

1291

*This index to pp 80 7/14/30 WAH*

MICROFILMED

DEC 22 1964

Our Leather Bound Engineers Note Books are carried in the following rulings:

- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
- No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.
- No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.
- No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

We also carry the Note Books listed above, bound in extra strong Fabri-Hide (otherwise the same quality of book), which can be furnished at a somewhat lower price.

In ordering Fabri-Hide covered books, add the letter "F" to catalog number.

**THE FREDERICK POST CO.**  
*ENGINEERING and DRAFTING SUPPLIES*  
IRVING PARK STATION  
CHICAGO, ILL.

92 FIFTH ST.  
PORTLAND, ORE.

79 NEW MONTGOMERY ST.  
SAN FRANCISCO, CAL.

AGENTS FOR  
"BERGER" TRANSITS and LEVELS  
"GURLEY" SURVEYING and HYDRAULIC INSTRUMENTS  
"CHICAGO" STEEL TAPES, etc.

This index to pp 80 7/14/20 HA

INDEX

		PAGE
Cross Section	54th bet. Adams + 6th	
"	" <sup>Plotted</sup> HINSON ST.	76-79
"	" <sup>Plotted</sup> 55th St. From El Cajon North	16-35
"	" <sup>Plotted</sup> 56th " to Adams	35- Holland Dr.
"	" <sup>Plotted</sup> ROBBAND Dr. bet. Adams + 55th	36-58
"	" <sup>Plotted</sup> COLLEGE AVE bet. 54th + 55th	
"	" <sup>Plotted</sup> Adams " bet. 54th + El Cerito Dr.	64-75
"	" <sup>Plotted</sup> MADISON Ave bet. 55th "	" 59-63
"	" Gilbert Dr. bet. Berling + 55th	7-12
"	" DAYTON " El Cajon + Gilbert	12-15
"	" Berling + bet. " "	1-6

Time interval top to 80 7/12/1900

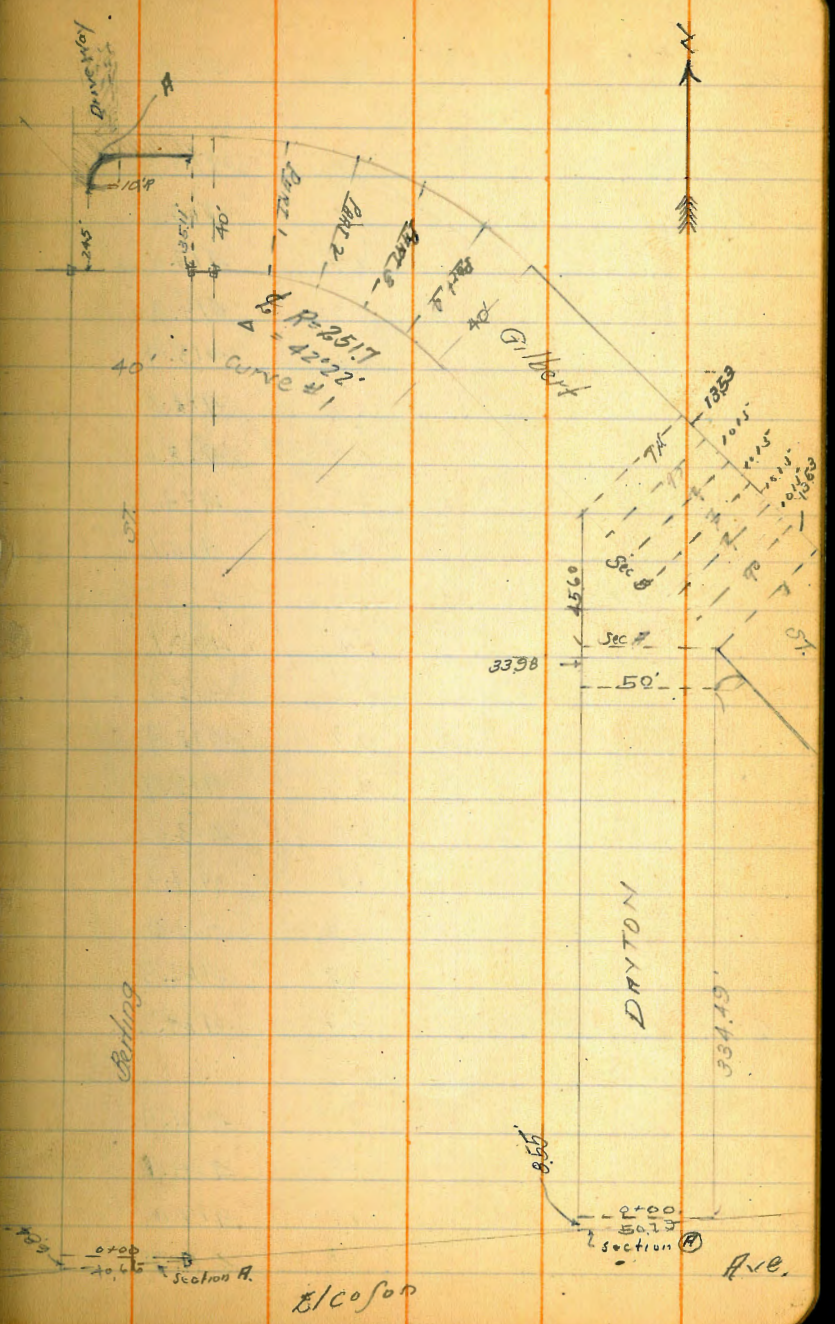
Walker  
Residence  
Sheet  
2-29-28

Cross Section BERTING ST.  
40' wide 5' chs 7.5' to  
from Elcoson to Gilbert

W. St. Mon. Elcoson  
+ Dayton

	2.17	421.45	419.28
	Section A		
N		10.4	414.1
ch.		10.3	411.2
i		10.1	411.4
d		10.1	411.4
i		9.9	411.6
ch.		9.7	411.8
F		9.1	411.4
	0+00		
E		9.1	411.4
ch.		9.7	411.8
i		9.9	411.6
d		10.0	411.5
i		10.2	411.3
ch.		10.2	411.3
N		10.2	411.3
	0+50		
N		7.4	412.1
ch.		9.6	411.9
i		9.4	412.1
d		8.9	412.6
i		8.7	412.8
ch.		8.8	412.7
+1		7.9	413.6

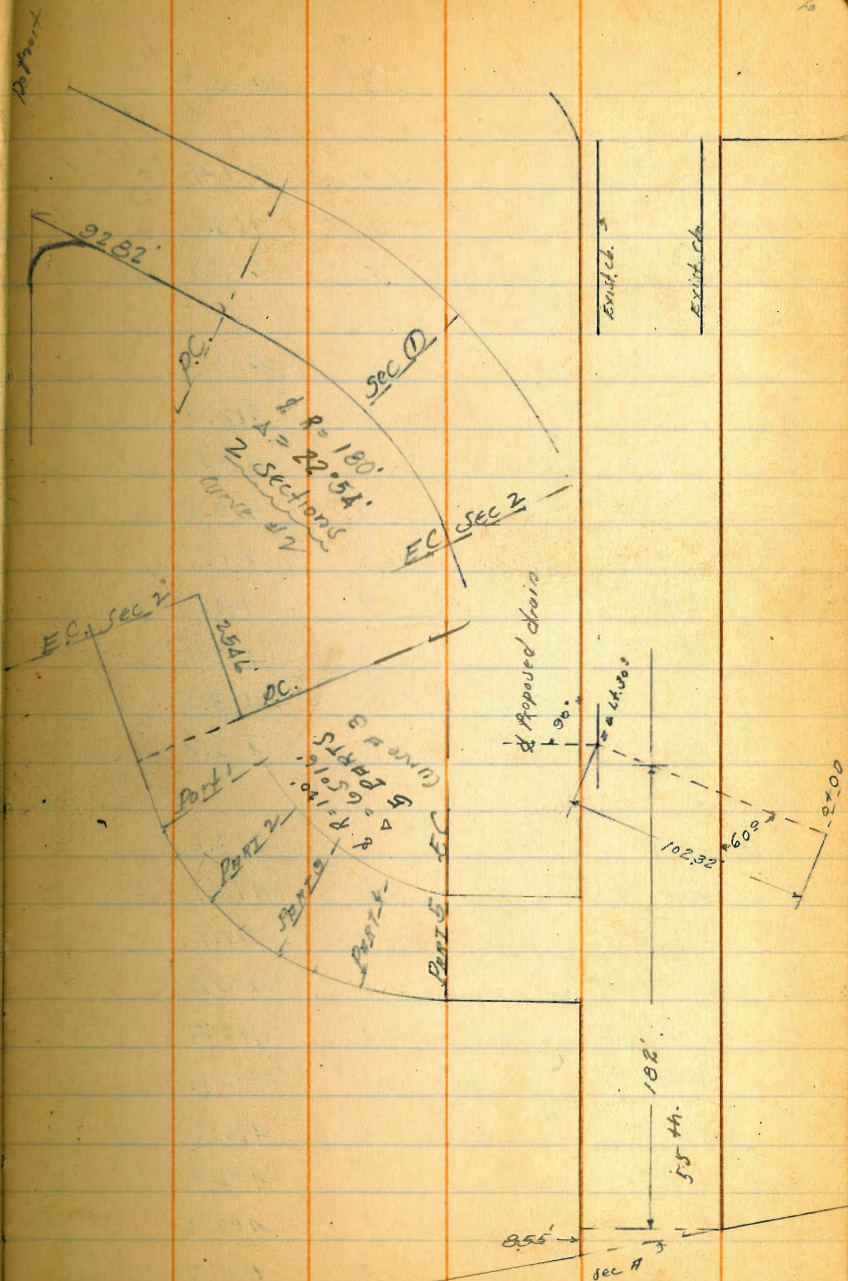
□ = 2" x 2" Redwood hubs



Elcoson

Ave.

E		7.8	413.7
	1+00		
E		6.7	414.8
+4		6.7	414.8
cb		7.9	413.6
$\frac{1}{4}$		8.2	413.3
$\frac{1}{2}$		8.1	413.4
$\frac{3}{4}$		8.5	413.0
cb		8.9	412.6
+1		8.2	413.3
Y		8.4	413.1
	1+50		
Y		8.4	413.1
+4		8.2	413.3
cb		9.1	412.4
$\frac{1}{4}$		8.8	412.7
$\frac{1}{2}$		8.5	413.0
$\frac{3}{4}$		8.5	413.0
cb		8.5	413.0
+1		7.7	414.3
E		7.7	414.3
	2+00		
E		7.1	414.4
+4		7.4	414.1
cb		9.5	412.0
$\frac{1}{4}$		9.8	411.7



421.45 ✓

2	9.5	412.0
$\frac{1}{4}$	9.9	411.6
cb.	10.1	411.4
+1	8.5	413.0
NY	8.7	412.8
2+34		
NY	9.3	412.2
+4	9.5	412.0
cb.	11.1	410.4
$\frac{1}{4}$	10.9	410.6
$\frac{1}{4}$	10.7	410.8
$\frac{1}{4}$	10.9	410.6
cb.	10.7	410.8
+1	8.0	413.5
E	7.7	413.8
2+52		
-5	7.9	413.6
E	9.4	412.1
+4	10.4	411.1
cb.	11.5	410.0
$\frac{1}{4}$	11.1	410.4
$\frac{1}{4}$	11.1	410.4
$\frac{1}{4}$	11.4	410.1
cb.	12.0	409.5
NY	15.1	406.4
+15	15.7	405.8

421.45 ✓

Berling St.

3

2+74		24.3	397.2
-25		22.0	399.5
-10		17.5	404.0
NY		14.1	407.4
cb.		11.4	410.1
+5		11.3	410.2
$\frac{1}{4}$		11.2	410.3
$\frac{1}{4}$		11.3	410.2
$\frac{1}{4}$		11.3	410.2
+5		12.1	409.3
cb.		12.3	408.2
E		12.3	408.2
+10		12.3	408.2
2+92		13.5	408.0
-20		15.5	406.0
E		13.4	408.1
cb.		11.1	410.4
+5		11.1	410.4
$\frac{1}{4}$		10.9	410.6
$\frac{1}{4}$		11.2	410.3
+4		11.2	410.3
cb.		12.9	408.6
NY		17.0	404.5
+7		20.2	401.3
+26		24.5	397.0

Note: This Section can be used for Culvert if all is made here small culvert 12"

421.45 ✓

+40		26.0	395.5
TP	9.72	420.91	10.26
	3+33		
-20		15.7	405.2
N		13.7	407.2
cb		10.4	410.5
4		10.1	410.8
8		9.8	411.1
4		10.0	410.9
cb		10.2	410.7
E		10.2	410.7
+5		10.0	410.9
+10		9.7	411.2
	3+35		
-5		7.1	413.8
E		7.1	413.8
+4		2.2	413.7
cb		10.0	410.9
4		9.5	411.4
8		9.3	411.6
4		9.7	411.2
+6		9.5	411.4
cb		8.3	412.6
N		8.3	412.6
+5		8.7	412.2
	3+50		

420.91 ✓

Berling St

4

N		7.7	413.2
+4		7.7	413.2
cb		9.0	411.9
4		9.1	411.8
8		8.7	412.2
4		9.0	411.9
cb		9.2	411.7
+1		6.6	414.3
E		6.4	414.5
	4+00		
E		5.0	415.9
cb		5.2	415.7
+1		7.0	413.9
4		7.3	413.6
8		7.0	413.9
4		7.3	413.6
cb		7.3	413.6
+1		6.4	414.5
N		6.5	414.4
	4+50		
N		4.2	416.7
+4		4.2	416.7
cb		5.2	415.7
4		5.4	415.5
8		5.4	415.7
4		5.3	415.6

+2091

✓

+5		5.5	415.4
cb		3.5	417.4
E		3.2	417.7
	5+00		
E		2.3	418.6
cb		2.7	418.2
+1		4.2	416.7
$\frac{1}{2}$		3.9	417.0
$\frac{1}{2}$		3.7	417.2
$\frac{1}{2}$		4.0	416.9
+6		4.1	416.8
cb		3.2	417.7
W		3.2	417.7
	5+50		
W		3.3	417.6
cb		3.3	417.6
$\frac{1}{2}$		3.1	417.8
$\frac{1}{2}$		2.8	418.1
$\frac{1}{2}$		3.1	417.8
+5		3.5	417.4
cb		1.6	419.3
E		1.6	419.3
	6+00		
E		1.3	419.6
cb		1.3	419.4
+1		3.2	417.7

+2091

BERTING ST

5

$\frac{1}{2}$		2.7	418.2
$\frac{1}{2}$		2.5	418.4
$\frac{1}{2}$		2.7	418.2
cb		3.2	417.7
+1		2.6	418.3
W		2.7	418.2
	6+50		
W		3.1	417.8
cb		3.0	417.9
$\frac{1}{2}$		3.0	417.9
$\frac{1}{2}$		2.8	418.1
$\frac{1}{2}$		3.0	417.9
+6		3.2	417.7
cb		2.3	418.6
E		2.0	418.9
	6+62.3 = South Line Gilbert St. on E		
E		2.0	418.9
cb		2.6	418.3
+1		3.1	417.8
$\frac{1}{2}$		3.1	417.8
$\frac{1}{2}$		3.1	417.8
E		3.4	417.5
cb		3.3	417.6
W		3.4	417.5
	6+86.8 = End of Exit cb. on W	3.88	417.03
	6+97.4 Sec. taken on gutter at cb. face		

See sketch  
Page 1.



420.91 ✓

N-10	5.7	415.2
-2	5.2	415.7
N	4.0	416.9
cb	4.0	416.9
$\frac{1}{2}$	4.2	416.7
$\frac{1}{4}$	4.0	416.9
$\frac{1}{4}$	4.2	416.7
cb	4.0	416.9
E	3.7	417.2

6+97.4<sup>1</sup> Sec. taken on top of exist cb.

E top cb	3.67	417.24
cb " "	3.76	417.15
$\frac{1}{4}$ " "	3.81	417.10
$\frac{1}{8}$ " "	3.86	417.05
+4' " " = edge drive way	3.88	417.03
Red at # in drive way	4.11	416.80
N	4.0	416.9
+2	5.2	415.7
+10	5.7	415.2

7+02.3<sup>3</sup> Section taken on top North edge of walk

N-10	6.3	414.6
N on top	3.17	416.94
cb	3.87	417.04
$\frac{1}{2}$	3.87	417.04
+7.5 = PC. See sketch Page 1	3.84	417.07
$\frac{1}{4}$	3.79	417.12

420.91 ✓

Note:  
this H.T. used on  
Page 7 for cbh. out see Page 12

6

3.78	417.13
3.67	417.24
3.60	417.31

Walker  
Ruppinger  
Sheg 2-29-28

X. Section G1/bert st. 40' wide 5' cbs  
From Berting to 355b 7.5' x 5'

420.91 = T from Page 6

P.C. Pt. 42°22' = 379' E.E.L. Berting

N	3.3	417.6
cb.	3.5	417.4
$\frac{1}{2}$	3.4	417.7
$\frac{1}{2}$	2.9	418.0
$\frac{1}{2}$	2.8	418.1
cb.	2.6	418.3
+3	2.5	418.4
S	2.0	418.9

PART 1

J.P.	7.64	426.46	2.09	418.82
S			6.7	417.6
cb			7.0	419.5
$\frac{1}{2}$			7.3	419.2
$\frac{1}{2}$			7.4	419.1
$\frac{1}{2}$			7.6	418.9
cb.			7.9	418.6
N			7.9	418.6
+5			8.1	418.4

PART 2

-5	7.3	419.2
N	7.1	419.4
cb	7.1	419.4
$\frac{1}{2}$	6.9	419.6
$\frac{1}{2}$	6.8	419.7

426.46

7

$\frac{1}{2}$	6.6	419.9
cb	6.5	420.0
S	6.3	420.2

PART 3

S	5.9	420.6
cb	5.9	420.6
$\frac{1}{2}$	6.0	420.5
$\frac{1}{2}$	6.3	420.2
$\frac{1}{2}$	6.7	419.8
cb.	6.9	419.6
N	6.9	419.6
+5	7.3	419.2

PART 4

-5	7.0	419.5
N	6.6	419.9
cb.	6.2	420.3
$\frac{1}{2}$	5.8	420.7
$\frac{1}{2}$	5.6	420.9
$\frac{1}{2}$	5.4	421.1
cb.	5.3	421.2
S	5.2	421.2

PART 5 = E.C. = 0+00

S	5.7	421.3
cb.	5.3	421.2
$\frac{1}{2}$	5.5	421.0
$\frac{1}{2}$	5.5	421.0

Y. G. Key  
Repl  
Sh

42646 ✓

42646 ✓ Gilbert St

8

1/2		5.6	420.9
cb		5.9	420.6
N		5.9	420.6
+5		6.1	420.4
	0+50		
-5		6.5	420.0
N		6.1	420.4
cb		6.2	420.3
1/4		5.6	420.9
2		5.3	421.2
1/4		5.2	421.3
cb		5.0	421.5
S		4.9	421.6
	1+00		
S		4.7	421.8
cb		4.9	421.6
1/4		4.9	421.6
2		5.0	421.5
1/4		5.4	421.1
cb		5.8	420.7
N		5.9	420.6
+5		6.3	420.2
	1+50		
-5		6.6	419.9
N		6.4	420.1
cb		6.9	420.2

1/2		6.0	420.5
2		5.8	420.7
1/4		5.6	420.9
cb		5.5	421.0
S		5.2	421.3
	1+89.61 = N.L. Dayton		
S		5.3	421.2
cb		5.5	421.0
1/4		5.5	421.0
2		5.8	420.7
1/4		6.0	420.5
cb		6.2	420.3
N		6.4	420.1
+5		6.9	419.6
	N cb		
-5		7.0	419.5
N		6.5	420.0
cb		6.3	420.2
1/4		6.0	420.5
2		5.8	420.7
1/4		5.5	421.0
cb		5.6	420.9
S		5.7	420.8
	N 1/2		
S		5.6	421.0
cb		5.5	421.0

Sections as per sketch Page 1

426.46 ✓

4	56	420.9
2	59	420.6
4	63	420.2
cb	63	420.2
N	67	419.8
+5	71	419.4
E. Dayton		
-5	72	419.3
N	67	419.8
cb	64	420.1
4	60	420.5
4	62	420.3
4	56	420.9
cb	56	420.9
S	55	421.0
E 4		
S	55	421.0
cb	56	420.9
4	60	420.5
4	59	420.6
4	63	420.2
cb	64	420.1
N	70	419.5
+5	75	419.0
E cb		
-5	77	418.8

426.46 ✓

Gilbert

9

N	7.0	419.5
cb	67	419.8
4	62	420.3
4	60	420.5
4	58	420.7
cb	57	420.8
S	61	420.4
E.L. Dayton = 0+00		
S	57	420.8
cb	57	420.8
4	59	420.6
4	60	420.5
4	64	420.1
cb	69	419.6
N	71	419.4
+5	77	418.8
0+4641		
-5	87	417.8
N	82	418.3
cb	77	418.8
4	70	419.5
4	66	419.9
4	64	420.1
cb	61	420.4
S	61	420.4
0+9282 = PC. Pt. 22°54'		

426.46 ✓

U	5.9	420.6
cb.	6.1	420.9
$\frac{1}{4}$	6.4	420.1
$\frac{1}{2}$	6.6	419.9
$\frac{3}{4}$	7.3	419.2
cb.	8.0	418.5
N	8.5	418.0
+5	8.7	419.8
+10	9.5	417.0

Section ①

-10'	8.3	418.2
N	7.7	418.8
cb.	7.5	419.0
$\frac{1}{4}$	7.0	419.5
$\frac{1}{2}$	6.5	420.0
$\frac{3}{4}$	6.1	420.4
cb.	5.6	420.9
S	5.5	421.0

Sec ② = E.C.

U	5.5	421.0
cb.	5.6	420.9
$\frac{1}{4}$	6.0	420.5
$\frac{1}{2}$	6.4	420.1
$\frac{3}{4}$	6.8	419.7
cb.	7.1	419.4
N	7.3	419.2

426.46 ✓

Gilbert

10

+10

-10

+10

Above P.C.

-10

N

cb.

 $\frac{1}{4}$  $\frac{1}{2}$  $\frac{3}{4}$ 

8.1  
 25.46' East of curve #2 = P.C. Lt. 65°16' = curve #3

Sketch Book

Below

13	419.2
6.7	419.8
6.4	420.1
6.4	420.1
6.0	420.5
5.6	420.9

426.46 ✓

cb.	5.3	421.2
S	5.3	421.2
PART 1		
S	5.2	421.3
cb	5.3	421.2
$\frac{1}{2}$	5.6	420.9
$\frac{2}{4}$	6.0	420.5
$\frac{3}{4}$	6.6	419.9
cb.	7.0	419.5
N	7.2	419.3
+10	7.8	418.7
Part 2		
-10	8.2	418.3
N	7.6	418.9
cb.	7.6	418.9
$\frac{1}{4}$	7.2	419.3
6	6.6	419.9
$\frac{1}{2}$	6.4	420.1
cb	6.1	420.4
S	5.8	420.7
PART 3		
S	6.3	420.2
cb.	6.6	419.9
$\frac{1}{2}$	7.0	419.5
$\frac{3}{4}$	7.5	419.0
$\frac{1}{4}$	8.1	418.4

426.46 ✓

Gilbert

11

cb.	8.4	418.1
N	8.6	417.9
+10	9.2	417.3
T.P.	5.65	424.04
PART 4		
N-10	8.1	415.9
N-5	7.8	416.2
N-1	6.9	417.1
N	6.6	417.4
cb	6.8	417.2
$\frac{1}{2}$	6.5	417.5
$\frac{3}{4}$	6.3	417.7
$\frac{1}{4}$	6.0	418.0
cb	5.0	419.0
S	5.0	419.0
PART 5 = B.C. = 0+00		
S	5.0	419.0
cb.	5.6	418.4
$\frac{1}{2}$	5.9	418.1
$\frac{3}{4}$	6.4	417.6
$\frac{1}{4}$	6.4	417.6
cb.	6.5	417.5
N	6.7	417.3
+1	7.7	416.3
+15	9.8	414.2
D+40		

42404

-15	9.7	419.3
N	7.0	417.0
+2	6.1	417.9
cb	6.1	417.9
$\frac{1}{2}$	6.2	417.8
$\frac{1}{2}$	6.0	418.0
$\frac{1}{2}$	5.5	418.5
cb	5.3	418.7
S	5.3	418.7
	0+80	
S	4.2	419.8
cb	4.7	419.3
$\frac{1}{2}$	4.9	419.1
$\frac{1}{2}$	5.2	418.8
$\frac{1}{2}$	5.5	418.5
cb	5.7	418.3
N	5.6	418.4
+10	7.0	417.0
	1+0597 = 2/4. 55 <sup>th</sup> st	
-10	5.2	418.8
N	4.7	419.3
+3	5.4	418.6
cb	5.4	418.6
$\frac{1}{2}$	5.2	418.8
$\frac{1}{2}$	5.1	418.9
$\frac{1}{2}$	4.9	419.1

42404

Gilbert

12

cb	4.8	419.2
+2	4.6	419.4
S	3.1	420.9
cbk. on <sup>8.14</sup> S.E. Mon. E. Canyon + 55 <sup>th</sup>	1.26	422.78
		422.78 = 5.11
		0.00 ✓

Volker  
 7/21/1904  
 Sta 2-29-28

Cross Section Dayton st. 50' wide 10' cbs  
 From E. Cojan to Gilbert st.  
 7.5' 2S

426.49 ✓

B.M. N.Y. Con. Man  
 E. Cojan - Dayton

7.81 426.49 419.28

Section (2) See sketch Page 1

				+9		6.9	419.6
				cb		7.5	419.0
				$\frac{1}{2}$		6.9	419.6
14		7.7	418.8	$\frac{1}{2}$		6.7	419.8
+5		8.2	418.3	$\frac{1}{2}$		6.6	419.9
cb		8.4	418.1	cb		7.2	419.3
$\frac{1}{4}$		8.4	418.1	+1		6.3	420.2
$\frac{1}{2}$		7.9	418.6	+8		6.3	420.2
$\frac{1}{4}$		8.1	418.4	E		4.7	421.8
cb		8.2	418.3		1+00		
+2		8.2	418.3	E		4.1	422.4
+3		7.9	418.6	+2		5.5	421.0
E		7.5	419.0	+9		5.4	421.1
	0+00			cb		6.0	420.5
E		7.5	419.0	$\frac{1}{2}$		5.7	420.8
+7		7.9	418.6	$\frac{1}{2}$		5.5	421.0
cb		8.1	418.4	$\frac{1}{2}$		5.8	420.7
$\frac{1}{2}$		8.1	418.4	cb		6.4	420.1
$\frac{1}{2}$		7.9	418.6	+1		5.9	420.6
$\frac{1}{4}$		8.3	418.2	+8		5.8	420.7
cb		8.4	418.1	14		4.9	421.6
+1		8.1	418.4		1+50		
14		7.7	418.8	14		4.6	421.9
	0+50			+4		5.0	421.5
14		5.4	421.1	+7		4.9	421.6
+2		7.1	419.4	+8		5.4	421.1



426.49 ✓

cb.	5.3	421.2
$\frac{1}{4}$	4.7	421.8
$\frac{1}{2}$	4.7	421.8
$\frac{1}{4}$	4.7	421.8
cb.	5.2	421.3
+1	4.8	421.7
+8	4.5	422.0
E	3.5	423.0
	R+00	
E	4.5	422.0
+9	4.6	421.9
cb.	5.1	421.4
$\frac{1}{4}$	4.4	422.1
$\frac{1}{2}$	4.6	421.9
$\frac{1}{4}$	5.0	421.5
cb.	5.4	421.1
+1	4.9	421.6
W	5.2	421.3
	R+50	
W	5.6	420.9
+9	5.4	421.1
cb.	5.9	420.6
$\frac{1}{4}$	5.2	421.3
$\frac{1}{2}$	5.2	421.3
$\frac{1}{4}$	5.1	421.4
cb.	5.4	421.1

426.49 ✓ Dayton

14

+1	5.1	421.4
E	5.2	421.3
	3+00	
E	5.5	421.0
+9	5.4	421.1
cb.	5.9	420.6
$\frac{1}{4}$	5.5	421.0
$\frac{1}{2}$	5.5	421.0
$\frac{1}{4}$	5.6	420.9
cb.	6.2	420.3
+1	5.5	421.0
W	5.7	420.8
	3+34.49 = R. on Foot. Sketch Page 1	
W	5.8	420.7
+8	5.6	420.9
cb.	6.3	420.2
$\frac{1}{4}$	5.7	420.8
$\frac{1}{2}$	5.7	420.8
$\frac{1}{4}$	5.8	420.7
cb.	6.2	420.3
+1	5.6	420.9
E	5.8	420.7
	Section F	
E	5.7	420.8
+9	5.7	420.8
cb.	6.4	420.3

i	56	420.9
z	56	420.9
7	55	421.0
+5	53	421.2
cb	60	420.5
+2	55	421.0
W.	53	421.2

## Section B.

W	54	421.1
cb	58	420.7
7	55	421.0
z	55	421.0
7	56	420.9
cb	62	420.3
+1	56	420.9
E	57	420.8

Yalther  
Rogers  
Shaw  
May 2-29-28

X. Section 55th St. 50' wide 10' cbs  
Sum Elevation Five North 7.5' 25

424.16 ✓

16

N.E. 8th on Center  
Elevation 455.73

138

424.16 ✓

422.78

Section # - Page 2

E	1.3	422.9
+6	2.0	422.2
cb.	2.4	421.8
$\frac{1}{4}$	2.7	421.5
$\frac{1}{2}$	2.6	421.6
$\frac{1}{4}$	2.9	421.3
cb.	3.0	421.2
+2	2.7	421.4
W	3.0	421.2
	0+00	
W	3.1	421.1
+8	2.7	421.5
cb.	3.2	421.0
$\frac{1}{2}$	3.0	421.2
$\frac{1}{4}$	2.8	421.4
$\frac{1}{4}$	2.7	421.5
cb.	2.4	421.8
+3	1.9	422.3
E	1.3	422.9
	0+50	
E	1.9	422.3
+8	2.1	422.1
cb.	3.1	420.5

$\frac{1}{4}$	3.8	420.4
$\frac{1}{2}$	3.8	420.4
$\frac{1}{4}$	4.2	420.0
cb.	4.9	419.3
+1	2.8	421.4
W	2.6	421.6
	0+81.45 = S.W. Gilbert on West.	
W	3.1	421.1
+8	3.0	421.2
cb.	4.9	419.3
$\frac{1}{4}$	5.3	418.9
$\frac{1}{2}$	4.7	419.5
$\frac{1}{4}$	4.8	419.4
cb.	4.7	419.5
+2	4.5	419.7
+4	3.0	421.2
E	3.0	421.2
	0+85	
E	3.1	421.1
+6	3.1	421.1
+9	4.5	419.7
cb.	4.5	419.7
$\frac{1}{4}$	4.8	419.4
$\frac{1}{2}$	4.9	419.3
$\frac{1}{4}$	5.5	418.7
cb.	5.5	418.7

424.16 ✓

N.		47	419.5
	1+18		
N		55	418.7
cb.		62	415.0
+5		71	417.1
$\frac{1}{2}$		68	417.4
$\frac{1}{4}$		66	417.6
$\frac{1}{2}$		65	417.7
cb		66	417.6
+3		57	418.6
E		60	418.2
+5		64	417.8
	1+21.45 = N.L. of Wood on N.		
-10		74	416.8
E		64	417.8
+6		59	418.3
cb.		67	417.5
$\frac{1}{2}$		67	417.5
$\frac{1}{4}$		67	417.5
$\frac{1}{2}$		71	417.1
+3		71	417.1
cb		59	418.3
+1		45	419.7
N		4.9	419.3
T.P	3.68 420.20	7.64	416.52
	1+40		

420.20 ✓

5545 st

17

N		2.0	418.2
-9		1.7	418.5
cb		3.8	416.4
$\frac{1}{2}$		4.1	416.1
$\frac{1}{4}$		3.6	416.6
$\frac{1}{4}$		3.6	416.6
cb.		3.5	416.7
E		6.3	413.9
+10		7.7	412.3
	1+60		
-30		10.6	409.6
-24		12.2	408.0
-23		13.8	406.4
-14		14.3	405.9
-9		12.4	407.8
E		11.6	408.6
cb.		5.0	415.2
$\frac{1}{2}$		4.5	415.7
$\frac{1}{4}$		4.4	415.8
$\frac{1}{2}$		4.7	415.5
cb.		5.5	414.7
+5		5.6	414.6
N		6.1	414.0
+10		1.3	412.9
	Levels for Gilbert see sketch Page 2		
	0700	1.46	407.6

42020 ✓

0+32	14.3	405.9
+43	12.5	407.7
+54	12.5	407.7
+69	5.3	414.9
+98	5.9	419.3
1402.32 = 10.41 cb. face 47.30 =	7.8	412.9
+13	14.8	405.4
+19	17.5	402.7
+28	19.7	400.5
+45 = 10.24	22.6	397.6
1+9.5		
-30	22.6	397.6
-7	17.5	402.7
Y	14.2	406.0
cb.	7.5	412.7
+2	6.7	413.5
$\frac{1}{2}$	5.5	414.7
$\frac{1}{2}$	5.0	415.2
$\frac{1}{2}$	5.2	415.0
+4	5.1	415.1
cb.	7.2	413.0
+7	11.2	409.0
5	11.9	408.3
+7	14.7	407.5
+20	9.2	411.0

2+35

42020 ✓

55th St

18

-15	4.0	416.2
5	4.3	415.9
cb	4.4	415.8
$\frac{1}{2}$	4.3	415.9
$\frac{1}{2}$	4.5	415.7
$\frac{1}{2}$	4.7	415.5
cb	4.8	415.4
Y	5.2	415.0
+10	5.0	415.2
2+50		
-10	8.0	418.2
Y	2.0	418.2
+8	2.2	418.0
cb.	4.0	416.2
$\frac{1}{2}$	4.5	415.7
$\frac{1}{2}$	4.2	416.0
$\frac{1}{2}$	4.1	416.1
+6	4.1	416.1
cb.	1.8	418.4
5	1.5	418.7
+5	1.5	418.7
3+00		
10.58 428.08	2.70	417.50
5	7.3	420.8
+6	7.6	420.5
cb.	10.1	418.0

42808 ✓

1		10.5	417.6
2		10.6	417.5
3		10.7	417.4
cb		10.6	417.5
+3		7.5	420.6
Y		7.6	420.5
	3+50		
Y		8.1	420.0
+8		7.9	420.2
cb		7.6	418.5
1/2		9.6	418.5
2		9.4	418.7
3/4		9.3	418.8
cb		9.0	419.1
+2		6.5	421.6
E		6.6	421.5
	4+00		
E		5.5	422.6
+8		6.2	421.9
cb		7.8	420.3
1/2		7.8	420.3
6		8.2	419.9
1/2		8.4	419.7
cb		8.8	419.2
+5		8.0	420.1
Y		8.4	419.7

42808 ✓

5519 st.

19

	4+50		
W		2.3	420.8
+5		7.0	421.1
cb		7.7	420.9
1/2		7.4	420.7
2		7.1	421.0
3/4		7.0	421.1
cb		6.7	421.4
+4		5.5	422.6
E		5.4	422.7
	5+00		
E		3.6	424.5
+8		4.0	424.1
cb		6.1	422.0
1/2		6.5	421.6
2		6.5	421.6
3/4		6.8	421.3
cb		6.9	421.2
+4		5.3	422.8
Y		5.3	422.8
	5+50		
Y		4.7	423.8
+8		3.4	424.9
cb		6.1	422.0
+4		7.1	421.0
1/2		7.4	420.9

42808 ✓

d	6.9	421.2
$\frac{1}{4}$	6.9	421.2
cb	6.0	422.1
+3	1.2	426.9
E	0.7	427.4
	G+00	
E	0.5	427.6
+8	1.0	427.1
cb	6.5	421.6
$\frac{1}{2}$	7.2	420.9
S	7.6	420.5
$\frac{1}{4}$	7.7	420.9
+5	7.5	420.6
cb	6.5	421.6
+2	4.6	423.5
+7	5.8	422.3
W	4.7	423.4
	G+15	
W	5.8	422.3
+5	6.6	421.5
cb	6.0	422.1
+3	8.0	420.1
$\frac{1}{4}$	7.9	420.2
$\frac{1}{2}$	7.7	420.4
$\frac{1}{4}$	7.6	420.5
+4	7.4	420.7

42808 ✓

55th St.

30

cb	6.4	421.7
+4	1.6	426.5
E	1.6	426.5
	G+19 = South edge Gen Dr. on E 1' back	
-4 on top DRIVE	4.8	424.70
E	5.1	423.0
+7	6.6	421.5
cb	6.8	421.3
$\frac{1}{2}$	7.5	420.6
$\frac{1}{4}$	7.7	420.4
$\frac{1}{4}$	8.0	420.1
+7	8.1	420.0
cb	7.2	420.9
+1	5.7	422.4
+6	6.6	421.5
W	5.3	422.8
	G+27 = North end #6 box DRIVE WAY	
W	6.3	421.8
+8	6.8	421.3
+8	5.9	422.2
cb	7.3	422.8
+4	8.2	419.9
$\frac{1}{4}$	8.0	420.1
$\frac{1}{2}$	7.9	420.2
$\frac{1}{4}$	7.7	420.4
cb	6.6	421.5

42808 ✓

E	49	423.2
+4 on Drive xly	437	423.21
6+30		
-5	10	427.1
E	1.8	426.3
+7	2.1	426.0
+9	3.2	424.9
cb.	6.7	421.4
+4	7.4	420.7
$\frac{1}{2}$	7.6	420.5
$\frac{1}{2}$	7.9	420.2
$\frac{1}{2}$	8.1	420.0
+5	8.2	419.9
cb.	7.1	421.0
+1	6.0	422.1
+5	6.9	421.2
N	6.1	422.0
6+50		
N	7.7	420.4
+3	8.0	420.1
+9	6.9	421.2
cb.	7.4	420.7
+3	8.8	419.3
$\frac{1}{2}$	8.6	419.5
$\frac{1}{2}$	8.1	420.0
$\frac{1}{2}$	7.9	420.2

42808 ✓

5515 st.

21

cb.	7.1	421.0
+3	3.6	424.5
E	2.8	425.3
6+57		
E	3.0	425.1
+5	4.1	424.0
cb.	8.3	419.8
$\frac{1}{2}$	8.4	419.7
$\frac{1}{2}$	8.8	419.3
$\frac{1}{2}$	9.0	419.1
+5	9.5	418.6
cb.	8.2	419.9
+3	7.6	420.5
+7	8.6	419.5
N	7.6	420.5
6+58.5 = Beginning Exist. cb. on SSB = 200' South of Station		(ONE)
N	8.8	419.3
+5 on Wedge of side walk.	8.9.5	419.13
cb. on top	9.01	419.07
Gut.	9.7	418.4
$\frac{1}{2}$	9.2	418.9
$\frac{1}{2}$	8.8	419.3
$\frac{1}{2}$	8.6	419.5
Gut	9.3	418.8
E top cb	8.54	419.36
$\frac{1}{2}$	8.0	420.1



428.08 ✓

TP Madison 1006 434.56 3.58 424.50  
 Chk. on B.M. NW top Piller 1.35  $\frac{433.21}{432.86} = 84.$   
 TP 8.61 440.18 2.99 431.57

400' North N.M. Madison = End of East Ch on West = 0+00

W 6.4 433.8  
 W top ch 6.64 433.54  
 Gut 7.3 432.9  
 $\frac{1}{4}$  6.7 433.5  
 $\frac{1}{2}$  6.4 433.8  
 $\frac{1}{4}$  6.2 434.0  
 +6 6.2 434.0  
 (No ch. on East)  
 ch. on ground 5.7 434.5  
 E 5.7 434.5  
 +2 2.7 437.3

0+20

-5 2.7 437.5  
 E 3.7 436.5  
 ch 4.9 435.3  
 $\frac{1}{4}$  5.7 434.5  
 +W 5.9 434.3  
 $\frac{1}{2}$  5.9 434.3  
 $\frac{1}{4}$  6.0 434.2  
 +3 6.3 433.9  
 ch 6.0 434.2  
 W 6.5 433.7

0+50

440.18 ✓

55th St

808

W 6.3 433.9  
 ch 6.1 434.1  
 $\frac{1}{2}$  6.0 434.2  
 $\frac{1}{4}$  5.6 434.6  
 $\frac{1}{2}$  5.3 434.9  
 ch 4.6 435.6  
 E 2.9 437.3  
 0+84 =  $\frac{1}{2}$  Cor. Walk and steps in E 27' side at home. 1.5' wide first.  
 E - 2 on top of Walk 2.83 437.35  
 -1 " " " step 3.33 436.85  
 E " " " " 3.83 436.35  
 +1 4.32 435.86  
 +5 on top Walk 4.81 435.35  
 +9 " " " = End. 5.21 434.97

1+13 =  $\frac{1}{2}$  Cor Ribbon Dr. on E

-10 on top Dr. 2.04 438.14  
 E " " " 3.69 436.49  
 ch " " " 5.70 434.48  
 $\frac{1}{4}$  5.8 434.4  
 $\frac{1}{2}$  6.1 434.1  
 $\frac{1}{4}$  6.3 433.9  
 ch 6.3 433.9  
 W 6.7 434.0

1+63

W 6.6 433.6  
 ch 6.5 433.7

44018 ✓

q	6.6	433.6
z	6.4	433.8
i	6.3	433.9
cb.	5.9	434.3
+7	5.3	434.9
E	4.3	435.9

10' chs this sb. should be 2+00  
 R+01 = S. Adams

E	5.1	435.1
cb.	6.1	434.1
i	6.4	433.8
z	6.6	433.6
i	6.9	433.3
+3	7.2	433.0
cb.	6.8	433.4
W	6.8	433.4

5 cb.

W	7.2	432.9
+6	7.7	432.5
cb.	7.2	433.0
i	6.8	433.4
to	6.7	433.5
i	6.5	433.7
cb	6.2	434.0
E	5.7	435.0

(South cb. + 5') = S. edge McAdams' Paving

E on Pavement. 7.8 434.4

44018 ✓

55th St

208

cb. on Pav.	6.1	434.1
i " "	6.3	433.9
z " "	6.5	433.7
i " "	6.7	433.5
cb " "	6.9	433.3
W " "	7.4	432.8

Adams + 55th  
 Put Spike in SW. Pole

E	4.1	435.77
---	-----	--------

For Future Reference

S 1/4 on Pav.

W	7.3	435.9
cb.	6.9	433.3
i	6.6	433.6
z	6.4	433.8
i	6.2	434.0
cb	6.1	434.1
E	5.5	434.7

S Adams on Pav.

E	5.3	434.8
cb	5.9	434.3
i	6.1	434.1
z	6.2	434.0
i	6.4	433.8
cb.	6.7	433.5
W	7.1	433.1

N 1/4 on Pav.

W	7.1	433.1
cb.	6.1	433.5

440.18 ✓

1/4	6.3	433.9
1/2	6.2	434.0
3/4	5.9	434.3
cb	5.8	434.4
E	5.3	434.9

(N 1/4 + 2') = N edge of Ravine on Adams

E on Pav	5.0	434.9
cb " "	5.8	434.4
1/4 " 4	6.0	434.2
1/2 " "	6.2	434.0
3/4 " "	6.3	433.9
cb " "	6.7	433.5
N " "	7.2	433.0

Ncb.

N	7.1	433.1
cb	6.6	433.6
1/4	6.1	434.1
1/2	5.9	434.3
3/4	5.8	434.4
cb	5.6	434.6
E	5.6	434.6

N.W. Adams - 0+100

E	18	438.4
+7	22	438.0
cb	53	434.9
1/4	56	434.6

440.18 ✓

1/4	5.6	434.6
1/2	5.8	434.4
cb	6.6	433.6
+2	5.8	434.4
N	6.2	435.0

0+50

N	3.0	437.2
+8	3.2	437.0
cb	3.8	436.4
+5 <sup>Wedge</sup> on Pav	3.6	436.6
1/4	3.5	436.7
1/2	3.3	436.9
3/4	3.2	437.0
+2	3.2	437.0

cb	3.5	436.7
+9	0.5	439.7
E	0.5	439.7
TP	8.23	443.93
4.48		435.70

15' North - 2' Pinus Palm Tree on N

46' " " " " " "

78' " " " " " "

110' " " " " " "

141' " " " " " "

173' " " " " " "

204' " " " " " "

235' " " " " " "

8.0

6.9

5.9

5.1

4.5

4.2

4.1

4.1

55th St.

24

435.19

437.1

438.0

438.8

439.4

439.7

439.8

439.8

6' tall

4' Back line

4' tall

5' Back

7' tall

5' Back

7' tall

5' Back

6' tall

5' Back

5' tall

5' to 11'

5' Back

5' to 11'

5' Back

44393

1+00

E	2.3	441.6
+6	2.8	441.1
+8	5.1	438.8
cb	5.5	438.4
+5 = east edge Pav.	5.3	438.6
$\frac{1}{4}$ on Pav.	5.3	438.6
$\frac{1}{6}$ " "	5.3	438.6
$\frac{1}{4}$ " "	5.7	438.2
+2 edge Pav.	5.7	438.2
cb	6.1	437.8
+2	5.2	438.7
W	5.3	438.6

1+50

W	4.2	439.7
+8	3.2	440.0
+9	4.9	439.0
cb	4.9	439.0
+5 = edge Pav.	4.7	439.2
$\frac{1}{4}$ on Pav.	4.6	439.3
$\frac{1}{6}$ " "	4.3	439.6
$\frac{1}{4}$ " "	4.3	439.6
+2 " " east edge	4.3	439.6
cb	4.4	439.5
+3	2.9	441.0
E	1.9	442.0

44393

2+00

E	2.1	441.8
cb	3.6	440.3
+5 = on Pav east edge	3.6	440.3
$\frac{1}{4}$ " "	3.6	440.3
$\frac{1}{6}$ " "	3.6	440.3
$\frac{1}{4}$ " "	3.8	440.1
+2 " " W "	3.8	440.1
cb	4.1	439.8
+1	3.6	440.3
W	3.8	440.1

2+50 = S.L. Collier st. on West. <sup>10' wide</sup> 5' chs 7.5'  $\frac{1}{4}$ S

W	3.9	440.0
+8	3.1	440.8
cb	3.9	440.0
+5 = W edge Pav.	3.8	440.1
$\frac{1}{4}$	3.6	440.3
$\frac{1}{6}$	3.3	440.6
$\frac{1}{4}$	3.3	440.6
+2	3.4	440.5
cb	3.1	440.8
+2	1.1	442.8
E	0.7	443.2
cb	0.6	443.3
+8	1.1	442.8

443.93 ✓

cb.		3.1	440.8	
+5 on Riv.		3.3	440.6	
$\frac{1}{4}$ " "		3.3	440.6	
$\frac{1}{4}$ " "		3.2	440.7	
$\frac{1}{4}$ " "		3.6	440.3	
+2 on "		3.8	440.1	
cb.		4.2	439.7	
W		4.5	439.4	
	5 $\frac{1}{4}$			
W		4.7	439.2	
cb.		4.1	439.8	
+5 on Riv.		3.7	440.2	
$\frac{1}{4}$ " "		3.5	440.4	
$\frac{1}{4}$ " "		3.2	440.7	
$\frac{1}{4}$ " "		3.3	440.6	
+2 " "		3.3	440.6	
cb.		3.0	440.9	
+1		1.1	442.8	
E		0.4	443.5	
J.P.	6.67	447.76	2.84	441.09
	L. Collier			
E		4.5	443.3	
+6		4.8	443.0	
cb.		6.5	441.3	
+5 on Riv.		7.1	440.7	
$\frac{1}{4}$		7.0	440.8	

447.76 ✓

55th St.

86

$\frac{1}{4}$ on Riv.		7.0	440.8
$\frac{1}{4}$ " "		7.3	440.5
+2		7.6	440.2
cb.		7.7	440.1
W		8.3	439.5
	N. $\frac{1}{4}$		
W		8.3	439.5
cb.		7.8	440.0
+5 on Riv.		7.6	440.2
$\frac{1}{4}$ " "		7.4	440.4
$\frac{1}{4}$ " "		7.1	440.7
$\frac{1}{4}$ " "		7.0	440.8
+2 " "		7.0	440.8
cb.		6.5	441.3
+3		4.7	443.1
E		4.4	443.4
	N. C. B.		
E		4.0	443.8
+7		4.4	443.4
cb.		6.8	441.0
+5		7.1	440.7
$\frac{1}{4}$ " "		7.0	440.8
$\frac{1}{4}$ " "		7.0	440.8
$\frac{1}{4}$ " "		7.3	440.3
+2		7.5	440.3
cb.		7.8	440.0

447.76 ✓

N	8.0	439.8
2+90 = N.L. Collier		
N	7.4	440.4
+8	7.2	440.6
cb	7.7	440.1
+5 on Pav	7.5	440.3
$\frac{1}{4}$ " "	7.2	440.6
$\frac{1}{2}$ " "	6.9	440.9
$\frac{1}{2}$ " "	6.9	440.9
+2 " "	7.0	440.8
cb	6.7	441.1
+3	4.1	443.7
E	3.8	444.0
3+20		
E	4.0	443.8
+7	4.5	443.3
cb	6.8	441.0
+5 on Pav	6.9	440.9
$\frac{1}{4}$ " "	7.0	440.8
$\frac{1}{2}$ " "	7.0	440.8
$\frac{1}{4}$ " "	7.2	440.6
+2 " "	7.4	440.4
cb	7.6	440.2
+1	6.7	441.1
N	7.7	440.6

447.76 -

55+5 st.

37

	3+50	
N	7.3	440.5
+9	6.8	441.0
cb	7.6	440.2
+5 on Pav	7.5	440.2
$\frac{1}{4}$ " "	7.4	440.4
$\frac{1}{2}$ " "	7.1	440.7
$\frac{1}{4}$ " "	7.1	440.7
+2 " "	7.1	440.7
+5	6.8	441.0
cb	6.1	441.7
+2	4.3	443.5
E	3.5	444.3
4+00		
E	3.7	444.1
+9	4.6	443.2
cb	6.3	441.5
+2	7.3	440.5
+5 on Pav	7.4	440.4
$\frac{1}{4}$ " "	7.4	440.4
$\frac{1}{2}$ " "	7.5	440.3
$\frac{1}{4}$ " "	7.6	440.2
+2 " "	7.9	439.9
cb	8.0	439.8
+2	6.7	441.1
N	7.5	440.3

447.76

4+50

W	80	439.8
+9	75	440.3
1 cb	83	439.5
+5 on Pav.	81	439.7
4 " "	80	439.8
2 " "	78	440.0
7 " "	78	440.0
+2 " "	78	440.0
cb	76	440.2
+4	49	442.9
E	44	443.4

5+00

E	52	442.6
+7	58	442.0
cb	77	440.1
+5 on Pav.	82	439.6
4 " "	82	439.6
2 " "	82	439.6
7 " "	85	439.3
+2 " "	86	439.2
+6	87	438.9
cb	84	439.4
W	90	438.8

5+50

-5	108	437.4
----	-----	-------

+47.76

55' 51"

38

W	97	438.1
cb	93	438.5
+5 on Pav.	91	438.7
4 " "	91	438.7
2 " "	87	439.1
2 " "	87	439.1
+2 " "	88	439.0
cb	85	439.3
+2	69	440.9
E	60	441.8

6+00

E	63	441.5
+8	74	440.4
cb	88	439.0
+5 on Pav.	91	438.7
2 " "	91	438.7
2 " "	91	438.7
4 " "	93	438.5
+2 " "	95	438.3
cb	97	438.1
+5	93	438.5
W	99	437.9
5	105	437.3

6+50

-5	106	437.2
W	100	437.8

447.76 ✓

+6	94	438.4
cb	95	438.3
+1	101	437.7
+5 on Pav.	98	438.0
1/4 " "	98	438.0
1/2 " "	96	438.2
1/2 " "	95	438.3
+2 " "	94	438.4
cb	89	438.9
+2	60	441.0
E	59	441.9

7+00 = PC. of Pav. to Rt.

E	62	441.6
+6	69	440.9
cb	94	438.4
+5 on Pav.	96	438.2
1/2 " "	97	438.1
1/2 " "	97	438.1
1/2 " "	99	437.9
+2	99	437.9
cb	98	438.0
W	102	437.6
+5	105	437.3

7+13

-5	107	437.1
W	104	437.4

447.76

55th St.

89

cb	97	438.1
+2	103	437.5
1/2	98	438.0
+2 on Pav.	96	438.2
1/2 " "	93	438.5
1/4 " "	92	438.6
cb " "	92	438.6
+1 on " "	92	438.6
+6	91	438.7
E	85	438.3

7+50

E	76	440.2
cb	83	439.5
1/4	86	439.2
1/2	92	438.6
1/4	99	437.9
cb	103	437.5
W	111	436.7
+5	116	436.2

Left B.M. on N.E. 1/4 Redland Dr.

TP	482	441.66	10.92	436.84
763' North = Cypress Trees on W			4.6	437.1
782' " " " " " "			5.9	436.4
800' " " " " " "			5.4	436.3
822' " " " " " "			6.9	434.8
842' " " " " " "			7.7	434.0
861' " " " " " "			9.4	432.3
901' " " " " " "			12.2	429.5

on edge of  
Walk.

54011 3rd St  
3' 10" St  
5' 10" St  
5' 12" St  
3' 10" St  
5' 10" St  
3' 12" St  
7' 5" St  
2' 5" St



441.66 ✓

	8+00		
N	53	436.4	
W	55	436.2	
cb	61	435.6	
1/2	61	435.6	
1/4	59	435.8	
1/4	59	435.8	
+5	60	435.7	
cb.	51	436.6	
E	43	437.4	
8+27 = 1/2 Con. Walk. on E 15' Wide 10' in W.			
E	620	435.46	
cb. on East end of Walk.	690	434.76	
+1	79	433.8	
1/4	76	434.1	
1/4	76	434.1	
1/4	78	433.9	
cb	81	433.6	
+2	71	434.6	
N	70	434.7	
Solid Con Apron Approach			
8+59 = South's edge Garage on E. Con Floor with			
N	70	432.7	
+7	92	432.5	
cb.	103	431.4	
1/4	102	431.5	
1/4	101	431.6	

441.66

55th St.

30

1/2	10.3	431.4	
cb.	10.0	431.7	
71.5 = toe of Apron	10.16	431.50	
E	9.94	431.72	
+1' on Floor Garage	9.78	431.88	
8+68 = North edge Phase Garage			
1' on Floor	9.83	431.83	
E " Apron	10.06	431.60	
+8" toe of Apron	10.17	431.49	
cb.	10.3	431.4	
1/2	10.6	431.1	
1/2	10.6	431.1	
1/2	11.0	430.7	
cb.	11.0	430.7	
N	10.0	430.7	
9+05.5 = North end 55th St.			
N-10	11.0	430.7	
N	12.5	429.2	
cb.	12.2	429.5	
1/2	12.4	429.3	
1/2	12.6	429.1	
1/4	12.8	428.9	
cb.	16.3	425.4	
+5	18.3	423.4	
E	18.6	423.1	
+20	19.2	422.5	

441.66 ✓

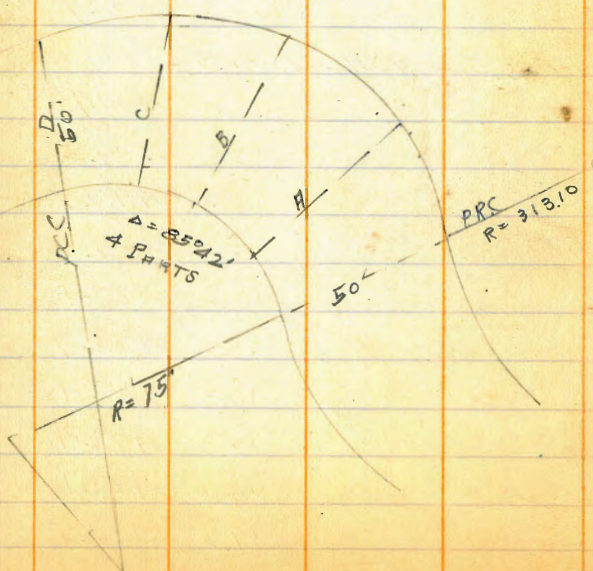
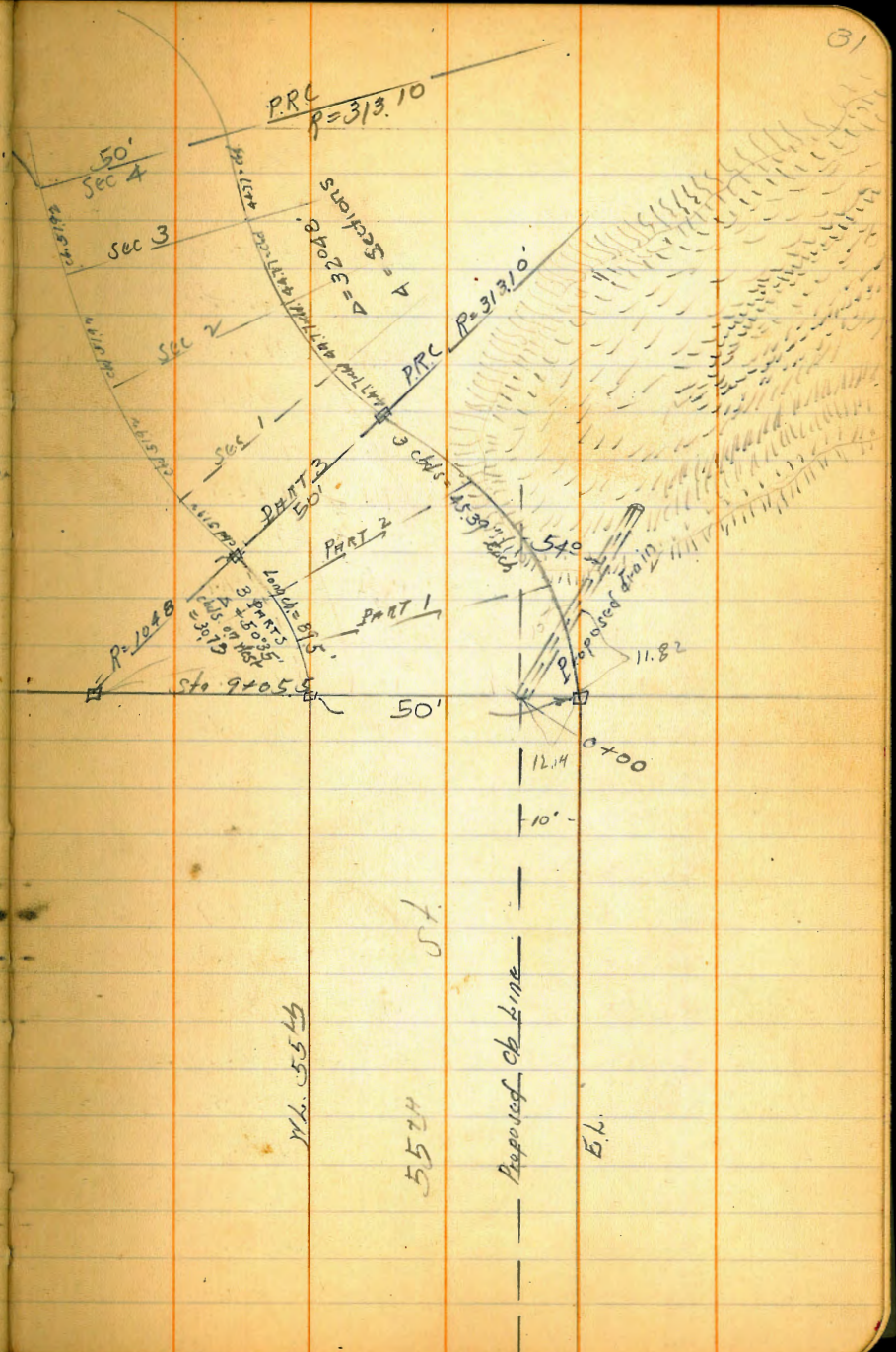
Levels For Drain

0+00	17.2	424.5
+15	21.7	420.0
+30	26.0	415.7
+45	30.5	411.2
T.P.	26.3	427.58
	1.71	439.95
chk. on Nat. in Pole page 23	6.81	435.77 ✓
T.P.	3.42	436.07
	9.93	432.65
chk. on N.Y. & M. Medicines + U.S. 2.89		433.18
		433.22
		0.04

55th St. Cont. page 32

top of Pillo

31



Walker  
Repl. 1998  
chea 3-2-28

X Section 55th St. 50' wide 10' chs. 1.45  
From Station 9+05.5 Page 81  
HS Per Sketch " "

B.M. Page 29  
on Can. Walk

126 441.62 ✓ 440.36

PART 1

-40	34.3	407.3
-25	30.8	410.8
E	26.3	415.3
+6	25.0	416.6
cb	23.4	418.2
$\frac{1}{4}$	19.1	422.5
$\frac{1}{2}$	15.1	426.5
+5	12.5	429.1
$\frac{1}{4}$	12.2	429.4
cb	12.1	429.5
Y	12.0	429.6
+4	12.0	429.6
+10	11.7	429.9

PART 2

-10	8.7	432.9
-6	9.3	432.3
-4	11.1	430.5
Y	11.3	430.3
cb	11.1	430.5
$\frac{1}{4}$	10.7	430.9
+3	10.9	430.7
$\frac{1}{2}$	10.7	428.9
$\frac{1}{4}$	16.3	425.3

441.62 ✓

318

cb	18.4	423.2
E	22.1	419.5
+10	25.0	416.6
+25 (Slope Grade continues)	29.6	412.0

PART 3 - P.R.C.

-35	22.6	419.0
-21	18.2	423.4
-13	16.1	425.5
-5	15.3	426.3
E	13.3	428.3
+1	12.5	429.1
cb	11.0	430.6
+5	10.4	431.2
$\frac{1}{2}$	9.6	432.0
+3	8.8	432.8
$\frac{1}{4}$	8.9	432.7
$\frac{1}{2}$	9.3	432.3
cb	9.6	432.0
+5	9.7	431.9
Y	6.2	438.4
+Y	5.3	436.3
+10	4.6	437.0

Section 1

-10	2.8	438.8
Y	3.4	438.4
cb	3.1	437.9

44162 ✓

+3	4.1	437.5
$\frac{1}{2}$	5.3	436.3
+3	7.6	434.0
$\frac{1}{2}$	1.5	434.1
$\frac{1}{2}$	7.1	434.5
cb.	6.6	435.0
+5	6.6	435.0
E	8.6	433.0
+10	10.6	431.0
+20	13.0	425.6
+30	16.5	425.1

## Section 2

-25	11.3	430.3
-13	9.1	432.5
-7	6.3	435.3
-3	5.3	436.3
E	4.9	436.7
cb.	5.1	436.5
$\frac{1}{2}$	5.5	436.1
+6	5.6	436.0
$\frac{1}{2}$	5.0	436.6
+5	3.3	438.3
$\frac{1}{2}$	3.0	438.6
cb.	2.7	438.9
Y	2.2	439.4
+10	1.8	439.8

44162

5519

33

TP	8.13	446.07	36.8	4379.4
Section 3				

-10			5.4	440.7
Y			5.7	440.4
cb.			5.9	440.2
$\frac{1}{2}$			6.1	440.0
+2			6.5	439.6
$\frac{1}{2}$			8.2	437.9
$\frac{1}{2}$			8.2	437.9
cb.			7.9	438.2
E			7.7	438.4
+25			12.6	433.5

## Section 4 = P.R.C

-10			7.5	438.6
E			6.7	439.4
cb.			6.3	439.8
$\frac{1}{2}$			6.5	439.6
$\frac{1}{2}$			6.7	439.4
$\frac{1}{2}$			7.0	439.1
+2			7.0	439.1
+5			5.4	440.7
cb.			5.4	440.7
Y			4.9	441.2
+10			4.6	441.5

## Section A

-10			4.7	441.4
-----	--	--	-----	-------

44607 ✓

NY	4.7	441.4
+8	5.0	441.1
cb	6.1	440.0
$\frac{1}{2}$	6.0	440.1
$\frac{1}{2}$	5.5	440.6
$\frac{1}{2}$	5.3	440.8
cb	5.3	440.8
E	5.6	440.5
+10	5.9	440.2

## Section B

-10	5.3	440.8
E	4.7	441.4
cb	4.5	441.6
$\frac{1}{2}$	5.0	441.1
$\frac{1}{2}$	5.3	440.8
$\frac{1}{2}$	5.7	440.4
cb	5.9	440.2
+5	6.0	440.1
+8	4.1	442.0
NY	4.0	442.1
+10	4.0	442.1

## Section C

-10	5.0	441.1
-2	5.0	441.1
NY	6.5	439.6
cb	6.3	439.8

44607 ✓

55th

34

$\frac{1}{2}$	5.9	440.2
$\frac{1}{2}$	5.6	440.5
$\frac{1}{2}$	5.1	441.0
cb	5.1	441.0
E	4.9	441.2
+10	4.7	441.4

## Section D = PCC

-10	7.2	438.9
E	6.7	439.4
cb	6.4	439.7
$\frac{1}{2}$	6.3	439.8
$\frac{1}{2}$	6.8	439.3
$\frac{1}{2}$	6.9	439.2
cb	7.1	439.0
NY	7.3	438.8
+3	7.3	438.8
+5	6.0	440.1
+10	5.8	440.3

Page 29  
chk. on BM NE. Cor. Redl. of 155th

5.71 440.36  
440.36 = BM  
0.00

Walker  
Topography  
Chart  
Sheet

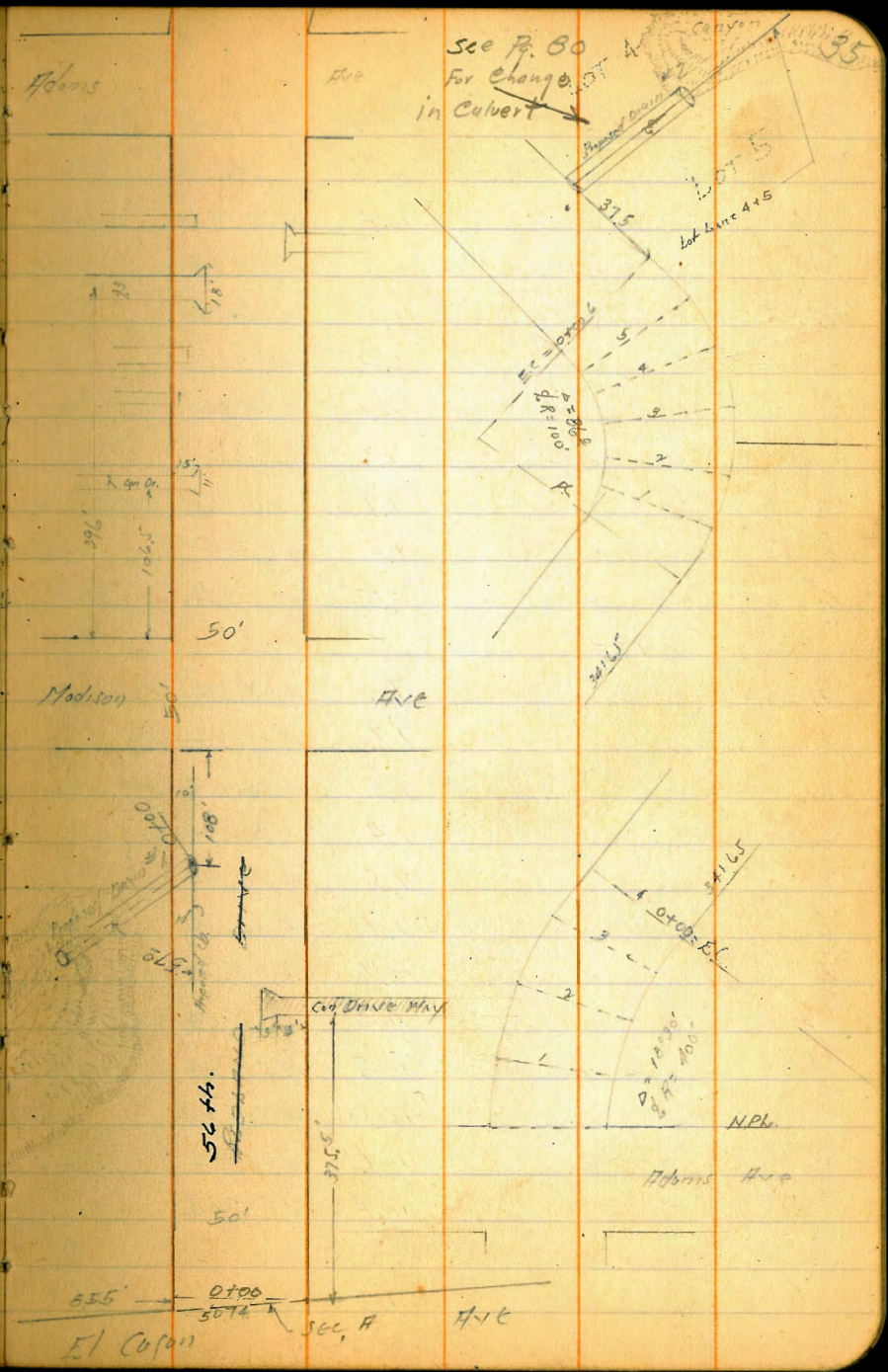
X. Section Redland Drive 50' Wide 10' cbs  
from El Cajon Ave to N.W. Terminaton

	11.57	434.35	422.78
TP	13.04	445.84	432.80
Section #			
-5		11.6	434.24
X		11.2	434.64
cb		11.0	434.84
+5 - Wedge NE Polarized Sw		10.7	435.14
$\frac{1}{4}$ - on Pav.		10.6	435.24
$\frac{1}{2}$ " "		10.5	435.34
$\frac{3}{4}$ " "		10.5	435.34
+2 " "		10.0	435.84
cb		9.7	436.14
E		8.7	437.14
0+100			
E		8.7	437.14
cb		9.7	438.14
+5 on Pav		10.0	435.84
$\frac{1}{2}$ " "		10.1	435.74
$\frac{1}{4}$ " "		10.4	435.44
$\frac{1}{8}$ " "		10.6	435.24
+2 " "		10.6	435.24
cb		10.8	435.04
X		10.9	434.94
+5		11.3	434.54

Yamoge  
A-18-25  
H. H. Hurling

0+100

0+20



-5	11.2	435.64
W	10.6	435.24
+7	10.4	435.44
cb.	10.6	435.24
+5 = Pav	10.5	435.34
$\frac{1}{4}$ on "	10.2	435.64
$\frac{1}{2}$ " "	10.0	435.84
$\frac{1}{2}$ " "	9.8	436.04
+2 " "	9.7	436.14
cb.	9.4	436.44
E	8.5	437.34
	0+35	
E	7.5	438.34
+6	7.7	438.34
cb.	7.5	436.34
+5 on Pav	7.4	436.44
$\frac{1}{2}$ " "	7.5	436.34
$\frac{1}{2}$ " "	9.7	436.14
$\frac{1}{4}$ " "	10.1	435.74
+2 " "	10.3	435.54
+6	10.5	435.34
cb.	10.0	435.84
W	10.6	435.24
+5	10.8	435.04
	0+85	
-5	9.5	436.34

W	9.2	436.84
+9	8.8	437.04
cb.	7.1	436.74
+5 on Pav.	8.9	436.94
$\frac{1}{2}$ " "	8.7	437.14
$\frac{1}{2}$ " "	8.5	437.34
$\frac{1}{2}$ " "	8.4	437.44
+2 " "	8.4	437.44
+6	8.3	437.54
cb.	8.0	437.84
+2	7.0	438.84
E	6.1	439.74
0+95 = d. Con W/4 on E	5.94	439.90
1+24 = $\frac{1}{16}$ Con Dr. on E 1' Back		
E - 1 on top Dr.	5.67	440.17
E	5.7	440.14
+7	6.2	439.64
cb.	7.8	438.04
+5 on Pav.	7.8	438.04
$\frac{1}{4}$ " "	7.8	438.04
$\frac{1}{16}$ " "	7.8	438.04
$\frac{1}{2}$ " "	8.0	437.84
+2 " "	8.1	437.74
cb.	8.2	437.64
W	8.1	437.84
+5	8.6	437.24

4' Wide  
2.0 in St.

44584

1+74

-5	7.9	438.54
11	7.0	438.84
cb	6.8	439.04
+5 on Pay	6.8	439.04
1/4 " "	6.7	439.14
1/6 " "	6.7	439.14
1/4 " "	6.7	439.14
+2 " "	6.7	439.14
+5	7.0	438.84
cb	6.4	439.34
+1	5.2	440.64
E	4.6	441.24
2+00		
E	3.7	442.14
+8	4.3	441.54
cb	6.0	439.84
+5 on Pay	5.9	439.94
1/4 " "	5.9	439.94
1/6 " "	6.0	439.84
1/4 " "	6.1	439.74
+2 " "	6.2	439.64
cb	6.3	439.54
+3	5.9	439.94
11	6.1	439.74
+5	6.6	439.24

44584.

REDBANDS DR.

67

2+50

-5	4.9	440.94
11	4.5	441.34
18	4.4	441.44
cb	4.9	440.94
+5 on Pay	4.8	441.04
1/4 " "	4.7	441.14
1/6 " "	4.6	441.24
1/4 " "	4.6	441.24
+2 " "	4.6	441.24
+5	5.0	440.84
cb	4.4	441.44
+2	2.9	442.94
E	2.2	443.64
TP	968	45113
3+00		
E	5.2	445.93
+7	5.9	445.23
cb	8.1	443.03
+5 on Pay	8.4	442.73
1/4 " "	8.5	442.63
1/6 " "	8.5	442.63
1/4 " "	8.6	442.53
+2 " "	8.7	442.43
cb	8.9	442.23
+1	8.5	442.63



451.13

W	8.7	442.43
+5	9.0	442.13
	3+37	
-5	8.9	442.23
W	8.5	442.63
+9	8.1	443.03
cb	8.3	442.83
+5 on Pay	8.1	443.03
$\frac{1}{4}$ " "	8.0	443.13
$\frac{1}{2}$ " "	7.8	443.33
$\frac{1}{4}$ " "	7.8	443.33
+2 " "	7.8	443.33
cb	7.6	443.53
+2	6.3	444.83
E	5.1	446.03
	3+44	
E	5.2	445.93
cb	7.5	443.63
+5 on Pay	7.6	443.53
$\frac{1}{4}$ " "	7.7	443.43
$\frac{1}{2}$ " "	7.7	443.43
$\frac{1}{4}$ " "	7.9	443.23
+2	8.0	443.13
cb	8.1	443.03
W	8.5	442.63
+5	9.0	442.13

451.13

Redland Dr.

98

3+80 = 2. Con. Dr. on E 15' in st. see sketch Page 35

-5	8.6	442.53
W	8.3	442.83
+9	7.7	443.43
cb	8.1	443.03
+5 on Pay	7.9	443.23
$\frac{1}{4}$ " "	7.7	443.43
$\frac{1}{2}$ " "	7.6	443.53
$\frac{1}{4}$ " "	7.5	443.63
+2 on Drive Way	7.49	443.64
cb " " "	7.70	443.43
E " " "	5.36	445.77
+20 " " "	0.7	451.06
	4+20	
E	5.0	446.13
cb	7.2	443.93
+5 on Pay	7.4	443.73
$\frac{1}{4}$ " "	7.4	443.73
$\frac{1}{2}$ " "	7.6	443.53
$\frac{1}{4}$ " "	7.7	443.43
+2 " "	7.7	443.43
cb	7.9	443.23
W	8.1	443.03
+5	8.5	442.63
	4+27	
-5	8.5	442.63

451.13

IV	81	443.03
cb	79	443.23
+5 on Pay	77	443.43
1/2 " "	72	443.43
1/2 " "	76	443.53
1/2 " "	74	443.73
+2 " "	74	443.73
cb	71	444.03
+3	53	445.83
E	50	446.13
	4+60	
E	48	446.33
+8	52	445.93
cb	74	443.73
+5 on Pay	77	443.43
1/2 " "	77	443.43
1/2 " "	77	443.43
1/2 " "	79	443.23
+2 " "	79	443.23
cb	80	443.13
IV	75	443.33
+5	81	443.03
	5+00	
-5	92	441.93
IV	89	442.23
cb	85	442.63

451.13

Redford Dr.

89

+5 on Pay	84	442.73
1/2 " "	83	442.83
1/2 " "	82	442.93
1/2 " "	81	443.03
+2 " "	81	443.03
cb	78	443.33
+3	54	445.73
E	47	446.43
	5+50	
E	60	445.13
+8	67	444.43
cb	85	442.63
+5 on Pay	87	442.43
1/2 " "	87	442.43
1/2 " "	87	442.43
1/2 " "	89	442.23
+2 " "	90	442.13
cb	90	442.13
IV	92	441.93
+10	108	440.33
	6+00	
-15	144	436.73
-5	123	438.83
IV	96	441.53
cb	99	441.23
+5 on Pay	96	441.53
1/2 " "	95	441.63

2 on Pav	95	441.63
1/4 " "	92	441.93
+2 " "	91	442.03
cb	91	442.03
+2	79	443.23
E	72	443.93
6+50		
E	77	443.43
cb	93	441.83
+5 on Pav	94	441.73
1/4 " "	94	441.73
2 " "	98	441.33
1/4 " "	102	440.93
+2 " "	103	440.83
cb	105	440.63
W	110	440.13
+10	144	436.73
+20	153	435.83
6+75		
-20	125	438.63
W	108	440.33
cb	104	440.73
+5 on Pav	105	440.63
1/4 " "	103	440.83
1/4 " "	104	440.93
1/4 " "	99	441.23

2 on Pav	98	441.33
cb	94	441.73
E	77	443.43
Levels for Drains 1 Page 35		
0+00 = W cb line Redlands Dr.	10.3	440.83
+26	122	438.93
+38	18.8	432.33
+53	24.1	427.03
+59	27.1	424.03
7+00		
E	80	443.13
cb	96	441.53
+5 on Pav	100	441.13
1/4 " "	100	441.13
1/4 " "	101	441.03
1/4 " "	102	440.93
+2 " "	103	440.83
cb	102	440.93
W	102	440.93
+5	107	440.43
7+33 = 1/2 Acacia Tree on W 7' incl.	92	441.93
+52 " " " " " "	84	442.73
+72 " " " " " "	75	443.63
+89 " " " " " "	69	444.23
7+64 = 1/2 Con. Walk on W 6' incl.	7.89	443.24
7+50		

35' wide

45113

-5	84	442.73
W	83	442.83
cb	86	442.53
+5 on Pay	84	442.73
1/4 " "	82	442.93
1/2 " "	80	443.13
1/4 " "	78	443.33
+2 " "	78	443.33
cb	80	443.13
+2	71	444.03
E	65	444.63
7+94.7 = S.W. Madison Ave 50' Wide		
E	45	446.63
+8	50	446.13
cb	63	444.83
+2	68	444.33
+5 on Pay	63	444.83
1/4 " "	63	444.83
1/2 " "	63	444.83
1/4 " "	65	444.63
+2	66	444.53
cb	69	444.23
W	68	444.33
T.P.	1293 457.57	649 444.64
SL +8'		
W	129	444.67

45757

Redlund Dr.

41

cb	131	444.47
+5 on Pay	128	444.77
1/2 " "	126	444.97
1/2 " "	124	445.17
1/2 " "	124	445.17
+2 " "	124	445.17
cb	127	444.87
W	122	445.37
+5	110	446.57
E	107	446.87
5 cb		
E	119	445.67
cb	126	444.97
+5 on Pay	124	445.17
1/2 " "	123	445.27
1/2 " "	124	445.17
1/2 " "	126	444.97
+2 " "	128	444.77
cb	130	444.57
W	132	444.37
5 1/2		
W	128	444.77
cb	125	445.07
+5 on Pay	125	445.07
1/2 " "	124	445.17
1/2 " "	122	445.37

457.57

1/4 on Pav	121	445.47
+2 "	122	445.37
cb.	119	445.67
E	113	446.27
	1	
E	112	446.37
cb.	119	445.67
+5 on Pav	120	445.57
1/4 " "	119	445.67
1/2 " "	119	445.67
1/4 " "	121	445.47
+2 " "	122	445.37
cb.	123	445.27
"	124	445.17
"	124	445.17
cb.	120	445.57
+5 on Pav	118	445.77
1/2 " "	117	445.87
1/2 " "	116	445.97
1/4 " "	116	445.97
+2 " "	117	445.87
cb.	114	446.17
E	111	446.47
E	109	446.67

457.57

Reckoned Dr.

42

cb.	111	446.47
+5 on Pav	113	446.27
1/2 " "	114	446.17
1/2 " "	114	446.17
1/2 " "	115	446.07
+2 " "	116	445.97
cb.	119	445.67
"	125	445.07
		N.C. +2'
"	113	446.27
+8	110	446.57
cb.	120	445.57
+5 on Pav.	116	445.97
1/2 " "	112	446.17
1/2 " "	113	446.27
1/2 " "	112	446.37
+2 " "	112	446.37
cb.	111	446.47
+3	110	446.57
+5	95	448.07
E	94	448.17
		N.L. Madison = 0+00
E	88	448.77
+8	93	448.27
cb.	114	446.17
+5	109	446.67

457.57

$\frac{1}{2}$ on Pav.	109	446.67
$\frac{1}{2}$ " "	109	446.67
$\frac{1}{4}$ " "	11.2	446.37
+2 " "	11.3	446.27
cb.	11.6	445.97
+2	10.3	447.27
W	10.6	446.97
	0+50	
W	7.5	450.07
+8	7.3	450.27
cb	8.5	449.07
+5 on Pav.	8.4	449.37
$\frac{1}{2}$ " "	8.1	449.47
$\frac{1}{4}$ " "	8.0	449.57
$\frac{1}{4}$ " "	8.1	449.47
+2 " "	8.2	449.37
cb.	8.3	449.27
+3	5.8	451.77
E	3.2	452.37
	0+75	
E	4.6	452.97
+8	4.8	452.77
cb	6.4	451.17
+2	7.7	449.87
+5 on Pav.	6.8	450.77
$\frac{1}{4}$ " "	6.8	450.77

457.57

Redwood Dr.

43

$\frac{1}{2}$ on Pav.	6.8	450.77
$\frac{1}{4}$ " "	6.9	450.67
+2 " "	6.9	450.67
cb	7.1	450.47
+2	5.4	452.17
W	5.5	452.07
	1+10 = $\frac{1}{2}$ Drive Way on West	see sketch Page 35
W on Drive	4.5	453.06
cb. " "	5.58	452.99
+5 " "	5.23	452.34
$\frac{1}{4}$ on Pav	5.2	452.37
$\frac{1}{4}$ " "	5.0	452.57
$\frac{1}{4}$ " "	5.0	452.57
+2 " "	5.0	452.57
cb.	5.2	452.37
+2	3.6	453.97
E	3.2	454.37
	1+50	
E	1.5	456.07
+8	2.0	455.57
cb	3.1	454.47
+5 on Pav	3.0	454.57
$\frac{1}{4}$ " "	3.0	454.57
$\frac{1}{4}$ " "	3.2	454.37
$\frac{1}{4}$ " "	3.3	454.27
+2 " "	3.4	454.17

457.57

cb	3.8	453.77
+2	3.1	454.47
W	29	454.67
	1+25	
W	15	456.07
+8	20	455.57
cb	30	454.57
+5 on Pav	27	454.87
$\frac{1}{4}$ " "	26	454.97
$\frac{1}{2}$ " "	25	455.07
$\frac{1}{4}$ " "	24	455.17
+2 " "	25	455.07
cb	25	455.07
+2	17	455.87
E	13	456.27
	2+00	
E	0.8	456.77
+9	0.8	456.77
cb	19	455.67
+5 on Pav	20	455.57
$\frac{1}{4}$ " "	20	455.57
$\frac{1}{2}$ " "	21	455.47
$\frac{1}{4}$ " "	23	455.27
+2 " "	24	455.17
cb	25	455.07
+2	1.8	455.77

457.57

Redland Dr.

44

W	1.6	455.97
T.P	495	460.63
	2+50	
W	4.4	456.23
+8	4.6	456.03
cb	5.0	455.63
+5 on Pav	5.0	455.63
$\frac{1}{4}$ " "	4.9	455.73
$\frac{1}{2}$ " "	4.8	455.83
$\frac{1}{4}$ " "	4.8	455.83
+2 " "	4.8	455.83
cb	4.7	455.93
+1	3.3	457.33
E	3.3	457.33
	3+00	
E	4.3	456.33
+9	4.4	456.23
cb	5.0	455.63
+5 on Pav	5.1	455.53
$\frac{1}{4}$ " "	5.0	455.63
$\frac{1}{2}$ " "	5.0	455.63
$\frac{1}{4}$ " "	5.2	455.43
+2	5.2	455.43
cb	5.4	455.23
+2	4.9	455.73
W	4.6	456.03

460.63

3+50

W	51	455.53
+6	52	455.43
cb	57	454.93
+5 on Pav.	57	454.93
$\frac{1}{2}$ " "	57	454.93
$\frac{1}{2}$ " "	56	455.03
$\frac{1}{2}$ " "	55	455.13
+2 " "	56	455.03
cb	55	455.13
+1	45	456.13
E	42	456.43
3+57 = <sup>Con</sup> Walk east 7' inst	497	455.66
3+68 = <sup>Con</sup> Drive on West		
E	45	456.13
+8	50	455.63
cb	57	454.93
+5 on Pav.	59	454.73
$\frac{1}{2}$ " "	59	454.73
$\frac{1}{2}$ " "	59	454.73
$\frac{1}{2}$ " "	60	454.63
+2 " "	60	454.63
+5 = toe of Opion to Drive way	585	454.78
cb on Drive way	560	455.03
+4 " " "	525	455.38
W " " "	528	455.35

35' wide

460.63

Redland Dr.

45

3+74 = Cypress Hedge on W 10' inst Running East + West

3+96 = <sup>Con</sup> Dr. on W 9' wide

W on Drive way	625	454.38
+5 " " "	616	454.47
cb " " "	625	454.38
+2 " " "	643	454.20
+4 " " " = toe	636	454.27
+5 on Pav.	638	454.25
$\frac{1}{4}$ " "	63	454.33
$\frac{1}{2}$ " "	62	454.43
$\frac{1}{2}$ " "	62	454.43
+2 " "	62	454.23
cb	63	454.33
+2	51	455.53
E	47	455.93
4+22 = <sup>Con</sup> Walk on W 9.5' inst	644	454.19
4+11 = <sup>Con</sup> Palm tree on W 5' inst	61	454.53
4+34 = " " " " " " "	65	454.13
4+50 = <sup>Con</sup> ? tree on West 3" dia. 10' tall		
E	58	454.83
+8	60	454.63
cb	72	453.43
+5 on Pav.	70	453.63
$\frac{1}{2}$ " " "	69	453.73
$\frac{1}{2}$ " " "	71	453.53
$\frac{1}{4}$ " " "	73	453.33



46063

+7	7.4	453.23
cb	7.5	453.13
+2	6.9	453.73
+5 = 9" tree	6.9	453.73
W	6.5	454.13
4+79.5 = 2" dia drive on E	7' Wide	
W	7.4	453.23
+8	7.5	453.13
cb	8.1	452.53
+5 on Pav.	7.8	452.83
7 " "	7.7	452.93
1 " "	7.5	453.13
7 " "	7.4	453.23
+2 " drive way	7.45	453.18
cb " " "	7.43	453.20
+6 " " "	6.25	454.38
E " " "	6.17	454.46
5+25 = 1/2" Tree on W 4" dia 5' inst.		
E	6.6	454.03
+9	7.1	453.53
cb	8.1	452.53
+5 on Pav.	8.1	452.53
7 " "	8.0	452.63
1 " "	8.1	452.53
7 " "	8.2	452.43
+2 " "	8.5	452.13

46063

Redland Dr.

46

cb	8.6	452.03
+2	8.2	452.43
+5 = tree	8.2	452.43
W	8.2	452.43
5+50		
W	8.3	452.33
+8	8.4	452.23
cb	8.9	451.73
+5 on Pav	8.6	452.03
7 " "	8.5	452.13
1 " "	8.4	452.23
7 " "	8.5	452.13
+2 " "	8.5	452.13
cb	8.4	452.23
+2	7.6	453.03
E	7.4	453.23
6+00 = S.W. Adams Ave		10" cb 7.5 4.5
E	7.9	452.73
+8	8.3	452.33
cb	9.0	451.63
+5 on Pav	9.0	451.63
7 " "	9.0	451.63
1 " "	9.1	451.53
7 " "	9.2	451.43
+2 " "	9.4	451.23
cb	9.8	450.83

+2	92	451.43
W	90	451.63
S. Adams + 8'		
W	90	451.63
+8	93	451.33
cb	97	450.73
+1 on Pav.	76	451.03
1/2 " "	93	451.33
1/2 " "	91	451.53
1/2 " "	91	451.53
+5 " "	92	451.43
cb	90	451.63
+3	82	452.43
E	82	452.43
S cb		
E	89	451.73
cb	93	451.33
+2 on Pav.	93	451.33
1/2 " "	91	451.53
1/2 " "	91	451.53
1/2 " "	94	451.23
cb " "	96	451.03
W	98	450.83
S 1/2		
W on Pav.	99	450.73
cb " "	95	451.13

1/2 on Pav.	92	451.43
1/2 " "	92	451.43
1/2 " "	91	451.53
cb " "	91	451.53
E " "	90	451.63
1/2		
E on Pav.	90	451.63
cb " "	90	451.63
1/2 " "	91	451.53
1/2 " "	92	451.43
1/2 " "	92	451.43
cb " "	95	451.13
W " "	98	450.83
N 1/2		
W on Pav.	100	450.63
cb " "	96	451.03
1/2 " "	92	451.43
1/2 " "	92	451.43
1/2 " "	92	451.43
cb " "	91	451.53
E " "	91	451.53
N cb		
E	91	451.53
cb	93	451.33
+5 on Pav.	92	451.43
1/2 " "	91	451.53

L on Pav	92	451.43
1/4 "	93	451.33
cb "	96	451.03
+1 "	97	450.93
W	10.4	450.23
Ncb +2		
W	9.5	451.13
+7	9.4	451.23
cb	97	450.93
+2 on Pav	95	451.13
1/4 " "	92	451.43
1/2 " "	91	451.53
1/4 " "	91	451.53
+2 " "	91	451.53
cb	92	451.43
+2	8.5	452.13
E	7.9	452.73
N.L. Adonis = 0+00 = PC. 84.18°30'		
E	8.1	452.53
+9	8.3	452.33
cb	91	451.53
+5 on Pav	92	451.43
1/4 " "	92	451.43
1/2 " "	92	451.43
1/4 " "	92	451.43
+2 " "	94	451.23

Ncb +2

N.L. Adonis = 0+00 = PC. 84.18°30'

*Yardage*  
*4/23/89*

cb	99	450.73
W	92	451.43
PART 1		
W	8.9	451.73
cb	9.5	451.13
+5 on Pav	9.4	451.23
1/4 " "	9.3	451.33
1/2 " "	9.3	451.33
1/4 " "	9.2	451.43
+2 " "	9.2	451.43
cb	92	451.43
+2	8.6	452.03
E	8.1	452.53
(Part 1) +2.6 =	8.8	451.65
Redd Property line = 6.00 on W 15' inst. 4' wide		
PART 2		
E	8.0	452.63
+9	8.2	452.43
cb	9.3	451.33
+5 on Pav	9.3	451.33
1/4 " "	9.3	451.33
1/2 " "	9.3	451.33
1/4 " "	9.3	451.33
+2 " "	9.4	451.23
cb	9.3	451.33
W	8.7	451.93
PART 3		

46063

Y		85	452.13
+8		88	451.83
cb.		95	451.13
+5 on Pav		95	451.13
$\frac{1}{4}$ " "		94	451.23
$\frac{1}{2}$ " "		94	451.23
$\frac{1}{2}$ " "		95	451.13
+2 " "		94	451.23
cb		94	451.23
+3		86	452.03
E		87	452.43
PART 4 = E.C. = 0+00			
E		82	452.43
+9		84	452.23
cb.		93	451.33
+5 on Pav		97	450.93
$\frac{1}{4}$ " "		96	451.03
$\frac{1}{2}$ " "		96	451.03
$\frac{1}{4}$ " "		95	451.13
+2 " "		94	451.23
cb. " "		88	451.83
Y		86	452.03
T.P.	373 45520	936	451.27
0+28 =	Macia Tree on W	38	451.40
+45 =	" " " "	39	451.30
+63 =	" " " "	37	451.50

3" dia  
7' 10" st.

45520 Redland Dr.

49

			0+50
Y		29	452.30
cb		43	450.90
+5 on Pav		42	451.00
$\frac{1}{4}$ " "		43	450.90
$\frac{1}{2}$ " "		43	450.90
$\frac{1}{2}$ " "		44	450.80
+2 " "		44	450.80
+6		42	451.00
cb.		31	452.10
E		31	452.10
0+77 2' Cor Walk on Y			
		255	452.65 1.5' Back
			1+00
E		36	451.60
+8		40	451.20
cb.		44	450.80
+5 on Pav		45	450.70
$\frac{1}{4}$ " "		44	450.80
$\frac{1}{2}$ " "		44	450.80
$\frac{1}{4}$ " "		44	450.80
+2 " "		45	450.70
cb.		42	451.00
+1		29	452.30
Y		26	452.60
			1+50
Y		27	452.50

455.20

+8	30	452.20
cb	46	450.60
+5 on Pav	47	450.50
$\frac{1}{4}$ " "	46	450.60
$\frac{1}{2}$ " "	46	450.60
$\frac{1}{4}$ " "	47	450.50
+2 " "	47	450.50
cb	47	450.50
+2	40	451.20
E	45	450.70
+5	49	450.30
2+00		
-5	60	449.20
E	56	449.60
cb	54	449.80
+5 on Pav	51	450.10
$\frac{1}{4}$ " "	51	450.10
$\frac{1}{2}$ " "	49	450.30
$\frac{1}{4}$ " "	50	450.20
+2 " "	50	450.20
cb	52	450.00
+2	30	452.20
W	25	452.70
2+50		
W	33	451.90
+8	38	451.40

455.20 Redland Dr.

50

cb	62	449.00
+5 on Pav	61	449.10
$\frac{1}{4}$ " "	60	449.20
$\frac{1}{2}$ " "	60	449.20
$\frac{1}{4}$ " "	61	449.10
+4 " "	61	449.10
cb	60	449.20
E	64	448.80
+5	70	448.20
3+00		
-10	93	445.90
E	81	442.10
cb	72	448.00
+5 on Pav	72	448.00
$\frac{1}{4}$ " "	71	448.10
$\frac{1}{2}$ " "	71	448.10
$\frac{1}{4}$ " "	71	448.10
+2	72	448.00
cb	73	447.90
+4	49	450.30
W	41	451.10
3+41.65 = PC Lt. 86°		
W	51	450.10
+9	60	449.20
cb	86	446.60
+5 on Pav	84	446.80

455.20

2 on Pay	83	446.90
2 " "	83	446.90
2 " "	83	446.90
+2 " "	82	447.00
cb	86	446.60
E	10.6	444.60
+10	11.4	443.80

## PART 1

-10	11.8	443.40
E	11.0	444.20
cb	90	446.20
+5 on Pay	88	446.40
2 " "	87	446.50
2 " "	89	446.30
2 " "	91	446.10
+2 " "	91	446.10
cb	89	446.30
+2	63	448.90
W	55	449.70

## PART 2

W	61	449.10
+8	70	448.20
cb	94	445.80
+5 on Pay	98	445.40
2 " "	97	445.50
2 " "	95	445.70

455.20

Redland Dr

51

2 on Pay	93	445.90
+2 " "	93	445.90
cb	93	445.90
+3	94	445.80
E	11.2	444.00
+10	12.2	443.00

## PART 3

-10	12.4	442.80
E	10.9	444.30
+3	99	445.30
cb	97	445.50
+5 on Pay	100	445.20
2 " "	100	445.20
2 " "	100	445.20
2 " "	101	445.10
+2 " "	103	444.90
cb	105	444.70
+3	74	447.80
W	69	448.30

## PART 4

W	75	447.70
+8	87	447.00
cb	110	444.20
+5 on Pay	110	444.20
2 " "	109	444.30
2 " "	108	444.40

1/4 on Pav	105	444.70
+2 " "	105	444.70
cb	104	444.80
E	105	444.70
+10	127	442.50

## PART 5

-10	141	441.10
E	134	441.80
+7	114	443.80
cb	113	443.90
+5 on Pav	114	443.80
1/4 " "	114	443.80
1/2 " "	115	443.70
1/4 " "	117	443.50
+2 " "	117	443.50
cb	113	443.90
+2	91	446.10
W	80	447.20

## PART 6 = E.C. = 0+00

W	91	446.10
+7	90	445.40
cb	122	443.00
+5 on Pav	122	443.00
1/2 " "	121	443.10
1/4 " "	121	443.10
1/4 " "	121	443.10

+2 on Pav	121	443.10
cb	122	443.00
+6	125	442.70
E	142	441.00
+10	162	439.00
TP	590	449.11
	1199	443.21

## Levels for Drain #2 on lot line 445

0+00 = E.C. as per sketch 6 pages	93	439.81
+37	154	433.71
+53	203	428.81
+63	241	425.01

## 0+37.5

-10	111	438.01
E	93	439.81
+5	75	441.61
cb	70	442.11
+5 on Pav	69	442.21
1/4 " "	69	442.21
1/2 " "	69	442.31
1/4 " "	66	442.51
+2 " "	66	442.51
cb	66	442.51
+3	43	444.81
W	33	445.81
		1+00
W	32	445.91

14911

+8	4.2	444.91
cb	6.4	442.71
+5 on Pav	6.8	442.31
$\frac{1}{4}$ " "	6.7	442.41
$\frac{1}{2}$ " "	7.0	442.11
$\frac{1}{4}$ " "	7.0	442.11
+2 " "	7.1	442.01
cb	7.1	442.01
+4	7.6	441.51
E	8.9	441.21
+10	11.2	437.92

1+50

-10	9.6	439.51
-5	8.5	440.61
E	6.8	442.31
cb	6.3	442.81
+5 on Pav	6.4	442.71
$\frac{1}{4}$ " "	6.4	442.71
$\frac{1}{2}$ " "	6.3	442.81
$\frac{1}{4}$ " "	6.4	442.71
+2 " "	6.4	442.71
cb	6.1	443.01
+2	3.9	445.21
11	3.1	446.01

2+00

11	2.0	447.11
----	-----	--------

44911

Redland Dr

53

+8	2.7	446.41
cb	5.0	444.11
+5 on Pav	5.4	443.71
$\frac{1}{4}$ " "	5.3	443.81
$\frac{1}{2}$ " "	5.3	443.81
$\frac{1}{4}$ " "	5.4	443.71
+2 " "	5.5	443.61
cb	5.1	444.01
E	5.3	443.81
+4	6.6	442.51
+10	7.5	441.61

2+50

-10	6.5	442.61
-5	5.3	443.81
E	4.1	445.01
cb	3.9	445.21
+2	4.5	444.61
+5 on Pav	4.4	444.71
$\frac{1}{4}$ " "	4.4	444.71
$\frac{1}{2}$ " "	4.3	444.81
$\frac{1}{4}$ " "	4.4	444.71
+2 " "	4.5	444.61
cb	4.2	444.91
+2	1.6	447.51
11	1.3	447.81

2+74



449.11

N	11	448.01
cb	17	447.41
+2	37	445.41
+5 on Pay	40	445.11
7 " "	40	445.11
6 " "	39	445.21
4 " "	40	445.11
+2 " "	41	445.01
cb	39	445.21
E	41	445.01
+10	58	443.31

2+76

-10	55	443.61
E	39	445.21
cb	40	445.11
+5 on Pay	40	445.11
7 " "	40	445.11
6 " "	39	445.21
7 " "	39	445.21
+2 " "	39	445.21
cb	37	445.41

N on Cor. Apron to Garage

P-

345

2+86 = Garage on W 4.6' Back. With Cor. Apron 0.6' in st.

2+92

N	33	445.81
cb	38	445.31

449.11

Redwood Dr.

54

+5 on Pay	39	445.21
7 " "	39	445.21
6 " "	39	445.21
7 " "	40	445.11
+2 " "	37	445.41
cb	37	445.41
+5	44	444.71
10	55	443.61

2+95

-10	54	443.71
-6	38	445.31
E	36	445.51
cb	37	445.41
+5 on Pay	40	445.11
7 " "	40	445.11
6 " "	39	445.21
7 " "	39	445.21
+2 " "	39	445.21
+5	38	445.31
cb	14	447.71
N	06	448.51

3+55

N	22	446.91
cb	24	446.71
+1	47	444.41
+5 on Pay	49	444.21

$\frac{1}{2}$ on Pav.	49	444.21	
$\frac{1}{2}$ " "	49	444.21	
$\frac{1}{2}$ " "	49	444.21	
+2 " "	48	444.31	
cb	47	444.41	
E	46	444.51	
+10	51	444.01	
3+57 = S edge of <sup>Dbld.</sup> Garage on West <sup>8' inst.</sup> Floor. With Cor Apron			
-10	51	444.01	
E	48	444.31	
cb	48	444.31	
+5 on Pav.	50	444.11	
$\frac{1}{2}$ " "	50	444.11	
$\frac{1}{2}$ " "	51	444.01	
$\frac{1}{2}$ " "	51	444.01	
+4 " "	52	443.91	
cb	48	444.31	
+2 on Cor. Apron	476	444.35	
X	473	444.38	
3+75 = N edge Dbld Garage on West			
X on Apron	475	444.36	
cb. " toe"	490	444.24	
+5 on Pav.	57	443.11	
$\frac{1}{2}$ " "	57	443.41	
$\frac{1}{2}$ " "	55	443.61	
$\frac{1}{2}$ " "	55	443.61	

+2 on Pav.	54	443.71	
cb	52	443.91	
E	52	443.91	
+10	58	443.31	
			3+78
-5	58	443.31	
E	53	443.61	
cb	53	443.81	
+5 on Pav.	56	443.51	
$\frac{1}{2}$ " "	56	443.51	
$\frac{1}{2}$ " "	57	443.41	
$\frac{1}{2}$ " "	59	443.21	
+2 " "	59	443.21	
cb	50	444.11	
+1	38	445.31	
X	35	445.61	
4+115 = sec. At Pt A to PC on W = South.			
S	48	444.31	
+9	56	443.51	
cb	74	441.71	
+3 on Pav.	75	441.61	
$\frac{1}{2}$ " "	73	441.71	
$\frac{1}{2}$ " "	71	442.01	
$\frac{1}{2}$ " "	71	442.01	
+2 " "	71	442.01	
cb	67	442.41	

449.11

E = N		69	442.21
+10		72	441.91
T.P. above BM		876	440.35
			440.36 = BM
			0.01 = Error
	3.86 444.22		440.36 = Above BM
	4 + 41.43 = sec A		
N		33	440.92
cb.		36	440.62
7 on Pav		39	440.32
6 " "		38	440.42
4 " "		39	440.32
cb. "		43	439.92
S " "		49	439.32
	Sec B		
-2993 = P.C. of D		26	441.62
-10		29	441.32
-7		51	439.12
-5 on Pav		52	439.02
S = P.I. on Pav		49	439.32
cb. on Pav		43	439.92
4 " "		40	440.22
6 " "		42	440.02
2		46	439.62
cb.		46	439.62
N		53	438.92

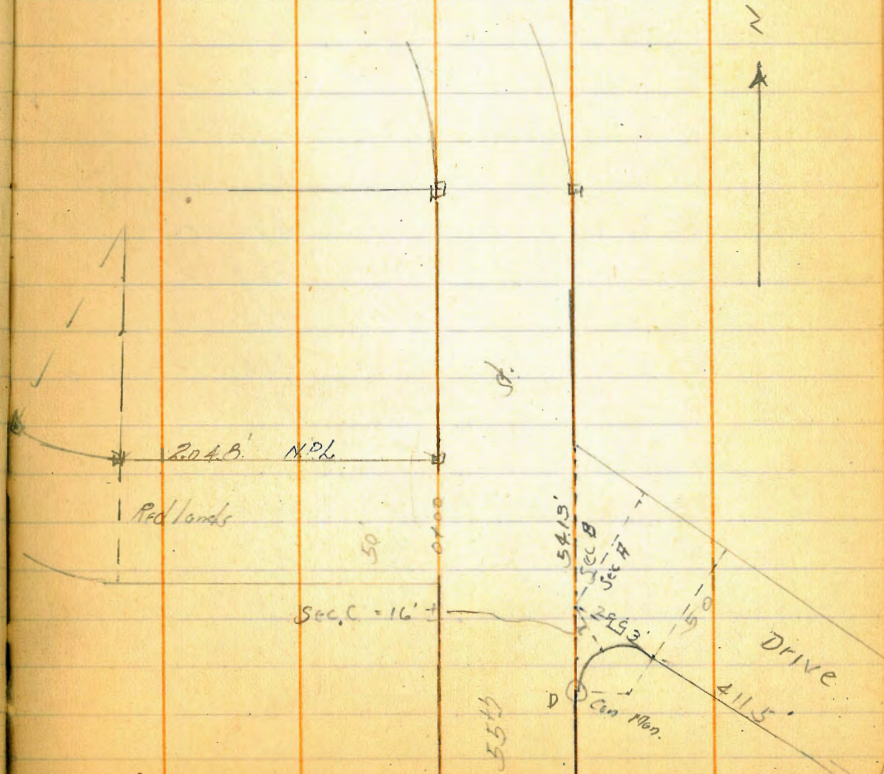
Sec C. = External

444.22

Redland Dr.

56

P.I. on Pav		49	439.32
+2		50	439.22
+6		49	439.32
+8		27	441.52
+16 at Curve		21	442.12
T.P.	108	441.74	3.86 440.36
	0+00		
N		49	436.84
+8		46	437.14



cb		5.2	436.54	
1/2		5.1	436.64	
1/2		5.0	436.74	
1/2		3.0	436.74	
+3		5.0	436.74	
cb		6.3	435.44	
+1		4.4	437.34	
5		4.4	437.34	3' inst 6' Tail
0+10	Gypress Tree 2.5" dia	5.2	436.54	"
+33	" " " "	5.9	435.84	"
+42	" " " "	6.7	435.04	"
+62	" " " "	7.7	434.04	"
+82	" " " "	9.1	432.64	"
1+02	" " " "	10.5	431.24	"
+22	" " " "	11.6	430.14	"
+32	" " " "	13.0	428.74	"
+52	" " " "	13.3	428.44	"
+72	" " " "	13.2	428.54	"
+92	" " " "	14.1	426.64	"
	0+50			"
5		7.7	434.04	
+8		8.1	433.64	
cb		9.2	432.54	
+2		8.4	433.34	
1/2		8.3	433.44	
1/2		8.3	433.44	

1/2		8.6	433.14	
cb		8.3	433.44	
+1		7.0	434.74	
N		7.1	434.64	
	1+00			
N		10.3	431.44	
+8		10.8	430.94	
cb		12.1	429.64	
1/2		12.1	429.64	
1/2		12.1	429.64	
1/2		12.1	429.64	
+5		12.3	429.44	
cb		12.8	428.94	
+1		12.4	429.34	
5		12.6	429.14	
+5		12.9	428.84	
	1+50			
-10		17.4	424.34	
5		16.4	425.34	
cb		16.0	425.74	
1/2		15.3	426.44	
1/2		15.1	426.64	
1/2		15.2	426.54	
cb		15.5	426.24	
+2		13.7	428.04	
N		12.8	428.94	

441.74

2+4B = PC PL ?

N	14.0	427.74
+9	14.8	426.94
cb.	16.5	425.24
$\frac{1}{4}$	17.4	424.34
$\frac{1}{2}$	17.3	424.44
$\frac{3}{4}$	17.3	424.44
cb.	17.2	424.54
S	17.8	423.94
+15	19.2	422.54

Redland Dr.

58

1/2" Ker  
 Ruptured = 1  
 Short ch.  
 Area = 80.  
 3-10-28

Cross Section MADISON AVE <sup>50' wide</sup>  
 from 55<sup>th</sup> to El Centro Drive <sup>10' cbs 75' 25'</sup>

436.24

	3.02	436.24		439.22
Top 5.5' ch.		10.97		425.27
	56.55 <sup>th</sup> = 0+00			
-10		11.3		424.94
S		10.8		425.44
cb		10.5		425.74
1/4		10.3		425.94
1/2		9.8		426.44
3/4		9.7		426.54
cb		9.3		426.94
N		9.1		427.14
	0+01			
N		6.6		429.64
+8		7.1		429.14
cb		9.4		426.84
1/4		9.7		426.54
1/2		9.7		426.54
3/4		9.3		426.94
cb		9.7		426.54
+3		9.2		427.04
S		9.5		426.74
+10		10.3		425.94
	0+50			
-10		8.5		427.74
S		7.1		429.14
+8		6.6		429.64

No cb in  
 on North

cb		7.0		429.24
1/2		7.0		429.24
1/4		6.9		429.34
1/2		6.8		429.44
cb		7.3		428.94
+2		5.4		430.84
N		5.1		431.14
	1+00			
N		1.8		434.44
+2		2.3		433.94
cb		4.3		431.94
1/4		3.8		432.44
1/2		3.9		432.34
3/4		3.9		432.34
cb		3.9		432.34
S		4.1		432.14
-10		5.2		431.04
TP	12.40	448.48	0.16	436.08
	1+50			
-10		13.7		434.78
S		13.2		435.28
cb		12.8		436.68
1/4		12.6		436.88
1/2		12.4		437.08
3/4		12.1		437.38
+5		12.4		437.08
cb		14.1		434.38

+2		107	437.78	
N		104	438.08	
1+77 = 2	Dirt floor Garage on South 13' Back	108	437.68	
1+89 = 2	Acacia Tree on South 8' inst	76	439.88	3" dia. 10' tall
2+15 = "	" " " " " " " "	83	440.18	" " " "
+36 = "	" " " " " " " "	69	441.58	" " " "
+58 = "	" " " " " " " "	63	442.18	" " " "
+80 = "	" " " " " " " "	56	442.88	" " " "
3+04 = "	" " " " " " " "	43	444.14	" " " "

2+00

N		76	440.88	
+7		80	440.48	
cb.		95	438.98	
+2		98	438.68	
+3		91	439.38	
$\frac{1}{4}$		90	439.48	
$\frac{1}{2}$		89	439.58	
$\frac{1}{4}$		91	439.38	
cb.		93	439.18	
S		94	439.08	
+5		96	438.88	
-5		76	440.88	
S		75	440.98	
cb.		78	440.68	
$\frac{1}{4}$		75	440.98	
$\frac{1}{2}$		75	440.98	

2+28

$\frac{1}{4}$		74	441.08	
+5		79	440.58	
cb		74	441.08	
+3		54	443.08	
N		49	443.58	
	2+50			
N		46	443.88	
+8		50	443.48	
cb.		64	442.08	
$\frac{1}{4}$		64	442.08	
$\frac{1}{2}$		64	442.08	
cb.		68	441.68	
S		66	441.88	
+5		67	441.78	
	3+04			
S		43	444.18	
cb.		43	444.18	
$\frac{1}{2}$		41	444.38	
$\frac{1}{4}$		38	444.68	
$\frac{1}{2}$		38	444.68	
cb.		38	444.68	
+2		30	445.48	
N		25	445.98	
	3+20 = N.L. Redland Dr.			X. Section Intersection on Page 41
N		14	447.08	
+8		22	446.28	

448.48

cb		33	445.18
1/2		33	445.18
1/2		33	445.18
1/2		37	444.78
cb		40	444.48
S		40	444.48
	El. Redland	Drive =	0700
S		17	446.78
+8		15	446.98
cb		29	445.58
1/2		22	446.28
1/2		21	446.38
1/2		21	446.38
cb		17	446.78
+2		04	448.08
N		+0.1	448.38
TP	1230	460.73	005 448.43
	0150		
N		93	451.43
+8		100	450.73
cb		117	449.03
1/2		117	449.03
1/2		117	449.03
1/2		120	448.73
cb		125	448.23
+2		118	448.93
S		122	448.53

460.73

Madison Ave

61

+5		123	448.43
	0+80		
-5		107	450.03
S		109	450.33
+8		102	450.53
cb		110	449.73
1/2		102	450.53
1/2		103	450.43
1/2		103	450.43
cb		108	449.93
+2		8.5	452.23
N		25	453.23
	1+00		
N		74	453.33
+8		80	452.73
cb		100	450.73
1/2		94	451.33
1/2		94	451.33
1/2		96	451.13
cb		100	450.73
S		97	451.03
+5		100	450.73
	1+27		
-5		91	451.63
S		8.5	452.23
+8		81	452.63
cb		90	451.73



46073

1/2	84	452.33
1/2	82	452.53
1/2	83	452.43
cb	57	452.03
+2	67	454.03
N	60	455.03
	1750	
N	58	454.93
+8	62	454.53
cb	76	453.13
1/2	77	453.03
1/2	73	453.43
1/2	75	453.23
cb	81	452.63
+8	73	453.43
S	77	453.03
+5	80	452.73
	2+00	
-5	59	454.83
S	59	454.83
cb	59	454.83
1/2	57	455.03
1/2	55	455.23
1/2	58	454.93
cb	61	454.63
+2	50	455.73
N	47	456.03

46073

Madison Ave

62

	2+50	
N		3.7 457.03
+8		4.0 456.73
cb		4.7 456.03
1/2		4.2 456.53
1/2		3.8 456.93
1/2		3.8 456.93
cb		3.7 457.03
S		3.5 457.23
+5		3.5 457.23
	3+00	
S		1.6 459.13
cb		2.3 458.43
1/2		2.3 458.43
1/2		2.3 458.43
1/2		2.3 458.43
1/2		2.5 458.23
cb		2.7 458.03
+2		2.1 458.63
N		2.0 458.73
	3+31.6 = YL 51 Cerito Drive	
N		1.3 459.43
+7 = N top cb		1.28 459.45
" Gut. on Pavng		1.84 458.89
" cb. " "		1.68 459.05
1/2		1.29 459.44
1/2		1.08 459.65
1/2		1.10 459.68

46073

cb			129	459.44
+3 = Gut			141	459.32
+3 on top cb			069	460.04
S			07	460.03

Note: for Detail <sup>Erst.</sup> cb Returns <sup>on W. El Cerito.</sup> See Plans for El Cerito Drive

TP	067	448.50	12.20	447.83
TP	122	438.04	11.68	436.82
cbk. on BM top NW pillar			4.84	433.20

433.22 - BM  
002 - Error

Madison Ave

69

Cross Section Adams Ave 50' wide 10' cbs  
 From E. h. 54th to El Centro Drive  
 7.5' 7.5'

Plotted

422.22 Adams Ave 64

4.28 437.50 433.22

B.M. N.Y. P. 110  
 Hudson 5589.9

3+72 = 2' Plumbago Palm Tree on N 5' Back 3.8 418.42

TP 0.76 431.25 7.01 430.49

4+01 = " " " " " " 3.0 419.22

TP 2.21 422.22 11.24 420.01

+21 = " " " " " " 2.1 420.12

Left CM on SW. Pole Adams Ave  
 Hinson Place 5.00 417.22

For future  
 Reference

+62 = " " " " " " 1.8 420.42

E. h. 54th = 0+00

+92 = " " " " " " 1.2 421.02

S 8.1 414.12

5+20 = " " " " " " 0.4 421.82

cb 8.0 414.22

TP 6.08 423.30 5.00 417.22

+5 on Pav. on S. Adams 8.0 414.22

0+39

1/2 " " 7.8 414.42

N 7.4 415.90

1/10 " " 7.5 414.72

cb 8.4 414.90

1/4 " " 7.6 414.62

+5 on Pav. 8.4 414.90

+2 " " 7.7 414.82

1/4 " " 8.2 415.10

cb 7.6 414.62

1/10 " " 8.2 415.10

+1 " " 7.2 415.02

1/2 " " 8.5 414.80

N 6.7 415.52

+2 " " 8.6 414.70

0+06 = 2' Plumbago Palm Tree on N 5' Back 6.7 415.52

cb 8.7 414.60

+39 = " " " " " " 6.0 416.22

+1 8.2 415.10

+69 = " " " " " " 5.5 416.72

S 8.2 415.10

1700 = " " " " " " 5.0 417.22

0+90 = 1/2 Henson Place on South 7.5' cbs  
 7.5' 7.5'

+30 = " " " " " " 4.7 417.52

7.4 415.90

+60 = " " " " " " 4.2 418.02

cb 7.3 416.00

+90 = " " " " " " 4.1 418.12

+1 7.9 415.40

2+20 = " " " " " " 4.3 417.92

+3 on Pav. 7.9 415.40

+50 = " " " " " " 4.3 417.92

1/2 " " 7.8 415.50

+80 = " " " " " " 4.3 417.92

1/10 " " 7.7 415.60

3+10 = " " " " " " 4.3 417.92

1/4 " " 7.7 415.60

+40 = " " " " " " 4.2 418.02

+2 on Pav	7.9	415.50
cb	8.0	415.30
+1	7.2	416.10
N	6.4	416.90
N	6.4	416.90
+9	7.0	416.30
cb	7.8	415.50
+5 on Pav	7.7	415.60
7 " "	7.6	415.70
8 " "	7.6	415.70
7 " "	7.7	415.80
+2 "	7.8	415.50
cb	7.7	415.60
S	8.4	414.90
S	5.3	415.00
cb	7.8	415.50
+5 on Pav	7.8	415.50
7 " "	7.7	415.60
8 " "	7.5	415.80
7 " "	7.5	415.80
+2	7.6	415.70
cb	7.7	415.60
+1	7.0	416.30
N	6.1	417.20

N cb

N 7

		Harris	Ave
L Henson Pl			
	N	6.0	417.30
	+9	7.0	416.30
	cb	7.7	415.60
	+5 on Pav	7.5	415.80
	7 " "	7.4	415.90
	8 " "	7.4	415.90
	7 " "	7.6	415.70
	+2 "	7.6	415.70
	cb	8.0	415.30
	S	8.0	415.30
	E 7		
	S	8.1	415.20
	cb	8.0	415.30
	+5 on Pav	7.6	415.70
	7 " "	7.5	415.80
	8 " "	7.4	415.90
	7 " "	7.3	416.00
	+2 "	7.5	415.80
	cb	7.7	415.60
	+2	6.8	416.50
	N	6.0	417.30
	E cb		
	N	6.2	417.10
	+9	7.1	416.20
	cb	7.6	415.70

423.30

+5 on Par	74	415.90
$\frac{1}{2}$ " "	73	416.00
$\frac{1}{2}$ " "	73	416.00
$\frac{1}{2}$ " "	74	415.90
+2 " "	75	415.80
cb	80	415.30
S	79	415.40
1+30 = E. L. Hanson Pl.		
S	69	416.40
+9	68	416.50
cb	79	415.40
+5 on Par	76	415.70
$\frac{1}{2}$ " "	74	415.90
$\frac{1}{2}$ " "	72	416.10
$\frac{1}{2}$ " "	72	416.10
+2 " "	73	416.00
cb	76	415.70
+1	70	416.30
N	61	417.20
1+50		
N	57	417.60
+8	68	416.50
cb	75	415.80
+5 on Par	71	416.20
$\frac{1}{2}$ " "	70	416.30
$\frac{1}{2}$ " "	72	416.10
$\frac{1}{2}$ " "	73	416.00

423.30

Adams Acc

66

+2	73	416.00
cb	75	415.80
+1	67	416.60
S	66	416.70
2+00		
S	70	416.30
+9	68	416.50
cb	72	416.10
+5 on Par	67	416.60
$\frac{1}{2}$ " "	66	416.70
$\frac{1}{2}$ " "	66	416.70
$\frac{1}{2}$ " "	65	416.80
+2 " "	65	416.80
cb	70	416.30
+2	63	417.00
N	57	417.60
2+50		
N	55	417.80
cb	65	416.80
+5 on Par	60	417.30
$\frac{1}{2}$ " "	60	417.30
$\frac{1}{2}$ " "	60	417.30
$\frac{1}{2}$ " "	62	417.10
+2 " "	63	417.00
cb	67	416.60
+1	61	417.20
S	67	416.60

423.30

+5		22	416.10
	3+00		
-5		63	417.00
S		58	417.50
+9		52	418.10
cb		61	417.20
+5 on Rev		56	417.70
$\frac{1}{4}$ " "		55	417.80
$\frac{1}{2}$ " "		54	417.90
$\frac{3}{4}$ " "		55	417.80
+2 " "		55	417.80
cb		60	417.30
+2		53	418.00
N		52	418.10
	3+50		
N		51	418.20
+9		50	418.30
cb		34	417.90
+5 on Rev		50	418.30
$\frac{1}{4}$ " "		49	418.40
$\frac{1}{2}$ " "		49	418.40
$\frac{3}{4}$ " "		50	418.30
+2 " "		51	418.20
cb		54	417.90
+1		48	418.50
S		50	418.30
+5		51	418.20

423.30

Adams Ave

67

3+84 = $\frac{1}{2}$ Gov. Mill on South	4.26	419.04	0.2 Back. 4' side
	4+00		
S	4.0	419.30	
+9	4.2	419.10	
cb.	4.6	418.70	
+5 on Rev	4.6	418.70	
$\frac{1}{4}$ " "	4.5	418.80	
$\frac{1}{2}$ " "	4.4	418.90	
$\frac{3}{4}$ " "	4.3	419.00	
+2 " "	4.3	419.00	
cb	4.7	418.60	
+1	4.3	419.00	
N	4.3	419.00	
	4+50		
N	3.3	420.00	
cb.	3.8	419.50	
+5 on Rev	2.0	419.30	
$\frac{1}{4}$ " "	3.8	419.50	
$\frac{1}{2}$ " "	3.8	419.50	
$\frac{3}{4}$ " "	4.0	419.30	
+2 " "	4.1	419.20	
cb	4.4	419.20	
+1	3.6	419.70	
S	3.2	420.10	
	5+00		
S	2.3	421.00	
+9	2.8	420.50	

cb.		37	419.60
+5 on Pav		34	419.90
$\frac{1}{2}$ " "		33	420.00
$\frac{1}{8}$ " "		32	420.10
$\frac{1}{4}$ " "		34	419.90
+2 " "		35	419.80
cb.		32	420.10
N		28	420.50
	5+50		
N		18	421.50
cb.		28	420.50
+5 on Pav		27	420.60
$\frac{1}{4}$ " "		26	420.70
$\frac{1}{8}$ " "		26	420.70
$\frac{1}{2}$ " "		27	420.60
+2 " "		29	420.40
cb.		32	420.10
+1		27	420.60
S		20	421.30
	6+00		
S		15	421.80
+9		20	421.30
cb.		24	420.90
+5 on Pav		23	421.00
$\frac{1}{4}$ " "		22	421.10
$\frac{1}{8}$ " "		21	421.20
$\frac{1}{2}$ " "		21	421.20

+2 on Pav		23	421.00	
cb.		25	420.80	
N		15	421.80	3' side on line
6+11 = 1/2 Con. 16' N. on South		140	421.90	
T.P. 1294 435.64		060	422.70	
	6+50			
N		133	422.34	
cb.		138	421.84	
+5 on Pav		138	421.84	
$\frac{1}{4}$ " "		138	421.84	
$\frac{1}{8}$ " "		137	421.94	
$\frac{1}{2}$ " "		137	421.94	
+2 " "		139	421.74	
cb.		135	422.14	
S		136	422.04	
5+52 = 1/2 Florida Palm Tree on North		136	422.04	5' Sect.
+91 = " " " " " "		137	421.94	" "
6+12 = " " " " " "		136	422.04	" "
+42 = " " " " " "		133	422.34	" "
+72 = " " " " " "		132	422.44	" "
7+02 = " " " " " "		123	423.34	" "
+31 = " " " " " "		111	424.54	" "
+62 = " " " " " "		96	426.04	" "
+92 = " " " " " "		76	428.04	" "
8+32 = " " " " " "		64	429.24	" "
+53 = " " " " " "		48	430.84	" "
8+03 = " " " " " "		35	432.14	" "

43564

9+12 = 1/2 Florida Plant on North 21 433.54 6' back

-143 = " " " " " 05 435.14 " "

6+72 = 1/2 Gov Walk on North 15' 112 St.

S 13.5 422.14

cb 13.0 422.64

+5 on Pav. 13.3 422.39

1/4 " " 13.2 422.44

1/2 " " 13.2 422.44

1/2 " " 13.1 422.54

+2 on edge of Gov Walk 13.6 422.38

+5 " Walk 13.8 422.26

cb " " 13.07 422.57

N " " 12.90 422.74

7+07 = 1/2 Gov Drive Way on North 15' 112 St. 6.5 wide 9.5 wide of Pav.

N on Drive 12.10 423.54

cb " " 12.23 423.41

+2 " " 12.71 422.93

+5 " " 12.61 423.03

1/4 on Pav 12.5 423.14

1/2 " " 12.6 423.04

1/2 " " 12.6 423.04

+2 " " 12.7 422.94

cb 12.9 422.74

S 12.1 423.54

7+50

S 11.3 424.34

+9 11.5 424.14

43564

Adams Ave

69

cb 12.0 423.64

+5 on Pav. 11.2 424.44

1/4 " " 11.0 424.64

1/2 " " 10.9 424.74

1/2 " " 10.9 424.74

+2 " " 11.0 424.64

cb 11.1 424.54

+2 11.0 424.64

+3 10.3 425.34

N 10.3 425.34

7+92

N 7.9 427.74

+7 8.2 427.94

cb 10.0 425.64

+5 on Pav. 9.2 426.44

1/2 " " 9.2 426.44

1/2 " " 9.2 426.44

1/4 " " 9.1 426.24

+2 " " 9.5 426.14

cb 10.9 424.74

+2 9.7 425.94

S 9.5 426.14

+5 9.5 426.14

8+50

S 7.4 428.24

+8 7.7 427.94

cb 8.8 426.84



+5 on Pav	7.2	428.44
$\frac{1}{2}$ " "	7.0	428.64
2 " "	6.8	428.84
$\frac{1}{2}$ " "	6.9	428.74
+2 " "	7.0	428.64
+5	7.5	428.14
cb	6.7	428.94
N	5.2	430.44

8+69 = 2<sup>1</sup>/<sub>2</sub> Lon. Walk on North

N on Walk	4.25	431.39
cb " "	6.2	429.52
+5 " "	6.15	429.49
$\frac{1}{2}$ " Pav	6.1	429.54
$\frac{1}{6}$ " "	6.0	429.64
$\frac{1}{4}$ " "	6.2	429.44
+2 " "	6.3	429.34
cb	7.0	428.64
+1	6.4	429.24
S	6.4	429.24

8+88 = 2<sup>1</sup>/<sub>2</sub> Lon Drive on North 6.5' Wide

S	5.0	430.64
+9	5.2	430.44
cb	6.4	429.24
+3	6.8	428.84
+5 on Pav	5.6	430.04
$\frac{1}{2}$ " "	5.5	430.14
$\frac{1}{2}$ " "	5.3	430.34

$\frac{1}{2}$ on Pav	5.3	430.34
+2 " Drive	5.44	430.20
cb " "	5.59	430.05
N	3.78	431.86

7+15

N	2.5	433.14
+9	3.6	432.04
cb	4.2	431.44
+2	5.0	430.64
+5 on Pav	4.3	431.34
$\frac{1}{4}$ " "	4.2	431.44
$\frac{1}{6}$ " "	4.1	431.54
$\frac{1}{3}$ " "	4.3	431.34
+2 " "	4.4	431.24
+5	5.3	430.34
cb	4.0	431.64
S	3.4	432.24

9+57 = 2<sup>1</sup>/<sub>2</sub> Lon 55'± for X-Section Intersection see Page 73

S	2.3	433.34
cb	2.8	432.84
+2	3.9	432.34
+5 on Pav	2.8	432.84
$\frac{1}{4}$ " "	2.7	432.94
$\frac{1}{6}$ " "	2.5	433.14
$\frac{1}{3}$ " "	2.6	433.04
+2 " "	2.6	433.04
+3	4.1	431.54

43564

cb		2.6	433.04
N.		0.7	434.94
TP	12.82	447.79	0.67
cb. on 55 <sup>th</sup> St	55 <sup>th</sup> See Page 23	12.01	435.78
			435.77 - 8M 0.01 = Error
	12.01	447.78	435.77 - Above 8M.
	0+00 = E. to 55 <sup>th</sup> St		
N		2.4	438.38
+8		12.1	435.68
cb		13.2	434.58
+5 on Pav.		12.9	434.88
$\frac{1}{4}$ " "		12.9	434.88
$\frac{1}{2}$ " "		12.8	434.98
$\frac{1}{4}$ " "		13.1	434.68
+2 " "		13.3	434.48
+3		13.7	434.08
cb		12.7	435.08
+3		12.1	435.68
S		13.3	435.48
	0+30		
S		10.0	437.78
+7		10.0	437.78
cb		10.9	436.88
+2		12.2	435.58
+4		12.1	435.68
+5 on Pav.		11.3	436.48
$\frac{1}{4}$ " "		11.2	436.58

44778

Adams Ave

71

$\frac{1}{2}$ on Pav.	11.0	436.78
$\frac{1}{2}$ " "	11.1	436.68
+2 " "	11.2	436.58
+3	11.4	436.38
+5	12.5	435.28
cb.	12.3	435.48
+3	9.7	439.08
N	8.4	439.38
	0+50	
N	7.3	439.48
+7	7.1	439.68
+9	11.7	436.08
cb.	11.5	436.28
+2	11.5	436.28
+3	10.2	437.58
+5 on Pav.	9.9	437.88
$\frac{1}{2}$ " "	9.7	438.08
$\frac{1}{4}$ " "	9.7	438.08
$\frac{1}{2}$ " "	9.9	437.88
+2 " "	10.0	437.78
+3	11.3	436.48
cb.	9.7	438.08
+4	8.5	439.28
S	8.3	439.48
	1+00	
S	4.9	442.88
+7	4.9	442.88

447.78

cb		76	440.18
+3		81	439.68
+5 on Pav		67	441.08
$\frac{1}{4}$ "	"	66	441.18
$\frac{1}{6}$ "	"	65	441.28
$\frac{1}{4}$ "	"	66	441.18
+2"	"	67	441.08
+4		70	440.78
+5		80	439.78
cb		76	440.18
+5		45	443.28
N		45	443.28
	1+50		
N		15	446.28
+7		20	445.78
cb		63	441.48
+2		63	441.48
+4		40	443.78
+5 on Pav		38	443.98
$\frac{1}{4}$ "	"	38	443.98
$\frac{1}{2}$ "	"	37	444.08
$\frac{1}{4}$ "	"	38	443.98
+2*		39	443.88
+4		54	442.38
cb		29	444.88
+3		19	445.88
5		16	446.18

447.78

Edwards Acc.

72

T.P.	11.61	458.94	0.45	447.33
	1+80			
S			11.7	447.24
+7			12.3	446.64
cb			13.4	445.54
+2			15.9	443.04
+5 on Pav			14.0	444.94
$\frac{1}{4}$ "	"		13.9	445.04
$\frac{1}{2}$ "	"		13.7	445.24
$\frac{1}{4}$ "	"		13.7	445.24
+2	"		13.8	445.14
+6			13.7	445.24
cb			15.4	443.54
+2			15.6	443.34
+3			11.6	447.34
N			10.7	448.24
	2+10			
N			10.7	448.24
+7			11.8	447.14
cb			14.5	444.44
+2			14.5	444.44
+2			12.6	446.34
+5 on Pav			12.6	446.34
$\frac{1}{2}$ "	"		12.6	446.34
$\frac{1}{2}$ "	"		12.4	446.54
6	"		12.4	446.54
4	"		12.5	446.44
+2	"			

458.94

+3	14.2	444.74
cb.	13.8	445.14
+3	10.4	448.54
S	10.3	448.64

2+36 = 1/2 Con Drive on North

S	9.6	449.34
+8	10.2	448.74
cb.	13.0	445.94
+4	13.1	445.84
+5 on Pav.	11.6	447.34
1/4 " "	11.5	447.44
1/2 " "	11.4	447.54
1/4 " "	11.6	447.34
+2 on Drive	11.99	447.45
cb " "	11.65	447.29
N " "	10.53	448.41

2+70

N	9.9	449.64
+7	9.9	449.64
+8	10.9	448.04
cb.	11.0	447.94
+3	11.2	447.74
+5 on Pav.	10.3	448.64
1/4 " "	10.3	448.64
1/2 " "	10.1	448.84
1/2 " "	10.1	448.84
+2 " "	10.2	448.74

458.94

Hdamps Fee

73

+4	11.5	447.44
cb.	11.8	447.14
+2	9.0	449.94
S	8.6	450.34

3+20 = 1/2 Redland Dr.

S	7.3	451.64
+8	7.6	451.34
cb.	8.6	450.34
1/5 on Pav.	8.3	450.64
1/4 " "	8.2	450.74
1/2 " "	8.1	450.84
1/4 " "	8.3	450.64
+2 " "	8.2	450.74
cb.	8.6	450.34
+2	8.8	450.14
+3	7.8	451.14
N	7.5	451.44

0+00 = 1/2 Redland Dr.

N	6.3	452.64
+8	6.4	452.54
cb.	7.3	451.64
+5	7.4	451.54
1/4	7.3	451.64
1/2	7.2	451.74
1/4	7.2	451.74
+2	7.4	451.54
cb.	7.4	451.54

458.94

+2	64	452.54
5	61	452.84
	0+50	
5	56	453.34
+8	58	453.14
cb.	71	451.84
+5 on Pav.	68	452.14
$\frac{1}{2}$ " "	68	452.14
$\frac{1}{2}$ " "	68	452.14
$\frac{1}{4}$ " "	69	452.04
+2 " "	69	452.04
cb.	69	452.04
+2	62	452.74
N	60	452.94
	1+00	
N	55	453.54
+8	57	453.24
cb.	65	452.44
+5 on Pav.	63	452.64
$\frac{1}{4}$ " "	62	452.74
$\frac{1}{2}$ " "	61	452.84
$\frac{1}{2}$ " "	62	452.74
+2 " "	62	452.74
cb.	64	452.54
+1	52	453.74
5	50	453.94

458.94

Adams Ave

74

	1+50	
5	38	455.14
+9	38	455.14
cb.	54	453.54
+5 on Pav.	57	453.24
$\frac{1}{4}$ " "	57	453.24
$\frac{1}{2}$ " "	55	453.44
$\frac{1}{4}$ " "	56	453.34
+2 " "	58	453.14
cb.	56	453.34
+1	50	453.94
N	49	454.04
	2+00	
N	40	454.94
+7	42	454.74
cb.	52	453.74
+5 on Pav.	53	453.64
$\frac{1}{4}$ " "	51	453.84
$\frac{1}{2}$ " "	49	454.04
$\frac{1}{4}$ " "	50	453.94
+2 " "	50	453.94
cb.	52	453.74
+1	33	455.64
5	32	455.74
	2+34.5 - 2' Con Drive on North	10' 12 St.
5	25	456.44

458.94

+9	27	456.24
cb.	46	454.34
+15 on Pav.	47	454.24
$\frac{1}{4}$ " "	47	454.24
$\frac{1}{6}$ " "	45	454.44
$\frac{1}{2}$ " "	48	454.14
+2 " "	48	454.14
cb. on top DRIVE	455	454.39
N " " "	397	454.97
3+50		
N	36	455.34
+8	38	455.14
cb.	47	454.24
+5 on Pav.	47	454.24
$\frac{1}{2}$ " "	46	454.34
$\frac{1}{6}$ " "	45	454.44
$\frac{1}{4}$ " "	45	454.44
+2 " "	46	454.34
+6	42	454.74
cb.	26	456.34
S	24	456.54
3+00		
S	23	456.64
cb.	28	456.14
+1	42	454.74
+5 on Pav.	41	454.84
$\frac{1}{4}$ " "	40	454.94

458.94

Adams Ave

75

$\frac{1}{2}$ on Pav	40	454.94
$\frac{1}{4}$ " "	41	454.84
+2 " "	41	454.84
cb.	43	454.64
+1	33	455.64
N	35	455.44
3+40.6 on N4 = N4. El Cerito DRIVE		
N	35	455.44
+10 = top of Exist. cb.	339	455.55
+10 = on gutter Pav.	401	454.93
$\frac{1}{4}$ " Paving	359	455.35
$\frac{1}{6}$ " "	360	455.34
$\frac{1}{2}$ " "	336	455.58
cb. " "	352	455.42
+2 " " at gutter	358	455.36
+2 " top Exist. cb.	291	456.03
S	27	456.24
3+35 = 5.6 West N4. El Cerito		
S	25	456.44
+9	30	455.94
cb.	38	455.14
+5 on Pav.	38	455.14
$\frac{1}{4}$ " "	38	455.14
$\frac{1}{6}$ " "	36	455.34
$\frac{1}{2}$ " "	38	455.14
+2 " "	39	455.04
cb.	38	455.14

+1	3.4	455.54
N	3.3	455.64
chk. on TP Page 19	7.67	451.27
		451.27 - TP
		0.00

Water  
Right  
Shall  
= 12.28

S.M. B.M.

Adams + Henson Pl. 090 418.17

417.22

Cross Section Henson Pl. <sup>40 wide</sup> 5<sup>8</sup> lbs 7.5' <sup>7</sup>/<sub>8</sub> S

Page 64

0+00 = Sdo. Adams Ave

N	2.3	415.82
+4	2.3	415.82
cb	3.1	415.02
$\frac{1}{4}$	3.1	415.02
$\frac{1}{2}$	3.1	415.02
$\frac{1}{4}$	2.9	415.22
cb	2.9	415.22
+1	2.0	416.12
E	1.8	416.32

0+30

E	2.7	415.42
+4	2.7	415.42
cb	5.2	412.92
+3	6.2	411.92
+4	4.5	413.62
$\frac{1}{4}$	4.6	413.52
$\frac{1}{2}$	4.2	413.92
$\frac{1}{4}$	4.6	413.52
cb	5.4	412.72

+1	3.6	414.52
N	3.4	414.72
0+70		
N	5.1	413.02
+4	5.4	412.72
cb	7.7	410.42
$\frac{1}{4}$	6.6	411.52
$\frac{1}{2}$	6.4	411.72
$\frac{1}{4}$	6.6	411.52
+3	6.7	411.42
+4	8.0	410.12
cb	7.3	410.82
+1	7.5	410.62
+2	5.3	412.82
E	5.3	412.82
1+00		
E	7.1	411.02
+3	7.4	410.72
+4	9.0	409.12
cb	9.1	409.02
+2	9.2	408.92
+3	8.9	409.72
$\frac{1}{4}$	8.0	410.12
$\frac{1}{2}$	8.0	410.12
$\frac{1}{4}$	8.3	409.82
+4	8.4	409.72
cb	9.5	408.62

Yardage Figured  
 8-6-28  
 T.G.H.

418.12

+1	67	411.42
W	66	411.52
	1+25	
W	83	409.82
+4	86	409.52
cb.	10.3	407.82
+3	9.5	408.62
$\frac{1}{4}$	9.6	408.52
$\frac{1}{2}$	9.1	409.02
$\frac{1}{4}$	9.1	409.02
+5	9.5	408.62
+6	10.1	408.02
cb.	10.0	408.12
+2	8.5	409.62
E	8.4	409.72
	1+50	
E	10.0	408.12
cb.	10.4	407.72
$\frac{1}{2}$	10.3	407.82
$\frac{1}{2}$	10.2	407.92
$\frac{1}{4}$	10.4	407.72
+5	11.0	407.12
cb.	10.7	407.92
W	9.7	408.42
	1+79 =	↳ Con Walk on E on line
W	11.2	406.92
+4	11.4	406.72

418.12

HINSON PL.

r. 77

cb.	12.1	406.02
$\frac{1}{2}$	11.3	406.82
$\frac{1}{2}$	11.2	406.92
$\frac{1}{4}$	11.5	406.62
cb.	11.2	406.92
E = top walk	10.91	407.21
	2+25	
E	12.3	405.82
cb.	12.4	405.72
$\frac{1}{2}$	12.5	405.62
$\frac{1}{2}$	12.4	405.72
$\frac{1}{4}$	12.6	405.52
cb.	12.6	405.52
W	12.8	405.32
+5	13.8	404.32
	2+75	
TP	4.04	409.38
-10	12.78	405.34
-5	6.2	403.18
W	5.2	404.18
cb.	4.7	404.68
$\frac{1}{4}$	4.8	404.58
$\frac{1}{2}$	4.8	404.58
$\frac{1}{2}$	4.5	404.88
$\frac{1}{4}$	4.5	404.88
cb.	4.3	405.08
E	3.3	406.08



409.38

3+00

E	2.9	406.48
+3	3.1	406.28
cb.	4.0	405.38
+1	4.5	404.88
$\frac{1}{4}$	4.7	404.68
$\frac{1}{2}$	4.9	404.48
$\frac{3}{4}$	5.0	404.38
cb	5.2	404.18
W	5.0	404.38
+10	5.9	403.48

Section OH = 5'cb 17.5'  $\frac{1}{2}$ S

W	5.7	403.68
cb.	6.0	403.38
$\frac{1}{4}$	5.9	403.48
$\frac{1}{2}$ = 0	6.1	403.28

Section OB. 5'cb 17.5'  $\frac{1}{2}$ S

$\frac{1}{2}$ = 0	6.1	403.28
$\frac{1}{4}$	6.5	402.88
cb	7.2	402.18
B = line	6.5	402.88

Sec. OC 5'cb 17.5'  $\frac{1}{2}$ S

C-5	8.1	401.28
C = line	7.8	401.58
cb.	7.6	401.78
$\frac{1}{4}$	7.0	402.38
$\frac{1}{2}$ = 0	6.1	403.28

409.38

Hinson Pl.

78

Section OD 5'cb 17.5'  $\frac{1}{2}$ S

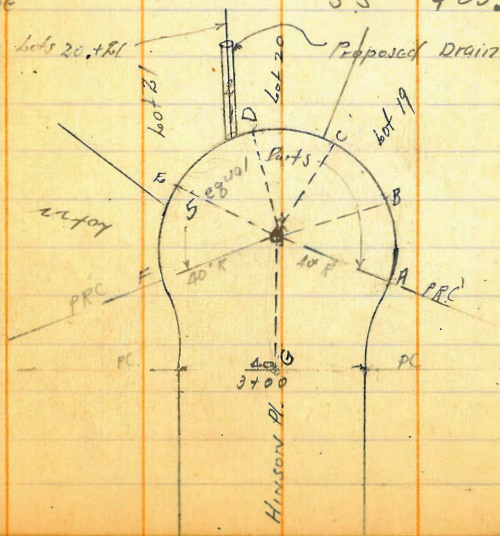
$\frac{1}{4}$	6.1	403.28
$\frac{1}{2}$	6.8	402.58
cb.	7.1	402.28
D = line	7.4	401.98
+10	8.6	400.78

Section OE = 5'cb 17.5'  $\frac{1}{2}$ S

E = line	5.7	403.68
cb.	6.1	403.28
$\frac{1}{4}$	6.1	403.28
$\frac{1}{2}$ = 0	6.1	403.28

Section OF = 5'cbs 17.5'  $\frac{1}{2}$ S

$\frac{1}{2}$ = 0	6.1	403.28
$\frac{1}{4}$	5.5	403.88
cb.	4.7	404.68
F = line	3.5	405.88



Section OG = 51'

4 = 0		6.1	403.28
+10		57	403.68
+20		54	403.98
+30		52	404.18
+40		49	404.48
+51 = G		49	404.48

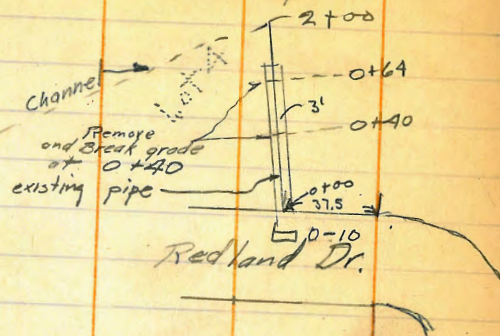
on lot line of lots 20+21

Levels For Drain

0+00		7.7	401.68
+50		11.8	397.58
+60		13.1	396.28
+72		15.8	393.58
TP	10.33	418.92	0.79
chk. on SW. 3/4. Hinson Pl.		169	417.3
			417.22 = 814
			0.01

Profile for change in  
culvert No 3 Redland Gardens

See Pg. 35  
For Original Notes

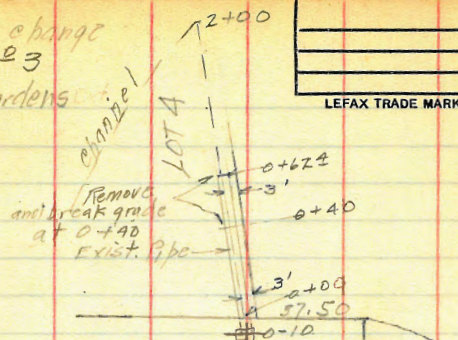


B.M.				
0-10	FL. Box	446.85	8.86	437.99
T.P.	0.17	433.93	13.09	433.76
0+64.2	Pipe		8.78	425.15
0+64.2	Ground		9.7	424.2
T.P.	0.06	420.98	13.01	420.92
0+72			2.0	419.0
0+92			9.5	411.5
T.P.	0.19	408.50	12.67	408.31
1+12			4.0	404.50
1+36			11.3	397.2
1+57			18.0	390.5
1+82			25.1	383.4
2+00	channel		29.9	378.6

BC

## IMPROVED TABLES AND INFORMATION

Profile for change  
in Culvert No 3  
Redland Gardens



Redland Drive

BM	11.74	446.85	435.11
0-10 M. Box		8.86	
T.P.	0.17	433.93	13.09
0+62 <sup>nd</sup> FL Pipe		8.78	
0+62 <sup>nd</sup> ground		9.7	
T.P.	0.06	420.98	13.01
0+72		2.0	
0+92		9.5	
T.P.	0.19	408.50	12.67
1+12		4.0	
1+36		11.3	
1+57		18.0	
1+82		25.1	
2+00 channel		29.9	

441

9 12.41  
97  
38

662.3 667.3  
24.5 35.1  
686.8 697.41

10.00  
97  
1376

794  
795  
62  
733  
752  
772  
789

795  
56  
739

8106  
2993  
5113

51  
50 = 10  
5

50 51 10.8  
50  
100

51  
50

51 50 10.8

500

85.2

3

255.6

110

365.6

21

320.6

437.50  
172  
435.78

700  
5.11  
8.15