1242

Our Leather Bound Engineers Note Books are carried in the following rulings:

No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.

No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.

No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.

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THE FREDERICK POST CO.

ENGINEERING and DRAFTING SUPPLIES

IRVING PARK STATION

CHICAGO, ILL.

54th Adams Plotted to Collier	Page 1
Collier Plotted Not linked 54TH 844' West	8
No? 1st Collier South	15
No? 2 St Collier South	19
Collier Plotted 54TH 55TH	24
Alley Blk 184 Univ. Hts. Lincoln to Richmond	34
" " 3. Frary Hts	44
Cooper Ave. Cont. from Book 1235	46
Alley Blk. 184 Univ. Hts.	45
X Sec. Kalmia	53
X Sec Maple W.L. Vancouver to Haller	61-67
X sec Boundary St.	68-77
Grade stakes Alley	
Valle Vista Terrace	78

Discontinued Apr 30 7/Wilson Mfg.

Cross Section 54th St 50' Wide — 10' Cls 7.5 ft S

from Adams to Collier

Plotted

See Book 1241 Page 64

S.W. B.M. Adams & Collier	491	422.13	417.22
5' South S.L. Adams			
E		8.6	413.53
cb.		8.9	413.23
¼		9.0	413.13
℄		9.3	412.83
¼		9.6	412.53
cb.		9.6	412.53
W		9.8	412.33
+5		9.9	412.23
S.L. Adams			
W - 5		9.9	412.23
W		9.6	412.53
cb.		9.3	412.83
¼		9.5	412.63
℄		9.2	412.93
¼		8.6	413.53
cb.		8.5	413.63
E		8.0	414.13
South cb.			
E		7.9	414.23
cb.		8.3	413.83
¼		8.5	413.63
℄		8.5	413.63
¼		8.8	413.33

422.13

F.B. 1284 p 43 for 60' Street

1

cb.	8.6	413.53
W	8.7	413.43
+5	8.1	413.33
South ¼		
-5	8.9	413.73
W	8.3	413.83
cb. on Pav.	8.3	413.83
¼ " "	8.2	413.93
℄ " "	8.1	414.03
¼ " "	8.0	414.13
cb " "	7.9	414.23
E " "	7.8	414.33
℄ Adams		
E on Pav	7.5	414.63
cb. " "	7.7	414.43
¼ " "	7.9	414.23
℄ " "	8.0	414.13
¼ " "	8.1	414.03
cb. " "	8.2	413.93
+5	7.8	414.33
W	8.0	414.13
N ¼		
W	7.7	414.43
cb. on Pav	8.0	414.13
¼ " "	8.0	414.13
℄ " "	7.9	414.23

422.13

℄ on Pav	7.7	414.43
cb " "	7.7	414.43
E " "	7.5	414.63
N cb.		
E	7.4	414.73
cb	7.6	414.53
℄	7.7	414.43
℄	7.7	414.43
℄	7.8	414.33
+4	8.0	414.13
cb.	7.6	414.53
W	7.5	414.63
N to Pclamp = 0+00		
W	7.3	414.83
cb.	7.4	414.73
+4	7.8	414.33
℄	7.6	414.53
℄	7.4	414.73
℄	7.5	414.63
+5	7.8	414.33
cb.	7.5	414.63
+3	6.6	415.53
E	6.5	415.63
0+06 = ℄ Palm tree on W 4' Back.	7.2	414.93
+25 = " " " " " "	6.8	415.33
+15 = " Plumosa Palm on E 5' Back	6.2	415.93

422.13 5445 Sf

0+46 = ℄ Plumosa Palm Tree on E 5' Back	5.7	416.43
+78 = " " " " " " "	5.2	416.93
1+09 = " " " " " " "	5.4	416.73
+41 = " " " " " " "	5.1	417.03
+73 = " " " " " " "	4.8	417.33
2+04 = " " " " " " "	5.1	417.03
+36 = " " " " " " "	5.2	416.93
0+37 = ℄ Con. Drive on West.		
E	5.9	416.23
+7	6.1	416.03
cb.	7.1	415.03
℄	6.9	415.23
℄	6.9	415.23
℄	7.1	415.03
+7 = toe of Plumas	7.01	415.11
cb. on "	6.90	415.23
+3 " drive = Bck	6.43	415.70
W	6.44	415.69
0+70		
W	6.2	415.93
+7	6.2	415.93
cb.	6.8	415.33
℄	6.7	415.43
℄	6.4	415.73
℄	6.5	415.63
cb.	6.6	415.53

		422.13		
+1			6.5	415.63
+2			5.8	416.33
E.			5.9	416.73
	1+00			
E			5.7	416.43
+7			5.7	416.43
+8			6.1	416.03
cb.			6.4	415.73
¼			6.3	415.83
℄			6.2	415.93
¼			6.4	415.73
cb.			6.6	415.53
+1			6.5	415.63
+2			5.9	416.23
W			6.0	416.13
	1+50			
W			6.0	416.13
+8			6.0	416.13
cb.			6.4	415.73
+1			6.5	415.63
¼			6.3	415.83
℄			6.1	416.03
¼			6.1	416.03
cb.			6.2	415.93
+1			6.0	416.13
+2			5.6	416.53

		422.13	54+½ St.	
E			5.0	417.13
	2+00			
E			5.5	416.63
+8			5.7	416.43
cb.			6.2	415.93
¼			6.1	416.03
℄			6.0	416.13
¼			6.3	415.83
+6			6.3	415.83
cb.			6.1	416.03
+1			5.8	416.33
W.			5.8	416.33
	2+50 = St. Bridge St. 40' wide 5'6" 7.5'0"		=St. corner	
W			6.0	416.13
+7			6.0	416.13
+8			6.2	415.93
cb.			6.1	415.73
¼			6.4	415.73
℄			6.1	416.03
¼			6.4	415.73
cb.			6.5	415.63
+7			5.8	416.33
E			5.5	416.53
	3 cb.			
E			6.5	415.63
cb.			6.6	415.53

		422.18		
¼			6.4	415.73
℄			6.3	415.83
¼			6.4	415.73
Cb.			6.6	415.53
X			6.4	415.73
	S ¼			
W			6.6	415.53
Cb.			6.6	415.53
¼			6.4	415.73
℄			6.3	415.83
¼			6.4	415.73
Cb.			6.5	415.63
E			6.6	415.53
	℄			
5			6.6	415.53
Cb.			6.4	415.73
¼			6.4	415.73
℄			6.4	415.73
¼			6.6	415.53
Cb.			6.6	415.53
W			6.7	415.43
	N ¼			
W			6.8	415.33
Cb.			6.8	415.33
¼			6.5	415.63
℄			6.4	415.73

		422.13	54½	SF
¼			6.4	415.73
Cb.			6.6	415.53
E			6.7	415.43
	N Cb.			
E			6.7	415.43
Cb.			6.8	415.33
¼			6.7	415.43
℄			6.5	415.63
¼			6.6	415.53
Cb.			6.8	415.33
Y			6.8	415.33
	N Cb. +2'			
W			6.2	415.93
+8			6.4	415.73
Cb.			7.0	415.13
¼			6.7	415.43
℄			6.5	415.63
¼			6.7	415.43
Cb			6.8	415.33
+4			6.8	415.33
+5			6.0	416.13
E			5.8	416.33
	NL Collier = 0+00			
E			5.9	416.23
+7			6.3	415.83
+9			6.8	415.33

		422.13			
cb.			69	415.23	
↓			67	415.43	
↓			65	415.63	
↓			68	415.33	
+6			70	415.13	
cb.			68	415.33	
+2			62	415.93	
W			63	415.83	
T.P.	0.62	418.07	468	417.45	BM. Nails in Pole S.W. Collier + 54th
	0+50				
W			27	415.37	
+8			28	415.27	
cb.			35	414.57	
↓			35	414.57	
↓			33	414.77	
↓			35	414.57	
cb.			36	414.47	
+2			30	415.07	
E			29	415.17	
	1+00				
-5			50	413.07	
E			48	413.27	
cb.			49	413.17	
↓			48	413.27	
↓			45	413.57	
↓			46	413.47	

	418.07	54TH St.		
cb.		49	413.17	
+?		36	414.47	
W		33	414.77	
	1+50			
W		46	413.47	
+5		50	413.07	
+7		55	412.57	
cb.		64	411.67	
↓		63	411.77	
↓		61	411.97	
↓		62	411.87	
cb.		63	411.77	
E		62	411.87	
+5		63	411.77	
	1+59			
-5		64	411.67	
E		63	411.77	
cb.		65	411.57	
↓		63	411.77	
↓		63	411.77	
↓		65	411.57	
cb.		66	411.47	
+3		63	411.77	
+5		57	412.37	
W		50	413.07	5' CbS

1+63.87 = S.E. Collier St. as Measured. 5' ↓S

418.07

W			6.0	412.07
+5			6.7	411.37
Cb.			6.7	411.37
I			6.6	411.47
D			6.4	411.67
¼			6.4	411.67
Cb			6.6	411.47
E			6.6	411.47
+5			6.6	411.47
	S Cb.			
-5			7.0	411.07
E			6.9	411.17
Cb			6.8	411.27
¼			6.6	411.47
D			6.5	411.57
¼			6.7	411.37
Cb			6.6	411.47
W			6.7	411.37
	S ¼			
W			6.6	411.47
Cb.			6.8	411.27
¼			6.7	411.37
D			6.7	411.37
¼			6.7	411.37
Cb.			7.0	411.07
E			7.1	410.97

418.07 54TH St.

+5			7.2	410.87
	D.			
-5			7.4	410.67
E			7.3	410.77
Cb.			7.1	410.97
¼			6.8	411.27
D			6.7	411.37
¼			6.8	411.27
Cb.			6.9	411.17
W			6.7	411.37
	N ¼			
W			6.8	411.27
Cb			7.0	411.07
¼			6.9	411.17
I			6.9	411.17
¼			7.0	411.07
Cb.			7.1	410.97
E			7.4	410.67
+5			7.7	410.37
	N Cb.			
-5			8.1	409.97
E			7.8	410.27
Cb.			7.4	410.67
¼			7.4	410.67
D			7.2	410.87
¼			7.0	411.07

418.07

cb.		7.1	410.97
W		7.0	411.07
	N.L. Collier		
W		6.8	411.27
cb.		7.2	410.87
℄		7.3	410.77
℄		7.4	410.67
℄		7.5	410.57
cb		7.6	410.47
E.		8.0	410.07
+10		8.8	409.27
	15' N N.L. Collier on West.		
-10		10.5	407.57
-5		2.8	408.27
E.		7.1	408.97
cb.		8.1	409.97
℄		7.9	410.17
℄		7.9	410.17
℄		7.7	410.37
cb		7.6	410.47
W		7.5	410.57

5445 St.

Water Rupingert: T
Rupinger = cb.
4 pegs shown = 804

Cross Section Collier St. 30' wide 5' cbs 5' ¼ S

From 54th St. West

Plotted Not inked.

418.07 = π from Page 7

0+00 = W.L. 54th

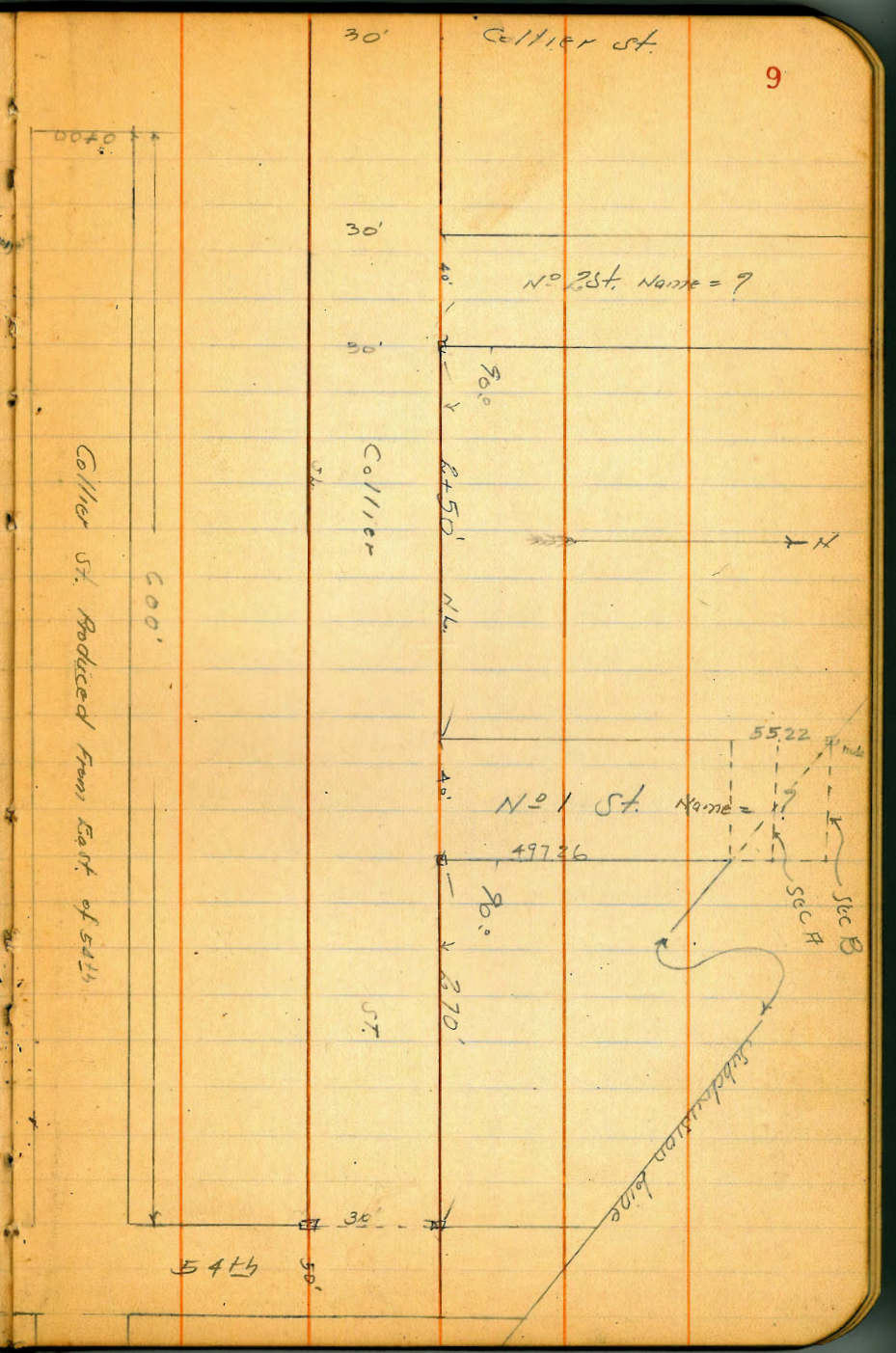
-5		7.1	412.97
N		6.8	411.27
cb.		7.0	411.07
¼		6.8	411.27
℄		6.7	411.37
¼		6.6	411.47
cb.		6.7	411.37
S		6.0	412.07
	0+50		
-5		4.1	413.97
S		4.6	413.47
+2		5.5	412.57
cb.		5.6	412.47
¼		5.3	412.77
℄		5.3	412.77
¼		5.4	412.67
cb		5.6	412.47
N		5.8	412.27
+1.7		4.9	413.17
+5		5.0	413.07
	1+00		
-5		3.9	414.17
N		4.9	413.17

418.07

cb.		4.7	413.37
¼		4.6	413.47
℄		4.6	413.47
¼		4.5	413.57
cb.		4.7	413.37
S		4.7	413.37
+5		3.8	414.27
	1+50		
-5		4.1	413.97
S		4.1	413.97
+1		4.9	413.17
cb		4.8	413.27
¼		4.6	413.47
℄		4.6	413.47
¼		4.6	413.47
cb.		4.8	413.27
N		4.8	413.27
+5		4.2	413.87
	2+00		
-5		5.0	413.07
N		5.3	412.77
cb.		5.1	412.97
¼		5.0	413.07
℄		4.9	413.17
¼		4.9	413.17
cb.		5.0	413.07

418.07

S			5.0	413.07	
+5			4.5	413.57	on rock in Collier East of Intersection on North
I.P.	210	415.26	4.91	413.16	
	2+50				
-5±			1.5	413.76	
S			1.7	413.56	
+1			2.4	412.86	
cb			2.3	412.96	
¼			2.0	413.26	
¼			2.1	413.16	
½			2.2	413.06	
cb			2.3	412.96	
N			2.4	412.86	
+5			2.0	413.26	
	2+70 = E.L.		N°1 St.	40' wide	
N			2.0	413.26	
+1			2.6	412.66	
cb			2.4	412.86	
¼			2.4	412.86	
¼			2.3	412.96	
¼			2.2	413.06	
cb			2.3	412.96	
S			2.0	413.26	
+5			1.5	413.76	
	2+90 = ℄ N°1 St				



	4+526			
-5		14	413.86	
S		18	413.46	
+1		24	412.86	
cb		25	412.76	
·4		23	412.96	
d		23	412.96	
·4		23	412.96	
cb		24	412.86	
N		23	412.96	
	3+10 = W6. N°1 N.			
N		20	413.26	
+2		26	412.66	
cb.		26	412.66	
·4		24	412.86	
d		23	412.96	
·4		22	413.06	
cb		24	412.86	
+4		25	412.76	
S		25	412.76	
+5		17	413.56	
	3+50			
-5		23	412.96	
S		24	412.86	
+1		30	412.26	
cb		31	412.16	
·4		29	412.36	

	415.26	Silver St.		
d		27	412.56	
·4		29	412.36	
cb.		32	412.06	
N		31	412.16	
+3		23	412.96	
	4+00			
-5		23	412.96	
N		34	411.86	
+1		40	411.26	
cb.		38	411.46	
·4		35	411.76	
d		35	411.76	
·4		35	411.76	
cb.		37	411.56	
+4		37	411.56	
S		32	412.06	
+5		28	412.46	
	4+50			
-5		35	411.76	
S		39	411.36	
+1		46	410.66	
cb.		45	410.76	
·4		42	411.06	
d		40	411.26	
·4		41	411.16	
cb.		43	410.96	

41526

N		4.5	410.76
+5		3.6	411.66
	5+00		
-5		3.9	411.36
N		4.9	410.36
+2		5.8	409.46
cb.		5.6	409.66
1		5.0	410.26
2		5.1	410.16
4		5.2	410.06
cb.		5.4	409.86
S		5.3	409.96
+5		4.5	410.76
	5+30		
-5		5.6	409.66
S		6.4	408.86
cb.		6.5	408.76
4		6.3	408.96
2		6.2	409.06
1		6.2	409.06
cb.		6.3	408.96
+1		6.4	408.86
+3		6.8	408.46
+4		6.8	408.46
N		5.8	409.46
+5		4.8	410.46

41526 Collier St.

	5+60 = Lt. No 2 St. 40' wide		
N		6.4	408.86
+2		7.4	407.86
cb.		7.7	407.56
1		7.6	407.66
2		7.7	407.56
4		7.6	407.66
cb.		7.8	407.46
S		8.0	407.26
+5		8.1	407.16
	5+65		
-5		8.2	407.06
S		8.2	407.06
cb.		8.0	407.26
1		7.8	407.46
2		7.8	407.46
1		7.8	407.46
cb.		7.8	407.46
N		7.8	407.46
	5+80 = 2 N. 2 Street		
N		7.9	407.36
cb.		8.0	407.26
1		8.1	407.16
2		8.2	407.06
1		8.1	407.16
cb.		8.1	407.16

41526

S		8.2	407.06	
+5		8.2	407.06	
	5+95			
-5		9.0	406.76	
S		8.6	406.66	
cb.		8.6	406.66	
¼		8.7	406.56	
℄		8.5	406.76	
¼		8.5	406.76	
cb.		8.3	406.96	
N		8.7	406.56	
	6+00 = W.L. N° 2 Street			
N.		9.5	405.76	
cb.		9.4	405.86	
¼		9.0	406.26	
℄		9.0	406.26	
¼		8.9	406.36	
+1		11.4	403.86	
+1		11.4	403.86	
¼		9.1	406.16	
cb.		8.9	406.36	
S		9.3	405.96	
+5		9.3	405.96	
	6+10			
-10		13.1	402.16	
-6		12.7	402.56	

41526 Corner St.

S-5			13.7	401.36
S			13.6	401.66
+2			12.3	402.96
cb.			12.0	403.26
¼			12.7	404.56
℄			12.3	404.96
¼			12.7	404.56
cb.			12.9	404.36
N			12.7	404.56
+5			12.2	405.06
	6+30			
T.P.	0.28	403.09	12.35	402.91
-10			1.4	401.79
N			2.0	401.19
cb.			2.5	400.69
¼			3.2	399.99
℄			3.7	399.49
¼			4.4	398.79
cb.			5.1	398.09
S			5.6	397.59
+25			7.7	395.29
	6+60			
-25			13.0	390.19
S			10.4	392.79
cb.			9.7	393.49
¼			8.8	394.39

40319

℄			7.9	395.29
¼			7.1	396.09
cb.			6.7	396.49
N.			6.4	396.79
+10			5.1	398.09
	7+00			
-10			10.2	392.99
N.			11.5	391.69
cb.			12.3	390.89
¼			12.4	390.79
℄			13.1	390.09
¼			13.5	389.69
cb.			14.2	388.99
S			14.4	388.79
+25			17.4	385.79
T.P.	1.18	391.34	13.03	390.16
	7+40			
-25			10.4	380.94
S			7.8	383.54
cb.			7.3	384.04
¼			6.7	384.64
℄			6.3	385.04
¼			5.9	385.44
cb.			5.3	386.04
N			4.7	386.64
+10			3.4	387.94

39134 Collier St.

	7+70			
-10			7.7	383.64
N			8.4	382.94
cb.			9.1	382.24
¼			9.6	381.74
℄			10.0	381.34
¼			10.4	380.94
cb.			10.8	380.54
S			11.4	379.94
+25			14.5	376.84
	8+00			
-25			20.4	370.94
S			17.0	374.34
cb.			15.9	375.44
¼			15.2	376.14
℄			14.7	376.64
¼			14.4	376.94
cb.			14.1	377.24
N			13.7	377.64
+10			12.8	378.54
	8+44 = End.			
-10			21.2	370.14
N			21.8	369.54
cb.			22.4	368.94
¼			22.6	368.74
℄			23.1	368.24

Collier St.

391.34

¼			23.4	367.94
cb.			24.2	367.14
S			24.8	366.54
+25			30.0	361.34
T.P.	11.59	402.78	0.15	391.19
T.P.	11.57	413.82	0.53	402.25
T.P.	6.99	420.14	0.67	418.15
Ckhon SW. BM. Collier + 54.5			2.70	417.44
" " " "			2.95	417.19

on Rock in Road Page 9

Adams + Kinsco Pk.

417.22 = BM
0.03

Walker Rod Bringer = W.
Harry = ch.
Shea = Rod
5-19-20

Cross Section No 1 St 40' Wide 5'Cbs 7.5'Fs

From N.L. Collier St North

See Sketch Page 9

	5.06	418.22		413.16
	0+00 = N.L. Collier			
E			4.8	413.42
cb.			5.2	413.02
¼			5.3	412.92
℄			5.1	413.12
¼			5.3	412.92
cb.			5.3	412.92
W			4.9	413.32
	0+50			
W			5.2	413.02
cb.			5.0	413.22
+2			5.6	412.62
¼			5.4	412.82
℄			5.2	413.02
¼			5.2	413.02
cb			5.2	413.02
+1			4.7	413.52
E			4.7	413.52
	1+00			
E			4.5	413.72
+4			4.6	413.62
cb.			4.9	413.32
¼			4.9	413.32
℄			4.9	413.32

Top of Rock Page 9

418.22

¼		5.1	413.12
+5		5.4	412.82
cb		4.6	413.62
W		4.6	413.62
	1+50		
W		4.6	413.62
cb.		4.7	413.52
+1		5.5	412.72
¼		5.2	413.02
℄		4.9	413.32
¼		5.0	413.22
cb.		4.9	413.32
+1		4.5	413.72
E		4.6	413.62
	2+00		
E		5.1	413.12
cb.		5.4	412.82
¼		5.4	412.82
℄		5.4	412.82
¼		5.5	412.72
+5		5.6	412.62
cb.		4.8	413.42
W		4.8	413.42
	2+30		
W		4.3	413.92
+4		4.5	413.72

		41822		
cb.			57	412.52
i			57	412.52
d			56	412.62
i			54	412.82
cb.			56	412.62
E			51	413.12
	2+60			
E			57	412.52
+4			57	412.52
cb.			60	412.22
i			61	412.12
d			61	412.12
i			63	411.92
+6			63	411.92
cb			57	412.52
W			53	412.92
	3+00			
W			55	412.72
cb			58	412.42
+1			68	411.42
i			70	411.22
d			68	411.42
i			71	411.12
cb			73	410.92
+2			69	411.32
E			69	411.32

		41822	N°1 St. X. Section	
	3+35			
5-10			91	409.12
E			81	410.12
cb.			78	410.42
i			78	410.42
d			76	410.62
i			76	410.62
+5			76	410.62
cb			67	411.52
W			64	411.72
	3+65			
W			69	411.32
cb.			70	411.22
+2			79	410.32
i			79	410.32
d			80	410.22
i			82	410.02
cb.			82	410.02
E			86	409.62
+10			105	407.72
	4+00			
-15			135	404.72
E			103	407.92
cb.			94	408.82
i			91	409.12
d			88	409.42

¼		8.6	409.62
+5		8.5	409.72
cb.		7.8	410.42
W		7.6	410.62
	4+25		
W		8.3	409.92
cb.		8.6	409.62
+1		9.3	408.92
¼		9.7	408.52
℄		9.7	408.52
¼		10.0	408.22
+4		10.5	407.72
cb.		11.2	407.02
℄		12.3	405.92
+15		14.6	403.62
	4+50		
-15		17.4	400.82
℄		14.3	403.92
cb.		12.5	405.72
+3		11.6	406.62
¼		10.9	407.32
℄		10.5	407.72
¼		10.1	408.12
+5		9.7	408.52
cb.		8.9	409.32
W		8.6	409.62

	4+75		
W		9.7	408.52
cb.		10.1	408.12
+2		10.9	407.32
¼		11.2	407.02
℄		11.7	406.52
¼		12.0	406.22
+4		13.2	405.02
cb.		15.2	403.02
℄		16.9	401.84
+15		21.5	396.72
		Section at Pt. D to No 1 St.	
	4+97.26 = Subdivision line on East		
-15		24.7	393.52
℄		20.0	398.22
cb		17.6	400.62
¼		18.5	401.72
℄		12.5	405.72
¼		12.4	405.82
cb.		12.0	406.22
W		11.2	407.02
		Section at Pt. D to No 1 St.	
	5+24.87 = Sec. A		
W		13.6	404.62
cb.		13.6	404.62
¼		14.3	403.92
+3		14.3	403.92
℄		15.9	402.32

418.22

¼		20.7	397.52
cb.		23.2	395.02
E		24.6	393.62
+2.5		29.5	388.72
	5+52.48 = Sec 8	Section at ℄ Δ to No 1 st	
-2.5		38.2	380.02
E		27.3	390.92
cb.		27.0	391.22
+5		26.5	391.72
¼		25.5	392.72
E		24.0	394.22
¼		20.9	397.32
+2		20.0	398.22
cb.		18.1	400.12
N		16.9	401.32
+10		15.4	402.82

No 1 st.
Δ Section

Walker Rapinoe Shirley Shaw 3-13-28

Cross Section №2 St. 40' Wide 5'C&S 7.5 ½S

From N.L. Collier St. North
(See sketch Page 9)

					T.P. on Rock
	5.06	418.22		413.16	Page 9
T.P.	2.45	414.83	5.84	412.38	
	0+00 = N.L. Collier				
E			6.0	408.83	
+4			6.2	408.63	
cb.			7.4	407.43	
½			7.5	407.33	
L			7.4	407.43	
¼			7.7	407.13	
cb.			8.2	406.63	
¼			8.9	405.93	
+10			10.1	404.73	
	0+50				
-5			6.9	407.93	
¼			6.5	408.33	
+4			6.7	408.13	
cb.			7.3	407.53	
¼			6.9	407.93	
L			6.7	408.13	
¼			6.6	408.23	
cb.			6.8	408.13	
+2			5.3	409.23	
E			5.0	409.53	
	1+00				
E			4.7	410.13	

	41483			
+3		4.9	409.93	
cb.		6.1	408.73	
¼		6.1	408.73	
L		6.3	408.53	
¼		6.4	408.43	
+6		6.8	408.03	
cb.		6.2	408.63	
¼		6.3	408.53	
+5		6.3	408.53	
	1+50			
-5		6.5	408.33	
¼		6.5	408.33	
+4		6.4	408.43	
cb		6.9	407.93	
¼		6.3	408.53	
L		6.0	408.83	
¼		6.1	408.73	
cb.		6.2	408.63	
+1		5.1	409.73	
E		4.8	410.03	
	2+00			
E		4.8	410.03	
+4		5.3	409.53	
cb		5.8	409.03	
¼		5.9	408.93	
L		5.8	409.03	

¼		6.1	408.73
cb.		6.5	408.33
+1		6.2	408.63
℄		6.4	408.43
+5		6.5	408.33
	2+50		
℄		5.7	409.13
+4		5.8	409.03
cb.		6.3	408.53
¼		5.8	409.03
ℓ.		5.4	409.43
¼		5.5	409.33
+6		5.3	409.53
cb.		4.6	410.23
E.		4.2	410.63
	3+00		
E.		4.0	410.83
+4		4.3	410.53
cb.		5.2	409.63
¼		5.2	409.63
ℓ.		5.1	409.73
¼		5.5	409.33
+6		6.0	408.83
cb.		5.4	409.43
℄		5.3	409.53
	3+55		

℄		5.0	409.83
+3		5.0	409.83
cb.		5.7	409.13
¼		5.2	409.63
ℓ.		5.0	409.83
¼		5.0	409.83
+6		5.0	409.83
cb.		4.1	410.73
E.		4.0	410.83
	3+95		
E.		3.8	411.03
+4		4.0	410.83
cb.		4.7	410.13
¼		4.8	410.03
ℓ.		4.7	410.13
¼		5.1	409.73
+6		5.3	409.53
cb.		4.9	409.93
℄		5.0	409.83
	4+30		
℄		4.3	410.53
+4		4.3	410.53
cb.		5.1	409.73
¼		4.8	410.03
ℓ.		4.6	410.23
¼		4.6	410.23

		41483		
+6			4.5	410.33
cb			3.9	410.93
E			3.8	411.03
	4+50			
E			3.8	411.03
+1			4.0	410.83
cb.			4.5	410.33
¼			4.5	410.33
℄			4.6	410.23
¼			4.8	410.03
+6			5.2	409.63
cb			4.8	410.03
W			5.2	409.63
	5+00			
W			5.2	409.63
+4			4.9	409.93
cb.			5.3	409.53
¼			4.9	409.93
℄			4.7	410.13
¼			4.5	410.33
cb.			4.5	410.33
+1			4.0	410.83
E			3.8	411.03
	5+50			
E			3.6	411.23
+4			3.9	410.93

		41483	N°2 St X. Section	
cb			4.5	410.33
¼			4.5	410.33
℄			4.4	410.43
¼			4.7	410.13
+1			5.0	409.83
cb.			4.5	409.33
W			4.5	409.33
T.P.	4.48	41448	4.82	410.00
	6+00			
W			4.4	410.08
+4			4.3	410.18
cb.			4.9	409.58
¼			4.6	409.88
℄			4.2	410.28
¼			4.3	410.18
cb.			4.5	109.98
+1			3.7	410.78
E			3.5	410.98
	6+50			
E			3.8	410.68
+4			4.0	410.48
cb.			4.5	409.98
¼			4.5	409.98
℄			4.4	410.08
¼			4.9	409.58
+6			5.1	409.38

cb.	46	409.88	
rr	47	409.78	
7+00			
rr	48	409.68	
+4	49	409.58	
cb.	53	409.18	
¼	50	409.48	
ℓ	47	409.78	
¼	48	409.68	
+6	49	409.58	
cb.	44	410.08	
E	42	410.28	
7+50			
E	46	409.88	
+4	48	409.68	
cb	53	409.18	
¼	51	409.38	
ℓ	50	409.48	
¼	53	409.18	
+6	55	408.98	
cb.	49	409.58	
rr	50	409.48	
8+00			
rr	53	409.18	
cb.	54	409.08	
+1	60	408.48	

¼	51	408.78	
ℓ	55	408.98	
¼	56	408.88	
+6	58	408.68	
cb.	53	409.18	
E	51	409.38	
8+50			
E	60	408.48	
cb.	60	408.48	
+1	68	408.68	
¼	65	407.98	
ℓ	63	408.18	
¼	65	407.98	
+6	69	407.58	
cb.	61	408.38	
rr	60	408.48	
9+00			
rr	74	407.08	
+2	75	406.98	
+3	80	406.48	
cb.	82	406.28	
¼	77	406.78	
ℓ	78	406.68	
¼	79	406.58	
cb.	88	405.68	
E	94	405.08	

		414.48	No 2 St. N. Section	
+10			10.0	404.48
	9+45.5	Section of Pl. A to No 2 St.		
25			23.8	390.68
E			16.8	397.68
Cb			14.7	399.78
¼			13.2	401.28
½			11.9	402.58
¾			10.0	404.48
+6			10.6	403.88
Cb			9.4	405.08
N			9.1	405.38
T.P.	7.00	417.35	4.13	410.35
Chk. on Rock. Page 9			4.20	413.15 +3.16 = Elev. Rock. 0.01 = Error.

Walter Rupbinger et Signal Proj 3-13-28

Cross Section Collier St. 40' wide 5' Cbs 7.5 1/4 S

As Per Sketch Page 9

Plotted 54th to 55th only

	also	54 to	600'	West	
	1.91	419.36		417.45	SW Cor Collier 1541
T.P.	0.71	407.10	12.97	406.39	
T.P.	0.52	394.84	12.78	394.32	
	0+00 = 600' W. of L. 54th				
-20			12.1	382.74	
S			12.8	382.04	
Cb.			13.8	381.04	
+5			14.2	380.64	
1/4			13.4	381.44	
℄			11.6	383.24	
1/4			10.7	384.14	
Cb.			10.2	384.64	
N			10.2	384.64	
+10			10.3	384.54	
	0+50				
-10			1.8	393.04	
N			2.4	392.44	
Cb.			2.5	392.34	
1/4			2.7	392.14	
℄			3.4	391.44	
1/4			3.8	391.04	
Cb.			4.3	390.54	
S			4.5	393.34	
+20			4.4	390.44	
T.P.	11.78	406.10	0.52	394.32	

Plotted

Yardage figured 54th to 55th T.G.H. 8-7-28

406.10

	1+00			
-10			7.7	398.40
S			7.5	398.60
Cb.			7.1	399.00
1/4			6.7	399.40
℄			6.4	399.70
1/4			6.1	400.00
Cb.			5.3	400.80
N			5.0	401.10
+5			4.2	401.90
	1+20			
-5			1.0	405.10
N			1.7	404.40
Cb.			2.0	404.10
1/4			2.5	403.60
℄			3.2	402.90
1/4			3.3	402.80
Cb.			3.7	402.40
S			3.6	402.50
+10			4.5	401.60
T.P.	10.69	416.56	0.23	405.87
	1+55			
-5			10.0	406.56
S			10.1	406.46
Cb.			10.5	406.06
1/4			10.1	406.46

℄		10.1	406.46	
℄		9.6	406.96	
cb.		9.5	407.06	
N		8.1	408.46	
1+94 = ℄ Rock in Tree on North 15in St		6.8	409.76	3" dia. 10' Rt.
2+19 = " " " " " "		6.1	410.46	" " "
+45 = " " " " " "		5.0	411.06	" " "
+69 = " " " " " "		4.3	412.26	" " "
3+08 = " " " " " "		3.3	413.26	" " "
+31 = " " " " " "		3.3	413.26	" " "
+53 = " " " " " "		2.7	413.86	" " "
	2+00			
N		6.6	~~409.96~~	
+4		6.8	409.76	
cb.		7.4	409.16	
℄		7.5	409.06	
℄		7.4	409.16	
℄		7.4	409.16	
cb.		7.4	409.16	
S		7.4	409.16	
	2+45			
S		6.1	410.46	
cb		6.0	410.56	
+7		6.3	410.26	
℄		6.7	410.36	
℄		5.9	410.66	

℄		6.1	410.46	
cb.		6.1	410.46	
+7		5.7	411.36	
N		5.0	411.56	5.7' Width
2+91 = ℄ Gravel Walk on North with curbs on Each side 4" 4" x 6" cbs 2' Back.				
N-2 on top ch		3.39	413.17	
N		3.9	412.66	
+3		4.1	412.46	
cb.		4.8	411.76	
℄		4.8	411.76	
℄		4.7	411.86	
℄		4.9	411.66	
+6		5.2	411.36	
cb.		4.6	411.96	
S		4.5	412.06	12' Wide
3+44 = ℄ Gravel Dr. on North with Con. cbs on each side 5" 5' in St.				
S		3.4	413.16	
+4		3.5	413.06	
cb		3.8	412.76	
℄		3.8	412.76	
℄		3.6	412.96	
℄		3.7	412.86	
cb.		3.5	413.00	
N		3.2	413.36	
N cb on top cb		2.91	413.65	
	4+00			

		416.56		
N			2.2	414.36
+3			2.2	414.36
cb.			3.0	413.56
¼			2.9	413.66
L			2.7	413.86
¼			2.9	413.66
cb.			3.0	413.56
+1			2.6	413.96
S.			2.6	413.96
	4+50			
S			1.7	414.86
+4			1.9	414.66
cb.			2.4	414.16
¼			2.3	414.26
L			2.2	414.36
¼			2.4	414.16
cb.			2.5	414.06
+1			1.9	414.66
N			1.6	414.96
TP	6.21	421.21	1.59	414.97
	5+00			
N			5.7	415.51
+4			5.7	415.51
cb.			6.4	414.81
¼			6.5	414.71
L			6.4	414.81

		421.21	Collier St.	
¼			6.4	414.81
cb.			6.5	414.71
+1			5.8	415.41
S			5.7	415.51
	5+50			
S			5.3	415.91
+4			5.5	415.71
cb.			6.1	415.11
¼			6.1	415.11
L			5.9	415.31
¼			6.1	415.11
cb.			6.2	415.01
+1			5.7	415.51
N			5.7	415.51
	6+00 =	N.L. 54½ St.		
N			5.4	415.81
+4			5.2	416.01
cb.			5.8	415.41
¼			5.8	415.41
L			5.6	415.61
¼			5.7	415.51
cb.			5.5	415.71
+1			5.1	416.11
S.			5.0	416.21
Chk. on SW Bolt Collier + 54½			3.75	
	0+00 =	E.L. 54½ St.		

421.21

Yardage figured 8-7-28 T. 16th

S		4.5	416.71	
+4		4.7	416.51	
cb.		5.5	415.71	
¼		5.7	415.51	
¿		5.6	415.61	
¼		5.7	415.51	
cb.		5.9	415.31	
+2		4.9	416.31	
N		4.9	416.31	3" dia 5' tall
0+11 = ℄ Phoenix Palm tree on South 5' Back		4.1	417.11	
+41 = " " " " " " "		4.2	417.01	
+71 = " " " " " " "		4.0	417.21	
1+00 = " " " " " " "		4.2	417.01	
+31 = " " " " " " "		4.0	417.21	
+62 = " " " " " " "		4.2	417.01	
+91 = " " " " " " "		4.5	416.61	
2+21 = " " " " " " "		4.3	416.91	
+52 = " " " " " " "		3.9	417.31	
+82 = " " " " " " "		4.2	417.01	
3+11 = " " " " " " "		5.3	415.91	
	0+50			
S		4.9	416.31	
cb.		5.3	415.91	
¼		5.7	415.51	
¿		5.4	415.81	
¼		5.7	415.51	

421.21

cb.		6.0	415.21	
+2		5.4	415.81	
N		5.2	416.01	
0+84 = ℄ Con. Wall on North on Line		5.27	415.94	4' wide on line
	1+00			
N		5.4	415.81	
+3		5.4	415.81	
cb.		5.9	415.31	
¿		5.7	415.51	
¿		5.5	415.71	
¿		5.6	415.61	
cb.		5.4	415.81	
S		4.8	416.41	
	1+50			
S		4.9	416.31	
cb.		5.3	415.91	
+3		5.8	415.41	
¿		5.7	415.51	
¿		5.4	415.81	
¿		5.7	415.51	
cb.		5.8	415.41	
+2		5.3	415.91	
N		5.1	416.11	
	2+00			
N		5.1	416.11	
cb.		6.0	415.21	

		421.21		
℄			5.8	415.41
℄			5.5	415.71
℄			5.8	415.41
cb.			5.6	415.61
S			4.8	416.41
	2+40			
S			4.5	416.71
+3			4.7	416.51
cb.			5.3	415.91
+5			6.2	415.01
℄			6.1	415.11
℄			5.9	415.31
℄			6.2	415.01
cb.			6.4	414.81
N			4.6	416.61
	2+82			
-5			6.7	414.51
N			6.7	414.51
cb.			6.7	414.51
℄			6.6	414.61
℄			6.3	414.91
℄			6.5	414.71
+5			6.6	414.61
cb.			5.8	415.41
S			4.5	416.71
T.P	2.69	417.48	6.42	414.79

		417.48.	Collier St.	
	3+31 = ℄ Conc. Walk on North to Residence			
S			2.1	416.38
cb.			3.2	414.28
℄			3.2	414.28
℄			3.0	414.48
℄			3.2	414.28
cb.			3.7	413.78
N on top Wall			3.33	414.15 4' Wide
3+45 = ℄ Conc. Drive on N			4.15	413.33 0.7' Back.
	3+71			
-5			4.3	413.18
N			4.3	413.18
cb.			4.1	413.38
℄			3.5	413.98
℄			3.3	414.18
℄			3.4	414.08
+5			3.5	413.98
cb.			2.9	414.58
S			2.3	415.18
3+41 = ℄ Pheonexa Palm tree on South 5' back			1.7	415.78
+71 = " " " " " " "			1.8	415.68
4+01 = " " " " " "			2.0	415.48
+32 = " " " " " "			2.3	415.18
+62 = " " " " " "			2.1	415.38
+91 = " " " " " "			2.4	415.08
5+32 = " " " " " "			3.4	414.08

		41748		
5+50 = ℄ Plumosa Palm trees on South 5' Back			5.3	412.18
6+43 = " " " " " " "			1.8	415.68
	4+06			
S			2.5	414.98
+4			3.1	414.38
cb.			3.8	413.68
¼			3.8	413.68
℄			3.6	413.88
¼			3.8	413.68
cb			4.1	413.38
N			3.7	413.78
+5			3.4	414.08
	4+50			
N			3.0	414.48
+2			3.2	414.28
cb			4.2	413.28
¼			4.1	413.38
℄			3.9	413.58
¼			4.2	413.28
cb.			4.2	413.28
S			3.0	414.48
	5+00			
S			3.2	414.28
cb.			4.4	413.08
¼			4.7	412.78
℄			4.5	412.98

		41748	Collier st	
¼			4.7	412.78
cb.			4.7	412.78
N			4.1	413.38
+5			3.7	413.78
+10			4.7	412.78
	5+15			
-15			11.2	406.28
N			5.6	411.88
cb.			4.9	412.58
¼			4.9	412.58
℄			4.6	412.88
¼			4.7	412.78
cb.			4.6	412.88
S			3.5	413.98
	5+31			
S			4.2	413.28
cb.			4.9	412.58
¼			4.9	412.58
℄			5.0	412.48
¼			5.1	412.38
cb.			5.8	411.68
N			9.7	407.78
+5			13.9	403.58
+10			19.4	398.08
	5+25			
-40			34.6	382.88

	41748		
←37	30.9	386.58	
←12.5	25.8	391.68	
N	11.9	405.58	
cb.	8.9	408.58	
+4	5.7	411.78	
¼	5.3	412.18	
d.	5.0	412.48	
¼	4.8	412.68	
cb.	5.0	412.48	
S	4.8	412.68	
+5	4.3	413.18	
5+50			
-5	5.3	412.18	
S	4.8	412.68	
cb.	5.0	412.48	
¼	4.8	412.68	
d.	5.0	412.48	
½	5.3	412.18	
+3	10.1	407.38	
cb.	11.6	405.88	
N	16.2	401.28	
+12.5	28.1	389.38	
+30	31.0	386.48	
+40	35.2	382.28	
5+55			
-46	31.5	385.98	

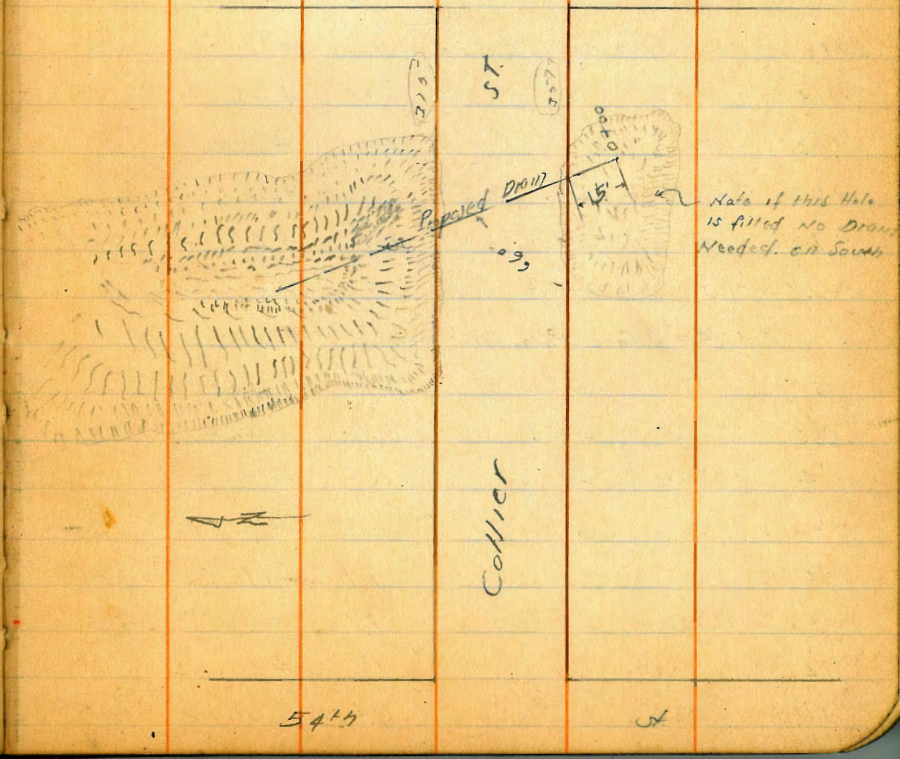
	41748		
-30	33.0	384.48	
-23	29.0	388.48	
N	11.9	405.58	
cb.	8.9	408.58	
+4	5.5	411.98	
¼	5.3	412.18	
d.	5.0	412.48	
¼	4.9	412.58	
cb.	5.1	412.38	
S	4.9	412.58	
+5	6.0	411.48	
5+85			
-15	10.6	406.88	
-5	10.6	406.88	
S	7.7	409.78	
cb.	5.2	412.28	
+2	4.8	412.68	
¼	4.6	412.88	
d.	4.6	412.88	
½	5.0	412.48	
+2	5.4	412.08	
cb.	10.4	407.08	
N	13.7	403.78	
+15	20.0	397.48	
+25	23.3	394.18	
+26	28.0	389.48	

+28		27.0	390.48
+30		23.0	394.48
+35		23.0	394.48
	6+00		
-20		17.7	399.78
-10		17.3	400.18
N		11.5	405.98
cb.		8.1	409.38
+5		4.5	412.98
¼		4.2	413.08
½		4.1	413.38
¼		4.2	413.28
cb.		5.1	412.38
+7		6.0	411.48
S		7.6	409.88
+10		9.7	407.78

Levels For Drain as Per Sketch opp. Page

0+00		10.3	407.18
+15 = South Prop Line		7.7	409.78
+27		4.8	412.68
+34		4.6	412.88
+47		5.5	411.98
+80		27.0	390.48
+88		30.6	386.88
+92		33.2	384.28
1+05 = End.		35.3	382.18

-10		21	415.38
S		27	414.78
cb.		23	415.18
¼		20	415.48
℄		20	415.48
¼		21	415.38
cb.		18	415.68
N		21	415.38

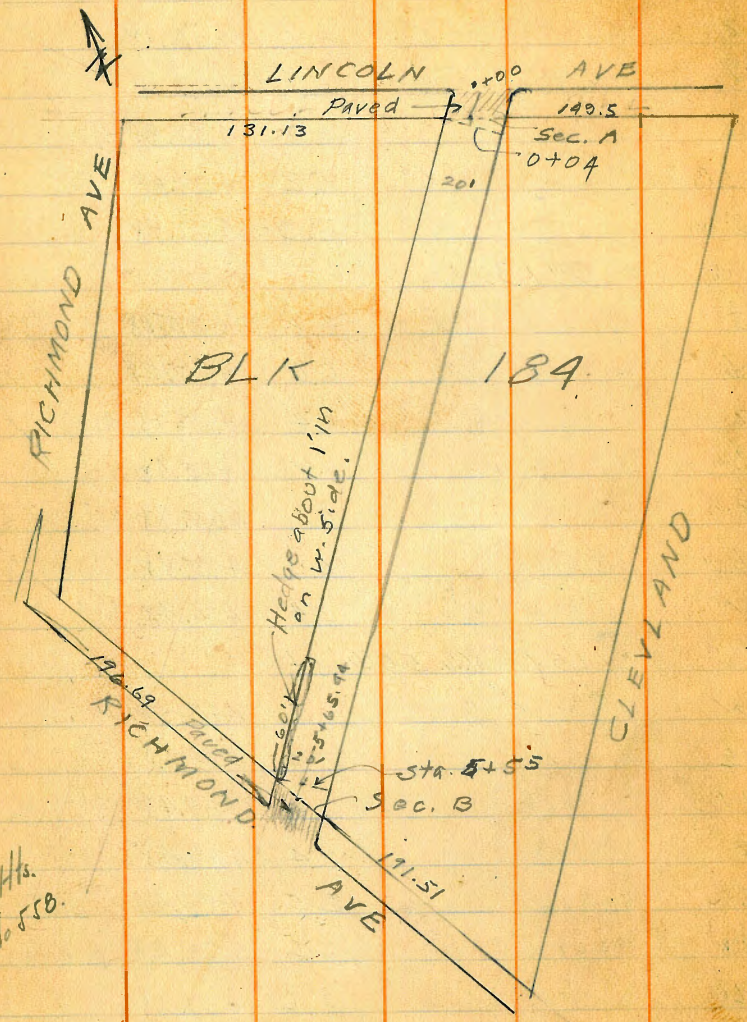


		41748		
+10			1.5	415.98
	6+60			
TP	12.88	42982	0.54	416.94
N			9.9	419.92
cb			13.1	416.72
¼			13.1	416.72
℄			13.0	416.82
¼			13.1	416.72
cb			12.9	416.92
+2			12.3	417.52
S			12.2	417.62
6+72 = ℄ Plumb to Point Rock on South Side of Road			11.0	419.82
7+04 = " " " " " " "			8.1	421.72
+32 = " " " " " " "			6.8	423.02
+62 = " " " " " " "			5.0	424.82
+93 = " " " " " " "			2.7	427.12
8+21 = " " " " " " "			0.5	429.32
7+04 = ℄ Con. Walk on North 3' wide				
S			8.7	421.12
cb			8.9	420.92
+4			10.8	419.02
+5			10.0	419.82
¼			9.9	419.92
℄			9.7	420.12
¼			9.8	420.02
cb			9.4	420.42

		42982		
+1 on Con. Walk			9.15	419.67
N " " "			8.70	421.12
+3 " " "			6.71	423.11
	7+25			
N			5.7	424.12
+2			6.2	423.62
cb			8.6	421.22
¼			8.4	421.42
℄			8.2	421.62
¼			8.3	421.52
+2			9.0	420.82
cb			7.9	421.92
S			7.5	422.32
	7+50			
S			6.0	423.82
cb			6.3	423.52
+2			7.0	422.82
+4			6.6	423.22
¼			6.5	423.32
℄			6.4	423.42
¼			6.4	423.42
cb			7.1	422.72
+3			4.4	425.42
N			4.4	425.42
	8+00			
N			1.6	428.22

		429.82		
+2			1.8	428.02
cb.			3.2	426.62
¼			3.0	426.82
℄			2.9	426.92
¼			3.0	426.82
+4			3.2	426.62
+6			4.1	425.72
cb.			2.9	426.92
S			2.6	427.22 Ribbon Dr.
8+31 = ℄ Can. Drive on South 25' in st. 11' Wide				
S on Drive			0.35	429.47
+05 " "			0.35	429.47
cb.			0.6	429.22
¼			0.7	429.12
℄			0.6	429.22
¼			0.5	429.32
cb.			0.8	429.02
+2			0.1	429.72
N			0.0	429.82
T.P.	12.47	441.88	0.11	429.41
8+53 = ℄ Plumosa Palm tree on S 5' Back			10.8	431.08
+83 = " " " " " " "			8.6	433.28
9+13 = " " " " " " "			5.8	436.08
+42 = " " " " " " "			3.2	438.68
	8+83			
N			8.3	433.58

		441.88		
cb.			8.6	433.28
¼			8.7	433.18
℄			8.7	433.18
¼			8.9	432.98
cb.			9.2	432.68
S			8.9	432.98
	9+13			
S			6.7	435.68
cb.			6.6	435.28
¼			6.4	435.48
℄			6.7	435.68
¼			6.1	435.78
cb.			6.0	435.88
N			5.4	436.48
	9+57 = W.L. 55th St.			
N			1.5	440.38
cb.			2.0	439.88
+1			2.4	439.48
¼			2.4	439.48
℄			2.5	439.38
¼			2.6	439.28
+6			2.6	439.28
cb.			2.2	439.68
S			1.8	440.08
Chk. on S.W.B.M. Adams & 55th			6.12	435.76
				435.77 = B.M. 0.01 = Error



Univ. Hts. Map No 558.

See P. 45 for Notes on Garages etc.

X Sections Alley Block 184 Univ. Hts. May 2-28. Loudon-Inst't.

Sta	+	H.I.	−	E.I.	
BM	2.77	313.51		310.74	B.P. S.W. Richmond & Hendrix 298.48
T.P.	6.46	318.73	1.24	312.27	

Scribing on T. Lincoln. top W. cb

Gutter at W.L.	4.70	314.03	
Gutter at ℄	4.64	314.09	
Gutter at E.L.	4.69	314.04	
top cb at E.L.	3.81	314.92	
Sec A. ✓			
E cb	3.63	315.10	
Pav. at E.L.	3.99	314.74	
℄ Pav.	4.30	314.43	
Pav at W.L	4.08	314.65	
W. cb (Ground Sec A Flushwith Pav.)	3.92	314.81	
0+04 ✓			
W.L	4.1	314.6	
℄	4.2	314.5	
+5	4.3	314.4	
E.L	4.8	313.9	
0+25			
E.L (earth on E.L floor Garage)	6.0	312.7	
+4	5.5	313.2	
℄	5.6	313.1	
W.L	5.3	313.4	
0+38 ✓	~~6.1~~		
W.L	6.1	312.6	

Plotted 5-7-28 Eisenbaugh

These Notes are 12.26 Ft Too high. Right BM 298.48 OK

Alley Blk 184

Sta	+	H.I	−	El
		318.73 ✓		
W.L.+5			6.4	312.3
℄			6.5	312.2
+7			6.3	312.4
E.L.			6.6	312.1
0+50	✓			
E.L.			7.8	310.9
℄			8.0	310.7
W.L			7.5	311.2
0+75	✓			
W.L.			9.7	309.0
℄			9.7	309.0
+5			9.7	309.0
E.L			9.4	309.3
1+00	✓			
E.L			10.5	308.2
℄			10.6	308.1
W.L			10.6	308.1
1+08	✓			
W.L.			10.1	308.1
+5			10.3	308.4
℄			10.8	307.9
E.L			10.8	307.9

Alley Blk 184.

Sta	+	H.I	−	El
1+14 ✓		318.73		
Brick - 3' E. Garage floor. E side			10.31	308.42
E.L.			10.6	308.1
℄			10.9	307.8
+4		old shack	11.6	307.1
W.L		earth - 1.5 in W side (Garage floor)	11.7	307.0
T.P	6.51	314.64	10.58	308.15
1+25 ✓				
W.L			6.5	308.2
℄			6.4	308.3
+6			6.0	308.7
E.L.			5.1	309.6
1+43 ✓				
E.L			2.4	312.3
℄			4.0	310.7
W.L			5.3	309.4
1+50 ✓				
W.L			4.0	310.7
℄			3.2	311.5
E.L			1.9	312.8
Garage floor 1+57		(cement - 7' W side	4.36	310.30
1+75 ✓				
E.L		earth - 8' E (Garage floor)	2.4	312.3
℄			3.8	310.9
W.L			4.6	310.1

Sta	+	H.I. 314.64	−	El.
Bar				
Garage floor (Cement)		1+75.5 W.	4.58	310.08
2+00 ✓				
Garage floor (Cement)		5' W.	5.23	309.43
W.L			5.2	309.5
℄			4.7	310.0
+6			4.0	310.7
E.L. (Euc. tree 1' in)			2.9	311.8
2+23 ✓				
E.L			5.2	309.5
℄			5.8	308.9
W.L			5.6	309.1
Garage floor (Cement)		5' W.	5.19	309.47
2+27 ✓				
5' W.			7.6	307.1
W.L			7.3	307.4
℄			6.9	307.8
+4			6.6	308.1
E.L			5.6	309.1
floor house		2' E.	3.64	311.02
2+37 ✓				
E.L.			6.4	308.3
℄			7.3	307.4
W.L			7.8	306.9
10' W			11.2	303.5

Alley Blk 184

Sta	+	H.I. 314.64	−	El.
2+50 ✓				
15' W			17.2	297.5
10' W			14.4	300.3
W.L			9.2	305.5
+5			7.2	307.5
℄			6.6	308.1
E.L			6.7	308.0
2+54 ✓				
8' E.			6.1	308.6
E.L			5.3	309.4
+5			6.6	308.1
℄			6.5	308.2
+5			7.1	307.6
W.L			9.0	305.7
12' W			17.4	297.3
22' W			19.6	295.7
2+67 ✓				
15' W			13.1	301.6
5' W			12.7	302.0
W.L			9.8	304.9
+7			6.1	308.6
℄			5.9	308.8
+6			5.5	309.2
E.L			4.7	310.0
10' E.			5.2	309.5
Garage floor		11' E. (earth)	5.71	308.95

Alley Blk 184

Sta	+	H.I	−	El.
2+95	✓	314.64		
10' E.			7.8	306.9
0' E.			5.9	308.8
E.L			5.9	308.8
+5			5.2	309.5
℄			5.3	309.4
+3			5.1	309.6
W.L			8.1	306.6
5' W			11.0	303.7
20' W			10.0	304.7
3+89	✓			
10' W.			4.5	310.2
5' W			5.5	309.2
W.L			5.0	309.7
+3			4.1	310.6
℄			4.4	310.3
E.L			4.7	310.0
4' E.			5.6	309.1
10' E.			6.2	308.5
3+00	✓		~~4.4~~	
5' E.			4.4	310.3
E.L.			4.4	310.3
℄			3.9	310.8
+5			3.4	311.3
W.L.	(earth)		3.3	311.4
Garage floor 5' E at 3+08			4.0	310.7

Alley Blk 184

Sta.	+	H.I	−	El
		314.64		
3+10	✓			
W.L			2.8	311.9
℄			2.9	311.8
E.L			3.8	310.9
T.P	4.82	316.84	2.62	312.02
3+25	✓			
E.L			4.9	312.0
℄			4.9	312.0
W.L			4.6	312.3
3+50	✓		~~4.6~~	
W.L	6' W Garage floor (earth)		4.6	312.7
℄			4.6	312.3
E.L.			4.2	3127
Garage	(cement) floor 1' E.		3.86	313.00
3+75				
Garage	floor 1' E.		4.20	312.66
E.L			4.3	312.6
℄			4.2	312.7
W.L			4.0	312.9
Cement walls on W.L			4.10	312.76
4+00				
W.L			3.9	313.0
℄			4.1	312.8
E.L			4.0	312.9
Garage	(earth) E.L floor at 4+08		3.81	313.05

Alley Blk 184

Sta	+	H.I. 316.84	−	El.
(Cement)	(1'W.) W. side.			
Garage floor at 4+08			3.97	312.89
4+25	0.5'E (Cement)			
E.L.	Garage floor)		3.83	313.03
℄			4.0	312.9
W.L			4.0	312.9
4+50 ✓				
	2'W (earth).			
W.L	(Garage floor)		4.4	312.5
℄			4.4	312.5
E.L	~~(Garage floor)~~		3.9	313.0
	0.5'E (Cement)			
Garage floor	~~on E.L~~		3.86	313.00
4+75				
E.L			4.0	312.9
℄			4.4	312.5
W.L			4.7	312.2
5+00 ✓				
W.L			4.8	312.1
℄			4.7	312.2
E.L			4.6	312.3
	0.5' E. (earth)			
Garage	floor at 5+10 E.L		4.7	312.2
5+25 ✓				
E.L			4.9	312.0
℄			4.9	312.0
W.L			5.0	311.9

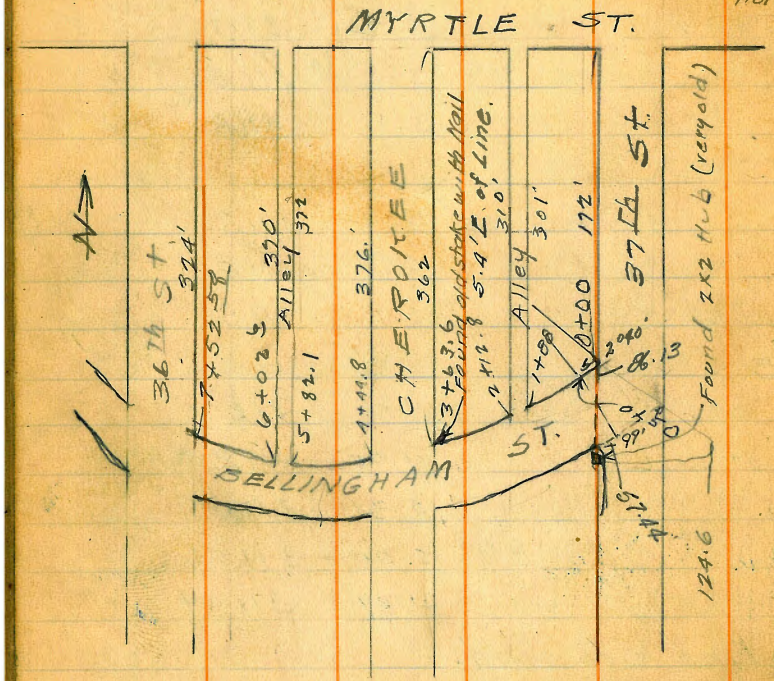
Alley Blk 184

Sta	+	H.I. 316.84	−	El.
5+50 ✓				
W.L			5.2	311.7
℄			5.1	311.8
E.L			5.1	311.8
5+55 ✓				
E.L.	Gar. floor (earth) 0.5'E.		5.2	311.7
℄			5.1	311.8
W.L			5.0	311.9
Sec B ✓				
W. cb.			4.86	312.00
Pav. at W.L			4.91	311.95
℄ Pav.			5.31	311.55
E.L. Pav.			5.00	311.86
E. cb			4.89	311.97
N cb. / ine Richmond.				
E. cb.			5.21	311.65
Gutter at E.L			5.83	311.03
Gutter at ℄			5.86	311.00
Gutter at W.L.			5.65	311.21
W. cb			5.06	311.80
B.M.			6.15	310.69

X Sections Bellingham From 36th To 37th

May 4-28

Loudon - Lundy Holbeck



Note:- All sections taken Radially unless otherwise Noted.

Curve aligned by eye only after measuring record distances on streets and alleys from Myrtle St. Stations measured by chords on North Line.

Sta	+	H.I.	-	El	
B.M	4.00	314.74		310.74	37th & Myrtle N.W. B.P.
T.P.	0.19	302.02	12.91	301.83	
Sec on W.L. of 37th					
N.L			12.3	289.7	
N.cb			12.4	289.6	
N¼			7.5	294.5	
E			11.0	291.0	
S¼			11.4	290.6	
S cb			12.2	290.8	
S.L			13.0	289.0	
0+50 - 0+57.44					
S.L			17.1	294.9	
S cb			15.4	286.8	
S¼			13.8	288.2	
+7			11.8	290.2	
E			11.2	290.8	
N¼			9.6	292.4	
N cb			8.6	293.4	
N.L			6.6	295.4	
1+00 - 1+12.88					
N.L			3.7	298.3	
N.C			5.2	297.8	
N¼			6.4	295.6	
E			7.9	294.1	
S¼			9.0	293.0	
S cb			10.8	291.2	

Sta	+	H.I	−	El	
1+00		302.02			
S.L			13.0	289.0	
1+50 = 171.32					1469.2
S.L			12.0	290.0	
Scb			10.5	291.5	
S¼			9.2	292.8	
℄			7.9	294.1	
N¼			6.5	295.5	
Ncb			4.9	297.1	
N.L			3.6	298.4	
1+88 = 215.99 S.L					2+12
N.L			4.5	297.5	
Ncb			5.9	296.1	
N¼			7.2	294.8	
℄			8.7	293.3	
S¼			10.5	292.5	
Scb			11.8	290.2	
S.L			13.0	289.0	
T.P.	5.20	298.17	9.05	292.97	
2+12.8 = 249.46 S.L					240
S.L			10.6	287.6	
Scb			9.4	288.8	
S¼			7.6	290.6	
℄			5.5	292.7	
N¼			4.6	293.6	

Sta	+	H.I	−	El	
2+12.8		298.17			
Ncb			3.0	295.2	
N.L			1.9	296.3	
2+50 = 237.20					2+87
N.L			2.0	296.2	
Ncb			4.0	294.2	
N¼			5.4	292.8	
℄			7.4	290.8	
S¼			9.2	289.0	
Scb			10.8	287.4	
S.L			12.2	286.0	
3+00 - 6+14.64			14		338
S.L			14.6	283.6	
Scb			12.3	285.9	
S¼			10.2	288.0	
℄			8.3	289.9	
N¼			6.2	292.0	
Ncb			4.6	293.6	
N.L.			3.0	295.2	
3+50 4402.08					394
N.L			5.6	292.6	
Ncb			6.9	291.3	
N¼			8.8	289.4	
℄			10.3	287.9	
S¼			12.2	286.0	

Sta	+	H.I	−	El
3+50 ✓		298.17		
S cb			14.1	284.1
S. L			16.0	282.2
T. P	1.75	291.92 ✓	8.00	290.17
3+50 ✓				
15' S			11.9	286.3
3+63.6 ✓		E line cherokee		
S. L			10.7	281.2
S cb			8.9	283.0
S ¼			6.9	285.0
℄			4.8	287.1
N ¼			3.4	288.5
N cb			1.3	290.6
N. L			−0.3	292.2
H+44.8 ✓	−5+22.58	N line cherokee		
N. L			3.2	288.7
N cb			4.6	287.3
N ¼			6.2	285.7
℄			7.9	284.0
S ¼			9.5	282.4
S cb			10.7	281.2
S. L			12.5	279.4
15' S.			14.1	277.8

Sta	+	H.I	−	El
5+00	5+85.95	291.92 ✓		
15' S			39.8	252.1
S. L.			32.2	259.7
S cb			26.9	265.0
S ¼			16.4	275.5
℄			11.9	280.0
N ¼			10.2	281.7
N cb			8.3	283.6
N. L			6.4	285.5
15' N			4.5	287.4
T. P	1.68	283.80 ✓	9.80	282.12
5+50	6+43.35			
15' N			0.8	283.0
N. L			3.7	280.1
N. cb			8.8	275.0
N ¼			13.0	270.8
℄			22.3	261.5
S ¼			25.1	258.7
S cb			30.8	253.0
S. L			36.3	247.5
25' S.			36.6	247.2
5+82	6+80.20 ✓			
20' S			30.6	253.2
S. L.			32.9	250.9
			33.7	250.1

Sta	+	H.I	-	El
		283.80		
5'/4			34.3	249.5
+8			33.9	249.9
℄			29.6	254.2
N'/4			22.9	260.9
N.cb			15.1	268.7
N.L			9.2	274.6
15' N			4.3	279.5
6+026	✓-7403.73			
15' N			8.1	75.7
T.P.	0.55	272.49	11.86	271.94
N.L			2.7	269.8
N.cb			11.6	260.9
T.P	1.73	263.98	10.24	262.25
N'/4			10.1	263.9
℄			14.1	259.9
S'/4			12.2	251.8
S.cb			7.9	256.1
S L			2.0	262.0
15' S.			-2.0	266.0
6+27	-7431.75		~~0.5~~	
15' N.			-0.5	264.5
N.L.			5.0	259.0
Ncb			8.7	253.3
N'/4			12.0	252.0

Sta	+	H.I	-	El.
6+27		263.98		6000
℄			8.1	255.9
5'/4			1.9	262.1
T.P.	11.36	✓274.58	0.76	263.22
S cb			10.0	264.6
S.L			3.0	271.6
15' S			-1.3	275.9
6+41	-7447.81			
15' N			20.1	254.5
N.L			21.6	253.0
N cb			20.2	254.4
N'/4			17.8	256.8
℄			12.1	262.6
S'/4			6.6	268.0
S cb			3.1	271.5
S.L			-1.8	276.4
15' S			-4.5	279.1
6+55	✓-7466.65			
15' N			18.5	256.1
N.L			16.8	257.8
Ncb			13.3	261.3
N'/4			6.2	268.4
℄			0.0	274.6
T.P	12.84	✓287.02	0.40	274.18
S cb			5.5	281.5

Sta	+	H.I	−	El.
6+55		287.02		
S.L.			4.4	282.6
15' S.			4.4	282.6
6+70				
15' S			3.6	283.4
S.L.			3.2	283.8
Scb			4.1	283.9
S 1/4			5.5	281.5
℄			8.5	278.5
N 1/4			12.2	274.8
N cb			16.8	270.2
N.L			21.0	266.0
15' N			23.2	263.8
6+85	+798.33			
15' N			16.4	270.6
N.L			13.8	273.2
N cb			10.2	276.8
N 1/4			7.2	279.8
℄			4.2	282.8
S 1/4			2.8	284.2
Scb			2.1	284.9
S.L			2.1	284.9
15' S			3.9	283.1
T.P.	8.65	294.63	1.04	285.98

Sta	+	H.I	−	El.
7+00	+813.55	294.63		
15' S			11.5	283.1
S.L.			9.8	284.8
Scb			9.2	285.4
S 1/4			9.4	285.2
℄			9.9	284.7
N 1/4			10.6	284.0
N cb			12.7	281.9
N.L.			16.4	278.2
15' N			18.4	276.2
7+17		S.E. Cor.		
15' N			13.7	280.9
N.L			11.5	283.1
N cb			9.5	285.1
N 1/4			6.1	286.5
℄			7.1	287.5
S 1/4			6.5	288.1
Scb			7.4	287.2
S.L			8.8	285.8
15' S			10.8	283.8
7+52	-875.91	N.E. line 36th Cor.		
15' S			11.7	283.4
S.L			8.6	286.0
Scb			6.3	288.3
S 1/4			5.0	289.6

Sta	+	H.I	−	El.	
7+52.58	/	294.63			
℄			4.6	290.0	
N/A			4.7	289.9	
N ch			5.2	289.4	
N.L			5.9	288.7	
15' N			7.0	287.6	
B.M	12.06	302.62	4.07	290.56	
T.P	13.03	315.27	0.38	302.24	
T.P.	12.80	328.04	0.03	315.24	
T.P	4.79	332.25	0.58	327.46	Dwight E 36th N.W B.P. (327.55)
B.M			4.78	327.47	

Notes on Alley Bk 5 Frary Hts.
Sec field book 1235 P56

Sta	+	H.I	−	El.	
	5.66	330.94		325.28	cb w.L. 0+00
0+75	6.2' E. N. Side 2 car garage		5.7	325.2	earth floor
0+97	6.3 E S side garage		5.7	325.2	" "
1+37 ℄	1 car garage 10.2' W		4.25	326.69	wood floor
1+61 ℄	Single garage 9.5' E				Conc. floor
T.P	6.75	332.26	5.43	325.51	
			7.13	325.18	
1+49	N end of Garage 1.3' in alley on W. Side Entrance on S. end. earth floor				
			4.7	327.6	
1+80	S end of Garage 1.5' in alley				
			4.8	327.5	
1+75	N side 2 car garage 4.5' E Conc. floor,				
			6.38	325.88	
1+93	S side 4' E same garage		6.50	325.76	
2+08	N end garage 0.4' in alley on E Side Entrance on N. Conc. floor		6.17	326.09	
2+23	S end same garage				
2+24	N end Garage 0.4' in alley Entrance on S. end earth floor				
2+40	S end same garage				
			6.0	326.3	
2+91 ℄	Single garage 5.5' E earth floor				
			5.4	326.9	

Same Garage

Alley Blk 3 Frary Hts.

Sta	+	H.I	−	El.	
		332.26			
3+02	N end 2 car garage Entrance on South end 1.6' W.		5.10	327.16	Conc. floor
3+20	S end same garage		5.17	327.09	
3+42 ℄	Single garage 0.9' E. Conc. floor		5.83	326.43	
3+92 ℄	Single garage 3' E earth floor		6.3		
0+94 ℄	Single garage 2.2' W. earth floor		5.8		
T.P		4.97	6.11	326.15	T.P
4+44 ℄	Single garage 4.8' E. Wood floor	331.12	4.79	326.33	
4+62	N. Side 2 car garage 6.9' W. Conc. floor		4.97	326.15	
4+82	S side same garage 6.6' W.		4.87	326.25	
5+07 ℄	Single garage 6' E (Lip 2.2 E.) Conc. floor		5.63	325.49	
T.P		4.54	5.71	325.41	
5+30 ℄	Single garage 4.5' W Conc. floor		4.79		
ok			7.41	322.74	

Notes on Alley Blk 184 Univ Hts.

(See P 34)

Sta	+	H.I	−	E.I.	
	1.28	316.38		315.10	
1+58	N end 2 car garage 7' W. Conc. floor		6.08	310.3	
1+96	Same garage 5.7' W		6.48	309.9	
1+96	Same garage		6.98	309.4	
2+23	S end Same garage 4.7' W		6.92	309.46	
1+78 ℄	Single garage earth floor. 6.5' E.		3.6	312.8	
T.P		9.22	8.21	308.17	
2+52	2 car garage 13' E N end. earth floor.		8.6		
2+72	S end same garage 12' E		8.4		
3+08 ℄	Single garage 4.5' E earth floor		6.8		
3+32	N end 2 car garage 0.6' back		4.12	313.27	wood floor N half Conc. floors ½
3+52	S end Same garage 0.6' E		4.43	312.96	
3+52	N end 2 car garage 0.6' E earth floor		4.6	312.8	
3+76	S end Same garage 0.6' E		4.8	312.6	

Sta	+	H.I.	−	El
		317.39		
3+56	℄ of Single garage 7.3' W. earth floor.		4.7	312.7
4+09	℄ Single garage 1.2' W Conc. floor		4.54	312.85
4+02	1 car garage Nend. 0.5' E earth floor.		4.5	312.9
4+41	S end same garage. 0.3' E		4.5	312.9
4+47	℄ Single garage 0.3' E Conc floor		4.42	
4+42	Nend of Single garage 8.5' W			
4+53	S end same garage 0.5' W			
	Garage sets on angle with W.L Conc floor.		4.94	312.95
5+03	2 car garage 0.6' E Nend. earth floor.		5.1	
5+23	S. end Same garage 0.4' E		5.3	
5+28	Nend 2 car garage 0.5' E earth floor		5.4	
5+48	S end Same garage 0.6' E		5.5	

London May 8-28.
Isbel

46

X Sections Cooper St.
Continued Fr. Book 1235 P. 80

Sta	+	H.I.	−	El.
3+00		260.79		
℄			2.3	258.5
E'/a			2.2	258.6
E cb			2.2	258.6
E.L.			2.2	258.6
15' E			2.8	258.0
3+25				
15' E			5.7	255.1
9' E			4.5	256.3
E L			3.8	257.0
E cb			3.4	257.4
E'/a			3.2	257.6
℄			3.2	257.6
W'/a			3.7	257.1
+5			3.9	256.9
W cb			4.7	256.1
W.L			5.9	254.9
House 4' W.			5.40	255.39
3+50				
15' W			8.1	252.7
9' W			6.9	253.9
W.L			5.9	254.9
W cb			5.3	255.5
W'/a			4.8	256.0
℄			4.5	255.3

Garage Framed
5/28/28 T.G.H.

Sta	+	H.I	−	El.
3+50		260.79		
℄ +5			4.3	256.5
E'4			4.5	256.3
+5			4.5	256.3
Ecb			5.0	255.8
E.L.			6.0	254.8
15'E			7.8	253.0
3+75				
15'E			11.1	249.7
E.L			9.1	251.7
Ecb			8.1	252.7
E'4			7.1	253.7
+5			6.7	254.1
℄			6.5	254.3
w'4			6.3	254.5
wcb			6.3	254.5
w.L.			7.0	253.8
10'w			8.3	252.5
20'w			10.0	250.8
4+00				
house	6' w.		8.28	252.51
w.L			8.9	251.9
wcb			8.7	252.1
w'4			8.7	252.1
℄			9.2	251.6

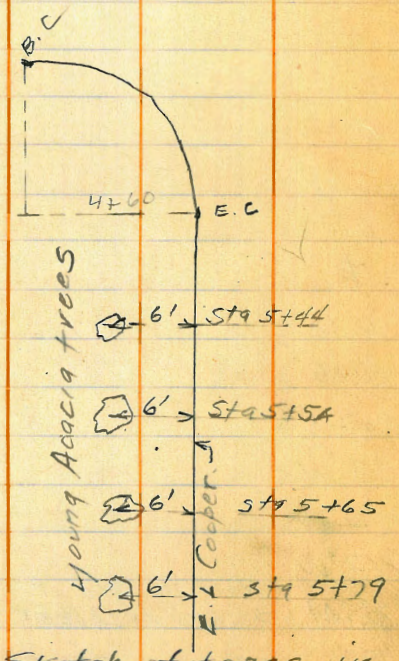
260.79

Sta	+	H.I	−	El.
4+00				
E'4			10.2	250.6
Ecb			11.2	249.6
E.L.			12.5	248.3
20'E			14.9	245.9
4+25				
20'E			18.8	242.0
E.L.			15.9	244.9
Ecb			14.8	246.0
E'4			13.8	247.0
℄			13.0	247.8
w'4			12.4	248.4
wcb			12.0	248.8
w.L.			12.0	248.8
13'w			12.5	248.3
20'w			13.5	247.3
T.P.	1.63	250.35	12.07	248.72
4+50				
25'w			6.6	243.8
w.L			5.4	245.0
wcb			5.4	245.0
w'4			5.6	244.8
℄			6.1	244.3
E'4			7.2	243.2
Ecb			8.5	241.9

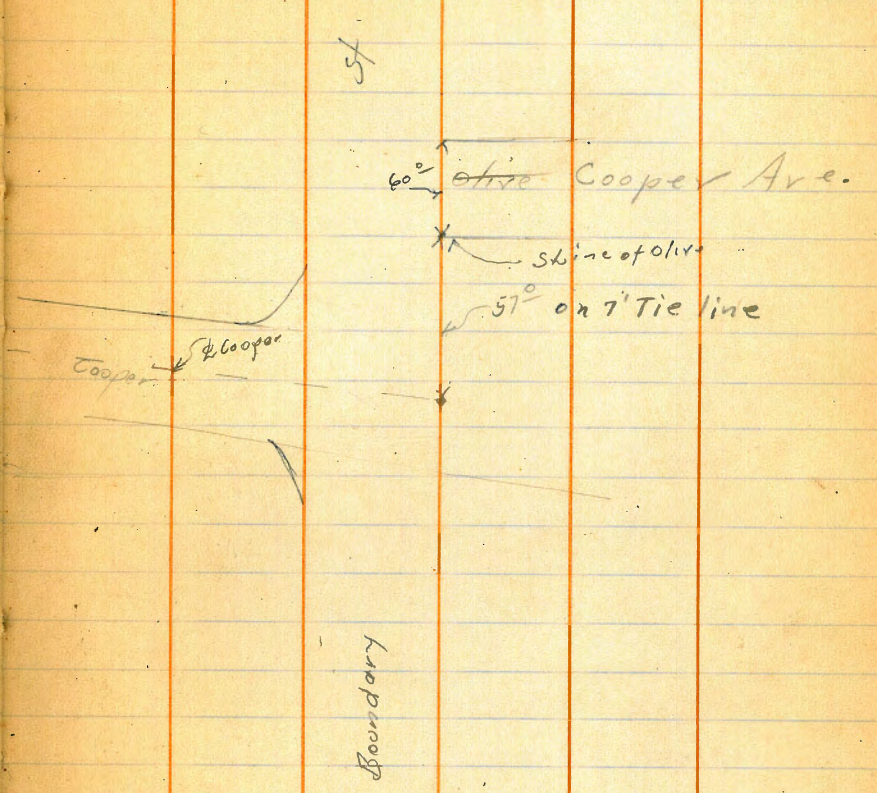
Sta	+	H.I	−	El.
4+50		250.35		
E.L.			10.2	240.2
13'E			12.4	238.0
25'E			14.5	235.9
4+75	↓			
30'E			21.1	229.3
15'E			18.0	232.4
E.L.			17.1	233.3
Ecb			13.4	237.0
E¼			11.8	238.6
℄			10.2	240.2
W¼			9.1	241.3
Wcb			8.6	241.8
W.L			8.6	241.8
15'W			9.2	241.2
30'W			10.2	240.2
4+96	= End of Cooper ↓			
30'W			13.5	236.9
13'W			11.5	238.9
W.L			10.0	240.4
Wcb			11.2	239.2
W¼			12.0	238.4
℄			12.8	237.6
E¼			13.8	236.6
Ecb			15.7	234.7

Sta	+	H.I	−	El.	
4+96		250.35			
E.L			17.9	232.5	
15'E			21.6	228.8	
35'E			25.5	224.9	
Section on N.L. Hartons Purchase					
40'E			35.8	214.6	
15'E			26.4	224.0	
E.L.			21.8	228.6	
Ecb			18.5	231.9	
E¼			16.0	234.4	
℄			14.4	236.0	
W¼			12.8	237.6	
Wcb			11.6	238.8	
W.L.			11.1	239.3	
13'W			10.8	239.6	
26'W			11.5	238.9	
40'W			12.6	237.8	
B.M.	Nail in Ble at S. end of Cooper		9.01	241.34	
T.P.	11.18	260.28	1.25	249.10	
T.P	12.48	272.07	0.61	259.67	
B.M	Nail in pole SW. Kalmia & Cooper		9.58	262.49	Nail in Pole SW
T.P.	11.00	282.47	0.60	271.47	
T.P	12.85	294.23	1.09	281.38	
B.M	Nail in post E.L. Boundary		2.46	291.77	
T.P	9.77	302.17	1.83	292.40	

sta	+	H.I	−	El.	
		302.17			
T.P	7.43	306.55	3.05	299.12	
T.P	4.00	304.21	6.34	300.21	
B.M	Beginning B.M		0.61	303.60	B.P.N.E Thorn 2 Nile. (303.69)



Sketch of trees in First Block of Cooper South, See Book 1235

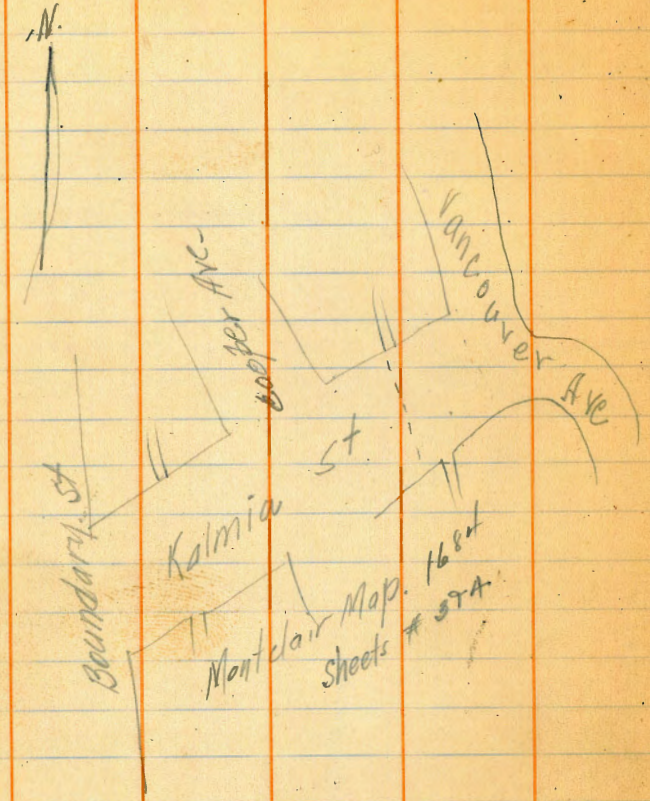

St.
60°
Olive
Cooper Ave.
Shine of olive
51° on T'Tie line
Cooper
℄ Cooper
Boundary

May 9-28

Cross-sections Kalmia From E.L. Loudon Esbell.
Cooper to W.L Vancouver.

Sta	+	H.I	−	El	
B.M.	12.44	274.93		262.49	Nail in Pole S.W Kalmia & Cooper
0+00 = E.L. Cooper					
S.L			4.4	270.5	
Scb			4.1	270.8	
S'4			4.0	270.9	
℄			3.8	271.1	
N'4			3.9	271.0	
Ncb			3.9	271.0	
N.L			3.7	271.2	
0+10					
N.L			2.8	272.1	
Ncb			3.1	271.8	
N'4			3.2	271.7	
℄			3.3	271.6	
S'4			3.3	271.6	
Scb			3.4	271.5	
S.L			3.5	271.4	
0+37					
S.L			2.7	272.2	
Scb			2.5	272.4	
S'4			2.3	272.6	
℄			2.0	272.9	
N'4			1.9	273.0	
+3			2.2	272.7	
+6			1.9	273.0	

Plotted S=N-28-East



Kalmia

27493

Sta	+	H.I	−	El.
0+37				
Ncb			1.9	273.0
N.L			1.5	273.4
0+50				
N.L.			1.4	273.5
Ncb			1.6	273.3
+6			1.9	273.0
N'/4			1.8	273.1
℄			1.8	273.1
S'/4			2.2	272.7
+2			2.4	272.5
Scb			2.3	272.6
S.L			2.4	272.5
10' S			2.8	272.1
0+75				
10' S			2.2	272.7
S.L			1.9	273.0
Scb			1.8	273.1
+7			2.1	272.8
S'/4			2.0	272.9
℄			1.6	273.3
N'/4			1.5	273.4
Ncb			1.3	273.6
N.L			1.0	273.9
10' N			0.9	274.0

Sta	+	H.I	−	El
1+00		274.93		
N.L			0.8	274.1
Ncb			0.9	274.0
N'/4			1.1	273.8
℄			1.2	273.7
+4			1.1	273.8
S'/4			1.4	273.5
Scb			1.6	273.3
S.L			2.0	272.9
10' S			2.2	272.7
1+25				
10' S			1.9	273.0
S.L.			1.4	273.5
Scb			1.0	273.9
S'/4			1.1	273.8
+6			0.7	274.2
℄			0.7	274.2
N'/4			0.7	274.2
Ncb			0.4	274.5
N.L			0.0	274.9
T.P.	387	278.15	0.65	274.28
1+50 = N.L Alley				
10'N			3.3	274.9
N.L			3.6	274.6
Ncb			3.8	274.4

Kalmia

278.15

Sta	+	H.I	−	El
1+50				
N'/4			3.9	274.3
℄			4.0	274.2
S'/4			4.5	273.7
Scb			4.5	273.7
S.L.			4.7	273.5
10'S			4.7	273.5
1+70 = E.L Alley.				
10'S			4.7	273.5
S.L			4.6	273.6
Scb			4.4	273.8
S'/4			4.4	273.8
+8			4.0	274.2
℄			4.1	274.1
N'/4			4.0	274.2
Ncb			3.8	274.4
N.L			3.6	274.6
10'N			3.5	274.7
2+00 = W.L. Alley				
10'N			3.4	274.8
N.L			3.5	274.7
+6			3.5	274.7
Ncb			3.9	274.3
+5			4.2	274.0
N'/4			4.2	274.0

Sta	+	H.I	−	El
2+00		278.15		
℄			4.3	273.9
+2			4.3	273.9
S'/4			4.5	273.7
Scb			4.6	273.6
S.L			4.5	273.7
10'S			4.6	273.6
2+20 = E.L Alley				
10'S			5.0	273.2
S.L			5.0	273.2
Scb			5.0	273.2
S'/4			5.1	273.1
℄			4.8	273.4
N'/4			4.6	273.6
+4			4.7	273.5
Ncb			4.2	274.0
N.L			4.3	273.9
10'N			4.2	274.0
2+50				
10'N			5.5	272.7
N.L			5.6	272.6
Ncb			5.7	272.5
+5			5.9	272.3
N'/4			5.8	272.4
℄			6.2	272.0

Kalmia

Sta	+	H.I	−	El
2+50		278.15		
S'/4			6.3	271.9
+3			6.6	271.6
Scb			6.3	271.9
S.L			6.5	271.7
10'S			6.5	271.7
2+80 = B.C. on S.L				
15'S			8.5	269.7
S.L			8.1	270.1
Scb			7.6	270.6
+4			7.5	270.7
S'/4			7.6	270.6
℄			7.2	271.0
+7			6.8	271.4
N'/4			6.9	271.3
+5			7.0	271.2
Ncb			6.6	271.6
N.L			6.1	272.1
10'N			5.9	272.3
3+00				
10'N			7.0	271.2
N.L			7.1	271.1
Ncb			7.1	271.1
N'/4			7.6	270.6
+3			7.4	270.8

Sta	+	H.I	−	El.
3+00		278.15		
℄			7.8	270.4
+9			8.0	270.2
S'/4			8.3	269.9
+6			8.1	270.1
Scb			8.3	269.9
S.L.			8.7	269.5
0.5'S. ℄ (on curve)			8.8	269.4
15'S			9.7	268.5
3+20.5 = W.L Vancouver				
15'S			10.2	268.0
2.5'S ℄ (on curve)			9.4	268.8
S.L			9.3	268.9
Scb			8.9	269.3
S'/4			8.9	269.3
℄			8.5	269.7
N'/4			8.4	269.8
Ncb			8.0	270.2
N.L			7.8	270.4
10'N			7.7	270.5
T.P	0.67	274.45	4.39	273.76
			11.95	262.50
T.P			1.20	273.25

7.47

May 9-28

Cross-sections Kalmia From E.L. Boundary to W.L. Cooper.

Sta.	+	H.I	−	El.
T.P.	7.49	280.74		273.25
0+00 = E.L Boundary.				
10' N			1.4	279.3
N.L			1.7	279.0
Ncb			2.2	278.5
N'4			2.6	278.1
℄			3.0	277.7
S'4			3.6	277.1
Scb			4.0	276.7
S.L.			4.5	276.2
7' S			5.0	275.7
0+25				
12' S			8.9	271.8
S.L			7.9	272.8
Scb			7.4	273.3
S'4			6.9	273.8
℄			6.6	274.1
N'4			5.9	274.8
Ncb			5.8	274.9
N.L			5.5	275.2
12' N			5.0	275.7
0+50				
16' N			8.9	271.8
N.L			9.0	271.7

Sta	+	H.I	−	El.
0+50		280.74		
Ncb			9.6	271.1
N'4			10.0	270.7
℄			10.4	270.3
S'4			11.1	269.6
Scb			12.0	268.7
S.L			11.9	268.8
14' S			12.0	268.7
0+75				
15' S			18.0	262.7
S.L			16.6	264.1
Scb			16.0	264.7
S'4			15.5	265.2
℄			14.7	266.0
N'4			14.6	266.1
Ncb			14.2	266.5
N.L			13.6	267.1
16' N			12.9	267.8
T.P	0.97	268.88	12.83	267.91
1+00				
18' N			6.4	262.5
N.L			7.7	261.2
Ncb			8.0	260.9
N'4			9.1	259.8
℄			9.5	259.4

Kalmia

Sta	+	H.I	−	El
1+00		268.88		
S'/4			10.2	258.7
Scb			10 5	258 4
S L			11.3	257.6
18'S			12.7	256.2
1+25				
25'S			19.4	249 5
S.L.			17.9	251.0
Scb			17.3	251.6
S'/4			17.2	251.7
℄			16.3	252 6
N'/4			15.7	253.2
Ncb			14.4	254.5
N.L			14.0	254.9
25'N			13.3	255.6
T.P.	1.85	257.72	13.01	255.87
1+40				
30'N			8.0	249.7
N.L.			6.2	251.5
Ncb			7.6	250.1
N'/4			8.6	249.1
℄			9 3	248 4
S'/4			9.8	247.9
Scb			10.4	247.3
S.L.			11.7	245.0

Sta	+	H.I.	−	El.
1+40		257.72		
30'S			15.4	242.3
T.P	0.29	244.95	13.06	244.66
1+52				
30'S			8.4	236 5
S.L			4.7	240 2
Scb			3.1	241 8
S'/4			3.3	241 6
℄			2.9	242.0
N'/4			1.7	243.2
Ncb			0.5	244.4
N.L			+1.3	246.2
30'N			1.7	243.2
1+60				
30'N			3.7	241 2
N.L			2.5	242 4
Ncb			4.0	240.9
N'/4			5.0	239.9
℄			5.8	239.1
S'/4			6.5	238.4
Scb			6.6	238.3
S.L			7.8	237.1
30'S			11.4	233.5
B.M.	4.51	244.27	5.19	239.76

Kalmia

Sta	+	H.I	−	El
1+74		244.27		
40' S			16.8	227.5
S.L.			14.3	230.0
S cb			13.2	231.1
S'/4			11.8	232.5
℄			10.1	234.2
N'/4			9.8	234.5
N cb			7.8	236.5
N.L			7.4	236.9
20'N			8.8	235.5
40'N			11.3	233.0
1+93				
50'N			15.9	228.4
20' N			14.5	229.8
N.L.			12.3	232.0
N cb			12.0	232.3
N'/4			13.2	231.1
℄			14.3	230.0
S'/4			16.7	227.6
S cb			18.8	225.5
S.L.			20.5	223.8
50'S			25.9	218.4
25' S			22.4	221.9

11.7

21.7 − 12 Co. = 9.1

Sta	+	H.I	−	El.
1+95		244.27		
50'S			23.4	220.9
25'S			22.8	221.5
S.L			22.8	221.5
S cb			22.3	222.0
S'/4			21.7	222.6
℄			20.8	223.5
N'/4			19.9	224.4
N cb			19.8	224.5
N.L			19.5	224.8
25'N			17.1	227.2
45'N			11.7	232.5
2+12				
45'N			4.0	240.3
25'N			7.4	236.9
N.L			10.5	233.8
N cb			12.0	232.3
N'/4			14.0	230.3
℄			15.4	228.9
S'/4			18.0	226.3
S cb			15.2	229.1
S.L			14.3	230.0
20'S			14.1	230.2
30'S			14.6	229.7

Kalmia

Sta	+	H.I	−	El
2+24		244.27		
30'S			10.6	233.7
15'S			9.7	234.6
S.L.			9.6	234.7
Scb			10.6	233.7
S'A			13.8	230.5
℄			10.6	233.7
N'4			8.7	235.6
Ncb			6.4	237.9
N.L			5.5	238.8
25'N			2.1	242.2
T.P	12.51	255.11	1.67	242.60
2+42				
25'N			5.0	250.1
N.L			8.0	247.1
Ncb			9.6	245.5
N'4			13.1	242.0
℄			18.2	236.9
+3			19.8	235.3
S'4			17.4	237.7
Scb			14.8	240.3
S.L			14.0	241.1
25'S			12.1	243.0

Sta	+	H.I	−	El
2+56		255.11		
20'S			7.2	247.9
S.L			7.4	247.7
Scb			9.2	245.9
S'4			10.7	244.4
℄			12.3	242.8
+5			14.0	241.1
N'4			12.4	242.7
Ncb			6.1	249.0
N.L			2.9	252.2
T.P	10.10	265.13	0.08	255.03
20'N			9.7	255.2
2+86				
15'N.			3.8	261.3
N.L			7.0	258.1
Ncb			12.1	253.0
N'4			10.2	254.9
℄			9.3	255.8
S'4			8.7	256.4
Scb			8.3	256.8
S.L			8.1	257.0
15'S			8.2	256.9
3+10 5 = W.L. Cooper				
S.L.			3.9	261.2
Scb			3.7	261.4

Kalmia

Sta	+	H.I	-	El.
3+10.5		265.13		
5¼			3.4	261.7
℄			3.2	261.9
N¼			3.0	262.1
N cb			2.6	262.5
+5			2.6	262.5
N.L.			1.8	263.3
B.M Nail Pole S.W. Cooper Kalmia			2.63	262.50

X sec. Maple From W.L Vancouver to Haller. Vancouver = Maple 60' wide 40' Roadway.

61

295.88 B.M. Brook

	>				
B.M	5.88	297.65		291.77	Nail in Post E.L. Boundary
	0.22	285.60	12.27	285.38	
	3.64	276.79	12.45	273.15	
W.L Vancouver					
S.L			4.3	272.5	
cb			4.5		
+5			4.7		
¼			4.5		
+8			4.4		
℄			4.5	272.3	
¼			4.9		
cb			5.1		
N.L.			5.4	271.4	
W.cb line Vancouver					
N.L			5.0	271.8	
cb			4.9		
+5			4.9		
¼			4.6		
℄			4.5	272.3	
+5			4.6		
¼			4.6		
cb			4.6		
+4			4.5		
S.L			4.6	272.2	

Plotted 1" = 20' T.G.H.

Maple

276.79

W'ly line Vancouver

S.L.	4.8	272.0	
cb	4.6		
¼	4.7		
+6	4.6		
℄	4.7	272.1	
+2	4.7		
¼	4.9		
+5	5.0		
cb	4.9		
N.L.	5.0	271.8	

℄ Vancouver

N.L.	4.9	2719	
cb	4.0		
+6	5 ℄		
¼	5.0		
+6	4.9		
℄	4.9	2719	
¼	4.9		
cb	4.9		
S.L.	4.9	271.9	

276.79

E'ly Line Vancouver

S.L.	5.3	271.5	
+5	5.2		
cb	5.2		
¼	5.3		
+9	5.2		
℄	5.2	271.6	
+1	5.3		
+5	5.2		
¼	5.3		
+5	5.3		
cb	5.2		
N.L.	5.1	271.7	

E cb line Vancouver

N.L.	5.2	271.6	
cb	5.2		
+4	5.5		
¼	5.4		
+3	5.4		
+7	5.6		
℄	5.5	271.3	
+2	5.6		
+4	5.4		
¼	5.5		
+5	5.8		
cb	5.6		
S.L.	5.7	271.1	

Maple

276.79

0+00 = E.L. Vancouver			
S.L.		6.2	270.6
c b		6.0	
+5		6.1	
¼		5.8	
+4		5.6	
℄		5.8	271.0
+7		5.7	
¼		5.7	
+5		5.9	
+8		5.6	
c b		5.5	
N.L.		5.4	271.4
0+25			
N.L.		5.6	271.2
+4		5.6	
c b		5.9	
+3		5.9	
+5		6.2	
¼		6.2	
+5		6.4	
℄		6.5	270.3
+8		6.4	
¼		6.5	
+5		6.9	
+7		6.8	

0+25			
S c b		6.8	
S.L.		7.1	269.7
0+50			
S.L.		8.2	268.6
c b		7.7	
+1		7.7	
+3		7.8	
¼		7.3	
+5		7.2	
℄		7.2	269.6
+3		7.3	
+6		7.1	
¼		7.0	
+6		6.9	
c b		6.6	
N.L.		6.4	270.4
0+64		℄	
N.L.		6.7	270.1
c b		7.0	
+2		7.1	
+3		7.3	
¼		7.3	
℄		7.5	269.3
+6		7.5	
¼		7.8	

Maple

	276.79		
+5		8.3	
cb		8.5	
+4		9.2	
+7		9.6	
+9		9.8	
S.L.		9.3	267.5
10's		9.8	
0+68			
10's		13.3	
S.L.		11.8	265.0
+3		11.2	
+5		9.9	
+7		8.9	
cb		8.7	
+5		8.4	
1/4		7.9	
+5		7.5	
℄		7.5	269.3
1/4		7.4	
+7		7.4	
+8		7.0	
cb		7.0	
N.L.		6.8	270.0

0+77		276.79			
N.L.			6.8	270.0	
cb			7.1		
+4			7.6		
1/4			7.4		
℄			7.6	269.2	
+6			7.6		
1/4			8.1		
+6			8.6		
cb			9.1		
+2			9.8		
+4			10.1		
+8			12.0		
S.L.			12.3	264.5	
3's			12.6		
6's			13.4		
10's			14.2		
B.M.	6.16	277.55	5.40	271.39	Hub NE Vancouver & Maple
0+84					
10's			15.0		
8'5			13.5		
3'5			11.7		
S.L.			10.0	267.6	
cb			9.2		
+4			9.0		
+7			9.0		

Maple

0+84	277.55		
S'ly		8.6	
+5		8.3	
℄		8.3	269.3
¼		8.1	
+5		8.2	
cb		8.0	
+1		7.7	
N.L.		7.5	270.1
1+00			
N.L.		6.9	270.7
cb		7.3	
+3		7.3	
+4		7.6	
¼		7.8	
℄		8.0	269.6
+8		8.1	
¼		8.3	
cb		8.8	
+8		9.1	
S.L.		9.3	268.3
5'S		9.6	
10'S		10.2	

1+25	277.55		
S.L.		8.1	269.5
+6		7.8	
cb		7.4	
+8		7.1	
¼		6.9	
+5		6.7	
℄ ¼		6.7	270.9
+6		6.5	
¼ ℄		6.2	
+7		6.0	
+8		5.8	
cb		5.6	
+5		5.4	
N.L.		5.3	272.3
1+50 = W.L. Alley			
N.L.		4.5	273.1
cb		4.9	
+2		5.3	
+8		5.5	
¼		5.5	
℄		5.7	271.9
+8		5.8	
¼		5.7	
+8		6.6	
cb		6.4	

Maple

1+50	277.55		
S.L.		7.1	270.5
1+70 = E.L	Alley		
S.L.		6.3	271.3
cb		5.9	
+3		6.0	
¼		5.2	
℄		5.3	272.3
+5		5.2	
¼		5.2	
+7		5.0	
+8		4.6	
cb		4.6	
N.L.		4.2	273.4
2+00			
N.L.		4.0	273.6
cb		4.1	
+2		4.1	
+3		4.4	
¼		4.4	
℄		4.6	273.0
+7		4.5	
¼		4.8	
+5		5.3	
cb		5.3	
+8		5.4	
S.L.		5.7	271.9

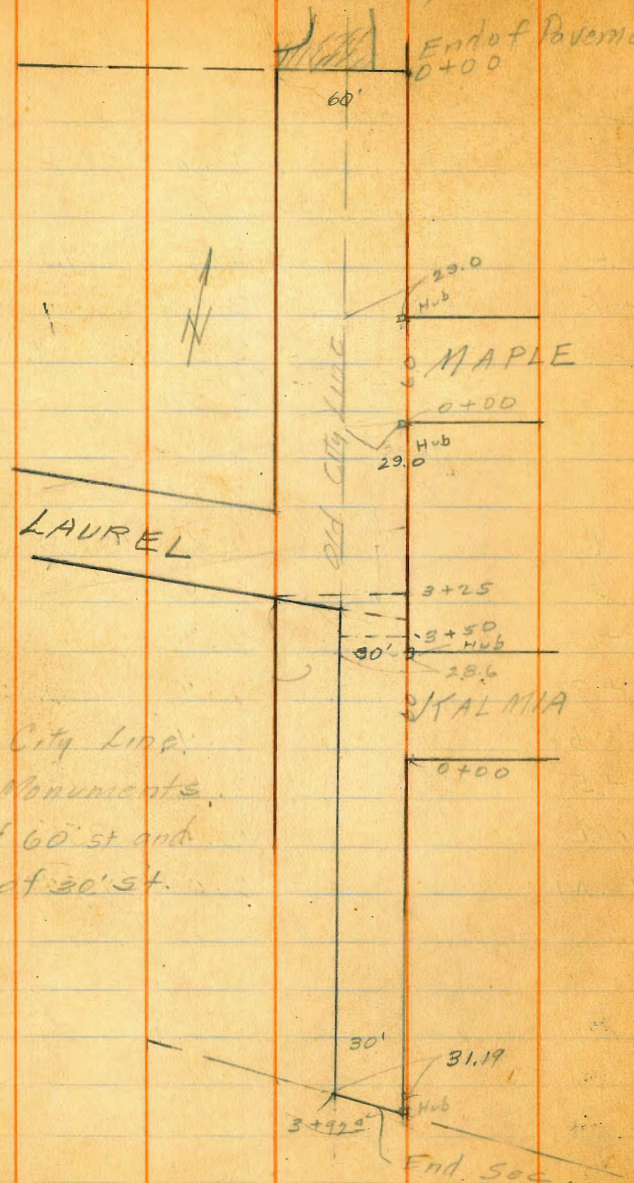
2+25	277.55		
S.L.		5.2	272.4
cb		4.8	
+5		4.8	
¼		4.4	
+3		4.2	
℄		4.3	273.3
¼		4.2	
+4		4.3	
+7		4.1	
+8		3.9	
cb		3.8	
N.L.		3.6	274.0
2+50			
N.L.		3.3	274.3
cb		3.5	
+2		3.5	
+4		3.8	
¼		3.8	
℄		3.8	273.8
+5		3.7	
+9		3.9	
¼		4.1	
+5		4.4	
+6		4.3	
cb		4.3	
S.L.		4.5	273.1

Maple

2+75	277.55		
S.L.	4.1	273.5	
+5	3.9		
cb	3.9		
+2	3.9		
+3	4.1		
¼	3.7		
+7	3.4		
℄	3.5	274.1	
+8	3.5		
¼	3.4		
+6	3.4		
cb	3.2		
+5	3.1		
N.L.	2.9	274.7	
3+00			
N.L.	2.5	275.1	
cb	2.6		
+2	2.8		
+4	3.1		
¼	3.2		
℄	3.2	274.4	
+3	3.1		
+8	3.3		
¼	3.6		
+6	3.8		
cb	3.7		

3+00	277.55			
S.L.		4.0	273.6	
3+25 = W.L. Haller.				
S.L.		3.3	274.3	
+5		3.1		
cb		3.3		
+3		3.5		
¼		3.1		
+6		2.6		
℄		2.6	275.0	
¼		2.7		
+6		2.7		
+8		2.4		
cb		2.4		
+5		2.2		
N.L.		2.1	275.5	
B.M.		2.08	275.47	Hub N.W. Maple & Haller

Cross-section Boundary St.



Note:
Used City Line as per Monuments for ℄ of 60' st and W. line of 30' st.

From End of Pavement to South Termination

6.0' wide
10' cb
10'-9+5
T.G.H.

Jun 7-28

Levels 292.12 / 35

B.M.	11.77	303.54		291.77	Nail in Post E.L. Boundary
0+00 = End Pavement					
W.L.	Pav		5.49	298.05	
cb	Pav		5.39	298.15	
¼	Pav		5.26	298.28	
℄	Pav		5.16	298.38	
¼	Pav		5.24	298.30	
gut.	Pav.		5.41	298.13	
top cb			4.67	298.87	
cb ground			5.0	298.54	
+3			4.6	298.9	
E.L.			4.3	299.2	
0+20					
E.L.			4.5	299.0	
+5			4.9	298.6	
cb			4.8	298.7	
+5			5.2	298.3	
+6			5.1	298.4	
¼			5.2	298.3	
+7			5.1	2984	
℄			5.5	298.0	
+6			5.2	2983	
¼			5.2	2983	
+5			5.3	298.2	
cb			5.4	298.1	
+3			5.2	2983	
W.L.			5.4	298.1	

Plotted 7-17-28 CBH
Grades figured 6-13-28 TGH

0+40		303.54		
w.L.			5.7	297.8
+8			5.3	298.2
cb			5.3	298.2
+5			5.3	298.2
¼			5.1	298.4
+6			4.7	298.8
℄			4.6	298.9
+7			4.5	299.0
¼			4.7	298.8
+8			4.6	298.9
cb			4.7	298.8
+5			4.4	299.1
E.L.			4.3	299.2
0+75				
E.L.			4.6	298.9
+8			4.5	299.0
cb			4.6	298.9
+7			4.9	298.6
¼			5.1	298.4
+6			4.9	298.6
℄			5.0	298.5
¼			5.3	298.2
+7			5.3	298.2
+9			5.2	298.3
cb			5.3	298.2
+2			5.7	297.8

0+75		303.54		
wcb +3			5.5	298.0
w.L.			5.8	297.7
1+00				
w.L.			5.8	297.7
cb			5.5	298.0
¼			5.5	298.0
℄			5.4	298.1
¼			5.2	298.3
cb			5.0	298.5
+4			4.7	298.8
E.L.			4.6	298.9
1+25				
E.L.			4.4	299.1
cb			4.7	298.8
+7			5.0	298.5
¼			4.9	298.6
+5			4.7	298.8
℄			4.8	298.7
+6			5.0	298.5
¼			5.1	298.4
cb			5.4	298.1
w.L.			5.6	297.9

1+50	303.54		
W.L.	5.6	297.9	
cb	5.2	298.3	
1/4	4.6	298.9	
℄	4.6	298.9	
1/4	4.6	298.9	
cb	4.5	299.0	
+8	4.1	299.4	
E.L.	4.1	299.4	
1+75			
E.C.	4.1	299.4	
+4	4.1	299.4	
+5	4.4	299.1	
cb	4.4	299.1	
+5	4.5	299.0	
1/4	4.5	299.0	
+5	4.6	298.9	
℄	4.6	298.9	
+6	4.7	298.8	
1/4	4.7	298.8	
+5	4.9	298.6	
cb	5.1	298.4	
+5	5.2	298.3	
W.L.	5.5	298.0	

2+00	303.54		
W.L.	5.5	298.0	
cb	5.2	298.3	
1/4	4.8	298.7	
+5	4.6	298.9	
℄	4.7	298.8	
1/4	4.5	299.0	
+8	4.4	299.1	
cb	4.5	299.0	
E.L.	4.3	299.2	
2+25			
E.C.	4.6	298.9	
+3	4.5	299.0	
cb	4.8	298.7	
+5	4.8	298.7	
1/4	4.6	298.9	
+6	4.7	298.8	
℄	4.8	298.7	
1/4	5.0	298.5	
+7	4.9	298.6	
W.C.	5.6	297.9	
2+50			
W.L.	5.5	298.0	
cb	5.2	298.3	
1/4	5.0	298.5	
℄	4.9	298.6	

2+50	303.54		
E ¼	4.9	298.6	
+5	5.0	298.5	
cb	5.1	298.4	
+6	4.6	298.9	
E.L.	4.7	298.8	
2+75			
E.L.	5.2	298.3	
+3	5.1	298.4	
cb	5.5	298.0	
+4	5.7	297.8	
+8	5.5	298.0	
¼	5.4	298.1	
℄	5.4	298.1	
¼	5.4	298.1	
cb	5.5	298.0	
+6	5.5	298.0	
w.L.	5.8	297.7	
3+00			
w.L.	5.9	297.6	
+5	5.6	297.9	
cb	5.7	297.8	
¼	5.5	298.0	
℄	5.7	297.8	
¼	5.8	297.7	
+5	6.1	297.4	
+7	5.5	297.6	

	303.54		
Ecb.	6.0	297.5	
+5	5.8	297.7	
+8	5.9	297.6	
E.L.	5.7	297.8	
3+25			
E.L.	6.0	297.5	
+6	6.1	297.4	
cb	6.4	297.1	
+5	6.4	297.1	
+9	6.3	297.2	
¼	6.0	297.5	
℄	5.8	297.7	
¼	5.6	297.9	
cb	5.8	297.7	
+8	5.9	297.6	
w.L.	6.1	297.4	
3+50			
w.L.	6.3	297.2	
+5	6.0	297.5	
cb	6.1	297.4	
¼	6.3	297.2	
℄	6.4	297.1	
¼	6.5	297.0	
+5	6.8	296.7	
cb	6.8	296.7	
+3	6.4	297.1	

3+50	303.54		
Ecb+5	6.2	297.3	
E.L.	6.3	297.2	
3+75			
E.L.	6.7	296.8	
+5	6.7	296.8	
cb	6.1	296.4	
¼	6.0	296.5	
+1	6.9	296.6	
+8	6.8	296.7	
℄	6.7	296.8	
¼	6.6	296.9	
cb	6.4	297.1	
+4	6.1	297.4	
w.L.	6.4	297.1	
4+00			
w.L.	6.6	296.9	
+5	6.4	297.1	
cb	6.4	297.1	
¼	6.8	296.7	
℄	7.0	296.5	
+8	7.2	296.3	
¼	7.4	296.1	
+8	7.5	296.0	
cb	7.3	296.2	
+3	7.0	296.5	
E.L.	7.0	296.5	

4+25.4 = N.L Maple	303.54		
E.L.	7.3	296.2	
cb	7.7	295.8	
+8	7.8	295.7	
¼	7.6	295.9	
+3	7.4	296.1	
℄	7.4	296.1	
+5	7.4	296.1	
¼	7.3	296.2	
cb	7.2	296.3	
+5	7.1	296.4	
w.L.	7.2	296.3	
N cb line Maple			
w.L.	7.4	296.1	
cb	7.2	296.3	
¼	7.5	296.0	
℄	7.4	296.1	
+7	7.3	296.2	
¼	7.6	295.9	
+3	7.9	295.6	
+5	7.8	295.7	
cb	7.7	295.8	
E.L.	7.6	295.9	

303.54

N ¼ line Maple

E.L.	7.7	295.8
cb	7.9	2956
+5	8.0	2955
¼	7.8	295.7
+5	7.5	296.0
℄	7.6	295.9
¼	7.7	2958
+5	7.7	2958
cb	7.5	2960
+4	7.2	2963
+5	7.4	2961
w.L.	7.4	296.1

℄ Maple

w.L.	7.6	295.9
+6	7.5	2960
cb	7.7	2958
¼	7.9	2956
℄	7.9	2956
¼	8.0	2955
+5	8.3	2952
cb	8.1	2954
E.L.	7.9	2956

303.54

S ¼ line Maple

E.L.	8.2	295.3
cb	8.3	2952
+4	8.4	295.1
+5	8.6	2949
+6	8.4	295.1
¼	8.3	2952
+1	8.2	2953
℄	8.1	2954
¼	7.9	2956
cb	7.8	2957
+5	7.7	2958
w.L.	7.8	295.7

S cb line Maple

w.L.	7.8	295.7
+5	7.8	295.7
cb	7.9	2956
¼	7.9	2956
℄	8.2	2953
¼	8.4	2951
+5	8.7	2948
cb	8.4	2951
+5	8.3	2952
E.L.	8.3	295.2

303.54

0+00 = S.L. Maple

E.L.		8.4	295.1
+7		8.5	295.0
cb		8.7	294.8
+6		8.8	294.7
1/4		8.7	294.8
+3		8.4	295.1
℄		8.2	295.3
1/4		8.1	295.4
+4		7.9	295.6
cb		7.8	295.7
w.l.		7.7	295.8
0+25			
w.l.		7.8	295.7
+5		7.7	295.8
cb		8.1	295.4
1/4		8.4	295.1
℄		8.7	294.8
+9		8.8	294.7
1/4		9.0	294.5
+2		9.2	294.3
+5		9.1	294.4
cb		9.0	294.5
E.L.		8.7	294.8

303.54

0+50

E.L.		9.0	294.5
cb		9.2	294.3
+3		9.5	294.0
+5		9.3	294.2
+8		9.4	294.1
1/4		9.3	294.2
+2		9.0	294.5
℄		9.0	294.5
1/4		8.8	294.7
cb		8.5	295.0
+5		8.4	295.1
w.l.		8.4	295.1
0+75			
w.l.		8.9	294.6
cb		9.1	294.4
1/4		9.2	294.3
℄		9.2	294.3
+9		9.4	294.1
1/4		9.6	293.9
+2		9.8	293.7
+5		9.7	293.8
+8		9.8	293.7
cb		9.7	293.8
+6		9.4	294.1
E.L.		9.4	294.1

1+00		303.54		
E.L.			9.8	293.7
+4			9.7	93.8
+5			9.9	93.6
cb			10.0	93.5
+2			10.2	93.3
+9			10.0	93.5
¼			9.7	93.8
℄			9.3	294.2
¼			9.3	94.2
cb			9.4	94.1
w.L.			9.3	294.2
1+25				
w.L.			9.7	293.8
cb			9.8	93.7
¼			10.0	93.5
℄			10.1	93.4
¼			10.2	293.3
+8			10.5	93.0
cb			10.5	93.0
+4			10.2	93.3
+9			10.0	93.5
E.L.			10.1	2934

1+50		303.54		
EL			10.7	292.8
+2			10.6	92.9
+8			10.6	92.9
cb			11.0	92.5
+3			10.7	92.8
+8			10.7	92.8
+9			10.5	93.0
¼			10.5	93.0
℄			10.2	2933
¼			9.8	93.7
cb			9.7	93.8
+5			9.7	93.8
w.L.			10.1	293.4
T.P.	1.98	295.35	10.17	293.37
1+75				
w.L.		295.4	2.3	2931
cb			1.9	93.5
¼			1.9	93.5
℄			2.4	2930
¼			2.6	92.8
+2			2.7	92.7
+5			3.1	92.3
+8			2.9	92.5
cb ¼			3.1	92.3
+5			2.9	92.5
E.L.			2.9	292.5

	295.35		
2+00			
E.L.	3.2	292.2	
cb	3.4	92.0	
+8	3.4	92.0	
+9	3.1	92.3	
1/4	3.1	92.3	
℄	3.0	292.4	
1/4	2.9	92.5	
cb	2.8	92.6	
+4	2.6	92.8	
w.l.	2.8	292.6	
2+25			
w.l.	2.6	292.8	
cb	3.0	92.4	
1/4	3.2	92.2	
℄	3.4	292.0	
1/4	3.6	91.8	
cb	3.9	91.5	
+5	3.8	91.6	
E.L.	3.7	291.7	
2+50			
E.L	4.0	291.4	
+5	4.2	91.2	
cb	4.2	91.2	
+4	4.3	91.1	
+6	4.5	90.9	

2+50	295.35		
E 1/4	4.1	291.3	
℄	3.7	291.7	
1/4	3.7	91.7	
cb	3.6	91.8	
+5	3.5	91.9	
w.l.	3.5	291.9	
2+75			
w.l.	3.9	291.5	
cb	4.2	91.2	
1/4	4.3	91.1	
+9	4.4	91.0	
℄	4.6	290.8	
+8	4.6	90.8	
1/4	4.9	90.5	
+3	4.6	90.8	
cb	4.5	90.9	
+6	4.5	90.9	
E.L	4.5	290.9	
3+00			
E.L.	5.2	290.2	
cb	5.1	90.3	
1/4	5.0	90.4	
℄	4.9	290.5	
1/4	4.9	90.5	
+7	5.4	90.0	
cb	5.4	90.0	

	295.35		
3+00			
W.C.b+5		5.5	R89.7
W.L.		5.3	290.1
3+25 = S.L. Laurel.			
W.L.		5.3	290.1
C.b		5.4	90.0
1/4		5.7	89.7
℄		5.5	289.9
1/4		5.6	89.8
C.b		5.8	89.6
E.L.		6.0	289.4
Sec. on S.L. Laurel. 60' Section,			
E.L.		6.4	289.0
C.b		6.2	89.2
1/4		5.9	89.5
℄		5.7	289.7
1/4		5.6	89.8
+3		5.5	89.9
C.b		5.4	90.0
+5		5.1	90.3
W.L.		5.2	290.2
Boundary 30' St. Sec's. 30'-20' Roadway 5' c.b.s. From Sta. 3+50 to end			
3+50 30' Sec.			
W.L.		6.2	289.2
C.b		6.3	89.1
1/4		6.5	88.9

3+50	295.35		
℄		6.4	289.0
1/4		6.6	88.8
C.b		6.8	88.6
E.L.		6.9	288.5
3+75			
E.L.		7.7	287.5
C.b		7.7	87.7
1/4		7.6	87.8
℄		7.5	287.9
1/4		7.5	87.9
+3		7.3	88.1
C.b		7.3	88.1
W.L.		7.1	288.3
4+00			
W.L.		8.1	287.3
C.b		8.3	87.1
+3		8.3	87.1
1/4		8.5	86.9
℄		8.5	286.9
1/4		8.8	86.6
C.b		9.0	86.4
E.L.		9.1	286.3
10' E		9.6	85.8

Continued in Book 1262 P.1

Grade Stakes Alley Valle Vista Terrace.

sta	+	H.I	-	El	Grade	
BM.	4.92	355.99		351.07		
	6.76	360.52	2.23	353.76		
0+00N			6.53	353.99	354.0	
0+00S			6.66	353.86	353.7	
0+20N			5.22	355.30	354.7	C 0.60
0+20S			5.76	354.76	354.4	C 0.36
0+40N			5.15	355.37	355.1	C 0.27
0+40S			5.51	355.01	354.7	C 0.31
0+60N			5.10	355.42	355.2	C 0.22
0+60S			5.49	355.03	354.8	C 0.23
0+80N			4.89	355.63	355.0	C 0.63
0+80S			5.81	354.71	354.6	C 0.11
1+20N			5.55	354.97	354.2	C 0.77
1+20S		356.52	2.99	353.53	354.0	C 3.53
1+60N			2.80	353.72	353.4	C 0.32
1+60S			2.88	353.64	353.4	C 0.24
2+00N			3.85	352.67	352.5	C 0.17
2+00S			4.71	351.81	352.30	F 0.49
2+40N			5.12	351.40	351.2	C 0.20
2+40S			6.79	349.73	351.0	F 1.27
2+80N			7.21	349.31	349.46	F 0.15
2+80S			8.26	348.26	349.41	F 1.15
3+20N			8.67	347.85	347.72	C 0.13
3+20S			9.32	347.20	347.82	F 0.62

360.52
7.15
353.37
3.15
356.52

2.70
5.13
2.43
2.36
4.79

4.18
.39
3.85

2.88

78

3.19
.39
2.80

3+55.49 N	356.52			346.18		
3+55 49 S		10.20	346.32	346.41	F 0.09	
3+73 26 S		10.91	345.61	345.67	F 0.06	
S		11.06	345.46			
N		10.35	346.17			
℄		10.90	345.62			

346.17
345.46
21.71
35

345.81
3
346.51

Voltaire & Villa Dr
E.P. N.E 96-26
Tennyson & Harrington
S.P N.E 85-68

1914

87

IMPROVED TABLES
AND
INFORMATION

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1½ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

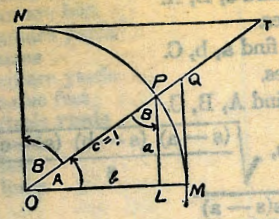


TABLE II

TRIGONOMETRIC FORMULÆ.

$\angle A = \angle MOP \qquad \angle B = \angle PON = \angle OPL$

$R = OB = c = 1$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

$$\sin \tfrac{1}{2} A = \sqrt{\frac{1 - \text{Cos } A}{2}} \qquad \cos \tfrac{1}{2} A = \sqrt{\frac{1 + \text{Cos } A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \qquad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Lines} \quad \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C^1}{C}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \tfrac{1}{2}(A+B)}{\tan \tfrac{1}{2}(A-B)}$$

TABLE VI (continued)

SINES, COSINES, TANGENTS, COTANGENTS (continued)

deg.	sin 0′	tan 0′	sin 10′	tan 10′	sin 20′	tan 20′	sin 30′	tan 30′	sin 40′	tan 40′	sin 50′	tan 50′	deg.
46	7193	1.0355	7214	1.0416	7234	1.0477	7254	1.0533	7274	1.0599	7294	1.0661	43
47	314	.0724	333	.0786	353	.0850	373	.0913	392	.0977	412	.1041	42
48	431	.1106	451	.1171	470	.1237	490	.1303	509	.1369	528	.1436	41
49	547	.1504	566	.1571	585	.1640	604	.1708	623	.1778	642	.1847	40
50	660	1.1918	7679	1.1988	7698	1.2059	7716	1.2131	7735	1.2203	7753	1.2276	39
51	771	2349	790	.2423	808	.2497	826	.2572	844	.2647	862	.2723	38
52	880	.2799	898	.2876	916	.2954	934	.3032	951	.3111	969	.3190	37
53	986	.3270	8004	.3351	8021	.3452	8039	.3514	8056	.3597	8073	.3680	36
54	8090	.3764	107	.3848	124	.3934	141	.4019	158	.4106	175	.4193	35
55	192	4281	208	.4370	225	.4460	241	.4550	258	.4641	274	.4733	34
56	290	.4826	307	.4919	323	.5013	339	.5108	355	.5204	371	.5301	33
57	387	.5399	403	.5497	418	.5597	434	.5697	450	.5798	465	.5900	32
58	480	.6003	496	.6107	511	.6212	526	.6319	542	.6426	557	.6534	31
59	572	.6643	587	.6753	601	.6864	615	.6977	631	.7090	646	.7205	30
60	660	1.7321	8675	1.7437	8689	1.7556	8704	1.7675	8718	1.7797	8732	1.7917	29
61	746	.8040	760	.8165	774	.8291	788	.8418	802	.8546	816	.8676	28
62	829	.8807	843	.8940	857	.9074	870	.9210	884	.9347	897	.9486	27
63	910	.9626	923	.9768	936	.9912	949	2.0057	962	2.0204	975	2.0353	26
64	988	2.0503	9001	2.0655	9013	2.0809	9026	.0965	9038	.1123	9051	.1283	25
65	9063	.1445	075	.1609	088	.1775	100	.1943	112	.2113	124	.2286	24
66	135	.2460	147	.2637	159	.2817	171	.2998	182	.3183	194	.3369	23
67	205	.3559	216	.3750	228	.3945	239	.4142	250	.4342	261	.4545	22
68	272	.4751	283	.4960	293	.5172	304	.5386	315	.5605	325	.5826	21
69	336	.6051	346	.6279	356	.6511	367	.6746	377	.6985	387	.7228	20
70	397	2.7475	9407	2.7725	9417	2.7980	9426	2.8239	9436	2.8502	9446	2.8770	19
71	455	.9042	465	.9319	474	.9600	483	.9887	492	3.0178	502	3.0475	18
72	511	3.0777	520	3.1084	528	3.1397	537	3.1716	546	.2041	555	.2371	17
73	563	.2709	572	.3052	580	.3402	588	.3759	596	.4124	605	.4495	16
74	613	.4874	621	.5261	628	.5656	636	.6059	644	.6470	652	.6891	15
75	659	.7321	667	.7760	674	.8208	681	.8657	689	.9136	696	.9617	14
76	703	4.0108	710	4.0611	717	4.1126	724	4.1653	730	4.2193	737	4.2747	13
77	744	.3315	750	.3897	757	.4494	763	.5107	769	.5736	775	.6382	12
78	781	.7046	787	.7729	793	.8430	799	.9152	805	.9894	811	5.0658	11
79	816	.1446	822	5.2257	827	5.3093	833	5.3955	838	5.4845	843	.5764	10
80	9848	5.6713	9853	5.7694	9858	5.8708	9863	5.9758	9868	6.0844	9872	6.1970	9
81	877	6.3138	881	6.4348	886	6.5606	890	6.6912	894	.8269	899	.9682	8
82	903	7.1154	907	7.2687	911	7.4287	914	7.5958	918	7.7704	922	7.9530	7
83	925	8.1443	929	8.3450	932	8.5555	936	8.7769	939	9.0098	942	9.2553	6
84	945	9.5144	948	9.7882	951	10.078	954	10.385	957	10.711	959	11.059	5
85	962	11.430	964	11.826	967	12.250	969	12.706	971	13.197	974	13.727	4
86	976	14.300	978	14.924	980	15.605	981	16.350	983	17.169	985	18.075	3
87	986	19.081	988	20.206	989	21.470	990	22.903	992	24.542	993	26.432	2
88	994	28.636	9995	31.242	9996	34.368	997	38.189	997	42.964	9998	49.104	1
89	9998	57.290	9999	68.750	9999	85.940	9999	114.58	1.000	171.88	1.000	343.77	0
deg.	60′ cos	60′ cot	50′ cos	50′ cot	40′ cos	40′ cot	30′ cos	30′ cot	20′ cos	30′ cot	10′ cos	10′ cot	deg.

TABLE VII

RODS IN FEET AND INCHES

Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches
1	16—6	21	346—6	41	676—6	61	1006—6	81	1336—6
2	33—0	22	363—0	42	693—0	62	1023—0	82	1353—0
3	49—6	23	379—6	43	709—6	63	1039—6	83	1369—6
4	66—0	24	396—0	44	726—0	64	1056—0	84	1386—0
5	82—6	25	412—6	45	742—6	65	1072—6	85	1402—6
6	99—0	26	429—0	46	759—0	66	1089—0	86	1419—0
7	115—6	27	445—6	47	775—6	67	1105—6	87	1435—6
8	132—0	28	462—0	48	792—0	68	1122—0	88	1452—0
9	148—6	29	478—6	49	808—6	69	1138—6	89	1468—6
10	165—0	30	495—0	50	825—0	70	1155—0	90	1485—0
11	181—6	31	511—6	51	841—6	71	1171—6	91	1501—6
12	198—0	32	528—0	52	858—0	72	1188—0	92	1518—0
13	214—6	33	544—6	53	874—6	73	1204—6	93	1534—6
14	231—0	34	561—0	54	891—0	74	1221—0	94	1551—0
15	247—6	35	577—6	55	907—6	75	1237—6	95	1567—6
16	264—0	36	594—0	56	924—0	76	1254—0	96	1584—0
17	280—6	37	610—6	57	940—6	77	1270—6	97	1600—6
18	297—0	38	627—0	58	957—0	78	1287—0	98	1617—0
19	313—6	39	643—6	59	973—6	79	1303—6	99	1633—6
20	330—0	40	660—0	60	990—0	80	1320—0	100	1650—0

TABLE VIII

LINKS IN FEET AND INCHES

Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches
1	0- 7.92	18	11-10.56	35	23- 1.20	52	34- 3.84	69	45- 6.48	86	56- 9.12
2	1- 3.84	19	12- 6.48	36	23- 9.12	53	34-11.76	70	46- 2.40	87	57- 5.04
3	1-11.76	20	13- 2.40	37	24- 5.04	54	35- 7.68	71	46-10.32	88	58- 0.96
4	2- 7.68	21	13-10.32	38	25- 0.96	55	36- 3.60	72	47- 6.24	89	58- 8.88
5	3- 3.60	22	14- 6.24	39	25- 8.88	56	36-11.52	73	48- 2.16	90	59- 4.80
6	3-11.52	23	15- 2.16	40	26- 4.80	57	37- 7.44	74	48-10.08	91	60- 0.72
7	4- 7.44	24	15-10.08	41	27- 0.72	58	38- 3.36	75	49- 6.00	92	60- 8.64
8	5- 3.36	25	16- 6.00	42	27- 8.64	59	38-11.28	76	50- 1.92	93	61- 4.56
9	5-11.28	26	17- 1.92	43	28- 4.56	60	39- 7.20	77	50- 9.84	94	62- 0.48
10	6- 7.20	27	17- 9.84	44	29- 0.48	61	40- 3.12	78	51- 5.76	95	62- 8.40
11	7- 3.12	28	18- 5.76	45	29- 8.40	62	40-11.04	79	52- 1.68	96	63- 4.32
12	7-11.04	29	19- 1.68	46	30- 4.32	63	41- 6.96	80	52- 9.60	97	64- 0.24
13	8- 6.96	30	19- 9.60	47	31- 0.24	64	42- 2.88	81	53- 5.52	98	64- 8.16
14	9- 2.88	31	20- 5.52	48	31- 8.16	65	42-10.80	82	54- 1.44	99	65- 4.08
15	9-10.80	32	21- 1.44	49	32- 4.08	66	43- 6.72	83	54- 9.36	100	66- .000
16	10- 6.72	33	21- 9.36	50	33- 0.00	67	44- 2.64	84	55- 5.28	101	66 -7.92
17	11- 2.64	34	22- 5.28	51	33- 7.92	68	44-10.56	85	56- 1.20	102	67- 3.84

Table X.

MIDDLE ORDINATES OF RAILS

Length of Rail (feet)

C ° ′	R Feet	30 Inch	28 Inch	26 Inch	24 Inch	22 Inch	20 Inch	C °	R Feet	30 Inch	28 Inch	26 Inch	24 Inch	22 Inch	20 Inch
0–20	17189	.08	.07	.06	.05	.04	.03	8	716.8	1.88	1.64	1.42	1.20	1.01	.84
0–40	8594	.16	.14	.12	.10	.08	.07	9	637.3	2.12	1.84	1.60	1.35	1.14	.94
1–0	5730	.24	20	.18	.15	.13	.10	10	573.7	2.36	2.05	1.78	1.50	1.27	1.04
1–20	4297	.31	.27	.23	.20	.17	.13	11	521.7	2.59	2.26	1.95	1.65	1.39	1.15
1–40	3438	.39	.34	.29	.25	.21	.17	12	478.3	3.83	2.47	2.15	1.81	1.54	1.26
2–0	2865	.47	.41	.35	.30	.25	.20	13	441.7	3.05	2.66	2.30	1.96	1.66	1.36
2–20	2456	.55	.48	.41	.35	.29	.23	14	410.3	3.30	2.87	2.48	2.10	1.78	1.46
2–40	2149	.63	.55	.47	.40	.33	.27	15	383.1	3.54	3.08	2.68	2.26	1.91	1.57
3–0	1910	.71	.62	.53	.45	.38	.31	16	359.3	3.76	3.28	2.83	2.40	2.04	1.67
3–20	1719	.78	.68	.59	.50	.42	35	17	338.3	4.00	3.48	3.02	2.57	2.16	1.78
3–40	1563	.86	.75	.65	.55	.46	38	18	319.6	4.21	3.67	3.18	2.70	2.28	1.87
4–0	1433	94	.82	.71	.60	.50	.42	19	302.9	4.45	3.89	3.36	2.86	2.41	1.98
4–20	1323	1.02	.89	.77	.65	.55	.45	20	287.9	4.70	4.09	3.55	3.00	2.54	2.09
4–40	1228	1.10	.96	.83	.70	.59	.48	22	262.0	5.16	4.44	3.84	3.30	2.80	2.29
5	1146	1.18	1.03	.89	.75	.63	.52	24	240.5	5.64	4.92	4.20	3.59	3.04	2.50
6	955.3	1.41	1.23	1.06	.90	.76	.62	26	222.3	6.07	5.29	4.58	3.88	3.29	2.70
7	819.0	1.65	1.44	1.24	1.05	.89	.73								

Table XI.

SHORT RADIUS CURVES

Radius Feet	Chord Feet	Central Angle	Deflection Angle	Deflection for 1 Foot
35	10	16-26	8-13	49.3
45	10	12-46	6-23	38.3
50	15	17-16	8-38	34.5
60	15	14-22	7-11	28.8
75	15	11-30	5-45	23.0
100	20	11-30	5-45	17.3
120	20	9-34	4-47	14.3
150	20	7-39	3-49	11.5
190	25	7-32	3-46	9.15
200	25	7-10	3-35	8.6
225	25	6-25	3-12	7.7
240	25	5-58	2-59	7.2
250	25	5-44	2-52	6.9
275	25	5-12	2-36	6.2
288	50	9-58	4-59	6.0
300	50	9-32	4-46	5.7
350	50	8-12	4-06	4.9
376	50	7-40	3-50	4.6
400	50	7-10	3-35	4.3
410	50	7-00	3-30	4.2

To find length of curve divide angle from P. C. to P. T. by central angle of chord and multiply by length of chord.

415.26
110.7
304.6

Table XII.

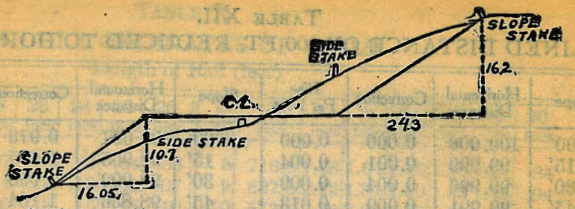
INCLINED DISTANCE OF 100 FT. REDUCED TO HORIZONTAL

Slope	Horizontal Distance	Correction	Rise Per Foot	Slope	Horizontal Distance	Correction	Rise Per Foot
0°00′	100.000	0.000	0.000	8°00′	99.027	0.973	0.139
15′	99.999	0.001	0.004	15′	98.965	1.035	0.143
30′	99.996	0.004	0.009	30′	98.902	1.098	0.148
45′	99.991	0.009	0.013	45′	98.836	1.164	0.152
1 00	99.985	0.015	0.017	9 00	98.769	1.231	0.156
15	99.976	0.024	0.022	15	98.700	1.300	0.161
30	99.966	0.034	0.026	30	98.629	1.371	0.165
45	99.953	0.047	0.031	45	98.556	1.444	0.169
2 00	99.939	0.061	0.035	10 00	98.481	1.519	0.174
15	99.923	0.077	0.039	15	98.404	1.596	0.178
30	99.905	0.095	0.044	30	98.325	1.675	0.182
45	99.885	0.115	0.048	45	98.245	1.755	0.187
3 00	99.863	0.137	0.052	11 00	98.163	1.837	0.191
15	99.839	0.161	0.057	15	98.079	1.921	0.195
30	99.813	0.187	0.061	30	97.992	2.008	0.199
45	99.786	0.214	0.065	45	97.905	2.095	0.204
4 00	99.756	0.244	0.070	12 00	97.815	2.185	0.208
15	99.725	0.275	0.074	15	97.723	2.277	0.212
30	99.692	0.308	0.078	30	97.630	2.370	0.216
45	99.657	0.343	0.083	45	97.534	2.466	0.221
5 00	99.619	0.381	0.087	13 00	97.437	2.563	0.225
15	99.580	0.420	0.092	15	97.338	2.662	0.229
30	99.540	0.460	0.096	30	97.237	2.763	0.233
45	99.497	0.503	0.100	45	97.134	2.866	0.238
6 00	99.452	0.548	0.105	14 00	97.030	2.970	0.242
15	99.406	0.594	0.109	15	96.923	3.077	0.246
30	99.357	0.643	0.113	30	96.815	3.185	0.250
45	99.307	0.693	0.118	45	96.705	3.295	0.255
7 00	99.255	0.745	0.122	15 00	96.593	3.407	0.259
15	99.200	0.800	0.126	15	96.479	3.521	0.263
30	99.144	0.856	0.131	30	96.363	3.637	0.267
45	99.087	0.913	0.135	45	96.246	3.754	0.271

Table XIII.

MINUTES IN DECIMALS OF A DEGREE.

0 30″	.00833	10′ 30″	.17500	20′ 30″	.34167	30′ 10″	.50833	40′ 30″	.67500	50′ 10″	.84167
1 00	.01667	11 00	.18333	21 00	.35000	31 00	.51667	41 00	.68333	51 00	.85000
30	.02500	30	.19167	30	.35833	30	.52500	30	.69167	30	.85833
2 00	.03333	12 00	.20000	22 00	.36667	32 00	.53333	42 00	.70000	52 00	.86667
30	.04167	30	.20833	30	.37500	30	.54167	30	.70833	30	.87500
3 00	.05000	13 00	.21667	23 00	.38333	33 00	.55000	43 00	.71667	53 00	.88333
30	.05833	30	.22500	30	.39167	30	.55833	30	.72500	30	.89167
4 00	.06667	14 00	.23333	24 00	.40000	34 00	.56667	44 00	.73333	54 00	.90000
30	.07500	30	.24167	30	.40833	30	.57500	30	.74167	30	.90833
5 00	.08333	15 00	.25000	25 00	.41667	35 00	.58333	45 00	.75000	55 00	.91667
30	.09167	30	.25833	30	.42500	30	.59167	30	.75833	30	.92500
6 00	.10000	16 00	.26667	26 00	.43333	36 00	.60000	46 00	.76667	56 00	.93333
30	.10833	30	.27500	30	.44167	30	.60833	30	.77500	30	.94167
7 00	.11667	17 00	.28333	27 00	.45000	37 00	.61667	47 00	.78333	57 00	.95000
30	.12500	30	.29167	30	.45833	30	.62500	30	.79167	30	.95833
8 00	.13333	18 00	.30000	28 00	.46667	38 00	.63333	48 00	.80000	58 00	.96667
30	.14167	30	.30833	30	.47500	30	.64167	30	.80833	30	.97500
9 00	.15000	19 00	.31667	29 00	.48333	39 00	.65000	49 00	.81667	59 00	.98333
30	.15833	30	.32500	30	.49167	30	.65833	30	.82500	30	.99167
10 00	.16667	20 00	.33333	30 00	.50000	40 00	.66667	50 00	.83333	60 00	1.00000



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1 65	1 80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3 45	3.60	3 75	3.90	4.05	4.20	4 35	2
3	4.50	4 65	4.80	4.95	5 10	5 25	5 40	5.55	5.70	5.85	3
4	6.00	6 15	6.30	6.45	6.60	6 75	6.90	7.05	7.20	7.35	4
5	7 50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9 00	9 15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10 65	10.80	10.95	11.10	11.25	11.40	11.55	11 70	11.85	7
8	12.00	12 15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13 50	13 65	13 80	13 95	14.10	14.25	14.40	14 55	14.70	14.85	9
10	15.00	15 15	15 30	15 45	15.60	15.75	15.90	16.05	16.20	16 35	10
11	16 50	16 65	16 80	16.95	17 10	17.25	17.40	17.55	17.70	17.85	11
12	18 00	18 15	18.30	18 45	18.60	18 75	18.90	19.05	19.20	19 35	12
13	19 50	19 65	19.80	19.95	20.10	20.25	20 40	20.55	20.70	20.85	13
14	21.00	21 15	21.30	21.45	21 60	21.75	21.90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24 15	24 30	24 45	24.60	24.75	24 90	25 05	25.20	25.35	16
17	25.50	25 65	25.80	25 95	26.10	26 25	26 40	26.55	26.70	26.85	17
18	27.00	27 15	27.30	27 45	27.60	27.75	27.90	28.05	28 20	28.35	18
19	28 50	28 65	28 80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30 00	30 15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31 50	31 65	31.80	31.95	32 10	32 25	32.40	32.55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33.60	33 75	33.90	34.05	34.20	34.35	22
23	34 50	34 65	34.80	34.95	35.10	35 25	35 40	35.55	35.70	35 85	23
24	36.00	36 15	36.30	36 45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37 80	37.95	38.10	38.25	38.40	38 55	38.70	38.85	25
26	39 00	39 15	39.30	39 45	39 60	39.75	39.90	40.05	40.20	40.35	26
27	40 50	40 65	40 80	40.95	41.10	41.25	41 40	41.55	41.70	41.85	27
28	42 00	42 15	42.30	42.45	42.60	42 75	42.90	43.05	43.20	43.35	28
29	43 50	43 65	43.80	43 95	44.10	44 25	44 40	44.55	44.70	44 85	29
30	45 00	45 15	45.30	45 45	45.60	45.75	45 90	46.05	46 20	46.35	30
31	46.50	46.65	46.80	46 95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48 00	48.15	48.30	48 45	48.60	48 75	48.90	49.05	49 20	49.35	32
33	49.50	49 65	49.80	49.95	50.10	50.25	50.40	50.55	50 70	50.85	33
34	51 00	51.15	51.30	51.45	51.60	51 75	51.90	52.05	52.20	52.35	34
35	52 50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54 00	54 15	54.30	54 45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55 50	55 65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57 00	57.15	57.30	57 45	57.60	57 75	57.90	58.05	58.20	58 35	38
39	58 50	58.65	58 80	58.95	59.10	59 25	59.40	59 55	59.70	59.85	39
40	60 00	60 15	60 30	60 45	60 60	60.75	60 90	61.05	61 20	61.35	40
41	61.50	61 65	61 80	61 95	62 10	62 25	62.40	62 55	62 70	62.85	41
42	63 00	63.15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64.35	42
43	64.50	64 65	64 80	64.95	65.10	65 25	65 40	65.55	65.70	65.85	43
44	66 00	66 15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67 50	67 65	67 80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69 00	69 15	69 30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70 50	70 65	70 80	70 95	71.10	71.25	71 40	71.55	71.70	71.85	47
48	72.00	72 15	72.30	72.45	72.60	72.75	72.90	73 05	73.20	73 35	48
49	73 50	73 65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.