

1236

PASTS

FIELD BOOK

No. 385

ENGINEERING DEPARTMENT,
CITY OF SAN DIEGO,
CALIFORNIA.

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No. 380 opp 80 7/15/20 H.H.

No. June 18pp 80 7/15/2014

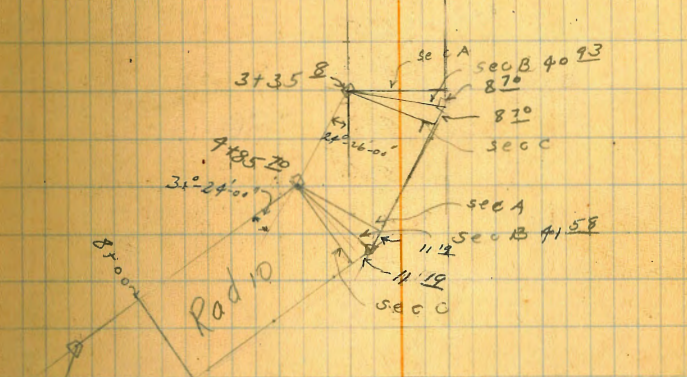
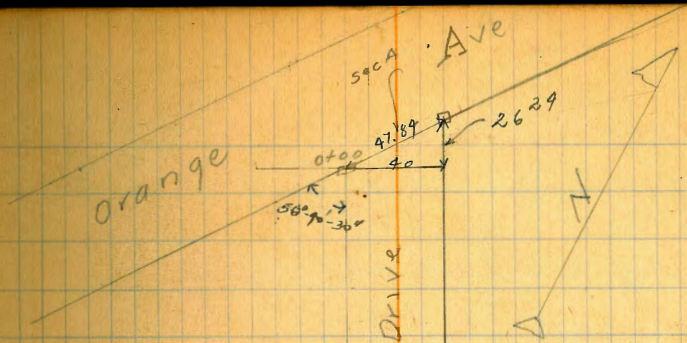
Radio Drive	Orange 800 S.W. 1/4	1
Alley 69, 80, 96, 108, 125	City Hts	12
Evergreen	Lowell to Oliphant	33
Newell	Evergreen to Willow	38
"	" to Resencians	39
Locust	Lowell to Oliphant	42
X sec Alley Blk 69	City Hts	47
X sec. Dwight & 38th		49-56
Mt View 33rd - 35th	Curb Levels	75-79

Bliss & Holbeck
 1025
 1291
 1217
 1298
 1159
 1320
 1203
 1160
 981

Station	Distance	Angle	Reading
1025	363.61		351.36
1291	375.80	0.72	362.89
1217	387.77	0.20	375.60
1298	400.55	0.20	387.57
1159	412.12	0.02	400.53
1320	425.17	0.15	411.97
1203	437.17	0.03	425.14
1160	447.72	1.05	436.12
981	457.32	0.21	447.51

Station	Distance
Sec A	47.89
E	1.2
cb	1.3
T 8	1.3
19	1.6
ϕ	2.2
1/4	2.6
cb	3.1
T 3	3.3
W	2.8
Set BM SW Prop. 6	2.80

Station	Distance
0+00	
W	2.8
T 3	3.4
cb	3.9
1/4	3.7
ϕ	2.8



Sketch of Radio Drive South of Orange St. Highdale Addition Encanto. Showing Distances, Angles & sections taken at angle points

26.28
957.32

1/4	2.5
cb	2.3
E	1.9
30' South	
E	3.2
cb	3.5
1/4	4.2
⊕	4.5
1/4	5.1
+4	5.8
cb	5.6
+3	5.5
W	4.6
60' S.	
W	7.2
cb	7.2
+3	7.2
1/4	6.7
⊕	6.2
+4	6.4
1/4	6.2
cb	5.8
E	5.2
85' S	
E	7.9
cb	7.9

π
457.32

2

1/4	8.0
⊕	7.6
+1	7.2
1/4	7.5
+5	7.9
cb	8.5
+1	8.2
W	8.0
100' S.	
W	7.9
+1	7.8
cb	9.0
+1	8.7
1/4	8.5
+1	8.6
⊕	9.1
1/4	8.9
cb	8.9
E	8.8
125' S.	
E	11.2
cb	11.9
+6	11.9
1/4	11.3
+5	11.5
⊕	10.8

π
457.32

+6 10.5
1/4 10.4
+7 11.1
cb 10.3
+2 9.3
W 9.2

150.5

W 10.5
cb 10.4
+2 12.7
1/4 12.0
E 12.2
+2 13.2
1/4 13.3
cb 13.3
E 12.9

T.P. 0.70 445.78 12.24 445.08
175.5

E-10 2.4
E 3.6
cb 4.0
+3 4.2
1/4 3.8
+5 2.9
E 3.0
+3 2.7

445.78

3

+6 3.0
1/4 3.0
+3 3.1
cb 1.2
W 0.4

181.5

W 0.5
cb 1.1
+3 3.4
1/4 3.5
+5 3.3
E 3.7
+2 3.9
1/4 4.7
cb 4.9
E 5.0
E+10 3.8

200.5

E-10 4.6
E 6.0
cb 6.5
1/4 6.5
+3 6.4
E 4.9
+5 4.4
1/4 4.5

7
445.78

+1 5.1
+3 5.0
cb 2.2
W 2.4

225'S

X1 4.0
+4 4.3
cb 4.4
+3 6.5
1/4 5.7
E 6.0
+2 6.1
1/4 8.2
+5 9.1
cb 9.1
E 8.6
E+15 6.1

250'S

E-15 9.0
E 11.4
cb 11.8
1/4 10.9
E 8.4
+5 7.9
1/4 7.8
+6 7.7

7
445.78

4

cb 7.0
+2 6.2
W 5.8
T.P. 3.35 139.48 9.65 736.13

275'S

W 0.8
+2 1.0
cb 2.4
1/4 2.4
+5 2.5
E 3.3
1/4 5.0
+6 7.1
cb 7.6
+1 8.4
E 8.1
E+15 5.9

300' SOUTH

E-15 9.4
E 10.9
cb 8.7
+6 7.5
1/4 6.9
+6 7.9
E 7.9
+2 7.8

939.98

+5	3.7
1/4	3.5
cb	3.5
+4	3.5
W	2.1
	3/8' 5
W	2.7
+0.5	4.2
cb	4.5
1/4	4.5
+1	4.4
E	6.5
1/4	8.5
cb	10.8
E	13.1
E+3	13.1
E+5	12.1
E+15	8.7

Δ 3+35 E Sec A see sk. 7/1

E-15	9.0
E-5	12.3
E	14.5
+3	14.5
cb	13.6
+5	11.0
1/4	10.6

439.98

400.2

5.2



572
369
11740
870

5

E	8.7
1/4	6.9
+4	5.4
cb	5.8
W	5.8

Sec B

90.93

N	5.8
cb	5.8
+3	5.6
1/4	7.3
E	8.9
1/4	10.9
cb	14.1
+1	14.6
E	14.9
+5	13.9
+15	10.7

Sec C

E-15	11.3
E-11	12.2
E-5	15.5
E	15.7
+1	15.7
cb	13.7
1/4	11.0
E	8.8

939.48

1/4	7.2
+3	5.7
cb	5.9
W	5.8
370' South	
W	6.5
+1	7.3
cb	7.8
+4	8.4
1/4	8.2
+2	8.3
+3	9.2
ϕ	10.2
1/4	11.5
cb	13.4
E	16.0
E+5	19.0
E+12	14.5
E+15	13.0

400' South

E-15	14.8
E-11	16.0
E-15	19.6
E	19.0
cb	16.0
+2	15.2

939.48

6

1/4	13.3
ϕ	11.5
+3	10.3
1/4	10.5
cb	9.6
+3	9.5
+4	7.5
W	7.5

425' S

W	9.3
+2	9.4
+3	11.3
cb	11.5
1/4	12.1
+3	11.7
ϕ	13.3

T.P. 2.35 429.18 12.65 926.83

1/4	9.9
cb	7.1
E	9.5
E-5	10.8
E-10	9.1
E-25	4.9

450' S

E-25	6.4
E-15	8.8

T
4/29/18

E-10	10.9
E-7	13.0
E	10.9
cb	8.4
1/4	6.5
2	9.8
+9	3.1
1/4	3.1
cb	3.0
+2	2.7
W	0.3

4+85.2 Sec A A

W	5.2
cb	4.9
+6	9.6
1/4	5.2
+3	6.6
2	7.3
1/4	8.9
cb	10.2
E	11.4
E+7	15.0
+17	11.6
+25	10.0

500 B

E-35	12.9
------	------

A 41.58
1.5

T
4/29/18

7

E-23	13.9
E-15	15.3
E	11.5
cb	10.7
1/4	9.3
2	7.6
+5	6.7
1/4	5.6
+2	4.7
cb	5.0
W	5.2

Sec C

W	5.2
cb	5.1
+6	9.8
1/4	5.6
+3	6.9
2	7.8
1/4	9.0
cb	10.4
E	11.2
E+13	13.6
E+20	16.2
+25	16.2

500 S.

E-20	17.6
------	------

7
92918

100

E-1	E-20	15.6
E-7	E	11.6
E	cb	10.5
cb	1/4	9.0
1/4	2	7.9
2	+5	5.2
+4	1/4	5.3
1/4	cb	5.6
cb	W	5.9
+2		525 S
W	W	4.8
	+3	5.2
W	+4	6.8
cb	cb	6.9
+6	1/4	7.0
1/4	+5	6.9
+3	2	8.4
2	+1	8.8
1/4	1/4	9.7
cb	cb	11.2
E	+2	12.0
E+1	E	12.3
+1	E+16	16.3
+2	E+22	18.5
	E+27	16.3
E-3		

7
92918

100

E-30	550 South
	16.0
E-20	20.5
E-11	16.8
E	14.2
cb	13.4
1/4	11.2
+6	9.9
2	9.5
+2	8.4
1/4	8.5
cb	8.1
+1	8.1
+3	5.5
W	5.3
	575'
W	6.9
+2	7.1
+3	9.1
cb	9.2
1/4	9.4
+5	9.7
2	11.0
1/4	12.5
cb	14.8
E	15.6
+5	16.8

8

7
429.18

+15	20.7
+25	17.0
600'S.	
E-35	17.5
E-23	21.5
E-15	20.0
E-8	18.0
E	16.~
cb	15.0
1/4	13.~
+6	12.0
♀	11.6
+2	10.6
1/4	10.~
cb	10.4
+2	10.4
+3	7.9
W	7.6
625'S	
W	9.2
+2	9.6
+3	12.1
cb	12.1
1/4	11.8
+5	12.0
TP	1.79

718.82

12.15

417.03

7
418.82

9

♀	3.0
1/4	4.3
cb	6.3
E	7.2
E+17	10.7
+19	11.7
+25	11.6
+36	6.5
650'	
E-35	8.0
-20	11.~
-17	12.3
-11	12.4
-5	10.5
E	9.0
cb	8.0
1/4	6.3
♀	4.7
+4	3.2
1/4	3.0
cb	3.0
+2	2.9
+3	1.0
W	0.8
675'S	
W	2.0

7
418.82

+1	2.0
+2	3.8
cb	9.0
1/4	4.1
+3	4.1
ϕ	5.8
1/4	7.5
cb	9.3
E	10.6
E+5	11.5
+10	13.0
+18	13.2
+30	8.7

700.50

E-30	8.5
E-18	13.3
E-9	13.4
E	11.7
cb	10.6
1/4	8.7
ϕ	6.7
+5	5.1
1/4	5.1
cb	4.8
+4	4.8
W	3.7

7
418.82

10

725.50

W	5.7
cb	5.7
1/4	5.7
+2	5.6
+6	7.3
ϕ	7.7
1/4	8.9
cb	11.2
E	12.6
+5	13.8
+20	14.0
+26	10.7

750.50

E-30	12.9
E-24	14.9
E-12	19.7
E	12.7
cb	11.4
1/4	9.7
ϕ	8.3
+4	7.8
+6	6.8
1/4	6.8
cb	7.0
W	7.0

X
418.8~

77550

W	7.9
cb	7.9
1/4	7.9
ϕ	10.0
1/4	11.3
+4	12.7
cb	13.1
E	13.9
+5	14.2
+10	15.0
+24	15.0
+35	11.3

800' S. out

E-25	11.7			
- 15	15.8			
E	16.0			
cb	19.7			
1/4	13.3			
ϕ	11.1			
+9	10.1			
1/4	8.7			
cb	9.1			
W	9.1			
TP	0.96	907.21	12.57	404.25
TP	0.85	399.79	13.27	393.94
TP	0.25	382.15	12.89	381.90

38215

11

TP	2.95	373.77	10.83	371.32
TP	1.22	361.98	13.01	360.76
check on starting ^{On N.W.} corner Paradise St. Radio Drive on ^{Hub} ³⁵¹ ^{3628M}				
			10.67	351.31
				0.05

Bliss
2038/1
Holbeck
3/17/56
B.M. NW. O.P.
41st + Wightman

X Sections Alleys Blocks 69 80 96 to 8
125 City H/B including levels on curb at curb
line of street B. Between a line of Wightman & the
N. line of Redwood. Central 1/4 1st 20' Alley

Top cb on steel line E side	1.53	338.15
" " " " " W side	0.93	338.75

at 00. S. line of Wightman

N Top cb	0.91	338.77
Gutter	1.7	338.0
+ 2.5	2.2	337.5
⊕	2.0	337.7
Gutter	1.7	338.0
E Top cb	1.60	338.1

05' South

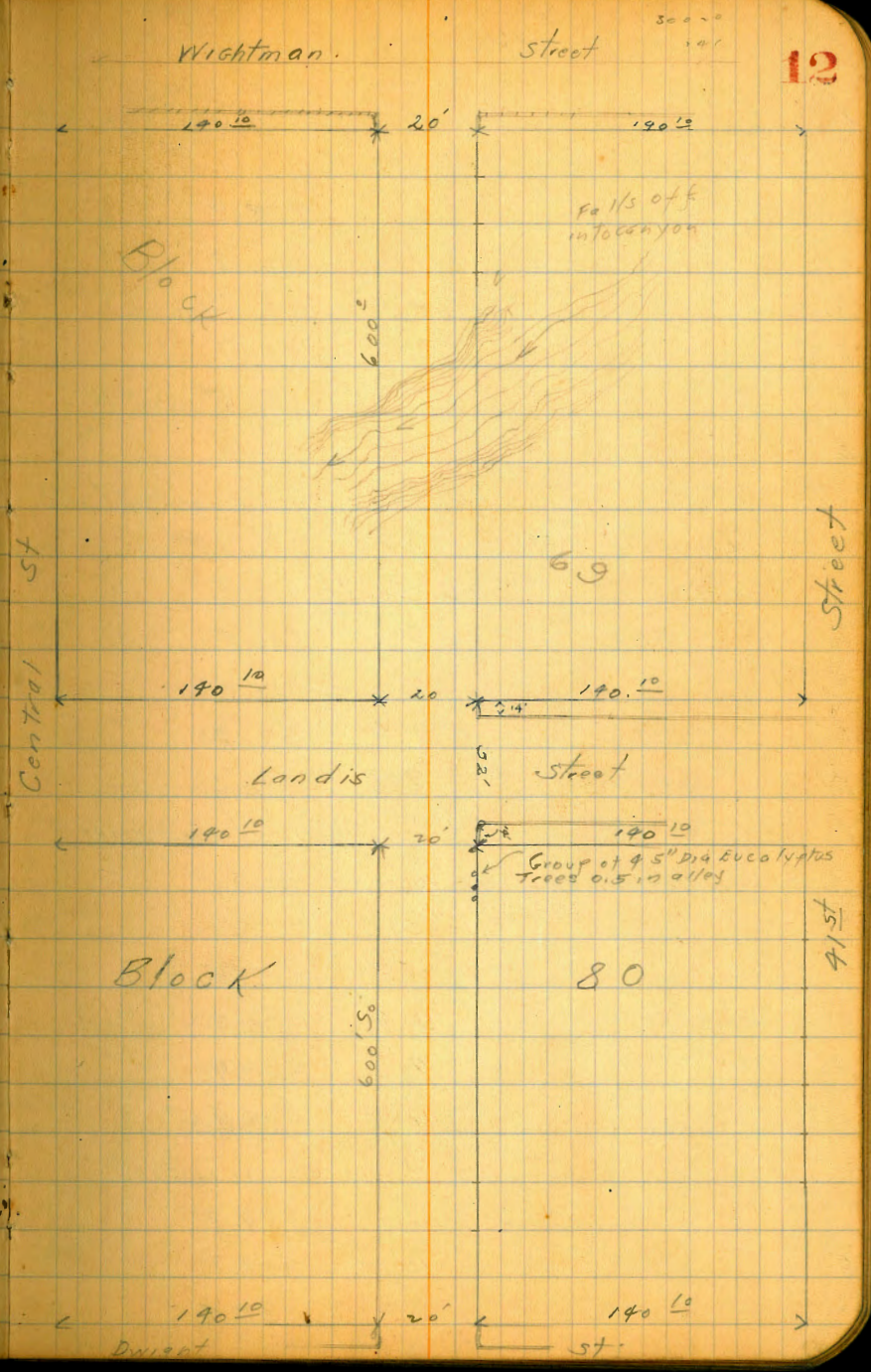
E	3.2	336.5
+ 7	2.7	338.0
⊕	3.4	336.3
+ 8	2.9	336.8
W	1.6	338.1

16' South

N	4.0	335.7
+ 1	5.1	334.6
+ 4	5.6	334.1
⊕	5.7	334.0
E	5.9	333.8

30' S

E	8.1	331.6
⊕	7.5	332.2
+ 8	7.2	332.5



Street

41st

T
33968

	30' South	
N	5.1	334.6
	50' South	
W	6.8	332.9
11	8.0	331.7
⊕	8.4	331.3
+3	8.6	331.1
+6	9.2	330.5
E	9.4	330.3
	72' South Dwelling on East	
0.1 Back floor	8.93	330.75
	75' South	
E	9.2	330.50
⊕	9.2	330.50
+7	8.9	330.80
N	9.1	330.60
	97' South Single Garage on East	
2.6 Back on floor	10.5	329.2
	100'S	
W	8.8	330.90
⊕	9.4	330.30
+6	9.8	329.90
E	10.3	329.40
	105'S Single Garage on East	
2.5 Back on floor	10.5	329.21
E	10.0	329.71
+5	9.2	330.51

T
33968

13

		9.1	330.6
		7.6	330.8
		8.6	331.1
	121.50 S. Sewer Manhole & lot		
	on Rim	8.81	330.87
	132' South Dwelling on East		
	0.7 in alley floor	8.32	331.36
	135'S		
W		8.8	330.9
⊕		9.2	330.5
+6		9.5	330.2
E		10.4	329.3
	155' South		
E		10.9	328.8
+3		10.3	329.4
⊕		9.8	329.9
+9		9.1	330.6
W		9.1	330.6
	164' South Dwelling on East		
	0.4 in alley floor	10.07	329.61
	165' South Single Garage on West		
	2.2 Back on floor	8.8	330.9
	172' South		
W		8.8	330.9
⊕		10.1	329.6
+5		10.7	329.0

339.68

E	10.0	329.3
	182' South	
E	10.7	329.0
+4	11.1	328.6
ϕ	11.4	328.3
+7	10.0	329.7
W	9.0	330.7
	196' South	
W	9.7	330.0
+2	10.7	329.0
+4	11.2	328.5
ϕ	11.7	328.0
+4	12.0	327.7
E	11.5	328.2
	200'S	
E	11.9	327.8
+5	12.2	327.1
ϕ	11.7	328.0
+3	10.9	328.8
+7	11.3	328.4
W	10.6	329.1
	207'S	
W	11.7	328.0
ϕ	11.5	328.2
+8	12.5	327.2
E	13.3	326.4

339.68

14

TP	0.15	327.89	119.4	327.79
	216' South			
E			9.7	323.2
ϕ			3.0	324.9
+5			1.6	326.3
W			1.5	326.4
	225'S			
W			3.0	324.9
ϕ			5.5	322.4
+6			5.9	322.0
E			7.1	320.8
	235' South			
E			10.4	317.5
+5			8.6	319.3
ϕ			8.0	319.9
+6			7.0	320.9
W			5.6	322.3
	250' South			
W			9.7	318.2
+7			12.0	315.9
ϕ			12.3	315.6
+4			12.8	315.1 ^{327.89}
E			15.5	312.4 ^{327.89}
TP	12.05	333.16	6.78	321.11

* Note Because of irregular No X sections were taken between 2150 and 4125

333.16

425' South

E	5.3	321.9
+2	5.9	321.3
ϕ	10.5	322.7
+1	11.1	322.1
+8	11.3	321.9
W	11.8	321.4
W+10	16.8	316.4

445' S

W-5	9.9	323.3
W	8.9	324.3
+7	6.0	327.2
ϕ	5.9	327.3
+1	9.9	328.3
E	0.2	333.0

7.70 338.90 1.90 331.26

63' South

E	5.0	333.9
+5	5.4	333.5
ϕ	8.4	330.5
+5	9.1	329.8
+7	10.0	328.9
+7 Bottom	11.7	327.0
W	12.0	326.9

466' South

W	11.9	327.0
+3	11.8	327.1

338.90

15

73 Top	9.5	329.4
+9	8.6	330.3
+7	8.5	330.4
ϕ	6.7	332.2
+4	5.3	333.6
E	9.8	334.1

476' S Dwelling on West

2. Back floor 10.70 328.2

479' S		
E	9.9	334.5
+4	5.5	333.4
ϕ	6.6	332.3
+7	8.0	330.9
+8	4.8	327.3
W	11.9	327.0

480' S

W	8.9	330.0
+4	7.6	331.3
ϕ	6.8	332.1 ✓
+3	5.3	333.6 ✓
E	4.5	334.4 ✓

482' S

E	9.9	334.5
+8	5.3	333.6
ϕ	6.5	332.4
+4	7.0	331.9

38890

N	6.7	332.2
	500's	
N	6.6	332.3
+3	6.8	332.1
+8	6.2	332.7
⊘	5.1	333.8
E	9.3	334.6
	525's	
E	4.1	334.8
⊘	5.0	333.9
+2	5.3	333.6
N	5.7	333.2
	550's	
N	5.0	333.9
⊘	4.6	334.3
+4	4.2	333.7
E	3.9	335.0
	575's	
E	3.5	335.4
+5	3.6	335.3
+8	4.4	334.5
⊘	4.4	334.5
+8	4.2	334.5
N	4.3	334.6
	585's	
N	4.4	334.5

38890

16

+5	5.1	333.8
⊘	5.2	333.7
+4	4.4	334.5
+5	3.7	335.2
E	3.9	335.5
	597's	
E	2.9	336.0
+3	3.0	335.9
+4	7.1	331.8
+7	7.8	331.1
⊘	8.0	330.9
+5	8.0	330.9
+7	6.8	332.1
N	6.4	332.5
	600's N. Line Lands	
N	7.5	331.4
+2	7.2	331.7
+3	8.4	330.5
⊘	8.6	330.3
+6	8.6	330.3
E Top cb	8.59	330.31
Top cb on street line E side	8.72	330.18

Continued from
Block 69. P. 16

X-Sections Alley Block 80 city Hts.
Between Landis + Dwight 91st + Central

338.90

0100 S Line of Landis

Topch. on East Side on street line 872 330.18

0100 S Line Landis

E Topch 863 330.27

Gutter Plotted 82 330.7

+5 80 330.9

+6 83 330.6

φ 82 330.7

+4 82 330.7

+7 80 330.9

W 80 330.9

02'S

W 5.1 335.8

+1 6.9 332.0

+6 7.7 331.2

φ 7.8 331.9

+4 7.5 331.4

+8 6.5 332.4

E 5.8 333.1

06'S

E 2.9 336.5

+1 2.4 336.5

+3 4.8 334.1

+6 5.7 333.2

+7 6.6 332.3

φ 7.0 331.9

X
338.90

35' South
Total 0.5 in alley 17

7.0 331.9

3.9 335.0

18' South

3.0 335.9

3.1 335.8

4.8 334.1

5.0 333.9

4.5 334.4

2.6 336.3

2.5 336.4

35' South

2.9 336.0

3.2 335.7

3.5 335.4

3.5 335.4

3.4 335.5

3.9 335.5

3.1 335.8

50' South

3.1 335.8

2.9 336.0

3.1 335.8

3.0 335.9

51' South 12" diameter tree
0.6 in alley

338.90

75' South

E	3.1	335.8
+4	2.8	336.1
φ	2.9	336.0
+6	3.0	335.9
W	3.2	335.7

77' South Single Garage ^{on West} Dirt floor

11 Back dt 3.1 335.8

T.P. 410 340.12 2.88 336.02

100' S

W	4.3	335.8
φ	4.2	335.9
+5	3.9	336.2
E	4.2	335.9

107' S. Single Garage on West

3 2 Back concrete lip φ 4.25 335.67

125' S

E	4.2	335.9
+5	4.0	336.1
φ	4.2	335.9
W	4.2	335.9

143' South Single Garage ^{on West}

Lip 3.3 Back φ 3.95 336.17

155' S

W	4.1	336.0
E	4.2	335.9
E	4.3	335.8

340.12

18

160' South Db Garage on West
North end of lip

Lip - 3.2 Back Nord. 4.29 335.83

165' So Single Garage on East

Lip 2.4 Back φ 4.34 335.78

175' South Sand Db Garage on W

3.2 Back Sandlip 4.60 335.5

180' So

E	4.4	335.7
+5	4.7	335.4
φ	4.7	335.4
W	4.8	335.3

187' South Single Garage ^{on East}

0.3 Back Dirt floor dt 4.4 335.7

200' So

W	4.6	335.5
φ	4.7	335.4
+6	4.8	335.3
E	4.7	335.4

205' So

E	4.9	335.2
+6	4.5	335.6
φ	4.6	335.5
W	4.3	335.8

225' So

W	4.9	335.2
---	-----	-------

340.12
225' So

+6	4.9	335.2
♀	5.1	335.0
E	5.1	335.0
242' South Single Garage on East		
E outline	5.2	334.9
♀	4.9	335.2
W	5.2	334.9
270' So		
W	5.3	334.8
♀	5.2	334.9
E	5.0	335.1
300' So.		
E	5.9	334.2
♀	5.9	334.2
W	5.8	334.3
320' South Single Garage on West		
1 ^o Back Dirt/Hor cts	5.7	334.4
323' So. Single Garage on East		
4.2 Back concrete floor cts	5.79	334.33
325' South		
W	6.0	334.1
+5	6.2	333.9
♀	6.1	334.0
E	6.1	334.0
343' So. Single Garage on East		
4.25 Back concrete floor cts	5.73	334.39

340.12

19

343' So. Single Garage on West		
2.7 Back Dirt/Hor	6.2	333.9
350' So		
E	6.3	333.8
+7	6.1	334.0
♀	6.2	333.9
W	6.2	333.9
354' So. Single Garage on East		
4.3 Back concrete floor cts	5.71	334.41
360' So. Man Hole		
on Rim	6.35	333.77
375' So.		
W	6.1	334.0
+3	6.0	334.1
♀	6.5	333.6
E	6.6	333.5
378' So. Single Garage on E		
2.3 Back cts	6.5	333.6
400' So.		
E	6.7	333.4
♀	6.6	333.5
W	6.7	333.4
T.P 3.5 4	337.14	6.52 333.60
404' So. Single Garage on E		
4 Back concrete floor cts	3.28	333.86

337.14

725

So

3.6 333.5

3.7 333.4

3.7 333.4

442' So Single Garage on W

1.2 Back Dirt floor th 3.7 333.4

444' So Single Garage on East

3.9 Back concrete th 3.7 333.71

450' So

3.8 333.3

3.9 333.2

3.7 333.4

475' So

4.3 332.8

4.3 332.8

4.3 332.8

488' So. Dbl. Garage on West

0.4 Back Dirt floor th 4.5 332.6

500' So

4.5 332.6

4.3 332.8

4.5 332.6

509' So Single Garage on W

Lip 0.4 in alley th 4.42 332.62

525' So

4.8 332.3

4.7 332.4

337.14

20

E

4.5

332.6

536' So Single Garage on W

Lip 0.4 in alley th 4.66 332.48

550' So

4.9 332.2

5.1 332.0

5.0 332.1

555' So Single Garage on East

1.4 Back Dirt floor th 5.1 332.0

560' So

5.2 331.9

5.4 331.7

5.0 332.1

4.9 332.2

585' South

5.1 332.0

5.2 331.9

6.0 331.1

6.1 331.0

5.6 331.5

597' So

6.4 330.7

6.7 330.4

6.2 330.3

5.6 331.5

5.5 331.6

337.14

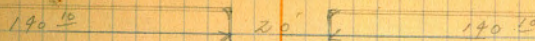
600' South N. Line of DWIGHT

E Topch	6.76	330.38
Gutter	6.8	330.3
K	6.9	330.2
Gutter	6.7	330.4
W Topch	6.64	330.50
Topch on st Line W	6.78	330.36
Topch on st Line East	6.86	330.28
T.P.	6.68	330.46

Dwight

St.

21



Block

96

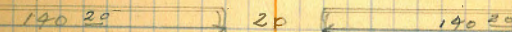
City

Heights



Myrtle

Street



Block

108

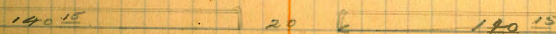
City

Heights



Thorn

St.



X sections Alley Block 96 City Hts
Between Dwight + Myrtle 41st + Central

Took off from
Alley Block 8 + Page 22

	3.59	334.05	330.96
E Topcb. on street line	4.18	329.87	
W " " on street line	4.24	329.81	
	0+00 S. Line		
N Topcb	3.99	330.06	
Gutter	4.0	330.1	
⊘	4.~	329.9	
Gutter	4.1	330.0	
E Topcb	4.11	329.94	
	16 South		
E	3.8	330.3	
⊘	3.9	330.2	
+ 4	4.1	330.0	
W	3.5	330.6	
	37 So		
W	3.4	330.7	
⊘	3.1	331.0	
+ 4	3.1	331.0	
E	3.5	330.6	
	44 South Single Garage on East		
8.1 Back. Dirt floor etc	3.8	330.3	
E	3.7	330.4	
+ 6	3.5	330.6	
⊘	3.3	330.8	
W	3.3	330.8	

Plotted

339.05

22

	55' South	
W	3.7	330.4
+ 3	4.0	330.1
⊘	3.8	330.3
E	3.9	330.2
	58' South Single Garage on West	
4' Back concrete floor etc	3.40	330.7
	70' South	
E	4.0	330.1
+ 5	4.3	329.8
⊘	4.1	330.0
W	4.1	330.0
	80' South	
W	4.3	329.8
+ 6	4.2	329.9
⊘	4.4	329.7
+ 7	4.6	329.5
E	4.5	329.6
	100' South	
E	4.8	329.3
+ 4	4.6	329.5
⊘	4.6	329.5
W	4.5	329.6
	125' So	
W	4.5	329.6
⊘	4.8	329.3
E	4.8	329.3

334.05

150' South

E	5.0	329.1
+7	5.0	329.1
E	5.2	328.9
W	4.8	329.3

161' South Single Garage on West

8.1 Back concrete floor etc 4.35 329.70

177' South

W	5.0	329.1
E	4.9	329.2
E	4.9	329.2

192' South Single Garage on West

8.2 Back concrete floor etc 4.48 329.57

200' South

E	4.7	329.4
E	5.0	329.1
+5	5.2	328.9
W	5.1	329.0

226' South

W	5.6	328.5
+5	5.6	328.5
E	5.6	328.5
E	5.3	328.8

250' South

E	5.7	328.4
+6	5.8	328.3
E	6.2	327.9

334.05

23

W 5.8 328.3

256' So Single Garage on West

6.1 Back Dirt floor 5.8 328.3

263' So.

W	5.9	328.2
E	6.3	327.8
+6	6.1	328.0
E	6.4	327.7

275' So.

E	6.3	327.8
+8	6.3	327.8
E	6.5	328.6
W	6.2	327.9

300' South

W	6.5	327.6
E	6.9	327.2
+5	6.7	327.4
E	7.0	327.1

320' South Single Garage on West

6.9 Back Dirt floor 7.0 327.1

325' South

E	7.3	326.8
E	7.2	326.9
W	7.3	326.8

350' So.

W	7.3	326.8
---	-----	-------

↑
339.05

⊘ 7.3 326.8

⊘ 7.4 326.7

370'So

E 7.5 326.6

⊘ 7.5 326.6

+7 7.8 326.3

W 7.6 326.5

380'So

W 7.8 326.3

⊘ 7.7 326.4

+3 7.8 326.3

E 7.8 326.3

400'South

E 8.0 326.1

+5 7.7 326.4

⊘ 7.8 326.3

W 7.8 326.3

TP 3.15 329.57 7.63 326.42

408'South Single Garage on East

4.4 Back concrete floor etc 3.35 326.72

425'South

W 3.3 326.3

⊘ 3.5 326.1

+5 3.5 326.1

E 3.5 326.1

↑
329.57

443 South

24

3.9 325.7

3.9 325.7

4.0 325.6

449'So Single Garage on West

3.63 325.94

458'South Single Garage on E

3.9 325.7

4.2 325.4

4.1 325.5

71 Back concrete floor etc 3.84 325.73

475'South

4.3 325.3

4.1 325.5

4.3 325.3

500'South

4.5 325.1

4.4 325.2

4.6 325.0

515'South

4.7 324.9

4.6 325.0

4.5 325.1

4.5 325.1

530'South

4.8 324.8

4.9 325.2

E

⊘

W

W

⊘

E

E

⊘

W

W

⊘

E

E

⊘

+5

W

W

+5

329.57

±	4.3	325.3
+5	4.3	325.3
±	4.5	325.1
5 43' So. of Single Europe on East		
±	4.28	325.29
5 50' South		
E	4.9	324.7
+5	4.8	324.8
±	4.9	324.7
+6	5.1	324.5
W	5.4	324.2
5 70' South		
W	5.8	323.8
±	5.8	323.8
E	5.7	323.9
5 92' South		
E	6.1	323.5
±	6.6	323.0
+7	6.5	323.1
W	6.9	323.2
5 99' So		
W	7.2	322.4
+3	7.4	322.2
±	7.5	322.1
+5	7.1	322.5
E	6.9	322.7

329.57

25

E Topch	600.60 South N line of My. It.	8.16	321.41
Eutter		7.8	321.8
+6		7.7	321.9
E		7.8	321.8
+6		7.9	321.7
Gutter		7.9	321.7
N Topch		8.18	321.39
N Topch on street line		8.45	321.12
E Topch on street line		8.37	321.20
T.P.		8.54	321.03
		8.64	

X sections Aiky Block 108 City Heights

Picked up +			
3/22/27	1.59	322.62	321.03
Topcb on W. Street Line	1.88	320.74	
Topcb on E " "	1.78	320.84	

0700 = S. Line of Myrtle

E Topcb	1.79	320.83
Gutter	1.7	320.9
E	1.6	321.0
Gutter	1.6	321.0
W Topcb	1.59	321.0

Plotted

14' South

W	1.7	320.9
+6	1.2	321.4
E	1.2	321.4
E	1.3	321.3

20' South

E	1.3	321.3
+4	1.3	321.3
E	1.6	321.0
+5	1.5	321.1
W	1.7	320.9

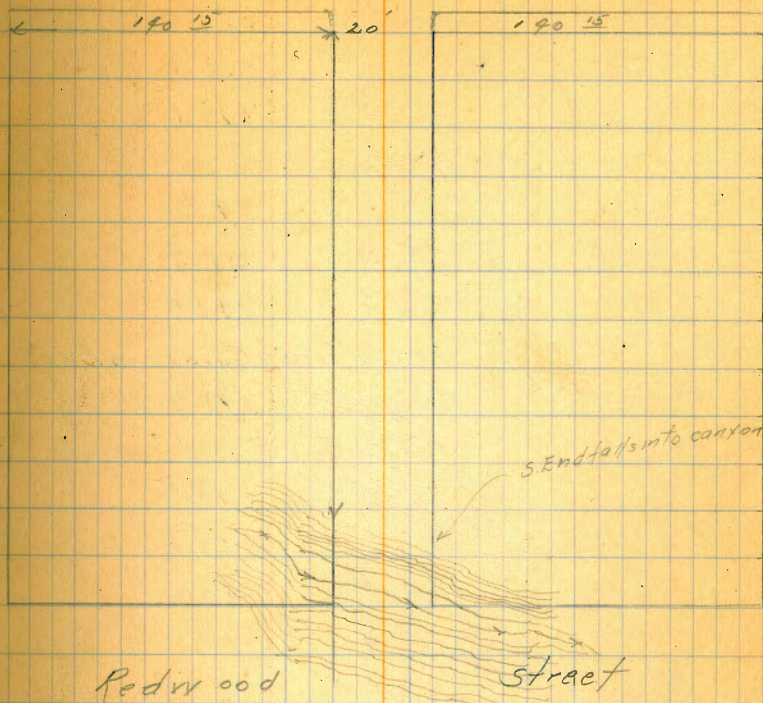
50' S

W	2.5	320.1
+5	2.3	320.3
E	2.5	320.1
E	2.5	320.1

Thorn

St

26



322.62

80' South

E	3.3	319.3	4
4	3.5	319.1	+6
W	3.5	319.1	W

100'S

W	3.8	318.8	W
4	3.7	318.9	4
E	3.8	318.8	E

109'S. Single Garage on East

Lip + 3 Back

ch 3.69 318.9

125' South

E	4.2	318.4	4
+5	4.0	318.6	+9
4	4.0	318.6	W
+9	4.3	318.3	
W	4.4	318.2	W

143' South Single Garage on East

43 Back concrete floor

ch 4.10 318.5

150' South

W	4.7	317.9	E
4	4.4	318.2	
+6	4.6	318.0	E
E	4.5	318.1	4

160' South Single Garage on East

Lip on line

ch 4.75 317.87

175' South

E	5.2	317.4	W
---	-----	-------	---

322.62

27

200' South

W	5.6	317.0	W
4	5.9	317.2	4
E	5.5	317.1	E

225'S

E	5.8	316.8	E
+5	5.8	316.8	+5
4	5.5	317.1	4
+9	5.6	317.0	+9
W	5.6	317.0	W

245' South

W	5.8	316.8	W
+5	5.9	316.7	+5
4	6.0	316.6	4
+5	6.0	316.6	+5
E	6.0	316.6	E

275' South

E	6.2	316.4	E
4	6.5	316.1	4
+6	6.2	316.4	+6
W	6.3	316.3	W

300' South

W	6.6	316.0	W
---	-----	-------	---

322.62

+4	6.6	316.0
⊕	6.9	315.7
E	6.6	316.0

302' South Walk on East

Walk on 312' S. to 6.31 316.31

325' South

E	6.8	315.8
+4	7.1	315.5
⊕	7.1	315.5
W	7.0	315.6

350' South

W	7.2	315.4
+6	7.3	315.3
⊕	7.3	315.3
E	6.9	315.7

380' South

E	7.7	314.9
⊕	7.2	315.4
+5	7.6	315.0
W	7.7	314.9

400' S.

W	8.1	314.5
⊕	7.9	314.7
E	7.9	314.7

425' S.

W	8.9	314.2
---	-----	-------

322.62

28

+5	8.9	314.2
⊕	8.1	314.5
E	8.3	314.3

443' South Single Garage on West

4' Back Concrete floor to 8.55 314.07

447' South

E	8.7	313.9
⊕	8.8	313.8
N	8.8	313.8
T.P.	3.60	317.31
	8.91	313.71

451' S. Single Garage on West

3.7 Back Dirt floor to 3.4 313.9

475' S.

W	9.0	313.3
+5	8.9	313.4
⊕	8.5	313.8
E	8.7	313.6

500' South

E	9.3	313.0
⊕	9.1	313.2
W	9.3	313.0

525' South

W	9.3	313.0
+4	9.6	312.7
⊕	9.5	312.8
+7	9.8	312.5

7
317.31

E	4.7	312.6
	550'S	
E	4.9	312.4
⊕	4.9	312.4
+3	4.9	312.4
+4	4.7	312.6
N	4.7	312.6
	575'South	
N	5.3	312.0
+5	5.0	312.3
⊕	5.4	311.9
+6	5.2	312.1
E	5.1	312.2
	585'South	
E	5.3	312.0
+5	5.6	311.7
⊕	6.1	311.2
+1	5.8	311.5
+4	5.6	311.7
+6	5.3	312.0
N	5.4	311.9
	593'S	
N	5.3	312.0
+3	5.4	311.9
+6	7.0	310.3
⊕	7.4	309.9

317.31

29

+3	7.3	310.0
+6	5.7	311.6
E	5.2	312.1
	597'South	
E	6.1	311.2
+4	6.6	310.7
+6	7.6	309.7
⊕	7.8	309.5
+4	7.7	309.6
+7	5.6	311.7
N	5.6	311.7
	600'S N. Line of Thorn	
N Top cb	9.02	308.3
Gutter	8.1	309.2
+5	8.3	309.0
⊕	8.3	309.0
Gutter	8.1	309.2
E Top cb	8.69	308.6
E Top cb on street	8.90	308.4
N Top cb on street	9.39	307.9
T.P	9.77	307.54

X. Sections Block 125 City Heights
 Between Thorny Redwood Central and 91st
 See sketch Page 26 From S.L. line of Thorny to 525' So.

311.83

30

Picked up pott
 seed post
 T.P. 29

9.29 311.83 307.54

W Topcb on street line 4.36 307.47

E Topcb on street line 3.99 307.84

0+00 = Shire of Thorny

E Topcb 3.81 308.0

Gutter plotted 3.4 308.4

E 3.4 308.4

Gutter 3.4 308.4

W Topcb 4.09 307.7

02' South

W 1.6 310.2

+ 4 1.9 309.9

+ 6 3.1 308.7

E 3.2 308.6

+ 4 3.1 308.7

+ 6 2.3 309.5

E 1.3 310.5

15' South

E 1.8 310.0

+ 3 1.7 310.1

E 2.1 309.7

+ 4 2.1 309.7

T6 1.8 310.0

W 1.9 309.9

36' South

W 2.4 309.4

E 1.8 310.0

+ 6 1.8 310.0

E 1.9 309.9

90' South

E 2.0 309.8

E 2.0 309.8

+ 6 2.5 309.3

W 2.7 309.1

55' South

W 2.9 308.9

E 2.8 309.0

E 2.5 309.3

70' S.

E 2.9 308.9

+ 5 3.3 308.5

E 3.3 308.5

W 3.3 308.5

85' South

W 3.7 308.1

E 3.7 308.1

E 3.4 308.4

91' South Single Garage on East

Lip 0.6 Back ch 3.95 307.88

100' South

E 3.8 308.0

E 3.8 308.0

317-83

+6	4.0	307.8	+2
W	4.0	307.8	W
W	4.5	307.3	
±	4.5	307.3	W
+6	4.2	307.6	+4
E	4.2	307.6	±
7.6 Back Dirt floor etc	3.9	307.9	E
	133' South	Single Garage on East	
41 Back Dirt floor etc	9.9	306.9	
	144' South		
±	4.4	307.4	E
+8	4.7	307.1	±
±	5.0	306.8	+3
+3	5.0	306.8	W
+5	5.3	306.5	
N	5.3	306.5	N
	159' South	Single Garage on East	±
W	5.6	306.2	E
±	5.6	306.2	
+6	5.3	306.5	E
E	4.7	307.1	+6
7.4 Back Dirt floor etc	4.7	307.1	±
	175' South		W
E	5.6	306.2	
+6	5.7	306.1	W
±	5.8	306.0	+7

311-83

31

6.0	305.8
6.1	305.7
200' South	
6.9	304.9
6.6	305.2
6.6	305.2
6.3	305.5
206' South	Single Garage on West
2.7 Back Dirt floor etc	7.0
225' S	
7.4	304.4
7.4	304.4
7.6	304.2
7.6	304.2
256' South	
8.3	303.5
8.4	303.6
8.1	303.7
275' South	
8.7	303.1
8.8	303.0
9.0	302.8
9.2	302.8
300' South	
10.5	301.3
10.1	301.7

311.83

	101	301.7	
E	9.8	302.0	
	306' South Single Garage on East		
	0.5 Back Driftline etc	9.9	301.9
	325'S		
E	10.4	301.4	
E	10.9	300.9	
W	11.2	300.6	
	350' South		
W	11.8	300.00	
E	11.6	300.2	
+E	11.3	300.5	
	370'S		
E	11.9	299.9	
+4	12.2	299.6	
W	12.5	299.3	
W	12.6	299.2	
W	T.P	1.20	300.95
		12.08	299.75
	400'		
W	3.2	297.8	
E	+4	3.2	297.8
E	3.1	297.9	
H	2.9	298.1	
EE	2.3	298.7	
	4.25 South		
E	3.5	297.5	

300.95

32

E	7.1	296.9
W	4.3	296.7
	450' South	
W	5.9	295.1
E	5.9	295.1
+5	5.4	295.6
E	4.9	296.1
	461' South Sewer Man Hole	
	on Rim	6.40
		294.6
	465' South	
E	6.2	294.8
+5	6.5	294.5
E	6.7	294.3
W	7.1	293.9
	475' South	
W	8.7	292.3
E	8.0	293.0
+4	7.4	293.6
E	6.6	294.4
	490' South	
E	8.3	292.7
+4	9.6	291.4
E	10.7	290.3
W	12.1	288.9
	500' South	
W	13.7	287.3

T
300.95

+ 9		12.7	288.3
±		12.6	288.4
+ 2		12.1	288.9
+ 6		11.8	289.2
E		11.9	289.6
	525 South		
E		16.3	284.7
+ 7		17.3	283.7
±		18.8	282.2
+ 3		18.9	282.1
W		20.8	280.2
T.P.	12.91	312.87	0.49 300.96
T.P.	7.89	315.93	4.83 308.09
T.P.	8.81	324.53	0.21 315.72
check on BM NW Myrtle 41 ±		3.06	321.47
			321.52 09 mo

J

McHugh

33

X SEC¹ Evergreen Lowell To Oliphant

70' wide 15' cbs 10' gts

0+00 = E.N. Lowell

B.M. Willow & Lowell S.W. B.P.	52.26	✓
T.P. 158	5384'	
T.P. 007	4084'	1307 40.77'
T.P. 302	3233'	11.53 2931'
0+00		
WL	2.6	29.73
cb	3.8	28.53
±	4.2	28.1
±	5.0	27.3
±	5.2	27.1
cb	5.4	26.9
+ 3	5.4	26.9
+ 5	4.8	27.5
EL	5.2	27.1
0+50		
EL	5.9	26.4
cb	5.4	26.9
±	5.5	26.8
±	5.2	27.1
±	5.2	27.1
cb	4.7	27.6
WL	4.2	28.1

Plotted
A 14/28
A

0+98 = ± 2' walk on west

32.33

WL	4.62	27.71
cb	5.04	27.29
+2.5 = End of Walk	5.27	27.06
$\frac{1}{4}$	5.3	27.0
$\frac{1}{4}$	5.3	27.0
$\frac{1}{4}$	5.9	26.4
cb	5.8	26.5
EL	6.2	26.1
1+50		
EL	5.5	26.8
cb	5.4	26.9
$\frac{1}{4}$	5.4	26.9
$\frac{1}{4}$	5.0	27.3
$\frac{1}{4}$	5.0	27.3
cb	4.8	27.5
NL	4.7	27.6
2+00 S.L. Mac Couley		
JWL	3.6	28.7
cb	3.9	28.4
$\frac{1}{4}$	3.9	28.4
$\frac{1}{4}$	3.7	28.6
$\frac{1}{4}$	4.2	28.1
cb	4.7	27.6
EL	5.1	27.2
CURB		
EL	4.8	27.5

32.33

34

cb	4.7	27.6
$\frac{1}{4}$	3.7	28.6
$\frac{1}{4}$	3.2	29.1
$\frac{1}{4}$	3.3	29.0
cb	3.4	28.8
WL	3.4	28.9
Quarter		
NL	1.9	30.4
cb	2.2	30.1
$\frac{1}{4}$	2.5	29.8
$\frac{1}{4}$	2.8	29.5
$\frac{1}{4}$	3.1	29.2
cb	3.4	28.9
EL	3.7	28.6
Center		
EL	3.9	28.4
cb	3.5	28.8
$\frac{1}{4}$	3.0	29.3
+8	2.7	29.6
+9	4.5	27.8
$\frac{1}{4}$	4.7	27.6
+4	4.4	27.9
+5	2.7	29.6
cb	2.5	29.8
NL	1.6	30.7
Quarter		

32.33

W.L.	2.6	29.7
cb	4.3	28.0
$\frac{1}{4}$	4.9	27.4
+5	2.8	29.5
$\frac{1}{4}$	3.1	29.2
$\frac{1}{4}$	3.3	29.0
cb	3.5	28.8
EL	4.1	28.2
Curb = S End of 12' Bridge across ditch		
EL	12.5	19.8
cb	12.0	20.3
$\frac{1}{4}$	11.3	21.0
$\frac{1}{4}$	10.8	21.5
$\frac{1}{4}$	10.3	22.0
cb	10.5	21.8
W.L.	10.2	22.1
Curb + 12		
W.L.	9.5	22.8
cb	10.1	22.2
$\frac{1}{4}$	10.7	21.6
$\frac{1}{4}$	11.0	21.3
$\frac{1}{4}$	11.7	20.6
cb	10.8	21.5
EL	12.0	20.3
0+00 = N.L. MacCauley = N End Bridge		
EL	5.0	27.3

32.33

35

cb	4.0	28.3
$\frac{1}{4}$	3.7	28.6
$\frac{1}{4}$	3.3	29.0
$\frac{1}{4}$	3.1	29.2
+1	2.5	29.8
cb	2.7	29.6
W.L.	2.2	30.1
T.P.	11.96	42.39
0+50	1.90	30.43
W.L.	10.1	32.3
cb	11.3	31.1
$\frac{1}{4}$	11.4	31.0
$\frac{1}{4}$	11.6	30.8
$\frac{1}{4}$	12.2	30.2
cb	12.2	30.2
EL	12.9	29.5
1+00 = $\frac{1}{4}$ garage on West (Wood floor)		
EL	11.8	30.6
cb	11.1	31.3
$\frac{1}{4}$	10.7	31.7
$\frac{1}{4}$	10.1	32.3
$\frac{1}{4}$	9.5	32.9
cb	8.6	33.8
W.L.	8.3	34.1
1+50		
W.L.	4.3	38.1
cb	5.5	36.9

42.39

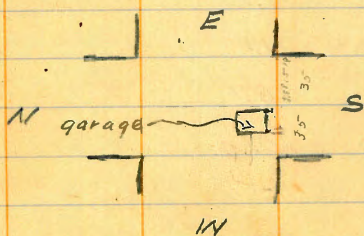
$\frac{1}{4}$	6.6	35.8
E	7.6	34.8
$\frac{1}{4}$	8.2	34.2
cb	8.9	33.5
EL	10.1	32.3

2+00 = S.L. Newell St.

EL	8.2	34.2	334
cb	6.4	36.0	352
$\frac{1}{4}$	5.1	37.3	365
E	3.9	38.5	377
$\frac{1}{4}$	3.2	39.2	384
cb	1.3	41.1	402

T.P	12.46	53.61	1.24	41.15
W.L.		10.0	43.6	42.8

S.L. Newell + 1.5' = S. End of 12' x 18' garage

S.E. corner = $\frac{1}{4} + 1$ S.W. corner = $\frac{1}{4} + 3$ 

Curb

W.L.	8.0	45.6	448
cb	10.8	42.8	420
+ 7 = W side of garage	12.6	41.0	402

53.6

36

$\frac{1}{4}$ (in garage)			
+ 9 = E side of garage	14.0	39.6	388
E	14.0	39.6	388
$\frac{1}{4}$	15.1	38.5	377
cb	16.6	37.0	362
EL	18.7	34.9	341

Quarter

EL	17.9	35.7	349
cb	15.4	38.2	374
$\frac{1}{4}$	14.3	39.3	385
E	13.0	40.6	398
$\frac{1}{4}$	11.3	42.3	415
cb	9.7	43.9	431
W.L.	5.7	47.9	471

Center

W.L.	3.9	49.7	489
cb	6.8	46.8	460
$\frac{1}{4}$	9.0	44.6	438
E	10.7	42.9	421
$\frac{1}{4}$	12.3	41.3	405
cb	14.2	39.4	386
EL	16.5	37.1	363

Quarter

EL	17.5	36.1	353
cb	14.3	39.3	385
$\frac{1}{4}$	12.4	41.2	404

53.6

£		10.7	42.9	42.1	
$\frac{1}{4}$		8.6	45.0	44.2	
cb		6.1	47.5	46.7	
WL		2.4	51.2	50.4	
Curb					
WL		0.3	53.3	52.5	
cb		3.8	49.8	49.0	
$\frac{1}{4}$		6.8	46.8	46.0	
£		8.3	45.3	44.5	
$\frac{1}{4}$		10.4	43.2	42.4	
cb		12.4	41.2	40.4	
EL		16.2	37.4	36.6	
0+00	N.L. Newell				
EL		14.4	39.2	38.4	
cb		11.1	42.5	41.7	
$\frac{1}{4}$		8.4	45.2	44.4	
£		6.3	47.3	46.5	
$\frac{1}{4}$		4.0	49.6	48.8	
cb		1.3	52.3	51.5	
T.P.	12.37	65.98	0.00	53.61	
WL			8.2	57.8	57.0
0+50					
WL			1.8	64.2	
+10			1.5	64.5	
cb			4.2	61.8	
$\frac{1}{4}$			6.7	59.3	

65.98
66.00

37

£		9.2	56.8	
$\frac{1}{4}$		12.2	53.8	
cb		15.0	51.0	
EL		19.8	46.2	
1+00				
EL		12.6	53.4	
cb		7.9	58.1	
$\frac{1}{4}$		4.9	61.1	
£		1.9	64.1	
T.P.	12.67	78.61	0.04	65.94
$\frac{1}{4}$			11.3	67.3
cb			8.3	70.3
+5			5.7	72.9
WL			6.1	72.5
1+50				
T.P.	12.72	91.09	0.24	78.31
WL		91.1	10.7	80.4
+10			10.7	80.4
cb			13.1	78.0
+2			14.7	76.4
$\frac{1}{4}$			17.0	74.1
£			19.9	71.2
$\frac{1}{4}$			22.5	68.6
cb			25.7	65.4
EL			31.1	60.0
2+00 = S.L. Oliphant				

91.1

EL	24.2	64.9
cb	19.7	71.4
$\frac{1}{4}$	16.9	74.2
E	13.6	77.5
$\frac{1}{4}$	8.8	82.3
cb	4.6	86.5
WL	3.7	87.4

X-sec Newell Evergreen to Willow

T.P. 1242 66.03 53.61

0+00 = WL Evergreen

0+00 = NL Evergreen

N.L.	8.0	58.0
cb	12.6	53.4
$\frac{1}{4}$	15.2	50.8
E	16.0	50.0
+5	15.6	50.4
$\frac{1}{4}$	17.1	48.9
cb	19.5	46.5
SL	22.2	43.8
0+25		
S.L.	17.2	48.8
cb	14.2	51.8
$\frac{1}{4}$	10.4	55.6
E	10.6	55.4
+5	10.6	55.4
$\frac{1}{4}$	8.3	57.7

66.03

38

cb	3.5	62.5
NL	2.7	63.3
T.P. 1292 7824	0.71	65.32
0+75		
NL	3.2	75.0
+3	3.6	74.6
+5	8.2	70.0
cb	8.9	69.3
$\frac{1}{4}$	9.4	68.8
E	11.4	66.8
$\frac{1}{4}$	11.6	66.6
cb	15.4	61.8
SL	19.9	58.3
1+25		
SL	12.2	66.0
cb	8.2	70.0
$\frac{1}{4}$	5.4	72.8
E	5.1	73.1
$\frac{1}{4}$	4.9	73.3
cb	3.9	74.3
+10	2.7	80.9
WL	3.0	81.2
1+75		
WL	7.0	85.2
+5	5.0	83.8
cb	1.5	76.7

78.24

1/4		2.1	76.1
1/2		2.6	75.6
3/4		2.9	75.3
+3		2.9	75.3
cb		6.8	71.4
SL		12.5	65.7

2+25

SL		16.3	61.9
cb		9.6	68.6
1/4		4.2	74.0
1/2		2.2	76.0
3/4		1.9	76.3
cb		1.5	76.7
+8		0.5	77.7
+12	3.8		82.0
NL	5.8		84.0

2+75

NL		0.2	77.4
cb		2.4	75.8
1/4		7.8	70.4
1/2		11.8	66.4
3/4		15.2	63.0
cb		18.5	59.7
SL		23.6	54.6

3+00 = FL WILLOW

SL		26.4	51.8
----	--	------	------

cb	21.1	57.1
1/4	17.8	60.4
1/2	13.5	64.7
3/4	10.5	67.7
cb	8.6	69.4
NL	4.4	73.8

X Sec NEWELL Evergreen To Rosecans.

T.P. 0.76 41.91 41.15 { T.P. NEWELL
+ Evergreen

0+00 = EL EVERGREEN

SL	7.7	34.2	33.1	176
cb	7.0	34.9	34.1	
1/4	6.2	35.7	34.9	
1/2	4.9	37.0	36.2	
3/4	5.7	36.2	35.4	
cb	4.2	37.7	36.9	
NL	2.6	39.3	38.5	
0+50				
NL	9.8	32.1	31.3	
cb	10.2	31.1	30.3	
1/4	11.4	30.5	29.7	
1/2	11.3	30.6	29.8	
3/4	11.7	30.2	29.4	
cb	12.0	29.9	29.1	
SL	12.0	29.9	29.1	
T.P.	0.05	29.08	12.88	29.03
1+00				

Plotted
4/14/28
T.P.Hardage
figured
Evergreen to
Rosecans
T.G.H.
6/2/28

Elevations

See page 46

59.1

SL	1.6	27.5	26.7
cb	2.1	27.0	26.2
$\frac{1}{4}$	2.3	26.8	26.0
$\frac{1}{2}$	1.7	27.4	26.6
$\frac{1}{4}$	1.5	27.6	26.8
cb	1.2	27.9	27.1
NL	1.4	27.7	26.9
1+50			
NL	4.5	24.6	23.8
cb	4.7	24.4	23.6
$\frac{1}{4}$	4.8	24.3	23.5
$\frac{1}{2}$	4.5	24.4	23.8
$\frac{1}{4}$	4.2	24.9	24.1
cb	4.0	25.1	24.3
SL	3.9	25.2	24.4
2+00			
SL	6.0	23.1	22.3
cb	5.8	23.3	22.5
$\frac{1}{4}$	5.7	23.4	22.6
$\frac{1}{2}$	6.4	22.7	21.9
$\frac{1}{4}$	6.3	22.8	22.0
cb	6.4	22.7	21.9
NL	6.4	22.7	21.9
2+50			
NL	8.4	20.7	19.9
cb	8.4	20.7	19.9

10

$\frac{1}{4}$	8.2	20.9	20.1
$\frac{1}{2}$	8.3	20.8	20.0
$\frac{1}{4}$	8.4	20.7	19.9
cb	8.6	20.5	19.7
SL	8.4	20.7	19.9
B+00 = WL Locast			
SL	11.0	18.1	17.5
cb	10.7	18.4	17.6
$\frac{1}{4}$	10.8	18.3	17.5
$\frac{1}{2}$	10.8	18.3	17.5
$\frac{1}{4}$	11.0	18.1	17.3
cb	11.1	18.0	17.2
NL	11.2	17.9	17.1
0+00 = EL Locast			
T.P.	0.93	12.37	12.04
16.44			
NL	2.0	15.4	14.6
cb	2.1	15.3	14.5
$\frac{1}{4}$	2.1	15.3	14.5
$\frac{1}{2}$	2.1	15.0	14.2
$\frac{1}{4}$	2.1	15.0	14.2
cb	2.2	15.2	14.4
SL	2.0	15.4	14.6
0+50			
SL	3.9	13.5	12.7
cb	3.7	13.7	12.9
$\frac{1}{4}$	4.0	13.4	12.6

17.4

£	4.1	13.3	125
$\frac{1}{4}$	3.7	13.7	129
cb	3.5	13.9	131
NL	3.7	13.7	129
1+05	= £ Ribbon drive on North		
NL	on concrete	4.45	12.92
+2	on End of Ribbon	4.64	12.73
cb	5.1	12.3	115
$\frac{1}{4}$	5.2	12.2	114
£	5.3	12.1	113
$\frac{1}{4}$	5.6	11.8	110
cb	5.1	12.3	115
SL	5.1	12.3	115
1+50			
SL	6.0	11.4	106
cb	6.3	11.1	103
$\frac{1}{4}$	6.5	10.9	101
£	6.1	11.3	105
$\frac{1}{4}$	6.2	11.2	104
cb	6.0	11.4	106
NL	5.8	11.6	108
2+00			
NL	7.1	10.5	95
cb	6.9	10.5	97
$\frac{1}{4}$	7.0	10.4	96
£	6.9	10.5	97

17.4

11

$\frac{1}{4}$	7.0	10.4	96
cb	7.1	10.3	95
SL	6.8	10.6	98
2+50			
SL	7.0	10.4	96
cb	7.2	10.2	94
$\frac{1}{4}$	7.4	10.0	92
£	7.4	10.0	92
$\frac{1}{4}$	7.4	10.0	92
cb	7.4	10.0	92
NL	7.4	10.0	92
3+00 = NL ROSECRAMS			
NL	7.9	9.5	87
cb	7.9	9.5	87
$\frac{1}{4}$	7.6	9.8	90
£	7.4	10.0	92
$\frac{1}{4}$	7.2	10.2	94
cb	7.5	9.9	91
SL	6.8	10.6	98
NL ROSECRAMS + 23.35 = Edge paving			
SL	8.45	8.92	
cb	8.62	8.75	
$\frac{1}{4}$	8.79	8.58	
£	8.90	8.47	
$\frac{1}{4}$	9.02	8.35	
cb	9.20	8.17	
NL	9.40	7.97	

T.P. 715 23.59 16.44 { T.P. NEWELL
+ Locast

X Sec Locast Lowell to Oliphant

0+00 = NL Lowell

2+00 = SL Oliphant

WL	7.4	16.2
cb	7.6	16.0
$\frac{1}{4}$	8.2	15.4
$\frac{1}{4}$	8.6	15.0
$\frac{1}{4}$	8.5	15.1
cb	8.7	14.9
EL	9.0	14.6
1+50		
EL	8.6	15.0
cb	8.4	15.2
$\frac{1}{4}$	7.9	15.7
$\frac{1}{4}$	7.6	16.0
$\frac{1}{4}$	7.4	16.2
cb	6.9	16.7
WL	6.7	16.9
1+00		
WL	6.2	17.4
cb	6.3	17.3
$\frac{1}{4}$	6.7	16.9
$\frac{1}{4}$	6.9	16.7
$\frac{1}{4}$	7.2	16.4
cb	7.5	16.1

Plotted
2.14
1.11

EL	7.9	15.7
0+50		
EL	7.3	16.3
cb	7.0	16.6
$\frac{1}{4}$	6.7	16.9
$\frac{1}{4}$	6.2	17.4
$\frac{1}{4}$	6.1	17.5
cb	5.9	17.7
WL	5.7	17.9
0+00 = NL Newell		
WL	5.6	18.0
cb	5.9	17.7
$\frac{1}{4}$	6.3	17.3
$\frac{1}{4}$	6.5	17.1
$\frac{1}{4}$	6.6	17.0
cb	7.1	16.5
EL	8.1	15.5
Curb		
EL	8.3	15.3
cb	7.7	15.9
$\frac{1}{4}$	7.3	16.3
$\frac{1}{4}$	7.0	16.6
$\frac{1}{4}$	6.6	17.0
cb	6.2	17.4
WL	5.6	19.0
Quarter		

23.6

WL	5.4	18.2
cb	6.3	17.3
$\frac{1}{4}$	6.7	16.9
£	7.3	16.3
$\frac{1}{4}$	7.7	15.9
cb	7.9	15.7
EL	8.5	15.1
Center		
EL	8.5	15.1
cb	8.0	15.6
$\frac{1}{4}$	7.6	16.0
£	7.2	16.4
$\frac{1}{4}$	6.7	16.9
cb	6.4	17.2
WL	5.3	18.3
Quarter		
WL	5.3	18.3
cb	6.1	17.5
$\frac{1}{4}$	6.7	16.9
£	7.1	16.5
$\frac{1}{4}$	7.4	16.2
cb	7.8	15.8
EL	8.5	15.1
Curb		
EL	8.3	15.3
cb	7.7	15.9

23.6

43

$\frac{1}{4}$	7.1	16.2
£	6.9	16.7
$\frac{1}{4}$	6.6	17.0
cb	6.3	17.3
WL	5.3	18.3
2+00 ²⁰ = SL Newell		
WL	5.4	18.2
cb	6.2	17.4
$\frac{1}{4}$	6.5	17.1
£	6.7	16.9
$\frac{1}{4}$	7.2	16.4
cb	7.7	15.9
EL	8.2	15.4
1+50		
EL	7.9	15.7
cb	7.3	16.3
$\frac{1}{4}$	7.0	16.6
£	6.7	16.9
$\frac{1}{4}$	6.4	17.2
cb	6.1	17.5
WL	5.1	18.5
1+00		
WL	4.2	19.4
cb	5.0	18.6
$\frac{1}{4}$	5.9	17.7
£	6.0	17.6

23.6

+	6.2	17.4
cb	6.4	17.2
EL	6.8	16.8
0+50		
EL	5.4	18.2
cb	5.1	18.5
$\frac{1}{4}$	4.9	18.7
$\frac{1}{4}$	4.9	18.7
$\frac{1}{4}$	4.8	18.8
cb	4.5	19.1
WL	3.8	19.8
0+072		
WL	2.9	20.7
cb	3.3	20.3
$\frac{1}{4}$	3.4	20.2
$\frac{1}{4}$	3.8	19.8
$\frac{1}{4}$	4.1	19.5
cb	4.3	19.3
EL	4.8	18.8
0+00 = NL MacCauley		
EL	4.7	18.9
cb	4.3	19.3
+5	4.2	19.4
$\frac{1}{4}$	7.5	16.1
$\frac{1}{4}$	8.1	15.5
+7	8.3	15.3

23.6

11

+	10.5	13.1
cb	10.6	13.0
WL	9.7	13.9
+10		
WL	9.8	13.8
cb	9.6	14.0
$\frac{1}{4}$	9.7	13.9
$\frac{1}{4}$	10.8	12.8
$\frac{1}{4}$	10.9	12.7
cb	10.4	13.2
EL	10.1	13.5
Curb		
EL	11.3	12.3
cb	11.0	12.6
$\frac{1}{4}$	10.5	13.1
$\frac{1}{4}$	9.8	13.8
$\frac{1}{4}$	9.5	14.1
+6	9.3	14.3
+7	6.6	17.0
cb	6.3	17.3
WL	5.0	18.6
Quarter		
WL	2.8	20.8
cb	3.4	20.2
$\frac{1}{4}$	4.0	19.6
$\frac{1}{4}$	4.4	19.2

23.6

$\frac{1}{4}$	4.7	18.9
cb	5.1	18.5
EL	5.0	18.0
Center		
EL	6.0	17.6
cb	5.8	17.8
$\frac{1}{4}$	5.4	18.2
$\frac{1}{4}$	5.1	18.5
$\frac{1}{4}$	4.8	18.8
cb	4.5	19.1
WL	4.1	19.5
Quarter		
WL	4.3	19.3
cb	5.0	18.6
$\frac{1}{4}$	5.3	18.3
$\frac{1}{4}$	5.5	18.1
$\frac{1}{4}$	5.7	17.9
cb	6.0	17.6
EL	6.4	17.2
Carb		
EL	6.4	17.2
cb	6.0	17.6
$\frac{1}{4}$	5.5	18.1
$\frac{1}{4}$	5.3	18.3
$\frac{1}{4}$	5.0	18.6
cb	4.5	19.1

23.6

45

WL	3.2	20.4
2400 = SL MacCawley		
WL	3.3	20.3
+5	3.2	20.4
cb	4.8	18.8
$\frac{1}{4}$	4.9	18.7
$\frac{1}{4}$	5.1	18.5
$\frac{1}{4}$	5.4	18.2
cb	6.0	17.6
EL	6.4	17.2
1+83		
EL	6.4	17.2
cb	5.8	17.8
$\frac{1}{4}$	5.3	18.3
$\frac{1}{4}$	5.3	18.3
$\frac{1}{4}$	5.1	18.5
cb	4.8	18.8
WL	3.3	20.3
1+66		
WL	3.7	19.9
cb	4.5	19.1
$\frac{1}{4}$	5.7	17.9
$\frac{1}{4}$	7.5	16.1
$\frac{1}{4}$	8.6	15.0
cb	9.0	14.6
EL	8.2	15.4

20.97
21.00

23.6

1746			
EL	5.0	18.6	
cb	4.8	18.8	
$\frac{1}{4}$	4.5	19.1	
$\frac{1}{4}$	4.5	19.1	
$\frac{1}{4}$	5.3	18.3	
+3	5.5	18.1	
cb	7.3	16.3	
WL	7.9	15.7	

1740			
WL	5.0	18.6	
cb	4.7	18.9	
$\frac{1}{4}$	4.5	19.1	
$\frac{1}{4}$	4.3	19.3	
$\frac{1}{4}$	4.3	19.3	
cb	4.8	18.8	
EL	4.9	18.7	
T.P.	2.18	21.00 20.97	4.80 18.79

0+50			
EL	2.8	18.2	
cb	2.5	18.5	
$\frac{1}{4}$	2.6	18.4	
$\frac{1}{4}$	2.4	18.6	
$\frac{1}{4}$	1.8	19.2	
cb	2.0	19.0	
WL	1.4	19.6	

0+00 = N2 Lowell

WL	2.3	18.7
cb	2.4	18.6
$\frac{1}{4}$	3.3	17.7
$\frac{1}{4}$	3.3	17.7
$\frac{1}{4}$	3.5	17.5
cb	3.5	17.5
EL	3.8	17.2
T.P.	12.41	

8.56
 B.M. Rosecrans + Lowell B.P. 8.06
 1 1 1
 No bueno por nada \rightarrow 1.50

T.P. 12.00	32.69	10.28	20.69
T.P. 12.63	45.24	0.08	32.61
T.P. 11.38	56.25	0.37	44.87
T.P.		4.07	52.18

B.M. S.W.B.P. Willow + Lowell 52.26
 { check between bench used + B.M. should have used .08
 B.M. used 5.24
 True elevation 49.8
 0.76 = error in all elevations

Bliss
Isbell
Derwit
1750' S
EM NW 8.0 st
Wrightman 2 41

X Section s of Alley Block 69
City H's. from a point 250' S of The Stone of Wightman
to a point 175' N of the N. line of Landis
Eley 20' Alley

X
315.65

47

	479	340.28		335.49	⊥		
TP	0.30	328.03	12.55	327.73	E		
TP	0.70	315.65	13.08	314.95	E+10		
			250' S. from original X Sec. of alley				
			262' S.				
E-10			6.9	308.8	E-10		
E			4.5	311.2	E		
⊥			2.7	313.0	⊥		
W			0.6	315.1	⊥		
			280' S.				
W-5			3.5	312.2	W+10		
W			5.7	310.0			
W-8.2	⊥	⊥	6.32	309.3			
⊥			7.3	308.4			
E			7.6	308.1			
E+10			7.5	308.2			
			300' S.				
E-10			7.5	308.2			
E			8.2	307.5			
⊥			8.4	307.3			
+2.⊥	⊥	⊥	7.28	308.4			
W			8.3	307.4			
+5			8.3	307.4			
+10			5.6	310.1			
			317' S.				
W-10			7.8	307.9			
W			8.9	306.8			

	8.4			307.3		
	8.4			307.3		
	8.1	Toeslope		307.6		
	345' S					
	4.0			311.7		
	7.5			308.2		
	7.8			307.9		
	9.0			306.7		
	9.0			306.7		
	9.2			306.5		
	350' S ⊥ sewer in Hole					
	⊥	25' West of Alley	Pin 8.21	307.4		
	368' S					
	10.9			305.3		
	10.0			305.7		
	9.5			306.2		
	8.8			306.9		
	6.8			308.9		
	5.0			310.7		
	382'					
	1.3			312.4		
	3.5			312.2		
	5.2			310.3		
	5.7			310.0		
	7.0			308.7		
	8.7			307.0		

315.65

W 9.5 306.2

W+10 10.3 305.4

395.5

W-10 10.5 305.2

W 7.7 308.0

W+2 6.9 308.8

+5 4.2 311.5

+8 2.6 313.1

Q 2.1 313.6

T.P. 12.87 325.93 2.59 313.06

+2 11.3 314.6

+7 8.7 317.2

E 6.8 319.1

407.5

E 3.6 322.3

+3 5.1 320.8

+7 7.3 318.6

Q 9.3 316.6

+2 9.7 316.2

+5 11.5 314.4

+8 12.5 313.4

W 14.2 311.7

+10 20.2 305.7

+20 21.5 304.4

925 South

TOKEN ON CRIPING!
K. Sec.

T.P. 11.74 334.48 3.19 322.79

334.48

48

T.P. 5.21 338.86 0.83 333.65

check ^{on E. A. Hwy} Return on ^{N. line} ^{to} ^{lands} 8.60 330.26 ^{0.08} Error

T.P.

X-Section Dwight St. from E.L. Alley East
to E.L. 38th Street. 80' - 14' S.W. 13' Quarters

JAEGER } June 23rd 1928.
Bailey
Clavert

49

Sta.	+	H.I.	-	Elev.
BM. NW. B.P. 37 th & Dwight				319.99
	3.26	323.25		
0+00	E.L. Alley			
N.L.		1.6		321.7
+2'		2.3		321.0
+2.5		3.2		320.1
N. Curb		3.8		319.5
N 1/4		3.7		319.6
¢		4.7		318.6
S 1/4		4.9		318.4
S. Curb		5.3		318.0
S.L.		4.0		319.3
0+50				
N.L.		1.30		322.0
N. Curb		2.4		320.9
N 1/4		2.8		320.5
¢		4.0		319.3
S 1/4		4.9		318.4
S. Curb		5.1		318.2
+10'		4.5		318.8
S.L.		3.5		319.8
1+00				
N.L.		1.4		321.9
N. Curb		3.0		320.3

STA	+	323.25 H.I.	-	Elev.
N/4			3.5	319.8
¢			3.8	319.5
S/4			4.0	319.3
S. Curb			4.3	319.0
S.L.			4.5	318.8
1+40	W.L. 38 th			
N.L.			3.2	320.1
N. Curb			3.8	319.5
N/4			4.2	319.1
¢			5.3	318.0
S/4			6.1	317.2
S. Curb			6.8	316.5
S.L.			8.3	315.0
1+54	W. Curb 38 th			
N.L.			4.5	318.8
+14'			5.4	317.9
N/4			5.7	317.6
¢			6.6	316.7
S/4			7.7	315.6
+13'			8.7	314.6
S.L.			9.9	313.4
1+69	W/4 38 th			
S.L.			12.8	310.5
+14'			11.2	312.1
S/4			9.9	313.4

STA		H.I.	-	Elev.
	±	323.25	8.8	314.5
	N ¹ / ₄		7.9	315.4
	+13'		7.1	316.2
	N.L.		5.6	317.7
1+80	± 38 th Str.			
	N.L.		7.6	315.7
	+14'		8.4	314.9
	N ¹ / ₄		9.8	313.5
	±		11.0	312.3
	S ¹ / ₄		12.3	311.0
	+13'		13.8	309.5
	S.L.		15.0	308.3
	T.P.		12.03	311.22 ✓
		5.18		316.40
1+93	E ¹ / ₄ 38 th			
	S.L.		10.0	306.4
	+14'		9.0	307.1
	S ¹ / ₄		7.9	308.5
	±		7.2	309.2
	N ¹ / ₄		6.3	310.1
	+13'		5.2	311.2
	N.L.		3.4	312.0
2+06	E. Curb 38 th			
	N.L.		5.4	311.0
	+14'		6.5	309.9

STA.	+	H.I.	-	Elev.
N ¹ / ₄		316.40	7.5	308.9
⊕			8.5	307.9
S ¹ / ₄			9.8	306.6
+13'			11.3	305.1
S.L.			13.2	303.2
2+20	E.L.	38 th		
S.L.			15.8	300.6
+14'			14.0	302.4
S ¹ / ₄			12.6	303.8
⊕			11.0	305.4
N ¹ / ₄			8.6	307.8
+13'			9.0	307.4
N.L.			8.0	308.4

38th 100' North from N.L. Dwight

B.M. 319.99

5.41 325.40

0+00 N.L. Dwight

0+50

W.L. 38 th			3.3	322.1
+14'			3.8	321.6
W ¹ / ₄			4.5	320.9
⊕			5.1	320.3
E ¹ / ₄			6.2	319.2
+13'			9.3	316.1

STA	+	H.I.	-	Elev.
E.L. 38 th		3254	11.0	3143
1+00				
W.L. 38 th			0.8	324.6
+14'			1.7	323.7
W $\frac{1}{4}$			2.0	323.4
¢			2.5	322.9
E $\frac{1}{4}$			3.2	322.2
+13'			4.4	321.0
E.L. 38 th			6.5	318.9

38th 100' South from S.L. Dwight

T.P. Page 51 311.22 ✓
1.65 312.87

0+00 S.L. Dwight

0+50

W.L. 38 th			2.0	310.9
+14'			4.4	308.5
W $\frac{1}{4}$			7.1	305.8
¢			10.0	302.9
E $\frac{1}{4}$			13.1	299.8
+13'			16.3	296.6
E.L. 38 th			20.8	292.1

1+00

W.L. 38 th			6.2	306.7
+14'			8.2	304.7

Jun 26 - 28
London.

13.0

54

STA	+	H.I.	-	Elev.	1+50	308.30
W 1/4 T.P.		312.87	12.0	300.87	w 1/4 +5	14.1 2942
Hand Level	0.0	300.87			±	17.3 291.0
±			3.5	297.4	+10	19.7 288.6
E 1/4			6.5	294.4	+11	20.5 287.8
+13'			11.2	289.7	1/4	21.3 287.0
E.L. 38 th			14.6	286.3	cb	24.2 284.1
BM. 0.90		320.87		319.99	E.L.	27.5 280.8
T.P. y		0.45		320.44	1+75	
T.P.	0.39	308.30	12.98	307.91	E.L.	31.5
1+25					cb	27.9 280.1
E.L.			24.2	284.1	1/4	24.7 283.6
cb			21.4	286.9	+8	22.8 285.5
1/4			17.5	290.8	±	21.2 287.1
±			13.7	294.6	+8	18.8 289.5
1/4			11.4	296.9	1/4	17.2 291.1
cb			8.0	300.3	cb	15.0 293.3
+5			6.4	301.9	+9	13.6 294.7
+10			5.0	303.3	+13	12.6 295.7
w.L.			5.0	303.3	w.L.	11.6 296.7
1+50					walk front of house at 1+75 23' W.	4.79 301.5
w.L.			7.8	300.5		
+7			9.4	298.9		
cb			11.0	297.3		
+3			12.0	296.3		
1/4			13.6	294.7		

X Sec ^{1/4} 9th St from 1+00 North.
 2+00 = N.L. Dwight.

55

TPx	12.00	333.44	320.44
1+25			
E.L.	13.5	319.9	
cb	12.2	3212	
1/4	10.3	3234	
1/4	9.7	3237	
1/4	9.1	324.3	
cb	8.8	324.6	
w.L.	8.4	325.2	
1+50			
w.L.	7.4	3260	
cb	7.7	325.7	
1/4	8.0	325.4	
1/4	8.3	325.1	
1/4	8.9	324.5	
cb	9.9	323.7	
E.L.	11.1	322.3	
1+75			
E.L.	9.6	3238	
cb	8.6	3248	
1/4	7.8	3256	
1/4	7.3	3261	
1/4	6.9	3265	
cb	6.7	3267	
w.L.	6.4	327.0	

2+00	332.44	
w.L.	5.7	327.7
cb	6.0	3274
1/4	6.2	3274
1/4	6.5	326.9
1/4	7.0	326.4
cb	7.6	325.8
E.L.	8.7	324.7
2+25		
E.L.	8.3	325.1
cb	7.3	326.1
1/4	6.5	326.9
1/4	6.0	327.4
1/4	5.8	327.6
cb	5.5	327.9
w.L.	5.1	328.3
2+50		
w.L.	4.6	3288
cb	5.0	3284
1/4	5.2	328.2
1/4	5.6	3278
1/4	6.1	3273
cb	7.1	3263
E.L.	8.3	325.1

2+75

333.44

E.L.	8.8	3246
cb	7.3	3261
1/4	6.3	3271
1/2	5.4	3280
1/4	4.9	3285
cb	4.6	3288
w.L.	4.2	3292

3+00

w.L.	4.0	3294
cb	4.5	3289
1/4	4.9	3285
1/2	5.8	3276
1/4	6.8	3266
cb	7.9	3255
E.L.	9.6	3238

3+25

E.L.	10.9	3225
cb	9.5	3229
+5	8.4	3250
1/4	7.8	3256
1/2	6.2	3272
1/4	5.5	3279
cb	4.8	3286
w.L.	4.0	3294

3+50

333.44

w.L.	4.5	3289
cb	5.2	3282
1/4	6.2	3272
1/2	7.1	3263
1/4	9.2	324.2
+8	10.1	3233
cb	10.9	3225
E.L.	13.0	3204

3+75

E.L.	14.8	318.6
cb	12.5	320.9
1/4	10.4	323.0
1/2	8.9	324.5
1/4	7.7	325.7
cb	6.2	327.2
w.L.	5.1	328.3

4+00

w.L.	6.2	327.2
cb	7.7	325.7
1/4	8.7	324.7
1/2	10.4	323.0
1/4	12.1	321.3
cb	14.3	319.1
E.L.	16.1	317.3

333.44

T.P. 3.86 324.84 12.46 320.98

D.M. Beginning 4.84 320.00 (319.99)

Nutmeg St 25cc
Columbia to State

To wide
10' curb N.
14' " S
46' Roadway
11.5' 14s

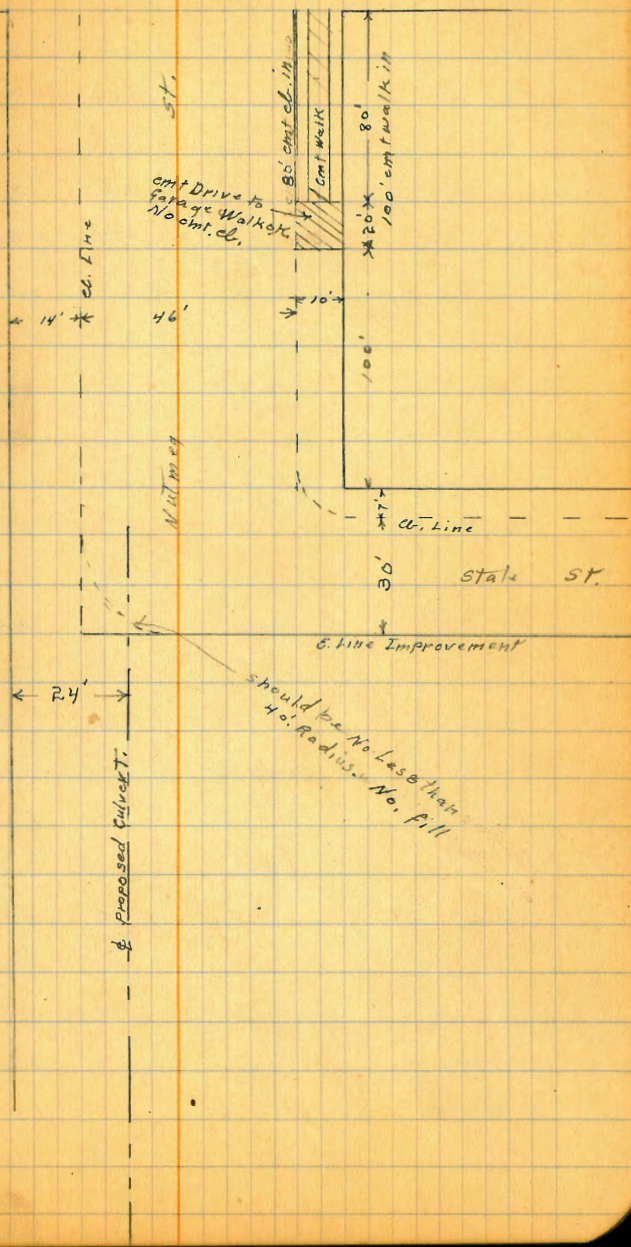
7-16-28
mille.

Columbia

ST

58

RM. B.P.	2.30	145.86	143.56	Columbia & Olive.
T.P.	4.78	138.69	11.95	133.91
E. Line Columbia.				
N. cl		7.64	131.05	cmt cl
N. gutter		8.29	130.40	Pavmt.
"		8.49	130.20	"
c		8.84	129.85	"
"		9.35	129.34	"
S. gutter		10.04	128.62	"
S. cl		9.58	129.11	cmt. cl
S		9.36	129.33	cmt Ret.
5' E				
S		9.1	129.6	
cl		9.4	129.1	
"		9.1	129.6	
c		8.4	130.3	
"		8.1	130.6	
N gutter		8.1	130.6	
50' E				
N. cl		5.18	133.5	cmt cl.
N gutter		6.3	132.4	
"		6.1	132.6	
c		6.3	132.4	
"		7.2	131.5	
"		8.3	130.4	
cl		7.6	131.1	
S		6.6	132.1	



138.69

80'E

S	5.7	133.0
+13	6.5	132.2
cl	7.0	131.7
'4	6.3	132.4
e	5.1	133.6
'4	4.9	133.8
N. gutter	4.7	134.0
N. cl	3.94	134.75
N	2.6	136.1
N	3.3	135.4
N. cl	3.55	135.14
N. gutter	4.3	134.4
'4	4.5	134.2
c	4.7	134.0
'4	5.6	133.1
cl	6.3	132.4
+5	5.4	133.3
S	5.2	133.5
S	5.3	133.4
cl	6.2	132.5
'4	5.7	133.0
e	4.8	133.9
'4	4.7	134.0
+9	4.8	133.9
cl	4.0	134.7
N.	3.0	135.1

100'E

cmtel

on dirt

on cmt Drive

Not Standard cl.

cmt. approach

To garage

138.69

Nutway St

59

+7	3.6	136.1
N.	2.5	136.2
150'E.		
N	3.9	134.8
c	4.3	134.4
+2	5.8	132.9
'4	5.3	133.4
c	5.4	133.3
'4	6.2	132.5
cl	6.9	131.8
+5	6.1	132.6
S	6.1	132.6
180'E		
S	6.6	132.2
cl	7.2	131.5
'4	7.1	132.6
c	6.6	132.1
'4	6.7	132.0
+9	6.6	132.1
cl	5.3	133.4
N.	5.0	133.0
200'E. = W line StaTe		
N.	5.5	133.2
cl	6.9	131.8
'4	7.2	131.5
c	7.3	131.4

138.69

200' E = W. Line State (cont)

S. 1/4		7.5	131.2
S. 1/4		7.7	131.0
+7		7.6	131.1
S.		8.8	129.9
+20		14.0	124.7
T.P.	4.14 134.91	7.92	130.77
	7' E. of W. Line = W. Line State.		
-30		19.0	115.9
-20		16.3	118.6
S		5.9	129.0
+5		3.9	131.0
1/4		3.9	131.0
1/4		3.8	134.9
C		3.7	125.0
1/4		3.5	125.2
1/4		3.2	131.7
N		2.6	132.3
	12' E. of W. Line		
N		2.6	132.3
1/4		3.6	131.9
1/4		3.6	135.1
C		3.7	125.0
1/4		3.8	131.1
S. 1/4		4.0	130.9
+2		5.8	127.1
S		8.0	126.9

134.91

Nulmed

60

+20		18.1	140.6
	15' E. of W. Line = State St Rdw.		
-20		19.0	119.7
-13		15.7	123.0
-10		18.8	121.9
S		11.9	123.0
1/4		4.1	130.8
1/4		3.8	131.1
C		3.7	135.0
1/4		3.6	130.1
1/4		3.0	131.9
N		2.6	132.3
	20' E. of W. Line		
N		2.6	132.3
1/4		3.3	131.6
1/4		3.5	131.2
C		3.3	131.6
1/4		4.3	130.6
+1		5.4	127.5
1/4		5.6	133.1
+5		7.4	131.3
+9		6.2	132.0
S		8.5	130.2
+10		14.4	122.3

134.91
25' E. of W. cl

-10	15.1	1236
S	9.3	129.4
+8	6.0	128.9
cl	6.3	128.6
+5	7.8	127.1
"	8.5	130.4
C	3.4	131.5
"	3.5	131.4
cl	3.2	131.7
N.	2.8	132.1

30' E. of W. cl = E. line improvement

N	3.0	131.9
cl	3.2	131.7
"	3.5	131.4
+5	3.5	131.4
+6	4.6	130.3
C	4.8	130.1
"	7.6	127.3
cl	9.8	125.1
+8	7.4	131.3
S	10.1	128.6
+10	12.6	126.1

40' E. of W. cl.

S	15.0	123.7
+6	14.0	124.7
cl	13.0	115.7

134.91

Nulmeq St

61

"	13.8	124.9
+6	12.7	122.2
C	8.8	126.1
"	5.2	129.7
cl	8.4	126.5
+8	10.4	124.5
N.	6.4	128.5

Levels for Proposed Drain
 24' N. of S. Line Nutmeg St.
 State St. to Reynard Way

This Line is
 on 2" Water
 main

60.58

Nutmeg St

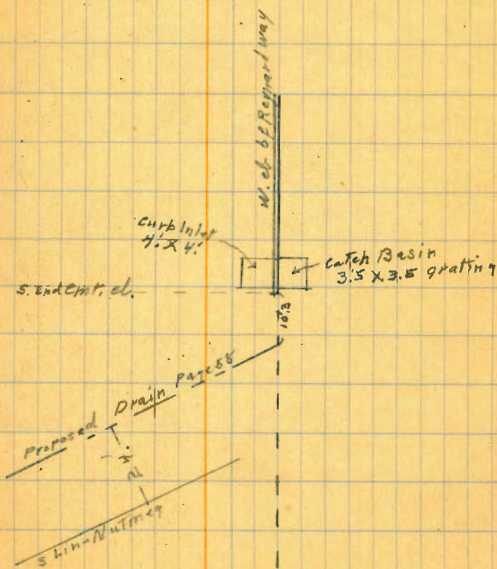
62

Σ 134.91

Page 61.

00 = W. Line State St.		3.8	131.1	
0+25		4.1	130.8	
0+40		9.8	125.1	
T.P.	0.17	122.14	12.94	121.97
0+50		3.1	119.0	
0+52		6.1	116.0	
0+66		12.8	109.3	
T.P.	0.32	109.39	13.07	109.07
0+75		6.2	103.2	in wash
0+85		5.3	104.1	
35.0' of 0+85		9.5	99.9	in wash
1+00		13.4	96.0	
T.P.	0.24	96.70	12.93	96.46
1+17		6.7	90.0	
T.P.	0.34	84.23	12.81	83.89
1+40		2.8	81.4	
1+57		8.0	76.2	
1+63		12.2	72.0	
T.P.	0.61	72.48	12.36	71.87
1+74		4.9	70.6	
1+75		6.0	66.5	
1+83		7.5	65.0	Water Meter on E. End 2" Pipe
4' N. of 1+83		12.0	60.5	in Wash
T.P.	0.15	60.58	12.05	60.43

1+88	4.6	56.0
2+00	4.7	55.7
2' N. of 2+00	8.3	52.3 in wash
2+00.7 = R.L. with W. el. Line of Reynard Way	8.3	52.3
10' N. of above P.T. on W. el. of Reynard Way	8.45	52.1 Top curb
Top of grating	10.05	50.5
Flowline Catch Basin	13.6	47.0



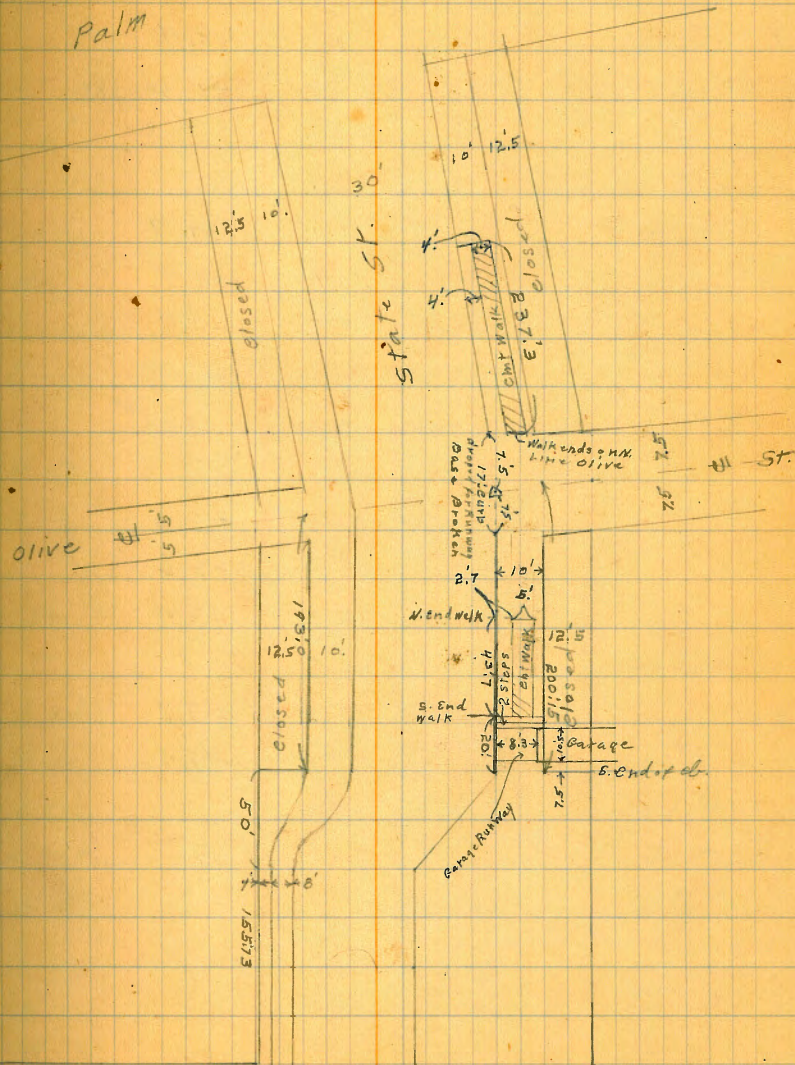
37' wide
 4' acceptance on W
 8' cl. on W
 25' Roadway

State St. X See Nutmeg to Palm 1-20-24 miles

T.P. Page 60 12.61 143.38 130.77

00 = N Line Nutmeg

W.	10.2	133.2
+4 = edge acceptance	10.8	132.6
+12 = N. cl.	11.1	132.3
cl + 12.5 = $\frac{1}{2}$ Roadway	11.1	132.3
cl + 25 = E. edge Roadway	11.1	132.3
25' N		
E. edge Rdw.	9.7	133.7
+3	9.1	
$\frac{1}{2}$ Rdw	9.5	
cl	9.9	133.5
+8 = acceptance	9.3	134.1
+10	7.2	136.2
W	6.4	137.0
25' N		
W	5.4	138.0
+3	5.9	137.5
+4	7.2	136.2
+12 = cl	7.4	136.0
$\frac{1}{2}$ Rdw	7.3	
$\frac{1}{2}$ +10	6.8	
E	7.7	135.7
+23	24.2	
+30	26.8	
+40	29.4	



ST.

33

143.38

70' N

E-45			30.8	
E-22			20.3	
E			4.7	138.7
+2			3.2	140.2
+4			3.7	
± rdw			3.7	
cb			3.7	139.7
+8			3.7	139.7
+9			2.7	140.7
W			2.2	141.2
T.P.	13.06	156.10	0.34	143.04
		95' N		
W			12.5	143.6
+4			12.5	143.6
cb			12.7	143.4
± Rdw			12.5	
± ± 10.5			12.5	143.6
E			14.2	141.9
+15			26.4	
+35			34.1	
		106' N		
-35			31.4	
-23			27.7	
E			11.8	144.3
+2			11.0	145.1
± rdw			10.8	

156.10

State St

64

cb			11.5	144.6
+8			11.4	144.7
W			11.4	144.7
				112' N = S. Line Garage on W dirt floor
W			9.8	146.3
+3 = E Line Garage			8.8	147.3 floor.
+4			9.6	146.5
cb			10.5	145.6
± Rdw			9.7	
± +10			9.8	
E			12.4	143.7
+13			22.5	
+30			28.4	
				125' = N Line Garage on W
-30			26.2	
E			17.8	148.3
± Rdw			7.5	
W cb			8.6	147.5
+8			8.7	147.4
+9 = Front of Garage			8.7	147.4 floor
W			7.5	148.6
				130' N
W			7.1	149.0
+4			7.3	148.8
cb			7.4	148.5
± Rdw			7.0	

156.10

130' N. (cont)

E		7.4	148.7	
	155.7 N.			
E		2.6	153.5	
φ Rdw		3.1	153.0	
+8		3.8	152.3	
Web		3.0	153.1	
+8		3.2	152.9	
W		3.4	152.7	
T.P.	13.04 168.78	0.36	155.74	
	180.7			
W		11.3	157.5	
+4		11.7	157.1	
+8		12.5	156.3	
+15		12.7	156.1	
+20.5		12.2	156.6	
+37		11.1	157.7	
+47		10.9	157.9	
	0+00 205.7 = S. End of	existing curbs closing on each side		
New E. line to N		7.0	161.8	
+10 = cl		7.70	161.1	S. End. em. cl.
φ		8.0		
+14		8.7		gutter
cl		7.8	161.0	emt cl
+10 = New W line to N		7.7	161.1	
+18.5		6.0	162.8	
cl + 2 = S. old Line		6.0	162.8	

168.78

Stat. St

	7.5 N of 0 + 00 = S. line Garage			
E. cl Top		6.60		162.2
E. cl. dipped for Runway		6.93		161.85 ^{emt Runway}
8.3 E. of 8. cl = W. line Garage		5.94		162.8 ^{emt Runway}
17.5 N of 00 = N. line emt Runway				
8.3 E. of 8. cl = W. line Garage		5.73		163.05
E. cl dipped for drive		5.40		163.18
20' N. of 0 + 00 = S. End Cmt. Walk on E				
E		4.2		164.6
E. cl		4.55		164.23
gutter		5.0		
"		5.0		
T.P. 6.97	174.97	0.78		168.00
φ		11.0		
"		11.2		
gutter		11.5		
Web		11.06		163.91
	54.5 N of 00			
W. cl		5.82		169.15
gutter		6.8		
"		6.2		
e		6.0		
"		6.1		
gutter		6.0		
E. cl		5.38		169.59
	69.5 N. of 0100 = BxK			
E. cl		3.02		171.95
gutter		3.7		
"		3.9		
e		3.8		

65

174.97

69.5 N (con) Brk

1/4			4.0	
gutter			4.7	
W. cl			3.43	171.54
	84.5 N			
W. cl			2.07	172.90
gutter			2.4	
1/4			2.3	
e			2.1	
1/4			2.1	
gutter			1.8	
E. cl			1.48	173.49
T.P.	12.10	182.05	0.02	174.95
		139.5 N		
E. cl			8.03	179.02
gutter			8.9	
1/4			8.5	
e			8.5	
1/4			9.0	
gutter			9.6	
W. cl			8.93	178.12
	154.5 N	Brk		
W. cl			7.46	179.59
gutter			8.4	
1/4			7.8	
e			7.2	
1/4			7.3	

187.05

State St.

66

gutter			7.6	
E. cl			6.50	180.55
	149.5 N			
E. cl			5.91	181.14
gutter			6.7	
1/4			6.4	
e			6.4	
1/4			7.0	
gutter			7.4	
W. cl			6.84	180.21
	192.0 N. on E. cl } = 5. Lines of Olive produced E & W to Curb lines			
	190.0 N. on W. cl }			
W. cl			6.05	181.00
gutter			6.5	
1/4			6.0	
e			5.5	
1/4			5.4	
gutter			5.8	
E. cl			5.17	181.88
	195.0 N. on W. cl } = Δ @ Olive St section on split			
	198.5 N on E. cl }			
E. gutter (curb dropped for drive way)			5.4	181.65
1/4			5.2	
e			5.2	
1/4			5.8	
gutter			6.3	
W. cl			5.86	181.29

187.05

5' N. of A on W. cl. }
7.5' N. of A " E cl. } N. hinges of olive St Produced E. + W. to cl Lines

W. cl	5.72	181.33
gutter	4.1	
"	5.7	
E	5.1	
"	5.0	
gutter	5.2	
E. cl	4.25	182.80
44.3' N. of (A & olive) on E. cl.		
40' N. of (A & olive) on W. cl. = Brk 0700 = 90°		
E. cl	3.09	183.96
gutter	4.2	
"	4.0	
E	4.1	
"	4.6	
gutter	5.0	
W. cl dipped for Runway (Figures)	4.58	182.47

50' N. of above 0700

W. cl	3.90	183.15
gutter	4.4	
"	4.0	
E	3.3	
"	3.1	
gutter	3.3	
E. cl	2.42	184.63

105' N. of 0700 Apparent Brk

E. cl	1.73	185.32
gutter	2.7	

187.05

"	2.6	
E	2.7	
"	3.4	
gutter	3.7	
W. cl	3.25	183.80

125' N. of 0700 Apparent B.

W. cl	3.21	183.14
gutter	3.9	
"	3.3	
E	2.5	
"	2.6	
gutter	2.6	
E. cl	1.82	185.23

145' N. of 0700

E. cl	2.07	184.98
gutter	2.9	
"	2.7	
E	2.4	
"	3.5	
gutter	4.2	
W. cl	3.48	183.57

145' N. of 0700

W. cl	3.94	183.11
gutter	4.7	
"	4.0	
E	3.2	

187.05
165' N. (con)

"4	3.3	
gutter	3.5	
E. cl	2.49	184.56

185' N

E. cl	3.22	183.83
gutter	4.2	
"4	4.0	
e	4.0	
"4	4.8	
gutter	5.5	
W. cl	4.80	182.25

205' N

W. cl	5.69	181.36
gutter	6.5	
"4	5.8	
e	5.0	
"4	5.0	
gutter	5.2	
E. cl	4.18	182.87

T.P. 1.84

182.42

6.47 180.58

225' N

E. cl	2.73	181.69
gutter	1.9	
"4	1.7	
e	1.7	
"4	2.4	

182.42

State St

68

gutter	3.1	
W. cl	2.17	180.25

245' N

W. cl	3.91	182.51
gutter	4.9	
"4	4.1	
e	3.3	
"4	3.0	
gutter	3.2	
E. cl	2.27	180.15

265' N

E. cl	3.99	178.43
gutter	5.1	
"4	4.8	
e	5.2	
"4	6.1	
gutter	7.0	
W. cl	5.96	176.46

285' N

W. cl	8.33	174.09
gutter	9.3	
"4	8.3	
e	7.3	
"4	7.0	
gutter	7.3	
E. cl	5.94	176.48

182.42
305' N.

E. cl		8.13	174.39
gutter		9.7	
"y		9.3	
e		9.6	
"y		10.5	
gutter		12.0	
W. cl		10.78	171.64
T.P.	5.78	176.62	170.84
		3.25' N.	
W. cl		7.48	169.14
gutter		8.4	
"y		7.2	
e		6.3	
"y		6.0	
gutter		6.1	
E. cl.		4.76	171.86
E. line	350' N. = N. Endemic cl. on E & W = S. line Palm	6.8	169.8
E. cl		7.62	174.40 169.0
gutter		8.8	
"y		8.9	
e		9.3	
"y		10.2	
gutter		11.3	
W. cl		10.55	166.07
			+71.87
+10 = New Trip		10.6	
+22.5 = old whine state		14.2	

176.62
10' N. of S. line Palm St

Palm St 25' cl. S
7.5' 145
stat st
69

old W line		15.5	
+12.5		12.2	
+22.5 = Del		12.4	
"y		10.2	
e		10.4	
"y		10.1	
E. cl		9.3	
+5		8.3	
+10 = New E. line		+3.3	179.9
	17' N of S. line Palm		
New E. line		+2.4	179.0
+4		5.6	
E. cl		9.7	
"y		10.8	
e		11.3	
"y		11.8	
cl		12.8	
+10		14.4	
+22.5		16.7	
	25' N of S. line Palm = S. cl		
N. cl = 22.5		16.4	
"y = 10		14.6	
W. cl		13.4	
"y		12.7	
e		12.0	
"y		11.0	

176.62

1/4 + 4	9.9	
E. cl	6.8	
+ 7	3.6	
MoNew E. line	10.5	177.1
	S. 1/4	
E	0.0	
+ 2	2.1	
+ 10 = cl	4.3	
+ 3	5.1	
1/4	9.0	
E	11.8	
1/4	13.2	
W. cl	13.5	
+ 10	14.8	
+ 22.5	17.1	
	Φ	
W. cl - 22.5	17.1	
- 10 = New line	15.0	
W. cl	13.7	
1/4	12.8	
E	11.4	
+ 2	7.0	
1/4	4.1	
E. cl	3.2	
+ 10 = New E. line	1.4	

176.62

State St

70

E.	N. 1/4	1.8
+ 10 = cl		3.7
1/4		5.1
E		7.3
1/4		9.3
W. cl		13.7
+ 10		14.9
+ 22.5		17.2
	N. cl	
W. cl - 22.5		16.3
W. cl - 10		13.9
W. cl		11.4
1/4		10.0
E		8.0
1/4		6.3
E. cl		4.4
E		2.3
	12.5 N of N. cl	
E		2.8
cl		5.0
1/4		6.6
E		7.9
1/4		9.4
cl		10.8
+ 10		12.7
+ 22.5		16.7

176.62
25' N. of N. cl = N. Line Palm

W cl - 2.5	17.6
W cl - 10	13.9
W. cl	12.0
14	10.6
e	9.1
14	7.4
cl	5.4
e	4.0

State St

71

14/4/88 Water Main alley int City Hqrs
 Moore

= NL Redw.	2.30	~67.10	263.8	= EL STOP NE Redwood
0+05 ✓			5.5	~61.6
0+15 ✓			6.8	~60.3
(0+03) alley = MH RPT ✓			4.70	262.1 ✓
T.P.	10.55	~74.35	2.30	~63.80
0+47.5 ✓			1.90	~72.45
T.P.	14.03	~84.48	1.90	~74.45
0+50 = 5 Redwood ↓			2.1	~82.4
0 alley "	"		1.1	~83.4 ✓

$$\begin{array}{r} 260.3 \\ 209.0 \\ \hline + 1.9 \\ \hline 261.6 \end{array}$$

$$\begin{array}{r} 261.6 \\ 259.9 \\ \hline + 1.9 \\ \hline 263.8 \end{array}$$

$$\begin{array}{r} 263.8 \\ 272.4 \\ \hline + 8.7 \\ \hline 272.4 \end{array}$$

$$\begin{array}{r} 272.4 \\ 268.4 \\ \hline + 14.0 \\ \hline 282.4 \end{array}$$

0+05 ✓
 0+15 ✓
 0+47.5 ✓
 0+50 = 5 Redwood
 0 alley "

Levels on Redwood Central, east,
 are N.G. BK 1259
 E run only

1/28/09
Moore
Level 91K 69 CITY HATS
5' east of E of alley
✓ - STATION AT CUTS for FL. of water line

HWBP	4.70	310.19		310.19
SL. Nightman = 00 ✓			2.6	337.6
0+4 ✓			6.7	333.5
0+50 ✓			9.4	330.8
1 ✓			10.3	329.9
450 ✓			10.4	329.8
8			13.1	327.1
T.P.	0.24	327.43	13.00	327.19
2+10 ✓			1.5	325.9
2+45 ✓			11.3	316.1
T.P.	0.06	314.73	12.76	314.69
2+65			4.2	310.5
2+80 ✓			6.7	308.0
2+100 ✓			7.6	307.1
2+50			7.6	307.1
3+65 ✓			5.8	308.9
3+90			0.0	314.7
T.P.	11.37	326.04	0.06	314.67
4+10 ✓			4.0	322.0
T.P.	12.34	338.38	0.00	326.04
4+30 ✓			11.8	326.6
4+50 ✓			5.5	332.9
4+75			4.5	333.9
4+85 ✓			4.2	334.2
5+20 ✓			3.7	334.7
5+40 ✓			3.6	334.8

4107 Nightman	5+60 ✓	3.1	335.3
	5+87	2.7	335.7
	5+15	2.8	335.4
	6 = N.L. Lenses ✓	7.7	330.7

8.00
330.32
330.32 = nail in pole
opt error

100' wide
25' cbs

Mt. View Drive

Curb Levels 35th to 33rd STs

Measurements taken on South Curb
shots on N. curb or radial lines opposite

7-20-28
m.l.l.

S.W. Mt. View Drive

(57)

398.87
150' W. on S. cb = W. Alley Ret

75

B.M.B.P	5.16	398.17 ^v	398.01	+ Hawley	15' S. of S. cb = S. end Alley Return	3.38	395.49
T.P.	4.18	398.87	4.48	394.69 ^v	S. cb	3.65	395.22
(58)		East line of 35 th ST	60' wide 12' cbs Produced		N. cb	4.26	394.61
N. cb Mt. View Drive		3.10		395.77	(56)	200' W. on S. cb	
S. " " " "		3.16		395.71	N. cb	4.40	394.47
(59)		E. cb. line 35 th ST			S. cb	3.69	395.18
S. line Mt. View Drive		3.23		395.64	(55)	250' W. on S. cb	
N. " " " "		2.95		395.92	S. cb	3.83	395.04
(62)		W. cb. line 35 th ST			N. cb	4.47	394.40
N. line Mt. View Drive		3.91		394.96	(54)	300' W. on S. cb	
S. " " " "		3.54		395.33	N. cb	4.52	394.35
(61)		W. line 35 th ST Produced			S. cb	3.93	394.94
S. cb. Mt. View Drive = 0+00		3.47		395.40	(53)	350' W. on S. cb	
N. " " " "		3.94		394.93	S. cb	3.97	394.90
(60)		50' W. on S. cb			N. cb	4.65	394.22
N. cb		4.06		394.81	(52)	400' W. on S. cb	
S. cb		3.65		395.22	N. cb	4.68	394.19
(59)		100' W. on S. cb.			S. cb	4.03	394.84
S. cb		3.62		395.25	T.P.	3.31	397.82 ^v
N. cb		4.13		394.74	(51)	429' W. on S. cb = E. Line Mansfield ST 12' cbs. Produced	394.51 ^v
(58)		129' W. on S. cb = E. Alley Ret			S. cb	3.02	394.80
N. cb		4.32		394.55	N. cb	3.56	394.26
S. cb		3.65		395.22	(50)	E. cb Mansfield on radial line	
15' S. of S. cb = S. end Alley Ret		3.38		395.49	14.6 S. of S. cb = N. end Pavment on Mansfield	3.02	394.80 on curb
					" " " " " " " " " " " "	3.46	394.36 on Pavment
					50' S. on E. cb Mansfield	3.10	394.72 on curb
					" " " " " " " " " " " "	3.57	394.25 on Pavment

Plotted
T.M.M.

		397.82	
(43)	on Radialline W. ch. Mansfield		
14.8 s. of s. ch.	W. end Parmit on Mansfield	3.50	394.82 on parmit
" " " " " " " "	" " " " " " " "	3.13	394.69 on ch
(44)	oo = Mine Mansfield Produced		
S. ch		3.13	394.69
N. ch		3.85	393.98
(47)	50' W. on s. ch		
N. ch		3.83	393.99 ^{4.00}
S. ch		3.36	394.46 ⁴⁸
(46)	100' W. on s. ch		
S. ch		3.47	394.35 ³⁷
N. ch		4.24	393.58 ⁶⁰
(45)	130' W. on s. ch = E. Alley Ret.		
N. ch		4.12	393.70 ⁷⁰
S. ch		3.62	394.20 ²⁰
14.6 s. of s. ch = S. end Alley Ret		3.14	394.68 ⁷⁰
(44)	141' W. on s. ch = W. Alley Ret.		
14.6 s. of s. ch = S. end Alley Ret		3.38	394.44 ⁴⁶
S. ch		3.79	394.03 ⁰⁵
N. ch		4.03	393.69 ¹¹
(45)	180' W. on s. ch.		
N. ch		4.40	393.44 ⁴¹
S. ch		3.79	394.03 ⁰⁵
(42)	210' W. on s. ch		
S. ch		3.84	393.98 ^{4.00}
N. ch		4.12	393.70 ⁷⁰

		397.82	
		250' W. on s. ch	
(41)	N. ch	4.31	393.54
	S. ch	3.90	393.51
			393.95
			393.97
			Hawley 100' W. of s. ch.
(39)	274 W. on s. ch = 0.7 W. of E. line Hawley = E. end Paved Intersection		
	S. ch	3.80	394.05
			394.02
			393.54
			393.51
			produced from W
			P.E. E. line Hawley, W. N. ch Mt. View Drive
			393.72
(40)	curb & Parmit	4.13	393.69
	Flow line E & W 1/2 Round Culvert. E & W	4.74	393.11
			393.08
			11' W. of E. line Hawley on s. ch Mt View Drive = E end Culvert
			394.05
			394.02
			393.37
			393.34
			Flow line 1/2 Round Culvert intake
			4.48
			E. ch. Hawley
			outlet of above Culvert
			393.27
			393.24
			Flow line
			393.98
			393.95
			Top Curb
			W. ch. Hawley
			393.27
			393.24
			Flow line
			393.92
			393.89
			16' S. of s. ch Mt View Drive
			4.58
			3.93
			15' W. of W. ch. Hawley = inlet above Culvert
			394.01
			393.98
			393.32
			393.29
			Top ch
			3.84
			Flow line
			4.53
(38)	23.3 W. of E. ch. Hawley on S. ch Mt View Drive = W. end Parmit		
	Top ch	3.83	394.02
			393.99
			393.52
			393.49
			gutter parmit
			4.33
			oo = Mine Hawley Produced from S.
			394.02
			393.99
			S. ch
			3.83

Mt View Drive
3.87
394.01 dk RM.

397.82

(31)	1.7 W. of W. line Hawley produced from N.			393.77	
N. cl Mt View Drive	4.08	393.77	Top cl		
" " " "		393.13			
" " " "	gutter	393.10	Flowline - End Column		
(36)	50' W. on S. cl from W. line Hawley produced from S.				
S. cl Mt View Drive	3.57	394.28			
" " " "		393.88			
" " " "	3.97	393.85			
(35)	100' W. on S. cl				
N. cl	3.90	393.95			
" " " "		393.92			
" " " "		394.27			
S. cl	3.58	394.24			
" " " "		393.90			
T.P.	5.70	399.57	3.95	393.87	
(31)	145' W. on S. cl = E. Alley Ret.				
on Radial line		394.81			
14.8 S. of S. cl = S. End Alley Ret.	4.79	394.78			
S. cl	5.25	394.35			
" " " "		394.32			
" " " "		394.10			
N. cl	5.50	394.07			
(33)	168' W. on S. cl = W. Alley Ret.				
N. cl	5.35	394.25			
" " " "		394.22			
" " " "		394.67			
S. cl	4.93	394.64			
on Radial line		395.01			
S. of S. cl = S. End Alley Ret	4.59	394.98			
(32)	200 W. on S. cl				
N. cl	5.11	394.49			
" " " "		394.46			
" " " "		394.84			
S. cl	4.76	394.81			
(31)	250' W. on S. cl				
S. cl	4.54	395.06			
" " " "		395.03			
" " " "		394.62			
N. cl	4.98	394.59			
(30)	300' W. on S. cl				
N. cl	4.79	394.81			
" " " "		394.78			
" " " "		395.43			
S. cl	4.17	395.40			

MT View Drive

399.57

	T.P.	4.83	399.84	4.56	395.05
					395.01
(29)	320' W. on S. = E. line 34 th produced from S.				60' wide 12' hrs.
S. cl			4.35		395.53 x
					395.49
	S. line Mt View 4 E. cl of 34 th St = N. End Pavmt.				
cl			4.36		395.52 x
					395.48
	pavmt		4.86		395.02 x
	← MT View Drive				394.98
	E. line Floral Drive + W. line		4.96		394.92
					394.88
	N. line Mt. View Drive E. cl Floral Drive		4.94		394.96
					394.90
	" " " " " W " " "		4.92		394.96
					394.92
	N. cl " " " W line " "		4.85		395.03
					394.99
	S. line Mt View Drive W. cl of 34 th St.	(28)			
Top cl			4.09		395.79 x
					395.75
	gutter N. End Pavmt		4.50		395.38 x
					395.34
(27)	21' W. of W. line of 34 th St on S. cl Mt. View Drive = N. End 15' Rad Ret.				
S. cl			3.98		395.90 x
					395.86
N. cl			4.91		394.97 x
					394.93
(26)	50' W. of W. line 34 th produced on S. cl.				
N. cl			4.97		394.91
					394.87
S. cl			4.13		395.75
					395.71
(25)	100' W. on S. cl.				
S. cl			4.33		395.55
					395.51
N. cl			5.16		394.72
					394.68
(24)	150' W. on S. cl				
N. cl			5.33		394.55
					394.51
S. cl			4.57		395.31
					395.27

399.84

200' W. on S. cl

(13) S. cl 4.89
N. cl 5.60

(22) 250' W. on S. cl

N. cl 5.71
S. cl 5.06

T.P. 3.77 398.11 5.56 394.34

(21) 300' W. on S. cl

S. cl 3.55
N. cl 4.02

(20) 350' W. on S. cl

N. cl 4.14
S. cl 3.70

(19) 389' W. on S. cl = E. Alley Ret

14.8 S. of S. cl = S. End Alley Ret 3.56

S. cl 3.99
N. cl 4.20

(18) 405.5' W. on S. cl = W. Alley Ret

N. cl 4.35
S. cl 4.08

14.8 S. of S. cl = S. End Alley Ret 3.60

(17) 450' W. on S. cl

S. cl 4.20
N. cl 4.44

(16) 500' W. on S. cl

N. cl 4.55
S. cl 4.55

398.11

(15) 546' W. on S. cl = N.E. line Arthur st Produced

S. cl 4.63
S. gutter = Flow Line 8" Culvert 5.56

N. cl 4.72

15' S. of S. cl + N.E. cl of Arthur st End Culvert

Top curb 4.76

Flow Line 8" Culvert 5.68

S. Line Mt View + N.E. curb Arthur

Top cl 4.78

S. Line Mt View + S.W. curb Arthur

Top cl 5.10

16' S. of S. cl Mt. View + S.W. cl Arthur

Top cl 5.05

Flow Line 8" Culvert 6.03

(14) 00 = S. cl. Mt View Drive + S.W. Arthur Produced

S. cl 4.93

Flow Line 8" Culvert 5.99

N. cl 4.97

(13) 50' W. on S. cl

N. cl 5.38

S. cl 5.07

(12) 100' W. on S. cl

S. cl 5.16

T.P. 3.76 396.60 5.27 392.84

N. cl 3.84

Mt. View Drive

78

(393.54)

393.48

(392.67)

392.55

(393.48)

393.39

(393.41)

393.35

(392.49)

392.43

(393.39)

393.33

(398.07)

398.01

(393.12)

393.06

(392.11)

392.08

(393.24)

393.18

(392.12)

392.12

(393.20)

393.14

(392.79)

392.73

(393.10)

393.04

(393.01)

392.95

(392.82)

392.76

	396.60	
⑪ 150' W. on S. cl		
N. cl	3.94	392.72 392.66
S. cl	3.71	392.90 392.89
⑩ 200' W. on S. cl		
S. cl	3.81	392.85 392.79
N. cl	4.07	392.59 392.53
⑨ 250' W. on S. cl		
N. cl	4.20	392.46 392.40
S. cl	3.83	392.83 392.77
⑧ 278' W. on S. cl = E. line Panama st (approx)		
S. cl	3.91	392.70 392.69
N. cl	4.30	392.37 392.30
N. line MT View Drive		
E. cl Panama 20' Roadway	4.47	392.20 392.13
W. " "	4.69	391.92 391.91
⑦ 325' W. on S. cl = W. line Panama (approx)		
N. cl	4.54	392.13 392.06
S. cl	4.06	392.67 392.54
⑥ 400' W. on S. cl		
S. cl	4.24	392.43 392.36
N. cl	4.72	391.95 391.88
⑤ 450' W. on S. cl		
N. cl	4.95	391.72 391.65
S. cl	4.32	392.35 392.28
④ 500' W. on S. cl		
S. cl	4.50	392.17 392.10
N. cl	5.04	391.63 391.56

③ 550' W. on S. cl = P.C. 2' Rad Ret into Alley		
N. cl	5.25	391.42 ✓ 391.35
S. cl	4.56	392.11 ✓ 392.04
on Radial line		392.46 ✓ 392.39
15' S. of S. cl = SE. End Alley Ret	4.21	
② 606' W. on S. cl = P.F. SW. Alley Ret		
S. cl	4.28	392.39 ✓ 392.32
15' S. of S. cl on Radial line		392.00 ✓ 391.99 ✓
S. cl at P.F.	4.61	391.81 ✓ 391.74
N. cl	5.36	
T.P.	4.73	396.50
	4.83	391.77
① 637' W. on S. cl = E. line 33 rd St Produced		
N. cl	5.37	391.70 ✓ 391.63
S. cl	4.50	392.07 ✓ 392.00
E. cl. 33 rd St		
15' S. of S. cl MT View on 33 rd	4.48	392.09 ✓ 392.02 Top cl.
" " " " " " " "	4.94	391.63 ✓ 391.56 gutter Parrot
W. cl 33 rd St		
15' S. of S. cl MT View = N. end Parrot on 33 rd	4.48	392.02 gutter Parrot
" " " " " " " "	4.10	392.47 ✓ 392.40 Top cl
W. line 33 rd Produced		
S. cl	4.14	392.32 392.39
N. cl	5.53	390.97 391.04 SW 33 rd
B.M. B.P.	4.19	392.31 = MT View 392.38

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 1/2 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not

**IMPROVED TABLES
AND
INFORMATION**

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given L may be found by dividing tangent (or external), opposite L by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

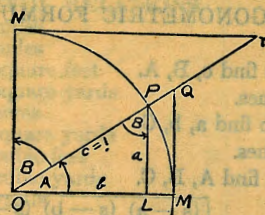


TABLE II
TRIGONOMETRIC FORMULÆ.

$$\angle A = \angle MOP \quad \angle B = \angle PON = \angle OPL$$

$$R = OB = c = 1$$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

$$\sin \frac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \quad \cos \frac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \quad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Lines} \quad \frac{\sin A}{a} = \frac{\sin B}{b} = \frac{\sin C}{c}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$$

5

ENGINEERING DEPARTMENT,
CITY OF
SAN DIEGO,
CALIFORNIA.

31° 24' x 2 .62° 48'

24° 06' x 2 42° 52'

56° 40' - 30'

4.02
38.17
34.15
2.40
26

319.99

5.41

325.40

1338.38

4113.41

56-40-30

33448

371

33737

529

33661

375

33786

33886

311

33575

520

34055

332

33227