2	404.1	
1/4	11.6	405.7	
+5	9.8	407.5	
cb	9.2	408.1	
N	8.0	409.3	
3+15 W			
N	10.1	407.2	
cb	11.3	406.0	
+5	12.0	405.3	
+7	14.1	403.2	
1/4	14.0	403.3	
C	13.6	403.7	
1/4	14.1	403.2	
+4	14.8	402.5	
cb	15.7	401.6	
S	16.4	400.9	
T.P. 1.01	406.82	11.92	405.41
3+25 W			
S	6.3	400.5	
cb	5.6	401.2	

406.82
3+25 cont. W

1/4	4.0	402.8
C	3.9	402.9
1/4	3.6	403.2
Ch	3.5	403.3
N	1.7	405.1

3+35 W

N	1.1	405.7
Ch	2.2	404.6
+5	4.1	402.7
1/4	4.1	402.7
C	4.7	402.1
1/4	5.0	401.8
Ch	6.3	400.5
S	7.6	399.2

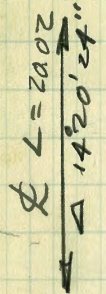
3+68 W

S	9.9	396.9
Ch	8.8	398.0
1/4	8.0	398.8
+4	8.6	398.2
C	8.0	398.8
1/4	7.3	399.5
+6	7.0	399.8
+8	5.5	401.3
Ch	5.4	401.4
+5	4.6	402.2
+6	1.6	405.2

406.82
3+68 cont

semitar 24

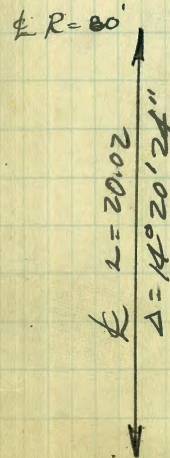
N	1.6	405.2
3+70 1/2 P.C.		4492.26
N	5.3	401.5
Ch	5.7	401.1
+8	5.8	401.0
1/4	7.2	399.6
1/4	7.4	399.4
C	8.1	398.7
+6	8.7	398.1
1/4	8.1	398.7
Ch	8.8	399.0
S	9.9	396.9



T.P. on Bench Hub P.C. 9.89 396.93 ✓
1.39 398.32 Curve #2

Sec #1 Δ 19° 20' 24"

S	2.7	395.6
Ch	1.9	396.4
+8	1.7	396.6
1/4	2.7	395.6
C	1.6	396.7
1/4	1.2	397.1
+7	1.8	396.5
Ch	0.2	398.1
N	0.0	399.3



398.32
Sec #2 Δ 28°-40'-48"

N	3.2	395.1
Ch	4.6	393.7
1/4	3.7	394.6
C	3.8	394.5
1/4	4.8	393.5
+3	5.1	393.2
+5	3.8	394.5
Ch	3.4	394.9
S	3.9	394.4

$L = 20.02$
 $\Delta = 14^{\circ}20'24''$

Sec #3 Δ 43°-01'-12"

S	5.0	393.3
Ch	5.1	393.2
+5	5.4	392.9
+7	6.8	391.5
1/4	6.4	391.9
C	6.1	392.2
1/4	6.9	392.0
Ch	6.7	391.6
N	6.9	391.4

$L = 20.02$
 $\Delta = 14^{\circ}20'24''$

Sec #4 Δ 57°-31'-46"

N	8.8	389.5
Ch	8.6	389.7
1/4	8.4	389.9
C	8.1	390.2
1/4	8.2	390.1
+5	8.6	389.7

$L = 20.26$
 $\Delta = 14^{\circ}30'34''$

398.32
Sec #4 (cont)

Ch	6.8	391.5
S	6.2	392.1
Sec #5 Δ 71°-42'		
E	7.4	390.9
Ch	8.1	390.2
+3	9.6	388.7
1/4	9.5	388.8
C	9.6	388.7
1/4	10.1	388.2
Ch	10.5	387.8
W	10.8	387.5

$L = 19.80$
 $\Delta = 14^{\circ}10'14''$

Sec #6 Δ 86°-02'-24"

W	15.7	382.6
Ch	14.2	384.1
1/4	11.9	386.4
C	10.9	387.4
1/4	10.8	387.5
+6	10.8	387.5
Ch	8.7	389.6
E	8.3	390.0

$L = 20.02$
 $\Delta = 14^{\circ}20'24''$

T.P. 131 388.61 11.02 387.30"

Sec #7 Δ 100°-22'-48"

E	0.0	388.6
Ch	0.4	388.2
+2	0.5	388.1
1/4	2.8	385.8

similar

25

388.61
Sec #7 South

386.61
Sec #10 143-24 P.C.C.

Scimitar
4+92.20

1/4	2.8	385.8
C	2.6	386.0
1/4	4.8	383.8
Ch	6.6	382.0
W	8.3	380.3
Sec #8 114-43-12		
W	8.2	380.4
Ch	8.3	380.3
1/4	6.6	382.0
C	4.6	384.0
1/4	4.5	384.1
+5	5.1	383.5
+6	2.0	386.6
Ch	1.4	387.2
E	0.3	389.3
Sec #9 129-03-36		
E	1.2	387.4
Ch	2.2	386.4
+3	3.1	385.5
+4	6.4	382.2
1/4	6.0	382.6
C	5.9	382.7
1/4	6.9	381.7
Ch	9.0	379.6
W	10.5	378.1

W	15.0	373.6
+3	13.1	375.5
Ch	11.7	376.9
1/4	8.9	379.7
C	7.6	381.0
1/4	7.8	380.8
+3	7.6	381.0
+5	4.7	383.9
Ch	3A	385.2
E	1.2	387.4
P.T. S.E. end. Curve #1 = Sta. 0+00		
N	3.4	385.2
Ch	4.9	383.7
+8	7.3	381.3
1/4	10.8	377.8
C	10.7	377.9
+7	11.3	377.3
1/4	13.1	375.5
Ch	15.7	372.9
S	18.0	370.6
T.P. 5.36	381.19	12.78
0+30 E		
S	12.6	368.6
Ch	10.3	370.9
1/4	7.2	374.0
C	6.6	374.6

Ar. 925
" 415

381.19

0+30 Cont. E

+8	6.6	374.6
1/4	3.5	377.7
Ch	1.5	379.7
N	0.1	381.1

0+65 E

N	2.7	378.5
+2	3.3	377.9
+5	5.1	376.1
Ch	5.8	375.4
1/4	5.4	372.8
+2	11.7	369.5
C	11.5	369.7
1/4	12.1	368.9
Ch	15.0	366.2
S	17.7	363.5

1+00 E

S	22.5	358.7
Ch	20.0	361.2
1/4	17.6	363.6
C	16.4	364.8
+8	16.9	364.3
1/4	13.7	367.5
Ch	12.2	369.0
+5	11.7	369.5
+8	8.9	372.3
N	8.1	373.1

369.60

semitar

27

1+40 E

T.P. 0.38	369.60	11.97	369.22
N		2.6	367.0
+3		6.0	363.6
Ch		6.8	362.8
1/4		7.7	361.9
C		9.6	360.0
+8		9.9	359.7
1/4		10.9	358.7
Ch		12.5	357.1
S		14.4	355.2

1+60 E

S	15.1	354.2
Ch	14.5	355.1
1/4	12.1	357.2
C	11.3	358.3
1/4	9.7	359.9
Ch	7.8	361.8
N	6.3	363.3

2+00 E

N	9.3	360.3
Ch	11.2	358.1
1/4	12.1	357.2
+5	15.0	354.6
C	14.7	354.9
1/4	15.0	354.6
+4	15.0	354.6

369.60
2+00 Cont. E

+6	16.3	356.3
Ch	16.5	353.1
S	19.0	350.6
2+30 E		
S	20.5	349.1
+5	20.1	349.2
Ch	19.3	350.3
+6	18.0	351.6
1/4	18.1	351.5
C	17.8	352.8
+5	18.3	351.3
1/4	15.3	354.3
Ch	14.9	354.7
+2	13.6	356.0
N	12.9	356.7
T.P. O.AA.	357.08	12.96 356.64
2+60 E		
N	3.3	353.8
Ch	4.6	352.5
1/4	5.6	351.5
+5	8.3	348.8
C	8.2	348.9
1/4	8.6	348.5
Ch	10.0	347.1
S	11.3	345.8

357.08
2+78 E

Soimitur

28

S	12.3	344.8
Ch	11.2	345.9
1/4	9.9	347.2
C	9.5	347.6
+6	10.0	347.1
1/4	7.2	349.9
Ch	5.2	351.9
N	4.8	352.3
2+90 E		
N	5.2	351.9
Ch	6.9	350.2
1/4	7.9	349.2
+5	10.7	346.4
C	10.6	346.5
1/4	10.7	346.4
+7	11.8	345.3
Ch	13.6	343.5
S	15.3	341.8
3+20 E		
S	16.9	340.2
Ch	16.6	340.5
+7	13.7	343.4
1/4	12.5	344.6
C	12.7	344.4
+5	12.6	344.5
1/4	10.2	346.9

35708

3+20 Cont.

Ch		8.8	348.3
N		7.3	349.8
3+55 E			
N		9.5	347.6
Ch		11.5	345.6
S		12.0	345.1
1/4		13.0	344.1
T.P.	3.62	347.63	13.07 344.01
+4		5.3	342.3
C		5.2	342.4
1/4		5.2	342.4
Ch		8.5	339.1
S		9.8	337.8
3+85 E			
S		10.5	337.1
Ch		9.6	338.0
1/4		7.4	340.2
+2		6.6	341.0
C		6.5	341.1
+7		6.2	341.4
1/4		4.3	343.3
Ch		3.0	344.6
+3		1.7	345.9
N		0.6	347.0

34763

Scimitar

4+03 92 E = N.W. Cor Scimitar + Bach 29

N		1.7	345.9
Ch		3.0	344.6
+2		4.4	343.2
1/4		5.7	341.9
+3		6.7	340.9
C		7.0	340.6
1/4		7.2	340.4
+6		9.6	338.0
Ch		9.6	338.0
+9		10.5	337.1
S		13.9	333.7
4+55 26 E			
E of Scimitar intersects with N. Rhine of Bach.			
C		8.6	339.0
1/4		7.2	340.4
Ch		4.7	342.9
N		3.0	344.6

Diagonal Line from N.E. Cor to N.W. Cor
Scimitar + Bach

E		5.0	342.6
Ch		5.4	342.2
1/4		7.0	340.6
C		8.6	339.0
1/4		9.5	338.1
Ch		10.1	337.5
+15		12.0	335.6
W		13.9	333.7 B.M. 337.73
T.P. on Bench 63 E + Bach		9.91	337.72

60' wide
10' C6's.
10' 1/2's

Attix St X Section.
Klauber to Radio Drive.

1-6-28
Northern
Semmermeyer 30
Matoon.

0+00

0.65

409.05

Nail in pole
408.37 E. Line. Klauber

W	6.1	403.0
Cl	6.2	402.9
+6	6.3	402.9
+7	7.5	401.6
1/4	7.3	401.8
C	7.0	402.1
1/4	7.8	401.3
+7	8.2	400.9
Cl	6.8	401.3
F	6.5	401.6

Plotted 3-9-28
C.B.H.

0+30 N. of N. Line of Klauber

F	9.3	399.8
Cl	9.2	399.9
+2	9.2	399.9
+3	11.8	397.3
1/4	11.2	397.9
C	11.0	398.1
1/4	11.6	397.5
+1	9.7	399.4
Cl	9.1	400.0
W	8.5	400.6

T.P. 0.41 396.91 12.55 396.50

0+70 N

W	2.5	394.4
Cl	2.9	394.0

396.91

0+70 cont

1/4	3.1	393.8
+1	5.5	391.4
C	5.3	391.6
1/4	5.3	391.6
+8	5.5	391.4
CB	2.6	394.3
E	2.7	394.2

0+90 N

E	6.4	390.5
CB	6.9	390.0
+1	8.9	388.0
1/4	8.5	388.4
C	8.5	388.4
+8	8.2	388.7
1/4	3.9	393.0
CB	3.9	393.0
W	4.1	392.8

1+05 N

W	5.5	391.4
CB	6.8	390.1
1/4	8.9	388.0
+2	8.9	388.0
+3	11.0	385.9
C	11.6	385.3
1/4	11.6	385.3
+8	12.2	384.7

396.91

1+05 cont

A+11x

37

CB		10.6	386.3	
E		10.6	386.3	
T.P.	0.01	384.32	12.60	384.315

1+40 N

E		4.6	379.7
CB		4.2	380.1
+1		6.2	388.1
1/4		5.6	378.7
C		6.0	378.3
+7		6.1	378.2
+8		3.7	380.6
1/4		3.6	380.7
CB		2.5	381.8
W		1.0	383.3

1+58 N

W		4.4	379.9
CB		5.5	378.8
1/4		6.9	377.4
+2		6.8	377.5
+3		9.8	374.5
C		9.4	374.9
1/4		9.3	375.0
+8		10.0	374.3
CB		9.0	375.3
E		8.9	375.4

384.32

1+72 N

E		12.0	372.3	
Ch		12.0	372.2	
+2		12.1	371.9	
1/4		11.9	372.4	
C		12.0	372.3	
+6		12.4	371.9	
+7		10.8	373.5	
1/4		10.3	374.0	
Ch		10.0	374.3	
W		9.6	374.7	
T.P.	0.35	372.28 [✓]	12.39	371.93 [✓]
2+00 N				
W		3.7	368.6	
Ch		4.7	367.6	
1/4		6.0	366.3	
+5		6.9	365.4	
C		6.1	366.2	
1/4		5.9	366.4	
Ch		6.2	366.1	
E		6.1	366.2	
2+25				
E		10.0	362.3	
Ch		10.3	362.0	
+		11.5	360.8	
1/4		10.6	361.7	
C		10.7	361.6	

372.28

2+25 Cont.

A+ix

38

+5		11.6	360.7	
1/4		10.5	361.8	
Ch		9.4	362.9	
W		7.9	364.4	
T.P.	0.21	359.42 [✓]	13.07	359.21 [✓]
2+50 N				
W		1.8	357.6	
Ch		2.4	357.0	
1/4		2.3	357.1	
+5		3.5	355.9	
C		2.4	357.0	
1/4		2.2	357.2	
+8		2.7	356.7	
Ch		1.8	357.6	
E		1.5	357.9	
2+75 ² N = S. Line of East Drive.				
E		6.4	353.0	
+6		7.1	352.3	
Ch		8.0	351.4	
1/4		7.3	352.1	
C		7.4	352.0	
+5		8.6	350.8	
1/4		7.2	352.2	
Ch		8.1	351.3	
W		7.6	351.8	

359.42

3+00⁸ = E of East Drive

W	11.5	347.9
Ch	11.5	347.9
1/4	10.9	348.5
+5	12.3	347.1
C	11.3	348.1
1/4	10.7	348.7
+8	11.3	348.1
Ch	10.6	348.8
E	10.3	349.1

3+23⁴ N = N. Line of East Drive

E	13.5	345.9
Ch	13.8	345.6
+3	14.7	344.7
1/4	14.0	345.4
C	14.3	345.1
1/4	14.7	344.7
Ch	14.0	345.4
W	14.1	345.3

T.P. 0.24 347.20 12.46 346.96

3+40 N

W	5.0	342.2
Ch	5.1	342.1
1/4	4.3	342.9
C	3.7	343.5
1/4	3.3	343.9
Ch	3.5	343.4

347.20

3+40 cont.

E	3.9	343.9
3+50 N		
E	3.9	343.3
Ch	3.9	343.3
+2	4.5	342.7
C	4.0	343.2
1/4	4.5	342.7
+5	6.5	340.7
1/4	6.5	340.7
Ch	7.6	339.6
W	8.6	338.6

3+75 N

W	8.6	338.6
Ch	7.8	339.4
1/4	7.1	340.1
+5	6.5	340.7
C	5.2	342.0
+5	5.6	341.6
1/4	5.3	341.9
+8	5.0	342.2
Ch	4.1	343.1
E	4.2	343.0

383.6 N on W = S. Line Radio Drive on diagonal

E	4.3	342.9
Ch	4.2	343.0
+2	5.0	342.2

Atlix

33

347.20

3+536 Cont

60' Wide
10' Cbs.
10' 1/4sOrange St. X Section
Springfield
Winnet to Paradise1-7-28
Northern 3A
Sommermeyer
Metoon0+00 = E. line of WinnetB.M. on hub NE.
330.56 Cor Winnet
Orange

1/4	5.2	342.0
C	5.9	341.3
+4	5.5	341.7
1/4	6.5	340.7
+5	8.3	338.9
Ch	8.1	339.1
W	8.3	338.9
T.P. on hub SECor. Attix + Radio	4.43	342.77

11.36

341.92

N	11.1	330.8
+7	12.2	329.7
Ch	13.7	328.2
1/4	14.4	327.5
C	15.3	326.6
+7	15.4	326.5
+7	14.1	327.8
1/4	14.7	327.2
Ch	15.6	326.3
S	16.3	325.6

Plotted 9-7-20
C.B.H.

0+10 E

S	15.0	326.9
Ch	13.8	328.1
1/4	13.0	328.9
+5	12.4	329.5
R	12.6	329.3
1/4	12.2	329.7
+6	12.4	329.5
+7	10.4	331.5
Ch	10.1	331.8
N	9.2	332.7

0+50 E

N	1.9	340.0
Ch	3.1	338.8
+4	3.4	338.5

341.92
0.50 Cont.

+5		4.4	337.5	
1/4		1.4	337.5	
C		1.7	337.2	
1/4		5.5	336.4	
Ch		6.4	335.5	
S		7.3	334.6	
T.P	13.02	354.54 ✓	0.40	341.52 ✓
		1+0.0 E		
S		9.7	344.8	
Ch		8.3	346.2	
1/4		7.8	346.7	
C		7.3	347.2	
1/4		7.1	347.4	
+1		5.3	349.2	
Ch		4.9	349.6	
N		3.5	351.0	
		1+30 E		
N		0.0	354.5	
Ch		0.1	354.4	
1/4		0.6	353.9	
3		1.3	353.2	
4		2.5	352.0	
C		2.2	352.3	
1/4		3.0	351.5	
Ch		4.1	350.4	
S		5.4	349.1	

354.54
~~1+65~~
0.65

Orange 35

T.P	12.91	367.31	0.14	354.40
S			13.4	353.9
Ch			12.1	355.2
1/4			11.1	356.2
C			10.9	356.7
+2			9.3	358.0
1/4			8.3	359.0
Ch			6.8	360.6
N			3.2	364.1
		2+00 E		
N			1.5	365.8
Ch			3.5	363.8
1/4			5.2	362.1
+8			6.0	361.3
C			7.9	359.4
1/4			8.2	359.1
Ch			8.8	358.5
S			10.3	357.0
		2+35 E		
S			9.5	357.8
+5			8.0	359.3
Ch			7.5	359.8
1/4			7.5	359.8
+2			7.3	360.0
3			5.7	361.6
C			4.7	362.6

367.31
2+35 cont

1/4		3.0	364.3
Ch		1.7	365.6
N		0.0	367.3
T.P.	9.86	368.66	8.51 358.80

2+70 F

N		1.2	367.5
Ch		4.5	364.2
1/4		5.9	362.8
C		7.5	361.2
+9		8.6	360.1
1/4		10.5	358.2
Ch		10.7	358.0
+8		12.0	356.7
S		13.0	355.7 355.7

3+00 F

S		16.1	352.6
Ch		14.4	354.3
1/4		14.1	354.6
+3		12.2	356.5
C		10.1	358.6
1/4		7.2	361.5
Ch		4.7	364.0
N		2.6	366.1

3+35 F

N		10.6	358.1
Ch		12.6	356.1

368.46

Orange

36

3+35 cont.

T.P.	0.07	356.77	12.36	356.30
1/4			2.6	354.2
C			3.9	352.9
+5			4.5	352.3
+6			6.4	350.4
1/4			6.4	350.4
+7			6.9	349.9
Ch			8.0	348.8
S			9.4	347.4

3+65 F

S			15.5	341.3
Ch			13.7	343.1
+5			13.2	343.6
1/4			11.5	345.3
+9			11.2	345.6
C			9.6	347.2
1/4			8.0	348.8
Ch			6.8	350.0
N			4.5	352.3

4+00 F

N			11.3	345.5
Ch			13.2	343.6
T.P.	0.76	344.73	12.80	343.97
1/4			2.7	342.0
+2			4.3	340.4
C			4.6	340.1

4+00 Cont.

+5	4.8	339.9
1/4	6.6	338.1
Ch	8.3	336.4
S	9.6	335.1

4+20 F

S	12.3	332.4
Ch	11.0	333.7
1/4	9.4	335.3
C	8.2	336.5
+5	6.5	338.2
1/4	6.1	338.6
+5	5.8	338.9
+7	4.6	340.1
Ch	4.2	340.5
N	3.2	341.5

4+35 E = W.P. Line Roosevelt or Oriole

60' W. of
10' Ch
10' 1/4

N	5.2	339.5
+2	6.0	338.7
Ch	6.5	338.2
+5	8.2	336.5
1/4	9.6	335.1
C	10.0	334.7
1/4	11.6	333.1
Ch	13.5	331.2
S	14.8	329.9

W. Ch

S	15.9	328.8
Ch	15.0	329.7
1/4	13.0	331.7
C	11.3	333.4
1/4	10.0	334.7
Ch	8.9	335.8
N	6.2	338.5

T.P. 0.36 336.50 8.59 336.14

W 1/4

N	0.4	336.1
Ch	1.9	334.6
1/4	3.2	333.3
C	4.5	332.0
1/4	6.0	330.5
Ch	7.6	328.9
S	9.1	327.4

Center Line of Roosevelt

S	10.5	326.0
Ch	8.9	327.6
1/4	7.1	329.4
C	5.5	331.0
1/4	4.3	332.2
Ch	3.1	333.4
N	1.3	335.2

E 1/4

2.9 333.6

1/4 Cont.

cb	4.4	332.1
1/4	5.7	330.8
C	7.1	329.4
1/4	8.5	328.0
cb	10.3	326.2
S	12.0	324.5
E cb.		
S	14.3	322.2
cb	12.0	324.5
1/4	10.5	326.0
C	8.3	328.2
1/4	6.5	330.0
cb	4.8	331.7
N	3.6	332.9
<u>E.P. Line Roosevelt or Oriole = 0.00</u>		
N	4.6	331.9
cb	6.0	330.5
1/4	8.0	329.5
C	9.6	326.9
1/4	12.0	324.5
cb	14.5	322.0
S	14.7	321.8
T.P. on B.M. SW. Cor. Orange - Roosevelt	6.64	329.86 ✓

66.88 336.74

15' E.

S	14.9	321.8
cb	14.3	322.4
1/4	13.8	322.9
C	11.8	324.9
1/4	9.7	327.0
cb	7.5	329.2
N	6.3	330.4
40' E		
N	10.7	326.0
cb	11.4	324.9
1/4	12.8	323.9
C	12.8	323.9
1/4	13.4	323.3
cb	13.5	323.2
S	10.7	326.0 326.7
50' E		
S	7.6	329.1
cb	8.9	327.8
1/4	10.7	326.0
C	11.6	325.1
1/4	12.1	324.6
cb	12.1	324.6
N	12.1	324.6
75' E		
N	8.2	328.5
cb	7.8	328.9

336.74

75' E. (COM)

1/4	7.8	328.9
E	6.7	330.0
1/4	5.3	331.4
cl	4.7	332.0
S	4.0	332.7

100' E

S	11.0	332.7
cl	10.8	331.5
1/4	0.0	336.7
E	1.3	335.4
1/4	2.0	334.7
cl	1.5	335.2
N	2.1	334.6
T.P.	12.82	349.11
	0.45	336.29

140' E

N	6.3	342.8
cl	5.9	343.2
1/4	5.3	343.8
E	4.5	344.6
1/4	3.7	345.4
cl	3.4	345.7
S	2.5	346.6
T.P.	12.94	362.02
	0.03	349.08

170' E

S	9.6	352.4
cl	10.1	351.9

362.02

Orange

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1/4	10.1	351.9
E	10.8	351.2
1/4	11.6	350.4
cl	11.7	350.3
N	12.0	350.0

200' E

N	6.5	352.5
cl	6.0	352.0
1/4	4.9	357.1
E	4.9	357.1
1/4	4.8	357.2
cl	4.6	357.4
S	4.2	357.8

225' E

S	1.2	360.8
cl	1.2	360.8
1/4	1.6	360.4
E	1.5	360.5
1/4	1.7	360.3
cl	2.0	360
N	2.0	360.0
T.P.	12.59	374.51
	0.10	361.92

250' E

N	11.8	362.7
cl	11.4	363.1
1/4	10.3	364.2

374.51

250' E. (con)

C	10.0	364.5
1/4	10.0	364.5
cl	10.6	363.9
S	10.4	364.1

275' E

S	6.8	367.7
cl	6.6	367.9
1/4	6.6	367.9
C	6.9	367.6
1/4	6.9	367.6
cl	7.5	367.0
N	8.0	366.5

300' E

N	3.5	371.0
cl	3.0	371.5
1/4	2.9	371.6
C	2.8	371.7
1/4	2.4	372.1
cl	2.2	372.3
S	2.8	371.7
T.P.	13.05	387.21
	0.35	374.16

338.8 E on N 4 350.3 E on S = $\Delta 21^\circ 44'$ ^{300'} on split

S	9.2	378.0
cl	8.7	378.5
1/4	8.3	378.9
C	8.2	379.0

387.21

Orange

40

1/4	8.5	378.7
cl	8.2	379.0
N	8.9	378.3

15' E. of Δ on N = 26' S. of Δ on S.

N	6.8	380.4
cl	5.8	381.4
1/4	5.7	381.5
C	5.2	382.0
1/4	5.0	382.2
cl	5.0	382.2
S	5.4	381.8

37' E. of N + 48.5' on S.

S	1.6	385.6
cl	1.0	386.2
1/4	0.8	386.4
C	1.0	386.2
1/4	1.0	386.2
cl	1.4	385.8
N	2.2	385.0
T.P.	12.92	399.60
	0.53	386.68

48' E. of Δ on N + 45.95' on S.

N	13.6	386.0
cl	11.9	387.7
1/4	10.6	389.0
C	10.2	389.4
1/4	10.0	389.6

399.60

48' E. (0.0H)

cl	10.4	389.2
S	12.2	387.4
50' E. of A on N. +61.5 = S		
S	11.8	387.8
cl	10.1	389.5
"4	9.6	390.0
E	9.7	389.9
"4	10.3	389.3
cl	11.7	387.9
+5	12.5	387.1
N.	11.8	387.8

65' E. of H N. +76.5 = S

N	7.6	392.0
cl	6.1	393.5
+7	6.1	393.5
"4	7.3	392.3
E	6.7	392.9
"4	6.2	393.4
cl	6.4	393.2
S	7.7	391.9

80' E. of H N. +91.5 = S

S	5.1	394.5
cl	3.3	396.3
"4	3.3	396.3
E	3.6	396.0
"4	2.8	396.8

399.60

orange

41

cl	2.5	397.1
N.	3.3	396.3
T.P.	12.95	412.30
194.24 E. of A on N = W. line		
set B.M. on Hub. N. 14155 = on S.		
cl	11.02	401.28
cl	10.9	401.4
"4	11.0	401.3
E	11.3	401.0
"4	11.2	401.1
cl	12.3	400.3
S	14.3	398.0

W. cl.

S	13.3	399.0
cl	10.9	401.4
"4	10.3	402.0
E	10.1	402.2
"4	10.4	401.9
cl	9.7	402.6
N	9.7	402.6

W. "4

N	8.3	404.0
cl	8.3	404.0
+3	9.3	403.0
"4	9.7	402.6
E	9.4	402.9
"4	9.5	402.8

Washington } 64.61 wide } Sectional
 Swan } 10.77 } 90% orange

#12.30

cl	10.8	401.5
S	12.5	399.8
E Swan		
S	11.8	400.5
cl	10.4	401.9
"4	9.1	403.2
E	8.9	403.4
"4	8.9	403.4
+4	8.7	403.6
cl	7.4	404.9
N	7.4	404.9
E. "4		
N	6.6	405.7
cl	6.9	405.4
+3	7.4	404.9
"4	7.9	404.4
E	8.3	404.0
"4	8.6	403.7
cl	9.8	402.5
S	11.4	400.9
E. cl		
S	10.6	401.7
cl	8.9	403.4
"4	8.2	404.1
E	8.1	404.2
"4	7.5	404.7

#12.30

Orange

42

+6	7.0	405.3
+7	6.2	406.1
cl	6.0	406.3
N	6.0	406.3
<u>00 = E. Line Swan.</u>		
N	5.3	407.0
cl	5.4	406.9
+3	6.4	405.9
"4	7.0	405.3
E	7.4	404.9
"4	7.7	404.6
cl	8.7	403.6
S	10.4	401.9
20'E		
S	8.2	404.1
cl	7.0	405.3
"4	6.5	405.8
E	6.6	405.7
"4	6.2	406.1
+8	5.2	407.1
cl	4.4	407.9
N	4.2	408.1
50'E		
N	3.1	409.2
cl	3.2	409.1
+4	3.5	408.8

4/2.30

50'E. (con)

t5	4.9	4074
114	5.0	407.3
e	5.1	407.2
114	6.1	406.2
cl	6.7	405.6
S	7.6	404.7

75'E.

S	8.5	403.8
cl	7.4	404.9
114	6.1	406.2
e	4.9	407.4
114	4.6	407.7
+3	4.4	407.9
+5	3.2	408.1
cl	2.7	409.6
N	2.2	410.1

100'E

N	1.9	410.4
cl	2.9	409.4
+5	3.2	409.1
+4	4.5	407.8
114	4.9	407.4
e	5.1	407.2
114	6.5	405.8
cl	7.5	404.8
S	9.0	403.3

4/2.30

Orange

43

140'E.

S	12.8	399.5
cl	10.7	401.6
114	18.5	403.8
e	6.8	405.5
114	6.3	406.0
+3	6.3	406.0
+5	4.8	407.5
cl	4.0	408.3
N	2.5	409.8

170'E.

N	4.8	407.5		
cl	7.0	405.3		
+3	7.2	405.1		
+5	9.3	403.0		
114	9.4	402.9		
+4	9.4	402.9		
e	11.7	400.6		
114	14.1	398.2		
cl	15.6	396.7		
S	17.0	395.3		
T.P.	3.25	406.09	9.46	402.84

200'E.

S	13.3	392.8
cl	12.1	394.0
114	11.1	395.0
e	9.2	396.9

406.09

200' E. (con)

14	5.8	400.3
cl	5.4	400.7
+2	3.0	403.1
N	1.8	404.3

240' E

N.	3.7	402.4
+8	6.0	400.1
cl	8.0	398.1
14	8.4	397.7
e	11.6	394.5
14	14.0	392.1
cl	16.4	389.7
S	18.4	387.7

270' E

S	19.0	387.1
cl	16.7	389.4
14	13.8	392.3
e	12.0	394.1
14	8.6	397.5
cl	8.4	397.7
+2	7.1	399.0
N	5.0	401.1

300' E

N.	1.9	404.2
cl	4.9	401.2
+1	7.3	398.8

406.09

Orange

44

14	7.5	398.6
e	9.6	396.5
14	12.8	393.3
cl	15.1	391.0
S	17.6	388.5

330' E

S	14.8	391.3
cl	11.4	394.7
14	8.6	398.2
e	5.7	400.4
+5	4.5	401.6
14	4.3	401.8
+5	5.3	400.8

T.P. 13.01 419.04 0.06 406.03 ✓

+8	13.7	405.3
cl	13.1	405.9
N	10.2	408.8

360' E

N	6.4	412.6
cl	9.4	409.6
+2	10.0	409.0
+4	13.5	405.5
14	13.1	405.9
+7	13.2	405.8
e	14.4	404.6
14	14.7	402.3

419.04

360' E. (EON)

cb 19.7 399.3

S 22.0 397.0

375' E

S 19.0 400.0

cb 16.4 402.6

114 12.1 406.9

14 10.2 408.8

c 9.8 409.5

14 9.4 409.2

16 9.3 409.7

cb 7.3 411.7

N 4.9 414.1

395' E

N 0.0 419.0

cb 3.2 415.8

14 6.9 412.1

14 8.0 411.0

c 8.2 400.8

14 9.7 409.3

cb 11.1 407.9

S 13.0 406.0

415' E.

S 11.2 407.8

cb 8.6 410.4

14 7.2 411.9

c 6.9 412.1

419.04

Orange

45

14 6.9 412.1

15 4.6 414.4

14 3.7 415.3

cb 1.3 417.7

T.P. 12.60 431.60 0.04 419.00 ✓

N 10.5 421.1

429' E.

N 7.7 423.9

cb 11.7 419.9

14 13.0 417.4

18 15.6 416.0

c 18.0 413.6

14 17.7 413.9

cb 18.4 413.2

S 18.7 412.9

445' E

S 15.5 416.1

cb 14.2 417.4

14 15.1 416.5

19 15.0 416.6

c 11.5 420.1

14 9.9 421.7

cb 8.2 423.4

N 5.4 426.2

431.60
465'E.

N.	3.2	428.4
cl	4.5	427.1
"4	6.1	425.5
C	6.1	425.5
+2	9.6	422.0
"4	11.0	420.6
cl	9.6	422.0
S	12.7	418.9

485'E

S	9.5	422.1
+4	7.2	424.4
cl	6.1	425.5
+7	7.8	423.8
"4	7.5	424.1
+9	7.2	424.4
C	3.3	429.3

T.P.	13.01	443.73	0.88	430.72
+6			15.3	416.3 428.4
"4			12.9	418.7 30.8
cl			13.1	418.5 30.6
+5			13.0	418.6 30.7
N			9.7	421.9 434.0

500'E

N	5.6	426.0 438.1
cl	7.6	424.8 36.1
"4	9.9	421.7 33.8

443.73

Orange

46

C	12.4	419.5 431.3
+2	12.8	413.8 25.9
"4	17.4	414.2 26.3
+3	17.6	414.0 26.1
+7	14.5	417.1 29.2
cl	14.8	416.8 28.9
S	20.3	411.3 423.4

520'E

S	15.5	416.1 428.2
cl	12.6	419.0 31.1
+5	13.5	418.1 30.2
"4	13.6	418.0 30.1
+7	13.8	417.8 29.9
C	8.2	423.4 435.5
"4	6.0	425.6 37.7
cl	3.3	45.83 40.4
N	0.4	420.2 443.3

T.P.	8.54	450.63	1.64	442.09
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550'E

N	1.6	449.0
cl	5.2	444.6
"4	9.0	441.6
C	11.5	439.1
+5	12.6	438.0
+7	16.5	435.5
"4	16.5	435.5

450.63

550'E. (con)

cb 16.3 4343

S 19.5 4311

600'E.

S 17.7 432.9

+3 15.2 435.4

cb 15.0 435.6

"4 15.0 435.6

+2 15.0 435.6

+4 12.8 4378

c 11.3 4393

"4 8.4 4422

cb 4.1 4465

N 1.7 4489

630'E

N 4.3 4463

cb 7.2 443.4

"4 10.4 440.2

c 12.9 4377

+6 13.8 4368

+7 15.5 435.1

"4 15.5 435.1

cb 15.9 434.7

S 17.5 433.1

660'E.

S 20.7 429.9

cb 19.0 431.6

450.63

Orange

47

"4 16.8 4338

+7 16.0 4346

c 15.4 435.2

"4 13.4 4372

cb 11.6 4390

N 9.2 4414

670'E

N 11.3 4393

cb 13.0 4376

T.P. 0.62 438.48 12.77 437.86

"4 2.5 4360

+6 3.4 4351

c 5.1 4334

"4 5.0 4335

cb 7.0 4315

S 8.9 4296

700'E

S 9.7 ~~429.8~~ 428.8

cb 8.1 4304

"4 6.9 4316

c 5.5 433.0

"4 5.5 4330

+5 5.5 4335

+7 3.3 435.2

cb 3.0 435.5

N 1.8 436.7

438.48

730'E

N	4.4	434.1
cb	4.4	434.1
"4	5.8	432.7
c	7.3	431.2
"4	8.8	429.7
cb	10.8	427.7
S	12.6	425.9

751'E on N.W. Line Paradise on diagonal

S	14.8	423.7
cb	12.8	425.7
"4	10.6	427.9
c	8.9	429.6
"4	7.2	431.3
cb	5.5	433.0

751
6.59
757.69 on S.W. L.

set BM. N Hub

4.74 433.74

N.M. Cor Orange
+ Paradise

00 = E. Line Paradise

N	1.0	437.5
cb	1.9	436.6
"4	3.2	435.3
c	3.7	434.8
"4	3.8	434.7
cb	4.0	434.5
S	5.3	433.2

50'E.

S	6.8	431.7
cb	6.0	432.5

438.48

Orange

48

"4	5.8	432.7
c	5.3	433.2
"4	4.8	433.7
cb	4.3	434.2
N	3.8	434.7

100'E.

N	6.3	432.2
cb	6.6	431.9
"4	7.2	431.3
c	7.1	431.4
"4	7.5	431.0
cb	8.0	430.5
S	8.7	429.8

150'E.

S	11.0	427.5
cb	9.8	428.7
T2	10.9	427.6
"4	10.6	427.9
c	10.3	428.2
"4	10.8	427.7
cb	10.7	427.6
N	11.4	427.1
T.P.	0.59	426.19
	12.88	425.60

200'E.

N	5.4	420.8
cb	5.1	421.1

426.19

200'E. (Con)

1/4	5.1	421.1
c	4.5	421.7
1/4	4.4	421.8
1/5	4.6	421.6
1/6	3.0	423.2
cb	2.9	423.3
S	3.1	423.1

240'E.

S.	7.3	418.9
cb	7.7	418.5
1/4	7.8	418.4
1/6	9.2	417.0
1/4	9.6	416.6
c	9.6	416.6
1/4	10.2	416.0
cb	10.4	415.8
N.	10.3	415.9
T.P.	3.79	419.23
	10.75	415.44

270'E.

N	7.3	411.9
cb	6.2	413.0
1/4	5.2	414.0
c	4.3	414.9
1/4	4.6	414.6
1/5	4.5	414.7
1/2	2.7	416.5

419.23

Orange

49

cb	2.3	416.9
S	2.2	417.0

300'E.

S.	4.2	415.0
cb	5.0	414.2
1/4	5.4	413.8
c	5.2	414.0
1/2	6.8	412.4
1/4	7.8	411.4
cb	8.7	410.5
N	9.4	409.8

330'E.

N	10.9	409.3
cb	9.3	409.9
1/4	8.4	410.9
c	7.4	411.8
1/4	5.8	413.4
1/4	5.8	413.4
cb	5.8	413.4
S	5.2	414.0

370'E.

S	4.7	414.5
cb	5.3	413.9
1/4	5.4	413.8
1/5	5.6	413.6
c	7.2	412.0

419.23

370' E. (con)

14	8.1	411.1
cl	8.9	410.3
N	10.0	409.2

400' E

N	7.9	411.3
cl	7.4	411.8
14	6.6	412.6
c	5.8	413.4
+2	4.8	414.4
14	4.9	414.3
+8	5.0	414.2
cl	4.0	415.2
S	3.4	415.8

435' E

S	0.8	418.4
cl	1.2	418.0
+2	1.4	417.8
+3	3.1	416.1
14	3.0	416.8
c	2.8	416.4
14	4.0	415.2
cl	4.6	414.6
N	5.4	413.8

470' E

N	1.3	417.9
cl	0.9	418.3

419.23

Orange

50

14		00	419.2	
T.P.	12.74	431.76	0.21	419.02
c			11.6	420.2
14			11.9	419.9
+6			11.8	420.0
+7			10.1	421.7
cl			10.0	421.8
S			9.2	422.6

500' E

S		6.5	425.3
cl		6.9	424.9
+3		7.1	424.7
+4		8.1	423.7
14		8.4	423.4
c		8.2	423.6
14		8.7	423.1
cl		8.8	423.0
N		9.2	422.6

550' E

N		2.3	429.5
cl		2.0	429.8
14		2.2	429.6
c		2.3	429.5
14		2.4	429.4
cl		1.9	430.4
S		0.9	430.9

431.76

T.P.	11.44	442.70	0.50	431.26
		600'E.		
S			8.8	433.9
cb			9.0	433.7
"4			9.6	433.1
e			9.7	433.0
"4			9.4	433.3
cb			9.2	433.5
N			9.7	433.0
		650'E.		
N			7.1	435.6
cb			6.7	436.0
"4			6.8	435.9
e			7.0	435.7
"4			7.3	435.4
cb			7.0	435.7
S			6.3	436.4
		700'E.		
S			4.7	438.0
cb			4.9	437.8
"4			5.4	437.3
e			4.9	437.8
"4			4.9	437.8
cb			4.7	438.0
N			4.5	438.2

442.70

Orange

51

725'E.

N	4.2	438.5
cb	4.2	438.5
"4	3.8	438.9
e	3.8	438.1
"4	4.1	438.6
cb	4.3	438.4
S	4.0	438.7

750'E.

S	2.9	439.8
cb	3.4	439.3
"4	3.2	439.5
e	2.8	439.9
"4	2.7	440.0
cb	2.9	439.8
N	2.5	439.2

800'E.

N	2.3	440.4
cb	2.6	440.1
"4	2.1	440.6
e	1.8	440.9
"4	2.3	440.4
cb	2.5	440.2
S	2.6	440.1

815'E.

S	1.6	441.1
cb	2.3	441.4

442.70

815' E. (cont)

14	2.3	440.4
e	1.9	440.8
14	2.0	440.7
cl	1.4	441.3
N	0.5	442.2

835' E.

N	1.6	441.1
cl	1.8	440.9
14	2.1	440.6
e	1.7	441.0
14	2.0	440.7
r7	2.1	440.6
cl	1.1	441.7
S	1.4	441.3

855' E.

S	1.4	441.3
cl	1.3	441.4
+3	1.9	440.8
14	1.6	441.1
e	1.7	440.0
+8	1.7	441.0
14	0.7	442.0
cl	0.3	442.4
N	0.2	442.5

880' E.

N	1.9	440.8
cl	1.9	440.8

442.70

orange

52

14	2.0	440.7
e	1.7	441.0
14	1.9	440.8
cl	1.9	440.8
S	2.1	440.6

930' E.

S	1.0	441.7
cl	1.0	441.7
+2	1.6	441.1
14	1.1	441.6
e	1.3	441.4
14	1.9	440.8
cl	2.1	440.6
N	1.5	441.2

960' E.

N	1.6	441.1
cl	1.6	441.1
14	1.7	441.0
e	1.3	441.4
14	1.6	441.7
+7	1.3	441.4
cl	0.0	442.7
S	0.5	442.2

980' E.

S	1.7	440.0
cl	1.5	440.2

442.70

980' E. (cont)

1/4	1.3	441.4
e	1.4	441.3
1/4	1.0	441.7
cb	0.1	442.6
N	0.0	442.7

1000' E

N	0.9	441.8
cb	1.8	440.9
1/4	2.0	440.7
e	1.5	441.2
1/4	1.4	441.3
+6	1.3	441.4
cb	0.6	442.1
S	1.0	441.7

1025' E

S	1.2	441.5
cb	0.8	441.9
1/4	0.9	441.8
e	1.1	441.6
1/4	1.7	441.0
cb	1.8	441.9
N	1.7	441.0
T.P.	7.49	449.67
	0.52	442.18

1050' E

N	6.6	443.1
cb	6.1	443.6

449.67

Orange

53

1/4	6.0	443.7
+4	6.2	443.5
+5	7.4	442.3
e	7.2	442.5
1/4	7.0	442.7
+6	7.4	442.3
+7	6.4	443.3
cb	6.2	443.5
S	6.5	443.2

1070' E

S	6.1	443.6
cb	5.6	444.1
+2	5.6	444.1
+4	7.0	442.7
1/4	6.4	443.3
e	7.0	442.7
1/4	7.3	442.4
cb	7.5	442.2
N	7.9	441.8

1090' E

N	7.9	441.8
cb	8.0	441.7
1/4	7.4	442.3
e	7.1	442.6
1/4	6.7	443.0
cb	7.0	442.7
S	6.6	443.1

449.67

1105'E

S	5.7	4440
cl	4.7	445.0
+3	5.3	444.4
+4	6.7	443.0
"4	6.3	443.4
E	7.0	442.7
"4	7.4	442.3
cl	7.4	442.3
N	7.4	442.3

1130'E

N	7.5	442.2
cl	7.2	442.5
"4	6.8	442.9
E	6.8	442.9
"4	6.3	443.4
cl	6.4	443.3
S	6.1	443.6

1150'E

S	4.9	444.8
cl	4.8	444.9
+2	4.8	444.9
+4	6.5	443.2
"4	6.1	443.6
E	6.2	443.5
"4	6.2	443.5
cl	6.6	443.1
N	7.1	442.6

449.67

Orange

54

1175'E

N	7.2	442.5
cl	6.6	443.1
"4	5.8	443.9
E	6.0	443.7
"4	6.1	443.6
cl	6.1	443.6
S	6.0	443.7

1200'E

S	5.6	444.1
cl	6.2	443.5
"4	6.0	443.7
E	6.3	443.4
"4	6.1	443.6
cl	7.0	442.7
N	7.0	442.7

1250'E

N	7.6	442.1
cl	6.6	443.1
"4	6.4	443.3
E	6.2	443.5
"4	6.1	443.6
cl	6.1	443.6
S	5.7	444.0

1300'E

S	5.4	444.3
cl	6.0	443.7

449.67

1300'E (cont)

114	6.0	443.7
C	6.4	443.3
114	7.0	442.7
cb	7.0	442.7
N	7.3	442.4

1350'E

N	6.0	443.7
cb	5.6	444.1
114	6.0	443.7
C	5.7	444.0
114	5.7	444.0
cb	5.3	444.4
S	4.8	444.9

1400'E

S	3.7	446.0
cb	4.6	445.1
114	5.0	444.7
C	5.0	444.7
114	5.2	444.5
cb	5.4	444.3
N	5.5	444.2

1450'E

N	5.3	444.4
cb	5.0	444.7
114	5.0	444.7
C	4.4	445.3

449.67

Orange

55

114	4.3	445.16
+14	4.5	445.2
cb	3.8	445.9
S	3.9	445.8

1500'E

S	4.3	445.4
cb	4.3	445.4
+6	5.0	444.7
114	4.8	444.9
C	4.5	445.2
+5	5.5	444.2
114	5.5	444.2
cb	5.5	444.2
N	6.2	443.5

1550'E

N	7.3	445.4
cb	7.2	445.5
114	6.7	443.0
C	5.6	444.1
114	5.3	444.4
+5	5.7	444.0
cb	5.1	444.6
S	5.3	444.4

1575'E

S	5.6	444.1
cb	5.4	444.3

449.67

1575' E. (com)

+2	6.5	4432
114	6.1	4436
c	6.5	4432
+4	7.9	4418
114	8.5	4412
cb	9.3	440.4
N	9.9	439.8

1600' E.

N	10.4	4393
cb	9.6	440.1
114	9.1	4406
c	7.7	440.0
114	7.3	442.4
+7	7.8	4419
cb	6.5	4432
S	6.4	4433

1630' E

S	7.3	4424
cb	8.0	441.7
+3	8.8	440.9
114	8.5	441.2
c	8.2	441.5
114	10.0	439.7
cb	11.0	438.7
N	11.6	4381

449.67

Orange

56

1655' E

N	12.8	4369
cb	12.2	4375
114	10.6	4391
c	9.1	4406
114	9.4	440.3
+8	9.9	437.8
cb	8.7	4410
S	8.9	4408

1685' E.

S	9.3	440.4
cb	9.0	440.7
+2	11.4	4383
114	11.2	4385
c	11.4	4383
+4	12.9	4368
T.P.	1.34	439.71 ✓
	11.30	438.37 ✓

114	3.8	435.9
cb	4.7	4350
N	5.7	4340

1700' E.

N	6.9	432.8
cb	5.8	433.9
114	5.0	434.7
+6	4.6	4351
c	2.6	4371
114	2.6	437.1

439.71

1700'E. (COH)

+8	2.6	437.1
cl	0.5	439.2
S	0.0	439.7

1745'E.

S	2.3	437.4
+8	3.2	436.5
cl	5.6	434.1
"4	5.7	434.0
+7	5.9	433.8
C	8.0	431.7
"4	9.7	430.0
cl	11.5	429.2
N	13.2	426.5

1770'E.

N	13.3	426.4
cl	11.2	428.5
"4	9.9	429.8
C	8.2	431.5
+3	6.2	433.5
"4	6.3	433.4
cl	6.3	433.4
+2	4.5	435.2
S	4.0	435.7

1800'E.

S	4.2	435.5
cl	5.4	434.3

439.71

Orange 57

+1	6.6	433.7
"4	6.7	433.0
+7	6.7	433.0
C	8.8	420.9
"4	10.7	429.0
cl	12.5	427.2
N	14.5	425.2

1835'E.

N	14.0	425.7
cl	12.3	427.4
"4	10.2	429.5
C	8.2	431.5
+3	5.9	433.8
"4	6.1	433.6
+7	6.2	433.5
cl	5.0	434.7
+5	4.0	435.7
S	2.1	437.6

1880'E.

S	70.5	440.2
+5	1.4	438.3
cl	2.3	437.4
+3	2.7	437.0
"4	4.1	435.6
"4	4.2	435.5
C	3.8	435.9

439.71

1880'E. (con)

"4	5.8	4339
cb	7.4	432.3
N	9.0	4307

1915'E.

N	6.0	433.7
cb	4.5	4352
"4	3.5	4362
C	1.8	438.9
"4	2.1	437.6
+5	2.1	437.6
+6	0.0	439.7
cb	+0.3	440.0
S	+2.3	442.0
T.P.	12.80	451.52
	0.99	438.72

1960'E.

S	7.4	4441
cb	8.8	4429.
+3	9.0	4425
+5	11.0	4405
"4	11.0	440.5
C	11.2	440.3
+5	13.0	4385
"4	13.3	4382
cb	14.4	4371
N	15.3	436.2

451.52

Orange

54

1985'E.

N	13.8	4377
cb	12.2	4393
"4	10.9	4406
C	9.3	4422
"4	9.4	4421
+5	9.6	4419
+7	8.1	4434
cb	7.7	4438
S	6.6	4449

2000'E

S	5.5	4460
cb	7.1	4444
+3	7.3	4442
+5	8.8	4427
"4	8.4	4431
C	8.3	4432
"4	9.2	4423
cb	9.6	4419
N	12.3	4392

2015

N	11.0	4405
cb	9.2	4419
"4	8.7	4428
+6	8.4	4431
C	7.5	4440
"4	7.4	4441

451.52

2015'E.

+5	7.7	443.9
+7	6.5	445.0
cl	6.4	445.1
S	5.0	446.5

2035'E.

S	3.8	447.7
cl	5.1	446.4
+5	6.6	444.9
'14	6.4	445.1
e	6.4	445.1
'14	6.8	444.7
cl	6.8	444.7
N	8.5	443.0

2055'E.

N	8.0	443.5
cl	7.0	444.5
'14	6.3	445.2
e	5.0	446.5
'14	5.0	446.5
+5	5.3	446.2
cl	4.4	447.1
S	3.1	448.4

2075'E.

S	1.6	449.9
cl	2.8	448.7
+5	3.9	447.6

Orange

59

451.52

'14	3.6	447.9
e	3.5	448.0
'14	3.3	448.2
cl	3.4	448.1
N	6.1	445.4

2100'E.

N	4.6	448.9
cl	3.5	448.0
'14	2.7	448.8
e	2.0	449.5
'14	1.9	449.6
+5	2.3	449.2
cl	1.1	450.4
S	0.2	451.3

T.P.	12.97	464.15 [✓]	0.34	451.18 [✓]
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2150'E.

S	8.4	455.8
cl	9.1	455.1
+3	9.7	454.5
+5	10.7	453.5
'14	10.4	453.8
e	10.8	453.4
'14	11.1	453.1
cl	11.9	452.3
N	12.9	451.3

464.15

2180'E

N	9.5	454.7
cl	8.8	455.4
"4	7.7	456.5
C	6.8	457.4
"4	7.0	457.2
+6	7.2	457.0
cl	6.2	458.0
S	5.8	458.4

2200'E

S	4.8	459.4
cl	5.2	459.0
"4	5.4	458.8
C	5.5	458.7
"4	5.2	459.0
cl	5.4	458.8
N	6.6	457.6

2230'E

N	4.6	459.6
cl	4.1	460.1
"4	3.8	460.4
C	3.8	460.4
"4	4.0	460.2
cl	4.2	460.0
S	4.4	459.6

464.15

2260'E

S	5.9	458.3
cl	5.7	458.5
+3	5.9	458.3
"4	5.6	458.6
C	5.0	459.2
"4	4.9	459.3
cl	4.6	459.6
N	4.0	460.2

2300'E

N	4.9	459.3
cl	5.3	458.9
"4	5.9	458.3
C	6.3	457.9
+3	7.0	457.2
"4	7.3	456.9
cl	7.8	456.4
S	8.3	455.9

2349.7 E = 90° from S.W. cor Orange & Radio Drive

S	9.8	454.4
+5	9.9	454.3
cl	8.6	455.6
+5	9.0	455.2
"4	8.7	455.5
C	8.2	456.0
"4	7.6	456.6
cl	7.2	457.0
N	6.8	457.4

Orange

60

464.15

2373.6 E. = $\frac{1}{2}$ Radio Drive at 90°

N	7.3	456.9
cl	7.7	456.5
"4	8.1	456.1
C	8.2	456.0
"4	8.6	456.6
cl	9.0	455.2
S	9.3	454.9

2397.5 E. = 90° from S.E. Cor Orange + Radio

S	8.2	456.0
cl	8.0	456.2
"4	7.5	456.7
C	7.3	456.9
+2	7.3	458.9
+5	5.8	458.4
"4	5.8	458.4
cl	6.4	457.8
N	7.1	457.1

2415' E

N	7.7	456.6
cl	7.2	457.0
"4	7.1	457.1
C	7.1	457.1
"4	7.1	457.1
cl	7.1	457.1
S	6.4	457.8

464.15

Orange

61

2430' E.

S	7.5	456.7
cl	7.4	456.8
"4	6.6	457.6
C	6.6	457.6
+5	6.8	457.4
+7	5.5	457.7
"4	5.6	457.6
cl	6.5	457.7
N	7.3	456.9

2450' E.

N	7.2	457.0
cl	7.2	457.0
"4	7.0	457.2
C	6.5	457.7
"4	6.3	457.9
cl	6.0	458.2
S	5.8	458.4

section

2475.5 E on N = S. line Mallard, at 90° = 0

S	6.3	457.9
cl	6.6	457.6
"4	6.0	458.2
C	6.0	458.2
+4	6.2	458.0
+6	4.7	459.5
"4	4.5	459.7
cl	4.4	459.8
N	5.5	458.7

464.15
2475.5 E on N. = S. line - Mallard section on S. line - Mallard on diagonal

Orange

62

N. = S.W. Cor Orange & Mallard

5.5 458.7

ch

5.3 458.9

114

5.9 458.3

E

4.7 459.5

114

3.9 460.3

ch

3.9 460.3

E

4.1 460.1

H46 S.E. Cor

ch K on B.M.

4.04 460.07 Orange & Mallard

Paradise. S & Sec.
Radio to Mariposa.

1-18-28
Miller.

376.98

63

B.M.	9.98	352.75 ✓		342.77	S.E. Cor Radio + Allix			
B.M. T.P.	13.01	344.37 ✓	1.39	351.36 ✓	N.W. Radio + Paradise			
		00 = N. Line Radio. on diagonal						
N.		11.8	352.6				100' N. on W	
cb		11.6	352.8					
"4		12.2	352.2					
c		11.3	353.1					
"4		10.4	354.0					
cb		9.8	354.6					
E		8.7	355.7					
		25' N on W						
E		4.8	359.6					
cb		5.3	359.1					
"4		6.3	358.1					
+2		7.6	356.8					
c		7.1	357.3					
"4		7.2	357.2					
cb		7.4	357.0					
W		7.4	357.0					
		60' N. on W						
W		1.6	362.8					
cb		1.1	323.3	63.9				
"4		0.6	323.7	63.8				
c		0.4	324.0	64.0				
+8		0.8	323.6	63.6				
T.P.	12.73	376.98 ✓	0.12	364.25				

Plotted
9-8-28
C.B.H.

"4						12.0		365.0
cb						11.3		365.7
E						11.3		363.7
E						3.1		373.9
cb						3.6		373.4
"4						4.5		372.5
+2						5.4		371.6
c						5.3		371.7
"4						5.4		371.6
cb						6.1		370.9
W						6.5		370.5
T.P.	12.94	389.88 ✓	0.04				376.94 ✓	
		150' N. on W						
W						10.1		379.8
cb						9.2		380.7
"4						8.5		381.4
c						8.0		381.9
+8						8.1		381.8
"4						7.2		382.7
cb						6.4		383.5
E						5.6		384.3
T.P.	11.81	401.48 ✓	0.21				389.67	
		200' N. on W						
E						6.0		395.5
cb						6.3		395.2

401.48

200' N. on W. (con)

1/4	7.2	394.3
1/4	8.4	393.1
c	8.5	393.0
1/4	9.0	392.5
cb	9.0	392.5
N	10.1	391.4

240' N. on W

W	8.3	399.2
cb	1.0	400.5
1/4	0.4	401.1
c	0.3	401.2
1/4	0.2	401.3
T.P.	12.74	413.97
cb	0.25	401.23
cb	11.6	402.4
E	11.2	402.8

270' N. on W.

E	5.3	408.7
cb	5.6	408.4
1/4	6.2	407.8
c	6.2	407.8
1/4	6.2	407.8
cb	6.2	407.8
W	6.4	407.6

300' N. on W.

W	0.0	414.0
cb	0.0	414.0

413.97

Paradise

64

1/4	0.1	413.9
c	0.3	413.7
1/4	0.4	413.6
T.P.	13.08	426.93
cb	0.12	413.85
cb	12.5	414.4
E	11.9	415.0

325' N. on W

c	8.0	418.9
cb	8.2	418.7
1/4	8.4	418.5
c	8.3	418.6
1/4	8.5	418.4
cb	7.7	419.2
W	8.3	418.6

355' N. on W = 5. line orange. from W. section at 90° from Paradise

W	3.2	423.7
cb	2.8	424.1
1/4	3.0	423.9
c	2.8	424.1
1/4	2.3	424.6
cb	1.7	425.2
E	1.5	425.4

T.P. 13.07 439.42 0.57 426.36

ohk on BM.

5.68 433.74

N.W. BM. cor.
orange & Paradise

439.42

S. db. Orange tow.

E	12.6	426.8
db	13.0	426.4
1/4	13.5	425.9
E	13.8	425.6
1/4	14.0	425.4
db	13.6	425.8
W	13.9	425.5

S. 1/4 Orange from W.

W	11.4	428.0
db	11.8	427.6
1/4	12.4	427.0
E	12.4	427.0
1/4	12.2	427.2
db	12.2	427.2
E	11.6	427.8

E Orange from W

E	10.5	428.9
db	10.7	428.7
1/4	10.6	428.8
E	10.8	428.6
1/4	10.8	428.6
db	10.4	429.0
W	10.5	429.9

N. 1/4 Orange from W

W	8.0	431.4
db	8.5	430.9

Paradise

65

439.42

1/4	9.3	430.1
E	9.3	430.1
1/4	9.5	429.9
db	9.2	430.2
E	9.0	430.4

N. db. of orange from W

E	7.4	432.0
db	7.3	432.1
1/4	7.8	431.6
E	7.8	431.6
1/4	7.5	431.9
db	6.5	432.9
W.	6.2	433.2

8.62 N. of above section = S. line Orange from E. to Paradise

W.	5.7	433.7
db	5.5	433.9
1/4	6.5	432.9
E	6.8	432.6
1/4	6.6	432.8
db	6.3	433.1
E	6.2	433.2

S.E. 40° Orange
433.24 Paradise

1.43 N. of above section = N. line Orange from W sec. at 90°

E.	6.2	433.2
db	6.2	433.2
1/4	6.4	433.0
E	6.7	432.7

439.42

N. Line Orange from W. (con)

1/4	6.3	4331
cl	5.3	4341
W	5.7	4337

8.57 N. of above = S. cl. orange to E.

W	4.6	4348
cl	4.7	4347
1/4	5.3	4341
E	5.5	4339
1/4	5.2	4342
cl	5.3	4341
E	5.3	4341

S. 1/4 Orange to E.

E	4.8	4346
cl	4.6	4348
1/4	4.5	4349
E	4.6	4348
1/4	4.1	4353
cl	4.0	4354
W	3.6	4358

E Orange to E

W	2.3	4371
cl	2.7	4367
1/4	3.2	4362
E	3.6	4358
1/4	3.8	4356
cl	4.3	4357
E	4.8	4346

439.42

Paradise

66

N. 1/4 Orange to E

E	3.9	4355
cl	4.0	4354
1/4	3.6	4358
E	2.8	4366
1/4	2.5	4369
cl	1.9	4375
W	1.7	4382
T.P.	12.33	451.10
		0.65
		N. cl Orange to E
		438.77

W	12.2	4389
cl	12.6	4385
1/4	13.3	4378
E	14.1	4370
1/4	14.6	4365
cl	14.5	4366
E	14.5	4366

oo = N. line orange to E

E	13.6	4375
cl	13.3	4378
1/4	13.3	4378
E	13.6	4375
1/4	12.8	4383
cl	11.9	4392
W	11.7	4394

50' N.

W	7.9	4432
cl	8.7	4424

451.10
50'N. (cont)

+3	9.6	4415
"4	9.9	4412
E	10.6	4405
"4	10.3	4408
cl	10.9	4404
E	11.4	4407

100'N

E	9.8	4413
cl	9.0	4421
"4	8.3	4428
C	7.9	4432
"4	7.2	4439
+7	6.5	4446
cl	5.6	4455
W	4.8	4463

150'N.

W	2.2	4489
cl	2.6	4485
+3	3.7	4474
"4	4.4	4467
E	4.8	4463
"4	5.8	4453
cl	6.7	4444
E	8.2	4429

Paradise

67

451.10
200'N

E	5.9	4452
cl	4.4	4467
"4	3.2	4479
C	2.1	4490
"4	1.9	4472
+8	1.1	4500

T.P.	12.58	462.90	0.78	450.32
cl			12.1	4508
W			11.6	4513

250'N.

W	7.8	4551
cl	8.5	4544
+4	9.4	4531
"4	10.5	4524
E	11.1	4518
"4	12.6	4503
cl	13.7	4492
E	15.2	4477

300'N.

E	12.1	4508
cl	10.5	4524
"4	9.2	4537
C	8.2	4547
"4	7.7	4552
cl	7.0	4559
W	5.7	4572

462.90

350' N.

N	4.6	4583
cl	4.6	4583
"y	5.8	457.1
e	5.8	4571
"y	6.0	456.9
cl	7.2	4557
E	8.6	4543

400' N.

E	5.0	457.9
cl	5.1	457.8
"y	4.7	4582
e	4.2	457.7
"y	4.6	458.3
cl	3.9	459.0
W	3.4	459.5

435.6 N = S. Line Mariposa 60' wide.

W	3.3	459.6
cl	3.5	4594
"y	3.8	4591
e	3.3	4596
"y	3.7	4592
cl	4.9	458.0
E	4.9	458.0

462.90

E Mariposa

Paradise

64

E	4.1	4589
cl	3.8	4591
"y	3.0	4579
e	2.5	4604
"y	2.8	4601
cl	1.9	4610
W	2.7	460.2

N. Line Mariposa

W	2.4	460.5
cl	2.0	460.9
"y	2.5	460.4
e	2.4	460.5
"y	2.8	460.1
cl	3.7	4592
B.M. E.	3.83	459.07
on Hub N.E. Cor Paradise + Mariposa		
T.P.	0.68	451.00
	12.58'	450.32
T.P.	1.43	442.05
	10.38	440.62
chk on B.M.	8.31	433.74
NW. orange Paradise		

60' wid.
10' els
10' 114s

Winnett St X Sec

Scimitar to Orange
to Springfield

1-19-28
Will

399.07

69

B.M. 595 399.07 393.12 + Winnett

00' N. Line Scimitar sec. on Ark

E	6.0	393.1
cb	6.5	392.6
14	7.1	392.0
e	6.7	392.4
14	6.1	393.0
cb	6.5	392.6
W	6.6	392.5

Plotted
3-8-28
CBH

40' N. on E.

W	3.1	396.0
cb	3.3	395.8
14	3.3	395.8
c	3.6	395.5
14	3.4	395.5
+8	3.0	396.1
cb	1.0	398.1
E	0.8	398.3

60' N. on E

E	0.5	398.6
cb	1.0	398.1
+3	3.0	396.1
14	3.1	396.0
c	3.0	396.1
14	2.5	396.6
cb	3.0	396.1
W	2.6	396.5

Hub N.E. Scimitar
+ Winnett

W	3.6	395.5
cb	2.6	395.5
14	3.5	395.6
c	3.9	395.2
14	4.5	394.6
+8	4.2	394.7
cb	1.6	397.5
E	1.4	397.7

75' N. on E.

90' N. on E. = S. Line Eider sec at 90°

E	4.2	394.9
+4	5.6	393.4
cb	5.6	393.4
14	5.2	393.8
c	5.3	393.8
14	5.6	393.4
cb	6.0	393.1
W	6.7	392.4

5.6' N = S. cb Eider sec at 70°

W	7.4	391.9
cb	6.9	392.2
14	6.7	392.4
c	5.9	393.2
14	5.7	393.4
cb	5.7	393.4
E	5.9	393.2

399.07

E Eider sec. at 90°

E	6.5	392.6
cl	7.6	391.5
"4	9.9	389.2
C	10.4	388.7
"4	10.8	388.3
cl	11.2	387.9
W	11.2	387.9
T.P.	0.65	387.06
	12.60	386.41

00° N. line Eider sec. at 90°

W	3.8	383.3
cl	3.1	384.0
"4	3.2	383.9
C	2.7	384.4
"4	1.6	385.4
cl	1.9	385.2
E	1.3	385.8

15' N.

E	3.6	383.5
cl	5.8	381.3
"4	6.5	380.6
C	7.0	380.1
"4	7.4	379.7
cl	7.7	379.4
W	6.8	380.3

40' N

W	13.7	373.4
---	------	-------

387.06

Winnett

70

cl	14.1	373.0
"4	13.7	373.4
C	12.0	375.1
"4	11.7	375.4
cl	12.4	374.7
E	11.4	375.7
T.P.	0.48	374.83
	12.71	374.35

65' N

E	6.1	368.7
cl	7.3	367.5
"4	7.7	367.1
C	8.5	366.3
"4	8.5	366.3
cl	8.2	366.6
W	8.6	366.4
T.P.	0.06	361.94
	12.91	361.92

100' N

W	4.6	367.4 357.4
cl	3.8	368.2 58.2
"4	3.0	369.0 59.0
C	4.1	367.9 357.9
"4	4.0	368.0 58.0
cl	3.6	368.4 58.4
E	3.2	368.8 358.8

361.98

130' N

E	10.4	351.6
dr	12.7	349.3
1/4	13.3	349.7
e	16.9	345.1
+5	13.1	349.9
1/4	13.1	349.9
dr	13.3	349.7
W	12.0	350.0
T.P.	0.16	342.94 ✓
	12.20	349.78 ✓

140' N

W	8.3	341.6
dr	10.2	339.7
1/4	12.0	337.9
+7	13.0	336.9
e	11.8	338.1
1/4	9.5	340.4
dr	7.6	342.3
E	6.4	343.5
T.P.	0.38	337.46 ✓
	12.86	337.08 ✓

200' N

E	1.6	335.9
dr	3.5	332.9
1/4	4.3	330.2
e	6.1	328.4 331.4
1/4	8.2	326.3
dr	11.4	323.1
W	10.3	321.2 327.2

337.46

Winnett.

71

215' N

W	16.0	318.5
+8	15.3	319.2
dr	19.4	315.1
+5	12.3	317.7
1/4	11.5	313.0
e	9.3	325.2 328.2
1/4	7.5	327.0
dr	6.2	328.3
e	4.6	329.9 332.9

230' N

e	7.3	327.5 330.2
dr	9.1	325.4
1/4	10.6	323.9
e	11.2	323.3 326.3
1/4	13.0	321.5
dr	15.5	319.0
+5	20.0	314.5
W	19.0	315.5 318.5
T.P.	0.50	325.15
	12.81	324.65

270' N

W	12.6	312.6
dr	10.2	315.0
1/4	8.4	316.8
e	7.7	317.5
1/4	5.5	319.7
dr	3.7	321.5
e	1.8	323.4

325.15

300' N.

E		7.5	3177
cl		9.5	3157
"4		11.5	3137
E		12.8	3124
T.P.	0.27	312.68 ^v	12.74 312.41 ^v
"4		2.7	31010
cl		3.9	3088
N		5.5	3072

340' N.

N		11.6	3011
cl		10.7	3020
"4		9.4	3029
E		8.9	3038
"4		7.4	3053
cl		6.3	3064
E		5.1	3076
T.P.	0.74	300.97 ^v	12.45 300.23 ^v

377' N.

E		7.2	293.8
			292.8
cl		7.4	2927
"4		8.0	2921
E		8.4	292.6 292.6
"4		9.7	2914
cl		9.0	2911
N		9.0	2911 292.0

300.97

Winnett

72

387' N.

N		10.2	2849 290.8
cl		10.9	2892
"4		15.0	2851 Wash
E		14.8	2853 Wash 286.8
"4		13.7	2864 Wash
cl		12.6	2875 Wash
E		12.8	2873 Wash 288.8

397' N.

E		9.5	2806 291.5
cl		10.3	2848
"4		10.7	2894
E		11.4	2887 289.6
"4		13.4	2867
cl		15.5	2846 Wash
N		15.7	2844 Wash 285.3

405' N.

N		11.6	2885 289.4
cl		11.3	2888
"4		10.8	2893
E		11.7	2884 289.3
"4		9.6	2805
cl		8.5	2816
E		8.1	2850 292.9

415' N.

E		7.9	2822 293.1
cl		8.2	2819

300.97

415' N. con

Winnett.

73

313.07

'14	8.9	291.2	291.2	C	14.7	2984.
e	9.4	2907	291.6	'14	14.0	2991
'14	8.6	2915		ch	14.3	2988
ch	9.1	291.0		+5	14.0	2991
W	9.9	2907	291.1	+7	12.3	3008

445' N

W	6.2	293.9	294.8	E	11.9	3012
ch	6.5	2936		E	7.3	3058
'14	6.5	2936		+6	9.4	3037
e	6.3	2938	294.7	+8	12.1	3010
'14	6.6	2935		ch	12.1	301.0
ch	6.4	293.7		'14	12.2	3009
E	5.7	294.4	295.3	+5	11.1	302.0

50' N. on E.

Sec. Taken on diagonal from S.E. to S.W. Cor. ignoring Angle PT.

<u>486' N. on E.</u>				C	13.4	2997
E	3.5	2966	297.5	'14	14.0	2991
ch	3.4	2967		ch	12.2	3009
'14	3.5	2966		W	10.2	3029
C	3.7	2964	297.3			
'14	3.9	2962		W	7.7	3054
ch	4.1	2960		ch	9.4	3037
W	4.3	2968	296.7	'14	11.4	3017

100' N. on E.

T.P. H46 B.M. 12.43 313.07 0.33 300.64

N.E. Cor Radio
+ Winnett

see Taken on Diagonal from N.W. To N.E. Cor. ignoring Angle PT.

N	14.7	2984		'14	9.6	3035
ch	15.3	2978		ch	9.6	3035
'14	15.1	299.0		+3	9.3	3038
				+4	7.0	3061
				E	4.4	3087

313.07

150' N. on E

E	0.8	312.3
+6	3.4	3097
+7	6.5	3066
cb	6.0	3091
"4	6.0	3071
+6	5.5	307.6
c	8.1	3050
"4	7.6	3055
cb	6.6	3065
W	4.4	3087

200' N. on E.

N	1.2	311.9
cb	3.6	3095
"4	4.3	3088
c	4.5	3086
+6	3.0	3101
"4	3.8	3093
cb	3.7	3094
+2	4.5	3086
+4	1.0	31201
T.P.	12.79	325.79
E,	0.07	313.00
	11.1	3147

250' N. on E

E	7.4	318.4
+5	9.5	3163
+8	13.2	3126

325.79

Winnett

74

cb	12.6	313.2
"4	12.7	313.1
+5	11.9	313.9
c	14.3	311.5
"4	14.6	311.2
cb	14.3	311.5
W	12.7	313.1

300' N. on E.

W	9.2	3166
cb	11.6	3142
"4	11.6	3142
c	11.4	3144
+6	9.6	316.2
"4	9.8	3160
cb	10.0	3158
+5	7.2	3186
c	5.0	3208

350' N. on E

E	2.2	3236
+8	4.2	3216
cb	6.8	3190
"4	6.3	3195
c	7.6	3182
"4	8.6	3172
cb	8.8	3170
W	8.2	3176

325.79

367.8 N. on E. = S. LineSpringfield
Orange

N.	7.9	317.9
cl	8.0	317.8
1/4	8.0	317.8
+5	7.4	318.4
c	4.2	320.9
1/4	4.7	321.1
cl	5.0	320.8
+1	5.0	320.8
+3	2.2	323.6
E	0.4	325.4

S. cl

E	+0.3	326.1
+7	1.4	324.4
cl	4.0	321.8
1/4	3.7	322.1
c	4.1	321.7
+5	7.1	318.7
1/4	7.5	318.3
cl	7.7	318.1
W	7.7	318.1

S. 1/4

W	7.5	318.3
cl	7.4	318.4
+5	6.8	319.0
1/4	6.0	319.8
c	3.2	322.6

325.79

Winnett

75

1/4	2.8	323.0
cl	2.3	323.5
E	+1.4	327.2
<u>Orange</u>		
E	+0.6	326.4
cl	1.2	324.6
1/4	1.8	324.0
c	2.1	323.7
1/4	5.4	320.4
cl	6.7	319.1
W	7.0	318.8

N. 1/4

W	6.0	319.8
cl	6.1	319.7
1/4	4.5	321.3
c	2.8	323.0
+3	1.4	324.4
1/4	0.9	324.9
T.P.	12.96	338.46
cl	0.29	325.50
cl	13.1	325.4
E	11.2	327.3

N. cl

E	9.7	328.8
cl	12.3	326.2
+3	13.1	325.4
1/4	12.6	325.9

"4 13.0 3255
 ch 14.3 3242
 W 17.1 3214
 18.1 320.4
 18.1 320.4

N Line Springfield
 Orange

W 17.7 3208
 ch 17.4 3211
 "4 16.2 3223
 E 13.4 3257
 +2 11.9 3266
 "4 11.9 3266
 ch 12.4 3261
 +4 9.3 3292
 E 17.8 330.7
 7.90 330.56

N.E. Winnett
 + Orange

SEE
 F.B. 1313, 14
 Springfield to Tooke

ch Ken Hub BM

C.B. Walker

Hardin
Wells

5-8-42

Levels on Winnett St.

10' East of E. Winnett - which is

the approximate E of existing siled
road. Cross sections this Book P-69-76
for ties on Winnett see E.B. 12/4 P-6

Also Cross Sections Winnett from Tooley
to Springfield
to Orange Ave E.B. 1313 Page 0 to 14

And from Tooley to Barton Grove Blvd.
see E.B. 1313 Page 15 to 31

From Radio to Tooley

10.86	311.50	300.64	
HA to NE Cor = 0+00		11.9	299.6
+50		10.2	301.3
1+00		8.0	303.5
+50		4.8	306.7
2+00		2.1	309.4
T.P. 12,13	<u>323.21</u>	0.42	311.08
2+50		10.5	312.7
3+00		7.5	315.7
+50		4.2	319.0
+67.8 = S.L. Orange		2.7	320.5
T.P. 12,10	<u>335.14</u>	0.17	323.04
+97.8 = Orange		11.5	323.6
+127.8 = N.L. Orange		8.8	326.3
Chk. N.E. Hub " Winnett	4.5%	330.62	
		330.56	P. 76
4+50		7.2	327.9

S.M. Hub #73
N.E. Cor.
Radio to Winnett

(W.)

Red. & Plot. 7/9/42

Indexed
C.S.K.335.14

77

5+00		3.6	331.5
+50		0.05	335.09
T.P. 12,60	<u>347.69</u>	0.05	335.09
6+00		9.2	338.5
+50		5.5	342.2
7+00		1.7	346.0
+50			
T.P. 13,12	<u>360.37</u>	0.44	347.25
7+50		10.31	350.06
8+00		6.0	354.4
+50		1.4	359.0
T.P. 12,92	<u>373.06</u>	0.23	360.14
8+75		12.2	360.9
9+00		10.8	362.3
+50		8.2	364.9
10+00		5.1	368.0
+50		0.9	372.2
T.P. 12,65	<u>385.39</u>	0.32	372.74
11+00		9.1	376.3
+50		4.6	380.8
T.P. 12,28	<u>397.14</u>	0.53	384.86
12+00		10.5	386.6
+50		4.2	392.9
T.P. 12,30	<u>409.27</u>	0.17	396.97
13+00		8.9	400.4
+50		1.3	408.0

	409.27	
T.P. 11.55	420.27	0.55 408.72
13+68 ⁰¹ = S. Tooley		9.7 410.6
10' Lt. = E Winnett		9.5 410.8
13+99 ⁰¹ = S. Tooley		5.2 415.1
14+28 ⁰¹ = N. "		4.6 415.7
10' Lt. Winnett + Tooley		4.7 415.6
chk. NW. B.M. Bolt by	375	416.52
FB 1313 - Page 0		= 416.64

0.12 = diff.

Levels on E Winnett St. from N.E. Radiol Rd
to a point on E Winnett 200' South of N.E.

	8.81	309.45	300.64 B.M. P-77
St. Δ to N.E. Cor			
= 0+00			
0+38	10.4	299.1	
0+48	11.0	298.5	
0+50	11.3	298.2	
0+50	12.0	297.5	
1+00	15.7	293.8	
+12	17.3	292.2	
+21	18.2	290.3	
+35 = N Bank West	19.7	289.8	
+39 = Bottom "	21.7	287.8	
+42 "	21.7	287.8	
+48 = S. Bank	16.8	292.7	
1+75	8.7	300.8	
2+00	2.9	306.6	

	309.45	
T.P. 12.29	320.04	2.40 307.05
2+25		8.3 311.7
750		4.4 315.6
775		+1.2 321.2
3+00		+6.8 326.8
chk. 2+00 P-77		10.7 309.3
		309.4
		0.1

RADIO ROAD — from Winnett St
West 500'

Levels on E Existing Traveled Roadway

	9.45	310.09	300.64 B.M. P-77
E Winnett St			
= 0+00 going West			
	11.7	298.4	
0+50	12.3	297.8	
1+00	12.6	297.5	
+50	12.7	297.4	
2+00	12.5	297.6	
750	12.7	297.4	
3+00	13.2	296.9	
750	14.7	295.4	
4+00	16.6	293.5	
750	17.3	292.8	
5+00	18.1	292.0	

RADIO ROAD from E Winnett 500' East			
E Winnett			
= 0+00	310.09	11.7	298.4
750		10.6	299.5
1+00		8.6	301.5
750		7.4	302.7

Cont. P-79

Radio Road Cont. from P. 78

79

310.09 ✓

2700	7.1	303.0
750	6.8	303.3
3400	6.6	303.5
750	6.7	303.4
4400	6.1	304.0
750	4.5	305.6
5400	1.7	308.4

Rad. & Phot. 5-19-42 (21)

	S	1	E	W	S
			4.00	4.00	
			<u>3.93</u>	<u>4.72</u>	
			+0.07	-0.72	
			+0.1"		
		2	4.00	4.00	
			<u>3.95</u>	<u>4.45</u>	
			+0.05	-0.45	
			+0-1/2"	-0.5"	
		3	4.00	4.73	
			<u>4.09</u>	<u>5.15</u>	
			-0.09	-0.42"	
			-0.1"	-0.54"	
4.73		4	4.00	4.73	
<u>4.92</u>			<u>4.07</u>	<u>5.05</u>	
-0.09			-0.07	-0.32	
			-0.1"	-0.4"	
		5	4.00	4.73	
			<u>3.91</u>	<u>4.53</u>	
			+0.09	+0.20	
			+0.1"	+0.2 1/2"	
N		6	4.00	4.73	N
			<u>3.81</u>	<u>4.61</u>	
			+0.19	+0.12	
			+0-2 1/4"	+0-1 1/2"	
			E	W	

68
 4.73
 72
5.45

DIRECTIONS FOR USE OF TABLES
 TABLE No. 1
 5.14
4.73
 45
 5.18
4.73
 45
 7.73

Distance of slope stake from side or shoulder to stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level, the correction is found in the correction table. Add this amount if cut, elevate if fill. Add this amount to cut or fill and find in table. Set up rod at this point, and line of sight should cut target.

IMPROVED TABLES AND INFORMATION

TABLE No. 2
 To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given L may be found by dividing tangent (or external), opposite L by given tangent (or external).
 The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

ENGINEERING DEPARTMENT,
CITY OF CALIFORNIA,
SAN DIEGO.

~~1/2" PIPE RE. X 807~~

~~TOOLEY & ORIOLE~~

NL

MINI Δ RE 913

Paradise 46206

338.8
8.27
433.78