

1233

1233

EASTMAN

FIELD BOOK

No. 385

1233

8851

36 ✓
40 ✓
51 ✓
59

No. 210 opp 80 7/16/20 AH

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CITY OF SAN DIEGO,
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762 in opp 80 7/16/20 AH

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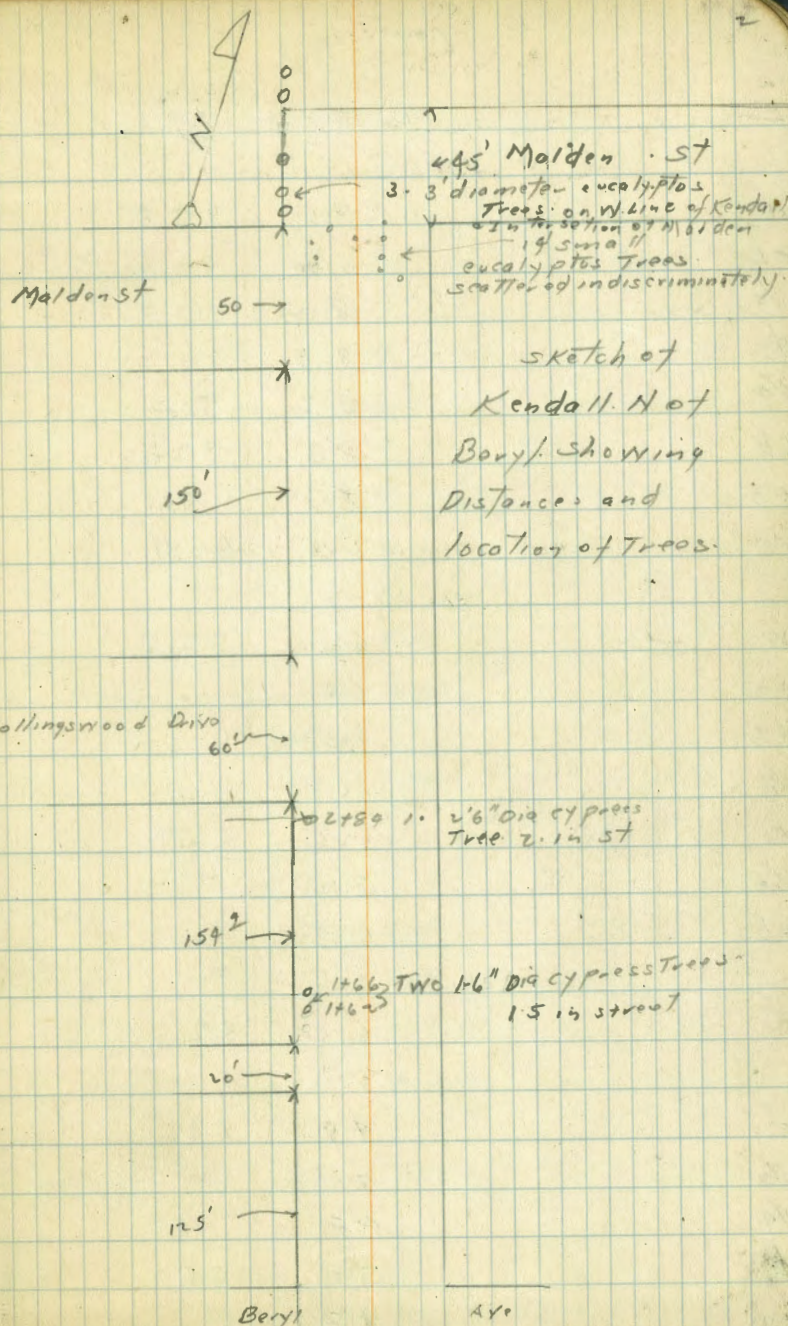
Congress Hts & C.M. Doty's Addition
Pacific Beach

- X-sections Kendall Blvd to N. end 2-9
- X-sections Malden St from Kendall to Wend 10-16
- X-sections Malden St from Kendall to Belmont 17-22
- X-sections Collingswood Drive from Kendall to E
Line of Colina Street. 23-27
- X Montecito Front to 4th
- X sec Sutter St Pringle to 218' South 28
- X sec Keating St Neale to Sutter 32
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- " " Neptune Place 72-78
- Levels in Alley, Bk 34 Pk. Villas 81
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Bliss
 1/1-8 X section Kendall St from the
 North line of Beryl to North end 50' st
 B.M. Spike + - Elev 10 cbs
 in Tree NW 177.54 175.97 75 1/4 S
 Beryl's Kendall
 # Intersection of Beryl taken in 740
 X section of Beryl 0+00 = N line of Beryl.

W	1.6	75.9
cb	1.9	75.6
1/4	1.7	75.8
1/4	1.6	75.9
1/4	2.5	75.0
cb	2.6	74.9
E	3.1	74.4
T.P.	13.09	189.04
	12' N	1.59
		175.95
E	13.0	76.0
cb	13.3	75.7
1/4	13.2	75.8
1/4	12.7	76.3
1/4	12.9	76.1
cb	12.8	76.2
W	12.8	76.2
	32' North	
W	11.7	77.3
+5	11.5	77.5
cb	11.9	77.1
1/4	11.6	77.4
1/4	11.5	77.5
1/4	11.5	77.5
cb	11.8	77.2

Profile plotted
 by Tolman 2-11-29



189.04

189.04

3

E 11.9 77.1
75' N

E 8.5 80.5
cb 8.8 80.2

1/4 8.2 80.8
E 8.3 80.7

1/4 8.7 80.3
cb 8.8 80.2

+5 9.1 79.9
W 8.3 80.7

100' North

W 6.5 82.5
+5 6.9

cb 6.5
1/4 6.4

E 6.3 82.7
1/4 6.2

cb 6.3
+5 6.8

E 6.2 82.8

115' N

E 4.9 84.1
cb 5.1

1/4 4.9
E 5.0 84.0

+2 4.8

1/4 5.1
cb 5.1

+3 5.0
W 5.1 83.9

125' N. S. Line of Alley on West

W 4.0 85.0
cb 4.4

1/4 4.3
E 4.1 84.9

1/4 4.2
cb 4.4

E 4.4 84.6
E + 20 ft Garage on E Corner of 7.68

145' N

E 2.9 86.1
cb 2.5

1/4 2.9
E 2.4 86.6

1/4 2.4
cb 2.9

+4 2.2
W 2.2 86.8

159' N

W 0.7 88.3
+3 0.6

cb 1.2

18904

200.55

4

1/4			1.2		cb	9.8	
2			1.1	87.9	76	10.0	
1/4			1.3		E	9.1	91.5
cb			1.1			212 North	
E			1.1	87.9	5	7.5	93.1
TP	12.35	200.55	0.84	188.20	+2	8.1	
		164 N			cb	8.1	
E			11.2	89.4	1/4	8.6	
+3			12.1		2	8.3	92.3
cb			12.1		tv	8.1	
1/4			12.4		1/4	8.5	
2			12.1	88.5	+5	9.2	
1/4			12.2		cb	9.2	
+5			12.6		+6	9.3	
2 cb			12.5		W	8.2	92.4
+2			12.5			224 N. Walk on East	
+6			11.6		2 Back	7.33	
W			11.6	89.0		237 North	
		190 N			W	6.7	93.9
W			10.3	90.3	+3	8.2	
+5			10.9		cb	7.9	
cb			10.8		+5	7.8	
1/4			10.0		1/4	7.3	
+5			9.6		2	7.0	93.6
2			9.7	90.9	1/4	7.2	
1/4			10.1		cb	7.3	

T
200.55

T
200.55

5

E	7.~	93.4	1/4	9.8	
	250'N		cb	4.5	
E	6.9	93.7	+3	4.0	
cb	7.0		W	3.6	97.0
1/4	6.6		Set B.M. S.W. Spk. in Pole - ^{Collingswood} Tandall	3.01	197.54
♀	6.4	94.2		5 cb	
1/4	6.6		W	2.8	97.8
cb	7.1		+3	3.5	
+7	7.6		cb	3.9	
W	6.3	94.3	+5	3.9	
	272'N		1/4	4.0	
W	5.0	95.6	♀	4.3	96.3
+3	5.7		1/4	4.5	
+8	6.3		cb	5.0	
cb	6.0		E	5.4	95.2
1/4	5.9			5 1/4	
♀	5.9	94.7	E	7.9	95.7
1/4	6.3		cb	7.5	96.1
cb	6.3		1/4	7.1	96.5
E	6.8	93.8	♀	3.8	96.8
	299.9 S. Line Collingswood Drive		1/4	3.8	96.8
E	5.6	95.0	cb	3.1	97.5
cb	5.3		W	2.7	97.9
1/4	5.0			♀	
♀	5.0	95.6	W	2.5	98.1
+5	4.6		cb	2.9	

20055

1/4	3.9	
2	3.5	97.1
1/4	3.8	
cb	4.3	
E	4.7	95.9
	N 1/4	
E	4.2	96.4
cb	3.8	
1/4	3.2	
2	2.9	97.7
+2	2.7	
1/4	2.8	
cb	2.4	
+5	2.3	
W	2.0	98.6
	N cb	
W	1.6	99.0
cb	1.8	
1/4	1.9	
2	2.0	98.6
1/4	2.4	
cb	2.9	
E	3.5	97.1
	N line of Coll	
E	2.8	97.8
+5	2.3	

20055

6

cb	1.7	
1/4	1.9	
2	1.2	99.4
1/4	1.9	
cb.	1.1	
W	1.1	99.5
T.P	11.95	212.31 0.19
		14' N. of the N line of Collingswood
W	11.9	00.4
cb	11.9	
+6	12.0	
1/4	11.9	
2	11.9	00.4
1/4	12.1	
cb	12.6	
E	13.2	99.1
	40' N	
E	11.2	01.1
cb	11.1	
1/4	10.9	
2	10.1	02.2
1/4	9.9	
cb	9.8	
W	10.1	02.2
	75' N	
W	7.9	04.9

7
 212.31
 75' N

+7	7.3	
cb	7.1	
1/4	7.1	
£	7.3	05.0
1/4	7.5	
cb	8.1	
E	8.5	03.8
88' N		
E	6.9	05.9
cb	6.1	
+3	6.3	
1/4	6.4	
£	5.7	06.6
1/4	5.4	
cb	5.6	
W	6.0	06.3
100' N		
W	3.6	08.7
+6	3.6	
+8	4.4	
zb	4.2	
+4	3.8	
1/4	4.1	
£	4.5	07.8
1/4	4.8	
cb	5.0	

7
 212.31

E	5.4	06.9
111' N		
E	9.3	08.0
cb	3.4	
1/4	3.4	
£	3.2	09.1
1/4	3.0	
cb	2.6	
+2	2.9	
W	2.3	10.1
125' N		
W	0.3	12.0
cb	0.7	
1/4	0.6	
£	0.9	11.4
1/4	1.2	
cb	1.4	
E	2.1	10.2
T.P	10.53	222.11 073 211.58
150' N S. line of Maiden		
E	8.7	13.4
cb	8.0	
+3	7.5	
1/4	7.7	
£	7.5	14.6
+2	7.2	

1/4 7.0
 +3 6.7
 cb 7.2
 W 6.8 15.3

168' N

N 4.0 18.1
 +7 4.8 17.3
 cb 4.7 17.4
 1/4 4.8 17.3
 +3 4.9 17.2
 +5 5.9 16.7
 k 5.2 16.9
 1/4 5.5 16.6
 cb 5.8 16.3
 E 6.3 15.8

186 = S. Line of Malden 45' st
 7.5 chs
 2.5 1/4 s

E 3.2 18.9
 cb 3.2
 1/4 3.1
 k 3.0 19.1
 1/4 2.7
 cb 2.5
 W 1.8 20.3

Set B.M. Pole S.W. Kendall 5.65 216.46

S. cb

W 0.8 21.3

+5 1.2
 cb 1.8
 1/4 1.5
 k 1.7 20.4
 1/4 1.5
 cb 1.7
 E 2.3 19.8

T.P 6.61 227.91 0.81 221.30

5 1/4

E 7.1 20.8
 cb 6.7
 1/4 6.7
 k 6.7 21.2
 1/4 6.5
 cb 6.6
 W 6.2 21.7

k

W 5.1 22.8
 +4 5.5
 cb 5.6
 +5 5.4
 1/4 5.9
 k 5.6 22.3
 1/4 5.6
 cb 5.8
 E 6.2 21.7

T
227.91
14 1/4

N 1/4
11409

1/4 E 5.4 22.5

+3 cb 4.8

cb 1/4 4.7

W 1/4 4.6 23.3

1/4 4.6

W cb 4.3

+7 W 4.0 23.9

cb W cb

1/4 W 3.1 24.8

+3 cb 3.2

+5 1/4 3.6

1/4 1/4 3.7 24.2

1/4 1/4 3.6

cb cb 3.9

E E 4.2 23.7

N Line

E E 3.5 24.4

cb cb 3.2

1/4 1/4 2.8

1/4 1/4 2.5 25.4

1/4 1/4 2.2

cb cb 2.0

W W 2.3 25.6

Set B set BM N.E. Prop 406 3.54 224.37

T.P. 9.16 228.05 9.02 218.89

1/4 B.N.I 11.60 216.45 ✓

1/6/28 X Section of Malden St.
 from the W line of Kendall to the E line of Collingswood
 Drive + * - Elev

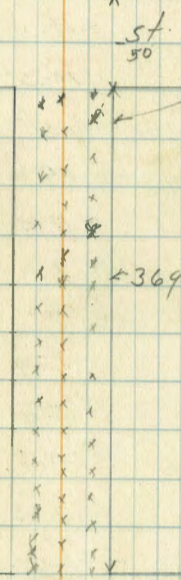
	11.60	228.06	216.96
		0200 W. line Kendall	
S		12.7	215.4
cb		11.0	
1/4		9.9	
1/2		9.3	218.8
1/4		8.4	
cb		7.4	
N		6.2	221.9
		21' West	
N		5.8	222.3
cb		7.1	
1/4		8.0	
1/2		8.8	219.3
1/4		9.9	
cb		10.8	
S		12.4	215.7
st 20		14.4	
		50' West	
S-20		14.5	
S		11.9	216.2
cb		10.5	
1/4		9.1	
1/2		7.8	220.3
1/4		6.3	
cb		5.3	

Profile plotted
2/28/28 Tolman

Collingswood Drive 10

Sketch of
Malden West
of Kendall

12.5' end of Trees
 6.6" Pepper
 Trees
 8' in st.
 set 20' on trees
 Colina



Note from the E
 line of Colina Ave
 to the W line of Kendall
 Street is forested with
 3 rows of spineless
 cactus of a dense growth

369.30

Kendall st

T
22806

N	3.7	224.4
	75' West	
N	2.9	225.7
cb	4.5	
1/4	5.8	
1/4	7.2	220.9
1/4	8.5	
cb	7.6	
S	11.2	216.9
S+20	14.5	
	100' West	
S-20	14.6	
S	11.0	217.1
cb	9.2	
1/4	8.1	
1/4	6.9	221.2
1/4	5.8	
cb	9.5	
N	2.3	225.8
	135' West	
N	3.5	224.6
cb	5.7	
1/4	6.9	
1/4	8.1	220.0
1/4	9.4	
cb	10.4	

T
22806

S	11.9	216.2
S+20	15.2	
	178' West	
S-20	13.7	
S	4.6	216.5
cb	10.1	
1/4	9.0	
1/4	8.0	220.1
1/4	6.9	
cb	5.5	
N	3.7	224.4
	200' West	
N	2.4	225.7
cb	9.2	
1/4	5.0	
1/4	6.3	221.8
1/4	7.3	
cb	8.3	
S	10.0	218.1
S+20	7.8	
	250' West	
S-20	11.0	
S	8.6	219.5
cb	7.0	
1/4	5.8	
T.P	12.20	239.56
	5.70	222.36

239.56

239.56

12

£	11.2	228.4
1/4	9.7	
cb	8.7	
N	7.1	227.5
300' West		
N	5.0	229.6
cb	6.7	
1/4	7.9	
£	9.1	225.5
1/4	10.2	
cb	11.4	
S	12.8	221.8
Stuo	16.1	
325' West		
S-20	14.8	
S	11.8	222.8
cb	9.9	
1/4	8.6	
£	7.4	227.2
1/4	6.1	
cb	5.1	
N	3.6	231.0
350' West		
N	1.6	233.0
cb	3.4	
1/4	4.5	

£	5.8	228.8
1/4	6.9	
cb	8.0	
S	10.1	224.5
Stuo	13.9	
369.3 E Line of Colina		
S-20	13.0	
S	9.4	225.2
cb	7.4	
1/4	6.3	
£	5.3	229.3
1/4	3.5	
T.P.	6.76	237.85
cb	5.0	3.47
N	3.8	251.09
T.P.	1.79	236.19
E cb		
N	2.0	234.1
cb	3.6	234.2
1/4	5.1	
£	6.4	229.8
1/4	7.4	
cb	8.3	
S	10.0	226.2
E 1/4		
S	9.7	226.5

π
236.19

π
236.19

13

cb	8.1	
1/4	7.2	
ϕ	6.1	230.1
1/4	5.0	
cb	4.0	
N	2.2	234.0
	ϕ	
N	1.9	234.3
+6	4.1	
cb	4.3	
1/4	5.4	
ϕ	6.5	229.7
1/4	7.3	
cb	8.3	
S.	9.8	226.4
	W 1/4	
S	9.9	226.3
cb	8.7	
1/4	7.6	
ϕ	6.6	229.6
1/4	5.5	
cb	4.5	
+4	4.1	
N	2.3	233.9
	W cb	
N	2.0	234.2

+5	4.4	
cb	4.7	
1/4	5.3	
ϕ	6.8	229.4
1/4	7.5	
cb	8.6	
S.	9.9	226.3
	W Line of Colina	
S.-20	11.2	
S-	9.9	226.8
cb	8.3	
1/4	7.3	
ϕ	6.4	229.8
1/4	5.2	
cb	4.5	
+5	4.0	
N	1.8	234.4
	50 West	
N	0.0	236.2
+5	2.1	
cb	2.4	
1/4	3.1	
+3	3.4	
ϕ	4.4	231.8
1/4	5.2	
cb	5.6	

236.19

293.92

14

S			5.8	230.4
St20			7.3	
		60' West		
S			5.8	230.4
cb			5.4	
1/4			4.9	
2			3.8	232.4
1/4			3.0	
cb			1.8	
+8			1.5	
N			0.1	236.1
T.P.	11.35	243.92	3.62	232.57
		81' St		
N			7.2	236.7
+3			8.5	
cb			9.3	
1/4			9.9	
2			10.6	233.3
1/4			11.3	
cb			11.6	
S			12.0	231.9
		100' West		
S			10.9	233.0
cb			10.2	
1/4			10.0	
2			9.4	234.5

1/4				8.8	
cb				8.6	
+7				7.9	
N				6.1	237.8
6.		150' West			
N				3.2	240.7
+3				5.4	
cb				5.6	
1/4				5.8	
2				6.7	237.2
1/4				6.7	
cb				7.1	
S				7.9	236.0
St10				8.9	
		200' West			
S-10				5.0	
S				4.1	239.8
cb				7.0	
1/4				8.7	
2				3.5	240.4
1/4				2.9	
cb				2.2	
+8				2.2	
T.P.	9.44	250.63	3.33		240.59
N				7.0	243.0

250.03

233' West

N	48	245.2
+2	56	
cb	60	
+6	64	
1/4	70	
2	75	242.5
1/4	76	
cb	78	
S	84	241.6
S+10	89	

250' West

S-10	80	
S	72	242.8
cb	65	
1/4	60	
2	59	244.1
1/4	59	
+3	49	
cb	49	
+8	45	
N	36	246.4

275' West

N	26	247.4
+3	41	
cb	41	
1/4	43	

250.03

15

2	4.9	245.1
1/4	5.2	
cb	6.0	
S	7.3	242.7
S+10	8.4	

300' West

S-10	9.1	
S	7.9	242.1
cb	6.6	
1/4	5.5	
2	5.0	245.0
1/4	4.7	
cb	4.3	
+7	4.3	
+8	3.8	
N	3.8	246.2

330' West

N	5.4	244.6
cb	5.8	
1/4	6.2	
2	6.1	243.9
1/4	6.6	
cb	7.2	
S	8.2	241.8
S+10	9.2	

250.03

370 West

S-10	10.3	
S	9.0	241.0
cb	8.1	
1/4	7.5	
ϕ	7.1	242.9
1/4	7.1	
cb	6.7	
N	6.3	243.7

386 West

N	6.5	243.5
cb	7.5	
1/4	7.8	
1/3	7.5	
ϕ	7.8	242.2
1/4	8.4	
cb	8.9	
S	10.1	239.9
S+10	11.1	

907 West

S-10	12.8	
S	11.8	238.2
cb	11.0	
1/4	10.~	
ϕ	7.8	240.2
1/4	9.7	
cb	9.0	

250.03

16

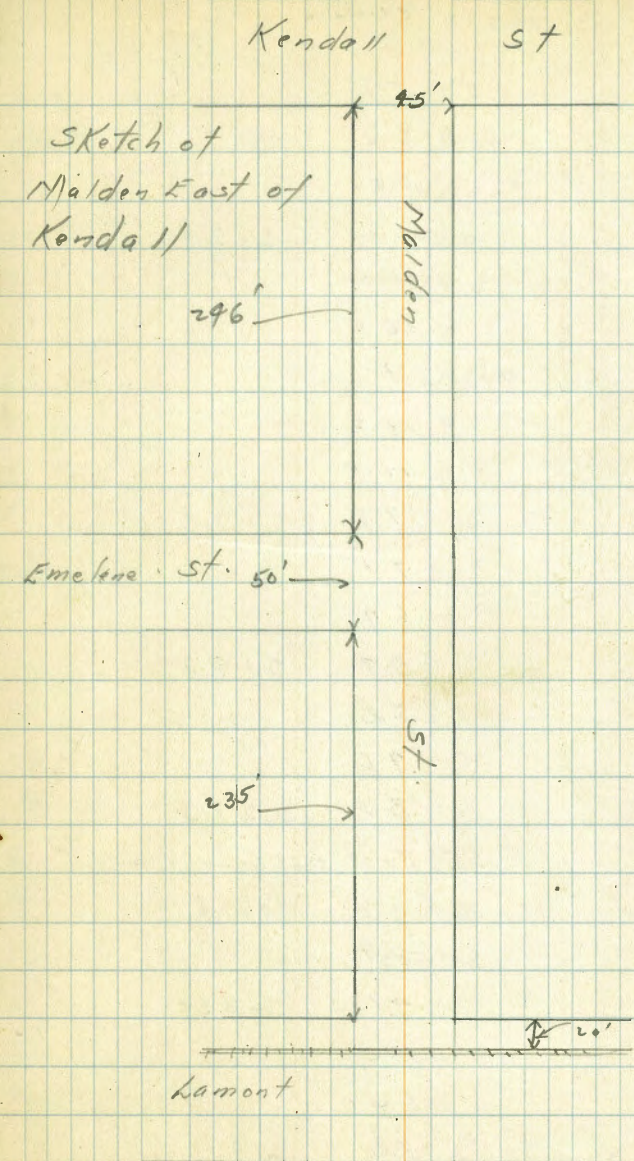
IX	81	241.9
TP 0.97	237.57	12.93
TP 1.79	226.42	12.89
BM spike in pole SW Kendall + Maiden	9.94	216.48
		<u>716.88</u>

207
270
157

2/7/28 X Sections of Malden St from the E. line
 of Kendall East to the W. line of Lamont
 B.M. NE Pop 45' st
 H. b. Malden 7.5 cbs
 of Kendall 7.5 1/4

	+	+	-	Elev
	0.77	225.14		224.37
		0+00 E		
N			07	224.4
cb			14	
1/4			24	
1/4			35	221.6
cb			42	
S.			52	
			59	219.2
		13' East		
S-15			94	
S-5			78	
S.			64	218.7
cb			56	
1/4			48	
1/4			38	221.3
cb			28	
cb			18	
N			07	224.4
		30' East steps of Dwelling on N		
on line			1.34	
		36' East		
N			25	222.6
cb			39	
1/4			48	
1/4			53	219.8

Profile plotted by Tolman 2/28/28



Note cbs continuous across Malden on Lamont

225.14

1/4	5.8	
cb	6.6	
+5	6.8	
S	7.3	217.8
S+7	10.5	
S+15	12.3	
97' East		
S-15	13.3	
S-8	12.4	
S	7.9	217.2
cb	7.1	
1/4	6.9	
⊕	5.9	219.2
1/4	5.2	
cb	9.6	
N	3.8	221.3
55' East D.H. Garage on N.		
11. Back floor etc	3.36	221.8
66' East		
N	7.1	221.0
cb	5.2	
1/4	6.2	
⊕	7.0	218.1
1/4	7.7	
cb	8.2	
S	9.1	216.0

225.14

18

S+8	14.2	
S+15	15.4	
73' East		
S-15	16.0	
S-6	14.8	
S.	10.3	214.8
cb	9.6	
1/4	9.1	
⊕	8.2	216.9
1/4	7.8	
cb	6.9	
N	9.5	220.6
84'		
N	6.5	218.6
cb	7.8	
1/4	8.9	
⊕	9.6	215.5
1/4	10.2	
cb	10.7	
S.	11.7	213.4
S+5	15.2	
S+15	16.6	
100' East		
S-15	17.7	
S-8	16.1	
S	13.2	211.9

225.14

cb		12.0	
1/4		11.7	
1/2		10.9	214.2
1/4		10.2	
cb		9.3	
N		8.7	216.4

150 East

N		12.7	212.4
T.P.	016	212.83	212.67

cb		1.2	
1/4		1.5	
1/2		2.5	210.36
1/4		3.2	
cb		3.9	
S.		4.6	208.2
S+6		6.3	
S+15		7.5	

165 East

S-15		8.4	
S.		6.6	206.2
cb		5.3	
1/4		4.5	
1/2		3.7	209.1
1/4		2.6	
cb		1.9	
N		1.2	211.6

212.83

19

177 East

N		1.9	210.9
cb		2.9	
1/4		3.8	
1/2		5.0	207.8
1/4		5.9	
cb		6.8	
S.		7.7	205.1
S+15		9.4	

200 East

S-15		10.3	
S		8.6	204.2
cb		8.0	
1/4		7.3	
1/2		6.4	206.4
1/4		5.5	
cb		4.5	
N		3.6	209.2

214 E.

N		4.9	207.9
cb		5.6	
1/4		6.4	
1/2		7.1	205.7
1/4		7.8	
cb		8.6	
S		9.5	203.3
S+15		11.1	

212.83

238' East

S-15	12.9		
S	10.9	201.9	
cb	10.1		
1/4	9.3		
1/2	8.6	204.2	
1/4	7.6		
cb	6.9		
N	6.9	206.4	
N	7.9	205.4	
cb	7.7		
1/4	8.4		
1/2	9.2		
1/4	9.9		
cb	10.7		
S	11.6	201.2	
St. 5	13.0		
	246' East	W line of	50 st 10' cbs 7.5 1/4
S.	12.3	200.5	
cb	11.7		
1/4	10.9		
1/2	10.5	202.3	
1/4	9.5		
cb	9.2		
N	8.5	204.3	
	Wcb		

212.83

20

Wcb

	W	9.7	203.1
	cb	10.1	
	1/4	10.6	
	1/2	11.1	201.7
	1/4	11.7	
	cb	12.2	
	S	12.9	199.9
	W 1/4		
	S	13.9	198.9
	cb	12.9	
	1/4	12.9	
	1/2	12.0	200.8
	1/4	11.1	
	cb	10.7	
	N	10.3	202.5
	1/2		
	N	11.0	201.8
	cb	11.3	
	1/4	11.9	
	1/2	12.8	200.0
	T.P	5.80	205.97
	1/4	12.66	200.17
	1/4	6.5	
	cb	6.8	
	S	7.4	198.6
	E 1/4		
	S	7.9	198.4

20597

cb	7.0	
1/4	6.7	
1/4	6.3	199.7
1/4	5.5	
cb	5.0	
N	4.6	201.4
	E. Line of	
N	9.2	201.4
cb	5.2	
1/4	5.6	
1/4	6.2	199.8
1/4	6.7	
cb	7.1	
S	7.6	198.4
St 10	8.4	
	25' East	
S-10	8.2	
S	7.4	198.6
cb	7.4	
1/4	6.6	
1/4	6.5	199.5
1/4	6.0	
cb	5.7	
N	5.0	201.0
	68' East	
ix	4.4	201.6

20597

21

cb	4.9	
1/4	5.3	
1/4	5.8	200.2
1/4	5.9	
cb	6.3	
S	6.8	199.2
St 10	7.4	
	100' East	
S-10	7.1	
S	6.2	199.8
cb	5.8	
1/4	5.8	
1/4	5.6	200.4
1/4	5.2	
cb	4.8	
N	4.1	201.9
	130' East	
N	3.6	202.4
cb	3.9	
1/4	4.6	
1/4	4.9	201.1
1/4	5.2	
cb	5.6	
S	5.7	200.3
	160' East	
S	4.7	201.3

T
20597

cb	4.9	
1/4	4.6	
2	4.1	201.8
1/4	3.9	
cb	3.2	
N	2.9	203.1

185' East

N	2.2	203.8
cb	2.8	
1/4	3.3	
2	3.9	202.1
1/4	4.4	
cb	4.6	
S	4.7	201.3

200' East

S	4.8	201.2
cb	4.6	
1/4	4.3	
2	3.7	202.3
1/4	3.2	
cb	2.8	
N	2.2	203.8

235' E. Whine of lament

N	2.0	204.0
cb	2.6	
1/4	3.2	

T
20597

22

2	3.8	202.2
1/4	4.2	
cb	4.7	
S	5.2	200.8
	8.43	197.54
B.M.	5.85	200.12

Pole S.W. Collingswood
Drive + Kendall

B.M.	6.30	203.84	197.54	197.54
check T _p	5.80	205.97	3.67	200.17
B.M.			8.93	197.54
				197.54
				00

				258.111
				00

X Sections of Collingswood Drive
from the W Line of Kendall to E Line
of Colina St

60' st
10' cbs
10' 1/4"

Sketch of
Collingswood
West of Kendall
to E line of Colina

13 M. Epix
in Po to S. W
Collingswood Kendall
370 201.29

197.59

0+00 = W line of Kendall

S 9.1 197.1

cb 3.9

1/4 3.9

1/2 2.8 198.4

3/4 2.6

cb 2.2

N 1.8 199.6

0+30 W

N 0.5 200.7

cb 1.2

1/4 1.9

+5 2.3

+6 2.9

1/2 2.7 198.5

3/4 3.1

cb 3.1

+5 3.3

S 9.2 197.0

60' W

S 3.9 197.3

cb 3.3

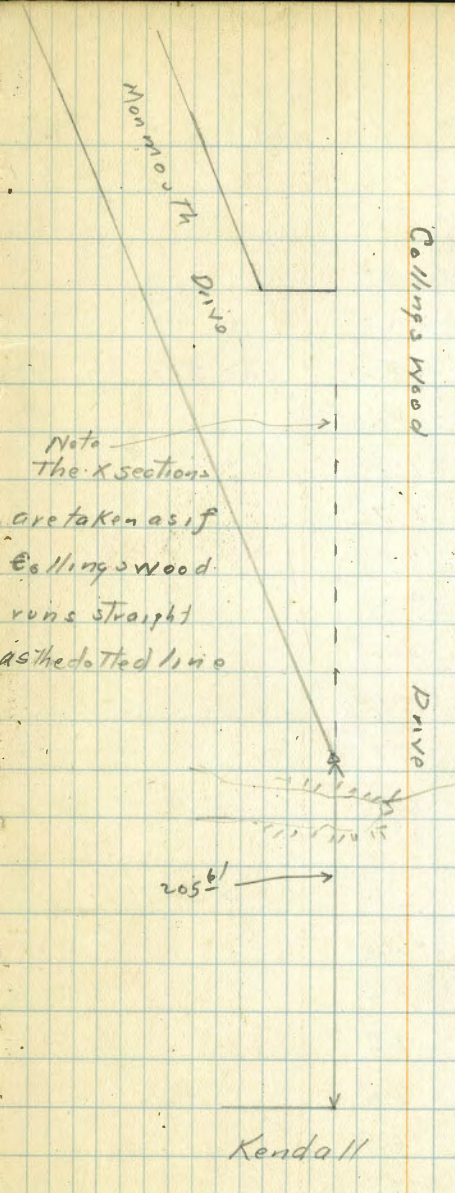
+2 3.2

+3 3.9

1/4 2.9

Profile plotted
2/10/88 Tolman

Note
The X sections
are taken as if
Collingswood
runs straight
as the dotted line



Collingswood

Drive

Colina Ave

369²⁰

This portion is natural
Drain for the section
starting to become a
water course
May need a drain pipe

Kendall

7
20/29

2	2.7	198.5
+9	3.0	
+6	2.1	
1/4	1.8	
CS	1.2	
IV	0.7	200.5
	80 West	
N	1.8	199.4
cb	2.9	
1/4	4.1	
+2	4.3	
+3	4.9	
2	5.1	196.1
1/4	5.7	
+5	6.1	
cb	6.0	
S	6.8	194.4
	100 West	
S-10	8.6	
S	7.6	193.6
cb	6.8	
+5	6.9	
1/4	6.3	
2	5.6	195.6
+7	5.8	
+9	4.8	

7
20/29

29

1/4	9.6	
cb	3.6	
N	2.7	198.5
	135 West	
N	4.0	197.2
cb	7.8	
+9	5.3	
1/4	6.7	
2	6.4	194.8
1/4	7.2	
+6	8.2	
cb	7.9	
S	8.9	192.3
S+10	10.4	
	155 West	
S-15	11.9	
S	10.2	191.0
cb	9.1	
+5	9.1	
1/4	8.3	
2	7.4	193.8
+8	7.3	
1/4	7.9	
+2	6.6	
cb	6.3	
+8	5.5	

7.
20114

N	46	196.6
175' W.		
N	54	195.8
cb	79	
+8	85	
1/4	77	
¢	81	193.1
+2	82	
+6	101	
1/4	10	
cb	113	
S	125	188.7
S+15	137	
188' West		
S-15	148	
S-12	144	
S-8	166	
S	142	187.0
cb	118	
1/4	103	
¢	81	193.1
1/4	81	
+4	85	
+5	80	
cb	74	
N	59	195.3

20114

(205.61?)

200' West A) Sveskitch

25

N	53	195.9
cb	71	
+4	77	
+6	81	
1/4	78	
¢	80	193.2
+5	95	
1/4	101	
cb	115	
S	132	188.0
S+15	108	
225' West		
S-15	143	
S	121	189.1
cb	106	
1/4	93	
+8	89	
¢	77	193.5
1/4	71	
+8	75	
cb	62	
+7	95	
N	94	197.1
240' West		
N	33	197.9
cb	47	

201.29

+1	6.0	
1/4	6.0	
+7	6.7	
1/2	8.1	193.1
1/4	9.9	
cb	10.6	
S	11.8	189.4
S+15	13.8	
	269'N	
S-15	13.4	
S	11.9	189.3
cb	10.9	
1/4	9.2	
1/2	7.5	193.7
+3	7.0	
+7	4.6	
1/4	4.8	
cb	4.6	
+3	3.6	
N	2.6	198.6
	300'N	
N	0.5	200.7
+5	1.8	
cb	1.7	
1/4	2.0	
+5	4.6	

201.29

26

1/2	5.6	195.6
1/4	7.3	
cb	8.8	
S	9.7	191.5
S+15	11.9	
S+25	12.8	
	312'N	
S-25	12.2	
S	9.3	191.9
cb	7.9	
1/4	6.2	
1/2	4.6	196.6
+7	3.7	
1/4	1.1	
cb	0.7	
T.P	6.49	207.18
+6	7.1	
+7	6.1	
N	5.6	201.6
	377'N (??) What station	
N	5.1	202.1
+3	5.9	
cb	5.6	
+8	5.8	
1/4	7.1	
+2	8.3	

20718

¢	9.6	197.6
1/4	10.7	
cb	11.9	
S.	13.2	194.0
St-25	17.4	
349 West		
S-25	15.5	
S.	11.2	196.0
cb	10.0	
1/4	9.0	
¢	7.9	199.3
1/4	6.2	
+4	4.1	
cb	3.7	
+8	3.7	
N	2.7	204.5
369 = E-Line Coling		
N	0.5	206.7
+1	1.8	
cb	2.3	
+6	2.5	
1/4	4.3	
¢	6.4	200.8
1/4	8.2	
cb	9.4	
S	10.8	196.4

20718

27

St-25	19.2	
BN	966	197.54 (2) -
		197.52
	0.71	198.25
TP	0.97	186.59 - 1263
		185.62
TP	1.62	177.52 - 10.69
		175.90
B.M.	Tree N.W.Side Box 1	
	1.54	175.98

Bliss X sections of Sutter Street from the
 1/2 mile S. line of Pringle to 218 South

BM NW
 NW Washington
 Blvd - Pringle

41st
 5' cbs
 775.42

π
 266.74

28

	+	π	-	Elev
	1.67	266.74		265.07
				0+00 Skinned Pringle
W Topcb	out paving	1.60		265.1
Gutter		2.08		264.6
1/4		1.49		265.2
1/4		1.13		265.6
1/4		1.13		265.6
Gutter		1.24		265.5
E Topcb		0.76		266.0
E		0.5		266.7
		0.6' S		
K		0.7		266.7
cb		1.0		265.7
1/4		1.5		265.2
1/4		1.7		265.0
1/4		2.0		264.7
Gutter		2.3		264.4
W Topcb		2.28		264.4
				25' South
W Topcb		5.07		261.7
Gutter		5.1		261.6
1/4		5.1		261.6
1/4		4.6		262.1
1/4		4.2		262.5
cb		3.9		263.3
1/4		2.5		264.2

X sections in Back 1235 page 12
 yardag 11-22-28
 T.G.H.

	E	
		2.6
		264.1
		90' South
E		5.5
		261.2
cb		5.7
		261.0
1/4		5.8
		260.9
1/4		5.7
		261.0
1/4		6.3
		260.4
1/4		6.8
		259.9
Gutter		7.1
		259.6
W Topcb		6.98
		259.7
		59' South Garage on East concrete
		2. Back etc floor
		7.45
		60' South
W Topcb		9.55
		257.1
Gutter		9.6
		257.1
1/4		9.5
		257.2
1/4		8.9
		257.8
1/4		8.4
		258.3
cb		7.9
		258.8
E		7.9
		258.8
		70' South
E		9.0
		257.7
1/4		8.8
		257.9
cb		9.4
		257.3
1/4		9.9
		256.8
1/4		10.5
		256.2

266.74

1/4	W.2	255.5
Gutter	11.4	255.3
Top cb	11.11	255.6
79' South		
W Top cb	12.30	254.4
Gutter	12.5	254.2
1/4	12.4	254.3
E	12.0	254.7
1/4	11.6	255.1
cb	11.9	254.8
+3	11.9	254.8
E	11.1	255.6

79 98 258.61 12.95 253.79
 9.7 South Walk of House on East
 on Line ch 446

100' South

E	5.8	252.8
cb	6.2	252.4
1/4	6.0	252.6
+5	5.8	252.8
E	6.1	252.5
1/4	6.7	251.9
Gutter	7.0	251.6
W Top cb	6.87	251.7

130' South

W Top cb	11.08	247.5
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268.61

29

Gutter	11.2	247.4
1/4	11.1	247.5
E	10.6	248.0
+7	10.0	248.6
1/4	10.0	248.6
cb	9.9	248.7
E	10.2	248.4
146 South end of cb on West		
E	11.2	247.4
cb	10.9	247.7
1/4	10.9	247.7
E	11.6	247.0
1/4	12.2	246.4

Gutter	12.3	246.3
W Top cb	12.28	246.3

150' South

W	12.6	246.0
+4	13.3	245.3
cb	13.8	244.8
1/4	13.9	245.2
E	12.8	245.8
1/4	11.8	246.8
+4	11.0	247.6
cb	10.7	247.9
E	11.3	247.3
E+1	12.4	246.0

T
258.61

E+10		15.0	2436
TP	0.07	246.40	12.28
		166' South	
E-15		19.5	231.9
E		19.3	237.1
cb		7.1	239.3
1/4		3.9	242.5
+9		2.3	244.1
ϕ		2.0	244.4
1/4		3.1	243.3
cb		3.0	243.4
W		3.0	243.4
		185' South	
W		5.0	241.4
+2		5.2	241.2
+6		11.1	235.3
cb		11.3	235.1
+4		10.9	235.5
1/4		5.7	240.7
+4		6.0	240.4
ϕ		8.2	238.2
1/4		12.5	233.9
+4		13.7	232.7
cb		16.1	230.3
E		18.4	227.6
E+7		21.5	224.9

T
246.40

30

E+11		24.1	222.3
E+20		27.0	219.4
		200' South	
E-25		3.3.0	213.4
E-12		3.0.0	216.4
E-5		2.5.1	221.3
E		2.4.5	221.9
cb		2.2.0	224.4
1/4		2.0.2	226.2
ϕ		1.8.5	229.9
1/4		1.3.0	233.4
+3		1.7.7	228.7
cb		1.7.5	228.9
+4		1.1.9	234.5
W		1.2.1	234.3
TP	0.60	234.26	12.74
		218' South	
W		9.8	224.5
cb		9.5	224.8
1/4		11.2	223.1
ϕ		13.7	220.6
1/4		14.8	219.5
+1		14.9	219.4
cb		18.8	215.5
E		20.2	214.1
E+7		21.5	212.5

λ
239.26

E+20

28.7 20 5.6

T.p.

12.59

221.72

31

Bliss 4/16 x sections of Keating Street Middletown
 Isbell Addition from the E line of Neale to the N
 Morgan line of Sutter
 B.M NW Washington Blvd
 Pringle

20908

	1.67	266.79		265.07	1/4	9.3	1948
TP	982	258.61	1295	253.79	ϕ	9.7	1944
TP	0.07	246.90	1228	246.33	+1	10.5	1936
TP	0.60	239.26	1274	233.66	1/4	10.1	1940
TP	0.57	222.29	1259	221.72	cb	9.1	1950
T.P	0.56	209.95	1290	209.39	+1	8.2	1959
T.P	6.94	209.08	1231	197.69	N	5.2	1989

0100 = E. line of Neale St

17' East

N	9.9			1942	N	2.1	2020
cb	10.6			1935	cb	7.4	1967
1/4	10.7			1934	1/4	8.3	1958
+2.5	11.2			1929	ϕ	8.5	1956
+6	11.3			1928	1/4	7.9	1962
ϕ	10.4			1937	cb	7.6	1965
1/4	10.2			1939	+5	8.0	1961
cb	9.2			1949	S	12.5	1916
+5	9.1			1950	S+16	18.0	1861
S	11.5			1926	S+30	26.2	1779
S+20	22.0			182.1			
S+30	27.5			1766			

50' East

		05' East					
S-30	27.9			176.2	S-30	23.0	181.1
S-20	22.5			181.6	S-20	19.8	1843
S	11.6			192.5	S-10	17.2	1869
+4	8.6			195.5	S	11.3	1928
cb	8.7			195.4	+7	5.9	1982
					cb	5.6	1985
					1/4	5.9	1982

Plotted 9-12-26 - C.B.H.

20f08

+5	6.1	198.0
¢	5.8	198.3
1/4	5.3	198.8
cb	4.8	199.3
+4	4.5	199.6
N	1.6	202.5
76' East		
N	0.6	203.5
+4	3.7	200.4
cb	4.4	199.7
1/4	4.7	199.4
¢	4.9	199.2
1/4	5.1	199.0
cb	5.3	198.8
+~	5.5	198.6
S	11.0	193.1
+S+10	15.1	189.0
S+20	18.0	186.1
S+30	21.1	183.0
100' East		
S-30	19.7	184.4
S-20	17.6	186.5
S-10	15.2	188.9
S	12.3	191.8
+cb	6.5	197.6
+~	4.8	199.3

20g08

27
26
128
635

33

1/4	4.5	199.6
¢	4.3	199.8
1/4	3.7	200.4
cb	3.3	200.8
+5	3.2	200.9
N	1.4	202.7
130' East		
N	1.8	202.3
cb	2.8	201.3
1/4	3.5	200.6
+2.5	3.8	200.3
¢	7.2	196.9
+4	8.8	195.3
1/4	10.1	194.0
cb	11.6	192.5
+6	13.8	190.3
S	16.3	187.8
S+10	21.2	182.9
S+20	25.0	179.1
S+30	28.9	175.2
152' East		
S-50	43.8	160.3
S-30	32.2	171.9
S-20	28.5	175.6
S-10	26.0	178.1
S	24.1	180.0

209.08

cb	21.2	182.9
1/4	18.0	186.1
1/2	16.6	187.5
3/4	11.0	193.1
cb	6.1	198.0
+6	2.6	201.5
N	2.2	201.9

165' East

N	5.4	198.7
cb	10.1	194.0
1/4	13.7	190.4
1/2	18.6	185.5
3/4	22.1	182.0
cb	26.5	177.6
+4	27.3	176.8
S	29.2	174.9
S+10	31.8	172.3
S+20	35.0	169.1
S+30	38.0	166.1
S+40	44.3	159.8
S+50	48.5	155.6
S+56	50.2	153.4

175' East

S-50	49.6	154.5
S-40	46.1	158.0
S-30	43.6	160.5

209.08

13
25
37

39

S-20	41.0	163.1
S-10	36.8	167.3
S	33.2	170.9
cb	27.2	176.9
1/4	23.0	181.1
1/2	20.5	183.6
3/4	17.1	187.0
cb	13.6	190.5
N	7.2	196.9

185' East

N	8.5	195.3
cb	15.7	188.4
1/4	20.3	183.8
1/2	23.6	180.5
3/4	26.2	177.9
cb	29.4	174.7
S	35.2	168.9
S+10	40.1	163.0
S+20	45.1	159.0
S+30	45.2	158.9
S+40	47.1	157.0
S+50	46.0	158.1

200' East W. Line of Sutter

S+50	40.0	164.1
S-40	41.0	163.1
S-30	43.6	160.5

T
209.08

35

S-20			93.1	161.0
S-19			93.0	161.1
S			37.2	166.9
cb			32.2	171.9
1/4			28.7	175.4
1/2			25.8	178.3
1/4			23.2	180.9
cb			20.2	183.9
N			16.0	188.1
Set BM. Pop Hub NW Sutter & Keating			15.11	188.97
T.P.	12.93	246.15	0.86	203.22
T.P.	12.63	228.77	0.01	216.14
check on sutter g.M.			7.07	24.70
T.P.	11.79	230.98	0.58	219.19
T.P.	12.79	293.28	0.49	230.49
T.P.	12.78	256.01	0.05	243.23
T.P.	7.67	261.46	2.22	253.79
BM check on sutter g.M.				
N.W. cor of W Washington Blvd & Pringle			5.41	256.05

Note: Cross Section KEATING Pt. Sutter & Tupper
in Book 1246-72
-Walker

Bliss
2/24/28
3M. Hub &
of 31st South
of Alley set top
the X' Sec of
31st

X Section of Alley Block 32 H.P.
Whitneys Addition. Between Colton & Bay
Key
31st + 32nd
+

12.05 27.89 15.89

0+00 = E. line of 31st Street

N. Right hand
end of sheet 3.5 24.4
+2 3.7 24.2
+5 6.0 21.9
± 6.2 21.7
+6 6.2 21.7
S. 7.2 20.7

Plotted
3/19/28
A.C.H.

15' East of the E. line of 31st

S-10 11.6 16.3
S 8.5 19.4
+2 7.7 20.2
+5 7.4 20.5
± 7.1 20.8
+5 7.0 20.9
+7 5.3 22.6
N 4.3 23.6

35' East

N 6.5 21.4
+4 7.8 20.1
± 7.9 19.9
+8 8.3 19.6
S 8.8 19.1
+2 10.5 17.4
+10 11.6 16.3

27.89

50' East

S-10	11.3	16.6
S-1	10.3	17.6
S	9.1	18.8
+9	8.8	19.1
£	8.3	19.6
N	7.8	20.1

67' East Single Garage on N ✓

on Line Dirt Floor etc

£	8.7	19.2
+6	9.0	18.9
S	9.7	18.2

88

S	8.6	19.3
£	8.2	19.7
+4	8.2	19.7
N	7.1	20.8

107' East

N	6.5	21.4
£	6.9	21.0
S	6.4	21.5

S+25 Dwelling Sill

125' East

S	4.2	23.7
+4	4.5	23.4
£	4.5	23.4
N	4.3	23.6

27.89

37

145' East

N	1.7	26.2
+7	1.5	26.4
£	1.2	26.7
S	1.0	26.9
T.P.	<u>10.45</u>	38.04
✓		<u>0.30</u>

163' East West of DB Garage on North

1.0 Back

7.4	20.6	
176' East		
S	7.3	20.7
£	7.4	20.6
N	7.4	20.6

✓

157' East End DB Garage on N

1.0 Back

7.4 20.6

200' East

N	5.5	32.5
£	5.7	32.3
+4	5.6	32.4
S	5.7	32.3

210' East

S	5.2	32.8
£	5.0	33.0
N	5.1	32.9

232' East

N	4.4	33.6
£	4.7	33.3
S	5.2	32.8

38,04

250' East

S	5.2	32.8	S
E	5.0	33.0	
N	4.7	33.3	
✓			
	4.6 Back - Dirt floor	4.8	33.2
N	4.8	33.2	E
E	5.1	32.9	N
S	5.2	32.8	✓

284 East end of Db/Garage N

S	5.1	32.9	
E	5.0	33.0	N
N	5.0	33.0	E
✓	4.6 Back	floor	5.0
			33.0

300 East

N	5.0	33.0	
E	5.0	33.0	
S	5.2	32.8	S
			E

325 East

S	5.2	32.8	N
E	5.0	33.0	TP. 415
N	4.8	32.7	

338 East Single Garage on S

	on line ctr	5.0	33.0	E
--	-------------	-----	------	---

343 East

N	4.8	32.2	S
E	4.8	33.2	+4

38,04

38

5.2 32.8

348 East Single Garage on South

on line ctr 5.1 32.9

361 East

5.0 33.0

4.7 33.3

4.8 33.2

369 East West Db/Garage on N

2 Back Dirt floor 4.6 32.4

372 East

4.9 33.1

5.1 32.9

5.2 32.8

392 East end of Db/Garage on N

2 Back Dirt floor 4.7 33.3

400 East

5.8 32.2

5.6 32.4

5.4 32.6

6.19 .85

418 East

4.1 32.5

4.1 32.4

4.5 32.1

4.8 31.8

430 E

4	50	31.6
+6	48	31.8
+8	44	32.2
♀	44	32.2
N	45	32.1

450' East

N	44	32.2
♂	47	31.9
S	48	31.8

475 E

S	47	31.9
♀	46	32.0
N	46	32.0

500' East

N	46	32.0
♀	52	31.4
+8	54	31.2
+9	48	31.8
S	48	31.8

510 East

S	49	31.7
+2	49	31.7
+3	51	30.9
♀	55	31.1
+8	52	31.4
+9	46	32.0

N

N

+2

+4

♀

+6

+8

S

S

+3

+4

♀

+8

+9

N

N

♀

S

T.P. 5.17

T.P. 11.89

N.E.
Cor. Boston + 31st

46

516 East

46

47

54

58

59

49

49

521 East

52

53

63

64

60

50

50

524 East. W. Line of 32nd

6.6

6.8

7.2

0.01

0.54

1.58

32.0

32.0

31.9

31.2

30.8

30.7

31.7

31.7

31.4

31.3

30.3

30.2

30.6

31.6

31.6

N.E. Cor. 30th

31st 31.93

29.8

29.4

36.07

Bliss
 Isbell
 Morgan
 2/2 9/28
 B.M. N.E.
 B.P. Palm
 Bancroft

X Section Palm Street from the
 W line of 32nd to 33rd West 5' Back

+ 4.74 309.78 305.04

60' st
 10' obs
 10' 1/4

Sec. A

N 6.6 303.2
 N Tape 6.84 302.94
 Cutter 7.47
 1/4 7.07
 2 6.95 302.8
 1/4 7.05
 Cutter 7.21
 S Tape 6.74 303.04
 S 6.3 303.5

Plotted
 2/16/28
 H.C.H.

Sec B 5' Back
 on No. 74

S 3.0 306.8
 cb 4.0
 1/4 4.7
 2 5.1 304.7
 +6 5.3
 1/4 6.4
 cb 6.4
 +2 5.7
 N 5.8 304.0

0+00

14 5.5 304.3
 cb 5.8
 +4 5.8
 +6 5.9

H.I.
30978

1/4	5.3		
2	7.9	304.9	
1/4	4.5		
cb	7.0		
5	3.0	306.8	
			18' W.
5	2.8	307.0	
cb	3.7		
1/4	4.3		
2	5.1	304.7	
1/4	5.5		
+5	5.5		
+7	6.3		
cb	6.6		
+1	6.4		
+3	5.5		
N	5.3	304.5	
			25' West
N	6.2	303.6	
+7	5.9		
+9	6.9		
cb	6.9		
+3	6.5		
+5	5.6		
1/4	5.6		
2	5.3	304.5	

H.I.
30978

41

1/4	7.6		
cb	3.8		
5	2.9	306.9	
			50' West
5	3.8	306.0	
cb	3.7		
1/4	4.3		
2	4.9	304.9	
1/4	6.0		
+7	6.3		
+9	7.9		
cb	8.0		
+2	8.1		
+5	7.1		
N	7.7	302.1	
			63' West
N	8.8	301.0	
+5	8.0		
+7	8.7		
cb	8.5		
+	6.7		
1/4	6.6		
2	5.4	304.4	
1/4	4.9		
cb	4.4		
5	4.1	305.7	

H.I.
309.78

75' West

S	4.7	305.1
cb	4.9	
+5	5.7	
1/4	5.9	
£	6.1	303.7
1/4	7.2	
+7	7.9	
cb	9.5	
+3	9.9	
+6	9.1	
N	9.5	300.3

80' West

N	9.8	300.0
+9	9.4	
+5	10.2	
+8	9.9	
cb	8.3	
+3	8.2	
1/4	7.6	
£	6.6	303.2
1/4	6.~	
cb	5.5	
+2	5.5	
+5	5.9	
S	5.8	304.0

H.I.
309.78

42

95' West

S	6.9	307.9
cb	7.4	
1/4	7.5	
£	7.9	301.9
1/4	8.7	
cb	9.6	
+3	10.9	
N	11.8	298.0

100' West

N	11.5	298.3
+3	10.5	
+7	10.7	
cb	10.0	
1/4	9.4	
£	8.5	301.3
1/4	8.2	
+7	8.2	
cb	7.6	
S	7.3	302.5

307.73 3.23

306.55

125' West

£	6.8	300.9
cb	7.1	
1/4	8.0	
£	8.3	299.4

↑
30773

1/4	8.6	
+7	8.9	
cb	9.4	
+5	10.6	
+9	10.9	
N	10.0	297.7
N+15	11.6	
	1.36 West	
N-10	12.0	
N	11.9	295.8
+4	10.5	
cb	9.8	
1/4	9.2	
£	8.7	299.0
1/4	8.1	
cb	7.8	
S	7.2	300.5
	1.50 West	
S	7.5	300.2
cb	7.8	
1/4	8.2	
£	8.8	298.9
1/4	9.5	
+5	9.7	
cb	10.1	
N	10.9	296.8

↑
30773

43

N+10	11.8	
	175 West	
N-10	10.2	
N	9.7	298.0
cb	9.4	
1/4	9.2	
£	8.6	299.1
1/4	8.3	
cb	8.0	
S	7.6	298.1
	200 West	
S	7.6	298.1
cb	7.6	
1/4	7.9	
£	8.2	299.5
1/4	8.6	
cb	8.8	
N	8.9	298.8
	225 West	
N	8.8	298.9
cb	8.7	
1/4	8.4	
£	8.2	299.5
1/4	8.0	
cb	7.8	
S	7.8	299.9

X
307.73

250 West

S	8.5	299.2
cb	8.7	
1/4	9.0	
ϕ	9.2	298.5
1/4	9.4	
cb	9.8	
N	10.3	297.4
N+10	11.0	

516 301.35 11.48

275 West

N-20	17.5	
N-15	16.0	
N	10.0	291.4
cb	6.5	
1/4	5.8	
ϕ	5.2	296.2
1/4	4.7	
cb	3.9	
S	3.5	297.9

300 West

S	5.8	295.6
cb	6.6	
1/4	7.0	
ϕ	7.8	293.6
1/4	8.9	
cb	13.8	

H.I.
301.35

14.0
16.0

27.0
12
95.4
44

N	20.3	281.1
N+10	25.5	
N+20	30.1	
N+30	37.3	

325 West

N-35	4.21	
N-25	3.7.2	
N	26.0	275.4
cb	21.7	
1/4	15.3	
ϕ	12.4	289.0
1/4	10.9	
cb	9.4	
S	8.7	292.7

335 West

S	11.2	290.2
cb	12.1	
1/4	12.9	
ϕ	13.9	287.5
1/4	16.5	
cb	22.1	
N	28.8	272.6
N+25	40.8	
N+35	44.3	

T.P. 11.23 310.50 2.08

BM-N Bancroft 5.47 305.03

30' Roadway
0+00 = EL Front

X sec Monticito Front to 4th

BM N.W.B.P. Bachman + Monticito 287.54

T.P. 749 295.03

Scb	8.04	286.99
Gut	8.44	286.59
$\frac{1}{4}$	8.05	286.98
$\frac{1}{4}$	7.81	287.22
$\frac{1}{4}$	7.78	287.25
Gut	7.94	287.09
Ncb	7.53	287.50
OT10		
NL	6.7	288.33
Cb	7.3	287.73
+1	7.7	287.9
$\frac{1}{4}$	7.6	287.4
$\frac{1}{4}$	7.2	287.8
$\frac{1}{4}$	7.1	287.9
Cb	7.1	287.93
S.L.	7.1	287.9
0+47 = $\frac{1}{4}$ 3.4' walk on south (0.2 inst feet).		
S.L.	6.4	288.6
SL+0.8	6.40	288.63
Cb	6.8	288.23
$\frac{1}{4}$	7.1	287.9
$\frac{1}{4}$	7.0	288.0
$\frac{1}{4}$	7.2	287.8

95

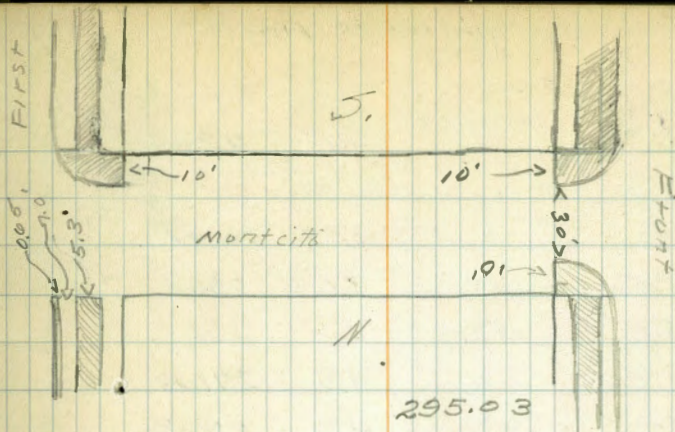
295.03

Cb	7.1	287.93
NL	6.5	288.5
0+94 = $\frac{1}{4}$ 7' drive on south (0.5 Back)		
NL	6.0	289.0
Cb	6.4	288.63
$\frac{1}{4}$	6.5	288.5
$\frac{1}{4}$	6.0	289.0
$\frac{1}{4}$	6.0	289.0
Cb	6.4	288.63
SL	5.9	289.1
+0.5 on concrete 5.94 289.09		
1+07 = $\frac{1}{4}$ garage on North + South		
SL-2	5.5	289.5
SL	5.7	289.3
Cb	5.9	289.13
$\frac{1}{4}$	5.6	289.4
$\frac{1}{4}$	5.8	289.2
$\frac{1}{4}$	6.3	288.7
Cb	6.3	288.73
NL	5.6	289.4
+8 = Garage floor 4.9 290.1		
1+41 ⁵⁰ = $\frac{1}{4}$ 2' walk on North (0.6 Back)		
NL-06 (on walk)	4.59	290.44
NL	4.8	290.2
Cb	5.4	289.63
$\frac{1}{4}$	5.7	289.3

Montecito Way

295.03

2 1/4	5.4	289.6
4	5.5	289.5
cb	5.5	289.53
SL	4.9	290.1
2400 = NL First (80' wide)		
3 cb.	4.01	391.02
Gut	4.5	290.5
1/4	4.1	290.9
2	4.4	290.6
1/4	4.4	290.6
cb	4.4	290.63
NL	3.9	291.1
Curb		
NL on cb.	4.05	290.98
NL on ground	4.7	290.3
cb	4.5	290.53
1/4	4.1	290.9
2	3.8	291.2
1/4	4.2	290.8
cb	4.6	290.43
SL on ground	4.8	290.2
SL on cb	4.04	290.99
Quarter		
SL	4.3	290.7
cb	4.2	290.8
1/4	4.1	290.9



46

2	3.7	291.3
1/4	3.9	291.1
cb	4.2	290.8
NL	4.4	290.6
Center		
NL	4.0	291.0
cb	3.9	291.1
1/4	3.9	291.1
2	3.8	291.2
1/4	3.9	291.1
cb	4.0	291.0
SL	4.0	291.0
Quarter		
SL	4.2	290.8
cb	4.1	290.9
1/4	4.1	290.9
2	4.0	291.0
1/4	4.0	291.0
cb	4.1	290.9

Montecito Way

295.03

47

NL	295.03	4.3	290.7
Curb			
NL on cb		4.05	290.98
NL on ground		4.6	290.4
cb		4.3	290.7
$\frac{1}{4}$		4.2	290.8
$\frac{1}{4}$		4.2	290.8
$\frac{1}{4}$		4.3	290.7
cb		4.4	290.6
SL on ground		4.7	290.3
SL on cb		3.92	291.01
0+00 = EL First (All curbs & walk in)			
s cb		4.03	291.00
Gut		4.7	290.3
$\frac{1}{4}$		4.5	290.5
$\frac{1}{4}$		4.3	290.7
$\frac{1}{4}$		4.4	290.6
Gut		4.8	290.2
Ncb		4.06	290.97
0+50			
n cb		4.93	290.10
Gut		5.6	289.4
$\frac{1}{4}$		5.3	289.7
$\frac{1}{4}$		5.0	290.0
$\frac{1}{4}$		5.1	289.9
Gut		5.3	289.7

s cb	465	290.38
0+90 = $\frac{1}{4}$ 15' con, drive on south		
$\frac{1}{4}$ 21' con drive on North		
S Gut	5.63	289.40
$\frac{1}{4}$	5.6	289.4
$\frac{1}{4}$	5.5	289.5
$\frac{1}{4}$	5.9	289.1
N Gut	6.19	288.84
(1+00 = $\frac{1}{4}$ 10.5 drive on N) ($\frac{1}{4}$ 9.6 drive on south)		
N Gut	6.48	288.55
S Gut	5.98	289.05
1+50		
Ncb	6.65	288.48
Gut	7.2	287.8
$\frac{1}{4}$	6.9	288.1
$\frac{1}{4}$	6.5	288.5
$\frac{1}{4}$	6.6	288.4
Gut	6.7	288.3
s cb	5.90	289.13
2+00 = WL Bachman		
S cb	6.55	288.48
Gut	7.5	287.5
$\frac{1}{4}$	7.4	287.6
$\frac{1}{4}$	7.2	287.8
$\frac{1}{4}$	7.7	287.3
Gut	7.9	287.1

Montecito Way.

295.03

N cb	7.50	287.53
Curb		
NL cb	7.49	287.54
NL on ground	8.3	286.73
cb	8.2	286.8
$\frac{1}{4}$	8.0	287.0
$\frac{1}{4}$	7.7	287.3
$\frac{1}{4}$	7.7	287.3
cb	7.5	287.5
SL ground	7.3	287.7
SL on cb	6.50	288.53
Quarter		
SL	7.1	287.9
cb	7.1	287.9
$\frac{1}{4}$	7.1	287.9
$\frac{1}{4}$	7.4	287.6
$\frac{1}{4}$	7.5	287.5
cb	7.7	287.3
NL	8.1	286.9
Center		
NL	7.5	287.5
cb	7.4	287.6
$\frac{1}{4}$	7.3	287.7
$\frac{1}{4}$	7.1	287.9
$\frac{1}{4}$	6.9	288.1
SL cb	6.6	288.4

295.03

48

SL	6.5	288.5
Quarter		
SL	7.2	287.8
cb	7.3	287.7
$\frac{1}{4}$	7.3	287.7
$\frac{1}{4}$	7.4	287.6
$\frac{1}{4}$	7.7	287.3
cb	7.9	287.1
NL	8.3	286.7
Curb		
NL on cb	8.03	287.00
NL on ground	8.3	286.7
cb	8.3	286.7
$\frac{1}{4}$	8.0	287.0
$\frac{1}{4}$	7.6	287.4
$\frac{1}{4}$	7.6	287.4
cb	7.9	287.1
SL on ground	7.4	287.4
SL on cb	7.00	288.03
T.P.	3.90	290.58
	7.85	287.18
0+00 = EL Bachman (walks + cbs in)		
S cb	2.53	288.05
Gut	3.3	287.3
$\frac{1}{4}$	3.5	287.1
$\frac{1}{4}$	3.2	287.4
$\frac{1}{4}$	3.7	286.9

Montecito Way

Gut	290.58	4.1	286.5
N cb		3.55	287.05
0+50			
N cb		4.19	286.39
Gut		4.6	286.0
$\frac{1}{4}$		4.3	286.3
$\frac{1}{4}$		3.9	286.7
$\frac{1}{4}$		4.0	286.6
Gut		4.3	286.3
S cb		3.42	287.16

0+95 = 2 9.4' con drives on N+S.

S Gut		4.73	285.85
$\frac{1}{4}$		5.0	285.6
$\frac{1}{4}$		4.7	285.9
$\frac{1}{4}$		5.1	285.5
N Gut		5.30	285.28

1+06 = 2 10' drives on N+S.

N Gut on con.		5.39	285.19
S Gut on con.		5.06	285.52

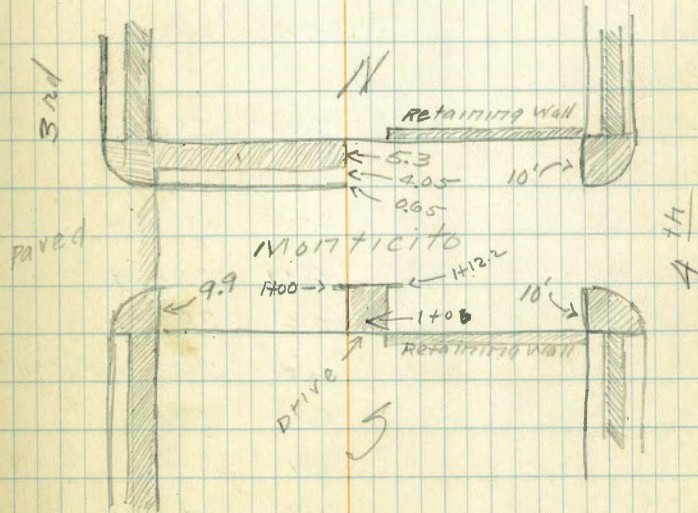
1+17⁸⁰ = 2 8.4' drive on south

S Gut		5.20	285.38
-------	--	------	--------

1+65 = 2 9.7' con. drive on North

N Gut on con		6.07	284.51
$\frac{1}{4}$		5.8	284.8
$\frac{1}{4}$		5.5	285.1
$\frac{1}{4}$		5.6	285.0

Gut	290.58	5.6	285.0
S cb		5.01	285.57
2+29 ⁸⁰ = WL 3 rd st			(intersection paved)
S cb		5.18	285.10
Gut on paving		6.00	284.58
$\frac{1}{4}$ " "		5.85	284.73
$\frac{1}{4}$ " "		5.89	284.74
$\frac{1}{4}$ " "		6.06	284.52
Gut " "		6.45	284.13
N cb		6.06	284.52
0+00 = EL 3 rd st			
N cb		5.56	285.02



Gut on paving		6.09	284.49
$\frac{1}{4}$ " "		5.79	284.29
$\frac{1}{4}$		5.58	285.00

Montecito Way

653
290.58

290.58

1/4	5.70	284.88
Gut	6.11	284.47
S cb	5.55	285.03
0+50		
SL	5.6	285.0
cb	6.3	284.28
+1	6.8	283.8
1/4	6.5	284.1
2	6.1	284.5
1/4	6.4	284.2
Gut	6.6	284.0
N cb	6.03	284.55
0+95 = 2 con drive on N		
Gut	6.92	283.66
1+00 = End of cb + walk on North		
N L	6.15	284.43
N cb	6.44	284.14
Gut	6.6	284.0
1/4	6.7	283.9
2	6.6	284.0
1/4	6.9	283.7
Gut	6.86	283.72
S cb W. End of drive on South	6.53	284.05
1+06 = 2 12' con drive on South (see sketch)		
S Gut	7.11	283.47

1+12.2 = E End of drive on south

S cb	6.65	283.93
1+50		
SL	6.9	283.68
cb	7.2	283.38
+2	7.6	283.0
1/4	7.4	283.2
2	7.0	283.6
1/4	7.1	283.2
cb	7.3	283.28
N L	6.7	283.88
2+00 = WL 4 th		
N cb	7.43	283.15
Gut	7.9	282.68
1/4	7.9	282.7
2	7.6	283.0
1/4	8.0	282.6
Gut	8.0	282.6
S cb	7.44	283.14
T.P	3.03	287.55
BM		287.54

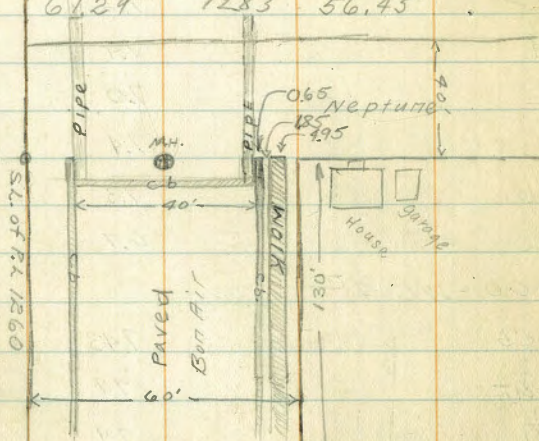
(40' wide 8' cb 6' gts.)

X sec Neptune, Bon Air
to Westbourne St
0+00 = N.L. Bon Air

B.M. N.W.B.P. Greville & LaJolly Blvd 68.86

T.P. 0.42 69.28

T.P. 4.84 61.29 12.83 56.45



T.P. 0.42 49.02 12.69 48.60

T.P. 0.37 36.76 12.63 36.39

T.P. 4.50 33.55 7.71 29.05

S.L. Bon Air - 19'

E.L. 22.5 11.1

C.B. 23.0 10.6

4 22.9 10.7

4 22.9 10.7

4 23.1 10.5

C.B. 23.3 10.3

W.L. 23.4 10.2

BL-10

W.L. 21.2 13.4

C.B. 21.4 12.2

4 20.9 12.7

4 20.9 12.7

+3 17.3 16.3

4 18.2 15.4

C.B. 17.8 15.8

E.L. 14.8 18.8

0+00 = S.L. Bon Air (60' wide) (8' cb 6' gts.)

E.L. 10.5 23.1

C.B. 12.5 21.1

4 13.5 20.1

4 16.3 17.3

4 18.0 15.6

C.B. 20.0 13.6

W.L. 18.4 18.2

+10 19.1 14.5

Curb

W.L.-10 12.0 21.6

W.L. 13.4 20.2

C.B. 15.2 18.4

4 15.4 18.2

4 9.9 23.7

4 6.4 27.2

+2 5.5 28.1

cb	5.5	28.1
EL on curb End	4.71	28.84
+3.0 = W Edge of cb	4.47	29.08
+3.65 = EL. 1' drain also pavement	5.27	28.28

Quarter

EL-3.65 on pavement	4.57	28.98
-3.0 on cb	4.40	29.15
EL.	4.5	29.1
cb	4.9	28.7
$\frac{1}{4}$	5.1	28.5
$\frac{1}{4}$	5.3	28.3
$\frac{1}{4}$	5.8	27.8
cb	6.9	26.7
WL	8.4	25.2
+10	10.3	23.3

Center

WL-10	8.6	25.0
WL.	6.7	26.9
cb	5.5	28.1
$\frac{1}{4}$	5.2	28.4
$\frac{1}{4}$	4.9	28.7
$\frac{1}{4}$	4.9	28.7
cb	4.6	29.0
EL	4.0	29.6
+1 = Q M.H.	3.88	29.67
Flowline M.H.	6.18	27.37

+3. = West edge of cb	4.29	29.26
+3.65 = Pavement	4.42	29.13

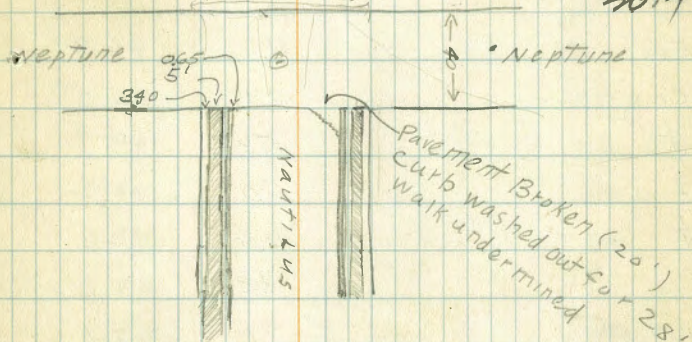
Quarter

EL-3.65 on pavement	4.47	29.08
-3. = wedge of cb	4.29	29.31
EL.	4.2	29.4
cb	4.2	29.4
$\frac{1}{4}$	4.5	29.1
$\frac{1}{4}$	4.5	29.1
$\frac{1}{4}$	4.7	28.9
cb	4.9	28.7
WL.	5.7	27.9
+10	6.9	26.7

Curb

WL-10	7.1	26.5
WL	6.9	26.7
cb	6.6	27.0
$\frac{1}{4}$	5.2	28.4
$\frac{1}{4}$	5.0	28.6
$\frac{1}{4}$	5.0	28.6
cb	4.6	29.0
EL on curb End	4.47	29.08
+3. = W. Edge of Pavement	4.19	29.36
3.8 = pavement	5.08	28.47
10+00 = N.L. Bon Air		
EL	3.9	29.7

cb	4.4	29.2	+	3.8	29.8
$\frac{1}{4}$	4.7	28.9	±	3.5	29.1
±	5.0	28.6	+	3.3	29.3
$\frac{1}{4}$	5.1	28.5	cb	3.8	29.8
cb	5.2	28.4	EL	3.7	29.4
WL	5.4	28.2			
0+28 ⁷⁰ = Concrete entrance to dwelling on East (8.7 wide)					
WL	5.8	27.8			
cb	5.6	28.0			
$\frac{1}{4}$	5.4	28.7			
±	5.4	28.7			
$\frac{1}{4}$	5.2	28.4			
cb	5.0	28.6	T.P.	761	4018 ✓
	4.08	29.47	0+81	0.98	32.57 ✓
EL on concrete entrance					
0+44 ⁵⁹ = Garage on East					
EL-2.5 = door	3.6	30.0	±	8.2	32.0
EL	3.9	29.7	cb	8.0	32.2
cb	4.3	29.3	$\frac{1}{4}$	6.7	33.6
$\frac{1}{4}$	4.7	28.9	±	6.6	33.6
±	5.0	28.6	±	7.1	33.1
$\frac{1}{4}$	5.2	28.4	cb	6.4	33.8
cb	5.4	28.7	WL	7.9	32.3
WL	5.4	28.7	0+92	9.3	30.9
0+65					
WL	5.3	28.3	WL	8.3	21.9
cb	4.4	29.2	cb	7.5	32.7
			$\frac{1}{4}$	6.2	34.0



£	6.0	34.2
$\frac{1}{4}$	5.3	34.9
cb	4.4	35.8
EL	3.4	36.8
1+40		
EL	4.0	36.2
cb	4.7	35.5
$\frac{1}{4}$	5.3	34.9
£	6.0	34.2
$\frac{1}{4}$	6.6	33.6
cb	7.2	33.0
WL	8.1	32.1
1+90		
WL	8.6	31.6
cb	7.8	32.4
$\frac{1}{4}$	7.3	32.9
£	7.1	33.1
$\frac{1}{4}$	6.4	33.8
cb	5.6	34.6
EL	4.5	35.7
2+40		
EL	5.9	34.3
cb	6.6	33.6
$\frac{1}{4}$	7.3	32.9
£	7.6	32.6
$\frac{1}{4}$	8.0	32.2

cb	8.5	31.7
WL	9.2	31.0
2+75 = SL Nautikus (60' wide) ^{10' cbs} 10' gts		
WL	9.5	30.7
cb	9.1	31.1
$\frac{1}{4}$	8.2	32.0
£	8.1	32.1
$\frac{1}{4}$	7.6	32.6
cb	6.8	33.4
EL	6.1	34.1
Curb		
EL on end of curb	6.70	33.48
EL on pavement	7.13	33.05
cb	7.1	33.1
$\frac{1}{4}$	7.6	32.6
£	8.2	32.0
$\frac{1}{4}$	8.3	31.9
cb	9.0	31.2
WL	9.2	31.0
Quarter,		
WL	10.0	30.2
cb	8.9	31.3
+3	9.1	31.1
$\frac{1}{4}$	10.1	30.1
+5	8.1	32.1
£	7.9	32.3

1/4	7.7	32.5
cb	7.4	32.8
EL on pavement	6.67	33.51
Center		
EL on Pavement	6.34	33.84
cb	7.0	33.2
1/4	8.0	32.2
1/2	8.4	31.8
1/4	8.6	31.6
{ +4.2 = 1/2 Man Hole	8.61	31.57
{ F.L. Man Hole	15.18	25.00
cb	14.2	26.0
WL	13.2	27.0
+10	16.4	23.8
Quarter		
WL-1	9.6	30.6
WL	16.3	23.9
cb	12.8	27.4
1/4	11.6	28.6
1/2	10.0	30.2
1/4	8.8	31.4
cb	7.3	32.9
EL (on dirt)	6.3	33.9
Curb		
EL on dirt	6.7	33.5
cb	7.6	32.6

1/4	8.4	31.8
1/2	9.5	30.7
1/4	10.4	29.8
cb	14.8	25.4
+2	8.7	31.5
WL	9.3	30.9
OWN L Nautilus		
WL	13.6	26.6
cb	13.5	26.7
1/4	13.0	27.2
+5 on Top water valve	9.15	31.03
1/2	11.5	28.7
1/4	10.5	29.7
cb	9.4	30.8
+6	9.4	30.8
+7	6.4	33.8
EL	6.0	33.2
T.P. 1.96	389.6	318
		37.00
0+15		
EL	4.8	34.2
cb	5.9	33.1
1/4	6.7	32.3
+5	7.1	31.9
1/2	9.6	29.4
1/4	10.4	28.6
+4	13.7	25.3

π 38.96

cb	13.8	26.2
+3	7.9	31.1
WL	8.4	30.6
0+36	11.1	
WL	11.1	27.9
cb	7.8	30.2
$\frac{1}{4}$	7.8	31.2
£	7.1	31.9
$\frac{1}{4}$	7.1	31.9
cb	6.7	32.3
E.L.	5.5	33.5
0+50		
EL	5.5	33.5
cb	6.5	32.5
$\frac{1}{4}$	6.8	32.2
£	7.4	31.6
$\frac{1}{4}$	8.5	30.6
cb	8.4	30.6
WL	8.6	30.4
1+00		
W-10	10.1	28.9
WL	8.6	30.4
cb	8.0	31.0
$\frac{1}{4}$	7.8	31.2
£	7.5	31.5
$\frac{1}{4}$	6.8	32.2
cb	6.0	33.0

2+30 2+70 2+99.50
 30.0 13.0 145.00
 124.05 124.95 1239.50

56

EL	5.2	33.8
1+45		
EL	5.6	33.4
cb	6.4	32.6
$\frac{1}{4}$	7.0	32.0
£	7.7	31.3
+5	7.9	31.1
$\frac{1}{4}$	9.2	29.8
cb	8.5	30.5
WL	9.0	30.0
1+70		
WL-15	23.0	16.0
WL	17.0	22.0
cb	11.6	27.4
+4	7.6	31.4
$\frac{1}{4}$	7.3	31.7
£	7.7	31.3
$\frac{1}{4}$	6.9	32.1
cb	6.7	32.3
EL	6.2	32.8
2+00		
EL	6.5	32.5
cb	6.7	32.3
$\frac{1}{4}$	7.2	31.8
£	9.6	29.4
$\frac{1}{4}$	12.3	26.7

2779.5
270.1
785.5

2779.5
271.3
1065

57

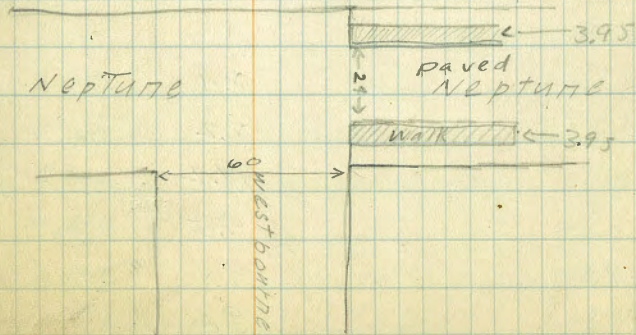
+15 = sewer pipe exposed

Top of pipe	14.5	24.5
cb	14.5	24.5
WL	16.8	22.2
+5	29.8	9.2
2+01		
WL-5	17.0	23.0
WL	16.8	22.2
2+13		
WL	9.8	29.2
cb	9.2	29.8
$\frac{1}{4}$	8.2	30.8
$\frac{1}{4}$	8.1	30.9
$\frac{1}{4}$	7.5	31.5
cb	7.1	31.9
EL	6.5	32.5
2+65		
EL	7.2	31.8
cb	7.5	31.5
$\frac{1}{4}$	8.0	31.0
$\frac{1}{4}$	8.5	30.5
$\frac{1}{4}$	8.5	30.5
cb	8.1	30.9
+5	10.2	28.8
WL	10.2	28.8

2+66		
WL	17.2	26.8
cb	8.4	20.6
$\frac{1}{4}$	8.4	20.6
2+79.50 = SL Westbourne (60' wide)		
WL	12.4	26.6
cb	10.1	28.9
$\frac{1}{4}$	8.7	30.3
$\frac{1}{4}$	8.4	30.6
$\frac{1}{4}$	7.8	31.2
cb	7.9	31.1
+4	8.0	31.0
EL	9.1	29.9
SL Westbourne +3		
EL - 2 = Fire plug		
Base of plug	10.3	28.7
Curb		
EL	9.3	29.7
+5	10.3	28.7
cb	8.4	20.6
$\frac{1}{4}$	8.9	30.1
$\frac{1}{4}$	9.0	30.0
$\frac{1}{4}$	9.0	30.0
cb	9.1	29.9
WL	10.4	28.6

Quarter

WL	10.5	28.5	cb	10.7	28.3 ⁵⁸
cb	9.2	29.8	$\frac{1}{4}$	10.7	28.3
$\frac{1}{4}$	8.7	30.3	$\frac{1}{4}$	10.7	28.3
$\frac{1}{4}$	9.2	29.8	$\frac{1}{4}$	10.4	28.6
$\frac{1}{4}$	8.8	30.2	cb	10.9	28.1
cb	8.4	30.6	WL	11.7	27.3
EL	8.6	30.4	+10 NL Westbourne	12.3	
Center			-10 WL	11.1	27.7
EL	8.9	30.1	cb (at end of curb)	11.3	26.92
+3	8.1	30.9	Gut on paving	12.03	26.40
cb	8.7	30.3	+1	12.56	
$\frac{1}{4}$	9.2	29.8	$\frac{1}{4}$	11.2+	
$\frac{1}{4}$	9.3	29.7	$\frac{1}{4}$	12.04	26.92
$\frac{1}{4}$	9.5	29.5	$\frac{1}{4}$	11.73	27.23
cb	9.8	29.2	Gut	11.63	27.33
WL	10.2	28.8	Ech	11.79	27.17
+10	10.6		+6	11.05	27.91
Quarter			EL	10.3	28.7
-10	11.7	27.9		9.0	30.0
WL	11.1				
cb	10.3	28.7			
$\frac{1}{4}$	10.0	29.0			
$\frac{1}{4}$	10.0	29.0			
$\frac{1}{4}$	10.0	29.0			
cb	9.7	29.3			
EL	9.7	29.3			
Curb					
EL	10.6	28.4			



60' wide
10' cbs 10' gts

59

X sec Westbourne ✓

T.P.	12.98	433.7	8.07	30.89
0+00 = E.L.	Neptune			
SL		13.3	30.1	
+5		15.2	28.2	
CB		14.0	28.6	
$\frac{1}{4}$		13.1	30.3	
☐		13.3	30.1	
$\frac{1}{4}$		14.2	29.2	
CB		14.8	28.6	
NL		13.4	30.0	
0+10				
NL		12.4	31.0	
CB		13.2	30.2	
$\frac{1}{4}$		13.6	29.8	
☐		12.7	30.7	
$\frac{1}{4}$		12.3	31.1	
CB		10.8	32.6	
SL		11.2	32.2	
0+30				
SL		8.4	35.0	
CB		8.2	35.2	
$\frac{1}{4}$		9.2	34.2	
☐		9.5	33.9	
$\frac{1}{4}$		9.8	33.6	
CB		9.6	33.8	

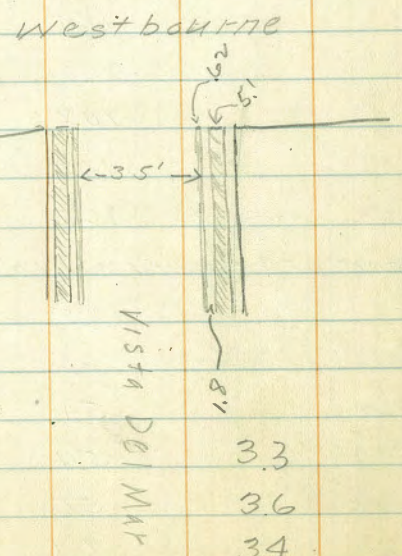
Plotted
H.C.H.
3/23/28

Wardage
1/24
6/19/28

NL		9.8	33.6
1+00			
NL		3.3	40.1
CB		3.6	39.8
$\frac{1}{4}$		2.8	40.6
☐		2.3	41.1
$\frac{1}{4}$		2.7	40.7
CB		1.4	42.0
SL		1.2	42.2
T.P.	12.42	55.39	0.90 42.97
1+25			
SL		10.8	44.6
CB		10.7	44.7
$\frac{1}{4}$		11.4	44.0
☐		11.0	44.4
$\frac{1}{4}$		10.8	44.6
CB		10.0	45.4
NL		12.2	43.2
1+67 ⁵⁰	= Start of retaining wall on North		
NL		8.5	46.9
+1		6.6	48.8
CB		5.4	50.0
$\frac{1}{4}$		5.9	49.5
☐		5.6	49.8
$\frac{1}{4}$		6.1	49.3
CB		6.2	49.2

SL	6.1	49.3
1+85		
SL	4.7	50.7
cb	4.5	50.9
$\frac{1}{4}$	4.3	51.1
$\frac{1}{4}$	4.4	51.0
$\frac{1}{4}$	4.6	50.8
+5	4.1	51.3
cb	4.5	50.9
NL	5.3	50.1

2+20 = W. Vista Del Mar	(55' wide)	$\left. \begin{matrix} 10 \text{ cbs} \\ 8.8 \text{ pts} \end{matrix} \right\}$
NL	4.4	51.0
cb	3.9	51.5



$\frac{1}{4}$	3.3	52.1
$\frac{1}{4}$	3.6	51.8
$\frac{1}{4}$	3.4	52.0
cb	3.0	52.4

SL	2.9	52.5
Curb		
SL	2.6	52.8
cb	2.5	52.9
$\frac{1}{4}$	2.7	52.7
$\frac{1}{4}$	3.4	52.0
$\frac{1}{4}$	3.5	51.9
cb	4.0	51.4
NL (on End of cb)	4.82	50.57
NL (on paving)	5.32	50.07

Quarter		
NL on paving	4.77	50.62
cb	4.0	51.4
$\frac{1}{4}$	3.4	52.0
$\frac{1}{4}$	3.0	52.4
$\frac{1}{4}$	2.9	53.0
cb	2.1	53.3
SL	2.2	53.2

T.P. 1029 62.36 3.32 52.07

Center		
SL	8.6	53.8
cb	8.8	53.6
$\frac{1}{4}$	9.1	53.3
$\frac{1}{4}$	9.8	53.6
$\frac{1}{4}$	10.4	52.0
cb	10.9	51.5

60

NL	on paving	11.29	57.07	0+50		
Quarter				SL	6.3	56.1
NL	" "	11.49	57.17	cb	6.6	55.8
cb		10.9	57.5	$\frac{1}{4}$	6.9	55.5
$\frac{1}{4}$		10.1	57.3	$\frac{1}{4}$	6.9	55.5
$\frac{1}{4}$		9.4	57.0	$\frac{1}{4}$	7.0	55.4
$\frac{1}{4}$		9.0	57.4	cb	7.0	55.4
cb		8.5	57.9	NL	7.6	54.8
SL		8.2	57.2	1+00		
Curb				NL	5.9	56.5
SL		8.0	57.4	cb	5.2	57.2
cb		8.4	57.0	$\frac{1}{4}$	5.4	57.0
$\frac{1}{4}$		8.4	57.0	$\frac{1}{4}$	5.3	57.1
$\frac{1}{4}$		9.2	57.2	$\frac{1}{4}$	5.3	57.1
$\frac{1}{4}$		9.7	57.7	cb	5.0	57.4
cb		10.4	57.0	SL	4.9	57.5
NL	(on curb)	10.79	57.57	1+50		
NL	(on paving)	11.47	57.89	SL	3.6	58.8
0+00 = EL Vista Del Mar				cb	4.0	58.4
NL		10.5	57.9	$\frac{1}{4}$	4.2	58.2
cb		9.3	57.3	$\frac{1}{4}$	4.1	58.3
$\frac{1}{4}$		8.9	57.5	$\frac{1}{4}$	4.4	58.0
$\frac{1}{4}$		9.1	57.3	cb	4.4	58.0
$\frac{1}{4}$		8.1	57.3	NL	5.0	57.4
cb		7.7	57.7	2+00		
SL		7.7	57.7	NL	3.8	58.6

2 + 79.50
 1 + 30
 1 + 49.50

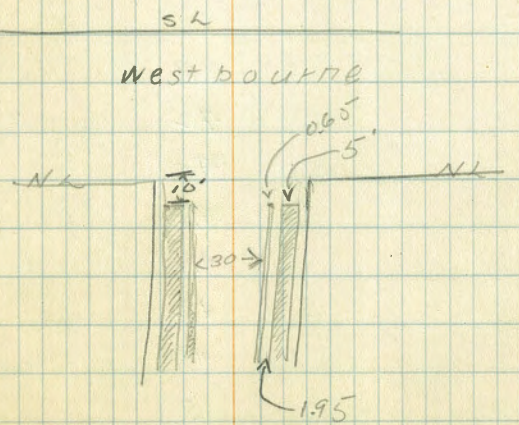
cb			3.0	59.4	7
7			3.2	59.2	2
2			3.0	59.4	7
7			3.1	59.3	cb
cb			3.0	59.4	NL
SL			2.7	59.7	4+00
2+50					NL
SL			1.8	60.6	cb
cb			2.0	60.4	7
7			2.2	60.2	2
2			2.1	60.3	7
7			2.2	60.2	cb
cb			1.9	60.5	SL
NL			2.6	59.8	4+60
T.P.	9.27	69.74	1.89	60.47	SL (on walk)
3+00					
NL			9.0	60.7	
cb			8.3	61.4	
7			8.4	61.3	
2			8.4	61.3	
7			8.4	61.3	
cb			8.2	61.5	
SL			8.1	61.6	
3+50					
SL			7.3	62.4	cb
cb			7.4	62.3	7

Hd. 6974

62

7.3	62.4
7.0	62.7
6.6	63.1
6.5	63.2
7.6	62.1
6.3	63.4
5.7	64.0
5.8	63.9
5.8	63.9
5.9	63.8
5.9	63.8
5.8	63.9
4.09	65.65

3' walk on South (0.25 in street), 10' cbs
 4+60 } = NL Monte Vista (50' wide) 7 1/2' gts
 SL (on walk)



4.4	653
4.5	652

♀	4.5	65.2	NL	4.7	65.0
$\frac{1}{4}$	4.5	65.2	cb	4.0	65.7
cb	4.6	65.1	$\frac{1}{4}$	3.8	65.9
NL	5.0	64.7	♀	3.7	66.0
+10	4.9	64.8	$\frac{1}{4}$	4.1	65.6
Curb			cb	4.0	65.7
NL-10 (on end of cb)	5.34	64.40	SL	3.6	66.1
NL-10 on ground	5.5	64.2	Quarter		
NL	5.2	64.5	SL	3.5	66.2
cb	4.7	65.0	cb	3.9	65.8
$\frac{1}{4}$	4.2	65.5	$\frac{1}{4}$	3.9	65.8
♀	4.2	65.5	♀	3.6	66.1
$\frac{1}{4}$	4.2	65.5	$\frac{1}{4}$	3.8	65.9
cb	4.3	65.4	cb	4.0	65.7
SL	4.1	65.6	NL	4.7	65.0
Quarter			+10	5.0	64.7
SL	3.8	65.9	Curb		
cb	4.2	65.5	NL-10 (on curb)	4.85	64.89
$\frac{1}{4}$	4.1	65.6	NL-10 (on ground)	5.2	64.5
♀	3.8	65.9	NL	5.1	64.6
$\frac{1}{4}$	4.0	65.7	cb	4.1	65.6
cb	4.2	65.5	$\frac{1}{4}$	3.8	65.9
NL	4.8	64.9	♀	3.6	66.1
+10	5.3	64.7	$\frac{1}{4}$	3.8	65.9
Center			cb	3.7	66.0
NL-10	5.0	64.7	SL	3.4	66.3

0+00 = EL

SL	3.3	66.4
cb	3.5	66.2
$\frac{1}{4}$	3.6	66.1
$\frac{1}{2}$	3.6	66.1
$\frac{3}{4}$	3.6	66.1
cb	3.7	66.0
NL	4.5	65.2
t/o	4.4	65.3

0+50

NL	3.0	66.7
cb	2.3	67.4
$\frac{1}{4}$	1.9	67.3
$\frac{1}{2}$	2.0	67.7
$\frac{3}{4}$	1.9	67.8
cb	2.2	67.5
SL	2.3	67.4

TP 11.39 79.86^v 1.27 68.47^v{ 0+81 = $\frac{1}{2}$ walk on South (0.8 in street)

on walk	11.39	68.47
1+00		
SL	11.1	68.9
cb	11.1	68.8
$\frac{1}{4}$	11.2	68.7
$\frac{1}{2}$	11.3	68.6
$\frac{3}{4}$	11.3	68.6

cb 11.4 68.5

NL 12.0 67.9

1+50

NL 10.8 69.1

cb 10.0 69.9

 $\frac{1}{4}$ 10.2 69.7 $\frac{1}{2}$ 10.2 69.7 $\frac{3}{4}$ 10.1 69.8

cb 9.9 70.0

SL 9.6 70.3

2+00

SL 8.4 71.5

cb 8.7 71.2

 $\frac{1}{4}$ 8.6 71.3 $\frac{1}{2}$ 8.5 71.4 $\frac{3}{4}$ 8.7 71.2

cb 8.3 71.6

NL 9.4 70.5

2+50

NL 7.7 72.2

cb 7.5 72.4

 $\frac{1}{4}$ 7.4 72.5 $\frac{1}{2}$ 7.3 72.6 $\frac{3}{4}$ 7.3 72.6

cb 7.2 72.7

SL 7.1 72.8

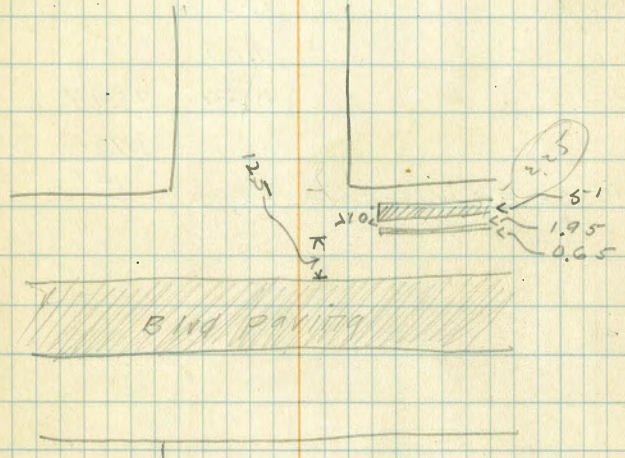
3700		
SL	6.0	73.9
cb	6.2	73.7
$\frac{1}{4}$	6.1	73.8
$\frac{1}{4}$	5.9	74.0
$\frac{1}{4}$	6.0	73.9
cb	6.0	73.9
NL	6.5	73.4

3750		
NL	4.9	75.0
cb	4.9	75.0
$\frac{1}{4}$	4.8	75.1
$\frac{1}{4}$	4.5	75.4
$\frac{1}{4}$	4.7	75.2
cb	5.0	74.9
SL	5.1	74.8

4100		
SL	3.0	76.9
cb	3.2	76.7
$\frac{1}{4}$	3.4	76.5
$\frac{1}{4}$	2.8	77.1
$\frac{1}{4}$	3.0	76.9
cb	3.1	76.8
NL	3.0	76.9

4+60.5 = NL La Jolla Blvd
 NL 1.8 78.1

cb	1.6	78.3
$\frac{1}{4}$	1.4	78.5
$\frac{1}{4}$	1.3	78.6
$\frac{1}{4}$	1.2	78.7
cb	1.0	78.9
SL	0.8	79.1



CURB

SL	0.7	79.2
cb	0.8	79.1
$\frac{1}{4}$	0.9	79.0
$\frac{1}{4}$	1.0	78.9
$\frac{1}{4}$	1.2	78.7
cb	1.2	78.7
NL	1.5	78.4
+10 = (on cb)	1.61	78.25

CURB + 12.5 = wedge paving

07 paring

NK	1.48	78.38
Cb	1.41	78.45
$\frac{1}{4}$	1.38	78.48
$\frac{1}{4}$	1.28	78.58
$\frac{1}{4}$	1.16	78.70
Cb	1.13	78.73
SL	1.09	78.77
T.P.	0.89	78.97

 79.01

.04

B.M. SE. BR. Westbourne Blvd.

Bliss
Isbell
Hobbs
410' E BP
B N N E BP
Rosecrans & Nichols

X. Sections of Nichols St. La Playa from
the E. line of Rosecrans to 296 East

4458

87

Elev 10 cbs
7 5/8'

2.96 44.58 41.62

Sec 1. On the cb line of Rosecrans

S Top cb on Street line 3.50 41.08

cb 3.4 40.7

1/4 3.5 41.1

1/2 3.4 41.2

1/4 3.3 41.3

cb 3.3 41.3

N Top on line 2.97 41.61

Sec 2. on Paving Rosecrans

N 3.16 41.42

cb 3.33 41.25

1/4 3.42 41.16

1/2 3.49 41.09

1/4 3.56 41.02

cb 3.61 40.97

S 3.73 40.85

of 00. E line Rosecrans

S 2.8 41.8

+1 3.3 41.3

cb 3.0 41.6

+5 3.4 41.2

1/4 3.4 41.2

1/2 3.4 41.2

1/4 3.4 41.2

+5 3.8 40.8

cb 3.8 40.8

N 3.3 41.3

05' E

N 3.5 41.1

+5 3.6 41.0

cb 4.0 40.6

1/4 3.5 41.1

1/2 3.5 41.1

1/4 3.5 41.1

cb 3.1 41.5

+3 2.6 42.0

S 2.9 42.2

16' E

S 3.2 41.4

+7 4.3 40.3

cb 4.2 40.4

1/4 4.0 40.6

1/2 4.1 40.5

1/4 4.3 40.3

+4 5.0 39.6

+6 5.0 39.6

cb 4.1 40.5

N 4.3 40.3

35' E

N 5.7 38.9

+5 5.6 39.0

X
94.58

+8	7.0	37.6
cb	7.0	37.6
+3	5.7	38.9
1/4	5.9	38.7
⊕	5.7	38.9
1/4	5.8	38.8
cb	5.9	38.7
+5	5.6	39.0
S	4.4	40.2
	50'E	
S	6.7	37.9
cb	7.0	37.6
1/4	7.1	37.5
⊕	7.8	36.8
1/4	7.9	36.7
+2	7.5	37.1
+6	7.3	37.3
cb	8.2	36.4
+2	7.3	37.3
N	7.8	36.8
	75'E	
N	9.8	34.8
+8	9.5	35.1
cb	9.2	35.0
1/4	9.7	34.9
⊕	9.7	34.9

X
49.58

18

1/4	9.9	35.2
+5	9.3	35.3
+6	9.0	35.6
cb	9.0	35.6
S	8.9	35.7
	100'E	
S	10.9	33.7
cb	11.0	33.6
1/4	11.2	33.4
⊕	11.4	33.2
1/4	11.3	33.3
cb	11.4	33.2
N	11.5	33.1
	115' East	
N	12.9	31.7
cb	12.6	32.0
1/4	12.6	32.0
⊕	12.8	31.8
1/4	12.7	31.9
cb	12.2	32.4
+5	12.2	32.4
S	12.2	32.4
T.P.	0.36	32.40
		12.59
		32.09
		125'E
S	1.3	31.1
+5	1.3	31.1

32.40

cb	1.0	31.4
1/4	1.4	31.0
1/2	1.5	30.9
1/4	1.0	31.4
cb	1.4	31.0
N	1.6	30.8
140'E		
N	2.8	29.6
cb	2.9	29.5
1/4	3.0	29.4
1/2	2.8	29.6
1/4	2.5	29.9
1/2	2.5	29.9
cb	2.2	30.2
S	2.2	30.2
152'E		
S	3.5	28.9
1/3	3.1	29.3
cb	3.1	29.3
1/4	3.3	29.1
1/2	3.6	28.8
1/4	3.9	28.5
cb	4.0	28.4
1/2	3.5	28.9
N	3.9	28.5

166' East

32.40

69

N	5.2	27.2
cb	4.7	27.7
1/4	4.9	27.5
1/2	4.9	27.5
1/4	5.0	27.4
1/2	5.0	27.4
cb	4.4	28.0
S	5.2	27.2
181' East		
S	5.8	26.6
cb	5.3	27.1
1/4	5.7	26.7
1/2	5.6	26.8
1/4	5.6	26.8
cb	5.5	26.9
N	5.3	27.1
193'E		
N	6.3	26.1
1/2	6.4	26.0
cb	6.7	25.7
1/4	6.6	25.8
1/2	6.7	25.7
1/4	6.6	25.8
cb	6.2	26.2
S	6.0	26.4

32.40

201'E

S	6.8	25.6
+8	6.9	25.5
cb	7.2	25.2
1/4	7.6	24.8
ϕ	7.6	24.8
1/4	7.7	24.7
cb	7.5	24.9
N	7.2	25.2

207 5 S. 071 N end 3 car Garage

3rd Back floor 7.98 24.42

216'E

N	8.1	24.3
+7	8.8	23.6
cb	8.7	23.7
1/4	9.0	23.4
ϕ	8.8	23.6
1/4	8.5	23.9
cb	8.3	24.1
S	8.2	24.2

234'E S end 3 car Garage

3rd Back floor 8.01 24.39

238'E

N	10.3	22.1
cb	10.3	22.1
1/4	10.0	22.4
ϕ	10.3	22.1

32.40

1/4	10.4	22.0
cb	10.6	21.8
N	9.9	22.5
T.P	9.86	26.25 11.01

299'E

N	5.0	21.3
+6	4.6	21.7
cb	5.4	20.9
1/4	5.0	21.3

ϕ	4.8	21.5
1/4	5.1	21.2
cb	4.8	21.5
+5	5.2	21.1
S	5.0	21.3

274'E

S	6.4	19.9
cb	6.3	20.0
1/4	6.6	19.7
ϕ	6.4	19.9
+1	6.2	20.1

1/4	6.6	19.7
cb	6.9	19.4
N	6.9	19.4

292'E

N	8.3	18.0
+5	7.6	18.7

26.25

71

cb	7.9	18.9
1/4	7.3	19.0
2	7.2	19.1
1/4	7.7	18.6
+5	8.1	18.2
cb	7.8	18.5
5	7.5	18.8

296 East

5	8.1	18.2
cb	8.2	18.1
1/4	8.3	18.0
2	7.8	18.5
1/4	7.8	18.5
cb	7.8	18.5
N	7.7	18.6

T.P.	12.52	3 833	0.44	25.81
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T.P.	6.77	44.80	0.30	38.03
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check on NF
starting BTH Rosecrans
+ Nichols

3.19	71.61	(01) ✓
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Bliss
Walbeck
3000 US
7/10/5

Additional X Sections of Neptune Place
La Jolla from the S Curline of Westbourne to
S Line of Bon Air

226 33 15 30.89

S. cb. Line of Westbourne

W	4.7	28.5
+7	9.9	28.3
+8	6.2	27.0
+10	7.8	25.4
+15	9.0	24.2

S Line of Westbourne = 00

W	6.7	26.5
+10	7.3	25.9
+14	12.7	20.5
+20	14.0	19.2

0+10

W	7.8	25.4
+5	10.2	23.0
+10	10.7	22.5
+15	11.3	21.9
+25		

0+14.5 = 2+65 old notes

W	7.2	26.0
+4	9.6	28.6
+10	3.0	28.2
+15	5.3	27.9
+20	5.7	27.5

0+16

W	9.5	28.7
+10	4.7	28.5
+15	5.2	28.0
+20	5.8	27.4

0+66.5 = 2+13 old notes

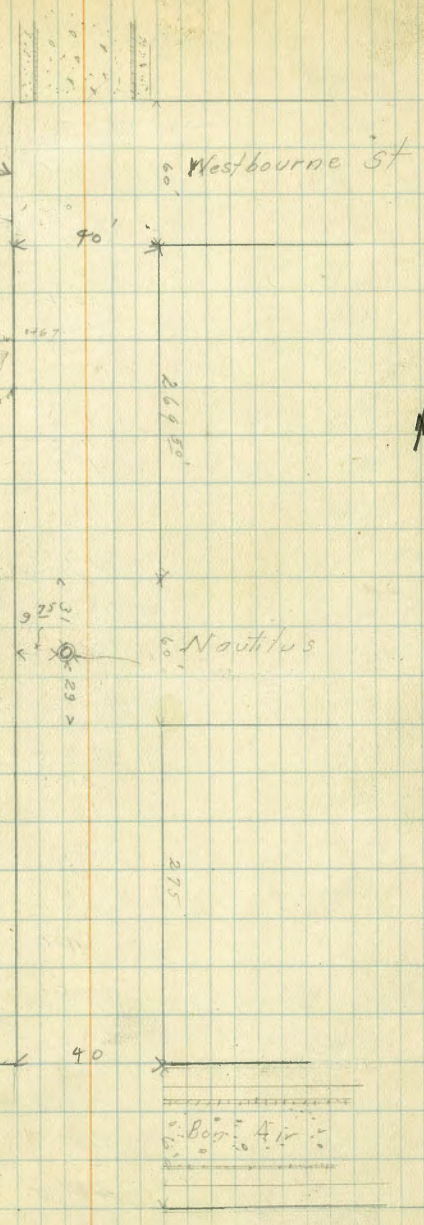
W	4.1	29.1
+10	4.4	28.8
+15	4.9	28.3
+20	5.7	27.5

0+74

W	9.2	24.0
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Note

The line called
the West line in
McHugh's X section of
Neptune Place
was used as a base
line in this additional
X Sec. all + and -
refer to it and it is
designated as the W. line



H.I.
33.15

0+74

+5	8.1	25.1
+10	8.5	24.7
+15	8.4	24.8
+20	9.4	23.8
0+79 ² = 270.0 old notes		
W	10.3	22.9
+10	10.4	22.5
+15	10.7	22.5
+25	11.4	21.8
0+82		
W	11.0	22.2
+10	11.3	21.9
+15	11.8	21.4
+20	14.2	19.0
+25	14.4	18.8
0+85		
W	20.1	13.1
+6	26.0	7.2
+8	20.5	12.7
+10	20.5	12.7
+18	18.0	15.2
+28	18.5	14.7
0+88		
W	14.4	18.8
+11	25.0	8.2
+4	29.5	3.7
+8	29.0	4.2
+9	22.5	10.7
+10	22.5	10.7
+13	22.0	11.2
+30	20.0	13.2

H.I.
33.15

1104

73

W	9.9	23.3
+8	13.0	20.2
+10	15.0	18.2
+11	23.0	10.2
+17	25.7	7.5
+19	28.2	4.6
+21	29.3	3.9
+32	29.3	3.9
+33	26.0	7.2
+39	29.2	4.2
1+09 ⁵⁰ = 1+70 old notes		
W-42	30.2	3.0
W-45	30.0	3.2
W-22	28.5	4.7
W-17	25.2	8.0
W-13	21.3	11.9
W-10	13.7	19.5
W-5	13.6	19.6
W	12.0	21.2
1+16		
W	8.9	24.3
1+23		
W	11.8	21.4
W+6	12.1	21.1
+10	13.3	19.9
+16	15.0	18.2
+18	17.2	16.0

T
33.15

+22	18.2	15.0
+28	22.4	10.8
+35	22.5	10.7

1+26	6.6	26.6
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W	18.0	15.2
W-23	15.0	18.2
W-16	11.3	21.9
W-10	7.2	26.0
W-7	3.9	29.3
W	3.9	29.8

1+34⁵⁰ = 1+95 old notes

W	3.2	30.0
+10	4.5	28.7
+16	9.3	23.9

T.P. 4.96 35 93 2.18 30.97

2+29⁵⁰ = 0+50 old notes

W	5.6	30.3
+2	5.6	30.3
+3	7.4	28.5
+5	7.6	28.3
+10	8.0	27.9
+20	13.6	22.3
+25	15.1	20.8

35.93

10.0

2+34

74

W-25	14.9	21.2
L 12	12.2	23.7
W	5.1	30.8

2+42

W	8.7	27.2
+10	10.3	25.6
+18	11.9	24.0
+21	8.3	27.6
+26	12.5	23.4
+35	16.6	19.3

2+44

W	5.7	30.2
+10	6.3	29.6
+15	9.9	26.0
+20	15.2	20.7
+35	18.5	17.4

2+53

W	13.2	22.7
+4	12.5	23.4
+7	10.5	25.4
+10	10.9	25.0
+13	15.1	20.8
+15	14.5	21.4
+19	15.2	20.7

+22	16.8	19.1
+30	20.8	15.1

20.8?

#1.
35.93

2758

-35	19.8	16.1
-25	16.4	19.5
-18	9.9	26.0
-16	6.7	29.2
-10	6.3	29.6
W	5.5	29.6

2772

W	5.3	30.6
+10	5.9	30.0
+13	6.4	29.5
+16	10.3	25.6
+19	11.3	24.6
+21	12.7	23.2
+28	15.9	20.0
+35	20.0	15.9

2778

-35	19.7	16.2
-22	16.9	19.0
-10	12.9	23.0
W	10.2	25.7

2795 N. Line of Nautilus

W	7.8	28.1
+5	11.6	24.3
+10	12.9	23.0
+22	16.7	19.2
+35	20.0	15.7

N. Line of Nautilus + 03

-35	19.8	16.1
-----	------	------

#2
35.93

1709
2779

27950
1709.50

75

-22	16.5	19.4
-10	12.8	23.1
-7	11.5	24.4
-3	9.8	28.1
W	5.4	30.5

N. Line to 8

W	5.2	30.7
+4	5.5	30.4
+6	9.2	26.7
+8	12.6	23.3
+10	13.9	22.0
+15	15.0	20.9
+22	19.2	16.1
+30	18.6	17.3

N. C. 6

W-30	18.8	17.1
-29	16.1	19.8
-19	13.1	22.8
-17	9.7	26.2
-12	6.6	29.3
-10	5.8	30.1
W	5.1	30.8

N. C. 6 + 9

W	5.9	30.5
+7	5.9	30.0
+10	6.3	29.6
+16	6.8	29.1
+18	9.3	26.6
+21	10.2	25.7

#2
35.93

+25	13.1	22.8
+30	14.5	21.4
	N/4	
-30	14.5	21.4
-25	13.~	22.7
-21	10.2	25.7
-18	9.0	26.9
-16	6.8	29.1
-10	6.3	29.6
-9	5.9	30.0
-2	5.4	30.5
W	12.1	23.8
	N/4+7	
W	10.5	25.4
+4	10.1	25.8
+8	12.1	23.8
+9	6.~	29.7
+10	6.~	29.7
+15	6.7	29.2
+17	12.7	23.2
+20	15.0	20.9
+25	10.3	25.6
	R	
W-25	15.4	20.5
-15	13.8	22.1
-10	11.8	24.1
W	10.0	25.9

#1
35.93

76

	E+7	
X	7.2	28.7
+5	8.~	27.7
+10	8.7	27.2
+12	13.1	22.8
+17	14.1	21.8
+25	13.6	22.3
	S/4	
W-25	13.0	22.9
-23	8.1	27.8
-12	6.0	29.9
-10	5.7	30.2
W	5.2	30.7
	S.06	
X	5.1	30.8
+10	6.2	29.7
	S. line of N actilis = 00	
W	5.3	30.6
+10	6.4	29.5
	Mn Hole for location, see 5671 page 72 this book	
Red oak Rim	4.90	31.5
	0+25 = 2+90	
W+10	5.6	30.3
+20	6.8	29.1
	0+25 = 1+90. old notes	
W	4.5	31.4
+10	5.7	30.2
+20	6.7	29.2

H.I.
35.93

1435 = 1790 old notes

W	4.0	31.9
+10	5.4	30.5
+20	6.5	29.4

1483 = 1492 old notes

W	4.3	31.6
+10	6.0	29.9
+20	6.6	29.3

1494 = 0481 old notes

W	5.3	30.6
+10	6.5	29.4
+20	7.0	28.9

2410 = 0465 old notes

W	7.5	28.4
+10	7.5	28.4
+15	7.3	28.6
+20	8.4	27.5

2430⁵⁰ = 0445⁵⁰ old notes

W	7.9	28.0
+10	7.8	28.1
+13	7.8	28.1
+18	10.4	25.5

2446³⁰ = 0428²⁰ old notes

W	8.2	27.7
+10	8.8	27.1
+20	10.3	25.6

H.I.
35.93

2475 = N. line Bonon

W	7.9	28.0
+10	9.2	26.7
+20	11.2	24.7
+25	14.1	21.8

N. 06 Bonon

W	9.3	26.6	-3.7
+10	9.8	26.1	
+20	11.0	24.9	
+25	12.7	23.2	

N 1/4

W	8.3	27.6
+10	9.5	26.4
+20	12.8	23.1
+25	15.4	20.5

T.P. 2.57 27.59 10.85 25.08

2

W	0.8	26.8
+10	2.6	25.0
+20	9.6	23.0
+24	5.6	22.0
+26	6.9	20.7

S 1/4

W	2.2	25.4
+10	4.2	23.4
+20	5.9	21.7
+25	6.7	20.9

77

42
2759

9.06

W	6.6	21.0
+8	6.0	21.6
+10	6.5	21.1
+20	7.5	20.1
+25	8.4	19.2
+35	9.8	17.8

S Line Bon Air

W	11.2	16.0
+10	12.0	15.6
+20	10.7	16.9
+30	12.1	15.5

10.5

W	17.6	10.0
+10	17.6	10.0
+20	17.6	10.0
+30	16.5	11.1

19.5

W	19.3	8.3
+10	19.0	8.6
+20	19.1	8.5
+30	18.0	9.6

TP	8.42	33.50	2.51	25.08
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+8 ~

28.28

28.89

0.16

observed
comb end
White Bon Air

78

Levels for Sea Wall on Neptune Pt.

7/29/28

3.3v 3x.8v 31.5

Inst. Sta 1731 - P_g H^o = 150°

Grd at 2v 29.8

9.9 24.9 1423

Dist	A ₂	V. A.	Hor. Dist.	ELEV.
20'	126	-37°30'	15.8	-12.2 +17.6
30	120	-31°30'	25.6	-15.7 +14.1
50	138	-38°30'	39.1	-31.1 -7.3
57	143	-33°40'	47.5	-31.6 -1.8
65	120	-28°45'	52.0	-31.2 -1.4
57	112	-34°20'	47.1	-32.2 -2.4
55	146°30'	-27°00'	49.0	-25.0 +4.8
58	149°15'	-17°30'	55.3	-17.4 +12.4
52	166°30'	-9°15'	51.3	-8.4 +21.4
		11.1	23.7	+47v

Levels for Culvert on WL Bon Air

7/29/28

79

4.4 35.9 31.5

W. Mark for
10'
20'

9.0 28.9
13.9 22.0
15. 20.9

40

Dist - 63 - 24

48 30R -20

HOR. DIST.
45.1

ELEV.
+16.4 | 14.5

20

40R

13.8 22.1

From W. proj of curb

Top fill stake

241°

$$\begin{array}{r} 6 \\ \hline 235 \end{array}$$

$$\begin{array}{r} 715 \\ \hline \end{array}$$

227.85

$$\begin{array}{r} 930 \\ \hline \end{array}$$

218.55

$$\begin{array}{r} 645 \\ \hline \end{array}$$

212.10

$$\begin{array}{r} 690 \\ \hline \end{array}$$

205.20

$$\begin{array}{r} 700 \\ \hline \end{array}$$

198.20

$$\begin{array}{r} 61 \\ \hline \end{array}$$

192.10

192.10

1475

$$\begin{array}{r} 25 \\ \hline \end{array}$$

2490

E+46

81.

Levels to establish elevations of Gutters
Alley Block 34 Park VillasB.M. NE Cor
Dwight + Ray
SP

	+	x	-	Elev
	5.65	338.11		332.46
Dwight St on S side				
W Gutter	Street			540
" "	Prop			490
E Gutter	Prop			485
E Gutter	Street			541
T.P.	1.22	331.71	7.62	330.49
Prop E				492
" W				497
Street W				550
Street E				553
B.M. NE Mylersham				480
				326.91

DIRECTIONS FOR USE OF TABLES

18

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1% to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not

IMPROVED TABLES

AND

INFORMATION

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius. Degree of curve with a given L may be found by dividing tangent (or external), opposite L by add correction found in column of corrections. any other degree, divide by degree of curve and To find Tangent and External for curve of

795
13
16.5

ENGINEERING DEPARTMENT,
CITY OF SAN DIEGO,
CALIFORNIA.

23.5
19.5
2.0

4.24

658.775
31
16
27

65
55
20
8
13
26
302
26
42

8 165
2

5.2
1.1
4.1

20.5
10.25
52
10.25
41.75
10.25
31.50
10.25
21.25