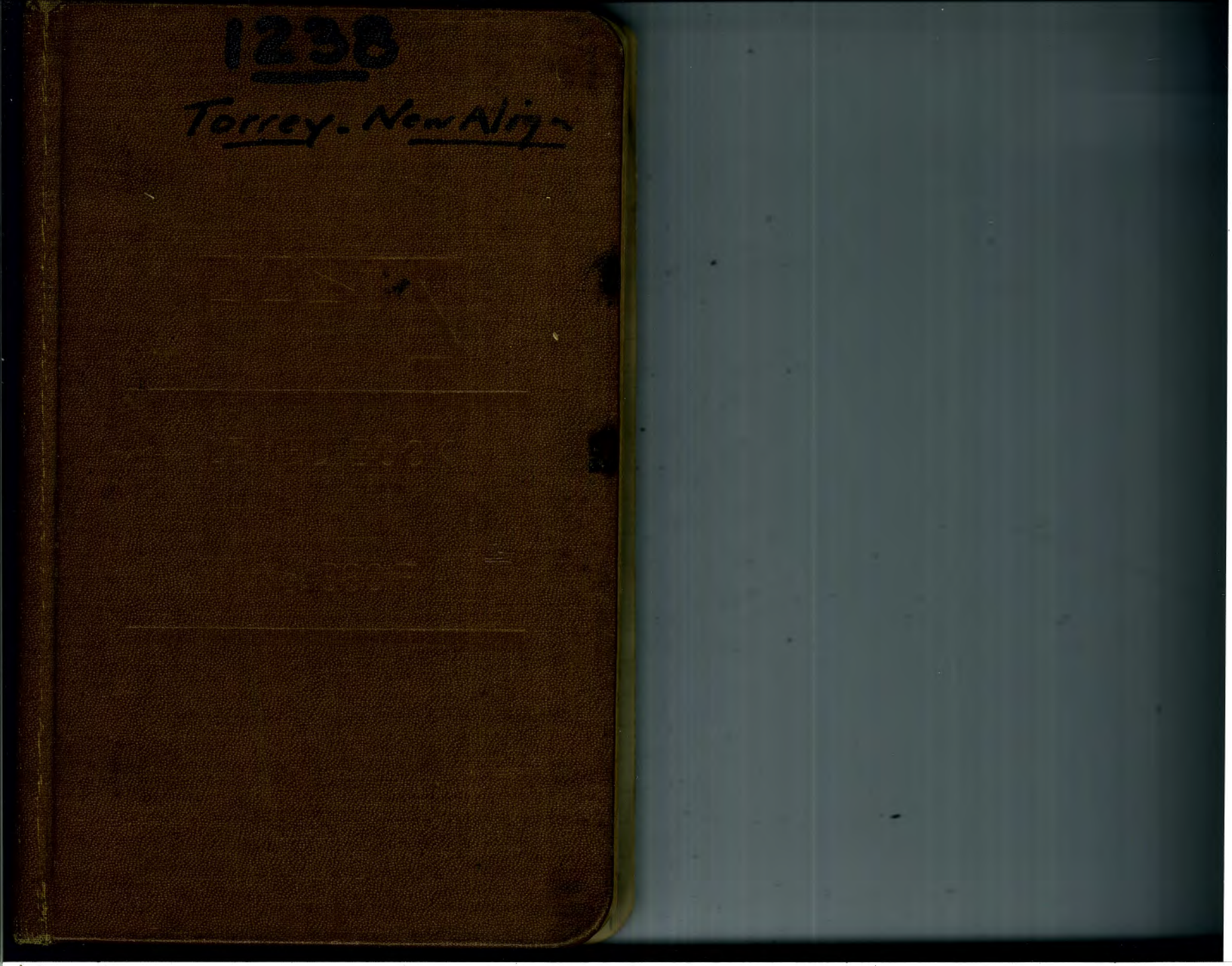
1238
Torrey - New Algæ

Our Leather Bound Engineers Note Books are carried in the following rulings:

No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.

No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.

No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.

No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

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THE FREDERICK POST CO.

ENGINEERING and DRAFTING SUPPLIES

IRVING PARK STATION

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JAEGER
Bailey
Clavert

Torrey Pines Road — Febr. 15th 1918

STA.	Dist	Defl. ∠	V.A.	Diff. El.	Elev.
	177.00				
20+79		38°10'R	7°13'-		
	71.00				
20+08		12°53'L	9°22'-		
	257.00				
17+57 ✓		45°56'L	1°57'-		187.41
	220.00			-46.38	
15+37.00 ✓	✓	29°27'-L	12°27'-		233.79
	84.00			-3.07	
14+53.00 ✓	✓	3°59'-L	2°05'-		236.86
	39.00			+4.45	
14+14.00 ✓		7°09'-L ✓	6°35'+		232.41
	97.00			-5.80	
13+17.00 ✓		4°11'-R ✓	3°25'-	- ✓	238.21
	48.00			-2.02	
12+69.00 ✓		27°58'-R ✓	2°28'-	✓	240.23
	292.00			-15.77	
9+77.00 ✓	✓	56°26'R	3°05'-	✓	256.41 ✓
	315.00			-29.14	
6+62.00		3°19'L ✓	5°20'-		285.55
	116.00			-8.73	
5+46.00	✓	11°16'R	4°20'-		294.28 ✓
	146.00			-5.72	
4+00			2°15'-		300.00
0+00					302.90

%	Elev.	Cut	
			Outer Edge of Road.
			Outer Edge of Road
			Outer Edge of Road
	243.95		Outer Edge of Road.
6%			
	258.65		
6%			
	277.55	8.00	
BC. of Curve			

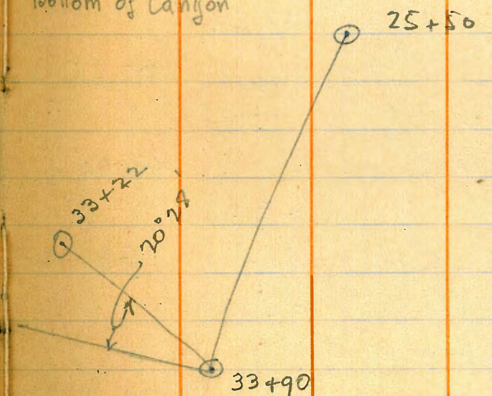
STA.	Dist	Defl. ∠	V.A.	Diff. El.	Elev.
25+35					
	279.00	70° 19'			
22+56			6° 48' -		

Change from Sta. 17+57 of Traverse on Page 1

Sta.	Dist.	Defl. ∠	V.A.	Diff. Elev.	Elev.
36+18					97.08
	81.00	0°-00'	+0°05'	+0.14	
35+37					71.88
	147.00	0°-00'	-9°-58	-25.06	
33+90					96.94 ✓
	68.00	4°13'-L ✓	-3°44'	-4.42	
33+22					101.36 ✓
	144.00	27°46'-L ✓	+0°44'	+1.84	
31+78					99.52 ✓
	64.00	304°04'-L ✓	-0°15'	-0.30	
31+14					99.82 ✓
	282.00	28°-11' R ✓	5°59'-	-29.24	
28+32					129.06
	92.0	31°31' -L ✓	4°12' +	+6.79	
27+40					122.27
	190	70°-53'-L ✓	1°09'+	+3.87	
25+50					118.40
	290. ✓	75°19R	6°4'	-30.47	
22+60					148.87
	185.	3° 7'L	9°30	-30.12	
20+75					178.99
	240	21°49'-R ✓		-8.30	
18+35					187.29
	78.00	59°41'-L ✓	0°04'-	-0.12'	
17+57					187.41

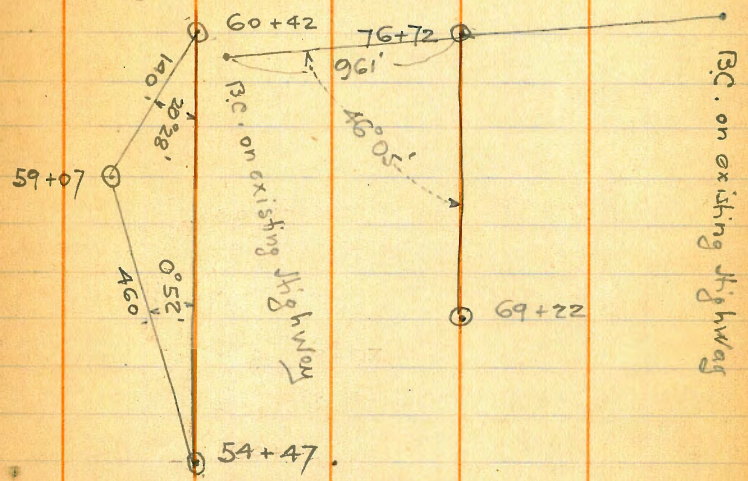
Change from 25+50 on.

Sta.	Dist.	Defl. ∡	V.A.	Diff. El.	Elev.	
38+68 ✓					43.13	≐ 44+64 Page 5
	560'	71°10' incl.	1°33'-	-14.95		
35+36 ✓					14.40	Bottom of Canyon
	228'		11°15'-	-43.68	5.69	
33+08 ✓					58.08	
	152'	15°-18-R	7°12'-	-18.89'		
31+56 ✓					77.18	
	50'	10°09'-R		-3.67'		
31+06 ✓					80.98	
	108	7°49'-R		-8.43'		
29+98 ✓					89.83	
	78	20°28' (incl.) ✓		-7.06'		
33+90 = 29+20 ✓					96.94	on Traverse on Page 3. Backsight on 33+22
25+50						



Continued from Page 3

Sta.	Dist	Defl. ∡	V.A.	Diff. El.	Elev.	
76+92					-35.19	℄ Road existing Pavement
	750			+6.53		
69+42		P.O.T.	0°30' +		-41.72	
	420			-9.28		
65+22		P.O.T.	1°16' -		-32.44	
	480'			-39.21		
59+07					6.18	
	460'			-16.83		
60+42		3°19'-L	4°42' -		6.77	
	595'	0°52'-L	2°06' -	-16.24		
54+47		5°15'-R	1°35' -		23.01	
	204'			-17.64		
52+43		P.O.T.	2°05' -		40.65	
	490'			—		
47+53		47°26R	Level		40.65	
	289'			-3.25		
44+64		69°51'-L	0°40' -		43.90	= 38+68 Page 4
	310			-23.71		
41+54		9°26'-L	4°25' -		67.61	
	236			+0.68		
39+18		43°10'-R	0°10' +		66.93	
	300			-30.15		
36+18		109°17'-R	-5°49'		97.08	



Change from Sta. 25+50 on

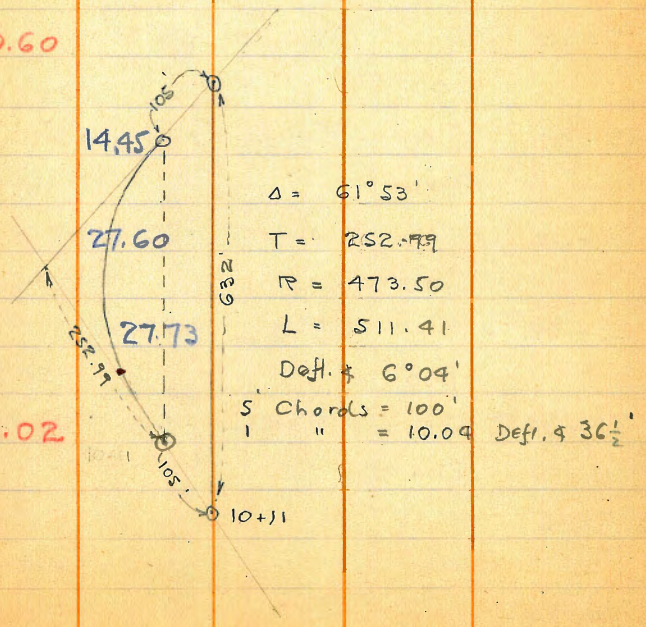
STA	DIST	DEFL Δ	VA	DIFF. EL	ELEV
38+26					42.93
	480			+ 9.07	
33+46		48°11L	4°5'		33.86
	210			-55.59	
31+36		30°30'-L ✓	15°59'-		89.45
	89			-5.74	
30+47		1°59R	✓		95.19
	130			-8.45	
29+17		37°16R	✓		103.64
	109			-7.02	
28+08		19°7L	✓		110.66
	94			-5.64'	
27+14		7°28'-L	✓		116.30
	164'			-2.10'	
25+50		66°30'-L			118.40

T.P.		+	H.I.	−	Elev.
Sta.					
TP	TP				248.40
		.40	248.80		
	TP			12.65 ✓	246.15
		3.10 ✓	249.20		
10+84				5.4	
10+94.17				5.6	
11+44.18	TP	~~4.00~~		4.00	~~253.20~~ 243.20
		12.10 ✓	257.30		
11+94.19	TP			2.60	254.70
		3.70	258.40		
12+19				11.40	
12+44.20		12.60			
		11.10			

Road Location # 2 at Torrey Pines.

JAEGER
Clavert
Bailey
} Febr. 24/28

STA.	Dist.	Defl. ∠	V.A.	Diff. El.	El.	Grade 7%	Cut	Fill
18 + 34.04				✓	255.59	221.27	34.32	
	108	Tangent	30' Canyon					
17 + 26.04				✓	251.31	228.83	22.48	
	105	Tangent	30' Canyon					
16 + 26.04 EC.		6°04'		✓	237.84	236.18	1.66	×
	100							
15 + 26.04		6°04'		✓	244.16	243.18	0.98	
	100							
14 + 26.04		6°04'		✓	240.77	250.18		9.41
	100							
13 + 26.04		6°04'	✓	✓	267.78	257.18	10.60	
	100							
12 + 26.04		6°04'	✓	✓	249.73	264.18		14.45
	100							
11 + 26.04		0°36½'		✓	243.58	271.18		27.60
	10.04							
11 + 16 B.C. 10.04				✓	244.15	271.88		27.73
	105							
10 + 11 105				✓	291.25	279.23	12.02	
	190							
8 + 21				✓	338.67			
	159							
6 + 62					333.15			



Δ = 61°53'
T = 252.99
R = 473.50
L = 511.41
Defl. ∠ 6°04'
5' Chords = 100'
1 " = 10.04 Defl. ∠ 36½'

STA.	Dist.	Defl. ∠	V.A.	Diff. El.	Elev.	Grade 7%	Cut	Fill
31+32				✓	86.37	130.41 ✓		44.04
	100			-15.34				
30+32	E.C.	4°-39'-L	-8°-56'	✓	92.83	137.41 ✓		44.58
	100 ✓			-18.30				
29+32	×	4°-39'-L	-10.44'	✓	100.79	144.41 ✓		43.62
	100 ✓			-23.47				
28+32	×	4°-39'-L	-14°-00'	✓	115.81	151.41 ✓		35.60
	100 ✓			-31.92				
27+32	×	4°39'-L	-19°50'	✓	147.73	158.41 ✓		10.68
	100 ✓			-25.80				
26+32		Tangent	-15°32'	✓	173.53	165.41 ✓	8.12	
	100 ✓			-19.00				
25+32	×	9°-18'-L	-11°10'	✓	192.53	172.41 ✓	20.12	
	100 ✓	Tangent		-13.35				
24+32		Tangent	-7°45'	✓	205.88	179.41 ✓	26.47	
	100 ✓			-4.65				
23+32.00 ✓	×	9°-18'-L	-2°40'	✓	210.53	186.41 ✓	24.12	
	200'			-20.22				
21+32.00	P.C.	9°-18'-L	-5°50'	✓	230.75	200.41	30.34	
	204.96							
19+27.04				✓	238.39	214.76	23.63	
	93		-4°45'	-17.20				
18+34.04			-10°30	✓	255.59	221.27	34.32	

Sta.	Dist.	Defl. ∠	V.A.	Diff El.	Elev.	Grade 7%	Cut	Fill
47+04				✓	36.59			
	100			-30.84				
46+04			-4°26'	✓	40.19			
	100			-27.24				
45+04			-5°14'	✓	56.01			
	100			-11.42 ✓				
44+04			-5°36'	✓	57.95			
	100'			-9.48 ✓				
43+04			-5°28'	✓	67.43	48.37		
	124			-1.78				
41+80				✓	69.21	57.05		
	681			-23.76				
37+99			-2°00'	✓	79.68	83.72		
	166'			-6.13				
36+33				✓	85.81	95.34		
	134'			-7.17				
34+99 ✓				✓	92.98 ✓	104.72 ✓		1.74
	67'			+6.61				
34+32			+1°02'	✓	86.37	109.41 ✓		23.04
	100			~				
33+32			0°00'	✓	81.71	116.41 ✓		34.70
	100'			-4.66				
32+32'			-1°20'	✓	80.39	123.41 ✓		43.02
	100'			-5.98				
31+32			-3°26'	✓	86.37	130.41 ✓		44.04

Sta.	Dist.	Defl. ∠	V.A.	Diff. El.	Elev.	El. 7% Sr.	Cut	Fill			
57 + 24	P.I.			✓	21.14						
	272.59	Tangent									
54 + 51.41	B.C.			✓	14.08						
	47.41			- 5.49							
54 + 04			- 1°04'	✓	7.5✓	End of	Slough	El. Water Level			
	250			- 12.05						3 pm.	28th Febr.
51 + 96				✓	7.52	Beg. "	Slough	" "	"		
	42'										
51 + 54	Δ		- 2°45'	✓	19.57						
	50'			- 47.86							
51 + 04			- 3°14'	✓	22.39						
	100			- 45.04							
50 + 04			- 3°14'	✓	22.77						
	100			- 44.66							
49 + 04			- 3°46'	✓	23.63						
	100			- 43.80							
48 + 04			- 4°12'	✓	28.33						
	100			- 39.10							
47 + 04			- 4°30	✓	36.59						

STA.	Dist.	Defl. ∠	V.A.	Diff. El.	Elev.	El. Grade	Cut	Fill		
	Tangent									
59+62 23	EC.	0°31'-R	—		21.14					
	10.8 ✓									
59+51 41		0°31'-R	—		21.76					
	100'									
58+51 41		4°47'-R	—		21.76					
	100'									
57+51 41		4°47'-R	+1°06'		14.08				R =	600'
	100'								Δ =	48°52'
56+51 41		4°47'-R	0.00'		10.8 ✓				T =	272.59'
	100'									
55+51 41		4°41'-R	-0°56'		14.37					
	100'									
54+51 41	B.C.	4°47'-R	+0°10'		14.08					

Change from Sta. 17+26 04

Sta	Dist.	Defl. ∠	V.A.	Diff. El.	Elev.	El. Grad 7%	Cut	Fill
45+17 99					56.07			
	324			-22.90				
41+93 94		9°24'-L	-4°04'		78.97	56.49	22.48	
	500			-34.50				
36+93 94		Tangent			113.47	91.42	22.05	
	200			-11.00				
34+93 94		9°-28'-R			123.47	105.42	18.05	
	300			-8.37				
31+93 94	P.R.C.	14°-29'-R	-1°36'		131.84	126.42	5.42	
	360			-16.5				
28+33 94		17°28'-L	-2°38'		148.36	151.62		3.26
	354.44			-45.49				
24+79 50		17°12'-L	-7°19'		193.85	176.40	17.45	
	282.50			-44.96				
21+97		13°37'-L			238.81	196.21	42.60	
	73'			-13.4				
21+24 04	P.C.	3°29'-L			252.21	201.32	50.89	
	48			-6.10				
20+76 04	Tangent				258.31	204.68	53.63	
	230			-5.00				
18+46 04	E.C.	11°03'-L			263.31	220.78	42.53	
	120'			+12.00				45' Bottom of Caisson
17+26 04	P.C.	5°44'-L	+5°46'		251.31	228.83	22.48	See Page 20

STA.	Dist.	Defl.∠	V.A.	Diff. El.	Elev.	% El. Grade	Cut	Fill
5582.94					20.80			
	580			-3.02				
5002.94		Tangent	-0°18'		23.82			
	485			-32.25				
45+17.94		Tangent	-3°49'					

Change from Sta. 21+32 P.C. Page 21
600' R. Curve to Left.

Sta.		Elev.
22+67		214.60
26+12		175.65
29+72		111.15
31+68	P.R.C.	115.16

"A" Line

Location Survey for Torrey Pines Road.

~ Definite Location ~

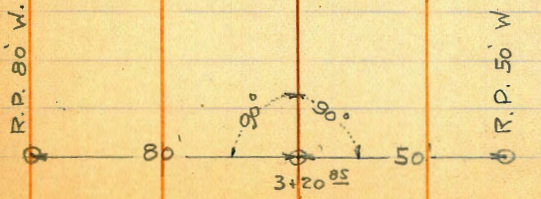
March 3rd 1928

JAEGER
BAILEY
CLAVERT

9+94 15		B.C.
	103.13	
8+91 02		E.C.
		7
8+60 17	0°53'-L	
		6
8+10 19	8°36'-L	
		5
7+60 11	7°-10'-L	
		4
7+10 08	5°44'-L	
		3
6+60 05	4°-18'-L	
		2
6+10 03	2°52'-L	
		1
5+59 99	1°26'-L	B.C.
5+00		P.O.T.
3+20 85		P.O.T.
0+00		

R = 1000'
Δ = 18°58' - L
T = 167.04'
L = 331.03'

Defl. 4 1°26' @ Short L = 50.03 @ Chords @ 50'
" " 0°53' 1 " L 30.85" 1 " 30.84'



E.C. of Curve of Existing Pavement

		12
15+44 26	2°23'16" R	
		11
14+94 25	2°23'16" R	
		10
14+44 24	2°23'16" R	
		9
13+94 23	2°23'16" R	
		8
13+44 22	2°23'16" R	
		7
12+94 21	2°23'16" R	
		6
12+44 20	2°23'16" R	
		5
11+94 19	2°23'16" R	
		4
11+44 18	2°23'16" R	
		3
10+94 17	2°23'16" R	
		2
10+44 16	2°23'16" R	
		1
9+94 15	2°23'16" R	B.C.

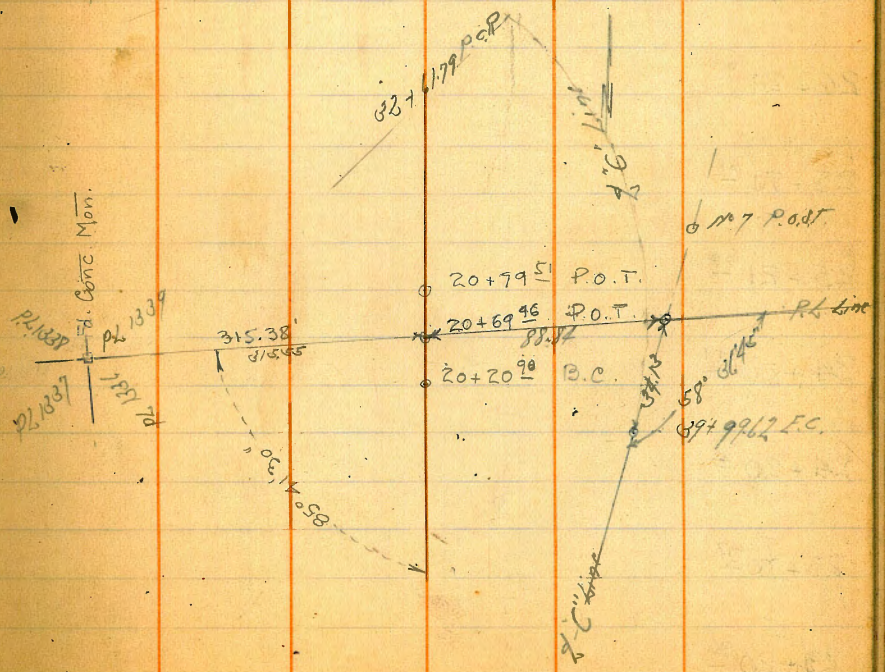
Δ = 59°00' - R
R = 600'
T = 339.46
L = 617.85

Defl. 2°23'-16" for 12 Short L^s = 50.01 Chord 50'
" 0°50'48" " 1 " L^s = 17.73 " 17.74'

		6
22+70	95	
		5
22+20	94	
		4
21+70	93	
		3
21+20	92	
		2
20+70	91	
		1
20+20	90	B.C.
25+68	45	P.I.
23+78	09	P.O.T
20+79	51	P.O.T.
17+80	58	P.O.T.
16+78	62	P.O.T.
16+12	00	E.C.
		13
15+94	27	0°50'48"

R = 600'
Δ = 84°46' - L
T = 547.55
L = 887.67

Defl.'s 2°23'16" for 17 Short L's @ 50.01' Chord 50'
" 1°47'28" " 1 " L's @ 37.51' " 37.50'



29	08.58	
	37.51	18
28 + 71 $\frac{07}{}$		
		17
28 + 21 $\frac{06}{}$		
		16
27 + 71 $\frac{05}{}$		
		15
27 + 21 $\frac{04}{}$		
		14
26 + 71 $\frac{03}{}$		
		13
26 + 21 $\frac{02}{}$		
		12
25 + 71 $\frac{01}{}$		
		11
25 + 21 $\frac{00}{}$		
		10
24 + 70 $\frac{99}{}$		
		9
24 + 20 $\frac{98}{}$		
		8
23 + 70 $\frac{97}{}$		
		7
23 + 20 $\frac{96}{}$		

		⑧
32 + 77	15	
		⑦
32 + 27	14	
		⑥
31 + 77	13	
		⑤
31 + 27	12	
		④
30 + 77	11	
		③
30 + 27	10	
		②
29 + 77	09	
	50.01	①
29 + 27	08	B.C.
31 + 46	30	P.I.
32 + 09	80	P.O.T.
	296	
29 + 13	80	P.O.T.
	5.23'	
29 + 08	57	E.C.

Δ = 30° 39' - R Δ/2 = 15° 19' 30"
R = 800'
T = 219.22
L = 427.95

Defl. ⅄ 1° 47' 27" for 8 short L^s @ 50.01 Chord 50'
" 0° 59' 54" " 1 " L^s 27.88 " 27.87

	50.03	1	
41 + 48 $\frac{55}{}$		B.C.	
	242.65		
39 + 05 $\frac{90}{}$		E.C.	
	38.12	5	
38 + 67 $\frac{78}{}$			
	50.03	4	
38 + 17 $\frac{25}{}$			
	✓	3	
37 + 67 $\frac{\text{Fv}}{}$			
	✓	2	
37 + 17 $\frac{69}{}$			
	50.03	1	
36 + 67 $\frac{66}{}$		B.C.	
42 + 84 $\frac{35}{}$		P.O.T.	
	497.00		
37 + 87. $\frac{35}{}$		P.O.T.	Made P.I.
	218.91		
35 + 68 $\frac{44}{}$		P.O.T.	
33 + 55 $\frac{03}{}$		E.C.	
	27.88		
33 + 27 $\frac{16}{}$			

$R = 1000'$

$\Delta = 13°39' - R$ $\quad \Delta/2 = 6°49'30'$

$T = 119.69$

$L = 238.24'$

Defl. Δ 1°26' for 4 Short L^S @ 50.03' Chord 50'

" Δ 1°5'30" " 1 " L^S @ 38.12' " 38.10'

$= 32 + 86 \frac{64}{}$ "B" Line

	✓	7
57+28 70		
	✓	6
56+78 69		
	✓	5
56+28 68		
	✓	4
55+78 67		
	✓	3
55+28 66		
	✓	2
54+78 65		
	50.01	1
54+28 64		P.C.
	1041.85	
43+86 79		E.C.
	38.12	5
43+48 67		
	50.03	4
42+98 64		
	✓	3
42+48 61		
	✓	2
41+98 58		
	✓	

R = 600'

Δ = 42°45' - R Δ/2 = 21°22'30"

T = 234.84

L = 447.68

Defl. @ 2°23'16" for 8 Short L^s = 50.01' Chord 50'

" @ 2°16'22" " 1 " L^s = 47.60' " 47.59'

R = 1000'

Δ = 13°39' - L' Δ/2 = 6°49'30"

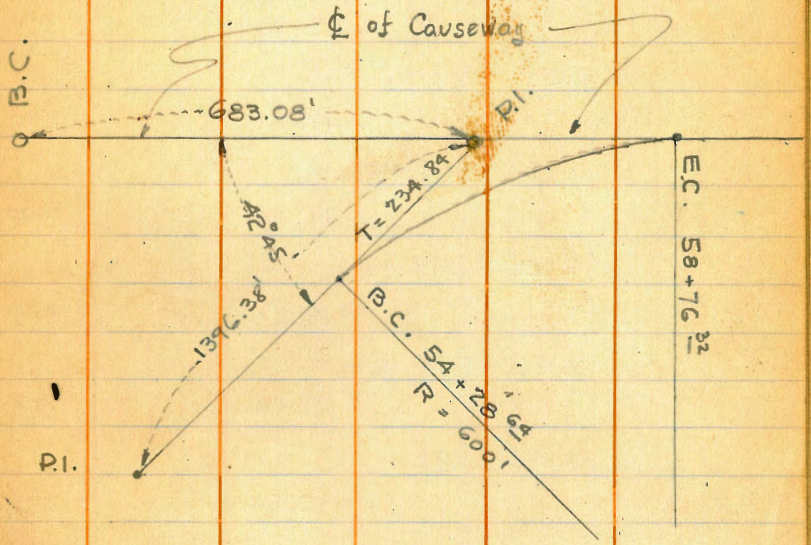
T = 119.69

L = 238.24'

Defl. @ 1°26' for 4 Short L^s @ 50.03' Chord 50'

" @ 1°05'30" " 1 " L^s @ 38.12' " 38.10'

Beginning of Torrey Pines Grade going South.



58 + 76 32/		E.C.
	47.60	9
58 + 28 72/		
	50.01	8
57 + 78 71/		

B.M^s along Alignment of Proposed Torrey Pines Road. See Page 28

	+	H.I.	−	Elev.
	5 5		∿ 5 3	
	3.22			350.00
T.P.		353.22	10.46	342.76
	4.17	346.93		
T.P.			12.70	334.23
	1.64	335.87		
T.P.			12.60	323.27
	0.76	324.03		
T.P.			13.00	311.03
	0.33	311.36		
T.P.			12.11	299.25
	5.72	304.97		
T.P.			11.14	293.83
	4.63	298.46		
T.P.			12.80	285.66
	8.46	294.12		
T.P.			12.44	281.68
	0.43	282.11		
T.P.			12.59	269.52
	0.75	270.27		
T.P.			12.91	257.36
	0.29	257.65		
T.P.			12.04	245.61
	0.07	245.68		
T.P.	30.47		12.33	233.35
	149.14			

Mar. 20th 1928

JAEGER
Bailey
Clavert

B.M. B.C. of Existing Curve of Highway

#1. B.M. on South Brink of Canyon

#2 B.M. on North Brink of Canyon

	+	H.I.	−	Elev.	
T.P.				233.35	
	0.38	233.73			
T.P.			12.20	221.53	
	0.16	221.69			
T.P.			12.60	209.09	
	0.49	209.58			
T.P.			12.88	196.70	
	0.59	197.29			
T.P.			11.96	185.33	
	0.25	185.58			
T.P.			12.01	173.57	
	0.17	173.74			
T.P.			12.87	160.87	
	0.62	161.49			
T.P.			11.89	149.60	#3 B.M. on East Edge of Trail leading into Canyon.
	1.07	150.67			
T.P.			11.46	139.21	#4 B.M.
	1.24	140.45			
T.P.			11.59	128.86	
	6.41	135.27			
T.P.			12.79	122.48	
	0.05	122.53			
T.P.			12.54	109.99	
	0.81	110.80			

	+	H.I.	−	Elev.
		110.80		
T.P.			12.52	98.28
	1.92	100.20		
T.P.			12.57	87.63
	0.17	87.80		
T.P.			10.02	77.78
	5.34	83.12		
T.P.			12.28	70.84
	1.69	72.53		
T.P.			12.77	59.76
	1.87	61.63		
T.P.			12.95	48.68
	0.62	49.30		
T.P.			11.67	37.63
	2.39	40.02		
T.P.			12.92	27.10
	0.58	27.68		
T.P.			9.89	17.79
	2.89	20.68		
			4.59	16.09
			4.49	16.19

	350.00	112.18
	17.47	134.79
B.M.# 5 on Trail	12.24	147.12
	30.47	394.09
	410.18	
	394.09	
	16.09	

B.M.# 7 on South End of Slough. 16.85 Correct

15.13 Correct

E.C. of Curve joining Causeway Sta. 58+76 32

P.I. " Causeway 15.23 Correct

Mar. 21st

JAEGER
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Clarert

Check on Levels going over existing Highway

	+	H.I.	−		Elev.
					16.19.
	4.78	20.97			
T.P.			-0.05		20.92
	11.77	32.69			
T.P.			0.38		32.31
	13.06	45.37			
T.P.			0.11		45.26
	12.29	57.55			
T.P.			0.23		57.32
	11.87	69.19			
T.P.			0.51		68.68
	12.50	81.18			
T.P.			0.58		80.60
	12.76	93.36			
T.P.			0.41		92.95
	11.90	104.85			
T.P.			0.10		104.75
	12.40	117.15			
T.P.			0.03		117.12
	13.11	130.23			
T.P.			0.06		130.17
	12.31	142.48			
T.P.			0.09		142.39
			11.44		131.04

P.I. of Curve on Causeway

	+	H.I	−		Elev.	
					131.04	
	12.94	143.98				
			3.72		140.26	B.M. 139.21
T.P.					142.39	
	12.37	154.76				
T.P.			0.06		154.70	
	12.27	166.97				
T.P.			0.29		166.68	
	12.24	178.92				
T.P.			0.35		178.57	
	12.45	191.02				
T.P.			0.16		190.86	
	12.05	202.91				
T.P.			0.02		202.89	
	12.11	215.00				
T.P.			0.42		214.58	
	11.99	226.57				
T.P.			0.43		226.14	
	12.46	238.60				
T.P.			0.22		238.38	
	12.49	250.87				
T.P.			0.01		250.86	
	12.50	263.36				
			0.29		263.07	

	+	H.I.	−		Elev.				
					263.07				
	12.18	275.25							
T.P.			0.45		274.80				
	12.04	286.84							
T.P.			0.12		286.72				
	13.07	299.79							
T.P.			0.27		299.52				
	12.56	312.08							
T.P.			0.51		311.57				
	12.36	323.93							
T.P.			1.24		322.69				
	13.12	335.81							
T.P.			0.23		335.58				
	8.10	343.68							
T.P.			1.99		341.69				
	11.31	353.00							
T.P.			4.33		348.67				
	6.00	354.67							
T.P.			3.50		351.17	350.00	B.M.	P.C. of Curve on Highway	

	Correction +	Levels H.I.	—	Elev.			
				350.00			
	1.74	351.74					
T.P.			10.11	341.63			
	0.47	342.10					
T.P.			12.92	329.18			
	1.36	330.54					
T.P.			12.76	317.78			
	0.04	317.82					
T.P.			12.63	305.19			
	0.11	305.30					
T.P.			11.44	293.86	293.83	B.M. # 1	✓
	4.55	298.41					
T.P.			12.74	285.67	285.66	B.M. # 2	✓
	8.40	294.07					
T.P.			13.09	280.98			
	0.06	281.04					
T.P.			12.80	268.24			
	0.23	268.47					
T.P.			12.98	255.49			
	0.42	255.91					
T.P.			13.06	242.85			
	0.20	243.05					
T.P.			11.84	231.21			
	0.23	231.44					
T.P.			12.33	219.11			

	+	H. I.	−	Elev.						
	0.31	219.42								
T.P.			13.07	206.35						
	0.03	206.38								
T.P.			12.96	193.42						
	0.20	193.62								
T.P.			12.70	180.92						
	0.10	181.02								
T.P.			12.02	169.00						
	0.11	169.11								
T.P.			12.96	156.15						
	0.59	156.74								
T.P.			7.16	149.58	149.60	B.M. # 3				
	0.02	149.60								
T.P.			12.61	136.99						
	0.81	137.80								
T.P.			12.88	124.92						
	0.19	125.11								
T.P.			12.43	112.68						
	0.65	113.33								
T.P.			13.23	100.10						
	3.04	103.14								
T.P.			12.89	90.25						
	1.58	91.83								
			12.38	79.45						

	+	H.I.	−	Elev.				
				79.45				
	3.13	82.58						
T.P.			4.80	77.78	77.78	BM # 5	✓	
	4.55	82.33					Check Levels on Rd. See Page 38	
T.P.			12.73	69.60 ✓			Diff. El.	334.98 feet
	0.42	70.02					" "	334.77 "
T.P.			10.24	59.78	59.76	BM. # 6	✓	
	7.31	67.09						
T.P.			12.50	54.59				
	1.14	55.73						
T.D.			11.92	43.81				
	0.79	44.60						
T.P.			12.78	31.82				
	0.08	31.90						
T.P.			11.88	20.02				
	3.33	23.35						
T.P.			6.50	16.85	17.79	BM. # 7	Changed to 16.85 Correct. ✓	
			8.12	15.23	16.19	P.I. of Causeway	Changed to 15.23 Correct ✓	

Final Levels on "A" Line See Page 28 — Note:— Subtract 3.57 for correct Elev. (See Page 10 Book-1291) — Mar. 23rd 1928 — Jaeger, Bailey, Clavert

Sta.		+	H.I.	−	Elev.	6.5% Grade Elev.	Cut	Fill	7% Grade	Cut	Fill
0+00					350						
		3.68	353.08								
1+01	Edge of Pavement			4.50	348.58	348.58	~		348.58	~	
1+57				4.20	348.88	344.87	4.01		344.66	4.22	
2+02				6.60	346.48	341.95	4.53		341.51	4.97	
2+86				5.10	347.98	336.49	9.49		335.63	12.35	
3+20.85				5.15	347.93	334.28	13.65		333.18	16.75	
3+30				4.10	348.98	333.70	15.28		332.55	16.43	
4+00				5.80	347.28	329.15	18.13		327.65	19.63	
	T.P.			7.76	345.32						
		2.00	347.32								
+50				1.8	345.52	325.90	19.62		324.15	21.37	
5+00				3.8	343.52	322.65	20.87		320.65	22.87	
+59.99				6.4	340.92	318.75	22.17		316.45	24.47	
6+10.02				9.1	338.22	315.50	22.72		312.95	25.27	
	T.P.			11.92	335.40						
		7.85	343.25								
6+60				10.50	332.75	312.25	20.50		309.45	23.30	
6+66				11.6	331.65	311.85	19.80		309.03	22.62	
+72				10.0	333.25	311.47	21.78		308.61	24.64	
7+10.08				8.35	334.90	309.00	25.90		305.95	28.95	
+60.11				6.70	336.55	305.75	30.80		302.45	34.10	
8+10.14				3.15	340.10	302.50	37.60		298.95	41.15	
8+19				3.35	339.90	301.91	37.99		298.32	41.58	

Sta		+	H.I.	−	Elev.	Elev. 6.5% Grade	Cut	Fill	7% Grade	Cut	Fill
8+28				7.70	335.55	301.33	34.22		297.69	37.86	
	T.P.			12.34	330.91						
		0.56	331.47								
8+60 17				2.90	328.57	299.25	29.32		295.45	33.12	
	T.P.			12.63	318.84						
		0.24	319.08								
+91 ON				2.35	316.73	297.23	19.50		293.28	23.45	
	T.P.			13.10	305.98						
		0.37	306.35								
				3.80	302.55						
				12.65	293.70	293.83	B.M. #1				
			306.48 ✓								
	T.P.			12.75	293.73						
		1.43	295.16								
9+94 15 BC.				2.65	292.51 ✓	290.54	1.97		286.07	6.44	
10+00				7.00	288.16	290.15		1.99	285.65	2.51	
+18	T.P.			12.45	282.71	288.98		6.27	284.39		1.68
		1.29	284.00								
	T.P.			12.28	271.72						
		0.12	271.84								
+44 16				7.00	264.84 ✓	287.29		22.45	282.57		17.73
	T.P.			12.59	259.25						
		0.37	259.62								
	T.P.			11.22	248.40						

Note - Subtract.

STA.		+	H.I.	−	Elev.	Elev. 6.5% Grade	Cut	Fill	7% Grade	Cut	Fill
					248.40						
		0.40	248.80								
	T.P.			12.65	236.15						
		3.10	239.25								
10+84 00				5.40	233.85	284.69		50.84	279.77		45.92
10+94 17				5.60	233.65 ✓	284.04		50.39	279.07		45.42
11+44 18	T.P.			4.00	235.25 ✓	280.79		45.54	275.57		40.32
		12.10	247.35								
11+94 19	T.P.			2.60	244.75 ✓	277.54		32.79	272.07		27.32
		3.70	248.45								
12+19				11.40	237.05	275.91		38.86	270.32		33.27
		14.73	251.78	12.60							
12+44 20					239.18 ✓	274.29		35.11	268.57		29.32
		4.88	253.88								
12+80 00				3.20	249.68	271.95		22.27	266.05		16.37
12+94 21	T.P.	Hand Level		8.90	243.98 ✓	271.04		27.06	265.07		21.09
	T.P.			12.41	240.47						
		0.65	244.63								
13+20	T.P.			12.80	231.83	269.35		37.52	263.25		31.42
		1.30	233.13								
13+44 22				2.60	230.53 ✓	267.79		37.26	261.57		31.04
+94 23				5.50	227.63 ✓	264.54		36.91	258.07		30.44
14+15				5.00	227.13	263.17		36.04	256.60		29.47
+24				13.30	219.83	262.59		42.76	255.97		36.14
+44 24	T.P.			3.40	229.73 ✓	261.29		31.56	254.57		24.84

Sta.		+	H.I.	−	Elev.
		13.00	242.73		
14+94 25				2.50	240.23 ✓
	T.P.				240.47
		8.89	249.36		
				1.61	247.75
					240.47
		0.10	240.57		
15+3 N				6.70	233.87
15+44 26				5.60	234.97 ✓
+69				3.70	236.87
15+94 27	T.P.			13.00	227.57 ✓
		1.10	228.67		
16+12 P.C.				12.20	216.47 ✓
16+30				11.40	217.27
	T.P.			0.00	228.67
		12.50	241.17		
	T.P.			0.30	240.87
		12.60	253.47		
	T.P.			0.20	253.27
		5.70	258.97		
16+78 6 N				5.00	253.97 ✓
					247.75
		1.30	249.05		
16+98				5.30	243.75
	T.P.			13.00	236.05

Elev. 6.5% Grade	Cut	Fill	7% Grade	Cut	Fill
			251.07		10.84
Instr.					
B.M.					
Hand Level.					
			248.41		14.54
			247.57		12.60
			245.82		8.95
			244.07		16.50
			242.81		26.34
			241.55		24.28
			238.12	15.85	
B.M. Hand Level					
			236.79	6.96	

Sta.		+	H.I.	−	Elev.	Elev. 6.5% Grade	Cut	Fill	7% Grade	Cut	Fill
		0.70	236.75								
17+78				9.30	227.45				234.69		7.24
					253.86	B.M.	253.86				
		1.65	255.51								
17+60				5.60	249.91				232.45	17.46	
17+80 58			Hand Level		256.3				230.98	25.34	
18+59 58				10.55	244.96				225.45	19.51	
	T.P.			12.12	243.39	B.M. Instrument					
					243.21	Hand Level					
		0.50	243.71								
18+89 58	T.P.			6.30	237.41				223.35	14.06	
		0.20	237.61								
18+95 58				9.20	228.41				222.93	5.48	
	T.P.			12.50	225.11						
		0.90	226.01								
19+10 58				7.10	218.91				221.88		2.97
	T.P.			12.10	213.91						
		0.20	214.11								
19+25 58	T.P.			12.20	201.91				220.83		18.92
		1.50	203.41								
19+38 58				8.50	194.91				219.92		25.01
19+53 58	T.P.			3.90	199.51				218.87		19.36
		13.30	212.81								
	T.P.			0.20	212.61						
		12.00	224.61								

STA.		+	H.I.	−	Elev.	Elev. 6.5% Grade	Cut	Fill	7% Grade	Cut	Fill
			224.61								
19+63 58				10.80	213.81				218.17		4.36
	T.P.			0.80	223.81						
		8.20	232.01		229.01						
19+88 58				3.00					216.47	12.59	
20+05				17.17	214.84				215.30		0.46
20+20 90 BC.				10.00	222.01				214.18	7.83	
20+23 90				6.00	226.01				213.98	12.03	
20+70 19	T.P.			2.40	229.61				210.75	18.86	
					243.39	B.M.					
		1.10	244.49								
	T.P.			11.90	232.59						
		3.20	235.79								
21+20 92				7.20	228.59				207.18	21.41	
	T.P.			11.90	223.89						
		5.30	229.19								
+70 92				8.20	220.99				203.68	17.31	
22+20 94	T.P.			10.80	218.39				200.18	18.21	
		2.20	220.59								
22+70 95				7.60	212.99				196.68	16.31	
23+20 96	T.P.			10.80	209.79				193.18	16.61	
		0.50	210.29								
+70 97				8.00	202.29				189.68	12.61	
	T.P.			11.90	198.39						

STA.		+	H.I.	−	Elev.	Elev, 6.5% Grade	Cut	Fill	7% Grade	Cut	Fill
		0.30	198.69								
24+20 98				5.00	193.69 ✓				186.18	7.51	
	T.P.			10.20	188.49						
		0.10	188.59								
24+70 99				6.10	182.49 ✓				182.68		0.19
+90	T.P.			13.00	175.59				181.35		5.76
		0.30	175.89								
25+21				8.40	167.49				179.18		11.69
	T.P.			12.50	163.39						
		0.10	163.49								
	T.P.			12.40	151.09						
		4.90	155.99								
+71 01				8.60	147.39				175.68		28.29
+85				9.20	146.79				174.70		27.91
26+06				4.10	151.89				173.72		21.83
				5.20	150.79	BM. 149.60 ✓					
		4.80	154.40								
+21 02				6.7	147.70				172.25		24.55
	T.P.			11.90	142.50						
		0.60	143.10								
+71 03				2.30	140.80				168.75		27.95
	T.P.			12.70	130.40						
		1.30	131.70								
27+21 04				7.70	124.00				165.25		41.25

Sta.		+	H.I.	−	Elev.	Elev. 6.5% Grade	Cut	Fill	7% Grade	Cut	Fill
27+36				15.80	115.90				164.20		48.30
+51	T.P.			11.40	120.30				163.15		42.85
		0.90	121.20				5.23				
							13.28				
+57				11.60	109.60				162.73		53.13
+71.05				12.20	109.00				161.75		52.75
+79				5.90	115.30				161.19		45.89
+95	T.P.			1.50	119.70				160.07		40.37
		3.60	123.30								
28+21.06				4.70	118.60				158.25		39.65
+55				4.20	119.10				155.87		36.77
+71.07	T.P.			0.00	123.30				154.75		31.45
		12.10	135.40								
	T.P.			1.40	134.00						
		5.50	139.50								
29+08.59	E.C.			3.90	135.60				152.05		16.45
+13.80				2.50	137.00				151.68		14.68
29+27.08	B.C.			3.10	136.40				150.75		14.35
	T.P.			1.90	137.60						
		10.40	148.00								
				8.30	139.70	B.M.# 4	139.21				
		0.10	139.31								
+77.09	T.P.			12.00	127.31 ✓						
		1.80	129.11								
30+27.10				4.3	124.81						
+77.11	T.P.			A.C	124.51						

Sta.		+	H.I.	−	Elev.	% Grade	Cut	Fill
		4.1	128.61					
31+27 12				5.9	122.71			
+77 13				6.0	122.61			
32+27 14				0.33	128.28			
		6.3	134.58					
+77 15				6.2	128.38			
		142.46	(Instr.)	2.7	131.88			
				11.49	130.97			
			142.46					
1	T.P.			13.05	129.45			
		2.10	131.51					
33+27 16				6.30	125.21			
+55 03	T.P.			8.70	122.81			
		5.2	128.01					
34+00				7.9	120.11			
+50	T.P.			9.41	118.60			
		10.41	129.01					
35+00				8.00	121.01			
+50				8.80	120.21			
+68 44	T.P.			9.10	119.91			
		4.50	124.41					
36+00				4.50	119.91			
+50				5.10	119.31			
+67 66	B.C. T.P.			5.20	119.21			

Sta.		+	H.I.	−	Elev.
		2.90	122.11		
37+17 69				5.5	116.61
+67 72				9.4	112.71
	T.P.			13.0	109.11
		1.53	110.64		
38+17 75				2.60	108.04
+67 78				6.30	105.34
39+05 90	T.P.			9.00	101.64
		2.50	104.14		
+50				7.8	96.34
40+00	T.P.			11.68	92.46
		4.30	96.76		
+50				7.80	88.96
41+00	T.P.			10.60	86.16
		4.10	90.26		
+48 55				7.00	83.26
	T.P.			9.10	81.16
		3.20	84.36		
+98 58				4.80	79.56
42+48 61	T.P.			8.20	76.16
		5.82	81.98		
				3.48	78.50
		3.48	81.26		
	T.P.			7.46	73.80

77.78 BM.

	7% Grade	Cut	Fill

Sta.		+	H.I.	−	Elev.	
		3.50	77.30			
42+98 69				5.4	71.99	
43+48 67	T.P.			10.4	66.80	
		4.40	71.20			
+86 79	T.P.			9.5	61.70	
		2.20	63.90			
44+00				3.60	60.30	
+50	T.P.			7.40	56.50	
		4.30	60.80			
45+00				6.30	54.50	
+50	T.P.			7.60	53.20	
		11.60	64.80			
				5.80	59.00	BM. 59.76
		1.00	60.76			
46+00	T.P.			11.50	49.26	
		1.30	50.56			
+50				5.60	44.96	
	T.P.			13.00	37.56	
		7.20	44.76			
47+00				5.90	38.86	
+50	T.P.			11.40	33.36	
		2.10	35.46			
48+00	T.P.			7.20	28.26	
		4.80	33.06			

Sta.		+	H.I.	−	Elev.	
48+50	T.P.			8.70	24.36	
		3.40	27.76			
49+00				6.60	21.16	
+50				7.20	20.56	
50+00	T.P.			7.90	19.86	
		3.30	23.16			
+50				4.40	18.76	
				7.00	16.16	16.85 B.M. ± 7
		4.20	21.05			
+75				2.70	18.35	
51+00	T.P.			10.80	10.25	
		2.10	12.35			
+22	T.P.			11.40	0.95	Water Level of Slough 2-10 pm. Mar. 26th 1928.
53+27					0.95	" " " " " "
		12.80	13.75			
+50				7.60	6.15	
54+00				6.00	7.75	
54+28 64				5.50	8.25	
+48	T.P.			1.60	12.15	
		3.10	15.25			
54+78 65				8.60	6.65	
55+28 66				8.40	6.85	
+78 67				10.40	4.85	
56+28 65				7.90	7.35	

STA.		+	H.I.	−	Elev.
$+78^{66}$	T.P.			6.10	9.15
		9.65	18.80		
56+98				8.10	10.70
$57+28^{67}$				3.30	15.50
$+78^{71}$				3.65	15.15
+28				3.65	15.15
$58+76^{34}$	EC.			3.67	15.13

"B" Line

Change of Alignment from STA. 19+18 39 To STA. 32+86 64 = 33+55 03 "A" Line

24+68 50		
		11
24+18 49		
		10
23+68 48		
		9
23+18 47		
		8
22+68 46		
		7
22+18 45		
		6
21+68 44		
		5
21+18 43		
		4
20+68 42		
		3
20+18 41		
		2
19+68 40		
	50.01	1
19+18 39		B.C.

Δ = 67° 55'
R = 600'
T = 404.07'.
L = 711.22.

Defl. 4' 2° 23' 16" for 14 Short L^S @ 50.01' Chord 50'
" 0° 31' 46" " 1 " L^S @ 11.09' " 11.09'

$\Delta = 13°47'$ $\Delta/2 = 6°53'30''$

$R = 1813.75$ $\Delta/4 = 3°26'45''$

$T = 219.22$

$L = 436.32$

= 33 + 55.03 "A" Line

32 + 86.60		E.C.
	436.3 N	
28 + 50.3 N		B.C.
		P.I.
	269.76	
27 + 99.78		P.O.T.
	170.17	
26 + 29.61		E.C.
	11.09'	15
26 + 18.53		
	50.01	14
25 + 68.5 N		
		13
25 + 18.51		
		12
24 + 68.50		

"B" Line

Levels for change of Alignment See Page 56.

Sta.		+	H.I.	−	Elev.	7% Grade	Cut	Fill
19+18.39	B.C.				208.91	221.36		12.45
		0.50	243.85		243.39 BM.			
	T.P.			-13.00	230.89			
		0.60	231.49					
	T.P.			13.25	218.24			
		2.50	220.74					
19+68.40				7.70	213.04	217.86		4.82
					243.39			
		0.00	243.39					
20+18.41				14.5	228.89	214.36	14.53	
+68.42				9.1	234.29	210.86	23.43	
+88				5.1	238.29	209.46	28.83	
21+18.43	T.P.			9.6	233.79	207.36	26.43	
		2.70	236.49					
+68.44				7.05	229.44	203.86	25.58	
22+18.45	T.P.			12.75	223.74	200.36	23.38	
		1.70	225.44					
+68.46				8.60	216.84	196.86	19.98	
	T.P.			13.25	212.19			
		0.60	212.79					
23+18.47				4.10	208.69	193.36	15.33	
	T.P.			10.20	202.59			
		0.80	203.39					
+68.48				2.20	201.19	189.86	11.33	

STA.		+	H.I.	−	Elev.	7% Grade	Cut	Fill
	T.P.			12.90	190.49			
		0.40	190.89					
24+18 99				5.60	185.29	186.36		1.07
	T.P.			13.00	177.89			
		0.40	178.29					
+68 50				14.20	164.09	182.86		18.77
				0.00	178.29			
		3.40	181.69					
25+02				0.50	181.19	180.51	0.68	
+18 51				0.10	181.59	179.39	2.20	
+34				4.70	176.99	178.41		1.42
				12.40	169.29			
		0.50	169.79					
	T.P.			12.40	157.39			
		0.20	157.59					
+68 54				1.30	156.29	175.89		19.60
	T.P.			12.90	144.69			
		0.50	145.19					
26+18 53				8.30	136.89	172.39		35.50
+29 61	EC.			11.20	133.99	171.64		37.63
+58	T.P.			11.10	134.09	169.59		35.50
		0.10	134.19					
+74				18.40	115.79	168.47		52.68
+94	T.P.			2.70	131.49	167.07		35.58

STA.		+	H.I.	−	Elev.	7% Grade	Cut	Fill
		12.60	144.09					
27+17				9.80	134.29	165.46		31.17
	T.P.			0.10	143.99			
		12.40	156.39					
	T.P.			1.60	154.79			
		10.00	164.79					
+99 78				4.90	159.89	159.65	0.24	
28+30	T.P.			9.50	155.29	157.55		2.26
		0.50	155.79					
+50 34	B.C.			9.40	146.39	156.15		9.76
+60				5.50	150.29	155.45		5.16
+86 64	T.P.			12.50	143.29	153.63		10.34
		1.40	144.69					
				4.2	140.49			
					139.21			
		2.60	141.81					
29+36 64				8.20	133.61	150.13		16.52
+86 64				13.00	128.81	146.63		17.82
30+36 64				14.70	127.11	143.13		16.02
+86 64				16.20	125.61	139.63		14.02
31+36				14.30	127.51	136.13		8.62
+86				13.00	128.81	132.63		3.82
32+36				13.00	128.81	129.13		0.32
+86 64	E.C.			16.50	125.31	125.59		0.28

Sta.		+	H.I.	−	Elev.

	+	+	−	Elev	
		4193 x 9			
		2935			
		350			
		56.40			
	2718.21				
	2680.71				
	39.50				
10 + 11				291.25	
	190				
8 + 21				338.67	
	159				
6 + 62.00			10.02	333.15	
	369	343.17			
			12.81	339.48	
	2.29	352.29			
					358.

338.67
+ 1.23
339.90 H.I.
− 12.42
327.48
+ .40
327.88 H.I.
− 12.51
315.37
+ .46
315.83 H.I.
+ 13.08
302.75

19.57
5.49
14.08

69.21
4.80
74.01
− 6.58
67.43

302.75
+ 1.52
304.27 H.I.
− 13.02
291.25

69.21
+ 6.58
75.79
− 4.80
71.00

1.86 x 295
372
1674
930
5487

124 x 7
8.68
47.05
38.37

Dist. 63 N V.A 3° 38'
Diff. ☆ 28° 07

17.26 x 6

350
21
329 ; 600 = 5

El. 96.94 ✓
+ 1.94
98.88
- 9.05
89.83 ✓
+ 0.25
90.08
- 9.10
80.98 ✓
+ 1.70
82.68
- 5.50
77.18 ✓
+ 1.70
78.88
- 13.00
65.88
+ 1.10
66.98
- 8.90
58.08

STA. 33+90
333.15
10.37
343.52
82.98
11.87
81.11
4.7
85.81
7.71 x 4
30.84
7.82 x 5
39.10
7.30 x 6
43.80
6.38 x 7
44.66
5.63 x 8
45.04

6+64
1 59
8+21

343.52
4.85
338.67

251.31
4.7
256.01
255.59

108 x 7
756
228.83
221.27

13.06
5.98
7.10
7.10
14.20

5.63 x 85
4504
2815
47855

700
137
563

10.11 x 2
20.22

5454
4304
850
563
1413

54+51.91
54.04
47.41

T = 600 x 1/2 Δ tang.
Δ = 24 - 26
.45432 x 600
272.59200
1420
7.41

57+24
27+.59
5451.41 ✓
4304.00
1147.41

4WD P.I.

9.71 x 2
11.42

5451.41
5404
47.41

1.86 x 295
372.4

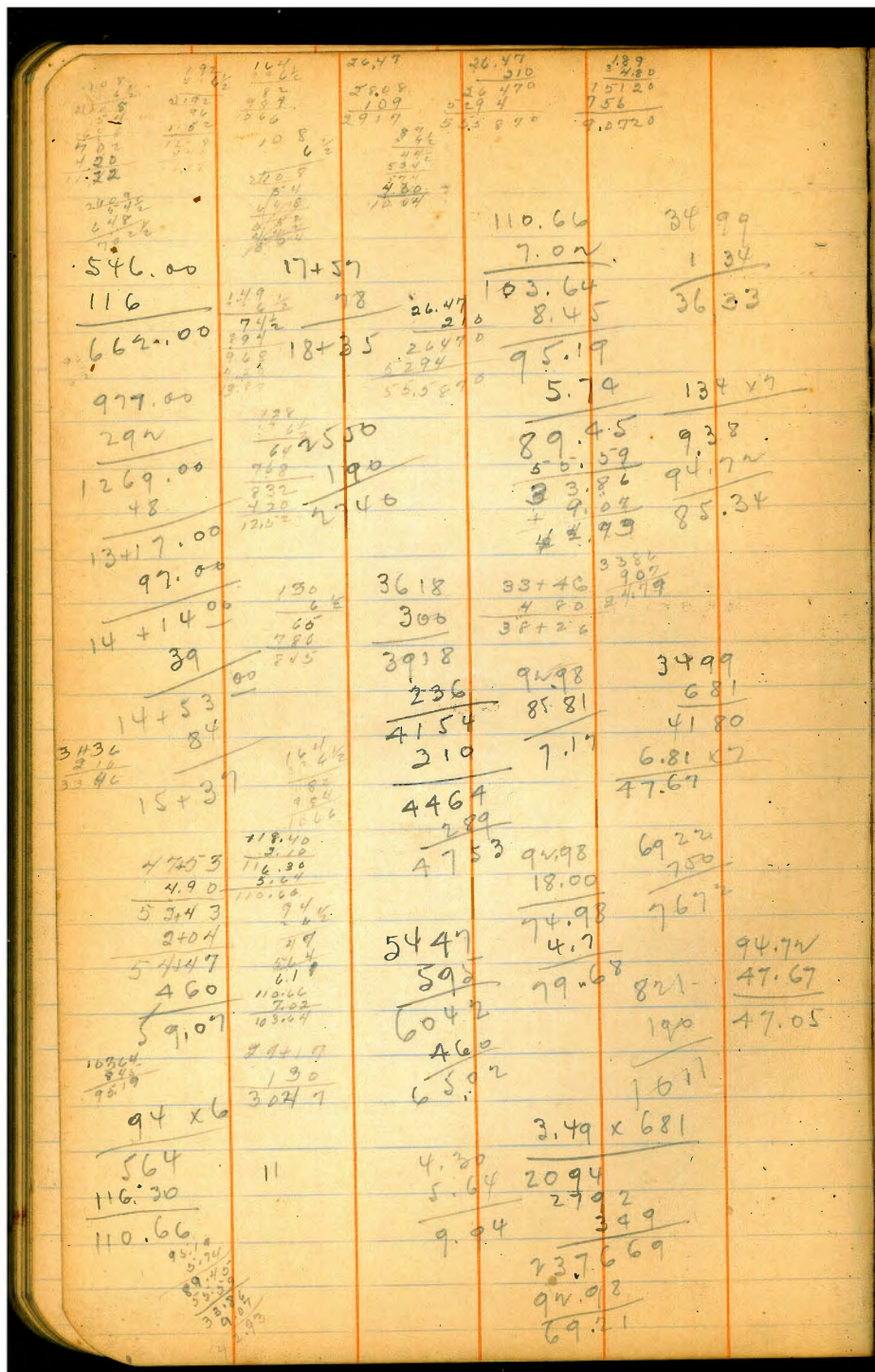
4.8 x 250
960
2410
12.05.00
19.57
7.52

67.43 | 67.43 | 67.43 | 67.43
9.48 | 11.42 | 27.24 | 30.84
57.95 | 56.01 | 40.19 | 36.59

67.43 | 67.43 | 67.43 | 67.43
39.10 | 43.80 | 44.66 | 45.04
28.33 | 23.63 | 22.77 | 22.39

67.43
47.86
19.57

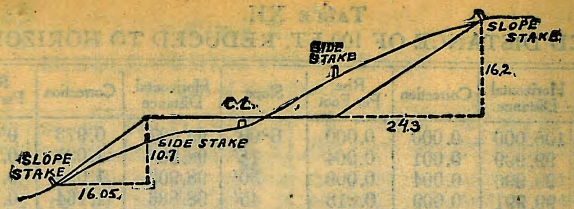
3.26 x 1420
1304
6520
4629.20
67.43
21.14



3667.66
3355.03
312.63

9+11 0040 W.

IMPROVED TABLES
AND
INFORMATION



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1 65	1 80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3 45	3.60	3 75	3.90	4.05	4.20	4 35	2
3	4.50	4 65	4.80	4.95	5 10	5 25	5 40	5.55	5.70	5.85	3
4	6.00	6 15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7 50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9 00	9 15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10 65	10.80	10.95	11.10	11.25	11.40	11.55	11 70	11.85	7
8	12.00	12 15	12.30	12.45	12.60	12.75	12.90	13 05	13.20	13.35	8
9	13 50	13 65	13 80	13 95	14.10	14.25	14.40	14 55	14.70	14.85	9
10	15.00	15 15	15 30	15 45	15.60	15.75	15.90	16.05	16.20	16 35	10
11	16 50	16 65	16 80	16.95	17 10	17.25	17.40	17.55	17.70	17.85	11
12	18 00	18 15	18.30	18 45	18.60	18 75	18.90	19.05	19.20	19 35	12
13	19 50	19 65	19.80	19.95	20.10	20.25	20 40	20.55	20.70	20.85	13
14	21.00	21 15	21.30	21.45	21 60	21.75	21.90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24 15	24 30	24 45	24 60	24.75	24 90	25 05	25.20	25.35	16
17	25.50	25 65	25.80	25 95	26.10	26 25	26 40	26.55	26.70	26.85	17
18	27.00	27 15	27.30	27 45	27.60	27.75	27.90	28.05	28 20	28.35	18
19	28 50	28 65	28 80	28.95	29.10	29.25	29 40	29.55	29.70	29.85	19
20	30 00	30 15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31 50	31 65	31.80	31.95	32 10	32 25	32.40	32.55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33.60	33 75	33.90	34.05	34.20	34.35	22
23	34 50	34 65	34.80	34.95	35.10	35 25	35 40	35.55	35.70	35 85	23
24	36.00	36 15	36.30	36 45	36.60	36.75	36.90	37.05	37 20	37.35	24
25	37.50	37.65	37 80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39 00	39 15	39.30	39 45	39 60	39.75	39.90	40.05	40.20	40.35	26
27	40 50	40 65	40 80	40.95	41.10	41.25	41 40	41.55	41.70	41.85	27
28	42 00	42 15	42.30	42.45	42.60	42 75	42.90	43.05	43.20	43.35	28
29	43 50	43 65	43.80	43 95	44.10	44 25	44 40	44.55	44.70	44 85	29
30	45 00	45 15	45.30	45 45	45.60	45.75	45.90	46.05	46 20	46.35	30
31	46.50	46.65	46.80	46 95	47.10	47 25	47.40	47.55	47.70	47.85	31
32	48 00	48.15	48.30	48 45	48.60	48 75	48.90	49.05	49 20	49.35	32
33	49 50	49 65	49.80	49.95	50.10	50.25	50.40	50.55	50 70	50.85	33
34	51 00	51.15	51.30	51.45	51.60	51 75	51.90	52.05	52.20	52.35	34
35	52 50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54 00	54 15	54.30	54 45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55 50	55 65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57 00	57.15	57.30	57 45	57.60	57 75	57.90	58.05	58.20	58 35	38
39	58 50	58.65	58 80	58.95	59.10	59 25	59.40	59 55	59.70	59.85	39
40	60 00	60 15	60 30	60 45	60 60	60.75	60 90	61.05	61 20	61.35	40
41	61.50	61 65	61 80	61 95	62 10	62 25	62.40	62 55	62 70	62.85	41
42	63 00	63.15	63.30	63 45	63 60	63 75	63 90	64 05	64 20	64.35	42
43	64.50	64 65	64 80	64.95	65.10	65 25	65 40	65.55	65.70	65.85	43
44	66 00	66 15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67 50	67 65	67 80	67.95	68.10	68.25	68 40	68.55	68.70	68.85	45
46	69 00	69 15	69 30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70 50	70 65	70 80	70 95	71.10	71.25	71 40	71.55	71.70	71.85	47
48	72 00	72 15	72.30	72.45	72.60	72.75	72.90	73 05	73.20	73 35	48
49	73 50	73 65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.

(1)

20+20 ^{9} — B.C.

108.90'

16+12 ^{00}. E.C.

R = 600'
Δ = 59°00' - R
T = 339.46'.
L = 617.85'.

9+94 ^{15}. B.C.

103.13

8+91 ^{02}. E.C.

R = 1000'
Δ = 18°58' L
T = 167.04'.
L = 331.03.

5+59 ^{99} B.C.

559.99'

0+00 E.C. of Curve of Existing Highway

9+ [illegible]

10+00

.51

N88.16

20+20 90 — B.C.

408.90'

16+12 00 — E.C.

R = 600'
Δ = 59°00' - R
T = 339.46'.
L = 617.85'.

9+94 15 — B.C.

103.13

8+91 02 — E.C.

R = 1000'
Δ = 18°58' L
T = 167.04'.
L = 331.03.

5+59 99 — B.C.

559.99'

0+00 — E.C. of Curve of Existing Highway

39+05 90 E.C.

R = 1000'
Δ = 13°39' - R
T = 119.69'
L = 238.24'.

36+67 56 B.C.

312.63'

33+55 93 E.C.

R = 800'
Δ = 30°39' - R
T = 219.22'.
L = 427.95'.

29+27 98 B.C.

18.51'.

29+08 57 E.C.

R = 600'
Δ = 84°46' - L
T = 547.55'.
L = 887.67'

20+20 90 B.C.

58+76 32 — E.C.

R = 600'
Δ = 42°45' Rt.
T = 234.84'.
L = 447.68'.

54+28 64 — B.C.

1041.85

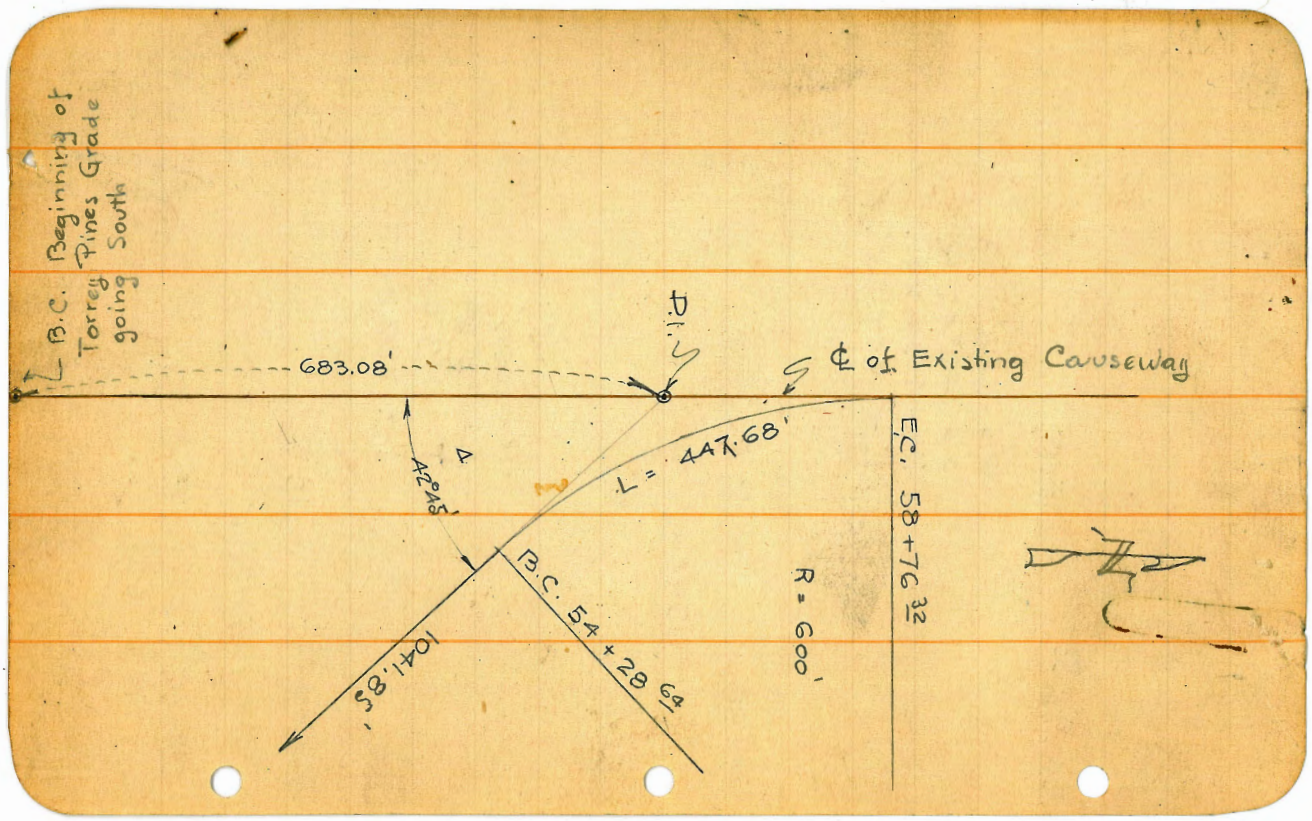
43+86 79 — E.C.

R = 1000'
Δ = 13°39' - L
T = 119.69'.
L = 238.24'.

41+48 55 — B.C.

242.65'

39+05 90 — E.C.


B.C. Beginning of Torrey Pines Grade going South
683.08'
P.I.
℄ of Existing Causeway
Δ
42°48'
L = 447.68'
E.C. 58+76.32
R = 600'
B.C. 54+28.64
1041.85'

STA.					Elev.
25+21					167.49
+71.01					147.39
+85					146.79
26+00					151.89
+21.02					147.70
+71.03					140.80
27+21.09					124.00
+36					115.90
+51					120.30
+57					109.60
+71.05					109.00
+79					115.30
+95					119.70
28+21.06					118.60
+55					119.10
+71.07					123.30
29+08.57	E.C.				135.60
+13.80					137.00
+27.08	B.C.				136.40

Levels on ℄ of Proposed Torrey Pines Rd.

JAEGER

STA.					Elev.
0+00	B.C. of Curve on existing Pavement				350.00
1+01	Edge of Pavement				348.58
+57					348.88
2+02					346.48
486					347.98
3+20.85					347.93
+30					348.98
4+00					347.28
+50					345.5v
5+00					343.5v
+59.99	B.C.				340.9v
6+10.02					338.22
+60					332.75
+66					331.65
+72					333.25
7+10.08					334.90
+60.11					336.55
8+10.19					340.10
+19					339.90
+28					335.55
+60.17					328.57
+91.02	E.C.				316.73
9+94.15	B.C.				292.51
10+00					288.16

STA.		Elev.
10+18		282.71
+44 16		264.84
+89		233.85
+94 17		233.65
11+44 18		235.25
+94 19		244.75
12+19		237.05
+44 20		239.18
+80		249.68
+94 21		243.98
13+20		231.83
+44 22		230.53
+94 23		227.63
14+15		227.13
+24		219.83
+44 24		229.73
+94 25		240.23
15+32		233.87
+44 26		234.97
+69		236.87
+94 27		227.57
16+12	E.C.	216.47
+30		217.27
+78 62		253.97
+98		243.75

STA.		Elev.
17+28		227.45
+60		249.91
+80 58		256.32
18+59 58		244.96
+89 58		237.41
+95 58		228.41
19+10 58		218.91
+25 58		201.91
+38 58		194.91
+53 58		199.51
+63 58		213.81
+88 58		229.01
20+05		214.84
+20 90	B.C.	222.01
+23 90		226.01
+70 19		229.61
21+20 92		228.59
+70 92		220.99
22+20 94		218.39
+70 95		212.99
23+20 96		209.79
+70 97		202.29
24+20 98		193.69
+70 99		182.49
+90		175.59

29+77 09		127.31
30+27 10		124.81
+77 11		124.51
31+27 12		122.71
+77 13		122.61
32+27 14		128.28
+77 15		128.38
33+27 16		125.21
+55 03	E.C.	122.81
34+00		120.11
+50		118.60
35+00		121.01
+50		120.21
+68 44		119.91
36+00		119.91
+50		119.31
+67 66	B.C.	119.21
37+17 69		116.61
+67 72		112.71
38+17 75		108.04
+67 78		105.34
39+05 90	E.C.	101.64
+50		96.34
40+00		92.46
+50		88.96
41+00		86.16

41+48 55	B.C.				83.26	53+50					6.15
+98 58					79.56	54+00					7.75
42+48 61					76.16	54+28 69	B.C.				8.25
+98 64					71.99	+48					12.15
43+48 67					66.80	+78 65					6.65
+86 79	E.C.				61.70	55+28 66					6.85
44+00					60.30	+78 67					4.85
+50					56.50	56+28 68					7.35
45+00					54.50	+78 69					9.15
+50					53.20	+98					10.70
46+00					49.26	57+28 70					15.50
+50					44.96	+78 71					15.15
47+00					38.86	58+28 72					15.15
+50					33.36	58+76 32	E.C.				15.13
48+00					28.26						
+50					24.36						
49+00					21.16						
+50					20.56						
50+00					19.86						
+50					18.76						
+75					18.35						
51+00					10.25						
+22					0.95	Water Level of Slough at 2-10 p.m. 26th 1928.					
53+27					0.95	"	"	"	"	"	"	"	"