

1228

HILLSIDE DRIVE  
SECTIONS AND LEVELS

~~ALCO~~

FIELD BOOK

760

TRAVERSE TABLE FOR TRANSIT BOOK.

From 1° to 90° for a distance of 100.

Degrees.	DEGREES.		¼ DEGREE.		½ DEGREE.		¾ DEGREE.		Degrees.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
0			100.00	0.44	100.00	0.87	99.99	1.31	89
1	98.98	0.75	99.98	2.18	99.97	2.62	99.95	3.05	88
2	99.94	2.49	99.92	3.93	99.91	4.36	99.88	4.80	87
3	99.86	3.23	99.84	5.67	99.81	6.10	99.79	6.54	86
4	99.76	3.98	99.73	7.41	99.69	7.85	99.66	8.28	85
5	99.62	4.73	99.58	9.15	99.54	9.58	99.50	10.02	84
6	99.45	5.45	99.41	10.89	99.36	11.32	99.31	11.75	83
7	99.25	6.19	99.20	12.62	99.14	13.05	99.09	13.49	82
8	99.03	6.92	98.97	14.35	98.90	14.78	98.84	15.21	81
9	98.77	7.64	98.70	16.07	98.63	16.50	98.56	16.93	80
10	98.48	8.36	98.40	17.79	98.33	18.22	98.25	18.65	79
11	98.16	9.08	98.08	19.51	97.99	19.94	97.90	20.36	78
12	97.81	9.79	97.72	21.22	97.63	21.64	97.53	22.07	77
13	97.44	10.50	97.34	22.92	97.24	23.34	97.13	23.77	76
14	97.03	11.19	96.92	24.62	96.81	25.04	96.70	25.46	75
15	96.59	11.88	96.48	26.30	96.36	26.72	96.25	27.14	74
16	96.13	12.56	96.00	27.98	95.88	28.40	95.76	28.82	73
17	95.63	13.24	95.50	29.65	95.37	30.07	95.24	30.49	72
18	95.11	13.90	94.97	31.32	94.83	31.73	94.69	32.14	71
19	94.55	14.55	94.41	32.97	94.26	33.38	94.12	33.79	70
20	93.97	15.20	93.82	34.61	93.67	35.02	93.51	35.43	69
21	93.36	15.84	93.20	36.24	93.04	36.65	92.88	37.06	68
22	92.72	16.46	92.55	37.86	92.39	38.27	92.22	38.67	67
23	92.05	17.07	91.88	39.47	91.71	39.87	91.53	40.27	66
24	91.35	17.67	91.18	41.07	91.00	41.47	90.81	41.87	65
25	90.63	18.26	90.45	42.66	90.26	43.05	90.07	43.44	64
26	89.88	18.84	89.69	44.23	89.49	44.62	89.30	45.01	63
27	89.10	19.40	88.90	45.79	88.70	46.17	88.50	46.56	62
28	88.29	19.95	88.09	47.33	87.88	47.72	87.67	48.10	61
29	87.46	20.48	87.25	48.86	87.04	49.24	86.82	49.62	60
30	86.60	21.00	86.38	50.38	86.16	50.75	85.94	51.13	59
31	85.72	21.50	85.49	51.88	85.26	52.25	85.04	52.62	58
32	84.80	22.00	84.57	53.36	84.34	53.73	84.10	54.10	57
33	83.87	22.48	83.63	54.83	83.39	55.19	83.15	55.56	56
34	82.90	22.95	82.66	56.28	82.41	56.64	82.16	57.00	55
35	81.92	23.40	81.66	57.71	81.41	58.07	81.16	58.42	54
36	80.90	23.84	80.64	59.13	80.39	59.48	80.13	59.83	53
37	79.86	24.26	79.60	60.53	79.34	60.88	79.07	61.22	52
38	78.80	24.67	78.53	61.91	78.26	62.25	77.99	62.59	51
39	77.71	25.07	77.44	63.27	77.16	63.61	76.88	63.94	50
40	76.60	25.45	76.32	64.61	76.04	64.94	75.76	65.28	49
41	75.47	25.82	75.18	65.93	74.90	66.26	74.61	66.59	48
42	74.31	26.18	74.02	67.24	73.73	67.56	73.43	67.88	47
43	73.14	26.52	72.84	68.52	72.54	68.84	72.24	69.15	46
44	71.93	26.85	71.63	69.78	71.33	70.09	71.02	70.40	45
45	70.71	27.17							
Degrees.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Degrees.
DEGREES.	¼ DEGREE.		½ DEGREE.		¾ DEGREE.		DEGREES.		

340 Dep. opp to 7/16/20 AH

1228

ENGINEERING DEPARTMENT,  
CITY OF  
SAN DIEGO,  
CALIFORNIA.

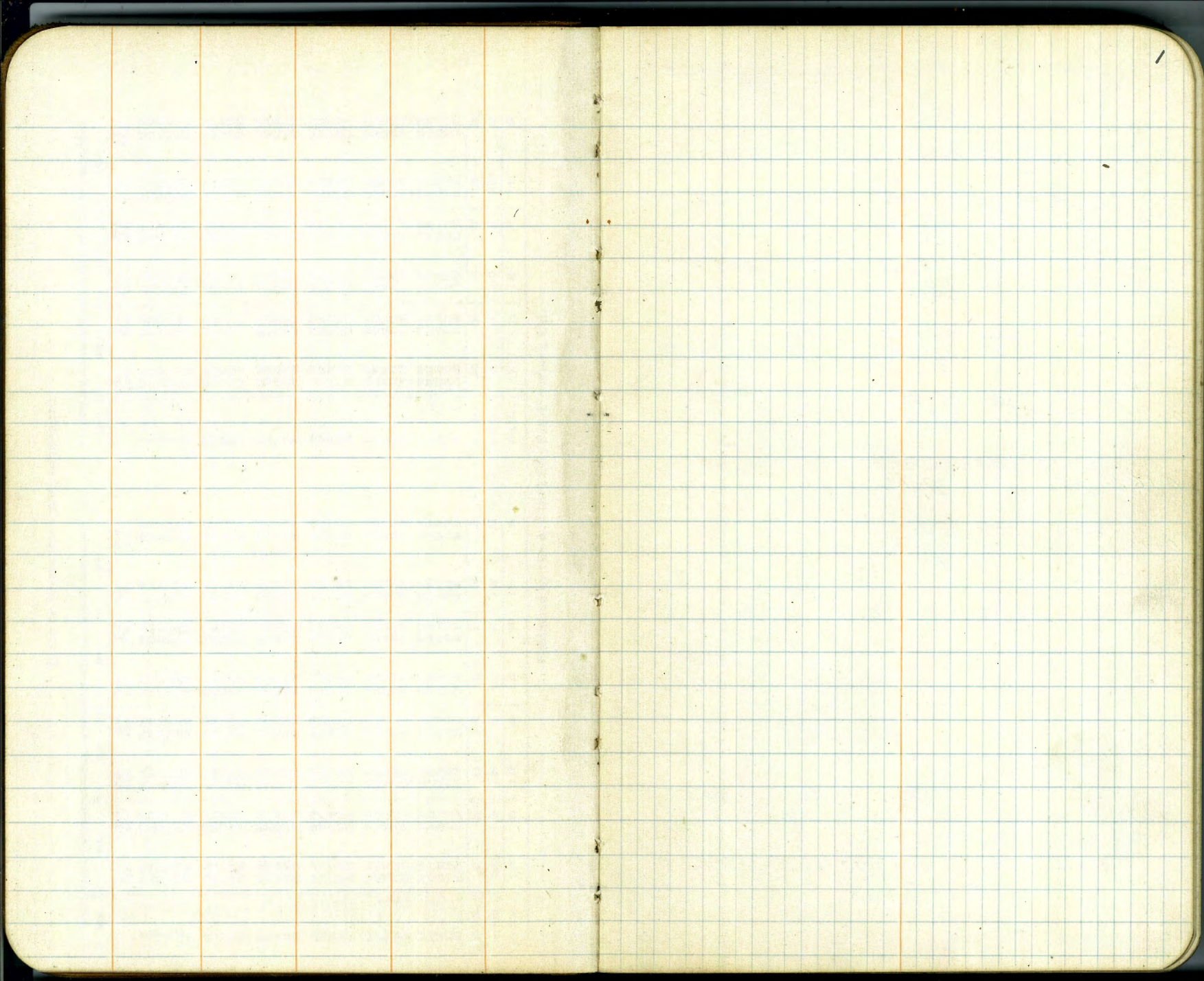




TABLE OF STADIA REDUCTIONS.—Continued.

Min.	24°		25°		26°		27°		28°		29°		30°	
	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.
0	83.46	37.46	82.14	38.30	80.78	39.40	79.39	40.45	77.96	41.45	76.50	42.40	75.00	43.30
2	83.41	37.20	82.09	38.34	80.74	39.44	79.34	40.49	77.91	41.48	76.45	42.45	74.95	43.33
4	83.37	37.23	82.05	38.35	80.69	39.47	79.30	40.52	77.86	41.52	76.40	42.46	74.90	43.36
6	83.33	37.31	81.98	38.41	80.65	39.54	79.26	40.58	77.81	41.55	76.35	42.49	74.85	43.39
8	83.29	37.31	81.94	38.41	80.61	39.54	79.22	40.58	77.77	41.55	76.31	42.50	74.81	43.42
10	83.24	37.35	81.82	38.49	80.55	39.58	79.15	40.62	77.72	41.61	76.25	42.53	74.75	43.45
12	83.20	37.39	81.87	38.53	80.51	39.61	79.11	40.66	77.67	41.65	76.20	42.59	74.70	43.47
14	83.15	37.47	81.78	38.56	80.46	39.65	79.06	40.69	77.62	41.68	76.15	42.62	74.65	43.50
16	83.11	37.47	81.73	38.56	80.41	39.65	79.01	40.70	77.57	41.71	76.10	42.63	74.60	43.53
18	83.07	37.51	81.74	38.64	80.37	39.72	78.96	40.72	77.53	41.74	76.06	42.64	74.56	43.56
20	83.02	37.54	81.69	38.67	80.32	39.76	78.92	40.79	77.48	41.77	76.00	42.71	74.49	43.59
22	82.98	37.58	81.65	38.71	80.28	39.79	78.87	40.82	77.42	41.81	75.95	42.74	74.44	43.62
24	82.93	37.65	81.58	38.73	80.18	39.83	78.77	40.85	77.38	41.84	75.90	42.77	74.39	43.65
26	82.89	37.70	81.55	38.75	80.13	39.85	78.72	40.87	77.33	41.87	75.85	42.80	74.34	43.68
28	82.85	37.70	81.51	38.82	80.14	39.90	78.73	40.92	77.28	41.90	75.80	42.83	74.29	43.70
30	82.80	37.74	81.47	38.86	80.09	39.93	78.68	40.96	77.23	41.93	75.75	42.86	74.24	43.73
32	82.76	37.77	81.42	38.89	80.04	39.97	78.63	40.99	77.18	41.97	75.70	42.89	74.19	43.76
34	82.72	37.85	81.33	38.97	79.95	40.04	78.54	41.06	77.13	42.03	75.65	42.92	74.14	43.79
36	82.67	37.85	81.28	39.00	79.90	40.07	78.49	41.09	77.08	42.06	75.60	42.95	74.09	43.82
38	82.63	37.89	81.23	39.00	79.85	40.07	78.44	41.12	77.04	42.09	75.55	42.98	74.04	43.84
40	82.58	37.83	81.24	39.04	79.86	40.11	78.44	41.12	76.99	42.09	75.50	43.01	73.99	43.87
42	82.54	37.86	81.19	39.06	79.81	40.14	78.39	41.15	76.94	42.12	75.45	43.04	73.93	43.90
44	82.49	38.00	81.15	39.11	79.75	40.18	78.34	41.16	76.89	42.15	75.40	43.07	73.88	43.93
46	82.45	38.04	81.10	39.15	79.72	40.21	78.30	41.22	76.84	42.19	75.35	43.10	73.83	43.95
48	82.41	38.08	81.05	39.18	79.67	40.24	78.25	41.26	76.79	42.22	75.30	43.13	73.78	43.98
50	82.36	38.11	81.01	39.22	79.62	40.28	78.20	41.29	76.74	42.25	75.25	43.16	73.73	44.01
52	82.32	38.15	80.97	39.25	79.58	40.31	78.15	41.32	76.69	42.28	75.20	43.19	73.68	44.04
54	82.27	38.19	80.92	39.29	79.53	40.35	78.10	41.35	76.64	42.31	75.15	43.22	73.63	44.07
56	82.23	38.23	80.87	39.33	79.48	40.38	78.05	41.39	76.59	42.34	75.10	43.24	73.58	44.10
58	82.18	38.26	80.83	39.36	79.44	40.42	78.01	41.42	76.55	42.37	75.05	43.27	73.52	44.12
60	82.14	38.30	80.78	39.40	79.39	40.45	77.96	41.45	76.50	42.40	75.00	43.30	73.47	44.15
c= 75....	68	31	.63	32	67	.33	.66	.35	.66	.36	.65	.37	.65	.38
c=1.15....	1.05	48	1.04	50	1.03	51	1.02	.53	1.01	55	1.00	.57	1.00	.58
c=1.90....	1.73	79	1.72	82	1.70	85	1.69	.58	1.67	91	1.65	.94	1.64	.96

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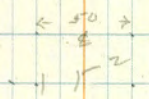
Levels  $\frac{1}{4}$  X-sections Hillside Drive

Tr Jack B. Randall  
Aug 26-28

5.63 230.55 224.92

B.M. Stake S.E. Cor Hillside Dr

220.0 219.0-219.8-221.3 222.1 222.25  
 0+00 10.5 11.5 11.7 9.2 8.5 8.3  
 1.5 4 +2.0 8 2.5



222.3 222.9-221.5-224.8 225.3 225.9  
 0+19.47 8.2 8.6 9.0 5.7 5.2 4.6  
 4.5 4 +3.0 2 1.5

222.9 222.5-222.3-226.3 226.8 227.0  
 0+25 7.7 8.0 8.2 4.2 3.7 3.5  
 +3.0



225.8 226.1-225.3-227.5  
 0+50 4.7 4.4 5.2 3.0  
 +3.0

227.0 227.4-226.8-230.2  
 0+62.54 3.8 3.1 3.7 0.3  
 +3.0

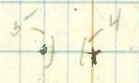
PC

228.6 229.0-228.2  
 0+73 1.9 1.5 2.3  
 +4.0

T.P. 11.46 241.71 0.30 230.25

0+62.54

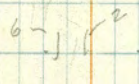
230.5 230.7  
 0+50 11.2 11.0



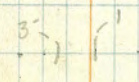
232.2 231.9  
 0+62.24 9.5 7.8

PC

232.6 234.3 234.0  
 0+75 9.1 7.4 7.7



230.1 231.7 231.4-235.7-236.9 237.0  
 1+00 11.5 10.0 10.3 8.0 4.8 4.5  
 +3.0



L R

241.71

229.8	232.5	234.6	234.4	236.6	238.2	239.0
1725	11.9	9.2	7.1	4.3	5.7	3.5
			+16.0	±	+11.0	

50  
15  
5

230.2	232.4	237.6	237.6	240.5	232.7
1750	11.5	9.3	4.1	4.1	4.2
		+11.0		+12.0	1.2
				R.	9.0

11  
15

234.5	236.0	240.6	240.6
1775	7.2	5.7	0.9
		+11.0	+3.0

238.9	240.1
2100	2.8
	1.6

T.P.	12.45	2 53.77	0.39	241.32
------	-------	---------	------	--------

1775	241.3	243.6	245.1
	12.4	10.1	8.6
	+18.5		

5  
15

2100	244.5	243.5	244.2	244.0
	9.2	9.9	9.5	9.6
	+7.0		+27.1	7.7

2  
12

2125	240.8	243.7	247.5	247.7
	12.9	11.0	5.4	5.0
			+3.0	+5.0

1  
5

2150	241.8	243.2	249.6	250.5
	12.0	10.6	4.2	3.0
			+3.0	+7.0

3  
3

2155.25	241.7	242.8	247.1	251.2
	12.1	11.0	4.5	2.6
			+3.0	+8.0

P.T.

4  
1

2175	242.3	244.7	251.6	252.5
	11.3	9.1	2.2	0.7
			+5.1	+4.0

4  
15

3100	243.4	246.3	252.3
	10.4	8.3	1.5

P.C.



253.77

3+05.64 243.4 246.0 250.6 ✓  
10.4 7.8 3.2  
+3.0

P.C

3+25 245.9 247.3 251.6 ✓  
7.9 6.5 3.2  
+3.0

3+50 252.0 252.6 ✓  
1.8 1.2

T.P 11.83 265.20 0.40 253.37

1866

3+00 254.0 254.0 255.6 ✓  
10.7 11.2 1.6  
+3.0

5-1-3

3+05.64 252.7 254.3 257.0 ✓  
10.5 10.5 10.9 3.2  
+7.0

P.C

5-1-3

3+25 259.1 256.6 260.2 ✓  
9.6 8.6 5.0  
+18.0

2-5

3+50 253.2 257.1 259.0 262.5 ✓  
12.0 7.8 8.1 6.2 2.7  
+18.0

2-7

3+75 254.3 254.9 260.3 265.2 ✓  
10.9 10.3 9.0 6.3 6.3 2.7  
+10.3 2 +18.0 R

3-7-15

3+95.99 258.2 259.0 260.3 265.2 ✓  
9.0 6.2 4.9 5.1 7.0  
+11.0 7.0

P.C.E

2-11

4+00 258.4 260.2 260.6 265.6 ✓  
6.8 5.0 4.6 5.0 7.4  
+11.0 +7.0

2-11

4+25 254.2 255.3 261.4 261.6 ✓  
11.0 9.9 3.7 3.8 3.6  
+7.0 +12.0

7-12

265:20

4+50	252.9	259.1	261.4	260.9	261.1	✓
	12.3	12.1	3.8	3.2	4.0	4.3
		+3.0	2	1120	+10	

Wash - Row culvert - 4+50 left side

8- 12

4+66.45	253.5	266.4	267.8	269.0	261.6	✓
	11.7	8.8	2.2	2.2	3.4	3.6
		+7.0	8	+9.0	+15.0	

P.C.C

8- 9

4+75	254.0	267.8	268.9	269.2	262.1	262.3	✓
	14.2	7.4	2.3	2.0	3.1	2.9	
		+10.0		+7.0			

10- 7

5+00	256.7	260.0	264.7	265.0	✓
	8.5	3.2	0.5	0.7	0.2
		+12.0		+3.0	

5+25	259.4	262.8	✓
	5.8	2.4	

J.P.	11.19	275.12	1.27	263.93
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3+75		264.2	264.9	✓
		10.9	10.2	

3+95.39		266.7	267.9	✓
		8.4	7.2	

P.C.C

B.M.	1	5.22	270.80
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B.M. - 10 ft intake, 3+95.39 Right side - P.C.C

4+00		267.2	268.8	✓
		7.9	6.3	

4+25		267.4	268.2	269.3	✓
		7.9	6.9	3.6	
		+1.5			

5+00		267.0	✓
		8.1	
		+6.0	

273.12

5+25 266.7 273.1 ✓  
8.4 89 2.0  
+ 13.0 + 460.0

5+50 260.8 264.2 269.1 269.2 269.0 ✓  
14.3 18.9 6.0 5.9 6.1  
+ 8.0 + 8.0

5+62.04 261.9 263.6 269.9 269.9 270.2 ✓  
13.2 11.3 5.2 5.2 4.9  
+ 7.0 + 13.

RT

5+68.94 263.1 264.3 270.7 270.5 270.9 ✓  
12.0 16.8 4.4 4.6 4.2  
+ 3.0 + 12.0

P.C

5+75 265.0 266.0 271.5 271.1 271.4 271.6 ✓  
16.1 9.1 3.6 4.0 3.7 3.5  
+ 4.0 + 17.0

6+00 267.7 268.9 274.5 273.1 272.7 273.3 ✓  
7.4 6.2 8.6 2.0 2.4 1.8  
+ 3.0 + 19.0

6+25 266.6 267.9 274.3 274.0 274.1 ✓  
8.3 7.2 8.8 1.1 1.0  
+ 3.0 + 17.0

6+36.04 267.0 268.9 275.0 274.5 274.7 ✓  
7.1 6.2 8.1 6.3 6.4  
+ 5.0 + 17.0

P.A.C

T.P. 9.57 284.38 0.31 274.81

5+00 272.4 275.0 ✓  
12.0 9.4

12-1-3

5+25 278.8 281.0 ✓  
5.6 3.4

13-1-6

5+50 279.4 281.0 283.1 ✓  
5.3 3.4 1.3  
+ 16.0

15-1-8

284.38

5+62.04	279.7	281.8 ✓
	4.7	2.6
5+68.94	279.9	282.3 ✓
	4.7	2.1
5+75		280.8 ✓
		3.6
6+00		277.8 ✓
		6.6
6+25	281.4	282.3 ✓
	3.0	1.9
6+36.04	279.9	281.4 ✓
	4.5	3.0

P.T

P.C

P.R.C

< 50 >
47 11
37 11
7 15.9
1 15.8
27 15
5 14
1 1

6+50	267.5	269.4	275.6	274.5	273.7	280.5	282.0 ✓
	16.9	18.0	8.8	9.9	8.7	3.9	2.4
		+10.		+10.			
6+70	276.1	274.7	276.2	277.3	277.8 ✓		
	13.3	9.7	8.2	7.1	6.6		
		+15.0					

10 11
1 1
15 12
1 1

B.17 6.08 278.30

B.M. Stake + letter S.W. Cor Garage Sta. 6+50 - 6+75

6+80	276.9						
	7.45						
	+13.0						
7+80	272.9	276.5	277.7	278.5	280.9	282.3 ✓	
	14.5	9.9	6.7	5.9	3.5	2.1	
		+16.0	+15.				
7+01.03	273.1	276.3	277.3	278.5	281.4	282.9 ✓	
	11.3	8.1	7.1	6.7	5.9	3.0	
		+16.0	+15.				

Concrete Drive - S.W. Cor side wall 7+7

+16.0 +10 on left Concrete Drive

P.T. #16 \* + 7 Left - Concrete Dr.

5 12
1 1
5 12
1 1

7+25	273.8	277.3	277.1	277.6	279.7	279.7	282.3 ✓
	10.6	7.4	6.7	6.8	4.7	4.7	2.1
		+15	+6				
7+48.62	274.1	275.9	277.7	277.6	279.3	279.7	284.4 ✓
	10.3	8.5	6.7	6.8	5.1	4.7	4.7
		+13	+4	+2			
7+50	273.7	275.3	277.7	277.5	279.3	279.6	284.1 ✓
	10.7	9.1	6.7	6.8	4.1	4.8	4.3
		+13	+2				
7+75	271.9	274.1	277.4	277.4	279.6	279.8	283.8 ✓
	12.5	10.3	7.0	7.0	4.8	4.6	0.6
		+13	+3				
8+0.0	272.3	275.4	277.4	277.4	280.1	282.8	284.8 ✓
	12.1	9.0	7.9	7.9	4.3	4.6	7
		+14	+5		+18		
8+10.18	272.7	275.3	277.7	277.7	279.5	283.7	284.8 ✓
	11.7	9.1	8.7	8.7	4.9	4.1	4.7
		+14	+5	+18	+17		
8+25	273.6	274.1	274.1	274.1	280.1	280.5	✓
	10.8	10.3	10.1	6.3	4.3	3.9	
		+16	+5	+7		+17	
8+50 P.	3.00	286.56	2.82	281.56			
8+25			284.3	285.1	✓		
			2.3	1.5			
8+50	271.4	271.4	271.4	276.2	279.5	281.0	283.7
	15.2	15.2	15.2	10.4	7.1	5.6	2.9
			+19.0	+16	+18.0		
8+75	274.5	275.9	277.4	277.4	281.4	284.7	286.6 ✓
	12.1	6.7	5.2	1.9	1.9	1.0	
	7.2		+17				
8+91.34	274.7	275.6	279.9	281.8	283.7	283.7	✓
	11.9	11.0	6.7	4.8	1.4	0.9	
				+28			

< 30 >  
 E  
 +15 +16 Concrete Driv 10' 10'  
 P.C. +134 +4 Concrete Drive 4' 1.6'  
 +12 +13 Concrete Driv 1.5' 1.6'  
 +13 +4 Concrete Drive 1.5' 1.6'  
 +14 +5 Concrete Driv 1.7' 1.6'  
 P.C. +14 +5 Concrete Driv + #23 Concrete Wall .7 wide 1.6' 1.8'  
 +16 +18 Concrete Drive - +7 Top Concrete wall 1.6' 1.8'  
 No End fence  
 +17.0 Edge Concrete Drive +16 Top Wall 1.6' 1.8'  
 +21.5 edge garage - Garage 8' W + 12' E of Sta - 1.9' 1.6'  
 P.T. 1.0' 1.5'

286.56

274.7 275.4 280.0 281.9 285.0 ✓  
9+00 11.9 11.2 6.6 4.7 1.6

(K)

1<sup>9</sup>  
1 1<sup>6</sup>

272.7 274.1 279.7 281.8 282.2 284.6 ✓  
9+15.30 13.9 12.5 6.9 4.8 4.4 4.3 2.0  
+5.1 +2.7

PC

1<sup>10</sup>  
1 1<sup>3</sup>

272.7 274.0 279.2 280.3 282.5 284.7 ✓  
9+25 13.9 12.6 7.4 4.3 4.1 4.1 1.8  
+7.1 +2.8

1<sup>10</sup>  
1 1<sup>2</sup>

275.4 275.7 279.8 283.3 283.2 283.3 ✓  
9+50 11.2 10.9 6.8 3.3 3.4 3.3  
+7.1

1<sup>9</sup>  
1

276.5 277.9 282.0 284.1 284.3 286.3 ✓  
9+75 10.1 8.7 4.6 2.5 2.5 2.3 0.3  
+6.1 +2.7

1<sup>9</sup>  
1 1<sup>3</sup>

T.P. 10.69 296.44 0.51 285.75

278.1 279.4 284.6 287.1 287.7 ✓  
9+94.51 18.3 17.0 11.8 11.7 8.7  
+1.8

P.T.

1<sup>3</sup>  
1 1<sup>6</sup>

277.8 281.2 284.0 285.1 286.6 287.5 ✓  
10+00 17.6 15.2 12.4 11.3 11.6 9.8 8.9  
+9.1 +1.8

1<sup>2</sup>  
1 1<sup>7</sup>

279.1 280.3 284.2 285.2 284.9 286.2 287.6 ✓  
10+01.91 17.3 16.1 12.7 11.2 11.0 9.8 8.8  
+7.1 +1.7

P.C.

1<sup>2</sup>  
1 1<sup>7</sup>

281.8 283.7 285.2 286.1 285.6 289.0 289.3 290.1 ✓  
10+25 14.6 12.7 11.2 10.3 10.6 7.4 7.1 6.3  
+1.3 +1.6 +1.8 X

(47.0) stake

1<sup>5</sup>  
1 1<sup>13</sup>

B.M. 3.86 292.58

B.M. 5' off 10+50 Right side Stake

285.2 286.3 289.9 292.1 291.6 ✓  
10+50 10.8 10.1 4.3 4.3 4.8  
+6.7 +8.1

10<sup>0</sup>  
1 1<sup>4</sup>

286.2 288.7 296.44 288.5 291.1 293.7 294.8 ✓  
 10775 10.2 7.7 7.9 5.3 2.7 1.6  
 +2.

288.2 290.8 291.9 291.7 293.4 ✓  
 10798 8.2 5.6 4.5 4.7 1.4  
 +17.0 +3.

288.2 290.8 291.9 291.7 293.4 ✓  
 11100 5.2 5.0 4.5 4.7 1.4  
 +17.0 +3.

289.7 291.9 295.2 295.2 295.8 ✓  
 11725 6.5 4.5 1.2 1.2 0.7  
 +12.0 +7

T.P. 12.83 308.03 1.24 295.20

10798 297.6 297.9 ✓  
 11100 297.6 297.9 ✓  
 11725 301.3 304.1 305.1 ✓  
 6.7 4.9 3.7  
 +10.

291.1 294.7 298.9 299.0 299.5 305.2 306.1 ✓  
 11750 16.9 18.3 7.1 9.0 7.5 2.8 1.7  
 +5. +18.0

293.6 294.3 298.0 301.0 302.8 302.8 307.6 ✓  
 11755 14.4 13.7 10.0 7.0 5.2 5.2 0.4  
 +6. +2.0

297.2 297.9 302.0 304.6 306.6 305.6 307.3 ✓  
 12100 10.5 10.1 6.0 3.4 1.4 2.4 0.7  
 +4. +3.0

T.P. 12.95 320.63 0.35 307.68

303.0 303.3 305.9 309.6 309.7 309.1 314.5 319.8  
 12+25 7.6 17.3 14.7 11.0 10.9 11.5 6.1 1.1  
 +12.4 +16.

50  
 5  
 5  
 1

P.T.

P.T.

15  
 10  
 1  
 1

30  
 1  
 14

40  
 1  
 15  
 10  
 130  
 120

25  
 1  
 14

12+50 308.9 326.23 311.3 ✓  
 117 307.8 312.4 311.3  
 10.8 8.2 91 7.3  
 +13 +8

B.M. 1.09 319.54

12+75 313.5 315.4 318.0 ✓  
 71 55.2 64 77 32 2.6  
 +28 +5+30

13+00 316.3 316.3 315.6 ✓  
 4.3 4.3 5.0  
 +16

T.P. 4.28 323.82 319.54

13+25 318.1 318.0 ✓  
 5.7 5.8

0+00 322.4 322.0 321.9  
 1.4 1.8 1.9  
 +17.0

T.P. 12.94 336.44 0.32 323.50

0+25 326.6 325.2 335.4  
 9.8 10.2 1.0  
 +6

0+50 322.1 323.7 330.2 330.3  
 14.3 10.7 6.2 6.1  
 +13 +75.0

0+66.45 321.1 323.0 333.8 334.6  
 15.3 13.4 2.6 2.4 1.8  
 +22 +17

B.M. Stake 3' off 12+25, right side -

T.P. 12+25

Check this against  
 Balance of Section

1271 50  
 522

3871 7

9

1320  
 500

508.0

T.P. 12+25

169

130.50

310.70



336.41

0+75	320.8	323.4	335.4	335.4
	15.6	13.0	1.0	1.0
		+	+1.9	R

1+00	321.7	324.9		
	14.7	11.5		

T.P.	13.1	348.80	0.64	335.80
------	------	--------	------	--------

1+00	335.8	340.0	339.1	339.5	343.3
	13.1	8.9	9.8	9.4	5.6
		+7.6		+2.0	

1+25	320.1	327.9	338.0	342.9	342.0	344.8
	23.8	21.0	10.9	6.0	6.9	6.9
				+8.0	+2.4	

1+50	330.0	335.1	345.0	345.8	344.4	346.4
	17.9	15.8	39.3	4.5	2.5	
			+2.0	+18.0		

1+75	341.9	344.8		
	7.0	4.1		

T.P.	11.44	359.82	0.52	348.38
------	-------	--------	------	--------

1+75	349.6	348.7	347.4	352.7	352.3	352.1
	10.2	11.1	12.4	7.1	7.5	7.7
	+7.0		+12.0	+16.0	R	

2+00	354.1	353.0	355.5	353.0	352.8
	3.7	3.8	8.5	5.8	6.5
			+11.0	+7.0	

2+25	336.0	336.3	355.4	356.9	353.3	352.8
	3.8	3.5	8.4	3.9	6.5	7.6
			+2.0			

14.9  
8.9  
2.5 3.0 2  
2.5 2.5

19.0

6.0  
123.2

5.0  
121.0

2.0  
127.0

7.0  
12.0

12.0  
12.0

12.0

$2750$      $359.4$      $359.821$      $356.6$      $354.6$      $355.0$      $352.8$   
 $0.4$      $14$      $33$      $52$      $0.8$      $7.0$   
 $+16.$      $+60$

B.M.     $110$      $358.72$

10 ft. back 2+25 left side stake

$12.11$      $331.85$      $319.54$

B.M. 12+25

$12+50$      $316.0$      $317.8$      $319.4$  ✓  
 $13.7$      $13.9$      $13.3$   
 $+13.0$

$12+75$      $319.1$      $322.3$      $323.5$  ✓  
 $13.6$      $9.4$      $8.2$   
 $+5.$

$13+00$      $323.2$      $324.7$      $327.4$      $328.5$  ✓  
 $8.5$      $7.0$      $4.3$      $3.2$   
 $+8.0$

T.P.     $12.98$      $343.06$      $110.7$      $330.08$  ✓

$13+25$      $324.2$      $327.7$      $331.2$      $331.8$  ✓  
 $18.9$      $14.4$      $11.9$      $11.3$   
 $+17$

$0+00$      $327.7$      $331.8$      $336.4$      $335.5$   
 $15.4$      $11.3$      $7.7$      $7.6$   
 $+15.0$

$0+25$      $331.5$      $334.5$      $338.7$      $339.7$   
 $11.6$      $8.6$      $4.7$      $3.4$   
 $+3.0$

$0+50$      $338.0$      $340.4$      $341.6$   
 $5.1$      $2.7$      $1.5$   
 $+12.0$

T.P.     $12.24$      $354.52$      $0.78$      $342.28$

$2.9$   
 $8.9$   
 $9.9$   
 $< 50 >$   
 $16.0$   
 $76.0$

G	PL(L)	E	PL(R)	G
	364.52			
0+66.45			3416	34213
			12.9	12.2
			R	
0+75			339.7	342.8
			14.8	11.7
				11.5
				22.0

T.P. 0:97	364.69		358.72	
357.8	357.5	357.4	354.4	353.1
2+75.97	6.9	7.2	7.3	12.3
				11.6
				R
3100	361.1	358.2	357.1	353.7
	3.6	6.5	6.6	9.0
				10.2
				R
3+25	363.1	362.3	361.8	358.2
	1.6	2.4	2.9	6.5
				6.2
				R
3+50	364.5	360.5	360.4	360.7
	0.2	4.2	4.3	3.9
				5.4
				R
3+66.45	361.4	361.7	362.0	360.5
	3.2	3.0	2.7	4.2
				8.9
				R
3+75	362.2	362.3	362.6	360.3
	2.0	2.4	2.1	4.4
				8.0
				R
4+00			361.7	359.2
			3.0	5.4
				R
T.P. 11.98	375.28	1.39	363.30	

3+50	366.0	265.8
	7.3	10.5

BM Station 2+25

P.R.C. 15.0 30' road

5.0 3.0 ✓

7.7 15.5 ✓

6.7 15.0

P.T. 8.0 5.0 ✓

5.2 6.0 ✓

366.3 375.28  
 3166.25 9.0 264.9 10.4

< 20.7  
 4

B.M. 7.26 368.02

Stake 10' back 3166.48 Leftside -

363.3  
 3175 10.0

364.8 364.4 364.6 364.8  
 4+00 10.2 10.9 10.7 10.5  
 4 +3.0 R

116.0 T 3.0 ✓

364.8 364.4 364.6 364.8  
 #401.49  
 73.0

P.C.

367.7 369.1 367.9 367.0 366.0  
 4+25 7.6 6.2 7.4 8.3 9.3

39.7 T 2.0 ✓

375.1 372.0 371.6 371.8 369.7  
 4+50 0.2 3.3 3.7 3.5 5.6

50.1 T 1.50 ✓

T.P. 10.46 384.11 1.63 373.65

380.9 379.1 379.7 374.1 374.5 374.1  
 4+75 3.2 3.2 10.4 10.0 9.6 10.1  
 382.5 379.4 374.7 374.9 375.0 374.4  
 4+83 1.6 4.7 9.4 9.2 9.1 9.7  
 +4.0

P.B.C.

49.1 T 5.0  
 15.50 ✓  
 T 8.0 ✓

382.7 376.2 376.1 376.3 376.3  
 5+00 1.4 7.9 9.0 7.8 7.8  
 +2.

2.07 T 12.0 ✓  
 1. ✓

382.8 382.2 379.0 378.5  
 5+25 1.3 1.9-6.1 5.1 5.6  
 +3.7 R

1.70 T 8. ✓  
 1. ✓

382.5 380.4 380.7  
 5+50 1.6 3.7 3.4  
 +1

1.3.0 T 1.40 ✓

T+05

384.71  
384.1  
384.4  
T+0.3

T.P. 13.05 396.77 0.39 383.72

5+00 384.5  
12.3

5+25 386.0 385.1  
10.8 11.7

5+50 389.2 388.0 386.5 384.9  
7.6 8.8 10.3 11.9  
+5

5+75 393.4 392.5 391.2 389.5  
5.3 4.2 3.5 7.3  
+5

6+00 396.5 395.3 393.9 389.5 389.1 389.1  
0.3 1.3 2.9 7.2 7.7 7.7  
+5.0

B.M. 2.95 393.82

T.P. 13.01 405.94 3.84 392.93

6+25 394.9 394.7 394.4 393.7 388.2 392.9  
11.0 11.2 11.5 12.2 17.7 13.0  
+7

6+50 396.1 395.0 401.3 398.2 397.2  
9.8 8.3 7.9 4.8 11.6 7.7 8.7  
+4.73

T.P. 11.82 416.28 1.48 404.46

← 30° 7  
+5.0 17 ✓ TC+0.5

15 10.0 ✓ R+90

B.M. stake 10' back 5775 Left.

Left: 6+25 R

8.0 +7 ✓ R+16

24.0 ✓ LAT+75 -]0

40.58

	405.8	405.3	404.0	401.4	400.0
6+75	10.5	11.0	12.3	14.8	16.3

	411.1	411.0	409.7	408.9	408.3
7+00	5.2	5.3	6.6	7.4	7.8

T.P.  
 7+25 12.74 427.74 1.38 414.90

	416.2	416.8	418.5	418.7	418.1
7+25	11.5	10.9	9.2	9.0	9.6

	418.4	419.8	423.0	423.1	425.4
7+50	9.3	7.9	11.7	2.6	2.3

B.M. 1.41 426.33

	416.9	419.7	421.1	424.4
7+75	10.8-8.0 +13.	6.6	3.3	

	419.7	417.8	419.6	421.6	424.7
8+00	10.0	9.9	9.1	5.1	3.8
		+5.0	+2.		

	417.9	421.2	421.6
8+25	9.8	6.5	6.1

	417.8	419.4	424.4
8+50	9.9	8.3	3.3

	422.8	423.1	427.2
8+75	4.9	4.6	0.5

	425.9
9+00	1.8

73

14.3  
11.4

17

15.3 ✓

L-5.0

15.2 ✓

→ L-8.3

P.T.

16.3 ✓

LAT 7+00-47

19 ✓

LAT 7+00+0.0

10ft. Rad. 7+50-R. stake

15.15 ✓  
25.1

R-15.0

R 7+75-11.0

70.15 ✓  
30.1

L 8+95+3.1

15.0 ✓  
30

R 8+50+0.0

15.0 ✓  
40

R 8+75+0.0

T.P. 8.30 434.63 426.33 13.14: 7+50

7+75 427.4 428.8  
7.2 5.8

8+00 424.6 426.6 428.3  
10.0 7.0 6.3  
+3.0

8+25 422.4 427.2  
12.2 7.4

8+50 425.0 424.9  
9.6 9.7

8+75 427.3 427.1  
7.3 7.5

9+00 426.0 426.9 429.3 428.9 428.8  
8.6 7.7 5.1 5.3 5.7 5.8  
+3.0

9+25 426.8 428.2 430.4 430.5 429.9 432.2 433.8  
7.8 6.4 4.2 4.1 4.7 2.4 1.8  
+6. +12-

9+50 428.4 432.1 432.2 432.0 431.9  
6.2 2.5 2.3 2.6 2.7  
+8. +8.

T.P. 9.55 443.46 0.72 433.91

9+75 432.4 434.0 433.9 434.0 436.1  
11.1 9.5 9.6 9.5:7.4  
+4.75

10+00 436.0 436.0 435.5 439.3  
7.5 7.5 8.0 4.2  
+3

2 15° 15°  
3.9 1.5 ✓

6.0 1.5 ✓

8.0 1.5 ✓

Back - 9+50

5.0 1.5 ✓

1.5° 1.5 ✓

10.1  
2  
8.1  
1.57

⊕

443.46  
437.5 437.4 437.4  
10+25 6.0 6.1 6.1

438.9 438.5 438.6 438.4  
10+50 4.6 5.0 4.9 5.1  
+2.

439.6 438.9 438.8 438.9  
10+62.7 3.9 4.6 4.7 4.6  
+3.

439.5 438.9 438.8 438.7  
10+75 4.0 4.6 4.7 4.8  
+5.

438.2 437.0 438.2 438.4 438.2 438.2  
11+00 8.3 6.5 5.0 5.1 5.3 5.3  
+5.

426.1 427.2 434.4 438.4 438.4  
11+25 17.4 16.3 10.9 5.1 5.1

419.7 424.9 432.2 439.0 440.1 440.2  
11+50 23.8 18.6 11.3 3.4 3.4 3.3  
+12.

425.3 427.5 434.3 441.2  
11+75 18.2 16.0 9.2 2.3

429.4 432.1 438.5 443.5  
12+00 14.1 11.4 5.0 7

429.8 433.2 439.2  
12+11.90 13.7 10.3 4.3

432.9 435.6 441.9  
12+25 10.7 8.9 1.6

441.5  
12+50 2.0

P.C

P.R.C

<115° 153  
150° ✓

150° 20° ✓

150° 30° ✓

150° 370° ✓

150° -150° ✓

150° 90° ✓ R 11+25+00

170° ✓ R 11+50+90

170° ✓ R 11+75+00

150° 40° ✓ R 12+00 +18

⊕ R 12+25 +30

R 12+50 +13



443.46

T.P.

1.73

441.73

Stake - 11+75 - R.

T.P.

12.82

446.73

433.91

Ride - 9+50

9+50

434.7  
12.0

436.0

10.7

9+75

434.9  
11.8  
+7

436.5

10.2

437.6

9.1

10+00

439.4  
7.3  
+4

441.5

5.2

442.8

3.9

T.P.

16.48

456.57

1.64

445.09

10+25

445.5  
11.6  
+7

446.6

11.0

445.3

10.1

10+50

446.0  
10.6  
+11

449.2

7.4

450.5

6.1

10+62.67

443.0  
11.6

451.4

5.2

R.L.

10+75

442.9  
13.7

449.9

6.7

T.P.

11.79

453.53

441.73

B.M. - 11+75

11+25

443.9  
9.6

G P E P G

453.52

12+00				446.9	0.6
				444.2	447.7
12+11.9				3.9	3.8
				446.4	448.5
12+25				7.1	3.0
	443.6	446.8	450.6	452.3	
12+50	9.9	6.7	3.9	1.2	

P.R.C

7.0  
116.9 ✓  
1.0  
116.1 ✓  
1.0  
116.1 ✓

T.P. 1173 452.25 3.00 450.52

12+75	445.4	449.5	454.5	453.3	454.2
	13.9	12.8	10.8	9.0	8.1
13+00	454.0	454.9	456.1	455.7	455.3
	8.3	7.4	6.2	6.6	7.6
13+25	457.6	458.2	458.1	456.9	456.4
	11.7	4.1	4.2	5.4	5.9

8.1  
116.1 ✓ R-10  
1.0  
116.1 ✓ R+00  
5.2  
116.1 ✓ R+00

B.M. 7.92 454.33

stake - 15ft left of 13125 left side

13+50	458.1	458.1	457.9	458.0	462.3	462.3
	4.2	4.2	4.4	4.30.2	T	T
				+2-+4		
13+57.24	458.0	458.0	452.2	462.3	462.3	
	4.3	4.3	10.0	0.1	T	T
				7.3		
13+75	458.0	458.2				
	4.3	4.1				

P.R.C

3.0  
112.0 ✓  
5.0  
113.0 ✓  
113.0  
110.0 ✓

$\frac{12.5}{11.4}$     13.0  
 12.14  
 11.4

462.25'

T.P. 10.31 471.92 0.64 467.68

13+75    452.3    464.4    465.3  
           9.6        7.5        6.6

14+00    459.2    458.9    461.8    463.4    467.2  
           13.7    13.5    12.9    10.1    6.5    4.7  
                   +8

14+25    458.9    458.8    460.2    463.7    466.7  
           13.0    13.1    11.7    8.2        5.2

14+50    460.0    460.0    460.9    463.8    465.5  
           11.9    11.9    11.0    7.1        6.4

14+75    461.3    461.7    461.8    464.7    465.8  
           10.6    10.2    10.1    7.7        6.1

15+00    459.2    461.5    464.0    464.0    473.8  
           14.7    10.4    7.9    7.9    7+1.9  
                   +6

15+25    456.4    460.6    466.8    466.3    466.1    466.1    470.3  
           15.5    11.3    5.1    5.6    5.8    5.8    7+3.4  
                   +2                    +12

15+50    456.2    459.2    467.9    467.2    467.5    474.5  
           15.7    12.7    4.0    4.7    4.4    7+2.6  
                   +14

15+75    453.6    457.1    464.5    467.8    467.9    467.7  
           18.3    14.8    7.4    4.1    4.0    4.2  
                   +2

16+00    450.9    453.6    463.6    467.8    467.7    467.4  
           21.0    18.3    8.3    4.1    4.2    4.5  
                   +3

16+25    452.5    455.8    464.9    467.6    467.0    466.8  
           17.4    16.1    7.0    4.3    4.9    5.1  
                   +4

$\frac{11.5}{10.7}$     12.5  
 11.5

$\frac{13.0}{13.0}$     4.0

$\frac{7.0}{7.0}$     7.0

$\frac{3.0}{3.0}$     3.0

$\frac{6.0}{6.0}$     5.0

$\frac{12.0}{12.0}$

$\frac{13.0}{13.0}$

$\frac{2.0}{2.0}$

$\frac{3.0}{3.0}$     3.0

$\frac{4.0}{4.0}$     4.0

471.92 461.4 467.3  
 452.6 453.9 466.9 466.9 466.7  
 16+28 19.3 16.0 7.5 4.4 5.0 4.2  
 +3.1  
 458.5 461.5 466.9 467.3 466.2 466.4 477.5  
 16+30 13.4 10.4 3.0 4.6 5.7 5.3 7 +5.6  
 +3  
 +12.0  
 461.3 466.4 466.2 465.9 477.2  
 16+75 10.6 5.5 3.7 6.0 7.3

T.P. 11.82 478.53 5.19 466.73  
 455.6 458.5 466.2 466.9 466.2 466.2  
 17+00 22.9 20.1 12.4 11.7 12.4 12.4  
 +2.1  
 448.0 452.0 468.9 466.3 467.8 467.3  
 17+25 30.6 26.6 19.7 12.3 10.8 11.3  
 +12  
 447.9 452.6 457.5 463.0 465.2  
 17+50 30.7 28. 21.1 14.6 13.4  
 445.0 459.8 457.2 463.3  
 17+59 33.6 20.8 21.4 19.2  
 Wash  
 443.0 448.4 464.5  
 17+63 43.6 39.2 14.1  
 444.6 466.0  
 17+69 34.0 12.6  
 447.5 449.2 457.9 465.8 467.3  
 17+75 31.1 29.4 20.7 12.8 11.3  
 459.1 457.5 468.0 469.1 469.5  
 18+00 24.5 21.1 15.6 9.5 9.1

11.2  
 13  
 24.2  
 6.1  
 18.1

18.1 +9.8  
 13.1  
 10.1

PRC

30  
 3  
 1.3  
 5.0  
 1.50

89

5  
 13.0

R+32

7.15

8.17

5  
 13.5

R+15

1  
 1.2

R+00

	461.0	462.6	468.7	470.0	470.3	470.2
18725	17.6	16.0	9.9	8.6	8.3	8.4
			+2.			

	461.3	464.3	470.8	470.5	470.4
18730	17.3	14.3	9.6	8.1	8.2

T.P. 9.69 486.97 127 497.28

B.M. 4.86 482.11  
485  
3.

End-

478.65  
Also ~~486.97~~ 481.7 - 481.00 18/12/17

< 30 >

2.0 1 1 3 ✓

1 1 3.0 ✓

50' WIDE

L

LT TO RIGHT

25

650

224.92

B.M. N.E. COR LUDINGTON PROPERTY (HUB)  
COMPLY

	220.1	219.0	231.42	221.6	222.2
0+00	11.3	12.4	12.5	9.8	9.2
	L	5	22	26	TC
	222.9		227.7	228.3	227.0
0+25	8.5		9.2	5.1	4.4
	L		21	26	TC
	225.8		225.4	228.0	230.7
0+50	5.6		6.0	3.4	0.7
	L		21	25	TC
	228.6		228.7	228.0	232.1
0+75	2.8		2.7	3.4	9.9
	L		14	21	26

TP 1090 242.30 0.02 231.40

ROCK

	230.1	231.7	231.9	231.5	233.9	237.2
1+00	12.2	10.6	10.4	10.8	8.4	5.1
	L	4	16	25	28	TC
	238.9		233.9	234.1	234.2	228.7
1+25	3.4		8.4	8.2	8.1	13.0
	R		29	19	9	TC

← REVERSE

34

	230.3	232.2	231.1	231.4	237.3	239.1	240.8
1+50	12.0	10.1	5.2	4.9	5.0	3.2	1.5
	L	5	15	25	36	39	TC

	234.5	237.2	240.3	241.5	244.0	245.2
1+75	7.8	5.1	2.0	1.8	1.0	1.05
	L	13	20	25	41	46

	238.9	244.5	244.0	244.5	244.0	245.5
2	3.4	10.0	10.5	10.0	10.5	8.6
	L	24	25	37	46	TC

TP 12.53 254.45 0.38 241.92

	241.2	248.5	247.5	247.6	247.8
2+25	13.3	6.0	7.0	6.9	6.7
	L	2.5	29	37	TC

2+50	2417 128 L	254.45 2508 54 37 25 30	2506 39 40	2505 40 2513
2+5525	2418 127 L	2517 52 33 25 30	2512 33 40	2513 32 2539
2+75	2426 119 L	2517 28 19 25 32	2530 15 40	2521 24 06 48 2
3+00	2433 110 L	2519 24 7+05 25 30	2545 00 40	2540 95 48
3+0564	2435 110 L	2520 22 25	2507 161 13 21	2567 10.1 94 2574
3+25	2439 86 L	2512 15.6 19	2545 123 10.6 25 28	2562 29 2539 2596
3+50	2521 24 L		2534 134 9.1 16 25	2571 9.1 40 43 2628

4	1267	26684	0.28	254.17
3+75	2466 122 L	2566 102 7.5 15 23	2597 7.1 8.1 32 40	2587 39 43
3+9539	2584 84 L	2607 6.1 63 61 15 25 30	2607 6.7 11 37	2657 11.4 42
4+00	2587 8.1 L	2611 5.7 6.1 58 15 25 29	2610 6.5 0.5 37	2663 10.5 42
4+25	2545 123 L	2556 112 5.1 48 8 18 28	2620 5.1 37 2617 42	2677 118 40

4+50	2528 140 L	26684 2667 46 18	2627 45 25	2627 41 37	261A 54 41	2617 51 R		
4+66.45	PCC. 130 L	2538 34 18	263A 34 25	263A 36 35	2632 51 41	2617 50 R		
4+75	25A3 12.5 L	2633 35 16	2635 33 25	263A 34 33	2627 41 36	2632 36 R		
5+00	2569 8.9 L	2648 20 13	2651 17 21	2649 19 28	265 20 30	2750 285.77 R		
5+25	2648 70 L	2661 124 12	2662 122 14	2666 129 15	2669 126 25	2737 127 29	2755 58 32	2815 40 40
5+50	2671 47 L	2688 10.7 14	2695 100 25	2693 102 32	2705 10 40	2794 283A 64	283A 24 R	
5+62.04	2672 46 L	2681 114 14	2704 91 18	2709 86 30	2708 87 39	2729 66 41	2799 59 45	2822 36 R
5+68.94	2673 33 L	2678 117 14	2708 87 19	2714 81 31	2714 81 40	2831 64 43	2815 43 47	2827 31 R
5+75	2657 16 L	2673 122 11	2712 78 20	2714 81 25	2721 74 33	2712 77 42	2737 58 43	2826 32 R
6+00	R 13.13 114	273 279 46	2746 46 65	2730 60 66	2735 66 33	2762 13 2787	26639 73 R	2885 73 R
6+25	2677 125 L	2707 88 14	27A5 50 25	27A8 41 34	27A4 51 42	2767 28 45	2870 38 46	2829 29 R
6+36.04	2673 122 L	2695 100 8	2752 43 20	2753 42 31	2750 45 40	2806 52 47	2819 40 R	

OLD BOX CULVERT 1.5x2 ADEQUATE



6+50 2681 2701 2794 6A 2759 2782 2812 2823  
 114 2A 36 36 36 76 46 35  
 L 6 7 2A 36 42 46 R

6+75 2714 2768 2776 2787  
 8.1 2.7 2.9 1.4  
 L 9 25 10

7+00

7+01.03 2732 277A 2779 2788 2785 2810 2826  
 6.3 2.1 1.6 0.7 38 43 R  
 L 8W 25 40 38 43 R

7+25 2741 277A 2776 2790 2790 2792 2831 2830  
 5.4 1.6 1.9 6.8 6.5 6.4 2.7 1.8  
 L 7 19 20 31 42 45 R

7+23.62 2740 2750 2778 2795 2798 2798 284A  
 5.1 4.5 1.6 8.0 6.3 6.0 6.0 1.4  
 L 3 9 22 23 36 44 R

7+50 2740 2750 2779 2776 2795 2799 2800 2843  
 5.5 4.3 1.6 8.2 6.3 5.9 5.8 1.5  
 L 10 23 21 37 47 R

7+75 2772 2775 2776 2775 2797 2801 2840  
 7.3 6.2 1.9 8.3 6.1 5.7 1.8  
 L 4 23 25 46 R

8+00 2775 2768 11 2765 279A 280A 280A 284A  
 7.0 2.7 9.0 6.4 5.4 1.9 1.4  
 L 9 21 23 44 47 R

8+10.18 2727 2770 2760 2797 2802 280A 283A 2850  
 6.8 2.5 9.8 6.6 5.6 5.4 2.4 0.8  
 L 6 20 20 26 43 45 R

TR 773 285.77 142 2780A  
 2795 274A 2745 2783 280A 2808 28AA 285A  
 8+25 11.9 11.4 11.3 7.5 5.4 5.0 1.4 0.4  
 L 9 20 20 25 42 44 R

113.7 Ro  
 BACK 6.5 END

6+85 8' L 5' R GARAGE

192 RoFL  
 9.5

101 RoFL  
 9.5

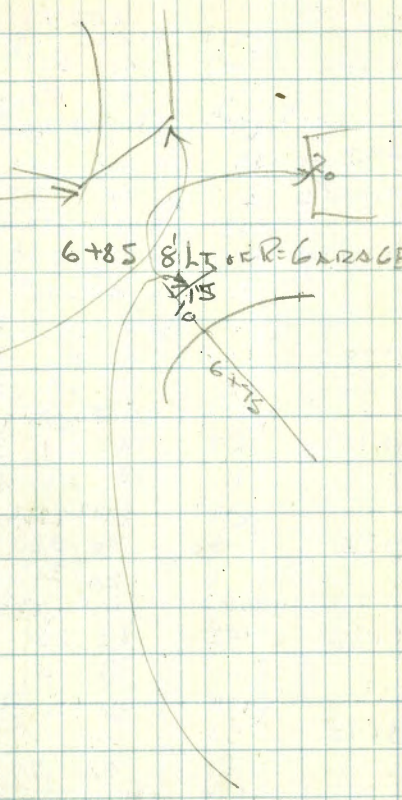
128 RoFL  
 5.5

9.7  
 132 RoFL

GARAGE FLOOR - H1 27946 AT R STA 6+90

117 RoFL  
 10

86 RoFL 10



8+50 2811 2817 28577 2812 2821 2852  
 147 141 5.1 280.1 46 17 06  
 L 10 27 44 45 70

8+75 2809 2809 2848 2850 2817 2817 2851 2858  
 149 149 110 108 46 4.1 07 00  
 GARAGE FLOOR L 4 4 7 29 44 46 70

8+9134 2848 2818 2819 2854 2858  
 109 40 39 87 83  
 L 30 44 47 70

9+00 2850 2806 2815 2822 2822 2846 2851  
 108 52 43 36 36 95 90  
 L 27 29 35 45 47 70

9+1530 2821 2821 2821 2826 2824 2844 2847  
 127 74 37 32 117 97 94  
 L 23 31 40 46 48 70

9+25 2828 2818 2826 2828 2827 2847  
 130 70 32 30 114 94  
 L 24 34 41 48 70

9+50 2856 2835 2835 2833 2846  
 102 63 23 108 95  
 L 23 34 48 70

9+75 2868 2818 2839 2844 2865  
 90 40 19 97 76  
 L 24 29 47 70

9+9451 2816 281A 2848 2849 287A 2850  
 72 44 93 92 67 61  
 L 12 26 24 46 70

10+00 2891 2811 2838 2851 2850 2868 2879  
 67 47 20 90 91 73 62  
 L 9 16 24 43 45 70

TR+ 1263 294.06 43A 28143  
 10+019 149 2797 60 2881  
 L 70

12100LT 91000LT

8 10+25 287.1 294.06 288.9 286.7 289A 291.1  
 12.0 9.2 7.9 4.7 3.0  
 L 8 38 40 R  
 8 10+50 288.5 287A 287.3 290.1 292.8  
 8.6 6.7 6.8 4.0 1.3  
 L 14 31 33 72

291CB.M 287.0 289.7 288.7 1.26 293.80  
 10+75 7.1 4.9 5.4 2.7 291A 12.1 294.7  
 L 6 26 28 72

10+98.87 288A 5.7 8.7 298.1  
 L 292.2 291.8 72  
 11+00 288.3 5.8 1.9 2.3 295.1 11.7 8.4 298A  
 L 9 2.6 28 72

11+25 290.7 3.9 295.3 295.6 300.6 304.3  
 L 11.5 11.2 6.2 2.5  
 11+50 291.3 2.8 295.6 299.1 299.3 305.3  
 L 11.2 7.7 7.5 1.5 307.4  
 1.4 2.1 4.1 4.4 72

TP 1290 306.80 0.16 293.50  
 11+75 293A 295.3 299.5 303.0 307.9 304A  
 12.9 11.5 7.3 3.8 3.9 2.4 307.6  
 L 12 2.2 2.9 4.1 4.6 72

12+00 297A 302.0 306.7 305A 307A  
 9.1 4.8 0.1 0.9 72  
 L 2.1 2.8 4.7 72

TP 10.83 316.77 0.86 305.94  
 12+25 303.0 307.0 310.0 308.6 311.6 315.1  
 13.8 9.8 6.8 8.2 5.2 1.7 317.2  
 L 1.7 2.2 4.1 4.5 4.6 72

	3092	316.77	3125	311A	3160	33546
12+50	76	60	43	54	08	319A
	L	7	12	32	37	16.1
						R
12+75	313A	3146	3133	3176	3188	3204
	34	22	35	116	167.1	5.1
	L	2	19	22	28.29	118
						R

TP	1257	329.24	0.10	316.67		
13+00	3163	316	320.1	320.1	523.1	3287
	129	131	9.1	61	124	68
	L	10	12	14	18	R
13+25	3182	3181	523.1	3208	3276	3320
	11.0	11.1	56	11.7	7.9	11.1
	L	5	7	8	20	7
						R

SECOND LA JOLLA HILLS TP 986 33546 059-334.87

0+00	3225	327A	329.24	331.2	344.73	3365
	6.7	6.8	3206	13.5	9.7	82
	L	9	11	23	39	R
0+25	3267	327.1		3318	3353	3399
	2.5	2.1		12.9	9.4	48
	L	20		23	32	R

ET ANGLE TO ROAD

CHIKTP

0+50	3222	561	373.23	3308	3316	337A	339A	3417
	7.0			13.9	13.1	7.3	5.3	30
	L			12	32	37	42	R
0+66.48	3208			3239	3346	3417		342A
	8.4			10.8	10.1	3.0		23
	L			20	41	45		R
0+75	3212			335A	3350	342A		343.1
	8.2			9.3	9.1	1.8	2.0	16
	L			24	42	48		R
1+00	3218			3402		339A		343)
	7.4			4.5		5.3		16
	L			30		48		R

PIPE IN ROAD COR LOT 71

TP	6.31	33546	0.09	329.15	7
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		34473	3423	3450	
1+25	3752	3430 17	134	107	
	L	31	48	7	
1+50	3303 144	3461	3448	3498	
	L	27	45	47	72
P	1228	35569	132	34341	
1+75	3470 137	3479 78	3475 82	3525 32	3523 34
	L	12	16	36	42
2+00	35A3 14	35A1 16	3515 42	35A6 16	3529 28
	L	8	29	32	7
P	8.50	36417	0.02	35567	
2+25	357A 68	3562 76	35A8 94	3563 79	3533 110
	L	8	24	27	72
2+50	355A 43	3557 55	3575 67	3571 71	35A8 74
	L	5	8	26	32
2+75	3608 34	3581 61	3577 65	35A5 97	3535 107
30	30	30	30	30	30
	L	10	26	35	46
3+00	3605 37	3602 41	3586 56	3587 55	357A 83
	L	7	4	18	25
3+25	3636 06	3621 21	3593 49	3596 46	358A 53
	L	8	9	24	72
3+50	3663 106	36A8 121	3605 37	3611 31	3596 46
	L	6	9	25	72
3+6648	3667 102	3651 118	3616 26	3625 17	3572 70
	L	5	7	22	72

CHANGE TO 30' WIDTH

3+75	3656 113 L	3645 124 3 3	36417 3622 20 6	3631 11 21	3569 73 R
4+00	3651 118 L	3645 120 5	3653 116 19		3596 46 R
4+01.49	365.3 114 L	3645 120 5	365.3 116 19		453597 R
P	13.05	37691	0.31	36286	

CXK.B.M)	3676 93 L	3686 83 3	3683 86 19	853 106 R	36838 3663	=36802	36842
4+25	3755 14 L	3718 51 5	3721 48 24	3700 69 R			
4+50	3767 126 L	3767 83 2	3763 24 10	3766 23 23	3751 18 27	3743 26 R	
4+75	12.14		0.03	37688			

← (2) LEFT READINGS

4+8382	3828 62 L	3817 73 3	38902 3751 139 7	3751 136 27	3748 147 R	
5+00	3848 42 L	3848 64 6	3826 124 13	3766 124 R	3766	
5+25	386A 26 L	3849 41 7	3826 64 18	3782 108 20	10.1 R	3789

	389A	38902	38853	3883A	3809	3810
5+50	120	37	56	81		80
	L	21	24	26		72
	3839	3876	3898			3847 3847
5+75	75	88	116			43 43
	L	12	20			25 72

TP 12.71 0.33 388.69

1 TC OF MARKER 6+00 IN TC

	396A	39A2	40140			3892
6+00	47	72	113			122
	L	9	12			72
	397A	397A				3972
6+25	70	70				72
	L	15				72
	3977	3985		4023		4018
6+50	37	29		108		115
	L	16		22		72
	3996	401A		401A	407A	4091
6+75	18	00		00	59	42
	L	9		16	20	72

TP 1282 090 400.50

	400.5	413.32		402.1	409.5	4108
6+8076	128	112		112	38	25
	L	12		18	22	72
	4067	4067	4037	4057		4130
7+00	71	71	86	81	93	
	L	3	5	25	72	
	4058	4087	4088	4077	4085	
7+25	75	46	45	56	48	
	L	8	12	14	72	
	4050	411A	411A	4108	25	4108
7+45.16	83	19	19	25	25	72
	L	13	15	16	72	

7+50	4053 8.0 L	41332 4116 17 13	41211 12 15	411A 19 18	411A 19 TC
7+75	4061 7.2 L	4099 34 11	4152 9.1 2.0	4150 9.2 TC	418A
8+00	403A 5.9 L	4076 5.7 10	413 11.2 2.2	5.9 TC	41A.2
8+25	4053 8.0 L	4076 5.7 10		10.1 TC	
8+50	4119 1.4 L	4154 8.9 1.5			4181 6.2 TC
TR	12.55		1.60		411.72
8+75	4206 3.7 TC	424.27 26 1.5	4217		423.5 0.8 TC
9+00	4227 1.6 L	4247 12.1 1.8			427.3 9.5 TC
TR	13.17	4367.5	0.69		423.58
9+25	4226 1.42 L	4260 10.8 1.6			429.1 7.7 R
9+50	4238 1.30 L	4269 9.9 1.4	4308 6.2 2.5	4327 2.8 TC	4328 41.40 TC
9+75	4305 6.3 L	4320 4.8 5	4322 3.6 1.6	43A.8 2.0 2.1	43A.8 2.0 TC



	A32A	A362	A367.5	A36.5	A362
10+00	34	06	03		06
	L	11	25		7c
IP	12.70		0.19		436.56
	A358	A370	429.26	A378	A388
10+25	134	123	A382	11.5	10.5
	L	3	11.1	29	7c
	A370	A393	A389	A385	AA01
10+50	123	100	104	104	82
	L	9	15	27	7c
	A371	A389	A393	A389	AA08
10+75	122	104	100	104	85
	L	5	9	27	7c
	A327	A378	A387	A386	AA10
10+9308	156	115	106	107	83
	L	6	9	27	7c
	A33A	A373	A384	A383	A385
11+00	155	120	109	110	108
	L	6	10	15	27
	A326	A381	A388	A385	A361
11+25	167	112	105	108	132
	L	8	11	26	7c
	A35A	A398	AA01	AA03	AA13
11+50	139	95	92	88	80
	L	7	15	27	7c
	A386	A428	AA35	A500	A6109
11+75	107	65	58	11.1	
	L	6	25	7c	
	AA07	AA63	AA61	A51A	
12+00	86	30	32	9.1	
	L	9	26	7c	
	AAAT	A501	A501	A503	A520
12+25	16	110	110	108	71
	L	10	17	27	7c

	117.8	449.26	AS3.7	
\$R+3867	1.5	AS1.7 94 AS1.8 93	74	
	L	9 27	R	
TP	1228	461.09	0.45	448.81
12+50	AAA.5 116 L	AS2.8 83 AS3.7 74 S 5	AS3.3 78 AS5.0 61 R 28 R	
12+75	AS6.5 46 L	AS7.0 41 AS6.1 50 17	AS5.8 53 26	460.7 R
13+00	AS9.5 16 L	AS8.7 24 AS8.1 30 21	462.9 10.7 24	463.9 R
13+25	460.6 0.5 L	AS9.9 12 17	464.2 94 20	465.0 86 R

P	12.98		0.43	458.66
13+50		473.64 AS9.8 138 L 17	464.4 92 21	465.4 8.2 R
13+59.21	460.1 135 L	460.1 135 463.8 98 16 20	465.4 8.2 R	⊗
13+75	460.3 133 L	460.5 13.1 462.6 11.0 18 22	464.9 8.7 R	
14+00	460.9 127 L	460.8 12.8 460.5 13.1 15 21	463.8 98 R	
14+25	462.1 115 L	462.0 11.2 462.3 11.3 15 24	463.6 10.0 R	

TURN OVER 3 PAGES

	4628	4626	4633	4650
14+3695	108	110	103	86
	L	20	26	TC
14+50	109	99	99	82
	L	3	21	23
14+75	106	80	78	81
	L	4	12	20
15+00	112	56	59	82
	L	2	18	22
15+25	109	108	109	114
	L	1	14	20
15+50	109	109	109	130
	L	14	17	TC
15+75	109	109	109	136
	L	1	14	19
16+00	109	109	109	150
	L	13	17	TC
16+1166	109	109	109	158
	L	12	16	TC
R	12.18	12.18	0.45	473.19
R	12.03	12.03	0.65	484.72

17+000 LD

R

12.96

0.86 473.30

485.26

9.72

4.42 484.84

491.56

6.50 485.06

B.7)

46284

11.32

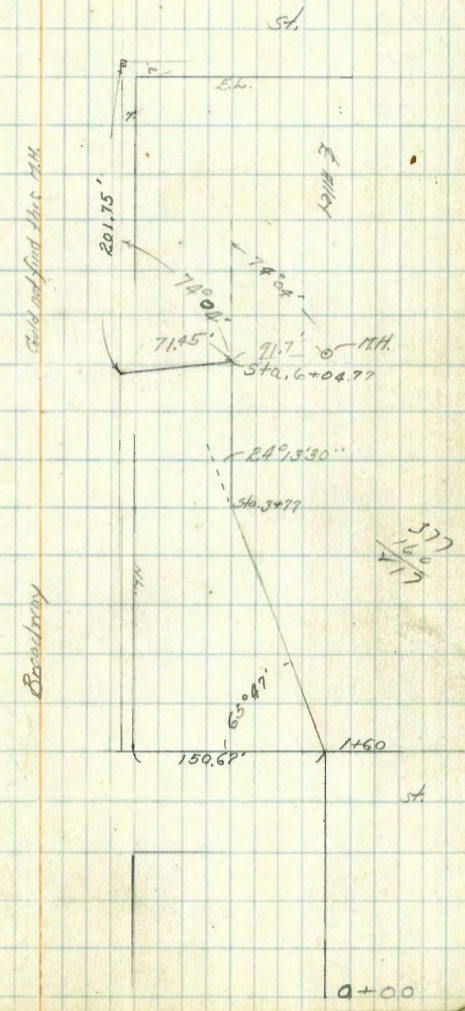
472.16

467.4

Preliminary Levels for Sewer.

Bet. Bdry. + E. bet. 30<sup>th</sup> + 29<sup>th</sup> St.

Station	9.82	204.90	9 204 2.7	195.08 194.1 ✓	SE. BR Bdry + 30 <sup>th</sup>
100' E. E.L. 30 <sup>th</sup> = 2+00					
+ 50			8.5	196.4 ✓	
1+00 = E.L. 30 <sup>th</sup> top of road			10.66	194.2 ✓	
+ 50 = top of ch			11.49	193.4 ✓	
1+60 = A			11.6	193.5 ✓	
T.P.	0.83	193.64	12.29	192.81	
1+70			12.9 192.6	186.2 ✓	
T.P.	0.81	182.19	12.26	181.38	
1+97			12.2 183.3	168.9 ✓	
2+23			16.8	165.4 ✓	
+ 47			14.2	168.0 ✓	
+ 57			11.6	170.6 ✓	
T.P.	1.50	120.94	12.75	169.41	
3+20			17.9 2.1	168.8 ✓	
Left 30' = Home of Gulch			14.4	156.5 ✓	
3+77 = Δ R 24° 13' 30"			8.46	164.6 ✓	
4+00			7.1	163.8 ✓	
4+30			10.2	160.7 ✓	
Left 25' = Bottom of Gulch			15.3	155.6 ✓	
T.P.	0.43	158.73	12.64	158.30	
4+85			15.7 3.9	154.6 ✓	
5+05			6.8	151.9 ✓	
5+20			11.2	147.5 ✓	
+ 50			12.0	146.7 ✓	
+ 90			11.3	147.4 ✓	



Cont. from preceding page

40

		158.73	<del>158.73</del>	
5+95			9.1	149.6 ✓
6+04.77 = top of Pipe			12.66	146.0 ✓
M.H. in Alley N. of Bldg. Floor line			12.55	
T.P.	11.52	170.14	0.11	158.62
T.P.	10.83	180.71	0.26	169.88
T.P.	10.33	190.94	0.10	180.61
T.P.	9.88	198.48	2.34	188.60
			3.39	195.09
				195.09 = BM
				0.01

RE-X SECTIONS HILLSIDE DR. IN LA

JOLLA HILLS #2

13959.27

10.00 47360 46360

1230 46360

Lt Rt

14+10.66PC	<u>461.3</u> 12.3 0	<u>461.2</u> 12.4 R	<u>461.3</u> 12.3 23	<u>463.0</u> 19.6 30	
+25	<u>462.2</u> 11.4 0	<u>462.0</u> 11.6 R	<u>462.1</u> 11.5 21	<u>463.6</u> 10.0 30	
+50	<u>461.4</u> 12.2 0	<u>462.7</u> 9.9 6	<u>463.5</u> 10.1 R	<u>463.8</u> 9.8 2.6	<u>465.2</u> 7.9 27
+75	<u>458.6</u> 15.0 0	<u>465.5</u> 8.1 9	<u>466.3</u> 7.9 R	<u>465.4</u> 7.8 2.8	<u>471.7</u> 2.5 30

47590	
1222	0.31
48781	
1313	0.51
500.43	
440	12.37
49246	488.06

15	<u>461.2</u> 11.9 0	<u>468.0</u> 5.6 8	<u>462.2</u> 5.9 R	<u>462.8</u> 5.8 2.5	<u>481.2</u> 6.6 30	48781
----	---------------------------	--------------------------	--------------------------	----------------------------	---------------------------	-------

+25	<u>463.2</u> 10.4 0	<u>469.8</u> 3.8 9	<u>469.3</u> 4.3 2.2	<u>485.1</u> 15.3 2.7	<u>482.3</u> 13.1 30	500.43
-----	---------------------------	--------------------------	----------------------------	-----------------------------	----------------------------	--------

+50	<u>463.8</u> 9.8 0	<u>470.7</u> 3.5 8	<u>469.9</u> 3.7 2.2	<u>484.3</u> 15.9 2.4	<u>482.3</u> 13.1 30
-----	--------------------------	--------------------------	----------------------------	-----------------------------	----------------------------

+75	<u>464.1</u> 9.5 0	<u>470.0</u> 3.4 7	<u>469.8</u> 3.8 2.2	<u>484.0</u> 16.4 2.5	<u>482.5</u> 13.2 30
-----	--------------------------	--------------------------	----------------------------	-----------------------------	----------------------------

16	<u>467.8</u> 5.8 0	<u>469.5</u> 4.1 2	<u>468.4</u> 4.2 R	<u>480.6</u> 19.8 1.9	<u>489.5</u> 10.6 30
----	--------------------------	--------------------------	--------------------------	-----------------------------	----------------------------

+25	<u>468.2</u> 4.3 0	<u>469.2</u> 4.4 1.1	<u>480.1</u> 12.4 1.2	<u>482.5</u> 9.9 R	<u>492.9</u> 7.5 30
-----	--------------------------	----------------------------	-----------------------------	--------------------------	---------------------------

CONT.

LT

47360

49246

50043

16+3196PRC

4692 4697  
44 44

4817 4833  
10.8 92

492.3  
7.1

0 10

12 k

30

+50

4691 4697  
45 43

4818 4825  
10.7 10.0

491.2  
9.2

0 11

13 k

30

+75

4692 4695  
44 41

4832  
9.3

487.6  
12.8

0 6

21

30

PR

531

353

47002

47533

17

4698 4697  
6.5 5.6

470.1  
5.2

470.0  
4.7

0 2

k

30

+25

4617 4643  
13.6 11.0

471.0  
4.3

470.8  
4.5

470.8  
4.5

0 3

k

30

40

+50

460.7  
14.6

4688  
6.5

471.3  
4.0

471.9  
3.4

472.3  
3.0

0 10

k

30

45

+7262

466.7 471.5 471.2  
8.6 3.8 3.6

471.7 472.7 473.7  
3.6 2.6 1.6

2.5 3.0

4.5

0 8

k

2.5

3.0

+75

467.4 471.5 471.5  
7.9 3.8 3.8

471.3 473.0  
4.0 2.3

2.5

3.0

0 7

k

2.5

3.0

+8377¢

469.4 470.7 470.8  
5.9 4.6 4.5

473.8 478.2  
1.5 1.6

2.6 3.0

3.0

0 3

2.3

2.6

3.0

+9269

469.9 4688 4689  
5.4 5.4 5.4

474.8 474.5 475.5  
0.4 0.8 0.0

1.7 2.1

3.0 4.2

0 k

1.7

2.1

3.0 4.2

CAMP S.L. LA JOLLA HILLS #2

X section Sapphire St.

From R.R. to Cass St.  
B.M. Pole by RR track north of Lawrence 70.90

	+	x	-		+	-	
T.P.	928	80.18		70.90	$\frac{1}{4}$	13.6	84.5
T.P.	1235	90.53	2.00	78.18	2	13.8	84.3
T.P.	896	98.09	1.40	89.13	$\frac{1}{4}$	16.4	81.7
	15' cbs 10' quarters				+5	15.3	82.8
0+00	= End of Sapphire St. taken on diag.				cb	15.2	82.9
N.L.		12.0	86.1		SL	18.9	79.2
cb		12.2	85.9		+10		
$\frac{1}{4}$		12.3	85.8		SL-10	26.0	76.1
2		12.4	85.7		SL	27.0	77.1
$\frac{1}{4}$		12.6	85.5		cb	23.1	75.0
+3		12.6	85.5		$\frac{1}{4}$	19.2	78.9
cb		14.3	83.8		2	16.8	81.3
SL		14.3	83.8		$\frac{1}{4}$	16.5	81.6
0+91 <sup>20</sup> = R+Ls to		Sapphire			+5	16.7	81.4
SL		14.3	83.8		cb	13.2	84.9
cb		14.0	84.1		+10	12.0	86.0
$\frac{1}{4}$		12.7	85.4		N.L.	9.0	89.1
2		12.1	86.0		+10	9.0	89.1
$\frac{1}{4}$		11.6	86.5		+45		
cb		11.3	86.8		N.L.	12.5	85.6
N.L.		11.1	87.0		cb	18.6	79.5
0+90					$\frac{1}{4}$	22.6	75.5
N.L.		9.3	88.8		2	26.5	71.6
+6		9.5	88.6		$\frac{1}{4}$	29.2	68.9
cb		12.5	85.6		cb	37.7	60.4

Stations run in on N. line



22 245  
125  
14.

	+	π 98.09	-		+	π 98.09	-
SL			38.3	59.8	+5		37.0 61.1
+25			38.8	59.3	cb		37.4 60.7
1+80					$\frac{1}{4}$		37.0 61.1
SL-25			36.8	61.3	+3		30.6 61.5
SL			36.3	61.8	+5		33.7 64.4
cb			37.2	60.9	$\frac{1}{4}$		33.0 65.1
$\frac{1}{4}$			32.4	65.7	2		30.8 67.3
2			29.2	68.9	$\frac{1}{4}$		29.1 69.0
$\frac{1}{4}$			23.3	74.8	cb		27.2 70.9
cb			12.8	80.3	NL		24.3 73.8
NL			12.2	85.9	+10		21.0 77.1
2+00					2+70		
NL			18.9	79.7	NL -10		32.9 65.2
cb			24.3	73.8	NL		33.0 65.1
$\frac{1}{4}$			26.7	71.4	cb		33.4 64.7
2			28.9	69.2	$\frac{1}{4}$		33.8 64.3
$\frac{1}{4}$			33.0	65.1	2		34A 63.7
cb			35.5	62.6	$\frac{1}{4}$		35.4 62.7
+1			37.8	60.3	cb		35A 62.7
SL			37.6	60.5	SL		34.9 63.2
+10			34.0	64.1	+15		34.1 64.0
2+30					+25		30.1 68.0
SL-10			30.5	67.6	2+85		
SL			34.0	64.1	SL-15 = top of bluff		25.1 73.0
+3			34.0	64.1			

	+	$\pi$ 98.09	-	
SL			29.7	68.4
cb			28.9	69.2
$\frac{1}{4}$			28.6	69.5
$\frac{1}{2}$			28.4	69.7
$\frac{1}{4}$			27.8	70.3
cb			27.6	70.5
NL			27.7	70.4
+15			27.0	71.1
3700				
NL-10			25.4	72.7
NL			26.5	72.6
cb			27.0	71.1
$\frac{1}{4}$			27.0	71.1
$\frac{1}{2}$			27.3	70.8
$\frac{1}{4}$			27.4	70.7
cb			27.2	70.9
SL			27.0	71.1
+8			25.9	72.2
+16			5.7	92.4
3+15				
SL-5			5.1	93.0
SL			5.1	93.0
cb			12.1	76.0
$\frac{1}{4}$			19.4	78.7
$\frac{1}{2}$			19.4	78.7

	+	$\pi$ 98.09	-	
$\frac{1}{4}$			21.8	76.3
cb			22.2	75.9
NL			21.0	77.1
+5			19.0	79.1
3+40				
NL-10			7.9	90.2
NL			7.7	90.4
+8			7.1	91.0
+14			3.3	94.8
cb			3.1	95.0
$\frac{1}{4}$			3.1	95.0
$\frac{1}{2}$			3.4	94.7
$\frac{1}{4}$			3.4	94.7
cb			3.7	94.4
SL			3.4	94.7
4+25				
T.P.	6.10	103.09 <sup>1</sup>	4.10	96.99
SL			7.0	96.1
cb			6.5	96.6
$\frac{1}{4}$			6.1	97.0
$\frac{1}{2}$			5.8	97.3
$\frac{1}{4}$			5.4	97.7
cb			5.1	98.0
NL			4.8	98.3
4+75				

	+	T 10309	-		+	T 10899	-	
NL			3.5	99.6	cb		2.8	100.3
cb			4.1	99.0	$\frac{1}{4}$		2.5	100.6
$\frac{1}{4}$			4.3	98.8	$\frac{1}{4}$		2.3	100.8
$\frac{1}{4}$			4.5	98.6	$\frac{1}{4}$		1.8	101.3
$\frac{1}{4}$			5.1	98.0	cb		1.5	101.6
cb			5.1	98.0	NL		1.0	102.1
SL			5.5	97.6	1+00			
5+27 <sup>6</sup>	= NL	Allison			NL		0.5	102.6
SL			4.7	98.4	cb		1.1	102.0
cb			4.2	98.9	$\frac{1}{4}$		1.4	101.7
$\frac{1}{4}$			3.8	99.3	$\frac{1}{4}$		1.6	101.5
$\frac{1}{4}$			3.4	99.7	$\frac{1}{4}$		2.0	101.1
$\frac{1}{4}$			3.1	100.0	cb		2.3	100.8
cb			2.7	100.4	SL		2.4	100.7
NL			2.1	100.7	T.P.	7.43	108.92'	1.60
0+00	= EL	Allison			1+50			
NL			1.5	101.6	SL		7.5	101.4
cb			1.8	101.3	cb		7.0	101.9
$\frac{1}{4}$			2.2	100.9	$\frac{1}{4}$		6.4	102.5
$\frac{1}{4}$			2.8	100.3	$\frac{1}{4}$		6.0	102.9
$\frac{1}{4}$			3.2	100.9	$\frac{1}{4}$		5.8	103.1
cb			3.5	99.6	cb		5.6	103.3
SL			4.1	99.0	NL		4.7	104.2
0+50					2+00			
SL			3.2	99.9	NL		3.8	105.1

	+	$\bar{x}$ 10892	-	
cb			4.0	104.9
$\frac{1}{4}$			4.6	104.3
$\frac{1}{4}$			5.2	103.7
$\frac{1}{4}$			5.7	103.2
cb			6.2	102.7
SL			7.7	101.2
2+50				
SL			6.3	102.6
cb			5.6	103.3
$\frac{1}{4}$			5.2	103.7
$\frac{1}{4}$			4.8	104.1
$\frac{1}{4}$			4.5	104.4
cb			4.1	104.8
NL			3.5	105.4
3+00				
NL			2.5	106.4
cb			3.0	105.9
$\frac{1}{4}$			3.5	105.4
$\frac{1}{4}$			3.8	105.1
$\frac{1}{4}$			4.3	104.6
cb			4.8	104.1
SL			5.2	103.7
3+00				
SL			4.8	104.1
cb			4.3	104.6

	+	$\bar{x}$ 10892	-	
$\frac{1}{4}$			4.0	104.9
$\frac{1}{4}$			3.7	105.2
$\frac{1}{4}$			3.3	105.6
cb			3.1	105.8
NL			2.4	106.5
3+85				
NL			1.8	107.1
cb			2.7	106.2
$\frac{1}{4}$			3.2	105.7
$\frac{1}{4}$			3.5	105.4
$\frac{1}{4}$			3.8	105.1
cb			4.2	104.7
SL			4.7	104.2
4+12				
SL			4.7	104.2
cb			4.1	104.8
$\frac{1}{4}$			3.7	105.2
$\frac{1}{4}$			3.7	105.2
$\frac{1}{4}$			3.5	105.4
cb			3.0	105.9
NL			2.8	106.1
4+28				
NL			1.4	107.5
cb			2.2	106.7
$\frac{1}{4}$			3.0	105.9

	+	$\pi$ 108.92	-	
Q			3.5	105 4
$\frac{1}{4}$			4.0	104 9
cb			4.5	104 4
SL			4.9	104 0
4+80				
SL			3.4	105 5
cb			2.8	106 1
$\frac{1}{4}$			2.2	106 7
Q			1.8	107 1
$\frac{1}{4}$			1.3	107 6
cb			0.9	108 0
NL			0.5	108 4
T.P.	10.07	116.94	2.05	106.87
5+50				
NL			5.6	111 3
cb			6.3	110 6
$\frac{1}{4}$			6.9	110 9
Q			7.4	109 5
$\frac{1}{4}$			7.8	109 1
cb			8.4	108 5
SL			9.2	107 7
6+00				
SL			8.0	108 9
cb			7.0	109 9
$\frac{1}{4}$			6.5	110 4

	+	$\pi$ 116.94	-	
Q			5.8	111.1
$\frac{1}{4}$			5.2	111.7
cb			4.6	112.3
NL			3.7	113.2
6+50				
NL			2.6	114.3
cb			3.5	113.4
$\frac{1}{4}$			3.8	113.1
Q			4.2	112.7
$\frac{1}{4}$			4.9	112.0
cb			5.3	111.6
SL			5.3	111.6
7+05 <sup>20</sup>	= NL Bayard			
SL			5.2	111.7
cb			4.5	112.4
$\frac{1}{4}$			4.3	112.4
Q			4.0	112.9
$\frac{1}{4}$			3.4	113.5
cb			3.1	113.8
SL			2.2	114.7
Q Bayard				
NL			1.5	115.4
cb			2.4	114.5
$\frac{1}{4}$			2.9	114.0
Q			3.3	113.6

	+	$\pi$	-	
$\frac{1}{4}$		116.94	4.1	112.8
cb			4.4	112.5
SL			4.9	112.0
0+00	= EL	Bayard		
SL			4.2	112.7
cb			3.9	113.0
$\frac{1}{4}$			3.3	113.6
$\frac{1}{4}$			2.6	114.3
$\frac{1}{4}$			2.1	114.8
cb			1.8	115.1
NL			0.8	116.1
TR	893	124.94	0.93	116.01
0+50 NL			7.3	117.6
cb			8.5	116.4
$\frac{1}{4}$			8.5	116.4
$\frac{1}{4}$			9.1	115.8
$\frac{1}{4}$			9.5	115.4
cb			10.3	114.6
SL			10.5	114.4
1+00				
SL			10.1	114.8
cb			9.6	115.3
$\frac{1}{4}$			9.1	115.8
$\frac{1}{4}$			8.5	116.4
$\frac{1}{4}$			8.3	116.6

	+	$\pi$	-	
cb		124.94	8.0	116.9
NL			7.4	117.5
1+50				
NL			6.8	118.1
cb			7.6	117.3
$\frac{1}{4}$			7.7	117.2
$\frac{1}{4}$			8.0	116.9
$\frac{1}{4}$			8.5	116.4
cb			9.0	115.9
SL			10.2	114.7
2+00				
SL			7.7	117.2
cb			7.5	117.4
$\frac{1}{4}$			7.2	117.7
$\frac{1}{4}$			6.4	118.5
$\frac{1}{4}$			6.3	118.6
cb			6.3	118.6
NL			5.5	119.4
2+50				
NL			4.1	120.8
cb			5.5	119.4
$\frac{1}{4}$			5.4	119.5
$\frac{1}{4}$			5.1	119.8
$\frac{1}{4}$			5.1	119.8
cb			5.7	119.2

	+	$\bar{x}$	-
SL		124.94	6.4
2+75			118 5
SL-15			9.4
SL			7.2
cb			5.7
$\frac{1}{4}$			5.2
$\frac{1}{4}$			5.0
$\frac{1}{4}$			4.2
cb			4.1
NL			3.8
3+00			
NL			2.7
cb			3.5
$\frac{1}{4}$			4.2
$\frac{1}{4}$			4.5
$\frac{1}{4}$			5.0
cb			5.2
SL			6.6
+10			8.0
3+50			
SL			5.8
cb			4.7
$\frac{1}{4}$			3.5
$\frac{1}{4}$			3.1
$\frac{1}{4}$			2.6

	+	$\bar{x}$	-
cb		124.94	2.6
NL			1.7
3+79 <sup>2</sup>			= NL Cass St
NL			0.9
cb			1.9
$\frac{1}{4}$			2.1
$\frac{1}{4}$			2.2
$\frac{1}{4}$			2.5
cb			3.6
SL			4.7
+23' = Edge of graded strip west of			
paring.			
SL			4.0
cb			3.5
$\frac{1}{4}$			3.1
$\frac{1}{4}$			2.8
$\frac{1}{4}$			2.1
cb			1.6
NL			1.0
+30' = Edge of pavement			
NL			0.76
cb			1.35
$\frac{1}{4}$			1.75
$\frac{1}{4}$			2.15
$\frac{1}{4}$			2.54

1/11/28

X Section Noyes St  
Garnet to Diamond

MoHug 51

	+	X	-	
cb		124.94	2.93	122.01
S.L			3.59	121.35
T.P	0.87	119.21	6.60	118.34
T.R			14.95	104.26

Check on T.R in Tourmaline E110429

104.26  
104.29  
0.02

B.N. Noyes + Garnet N.W. B.P. 62.02

0+00 = NL Garnet

+ 5.65 67.67 62.02  
20' obs 10' quarters

0+00		
WL	5.2	62.5
Top of Ch.	5.74	61.93
Gut	5.8	61.9
1/4	6.4	61.3
1/2	6.4	61.3
3/4	7.1	60.6
Tip of cb	7.71	59.96
EL	7.6	60.1
0+08 = 3' palm tree 12' in street on West		
EL	7.7	60.0
cb	7.1	60.6
1/4	6.8	60.9
1/2	6.2	61.5
3/4	6.0	61.7
+8	5.8	61.9
cb	4.8	62.9
+5	3.0	64.7
WL	2.3	65.4
0+50		
WL	1.7	66.0
cb	3.7	64.0
1/4	5.1	62.6



	+	π 67.67	-	
℄			5.4	623
$\frac{1}{4}$			5.3	624
cb			6.1	616
+3			7.5	602
EL			8.2	595
1+00 =	4' Palm	12' in street	on West	
EL			7.6	601
cb			6.9	608
$\frac{1}{4}$			5.0	627
+2			4.5	632
℄			4.4	633
$\frac{1}{4}$			4.3	634
cb			4.0	637
WL			3.8	639
1+50				
WL			4.3	634
cb			4.1	636
$\frac{1}{4}$			4.4	633
℄			4.9	628
$\frac{1}{4}$			5.5	622
cb			5.6	621
EL			5.7	620
1+68 =	3' Palm tree	12' in street	on west	
1+95 =	3' "	" " "	" " "	
2+00				

	+	π 67.67	-	
EL			4.1	636
cb			3.9	638
$\frac{1}{4}$			3.8	639
℄			3.8	639
$\frac{1}{4}$			3.6	641
cb			3.5	642
WL			3.3	644
2+50				
WL			2.0	657
cb			2.4	653
$\frac{1}{4}$			2.3	654
℄			2.5	652
$\frac{1}{4}$			2.3	654
cb			2.3	654
EL			2.6	651
2+70 =	3L	Felspar st.		
EL			2.5	652
cb			2.1	656
$\frac{1}{4}$			2.0	657
℄			1.8	659
$\frac{1}{4}$			1.8	659
cb			2.0	657
WL			0.4	673
T.P.	10.13	7627	1.53	6614
curb line				

	+	T 76.27	-		+	T 76.27	-	
NL			9.2	671			8.8	685
cb			9.7	666			9.1	672
$\frac{1}{4}$			9.7	666			9.0	673
$\frac{1}{4}$			9.8	665			8.9	674
$\frac{1}{4}$			9.7	666			8.8	675
cb			10.1	662			8.4	679
EL			11.3	650				
quarter							8.2	681
EL			11.3	650			8.7	676
cb			9.8	665			8.7	676
$\frac{1}{4}$			9.4	669			8.9	674
$\frac{1}{4}$			9.6	667			9.1	672
$\frac{1}{4}$			9.4	669			9.3	670
cb			9.6	667			12.7	636
NL			9.0	673			7.4	689
center line								
NL			8.6	677			9.6	667
cb			9.1	672			11.4	649
$\frac{1}{4}$			9.1	672			9.5	668
$\frac{1}{4}$			9.3	670			8.9	674
$\frac{1}{4}$			9.5	668			8.7	674
cb			9.8	665			8.4	679
EL			11.5	648			8.1	682
quarter							8.3	680
EL			12.2	641			7.8	685

0+00 = NL Fal spar = First of row of Evergreen trees  
on EAST Line

	±	π 76.27	-
0+50			
WL			6.2 70 1
cb			6.7 69 6
$\frac{1}{4}$			7.4 68 9
$\frac{1}{4}$			7.6 68 7
$\frac{1}{4}$			8.0 68 3
cb			8.3 68 0
EL			8.4 67 9
1+00			
EL			7.4 68 9
cb			7.1 69 2
$\frac{1}{4}$			7.1 69 2
$\frac{1}{4}$			7.0 69 3
$\frac{1}{4}$			6.8 69 5
cb			6.1 70 2
WL			5.4 70 7
1+50			
WL			4.6 71 7
cb.			5.1 71 2
$\frac{1}{4}$			5.3 71 0
$\frac{1}{4}$			5.1 71 0
$\frac{1}{4}$			5.3 71 0
cb			5.4 70 9
EL			5.5 70 8
2+00			

	±	π 76.27	-
EL			3.6 72 7
cb			3.5 72 8
$\frac{1}{4}$			3.7 72 6
$\frac{1}{4}$			3.3 73 0
$\frac{1}{4}$			3.4 72 9
cb			2.7 73 6
WL			2.6 73 7
2+50 = End of Evergreen grove on East			
WL			0.8 75 5 <sup>line</sup>
cb			1.7 74 6
$\frac{1}{4}$			1.4 76 9
$\frac{1}{4}$			1.8 74 5
$\frac{1}{4}$			1.8 74 5
cb			2.4 73 9
EL			3.1 73 2
TP	11.52	86.12	1.67 74.60
2+70 = SL Emerald St			
EL			12.4 73 7
cb			12.0 73 1
$\frac{1}{4}$			11.1 75 0
$\frac{1}{4}$			11.0 75 1
$\frac{1}{4}$			10.6 75 5
cb			10.5 75 6
WL			10.1 76 0
Curb line			

	+	$\pi$ 86.12	-
WL	TOP of END of curb 10.07		
cb			76 05
$\frac{1}{4}$		10.7	75 4
$\frac{1}{4}$		10.8	75 3
$\frac{1}{4}$		10.2	75 9
$\frac{1}{4}$		10.1	76 0
cb		10.8	75 3
EL		10.9	75 2

Quarter

EL		10.4	75 7
cb		10.8	75 3
$\frac{1}{4}$		10.0	76 0
$\frac{1}{4}$		10.0	76 0
$\frac{1}{4}$		10.3	75 8
cb		10.4	75 7
WL		10.0	76 1

Center line

WL		9.7	76 4
cb		10.1	76 0
$\frac{1}{4}$		10.1	76 0
$\frac{1}{4}$		9.9	76 2
$\frac{1}{4}$		9.6	76 5
cb		10.4	75 7
EL		9.0	76 5

Quarter

EL		9.4	76 7
----	--	-----	------

	+	$\pi$ 86.12	-
cb			76 1
$\frac{1}{4}$		9.4	76 7
$\frac{1}{4}$		9.6	76 5
$\frac{1}{4}$		10.0	76 1
cb		9.8	76 3
WL		9.4	76 7

Curb Line

WL		8.66	77 46
+1		9.2	76 9
cb		9.4	76 7
$\frac{1}{4}$		9.4	76 7
$\frac{1}{4}$		9.2	76 9
$\frac{1}{4}$		9.2	76 9
cb		9.4	76 7
EL		9.0	77 1

0+00 = N.L. Emerald

EL		8.0	78 1
cb		8.8	77 3
$\frac{1}{4}$		8.5	77 6
$\frac{1}{4}$		8.6	77 5
$\frac{1}{4}$		8.4	77 7
cb		8.2	77 9
WL		8.2	77 9
0+50			
WL		6.3	79 8

	+	T 86.12	-		+	T 86.12	-	
cb			6.3	79 8	EL		2.4	837
$\frac{1}{4}$			6.6	79 5	cb		3.2	829
2			7.0	79 1	$\frac{1}{4}$		2.2	839
$\frac{1}{4}$			6.7	79 4	2		2.9	837
cb			7.2	78 9	$\frac{1}{4}$		2.1	840
+3			6.4	79 7	+5		1.8	843
EL			6.5	79 6	WL		0.0	861
1+00					T.P.	12.77	9794	0.95
EL			5.5	80 6	2+50			
+17			5.2	80 9	WL		9.7	882
cb			5.9	80 2	cb		11.4	865
$\frac{1}{4}$			5.2	80 9	$\frac{1}{4}$		12.8	851
2			5.5	80 6	2		12.1	858
$\frac{1}{4}$			5.0	81 1	$\frac{1}{4}$		11.6	863
cb			4.8	81 3	+5		10.8	871
WL			5.1	81 0	+6		9.6	883
1+50					cb		9.3	886
WL			3.9	82 2	EL		7.6	903
cb			3.7	82 4	2+70 = S.L. DIAMOND			
$\frac{1}{4}$			4.1	82 0	EL		4.7	932
2			4.4	81 7	cb		7.1	908
$\frac{1}{4}$			3.8	82 3	+3		7.7	902
cb			4.5	81 6	+5		10.8	871
EL			4.5	81 6	$\frac{1}{4}$		11.2	867
2+00					2		11.4	867

X section Emerald  
Noyes to Olney

57  
McHugh  
11/28

20' cbs, 10' quarters

0+00 = W.L. Olney

H.L. continued from preceding page

	+	X	-	
$\frac{1}{4}$		97.99	12.2	857
cb			10.1	878
WL			10.9	875

+	X	-
	86.42	

+30' = Edge of Pavement

WL		10.91	8763	
cb		10.64	8730	
$\frac{1}{4}$		10.67	8727	
2		10.50	8744	
$\frac{1}{4}$		10.34	8760	
cb		10.05	8789	
FL		9.48	8846	
T.P.	0.32	86.42	11.84	8610

0+00

WL	13.3	731
cb	13.6	728
$\frac{1}{4}$	13.6	728
2	14.9	715
$\frac{1}{4}$	13.4	730
cb	13.1	733
SL	13.3	731

0+25

SL	12.5	749
cb	11.9	745
$\frac{1}{4}$	11.9	745
2	12.1	743
$\frac{1}{4}$	13.1	733
cb	12.7	737
WL	12.6	738

0+75

WL	10.3	761
cb	10.2	762
$\frac{1}{4}$	10.0	764
2	9.8	766
$\frac{1}{4}$	9.7	767

	+	T	-	
cb		86.42	10.1	76 3
SL			11.0	75 4
1+25				
SL			11.0	75 4
cb			10.2	76 2
$\frac{1}{4}$			9.8	76 6
$\frac{1}{4}$			9.3	77 1
$\frac{1}{4}$			9.1	77 3
cb			9.0	76 4
NL			8.8	77 6
1+75				
NL			7.3	79 1
cb			7.6	78 8
$\frac{1}{4}$			7.7	78 7
$\frac{1}{4}$			7.8	78 6
$\frac{1}{4}$			7.7	78 7
cb			7.9	78 5
SL			8.7	77 7
2+25				
SL			7.6	78 8
cb			6.7	79 7
$\frac{1}{4}$			6.2	80 2
$\frac{1}{4}$			6.1	80 3
$\frac{1}{4}$			5.9	80 5
cb			5.7	80 7

	+	T	-	
NL		86.42	5.6	80 8
2+75				
NL			3.6	82 8
cb			4.2	82 2
$\frac{1}{4}$			4.9	81 5
$\frac{1}{4}$			5.1	81 3
$\frac{1}{4}$			6.0	80 4
cb			6.6	79 8
SL			8.0	78 4
3+25				
SL			10.6	75 8
cb			7.5	78 9
$\frac{1}{4}$			6.1	80 3
$\frac{1}{4}$			5.0	81 4
$\frac{1}{4}$			3.8	82 6
cb			3.1	83 3
NL			2.4	84 0
3+75				
NL			2.4	84 0
cb			2.9	83 5
$\frac{1}{4}$			3.6	82 8
$\frac{1}{4}$			4.0	82 4
$\frac{1}{4}$			5.1	81 3
cb			7.2	79 2
SL			9.7	76 7

	+	T. 86.42	-		T.P.	+	π	-	
4+25					5+00 = FL NOYES	0.18	77.80 ✓	885	77.62 ✓
SL			10.7	757	NL	0.4			774
CB			8.3	781	CB			0.6	772
+8			7.4	790	$\frac{1}{4}$			1.0	768
$\frac{1}{4}$			6.1	803	♀			1.4	764
♀			4.7	817	$\frac{1}{4}$			1.9	759
$\frac{1}{4}$			4.6	818	CB			2.5	753
CB			3.6	828	SL			4.0	738
NL			2.4	840	T.P.	0.13	67.89 ✓	10.04	67.76
4+50					T.P.			5.85	62.04 ✓
NL			3.4	830	BM				
CB			4.5	819					
$\frac{1}{4}$			6.7	797					
♀			7.0	794					
$\frac{1}{4}$			8.0	784					
CB			9.3	771					
SL			10.5	759					
4+75	= 6 Eucalyptus trees on SL.								
SL			12.1	743					
CB			10.7	757					
$\frac{1}{4}$			10.1	763					
♀			9.3	771					
$\frac{1}{4}$			8.7	777					
CB			7.8	786					
NL			5.1	813					

BM  $\frac{6204}{6202}$   
 $\frac{6204}{6202}$   
 .02



Mohagh  
Vilist

X section Felspar St  
Morrell to Olney

B.M. N.W. BR Garnet + Morrell 6630

T.P. 7.92 7.22 66.30

0+00 = E.L. Morrell  
20' cbs 10' quarters

0+00			
SL	3.1	71 1	
Top of curb	3.32	70 90	
+1	4.1	70 1	
$\frac{1}{4}$	3.3	70 9	
$\frac{1}{2}$	2.8	71 4	
$\frac{3}{4}$	2.8	71 4	
Gwt.	2.6	71 6	
Top of curb	2.00	72 2	
NL	1.2	73 0	
0+50			
NL	2.3	71 9	
cb	3.2	71 0	
$\frac{1}{4}$	3.6	70 6	
$\frac{1}{2}$	3.7	70 5	
$\frac{3}{4}$	4.0	70 2	
cb	4.3	69 9	
SL	6.4	67 8	
1+00			
SL	5.3	68 9	
cb	4.1	70 1	
$\frac{1}{4}$	3.9	70 3	
$\frac{1}{2}$	3.5	70 7	

60

	+	T	-	
$\frac{1}{4}$		74.22	34	70 8
cb			2.6	71 6
NL			2.3	71 9
1+23 =	$\frac{1}{2}$		0.14	cement walk on North 2' back
1+45 =	$\frac{1}{2}$		0.15	" driveway on North 5' "
1+50				
NL			0.6	73 6
cb			1.3	72 9
$\frac{1}{4}$			1.6	72 6
$\frac{1}{2}$			1.7	72 5
$\frac{3}{4}$			1.8	72 4
cb			2.2	72 0
+2			1.3	72 9
SL			2.0	72 2
2+00				
SL			1.3	72 9
cb			1.4	72 8
$\frac{1}{4}$			1.7	72 5
$\frac{1}{2}$			1.5	72 7
$\frac{3}{4}$			1.9	72 3
cb			2.0	72 2
NL			1.6	72 6
T.P.	2.66	75.45	1.43	72.79
2+50				
NL			2.6	72 8

	+	$\bar{x}$ 75.45	-	
cb			3.6	71 8
$\frac{1}{4}$			4.1	71 3
$\frac{1}{4}$			4.2	71 2
$\frac{1}{4}$			4.2	71 2
cb			4.6	74 8
SL			5.7	69 7
3+00				
SL			2.0	73 4
cb			2.4	73 0
+2			3.7	71 7
$\frac{1}{4}$			3.2	72 2
$\frac{1}{4}$			2.9	72 5
$\frac{1}{4}$			2.9	72 5
cb			2.4	73 0
NL			1.9	73 5
3+50				
NL			4.3	71 1
cb			4.7	70 7
$\frac{1}{4}$			4.8	70 6
$\frac{1}{4}$			4.8	70 6
$\frac{1}{4}$			4.8	70 6
cb			5.0	70 4
+2			4.4	71 0
SL			4.2	71 2
4+00				

	+	$\bar{x}$ 75.45	-	
SL			6.9	68 5
cb			6.8	68 6
$\frac{1}{4}$			6.3	69 1
$\frac{1}{4}$			6.1	69 3
$\frac{1}{4}$			5.8	69 6
cb			5.7	69 7
NL			5.1	70 3
4+50				
NL			5.8	69 6
cb			6.4	69 0
$\frac{1}{4}$			6.5	68 9
$\frac{1}{4}$			6.8	68 6
$\frac{1}{4}$			6.9	68 5
cb			7.7	67 7
SL			7.5	67 9
5+00 = NL Noyes				
SL			8.3	67 1
cb			8.1	67 0
$\frac{1}{4}$			8.0	67 4
$\frac{1}{4}$			7.7	67 7
$\frac{1}{4}$			7.6	67 8
cb			7.9	68 0
NL			7.0	68 4
0+00 = EL Noyes				
NL			9.0	66 4

	+	$\Sigma$	-	
cb		75.15	10.7	647
$\frac{1}{4}$			12.0	634
Q			10.7	647
$\frac{1}{4}$			10.5	649
cb			10.4	650
SL			10.3	651
T.P.	296	6840	10.01	65.49
0+30				
SL-20			4.8	636
SL			6.8	616
cb			4.7	637
$\frac{1}{4}$			4.1	643
Q			3.7	647
$\frac{1}{4}$			3.6	648
cb			3.4	650
NL			2.9	655
0+50				
NL			4.1	643
cb			4.1	643
$\frac{1}{4}$			3.9	645
Q			4.1	643
$\frac{1}{4}$			4.2	642
cb			4.5	639
SL			5.4	630
1+00				

	+	$\Sigma$	-	
SL		68.90	6.4	620
cb			6.1	623
$\frac{1}{4}$			6.1	623
Q			5.7	627
$\frac{1}{4}$			5.9	630
cb			5.1	633
NL			4.9	635
1+50				
NL			5.9	625
cb			6.8	616
$\frac{1}{4}$			7.4	610
Q			8.6	598
$\frac{1}{4}$			7.2	612
cb			7.2	612
SL			7.2	612
2+00				
SL-15			10.0	584
SL			10.5	579
+5			10.7	577
cb			8.8	595
$\frac{1}{4}$			8.5	595
Q			8.6	598
$\frac{1}{4}$			8.7	597
cb			8.2	602
NL			6.4	620

	+	X 68.40	-		+	X 68.40	-
2+50				SL			11.2 572
NL			2.8 656	cb			10.3 581
cb			4.2 642	$\frac{1}{4}$			9.6 588
$\frac{1}{4}$			5.3 631	2			8.9 595
2			6.1 623	$\frac{1}{4}$			7.8 606
$\frac{1}{4}$			7.3 611	cb			7.1 613
cb			8.3 601	NL			5.4 630
SL			9.6 588	4+50 = Palm tree on N. line			
3+00				NL			9.6 586
SL			10.6 578	cb			11.3 571
cb			8.8 596	$\frac{1}{4}$			11.6 568
$\frac{1}{4}$			7.8 606	2			12.4 560
2			6.5 619	$\frac{1}{4}$			12.9 555
$\frac{1}{4}$			4.9 635	cb			13.9 545
cb			3.6 648	SL			15.3 531
NL			1.4 670	TP 1.88 157.49 ✓			12.79 55.61
3+50				5+00 = Wk Olney			
NL			3.1 653	SL			7.3 502
cb			4.0 644	cb			6.7 508
$\frac{1}{4}$			4.6 638	$\frac{1}{4}$			5.9 516
2			5.6 628	2			5.1 524
$\frac{1}{4}$			6.8 616	$\frac{1}{4}$			4.4 531
cb			7.8 606	cb			3.5 540
SL			9.7 587	NL			1.5 560
4+00				T.P.			12.32 45.17

BM NW B.P. Olney + Garnet  
 El. 45.17  
 0.07

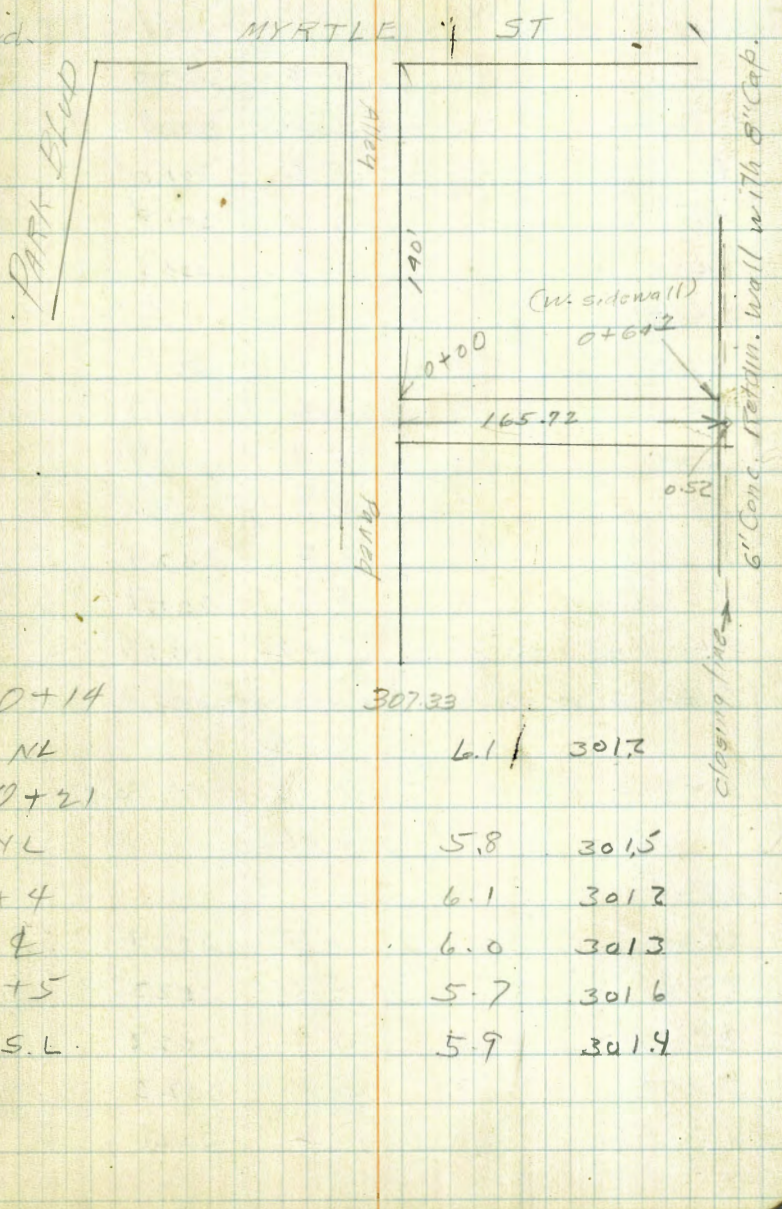
Cross-section E-W Alley BIK 246 Univ. Hts

May 31-28  
Lourton  
Isbell  
Morgan 64

B.M	5.33	391.13	295.80
T.P.	7.64	307.33	1.44
0+00 = EL N-S Alley			
S.L.	Pav.	7.33	300.00
±	Pav	7.45	299.90
N.L.		7.23	300.10
0+00 W end 4 car garage 3.6' N			
		5.65	301.7
0+31 E end same garage 3.8' N			
		5.64	301.7
0+03			
N.L.		6.2	301.1
+2		6.6	300.7
+5		6.8	300.5
+7		6.7	300.6
±		7.0	300.3
+3		6.8	300.5
+8		6.8	300.5
S.L.		6.9	300.7
0+14			
S.L.		6.3	301.0
+9		6.2	301.1
±		6.3	301.0
+3		6.2	301.1
+5		6.3	301.0

Platted 6/16/28  
T.G.H.

B.P.S.W  
NE 1/2 Park Blvd.



0+14  
NL  
0+21  
NL  
+4  
±  
+5  
S.L.

307.33  
6.1 | 301.3  
5.8 301.5  
6.1 301.2  
6.0 301.3  
5.7 301.6  
5.9 301.4

Alley - 246 - U.H.  
H.I.  
307.33

0+30

S.L.	5.5	3018
+3	5.3	3020
+7	5.4	3019
♀	5.6	3017
+5	5.8	3015
N.L.	5.8	3015

0+36

N.L.	5.6	3017
+5	5.6	3017
♀	5.4	3019
+1	5.3	3020
+6	5.2	3021
+9	5.6	3017
S.L. side door on sl.	5.52	3018

0+43 W end 3 Car garage 0.2 in on South  
4.82

0+71 E end Same garage 0.2 in  
4.81

0+47

S.L.	4.9	3024
+8	5.0	3023
♀	5.1	3022
+3	5.0	3023
N.L.	5.2	3021

307.33

0+57 W end 2 car garage 4' N conc. floor  
4.69

0+77 E end Same garage 0.2' N  
4.62

0+68

N.L.	4.7	3026
+3	4.7	3026
+6	4.8	3025
♀	4.7	3026
+1	4.6	3027
+3	4.5	3028
+7	4.8	3025
S.L.	4.9	3024

T.P 5.21 309.91 4.63 302.70

0+80 ♀ single garage 6.8' S. Conc floor  
5.14

0+80

S.L.	5.3	3026
+6	5.3	3026
+7	5.2	3027
♀	5.2	3027
+5	5.3	3026
N.L.	5.1	3028

Alley 296 - U.H.

66

1+04

307.91

N.L.	5.3	3026
+2	5.2	3027
+7	5.3	3026
¢	5.3	3026
+2	5.2	3027
+5	5.4	3025
S.L.	5.2	3027

1+10

S.L.	5.1	3028
+6	5.2	3027
+2	5.1	3028
¢	4.8	3031
+4	4.6	3033
+6	5.0	3029
N.L.	5.1	3028

1+15

N.L.	5.1	3028
+4	5.1	3028
+6	5.1	3028
¢	5.2	3027
+5	5.2	3027
S.L.	5.2	3027

307.91

1+18 went 4 car garage 4.6' N Conc floor  
4.85

1+61 Fend Same Garage 4.2 N  
4.85

1+25

S.L.	5.2	3027
+4	5.4	3025
+8	5.1	3028
¢	5.1	3028
+3	5.1	3028
+6	5.1	3028
+8	4.6	3033
N.L.	4.8	3031

1+33

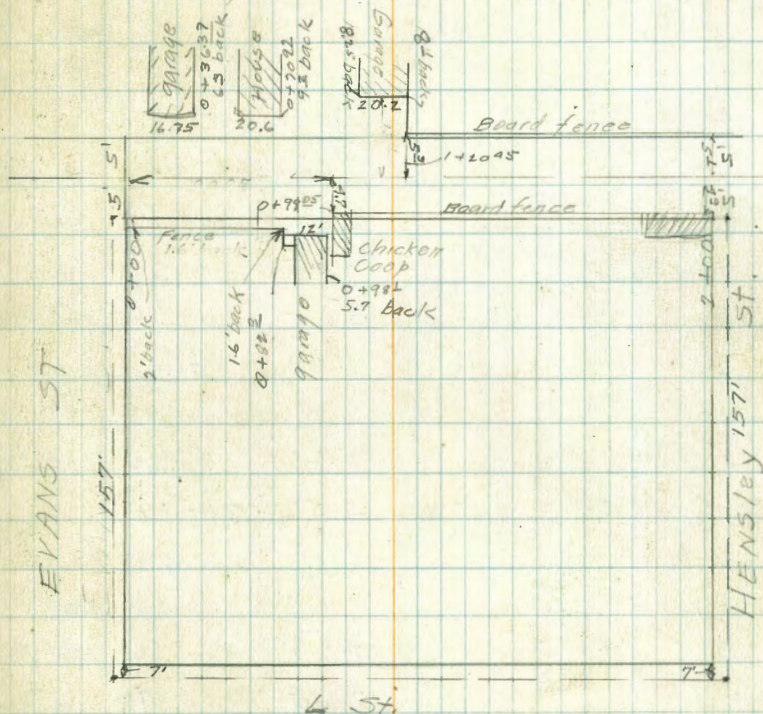
N.L.	4.3	3036
+4	4.5	3034
+6	5.2	3027
¢	5.4	3025
+1	5.6	3023
+3	5.5	3024
+4	5.4	3025
S.L.	5.5	3024

Alley 246 - U.H.

1+48	307.91		
S.L.	5.3	3026	
+5	5.4	3025	
±	5.0	3029	
+3	5.0	3029	
+6	5.2	3027	
N.L.	4.7	3032	
1+57			
N.L.	4.8	3031	
+1	4.5	3039	
+2	4.7	3032	
+4	6.1	3018	
±	6.3	3016	
+6	6.0	3019	
+7	5.4	3025	
S.L.	5.3	3026	
1+60			
S.L.	5.4	3025	
±	6.1	3018	
+6	6.2	3017	
N.L.	6.4	3015	
1+647 = W. edge Retaining wall			
N.L. top wall	8.56	2993.5	
± top wall	8.68	2992.3	
S.L. top wall	8.76	2991.5	

67

307.91  
 T.P. 2.91 301.73 7.09 300.82  
 B.M. Beginning 5.93 295.80



Location of Buildings  
 in alley rear of lots D & E  
 BIK 219.

Jun. 1-28

London  
 Morgan  
 T. S. Bell



## Grade Stakes Alley

BIR 189 U.H.T.S.

Jun 1-28  
Loudon

68

B.M.	6 38	304.86		298.48	3w Hendricks & Richmond	
T.P	2.90	305.79	1.97	302.89		
W				3.02	302.77	
E				2.80	302.99	
4				5.13	302.66	
E			3.87	301.92	302.22	F 0.30
W			3.69	302.10	302.08	C 0.02
W			4.05	301.74	301.38	C 0.36
E			3.65	302.14	301.46	C 0.68
E			4.33	301.46	300.70	C 0.76
W			4.86	300.93	300.70	C 0.23
W	L		5.27	300.52	300.50	C 0.22
T.P	5.67	305.89	5.57	300.22		
E			5.17	300.92	300.50	C 0.42
E	L		4.61	301.28	300.45	C 0.83
E			5.23	300.66	300.37	C 0.27
S			5.68	300.29	300.20	C 0.09
N			5.86	300.03	299.90	C 0.13
N			6.06	299.83	299.70	C 0.13
S			6.29	299.61	299.99	F 0.38
S			5.84	300.05	299.78	C 0.27
N			6.25	299.64	299.58	C 0.06
S			4.95	300.94	299.35	C 1.59
T.P	4.87	304.64	6.12	299.77		
			5.15	299.49	299.28	C 0.21

304.64

S	4.92	299.72	298.89	00.83
N	5.48	299.16	299.00	00.16
	5.89	298.75		
	6.14	298.50		
±	6.38	298.26		

298.75  
299.16  
299.00  
298.69  
298.32

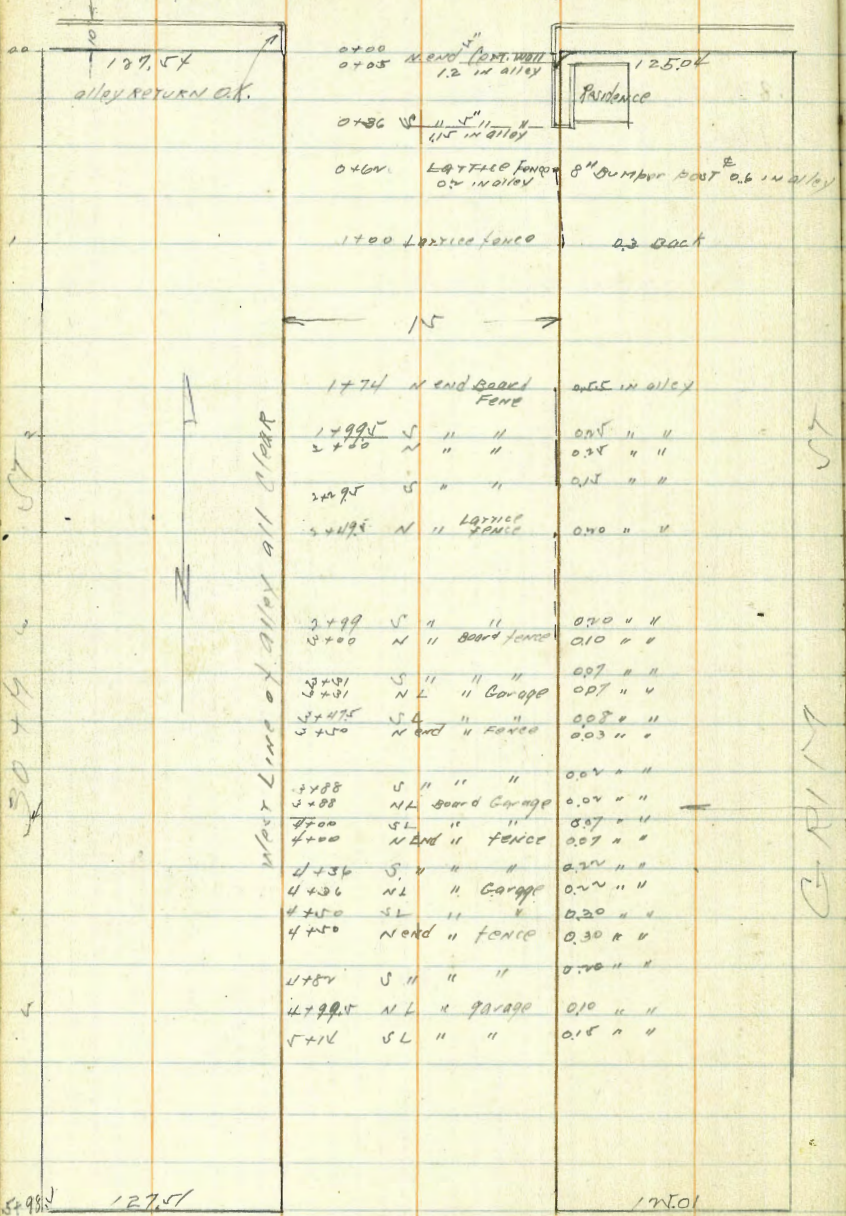
298  
299

69

Location of Signs in Annex Bix & Frary Hqts  
THORN

EAST ALLEY RETURN ST  
1.20 IN ALLEY

MOORE  
OSBORNE  
PEARCE 8/30/48



EAVERs of Residence over hang in alley edge of 5' cement wall  
west edge foundation at 0.9' back alley line  
" " " 0.74 0.70 " " "

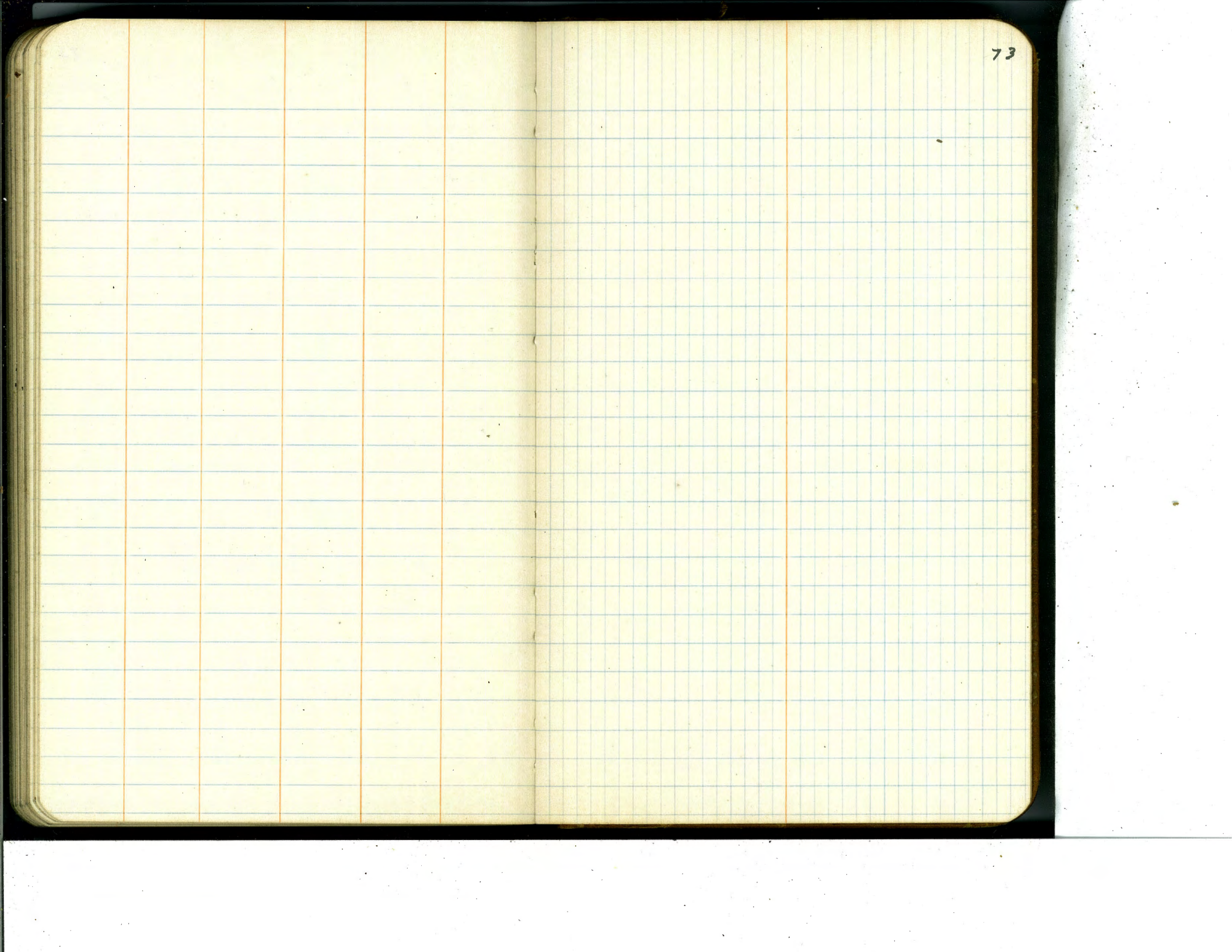
Mr. Froburg 4.3136 GRANT ST has survey  
by Loebenstein showing lat depth of  
126.30. evidently, erroneously placing alley  
IN CENTER of Block

Garage door 7.6 wide & garage, overhangs in alley side  
" " 8' " " " " 0.45'

5498 127.57 RedWOOD  
121.01 ST













## ALBERTA PLACE

5373

76

NL

2+40	197.20	197.10 ✓
+60	197.48 ✓	197.56 ✓
+80	197.52 ✓	197.74 ✓
3	197.30 ✓	197.65 ✓
+20	196.86 ✓	197.27 ✓
+40	196.15 ✓	196.62 ✓
+60	195.20	195.70 ✓
4	193.07	193.57
+43.67	190.74	191.24

201.61	201.61
197.2	197.48
<u>4.41</u>	<u>4.13</u>

201.61	201.61	201.61
197.52	197.30	196.82
<u>4.09</u>	<u>4.31</u>	<u>4.79</u>

201.61	201.61	201.61	201.61
196.15	195.20	193.07	190.74
<u>5.46</u>	<u>6.41</u>	<u>8.54</u>	<u>10.87</u>

193.33	201.32	201.32
7.99	197.56	197.74
XI = <u>101.3</u> ✓	<u>3.76</u>	<u>3.58</u>
197.10		

201.32	201.32	201.32
197.65	197.27	196.62
<u>3.67</u>	<u>4.05</u>	<u>4.70</u>
38	35	

3	201.32	201.32
	195.70	193.57
	<u>5.62</u>	<u>7.75</u>

201.32
191.24
<u>10.08</u>

	S		N	
		20000		
0	660	19340	667	19333
+25	640	19360	635	19365
+50	613	19387	600	19400
+75	583	19417	575	19425
1	547	19453	544	19456
+25	518	19487	506	19494
+50	<sup>+50</sup> 485	19515	475	19525
+75	448	19552	414	19586
2+00 - 125	407 <sup>(49)</sup>	19593	357 <sup>P</sup>	19643
			365	19635
2+00	40	19600		
+25	37	19630		
TP	592		357	19643
		20235		
2+00		141	62	1962
+25			58	1966
+50	53	197.1	50	1974
+75	49	197.5	49	197.5
3	49	197.5	52	197.2
+25	5.1	1973	5.6	196.8
+50	5.7	196.7	6.7	195.7
+75	7.1	195.3	7.9	194.5
4	8.2	194.2	9.0	193.4
+25	10.3	192.9	10.6	191.8
+43	11.4	191.0	11.8	190.6

141 = 198.25 = ELEV.  $\phi$ TR

$$\begin{array}{r} 193.33 \\ 793 \\ \hline HI \ 201.26 \\ 533 \\ \hline P \ \checkmark \ 19593 \\ 568 \\ \hline HI \ 201.61 \end{array}$$

The image shows an open notebook with two facing pages. Both pages are cream-colored and feature light blue horizontal ruling. The left page is divided into five vertical columns by four orange margin lines. The right page is divided into two vertical columns by one orange margin line. The notebook is bound in the center, and the pages are slightly aged. The number '78' is written in the top right corner of the right page.

Diamond + Lammont	SWBW	105.95	
Noyes + Carmet	NW	62.02	79
Carnet + Olney	NW	45.10	
" Murtell	NW	66.30	



