

1247

WEST

FIELD BOOK

No. 385 F

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ENGINEERING DEPARTMENT
CITY OF SAN DIEGO,
CALIFORNIA.

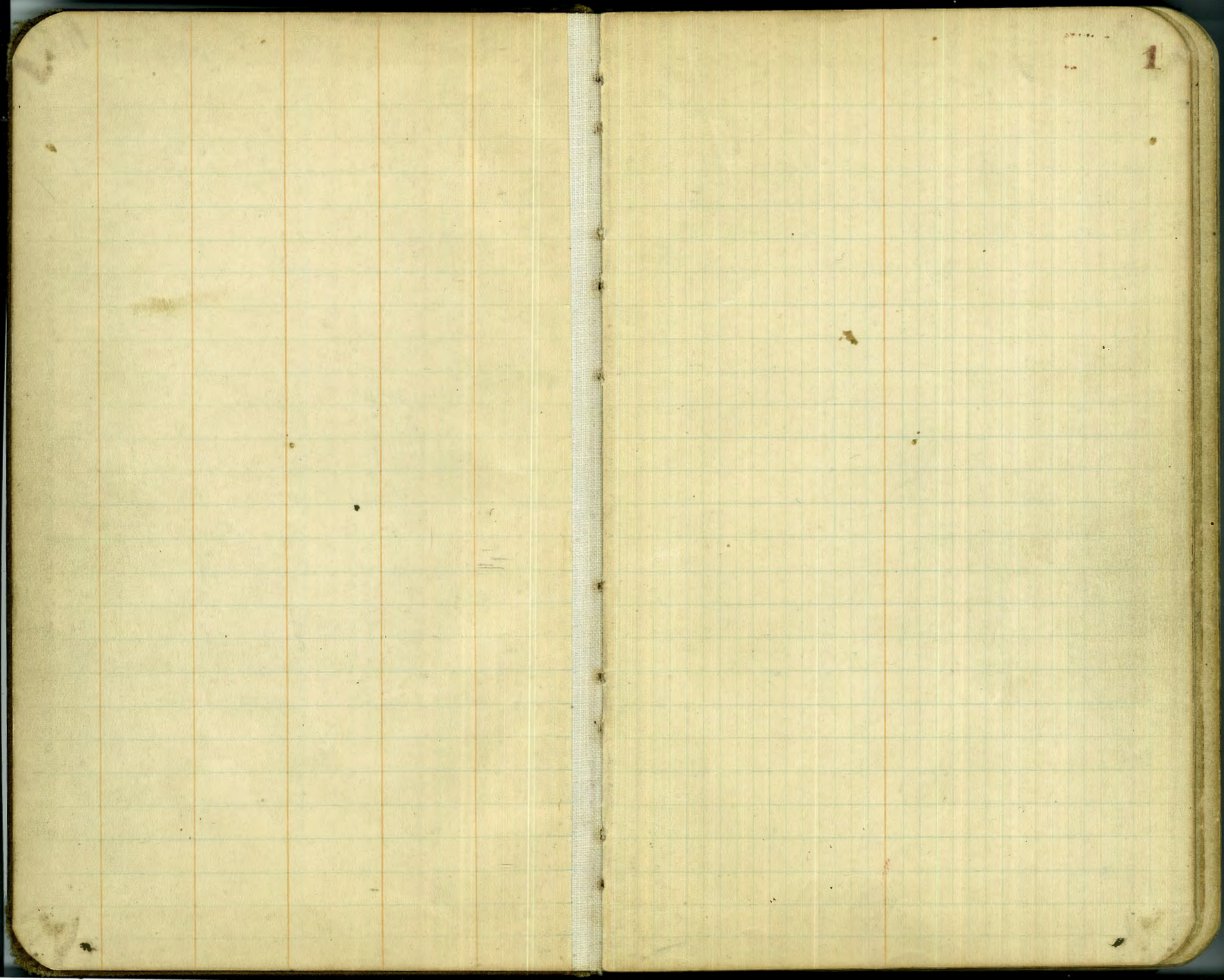
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South Chollas Rd. connecting 54th Street
with Euclid Ave.

STA. Dist. Defl. α

0+00 Intersection of Chollas Rd. & 54th St.

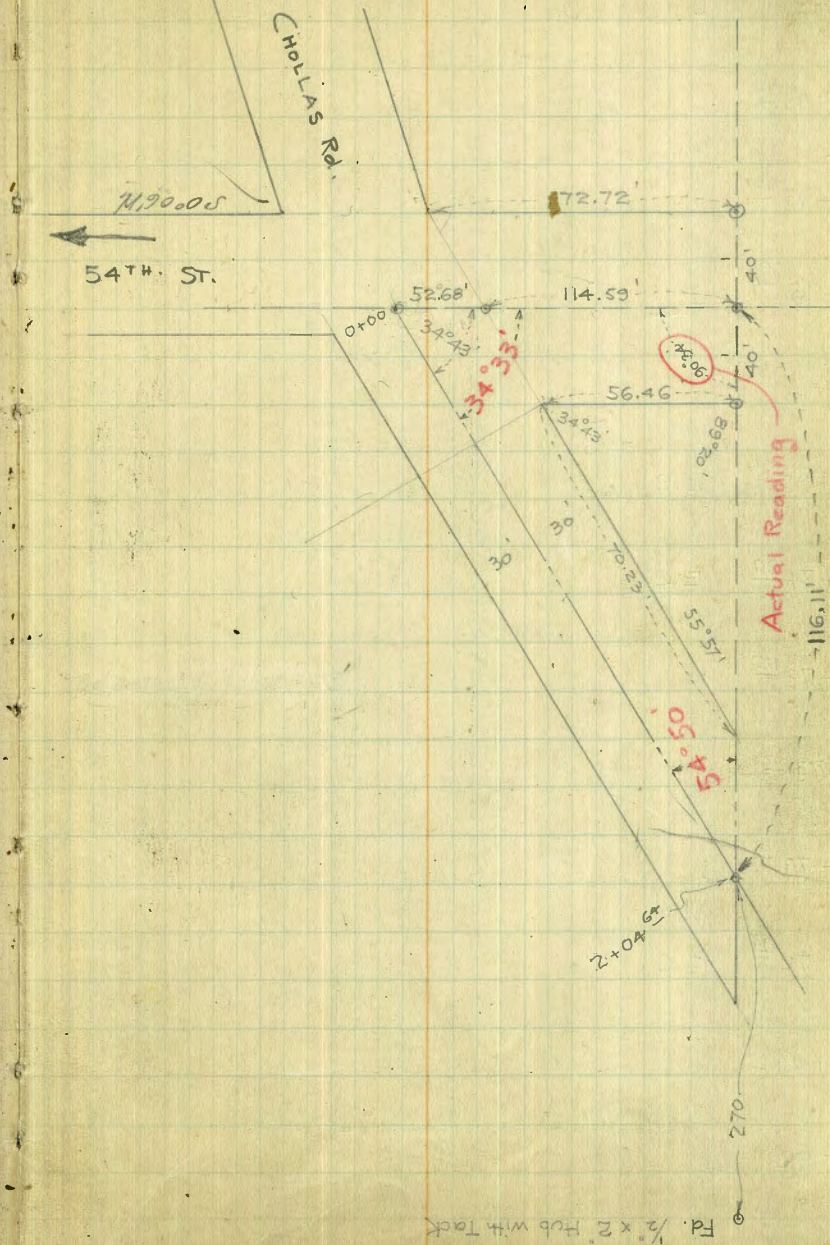
204.64

2+04⁶⁴ Intersection of Chollas Rd. & So. Line Lemon Villas

JAEGER
Bailey
Clavert

April 19th 1928

2



STA. Dist. Defl. \pm

11+95⁹²
100

10+95⁸⁶
100

9+95⁷⁸
100

8+95⁷³
100

7+95⁶⁶ B.C.

6+74³⁰ E.C.
1.75

6+73¹³
100

5+73⁰⁷
100

4+73⁰¹
100

3+72⁹⁴ B.C.

2+04⁶⁴

0+00

Plotted hard copy 5-19-28

P.I. to P.I. 63425

$\Delta = 17^{\circ}18' - R$

$R = 1000'$

$P.I. 5+25.07$

$L = 301.94$

$T = 152.13$

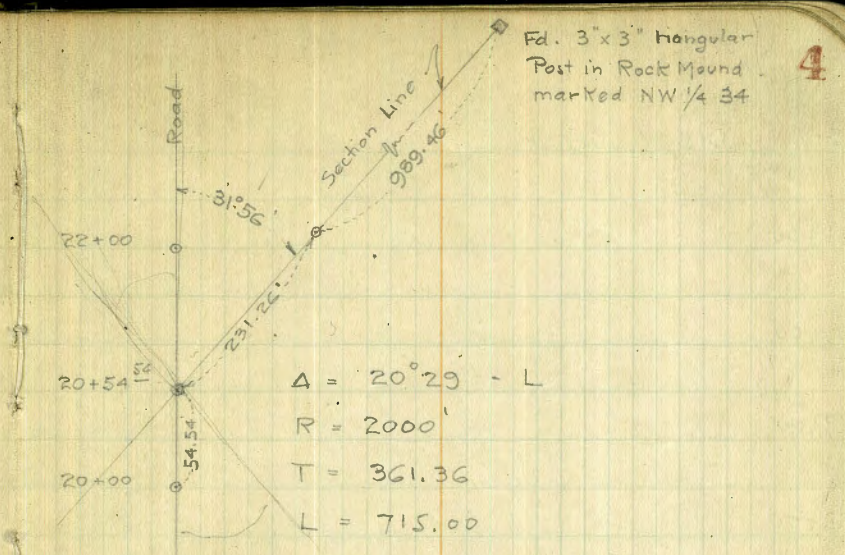
3 - 100' Chord Defl. \pm $2^{\circ}52'$ Arc = 100.07'

1 - 1.75' " " \pm $0^{\circ}03'$ " 1.75'

Sta.	Dist.	Defl. Δ
22+00	R.O.T.	
21+00	"	
20+54 ⁵⁴	" Intersection with Section Line	
20+00	"	
19+00	"	
18+00	"	
17+00	"	
16+26 ⁰⁰	" ϕ 36" Galloway W.S. Pipe Line	
	26.00	
16+00	P.O.T.	
	89.34	
15+10 ⁶⁰	E.C.	
	14.54	
14+96 ¹²		
	100	
13+96 ⁰⁵		
	100	
12+95 ⁹⁹		
	100	

PI to PI 1067' $\frac{1}{2}$

PI 11+44' $\frac{00$



7 - 100' Chords Defl. $\frac{1}{2}$ 1° 26' Arc = 100.07
 1 - 14.54 " Defl. $\frac{1}{2}$ 0° 12' 30'' = 14.54

0-12'-30" ✓	1-26
1-26	1-26
1-38'-30" ✓	2-52 ✓
1-26	1-26
3-04'-30" ✓	4-18 ✓
1-26	1-26
4-30'-30" ✓	5-44 ✓
	1-26
	7-10 ✓

STA. Dist. Defl. α

31+00

30+00

29+00

28+00

27+00

26+00

25+00

24+00

23+00

22+56⁵⁶ E.C.

L = 79.12

21+77⁴⁴ B.C.

22+17 P.I.

PI to P.T. 13 9851

PI 2217

$$\Delta = 2^{\circ}16' - L$$

$$R = 2000'$$

$$T = 39.56$$

$$L = 79.12'$$

STA. Dist. Defl. \angle

40+47³⁰

40+00

39+00

38+00

37+00

36+00

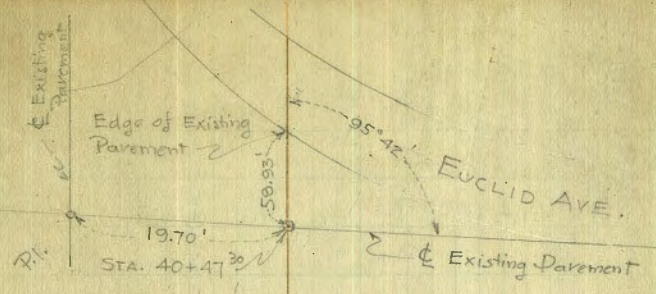
35+00

34+55⁵¹ P.I. 1°28'-R
55°51'

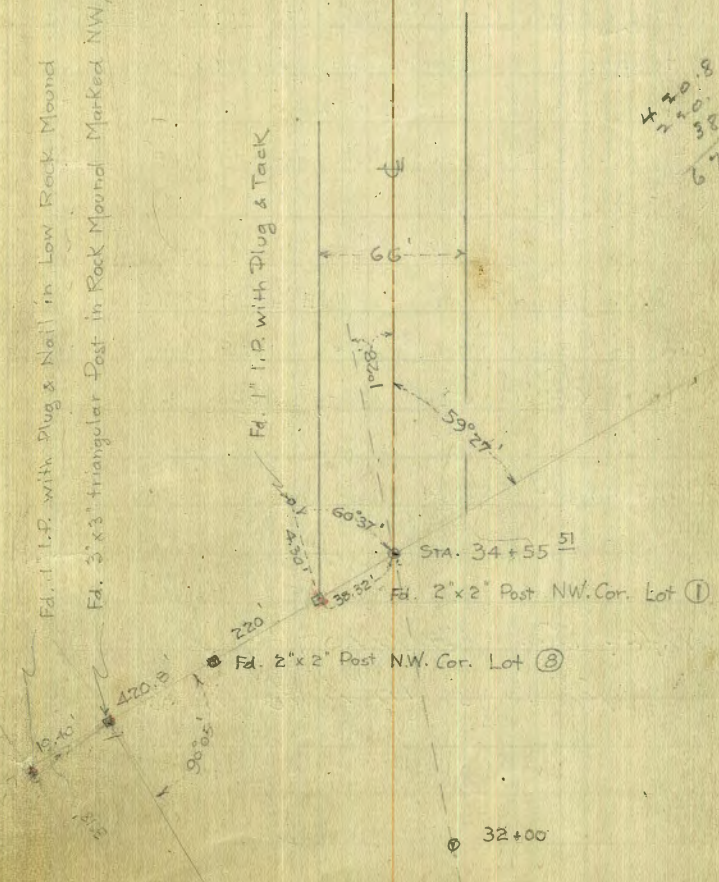
34+00

33+00

32+00



Fd. 1" I.P. with Plug & Nail in Low Rock Mound
 Fd. 3' x 3' triangular Post in Rock Mound Marked NW 1/4 34



420.8
 220.0
 38.32
 679.12

STA.	Dist.	Defl. α
11+17 ⁶⁴	E.C.	
4	99.10	
10+18 ⁵³		
3	100	
9+18 ³⁷		
4	100	
8+18 ²⁰		
1	100	
7+18 ⁰³	B.C.	

Hard copy Plotted 5-19-28

55°15' - L with S.L. Wadsworth Olive Grove Sub.

1+13⁰³ 12°40' with ϵ Tangent Existing Parem^t
 0+23⁰⁰ Edge of Parem^t
 0+00 ϵ Existing on Euclid Ave.

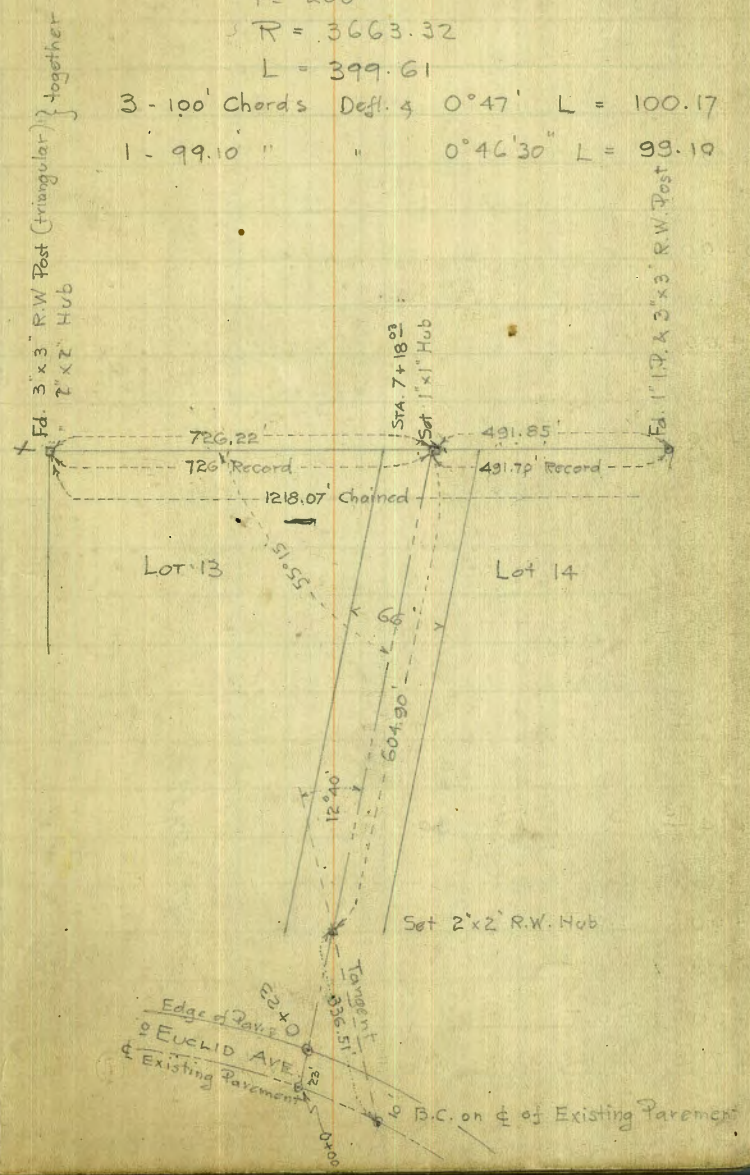
$$\Delta = 6^{\circ}15' - L$$

$$T = 200'$$

$$R = 3663.32$$

$$L = 399.61$$

3 - 100' Chords Defl. α 0°47' L = 100.17
 1 - 99.10 " " 0°46'30" L = 99.10



STA. Dist. Defl. \angle

20+00

19+00

18+00

17+00

16+00

15+00

14+93⁴³ E.C.

L 157.08

13+36³⁵ B.C.

14+14⁹³ P.I. $4^{\circ}30' - R$

14+00 P.O.T.

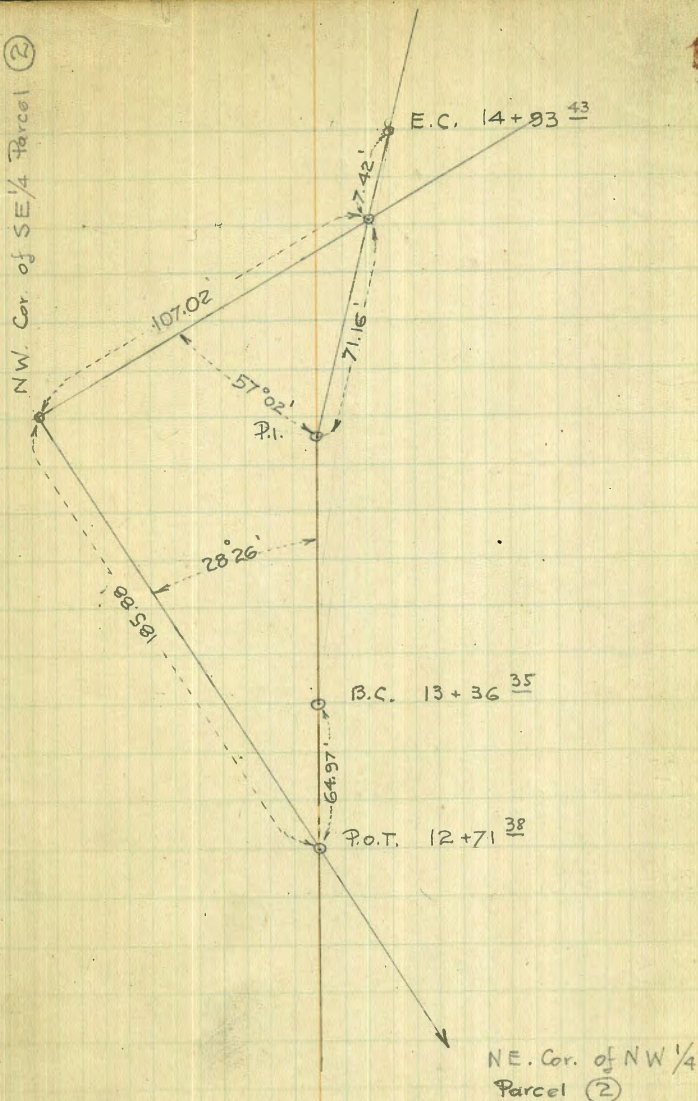
13+00 P.O.T.

+71³⁸ Intersection with E.L. of NW $\frac{1}{4}$ Parcel ②

12+00 P.O.T.

PT 76 FT. 497.29

NW. Cor. of SE $\frac{1}{4}$ Parcel ②



$$\Delta = 4^{\circ}30' - R$$

$$R = 2000$$

$$T = 78^{\circ}58'$$

$$L = 157.08$$

10

24+79⁷⁵ E.C.
 22+39⁵¹ B.C.
 23+66⁴⁹ P.I. 45°53'-R
 23+00
 22+00
 21+00

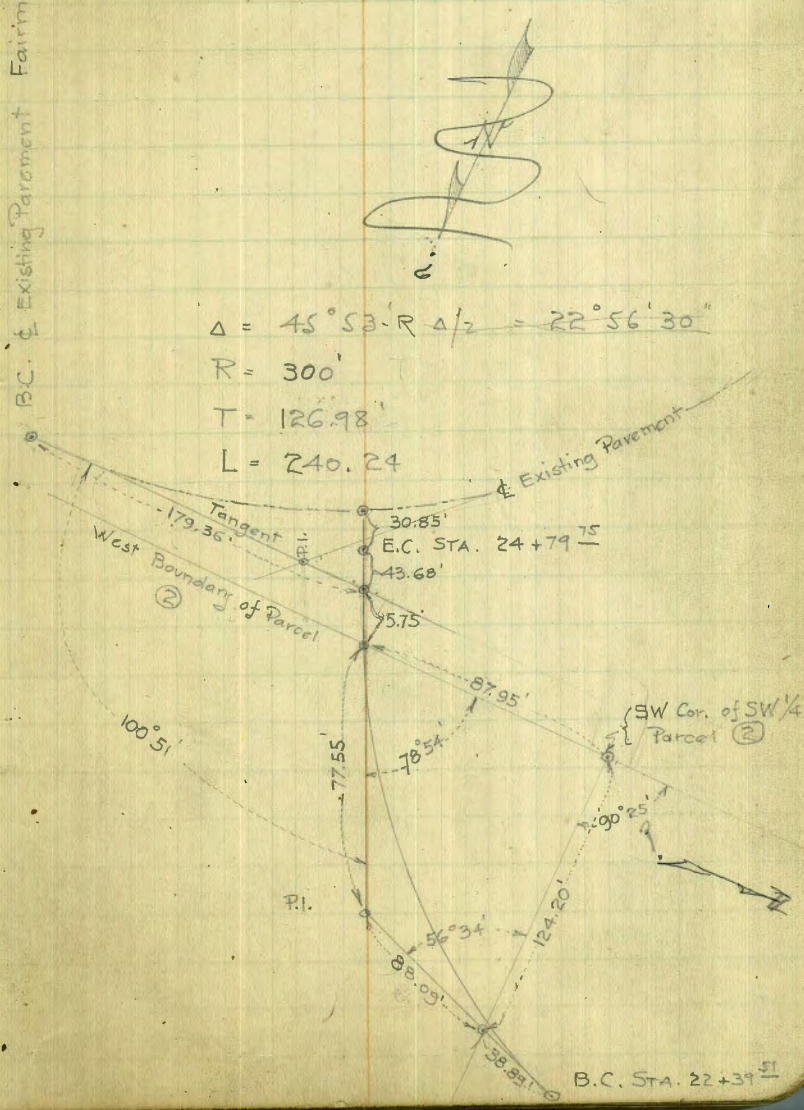
B.C. & Existing Pavement Fairmont Ave.

$$\Delta = 45^{\circ}53' - R \quad \Delta/2 = 22^{\circ}56'30''$$

$$R = 300'$$

$$T = 126.98'$$

$$L = 240.24'$$



Proposed Location of 54th Str.

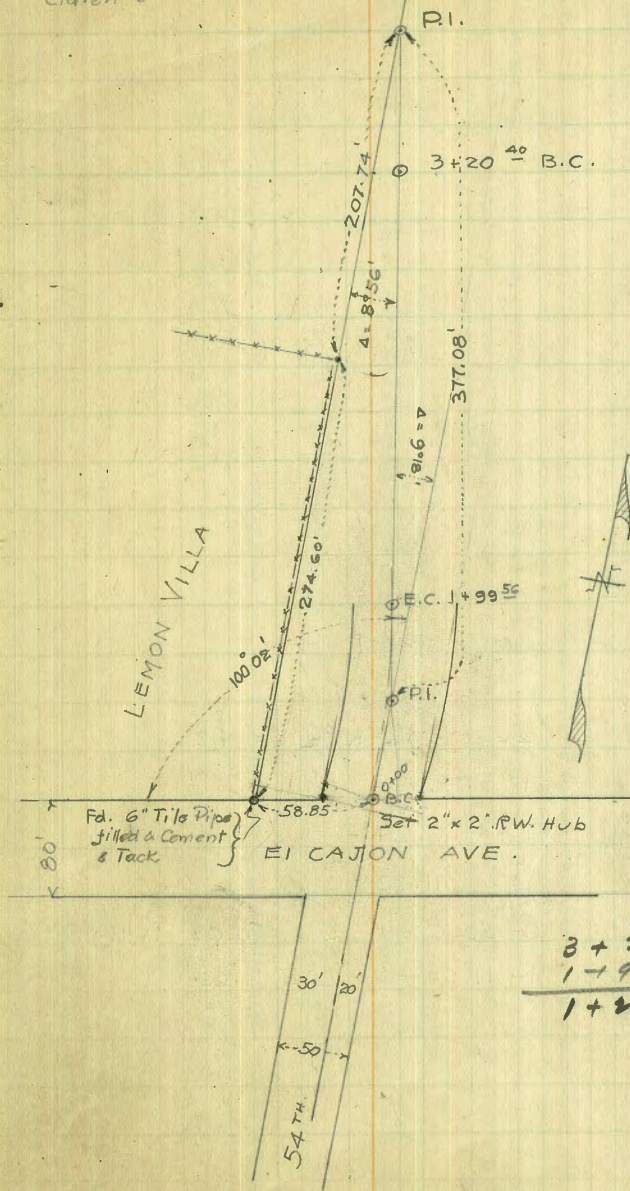
STA.
 3+70⁴³
 3+20⁴⁰ B.C.
 3+00 P.O.T.
 2+50 "
 1+99⁵⁶ E.C.
 1+50²¹
 1+60¹⁴
 0+50⁰⁷
 0+00 B.C.

$\Delta = 9^{\circ}18' - L \Delta/2 = 4^{\circ}39'$
 $R = 1229.46$
 $T = 100'$
 $L = 199.56$
 3- 50' chords $L^s = 50.07$ Defl. $\approx 1^{\circ}10'$
 1- 49.35 " $L^s = 49.35$ " $1^{\circ}09'$

See Field Book 1240 Page 103

JAEGER }
 Bailey } May 22nd 1928
 Clavert }

13



3+2040
 1+9956
 1+2084

8+10⁹³8+00⁰⁰7+50⁰⁰7+00⁰⁰6+50⁰⁰6+32²³ E.C.

7

6+20⁵⁸

6

$$\Delta = 8^\circ 56' - R \frac{1}{2} = 4.28'$$

$$R = 2000'$$

5+70⁵⁵

5

$$T = 156.24'$$

5+20⁵²

$$L = 311.83'$$

4+70⁴⁹

4

$$6-50' \text{ Chords } L^s = 50.03' \text{ Defl. } 30^\circ 43'$$

$$1-11.64' \quad L^s = 11.65' \quad " \quad 0^\circ 10'$$

3

4+20⁴⁶

2

3+70⁴³

SE. Cor. of Portion
of Lot 22 Partition
of Rancho Mission of
SAN DIEGO

8+10⁹³E.C. 6+32²³

P.I.

Road

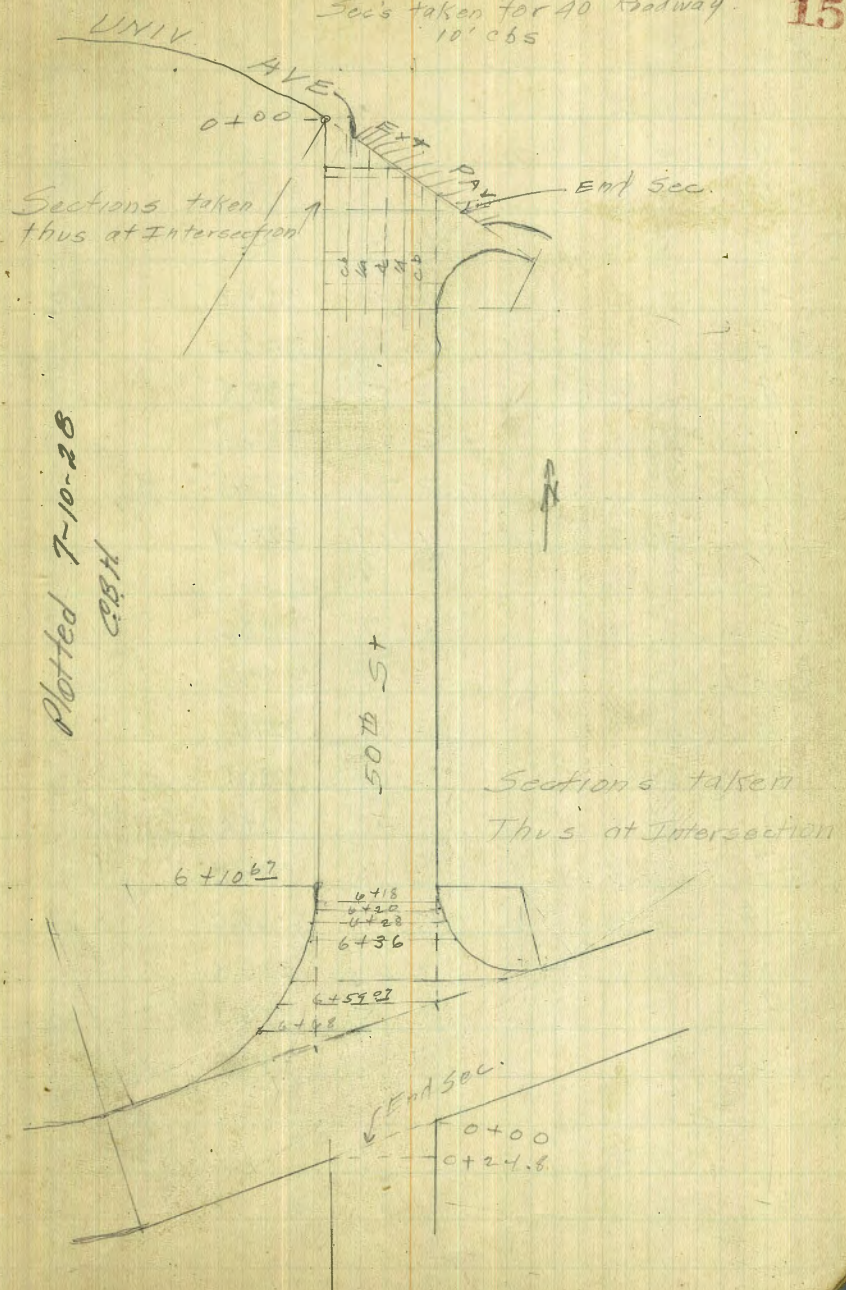
E

Xsec. 50th St. From Univ. Ave

B.M.	0.41	315.98	315.57	20' x 11' 52' x Univ.
T.P.	11.84	322.48	5.34	310.64
T.P.	11.75	333.88	0.35	322.13
T.P.	3.19	333.27	3.80	330.08
End Sec				
w.L.		3.0		330.27
top w cb		3.20		330.07
w gut		3.97		329.30
1/4 Pav.		3.85		329.42
1/2 Pav		3.78		329.49
1/4 Pav		3.90		329.37
cb Pav		4.15		329.12
E.L. Pav		4.51		328.76
10'E Pav.		4.86		328.41
gut at E rot.		5.43		327.84
top of cb E rot & L		4.89		328.38
D + 34				
E 1/4 + 3 Pav Int		3.97		329.30
E 1/4		3.8		329.5
1/2		3.3		330.0
1/4		3.3		330.0
+7		4.0		329.3
+8		3.1		330.2
cb		2.8		330.5
W? E.L.		3.0		330.3

to Landis St.

Secs taken for 40' Railway. 10' cbs



0+37	333.27		
w.L.	1.0	332.3	
+2	2.8	330.5	
cb	2.7	330.6	
+2	2.8	330.5	
+3	4.0	329.3	
+5	3.8	329.5	
1/4	3.5	329.8	
⊕	3.2	330.1	
1/4	3.7	329.6	
+7 Int. with Pav	4.06	329.21	
0+57			
E.L.	4.9	328.6	
cb	3.7	329.6	
1/4	3.4	329.9	
⊕	3.2	330.1	
1/4	3.5	329.8	
+6	4.1	329.2	
+8	3.3	330.0	
cb	3.0	330.3	
+9	2.5	330.8	
w.L.	1.6	331.7	

0+59	333.27		
w.L.	2.5	330.8	
cb	3.5	329.8	
+5	4.1	329.2	
1/4	3.6	329.7	
⊕	3.2	330.1	
1/4	3.5	329.8	
cb	3.6	329.7	
E.L.	4.5	328.8	
0+84			
95'E Int with Erot	4.5	328.8	
E.L.	4.6	328.7	
cb	4.6	328.7	
1/4	4.5	328.8	
⊕	3.8	329.5	
1/4	4.1	329.2	
+5	4.6	328.7	
cb	3.9	329.4	
+6	3.3	330.0	
+8	2.6	330.7	
w.L.	2.6	330.7	
0+88			
w.L.	2.7	330.6	
cb	3.0	330.3	
+2	4.0	329.3	
+5	4.6	328.7	
1/4	4.2	329.1	

50th

0+88		333.27	
♀	4.0	329.3	
1/4	4.5	328.8	
cb	4.7	328.6	
E.L.	4.8	328.5	
7/8 Int with E rot	4.9	328.4	
1+00			
in E Int with E rot	5.4	327.9	
E.L.	5.3	328.0	
+7	4.8	328.5	
cb	5.0	328.3	
1/4	4.9	328.4	
♀	4.3	329.0	
1/4	4.6	328.7	
+5	4.9	328.4	
+7	4.7	328.6	
cb	3.7	329.6	
w.L.	3.3	330.0	
1+07 ⁴³ = Endrot one			
w.L.	3.6	329.7	
cb	3.8	329.5	
+3	5.1	328.2	
+5	5.2	328.1	
1/4	4.9	328.4	
♀	4.6	328.7	
1/4	5.2	328.1	
cb	5.3	328.0	
E.L.	5.7	327.6	

1+25		333.27	
E.L.	6.1	327.2	
cb	5.6	327.7	
+2	5.6	327.7	
+5	5.9	327.4	
1/4	5.7	327.6	
♀	5.4	327.9	
1/4	5.6	327.7	
+3	5.7	327.6	
+4	6.0	327.3	
+7	5.6	327.7	
cb	4.7	328.6	
+3	4.1	329.2	
w.L.	4.7	328.6	
1+50			
w.L.	5.8	327.5	
cb	5.9	327.4	
+4	6.4	326.9	
+4	7.3	326.0	
+7	7.6	325.7	
+8	7.3	326.0	
1/4	7.0	326.3	
♀	6.5	326.8	
1/4	6.7	326.6	
+5	7.1	326.2	
+8	6.4	326.9	
cb	6.2	327.1	

17

50th

1+50	333.27		
E.L.	6.6	326.7	
1+75			
E.L.	7.4	325.9	
+5	7.2	326.1	
cb	7.5	325.8	
+2	7.8	325.5	
+5	8.4	324.9	
+7	8.5	324.8	
1/4	8.1	325.2	
1/4	7.8	325.5	
1/4	8.2	325.1	
+3	8.6	324.7	
+5	8.5	324.8	
+8	7.2	326.1	
cb	6.7	326.4	
w.L.	7.0	326.3	
2+00			
w.L.	8.4	324.9	
+2	8.8	324.5	
cb	8.9	324.4	
+2	8.7	324.4	
+5	7.7	323.4	
+7	10.3	323.0	
+9	9.9	323.4	
1/4	7.8	323.5	

18

2+00	333.27		
1/4	9.4	323.9	
E 1/4	9.6	323.7	
+3	10.2	323.1	
+5	10.0	323.3	
cb	9.2	324.1	
+5	8.5	324.8	
E.L.	8.6	324.7	
2+25			
E.L.	9.7	323.6	
cb	10.3	323.0	
+2	11.2	322.1	
+5	11.8	321.5	
1/4	11.4	321.9	
1/4	11.3	322.0	
1/4	11.5	321.8	
+5	11.8	321.5	
+6	12.2	321.1	
+9	10.7	322.6	
cb	10.7	322.6	
+8	10.7	322.6	
w.L.	9.7	323.6	

50th

2+28	333.27	
w.l.	11.2	322.1
cb	10.9	322.4
+2	11.3	322.0
+4	12.5	320.8
+5	12.1	321.2
1/4	11.8	321.5
¢	11.6	321.7
1/4	11.7	321.6
+5	12.0	321.3
+9	11.6	321.7
cb	10.5	322.8
E.L.	10.0	323.3
2+62		
E.L.	12.9	320.4
cb	13.0	320.3
+1	13.2	320.1
+2	14.2	319.1
+5	14.8	318.5
1/4	14.5	318.8
¢	14.4	318.9
1/4	14.6	318.7
+3	14.8	318.5
+6	15.4	317.9
+9	13.3	320.0
cb	13.2	320.1
w.l.	13.2	320.1

19

	333.27	
0.67	321.14	12.80
2+82		320.49
w.l.		3-2
cb		2.8
+2		3.0
+3		4.5
+7		4.3
+8		4.0
1/4		4.0
¢		3.6
1/4		3.9
+5		3.4
cb		2.5
E.L.		2.4
2+97		
E.L.		3.1
+5		3.2
cb		3.9
+5		4.6
1/4		4.6
¢		4.5
1/4		4.8
+5		5.2
+9		5.0
+8		4.0
cb		4.0

50th

2+97	321.44		
wL	4.6	316.5	
3+00			
wL	5.5	315.6	
cb	4.2	316.9	
+2	4.3	316.8	
+4	5.3	315.8	
+6	5.3	315.8	
1/4	5.0	316.1	
1/2	4.7	316.4	
3/4	4.7	316.4	
+7	4.6	316.5	
+9	3.7	317.4	
cb	3.4	317.7	
E.L.	3.1	318.0	
3+15			
E.L.	3.8	317.3	
cb	3.9	317.2	
+2	5.4	315.7	
1/4	5.6	315.5	
1/2	5.7	315.4	
3/4	6.1	315.0	
+5	6.4	314.7	
+6	7.1	314.0	
+7	6.4	314.7	
cb	7.0	314.1	
wL	8.3	312.8	

20

3+15	321.14		
10'w	8.0	313.1	
3+30			
10'w	9.2	311.9	
wL	9.1	312.1	
cb	8.2	312.9	
1/4	7.7	313.4	
+5	7.7	313.4	
1/2	7.1	314.0	
3/4	7.0	314.1	
+5	7.1	314.0	
cb	4.9	316.2	
E.L.	4.7	316.4	
3+55			
E.L.	6.4	314.7	
cb	6.9	314.2	
+5	9.6	311.5	
1/4	9.4	311.7	
1/2	9.8	311.3	
3/4	10.0	311.1	
cb	10.4	310.7	
wL	10.8	310.3	
10'w	10.3	310.8	

5074

3+75		321.14	
10' W		10.4	310.7
5' W		11.6	309.5
w.l.		12.0	309.1
cb		11.9	309.2
+3		11.7	309.4
+4		12.1	309.0
1/4		11.8	309.3
1/2		11.7	309.4
1/4		11.8	309.3
+8		11.5	309.6
cb		8.5	312.6
E.L.		8.2	312.9
3+84			
E.L.		8.9	312.2
+5		9.1	312.0
cb		11.7	309.4
+3		12.6	308.5
1/4		12.7	308.4
1/2		12.6	308.5
1/4		12.7	308.4
+5		12.8	308.3
+8		12.0	309.1
cb		12.1	309.0
w.l.		12.0	308.9
T.P.	2.36	311.47	12.03 309.11

21

3+87		311.47	
w.l.		2.6	308.9
+5		2.7	308.8
cb		2.5	309.0
+2		2.5	309.0
+5		3.3	308.2
1/4		3.4	308.1
1/2		3.4	308.1
1/4		3.3	308.2
+7		3.2	308.3
cb		2.4	309.1
E.L.		1.2	310.3
4+00			
E.L.		3.5	308.0
+3		4.0	307.5
+5		5.0	306.5
cb		4.3	307.2
+5		4.1	307.4
1/4		4.3	307.2
1/2		4.5	307.0
1/4		4.3	307.2
+5		4.0	307.5
cb		2.8	308.7
+1		2.9	308.6
+2		3.7	307.8
w.l.		2.6	308.9

50th

H+16	311.47		
w.L.	1.7	309.8	
+7	4.1	307.4	
+9	4.1	307.4	
cb	3.8	307.7	
+2	4.2	307.3	
+7	5.3	306.2	
1/4	5.4	306.1	
+5	5.9	305.6	
⊕	5.8	305.7	
1/4	5.9	305.6	
+5	5.6	305.9	
cb	6.5	305.0	
E.L.	8.3	303.2	
3'E	7.2	304.3	
10'E	6.9	304.6	
H+28			
10'E	8.1	303.4	
E.L.	7.9	303.6	
cb	7.7	303.8	
+5	7.4	304.1	
1/4	6.7	304.8	
⊕	6.5	305.0	
1/4	6.9	304.6	
+2	6.8	304.7	
+5	4.6	306.9	

22

4+28	311.47		
web	4.4	307.1	
w.L.	0.3	311.2	
4+34			
w.L.	0.4	311.1	
+5	2.5	309.0	
cb	4.0	307.5	
1/4	5.9	305.6	
+5	7.0	304.5	
⊕	6.8	304.7	
+5	6.7	304.8	
1/4	6.8	304.7	
+7	7.2	304.3	
cb	8.0	303.5	
+3	9.1	302.4	
E.L.	9.0	302.5	
10'E	8.7	302.8	
A+35			
10'E	13.0	298.5	
E.L.	14.7	296.8	
+5	13.4	298.1	
cb	8.6	302.9	
+5	7.1	304.4	
1/4	6.9	304.6	
⊕	7.1	304.4	
+5	7.0	304.5	
1/4	6.0	305.5	

504

4+35	311.47		
w 1/4+5		5.1	306.4
cb		4.0	307.5
w.L		0.5	311.0
E garage at 2' w 4+40		2.77	308.7
4+38			
w.L		2.8	308.7
+5		3.1	308.4
cb		4.1	307.4
+5		5.4	306.1
1/4		6.2	305.3
+5		7.2	304.3
1/4		7.2	304.3
+5		7.0	304.5
1/4		7.1	304.4
+6		7.0	304.5
cb		9.4	302.1
+7		14.2	297.3
E.L		14.5	297.0
10'E		13.4	298.1
15'E		12.6	298.9

23

4+46	311.47		
15'E		15.3	296.2
5'E		17.0	294.5
E.L		17.3	294.2
+5		13.6	297.9
cb		10.5	301.0
+3		8.9	302.6
+7		7.5	304.0
1/4		7.6	303.9
+2		10.1	301.4
+4		7.6	303.9
1/4		7.6	303.9
1/4		7.1	304.4
+5		5.6	305.9
cb		4.3	307.2
+5		3.1	308.4
w.L		2.9	308.6
4+48			
w.L		0.5	311.0
+2		2.3	309.2
+5		2.8	308.7
cb		4.3	307.2
+5		4.9	306.6
+5		7.1	304.4
1/4		7.5	304.0
+5		7.6	303.9
1/4		7.7	303.8

50th

4+48	311.47		
E+6	7.7	303.8	
1/4	10.5	301.1	
+5	11.4	300.1	
cb	11.8	299.7	
+5	13.2	298.3	
E.L.	17.2	294.3	
5'E	18.4	293.1	
15'E	15.2	296.3	
4+53			
10'E	19.4	292.1	
E.L.	18.4	293.1	
cb	13.4	298.1	
+8	11.1	300.4	
1/4	8.3	303.2	
+5	7.8	303.7	
E	7.8	303.7	
+5	7.7	303.8	
1/4	7.7	303.8	
+3	7.5	304.0	
+6	5.2	306.3	
cb	4.8	306.7	
+5	2.8	308.7	
W.L.	0.5	311.0	

4+57

311.47

4+57	311.47		
W.L.	0.0	311.5	
+5	3.4	308.1	
cb	4.9	306.6	
+7	5.9	305.6	
+8	7.2	304.3	
1/4	7.8	303.7	
+5	7.8	303.7	
E	8.4	303.1	
+5	7.9	303.6	
1/4	7.8	303.7	
+6	9.1	302.4	
cb	9.8	301.7	
+5	12.3	299.2	
E.L.	16.2	295.3	
5'E	19.1	292.4	
10'E	20.6	290.9	
15'E	17.1	294.4	
4+75			
18'E	24.8	286.7	
7'E	17.1	292.4	
E.L.	16.0	295.5	
+5	14.1	297.4	
cb	10.6	300.9	
+3	7.5	302.0	
1/4	8.8	302.7	

$$\begin{array}{r} 315 \\ 25 \\ \hline 106 \end{array}$$

24

50th

25

4+75	311.47		
ϕ	8.8	302.7	
1/4	8.2	303.3	
+2	7.9	303.6	
+5	5.9	305.6	
cb	5.4	306.1	
+5	5.0	306.5	
w.L.	0.4	311.1	
5+00			
w.L.	0.0	311.5	
+2	0.7	310.8	
+7	5.2	306.3	
cb	5.8	305.7	
+8	5.8	305.7	
1/4	6.4	303.3	
+5	8.9	302.6	
ϕ	8.7	302.8	
1/4	9.1	302.4	
cb	9.9	301.6	
+5	10.7	300.8	
EL	13.8	297.7	
10'E	17.2	294.3	
15'E	20.0	291.5	

5+25	311.47		
15'E	16.6	294.9	
10'E	15.5	296.0	
EL	13.3	298.2	
+5	10.9	300.6	
cb	10.0	301.5	
1/4	9.7	301.8	
ϕ	9.2	302.3	
+5	9.4	302.1	
1/4	8.5	303.0	
+3	6.5	305.0	
cb	6.5	305.0	
+6	2.0	309.5	
w.L.	0.6	310.9	
5+50			
w.L.	2.4	309.1	
+3	3.0	308.5	
+8	6.7	304.8	
cb	7.6	303.9	
+3	7.4	304.1	
1/4	9.2	302.3	
ϕ	9.7	301.8	
+5	9.4	302.1	
1/4	10.3	301.2	
+5	11.5	300.0	
1/4	11.4	300.1	

50th

305.2

5+50	311.47		
E'9+7	11.7	299.8	
EL.	13.2	298.3	
15'E	15.6	295.9	
T.P. 5.91	305.24	12.14	299.33
5+75			
15'E	11.3	293.9	
EL.	8.9	296.3	
+5	6.8	298.4	
cb	7.5	297.7	
+5	7.6	297.6	
1/4	7.3	297.9	
+5	5.7	299.5	
1/2	4.4	300.8	
+5	4.1	301.1	
1/4	4.0	301.2	
+1/2	2.9	302.3	
+5	2.7	302.5	
cb	2.7	302.5	
+3	1.9	303.3	
+7	+1.2	306.4	
W.L.	+2.0	307.2	

26

6+00	305.24		
W.L.	1.3	303.9	
+3	1.9	303.3	
+6	4.0	301.2	
cb	4.6	300.6	
+5	4.4	300.8	
1/4	5.2	300.0	
+1/2	6.0	299.2	
1/2	7.6	297.6	
+5	8.4	296.8	
1/4	9.7	295.5	
cb	9.6	295.6	
+3	9.5	295.7	
+5	8.6	296.6	
+8	8.8	296.4	
EL.	9.8	295.4	
5'E	11.8	293.4	
15'E	12.8	292.4	
6+10 ⁶²	= B.C. ONE = B.C. ret. ONE		
15'E	14.3	290.9	
EL.	11.6	293.6	✓
+3	10.5	294.7	
+5	10.5	294.7	
+6	11.3	293.9	
cb	11.2	294.0	
+5	11.1	294.1	

50th

6+1062		305.24	
E 1/4	10.7	294.5	
±	8.4	296.8	
1/4	7.4	297.8	
+3	5.3	299.9	
cb	5.3	299.9	
+5	4.8	300.4	
w.L	2.5	302.7	
6+18			
0 5/8 W Int with curve ^{on W}	2.9	302.3	
w.L	2.9	302.3	
+2	4.6	300.6	
cb	5.1	300.1	
+7	5.6	299.6	
1/4	7.4	297.8	
±	9.3	295.9	
+5	10.3	294.9	
1/4	11.4	293.8	
+4	12.3	292.9	
+6	11.9	293.3	
cb	12.2	293.0	
+4	10.5	292.7	
+5	12.0	293.2	
E.L	13.0	292.2	
0 5/8 E Int with reton E	13.2	292.0	
15'E	14.9	290.3	

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6+20		305.24	
15'E	15.1	290.1	
1.5'E Int with reton E	13.3	292.7	
E.L	13.3	291.9	
+4	12.0	293.2	
+6	12.6	292.6	
cb	12.3	292.9	
+4	12.0	293.2	
+7	12.5	292.7	
1/4	12.7	292.5	
cb	9.5	295.7	
+2	9.1	295.1	
+8	8.5	296.7	
1/4	7.4	297.8	
+3	5.9	299.3	
cb	5.1	300.1	
w.L	4.2	301.0	
0 7/8 W Int with curve on W	3.6	301.6	
6+28			
1' W Int with curve on W	4.2	301.0	
w.L	4.4	300.8	
+5	4.8	300.4	
cb	5.8	299.4	
+8	6.5	298.7	
1/4	8.1	297.1	
±	10.0	295.2	

50th

6+28

305.29

E 1/4	12.0	293.2
+5	13.2	292.0
cb	13.4	291.8
+5	13.4	291.8
+7	12.7	292.5
E.L.	13.4	291.8
5.3'E Int with ret. on E	12.3	292.9
15'E	15.8	289.4

6+36

13'E Int with ret on E	15.7	289.5
E.L.	14.1	291.1
cb	13.6	291.6
+3	14.0	291.2
1/4	12.6	292.6
±	10.8	294.4
4	9.2	296.0
+3	7.2	298.0
cb	6.7	298.5
+2	6.0	299.2
+5	4.4	300.8
E.L.	3.9	301.3
2.3'W Int with curve on W	3.9	301.3

6+50

305.29

6.5'W Int with curve on E	6.0	299.2
W.L.	6.8	298.4
cb	8.1	297.1
+8	9.4	295.8
1/4	10.2	295.0
+5	12.3	292.9
±	12.2	293.0
1/4	14.4	290.8
+5	14.4	290.8
cb	14.9	290.3
+5	15.3	289.9
+6	14.5	290.7
E.L.	14.0	291.2
12'E Int with ^{Wightman} N.L.	12.0	293.2

6+59⁰²

EL = N.L. Wightman	14.1	291.1
+5	14.7	290.5
+7	16.3	288.9
cb	15.9	289.3
+5	15.7	289.5
1/4	15.2	290.0
+5	13.5	291.7
±	13.0	292.2
+8	11.9	293.3
1/4	10.5	294.7

28

50th

6+59⁰⁷ 305 29

wcb	8.9	296.3
w.L.	8.2	297.0
9 ⁰ w Int. with ^{on w.} curve.	7.2	298.0
6+68		
14' w Int. with curve on W.	7.4	297.8 ✓
w.L.	9.0	296.2 ✓
cb	10.0	295.2
1/4	11.3	293.9
+3	12.7	292.5
±	13.8	291.4
+8	15.0	290.2
E 1/4 = Int with N.L. Wightman	16.0	289.2

End Section on N.L. Wightman

E.L.	13.8	291.4	✓ on N.L. 50th Produced South (Walker)
+7	15.3	289.9	
cb	16.4	288.8	
+7	17.1	287.1	
1/4	16.3	288.9	
+3	16.4	288.8	
+5	15.2	290.0	
±	14.6	290.6	
+9	14.1	291.1	
1/4	13.3	291.9	
cb	12.0	293.2	on N.L. 50th St
w.L.	11.6	293.6	Produced South } Walker

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305 29

T.P. 025	293.39	12.13	293.11
B.M. top pipe sw ^{wightman} 50th	10.45		282.94
B.M. 113	327.81		326.68
T.P. 11.40	327.60	11.61	316.20
T.P. 5.68	332.68	0.60	327.00
T.P. 2.08	321.94	12.82	319.86
T.P. 0.56	309.61	12.89	309.05
T.R. 0.81	297.78	12.64	296.97
T.P. 2.31	288.44	11.65	286.13
B.M. top pipe sw ^{wightman} 50th	5.44		283.00

sw B.P. Univ. of Florida

Sec 50th St From S.L.
50 wide 10' cbs

B.M.	1.57	284.57	283.00
End section on sl Wightman.			
E.L.	2.6	282.0	
+6	1.7	83.2	
cb	1.5	83.1	
1/4	1.9	82.7	
±	2.5	82.7	
+6	2.4	82.2	
1/4	2.4	82.2	
cb	1.9	82.7	
w.l.	1.8	82.8	
O+242			
w.l.	1.8	82.8	
cb	2.1	82.5	
1/4	2.9	81.7	
+5	3.5	81.1	
+7.	4.6	80.0	
±	4.2	80.4	
1/4	4.1	80.5	
+3	3.9	80.7	
cb	4.1	80.5	
+2	4.3	80.3	
E.L.	7.4	77.2	
10'E	10.2	74.4	

Plotted 7-10-28-C.B.H.

Wightman to Landis

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O+50	284.57	
10'E	14.3	70.3
E.L.	11.6	73.0
cb	8.5	76.1
+3	7.7	76.9
1/4	7.6	77.0
±	6.9	77.7
1/4	5.8	78.8
+5	5.4	79.2
+L	5.8	78.8
cb	5.4	79.2
w.l.	4.5	80.1
O+75		
w.l.	7.2	77.4
cb	8.4	76.2
1/4	9.1	75.5
±	10.5	74.1
+2	11.7	72.7
+3	11.1	73.5
1/4	11.5	73.1
+3	11.6	73.0
cb	12.8	71.8
+4	14.2	70.4
E.L.	14.5	70.1
10'E	15.2	69.4

50th

0+86	284.57		
10'E	16.1	68.5	
EL	15.0	69.6	
cb	14.0	70.6	
1/4	14.0	70.6	
ϕ	13.9	70.7	
+2	13.1	71.5	
1/4	12.6	72.0	
cb	11.8	72.8	
w.L.	10.5	74.1	
10'w	7.5	77.1	
1+00			
10'w	11.4	75.2	
w.L.	12.6	71.8	
cb	13.6	71.0	
+7	14.3	70.3	
1/4	14.7	69.9	
ϕ	14.9	69.7	
1/4	15.0	69.6	
cb	15.8	68.8	
EL	16.1	68.5	
10'E	16.6	68.0	
T.P.	1.25	273.94	11.88
			272.69

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1+30	273.94		
15'E	11.5	62.4	
14'E	10.6	63.3	
10'E	9.5	64.4	
8'E	7.2	66.7	
EL	6.7	67.2	
cb	6.4	67.5	
1/4	6.4	67.5	
ϕ	5.9	68.0	
1/4	5.8	68.1	
cb	5.8	68.1	
w.L.	5.7	68.2	
4'w	5.7	68.2	
10'w	5.1	68.8	
1+65			
10'w	7.9	66.0	
w.L.	8.0	65.9	
cb	7.9	66.0	
1/4	7.9	66.0	
ϕ	7.8	66.1	
1/4	8.0	65.9	
cb	8.2	65.7	
EL	8.3	65.6	
1'E	8.6	65.3	
3'E	11.2	62.7	
8'E	11.2	62.7	
11'E	12.4	61.5	

1+65	273.94		
15'E		8.8	65.1
1+73			
15'E		8.5	65.4
12'E		9.1	64.8
10'E		12.0	61.9
E.L.		11.4	62.5
+4		9.0	64.9
+6		8.3	65.6
cb		8.3	65.6
1/4		8.3	65.6
±		8.0	65.9
1/4		8.0	65.9
cb		8.2	65.7
w.L.		8.3	65.6
10'w		8.2	65.7
1+83			
10'w		8.7	65.2
w.L.		8.7	65.2
cb		8.3	65.6
1/4		8.3	65.6
±		8.4	65.5
+5		8.7	65.2
1/4		8.5	65.4
+7		8.4	65.5
cb		8.9	65.0

1+83	273.94		
+2		9.6	64.3
+4		12.1	61.8
E.L.		11.9	62.0
3'E		9.0	64.9
10'E		8.7	65.2
1+91			
10'E		8.8	65.1
5'E		8.9	65.0
E.L.		9.1	64.8
+2		9.7	64.2
+3		11.7	62.2
cb		12.1	61.8
+3		9.1	64.8
1/4		8.7	65.2
±		8.8	65.1
1/4		8.4	65.5
cb		8.6	65.3
w.L.		8.8	65.1
10'w		9.1	64.8
2+00			
10'w		9.4	64.5
w.L.		9.1	64.8
cb		8.8	65.1
+5		8.7	65.2
1/4		9.2	64.7

50th

2+00	273.94		
w'a+6	9.4	64.5	
+7	8.9	65.0	
¢	8.9	65.0	
¼	9.1	64.8	
+2	10.1	63.8	
+3	12.0	61.9	
+6	12.1	61.8	
cb	10.1	63.8	
+3	9.1	64.8	
E.L.	9.2	64.7	
3'E	9.1	64.8	
10'E	8.3	65.6	
2+25			
10'E	8.9	65.0 =	
E.L.	8.9	65.0	
+6	9.3	64.6	
cb	9.1	64.8	
¼	9.4	64.5	
+5	9.7	64.2	
¢	9.8	64.1	
+2	12.0	61.9	
¼	11.7	62.0	
+3	11.7	62.2	
+5	9.7	64.2	
cb	9.4	64.5	
w.L.	9.5	64.4	

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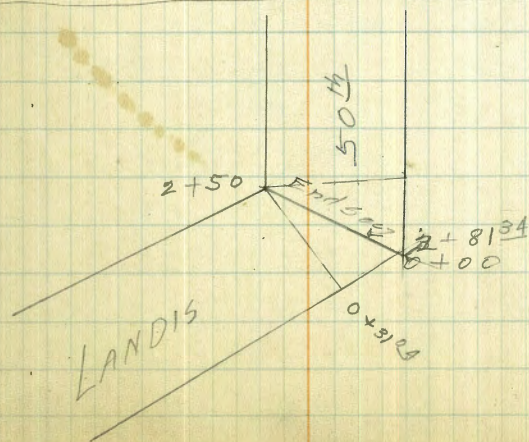
2+25	273.94		
10'w	9.9	64.0	
2+40			
10'w	9.9	64.0	
5'w	9.3	64.6	
w.L.	9.2	64.7	
+5	9.4	64.5	
+8	12.2	61.7	
cb	12.1	61.8	
+4	11.7	61.0	
+5	10.0	63.9	
¼	9.4	64.5	
¢	9.4	64.5	
¼	9.0	64.9	
cb	9.1	64.8	
+5	9.2	64.7	
E.L.	9.1	64.8	
10'E	9.0	64.9	
2+47			
10'E	9.3	64.6	
E.L.	9.4	64.5	
+7	9.0	64.9	
cb	9.2	64.7	
¼	9.3	64.6	
¢	9.2	64.7	
+3	9.5	64.4	

50th

2+47	273.99		
w 1/4	9.6	64.3	
+6	10.1	63.8	
cb	11.7	62.2	
+9	12.1	61.8	
w.l.	9.8	64.1	
5' w	9.6	64.3	
10' w	10.1	63.8	
2+50 = End 50 th on W.			
10' w	10.1	63.8	
5' w	9.2	64.7	
4' w	9.8	64.1	
2' w	12.0	61.9	
w.l.	12.0	61.9	
+6	12.0	61.9	
+8	9.7	64.2	
cb	9.2	64.7	
1/4	9.5	64.4	
1/2	9.2	64.7	
+5	9.5	64.4	
1/4	9.5	64.4	
cb	9.2	64.7	
+5	9.0	64.9	
E.L.	9.5	64.4	
10' E	9.3	64.6	

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End section	End 50 th	
10' E (on diag.)	8.2	65.7
E.L.	9.5	64.4
cb	9.6	64.3
1/4	9.6	64.3
1/2	9.8	64.1
1/4	9.8	64.1
cb	9.5	64.4
+4 (on diag.)	9.4	64.5
+8 "	10.4	63.5
+9 (on diag.)	12.2	61.7
w.l.	12.0	61.9
+1 (on diag.)	12.0	61.9
+2 w "	9.8	64.1
+5 w "	9.4	64.5
7' w "	10.2	63.7
+10 w "	10.3	63.6



X Sec Landis From 50th to
Winona. 50' wide 10' cbs.

27394

End section - Same as End 50th.

0+00 = Beginning of Landis on South

0+31⁰⁴ = Beginning of " " North

10' N	9.6	64.3
3' N	10.3	63.6
2' N	11.8	62.1
N.L.	12.0	61.9
+3	12.0	61.9
cb	10.3	63.6
+2	9.6	64.3
1/4	9.4	64.5
1/4	9.7	64.2
1/4	9.7	64.2
cb	9.7	64.2
S.L.	10.0	63.9
10' S	10.3	63.6
0+43		
10' S	10.2	63.7
S.L.	10.0	63.9
cb	9.9	64.0
1/4	9.6	64.3
1/4	9.7	64.2
+6	10.1	63.8
1/4	12.1	61.8
cb	11.9	62.0
+3	11.8	62.1

Plotted 7-10-28.

C.B.H.

35

0+43

27394

N.L.	10.2	73.7
N.L.	9.4	74.5
4' N	9.5	74.4
5' N	10.4	73.5
10' N	10.3	73.6
0+50		
10'	10.4	73.5
N.L.	10.5	73.4
+1	10.6	73.3
+5	9.2	74.7
+9	9.4	74.5
cb	9.6	74.3
+4	10.4	73.6
+5	12.2	71.7
1/4	12.1	71.8
+7	12.3	71.6
1/4	11.7	72.2
+3	10.4	73.5
+5	9.9	74.0
1/4	9.7	74.2
cb	9.9	74.0
S.L.	9.9	74.0
5' S	10.3	73.6
10' S	10.1	73.8

10' S of 10' N

O+62 273.94

10'S 10.1 63.8

S.L. 10.3 63.6

+7 10.2 63.7

cb 11.3 62.6

+1 12.1 61.8

1/4 12.2 61.7

+4 12.4 61.5

⊕ 10.2 63.7

1/4 9.7 64.2

7 9.9 64.0

cb 10.2 63.7

N.L. 10.7 63.2

10'N 10.6 63.3

O+70

10'N 10.9 63.0

N.L. 10.8 63.1

+5 10.7 63.2

cb 10.8 63.1

+9 10.0 63.9

1/4 9.8 64.1

⊕ 9.7 64.2

1/4 10.2 63.7

+3 12.1 61.8

cb 12.2 61.7

S.L. 11.8 62.1

10'S 11.2 62.7

O+80 273.94

10'S 11.9 62.0

S.L. 11.9 62.0

+7 10.1 63.8

cb 10.0 63.9

1/4 9.8 64.1

⊕ 9.8 64.1

1/4 9.9 64.0

+3 10.1 63.8

+6 11.7 62.2

cb 11.6 62.3

+2 11.1 62.8

N.L. 11.0 62.9

10'N 11.1 62.8

O+87

10'N 11.2 62.7

N.L. 11.1 62.8

cb 11.5 62.4

+5 11.6 62.3

1/4 11.0 62.9

+3 10.0 63.9

⊕ 9.9 64.0

1/4 9.8 64.1

cb 9.9 64.0

S.L. 10.0 63.9

+1 S 10.5 63.4

+1 S 11.3 62.6

O+87 273.99
 10's 11.6 62.3
 1+00
 10's 10.3 63.6
 S.L. 10.2 63.7
 cb 10.4 63.5
 1/4 10.5 63.4
 Φ 10.4 63.5
 1/4 10.5 63.4
 cb 10.7 63.2
 +2 11.7 62.2
 +6 11.6 62.3
 N.L. 11.4 62.5
 10'N 11.5 62.4
 1+25
 10'N 12.2 61.7
 N.L. 11.9 62.0
 +2 11.3 62.6
 cb 11.0 62.9
 1/4 11.1 62.8
 Φ 11.2 62.7
 1/4 10.9 63.0
 cb 10.7 63.2
 S.L. 10.6 63.3
 10's 10.8 63.1

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O+50 273.99
 10's 11.5 62.4
 S.L. 11.4 62.5
 cb 11.3 62.6
 1/4 11.5 62.4
 Φ 11.5 62.4
 1/4 11.6 62.3
 cb 11.9 62.0
 N.L. 12.3 61.6
 10'N 12.6 61.3
 1+67
 10'N 12.7 61.2
 1'N 12.8 61.1
 N.L. 12.2 61.7
 cb 11.9 62.0
 1/4 12.1 61.8
 +5 11.9 62.0
 Φ 11.6 62.3
 1/4 11.9 62.0
 cb 12.1 61.8
 S.L. 12.4 61.5
 2'S 12.6 61.3
 3'S 13.9 60.0
 10'S 13.7 60.2
 13'S 12.3 61.6

1+72	273.94		
10's		12.1	61.8
6's		12.4	61.5
5's		14.6	59.3
S.L.		14.5	59.4
+5		14.3	59.6
+7		12.6	61.3 ✓
cb		12.4	61.5
1/4		12.3	61.6
⊕		12.3	61.6
1/4		12.4	61.5
cb		12.1	61.8
N.L.		12.3	61.6
4'N		12.6	61.3
10'N		12.7	61.2 =
T.P. 9.25	270.48	12.71	261.23
1+78			
10'N		9.4	61.1
5'N		9.0	61.3
N.L.		9.0	61.5
cb		9.0	61.5
1/4		9.2	61.3
⊕		9.2	61.3
1/4		9.0	61.5
+3		9.1	61.4
+4		10.7	59.8
+6		11.2	59.3

1+79	270.48		
Scb		11.3	59.2
+5		11.2	59.3
+6		9.7	60.8
S.L.		8.8	61.7
10's		8.7	61.8
1+93			
10's		9.5	61.0
S.L.		9.4	61.1
cb		9.5	61.0
1/4		9.6	60.9
+3		9.7	60.8
+4		11.7	59.8
⊕		12.1	58.9
1/4		11.6	58.9
+6		11.3	59.2
+7		9.8	60.7
cb		9.7	60.8
N.L.		7.2	61.3
10'N		9.6	60.9

2+00	27048		
10'N	9.9	60.6	
5'N	9.6	60.9	
N.L.	10.0	60.5	
+6	10.6	59.9	
cb	12.1	58.4	
1/4	11.4	59.1	
1/2	10.9	59.6	
1/4	10.0	60.5	
cb	9.7	60.8	
+2	9.5	61.0	
+3	10.4	60.1	
S.L.	11.3	59.2	
3'S	9.5	61.0	
5'S	9.0	61.5	
10'S	8.8	61.7	
2+04			
10'S	9.0	61.5	
S.L.	9.4	61.3	
+6	10.5	60.0	
cb	10.8	59.7	
+3	9.9	60.6	
1/4	10.0	60.5	
1/2	10.9	59.6	
1/4	11.3	59.2	
cb	11.9	58.6	
+4	11.4	59.1	

2+04	27048		
N.L.	10.7	59.8	
3'N	9.6	60.9	
10'N	9.7	60.8	
2+16			
10'N	9.8	60.7	
7'N	10.0	60.5	
6'N	12.2	58.2	
N.L.	12.1	58.4	
+4	12.3	58.2	
+8	10.4	60.1	
cb	10.0	60.5	
+4	9.8	60.6	
+6	10.5	60.0	
1/4	10.0	60.5	
1/2	9.6	60.9	
1/4	9.1	61.4	
cb	9.1	61.4	
S.L.	8.8	61.7	
10'S	9.2	61.3	
2+21			
10'S	9.4	61.1	
2'S	9.6	60.9	
S.L.	9.7	60.8	
cb	9.7	60.8	
1/4	9.6	60.9	

2+21 270.98

☒	9.2	61.3
+5	9.5	61.0
1/4	10.4	60.1
+3	9.7	60.8
cb	9.8	60.7
+7	10.2	60.3
N.L.	12.4	58.3
9'N	13.1	57.4
10'N	11.0	59.5
13'N	10.2	60.3

2+25

15'N	10.2	60.3
12'N	12.7	57.8
3'N	12.2	58.3
N.L.	11.3	59.2
+1	10.2	60.3
cb	9.6	60.9
+5	9.6	60.9
1/4	10.2	60.3
+5	9.4	61.1
☒	9.4	61.1
+5	9.8	60.7
1/4	9.7	60.8
cb	9.3	61.2
S.L.	8.9	61.6

2+25 270.48

10'S	8.9	61.6
2+32		
10'S	8.9	61.6
S.L.	8.8	61.7
+5	9.1	61.4
cb	9.2	61.3
1/4	9.3	61.2
☒	10.1	60.4
+3	9.7	60.8
1/4	10.2	60.3
+2	9.5	61.0
cb	9.6	60.9
+5	10.0	60.5
N.L.	9.6	60.9
2'N	9.7	60.8
5'N	10.9	59.6
6'N	11.7	58.8
8'N	12.3	58.2
15'N	12.5	58.0

2+50

10'N	10.1	60.4
5'N	10.0	60.5
N.L.	10.3	60.2
+5	10.9	59.6
cb	10.8	59.7
1/4	10.6	59.9

2+50	270.48	
w 1/4 +3	10.2	60.3
¢	9.9	60.6
1/4	10.0	60.5
cb	9.9	60.6
S.L.	9.8	60.7
10'S	9.4	61.1
2+75		
10'S	9.7	60.8
S.L.	10.3	60.2
+1	10.5	60.0
cb	10.6	59.9
1/4	10.8	59.7
¢	10.4	60.1
1/4	10.4	60.1
cb	10.4	60.1
+4	10.5	59.8
+6	11.6	58.9
N.L.	12.3	58.2
5'N	11.8	59.7
6'N	11.0	59.5
10'N	10.5	60.5

2+94	270.98	
10'N	13.5	57.0
6'N	12.7	57.8
N.L.	12.0	58.5
+2	10.8	59.7
cb	10.8	59.7
1/4	11.0	59.5
¢	10.8	59.7
1/4	10.8	59.7
cb	11.1	59.4
SL	11.0	59.5
3'S	10.4	60.1
10'S	10.0	60.5
3+00		
10'S	10.4	60.1
SL	11.0	59.5
cb	11.1	59.4
1/4	10.9	59.6
¢	10.9	59.6
1/4	11.0	59.5
cb	10.9	59.6
+5	11.0	59.5
+8	12.1	58.4
+9	14.2	56.3
N.L.	13.7	56.8
10'N	13.8	56.7

270.48
3+21¹³ = E.L. Winona on North

10' N	11.3	69.2
N.L.	12.7	67.8
+8	14.2	66.3
cb	13.8	66.7
+3	12.1	68.4
1/4	11.5	69.0
Φ	11.2	69.3
1/4	12.0	68.5
cb	11.8	68.7
S.L.	11.4	69.1
8's	11.3	69.2
10's	10.7	68.8

End Section on E.L. Winona

10's	11.4	69.1
S.L.	12.3	68.2
+7 on diag.	12.2	68.3
cb	11.2	69.3
1/4	11.5	69.0
Φ	11.3	69.2
1/4	11.2	69.3
cb	11.0	69.5
+1 on diag.	11.3	69.2
+2 "	14.0	66.5
+4 "	12.7	67.8
+8 "	11.8	68.7

10' L. High

270.48
End Section

N.L.	12.7	257.8
3+45 ²² = E.L. Winona on South		
T.P. 12.78	282.50 0.76	269.72
T.P. 12.43	294.39 0.54	281.96
T.P. 11.71	305.46 0.64	293.75
T.P. 11.62	316.78 0.30	305.16
B.M. Hub NE Winona & Wightman	2.23	314.55

X Sec. Wightman From E.L.

60' wide 10' cts.

316.78

314.6

0+00 E.L. Winona B.C. 2.2 B.C. on E.

0+34.52 rt. L.S. to Winona

E.L. Winona 6.1 310.7

2'E 6.0 310.8

5'E Int with curve 5.6 311.2

0+69.04 rt. L.S. to Winona

18.8'E Int with curve 8.2 308.6

2'E 9.1 307.7

E.L. winnong (prod.) 9.8 307.0

1+03.61 rt. L.S. to Winona

E.L. winnong (prod.) 11.1 305.7

5'E 11.2 305.6

6'E 11.6 305.2

8'E 11.4 305.4

10'E 10.4 306.4

25'E 9.8 307.0

40.8'E Int with Curve 9.5 307.3

64' in street on E. 7' wide
Conc. Drive at 1+08 9.52 307.26

1+03.61 = B.C. on E. Sec's radial from Here. to E.C. 316.78

N.L. 9.5 307.3

cb 10.3 306.5

1/4 10.9 305.9

1/2 11.9 304.9

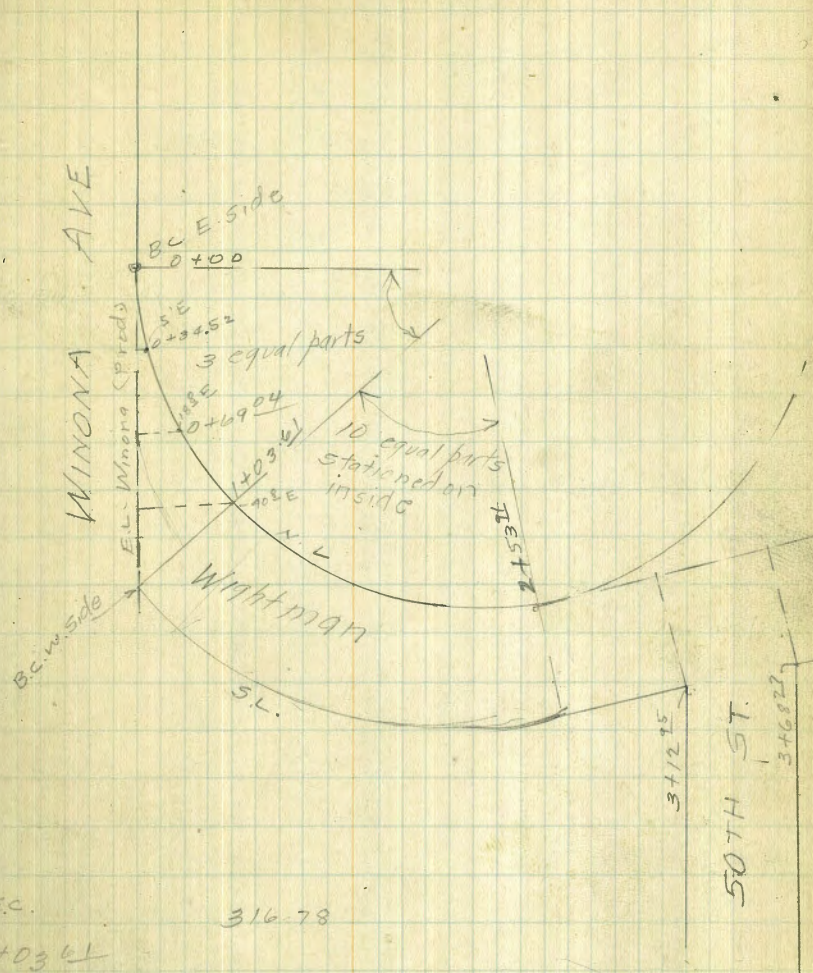
3/4 12.2 304.6

cb 12.7 304.1

+5 12.9 303.9

Winona to Altedena St.

43



1+03.61

5.L.

10'S

T.P. 4.50

12.9 | 303.9

13.4 | 303.4

12.90 | 303.88

1+18⁶² No1 308.38

10's	5.8	302.6
S.L.	4.9	303.5
+7	3.9	304.5
cb	3.8	304.6
1/4	4.0	304.4
+8	4.2	304.2
ϕ	4.3	304.1
+1	4.0	304.4
+4	2.6	305.8
1/4	2.3	306.1
+4	2.2	306.4
cb	1.7	306.7
N.L.	1.0	307.4

1+33⁶² No2

N.L.	1.5	306.9
cb	2.2	306.2
+6	2.5	305.9
1/4	2.8	305.6
+8	3.2	305.2
ϕ	5.7	302.7
+5	5.2	303.2
1/4	4.9	303.5
+4	4.7	303.7
+8	4.4	304.0
cb	4.3	304.1
+5	4.4	304.0

1+33⁶² 308.38

S.L.	5.1	303.3
10's	6.0	302.4

1+48²⁰ No3

10's	8.0	300.4
S.L.	7.1	301.3
+7	6.2	302.2
cb	5.9	302.5
+1	5.9	302.5
1/4	6.7	301.7
ϕ	7.3	301.1
+1	7.1	301.3
+3	4.3	304.1
1/4	3.8	304.6
cb	3.1	305.3
N.L.	2.4	306.0

1+63²³ No4

N.L.	3.7	304.7
cb	4.0	304.4
1/4	5.1	303.3
+7	6.0	302.4
+8	8.7	299.7
ϕ	8.9	299.5
1/4	8.5	299.9
+5	8.4	300.0
+8	8.1	300.3
cb	8.4	300.0

176329

308.38

S.L. 9.2 ✓ 299.2

10's 10.2 298.2

177826 no 5

10's 13.5 299.9

S.L. 12.6 295.8

+9 11.4 297.0

cb 10.9 297.5

+2 10.6 297.8

1/4 11.1 297.3

+5 11.0 297.4

E 11.0 297.4

+4 10.6 297.8

+5 8.6 299.8

+8 7.4 301.0

1/4 7.1 301.8

cb 6.3 302.1

+5 6.2 302.2

N.L. 5.5 302.9

179329 no 6

N.L. 5.7 302.7

+4 7.4 301.6

cb 7.8 300.6

1/4 9.0 299.4

+4 10.0 298.4

+8 12.9 295.5

45

179328

308.38

E 13.1 295.3

+7 12.8 295.6

1/4 12.8 295.6

+8 12.4 296.0

cb 13.0 295.4

S.L. 14.7 293.7

10's 16.5 291.9

15's 17.4 291.0

T.P. 5.74 301.39 12.73 295.65

270872 no 7

15's 13.6 287.8

S.L. 10.3 291.1

+7 8.7 292.7

cb 7.7 293.7

+1 7.2 294.2

1/4 7.5 293.9

+6 7.4 294.0

E 7.4 294.0

+4 7.5 293.9

+6 4.9 296.5

1/4 4.3 297.1

cb 3.0 298.4

+5 2.0 299.4

N.L. 1.9 299.5

2+2325 768

301.39

N.L.	2.9	298.5
cb	3.3	298.1
1/4	5.0	296.4
+5	6.0	295.4
+7	8.9	292.5
¢	9.0	292.4
+8	9.3	292.1
1/4	9.4	292.2
+6	9.0	292.4
cb	10.4	291.0
+5	12.7	288.7
S.L.	14.3	287.1
15's	17.6	283.8
2+3828 109		
15's	18.7	282.7
S.L.	17.3	284.1
+4	16.3	285.1
cb	12.9	288.5
+4	11.0	290.4
1/4	11.1	290.3
¢	11.2	290.2
+3	11.3	290.1
+6	8.4	293.0
1/4	7.6	293.8
cb	5.7	295.7
N.L.	3.9	297.5

2+53 91 = EC on S

301.39

N.L.	5.1	296.3
cb	7.5	293.9
1/4	9.7	291.7
+6	11.2	290.2
+7	12.8	288.6
¢	12.9	288.5
1/4	13.0	288.4
+7	12.9	288.5
cb	13.7	287.7
+7	17.1	284.3
S.L.	17.8	283.6
15's	19.3	282.1
2+80		
15's	19.9	281.5
S.L.	18.1	283.3
+5	17.4	284.0
cb	15.1	286.3
+7	14.7	286.7
1/4	14.9	286.5
¢	14.5	286.9
+8	11.6	289.8
1/4	11.0	290.4
cb	8.5	292.9
N.L.	4.3	295.1

Yardage figured from Head

To Sta. 41+46.79

301.39

$$\begin{array}{r} 2.5 \\ 2.2 \\ \hline 10.3 \end{array}$$

$$\begin{array}{r} 8.3 \\ 2.8 \\ \hline 5.5 \end{array}$$
3+12⁹⁵ = W.L. 50th

N.L.	7.4	296.0
Lb	9.2	292.2
1/4	12.1	289.3
+6	13.5	287.9
+8	15.4	286.0
⊕	15.4	286.0
1/4	15.9	285.5
cb	16.3	285.1
+5	17.7	283.7
S.L.	18.7	282.7
15'S	20.6	280.8
T.P.	3.17	292.97
BM.	9.99	282.98 (293.00)

3+12⁹⁵ = W.L. 50th

N.L.	+11.0	294.0 ✓
cb	1.0	292.0
1/4	3.5	289.5
+4	4.4	288.6
+6	5.1	287.9
+8	7.1	285.9
⊕	7.1	285.9
1/4	7.6	285.4
cb	8.0	285.0
+5	9.2	283.8
S.L.	10.2	282.8
15'S	12.4	280.6

3+40. 292.97

15'S	12.6	280.4
S.L.	11.0	282.0
cb	9.0	284.0
+2	8.5	284.5
1/4	8.1	284.9
⊕	7.7	285.3
+2	7.7	285.3
+5	5.6	287.4
1/4	4.3	288.7
cb	2.0	291.0
+5	1.0	292.0
N.L.	+0.5	292.5

3+55

N.L.	1.1	291.9
cb	3.2	289.8
1/4	5.2	287.8
+8	7.0	286.0
+9	8.0	285.0
⊕	8.0	285.0
1/4	8.7	284.3
+7	8.7	284.3
1/4	9.1	283.9
S.L.	10.0	283.0
10'S	11.8	281.2
15'S	13.3	279.7

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3+63

S.L.	9.9	283.1
cb	9.0	284.0
+3	8.9	284.1
1/4	8.9	284.1
+9	8.2	284.8
ϕ	7.8	285.2
+5	7.5	285.5
+7	6.2	286.8
1/4	5.6	287.4
cb	3.9	289.1
N.L.	2.1	290.9

3+68²² = EL 50th

N.L.	2.5	290.5
cb	4.5	288.5
+2	5.5	289.5
1/4	6.6	286.4
+8	8.0	285.0
ϕ	8.4	284.6
1/4	9.1	283.9
cb	9.0	284.0
+4	9.6	283.4
S.L.	11.0	282.0

292.00
292.97

48

3+73

S.L.	13.0	280.0
+5	11.2	281.8
+8	9.5	283.5
cb	9.0	284.0
1/4	9.2	283.8
+6	9.0	284.0
ϕ	8.6	284.4
1/4	7.0	286.0
cb	5.4	287.6
+8	4.2	288.8
N.L.	2.9	290.1

3+82

N.L.	4.2	288.8
cb	5.4	287.6
1/4	7.1	285.9
+5	8.5	284.5
ϕ	9.4	283.6
1/4	9.6	283.4
+6	9.2	283.8
+9	9.3	283.7
cb	9.6	283.4
+5	11.1	281.9
S.L.	13.2	279.8
15's	17.6	275.4

292.00

3 + 89

15'S	18.5	274.5
S.L.	14.6	278.4
+8	10.6	282.4
cb	10.1	282.9
1/4	10.1	282.9
¢	10.2	282.8
+6	10.0	283.0
+8	6.8	286.2
1/4	6.4	286.6
+3	4.2	288.8
cb	3.5	289.5
+6	4.2	288.8
N.L.	4.1	288.9

4 + 02

N.L.	1.5	291.5
+6	2.0	291.0
+8	2.7	291.3
cb	3.4	289.6
+6	5.3	287.7
1/4	6.3	286.7
+5	7.8	285.2
+6	11.3	281.7
+7	11.3	281.7
¢	10.9	282.1
+5	10.8	282.2
1/4	11.2	281.8

292.00

49

H + 02

5/4 + 8	10.8	282.2
cb	11.3	281.7
+4	11.8	282.2
S.L.	16.9	276.1
15'S	21.1	271.9
4 + 10		
15'S	22.1	270.9
S.L.	18.2	274.8
+8	12.3	280.7
cb	11.8	281.2
+4	11.2	281.8
+8	11.5	281.5
1/4	11.8	281.2
¢	11.4	281.6
+4	11.8	281.2
+5	8.2	284.8
1/4	6.8	286.2
cb	5.0	288.0
+3	4.0	289.0
N.L.	3.3	289.7

292.97

299.80

U R Stationed on inside 10 parts
 4+96 $\frac{1}{2}$ = B.C. = E.C. N.E. return

N.L.	7.7	285.3	\checkmark 3/11/21
cb	9.1	283.9	
$\frac{1}{4}$	10.5	282.5	
+6	11.7	281.3	
+8	14.9	278.1	
$\frac{1}{2}$	14.9	278.0	
$\frac{1}{4}$	15.4	277.6	
+7	15.1	277.9	
cb	17.9	275.1	
S.L.	21.7	271.3	
15'S	22.8	270.2	
T.P. 5.86	286.01	12.82	280.15
4+92 ²⁶	11.01		
15'S	16.5	269.5	
S.L.	14.9	271.1	
+5	13.9	272.1	
cb	11.7	274.3	
+2	10.8	275.2	
$\frac{1}{4}$	11.1	274.9	
+8	10.4	275.6	
$\frac{1}{2}$	10.4	275.6	
+2	10.3	275.7	
+4	6.0	280.0	
$\frac{1}{4}$	4.9	281.1	
cb	4.0	282.0	
N.L.	3.4	282.6	

50

4+84⁸ 286.01

N.L.	5.5	280.5	
cb	5.2	280.8	
+5	5.7	280.3	
$\frac{1}{4}$	6.4	279.6	
+6	8.0	278.0	
+8	12.0	274.0	
$\frac{1}{2}$	12.0	274.0	
$\frac{1}{4}$	12.5	273.5	
+7	12.3	273.7	
cb	13.6	272.4	
S.L.	15.5	270.5	
15'S	16.6	269.4	
Nail in Pole			
T.P. 2.33	275.55	12.79	273.22
4+97 ²³	11.01		
15'S	6.8		
S.L.	6.0	269.6	
+8	5.3		
cb	3.9		
+1	3.4		
$\frac{1}{4}$	3.4		
$\frac{1}{2}$	3.5	272.1	
+3	3.8		
+7	3.8		
$\frac{1}{4}$	4.4		
cb	4.4		
N.L.	3.7	271.9	

J.P	5.27	278.49	273.22
5+2320	103		
NL		7.7	270.8
+3		7.7	
+8		8.6	
+9		9.4	
cb		9.3	
+1		8.6	
4		7.8	
4		7.7	270.8
1/4		8.1	
+2		8.8	
+3		8.0	
+7		8.6	
cb		8.6	
3.L		9.0	269.5
9's		9.2	
13's		12.2	
5+2970			
10's		12.1	
5's		11.9	
3's		9.9	
3.L		9.5	269.0
cb		8.9	
+1		8.9	
+4		11.5	

5+2920	278.49
+9	11.3
1/4	10.9
+4	7.9
4	7.9
1/4	7.6
+7	8.2
cb	9.0
+6	10.4
+8	9.6
NL	9.4
5'N	9.7
10'N	10.4
5+3220	
10'N	10.6
NL	10.9
cb	10.8
+2	10.7
+3	8.3
+8	7.8
1/4	7.8
cb	7.8
+4	7.9
1/4	11.5
+4	11.8
cb	11.8
+1	9.1

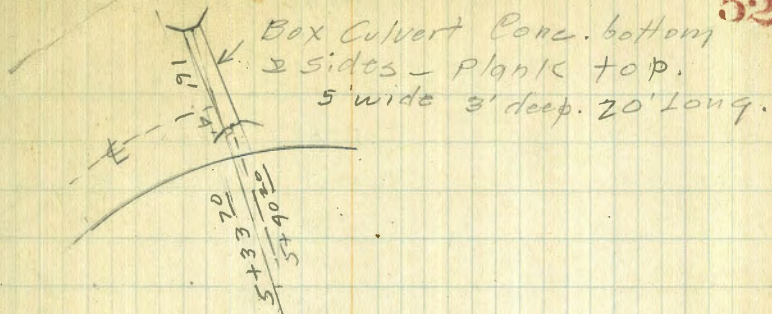
270.7

269.1

267.6

278.49

5+3270		
S.L.	9.5	269.0
2'S	11.9	
10'S	12.2	
5+3420		
10'S	12.0	
S.L.	12.1	266.5
cb	11.6	
1/4	12.0	
+5	8.1	
±	7.9	270.6
1/4	7.9	
+5 top head culvert	7.9	
+5 bottom head culvert	11.2	
cb	11.1	
N.L.	10.7	267.8
10'N	10.5	
5+4120		
10'N	8.1	
N.L.	8.3	270.2
+1	8.5	
+3	9.5	
+6	9.7	
cb	8.1	
+6	7.9	
1/4	7.9	
±	8.0	270.5



52

±4 top culvert s. end.	8.0	
+4 bottom culvert s. end.	12.0	
1/4	12.5	
cb	11.9	
S.L.	12.3	266.2
7'S	12.3	
10'S	10.7	
5+4867		
10'S	8.9	
S.L.	9.6	268.9
cb	10.0	
+5	11.3	
1/4	11.6	
+6	8.3	
±	8.0	270.5
1/4	7.9	
+9	8.3	
cb	8.8	
+2	9.2	
+3	8.3	

278.49

5+4862

N.C.B +7

8.1

N.L.

8.7

269.8

10'N

8.8

5+74¹⁴ Nos

10'N

7.9

N.L.

7.9

270.6

+5

7.9

C.B.

7.5

+1

8.5

+3

8.6

+5

7.8

1/4

8.4

Φ

8.4

270.3

1/4

8.3

+4

8.7

+5

9.3

+6

9.3

+7

8.4

C.B.

8.3

S.L.

8.2

270.3

10'S

8.9

278.49

53

5+996L No6

10'S

6.7

S.L.

7.3

271.2

+7

7.6

C.B.

7.0

+2

7.1

+4

7.4

1/4

6.8

+3

7.2

+6

7.1

Φ

6.7

271.8

+3

6.5

1/4

6.8

+3

7.0

+6

6.4

+9

7.5

C.B.

7.1

+1

6.2

+7

6.3

+9

7.1

N.L.

7.3

271.2

10'N

7.2

278.49

6+2408 No7

10'N	5.3	
N.L.	5.1	273.4
+8	5.0	
cb	5.3	
+2	5.6	
+5	5.6	
1/4	4.9	
+4	4.9	
↓	5.4	273.1
+5	5.8	
1/4	5.6	
+8	6.1	
cb	5.8	
+2	5.8	
+5	5.5	
S.L.	5.4	273.1
10'S	5.4	
6+5055 No6		
10'S	3.8	
S.L.	3.7	274.8
+8	3.5	
cb	4.0	
+1	5.0	
+3	4.6	
+8	4.1	
1/4	4.1	

54

+6	4.1	
↓	3.7	274.6
+7	3.4	
1/4	3.5	
+5	3.4	
+6	4.4	
+8	4.5	
cb	3.7	
+3	3.4	
N.L.	4.6	273.9
10'N	4.9	
6+7602 No9		
10'N	3.6	
N.L.	3.3	275.2
cb	2.8	
+3	3.8	
+5	3.2	
+7	2.0	
1/4	1.8	
+5	2.1	
↓	2.6	275.9
+2	2.7	
1/4	2.8	
+3	1.7	
+5	3.1	

6+76⁰² 278.49
 S.C.B 3.3
 +2 3.1
 +3 1.8
 S.L. 1.9 276.6

T.P. 12.73 290.00 1.22 277.27

7+01⁵⁴ E.C. No 10
 S.L. 11.9 278.1

cb. 12.2
 +1 12.1
 +3 13.4
 +7 13.3
 +8 12.9
 1/4 12.9
 +5 12.7

1/2 12.4 277.6

1/4 11.4
 +4 11.9
 +5 14.1
 +7 14.1
 +8 12.8
 cb 12.9
 +4 13.6

N.L. 13.5 276.5

10'N 13.3

7+06 290.00

10'N 11.7

N.L. 12.2 277.8

cb 12.1

+2 12.2

+3 14.0

+6 13.9

+7 12.0

1/4 11.1

1/2 12.3 277.7

+4 12.5

1/4 12.6

+1 12.6

+3 12.9

+7 13.1

cb 11.8

S.L. 11.5 278.5

7+28

S.L. 8.9 281.1

cb 10.4

+3 11.0

+5 12.0

1/4 11.5

+5 11.5

1/2 11.0 279.0

1/4 10.0

+5 10.1

290.00

7+28		
+5	12.7	
+8	12.7	
+9	10.1	
cb	10.3	
N.L.	10.5	279.5
7+56		
N.L.	8.8	281.2
cb	9.0	
+1	11.0	
+4	11.3	
+5	8.9	
+7	8.4	
1/4	9.0	
+5	9.5	
⊕	9.8	280.2
1/4	10.2	
+3	10.8	
cb	7.5	
S.L.	5.2	284.8

290.00

56

7+78		
S.L.	1.0	289.0
cb	3.6	
+5	5.6	
+8	9.6	
1/4	9.2	
+3	8.4	
⊕	8.4	281.6
+5	8.6	
1/4	8.2	
+5	7.7	
+8	8.3	
cb	7.7	
+5	7.7	
N.L.	7.5	282.5
8+00		
N.L.	7.3	282.7
+3	7.6	
cb	7.0	
+5	7.0	
1/4	7.5	
+4	7.5	
⊕	7.4	282.6
+5	7.6	
+9	8.4	
1/4	7.4	

290.00

8+00

5'A+2	5.3	
+7	2.2	
cb	1.1	
s.l.	+3.2	293.2
6+25		
s.l.	+4.2	294.2
cb	0.3	
+4	2.2	
+8	6.7	
1/4	6.4	
+4	6.6	
⊕	6.7	283.3
+2	6.2	
+6	6.6	
1/4	6.6	
+3	6.4	
+5	5.9	
+7	6.3	
cb	6.1	
+7	6.2	
N.L.	6.9	289.1

290.00 5.1

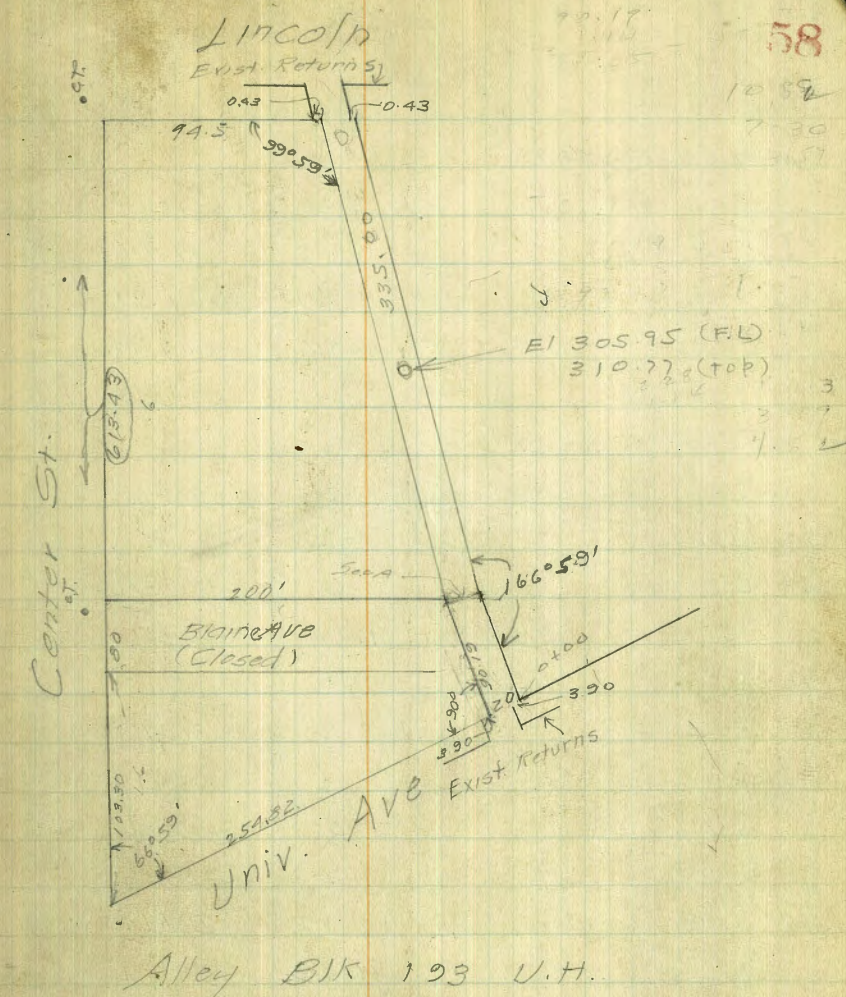
57

8+50

N.L.	5.3	284.7
+4	4.4	
cb	4.6	
+5	4.5	
+8	5.3	
1/4	5.6	
+6	5.3	
⊕	5.3	284.7
1/4	5.5	
+2	6.3	
+7	1.9	
cb	1.0	
s.l.	+2.7	292.7
8+75		
s.l.	+0.6	290.6
cb	1.6	
+1	1.9	
+4	4.4	
1/4	4.2	
⊕	3.8	286.2
+3	3.9	
1/4	3.9	
cb	3.4	
N.L.	3.1	286.9

290.00

8 + 94 ¹⁶	= N.L. Altadena	
N.L.	2.6	287.4
CB	3.3	
+3	3.7	
+6	2.6	
4	3.1	
+3	3.2	
4	3.1	286.9
4	3.2	
+9	3.5	
CB	2.9	
+2	1.9	
S.L.	1.0	289.0
B.M.	Nail Pole N.E.	
B.M.	Wrightman & Altadena	1.76 288.24
T.P.	4.49 285.52	12.97 277.03
B.M.	pipe SW. Wrightman 50th	2.49 283.03
W.	5.2	
E	5.2	
+	5.0	
F.C.	2.3	
M.H.	12.12	
M.H.	4.02	



188.25

Xsec. Alloy Bldg. 193 Univ. Hqs
20' wide As per sketch on P. 50.

B.M. 10.47 314.35 303.88 ^{SP NW} Center Univ.

Nobline Univ.

top Ech 3.90 310.45

E.L. gut 4.59 309.74

± gut 4.59 309.74

w.l. gut 4.90 309.45

top web 4.06 310.29

0+00 = N.L. Univ. Ave.

w.l. 3.68 310.67

± 3.75 310.60

E.L. 3.6 310.8

T.P. 5.42 308.26 11.51 302.84

0+11

w.l. 5.2 303.1

± 5.2 303.1

+7 5.0 303.2

E.L. 5.3 303.0

M.H. at 0+14 1' W. FL. 12.12 296.14 X

top M.H. 4.82 303.44 X

0+20

10'E 7.4 300.9

3'E 7.4 300.9

E.L. 6.1 302.2

+3 5.6 302.7

+4 7.4 300.9

± 7.4 300.9

Jun 26-28

London

Zobell

Neigan.

0+20 308.26

± +L 8.0 300.3

w.l. 8.0 300.3

0+28

12' W door bldg 8.35 299.91 X

10' W 8.5 299.8

8' W 8.8 299.5

7' W 9.0 300.3

4' W 7.1 301.2

w.l. 6.3 302.0

+4 5.6 302.7

± 5.4 302.9

+5 5.5 302.8

E.L. 6.4 301.9

3'E 7.1 301.2

10'E 7.5 300.8

0+38

10'E 7.0 301.3

6'E 6.8 301.5

E.L. 6.3 302.0

+1 5.2 303.1

+5 5.4 302.9

± 4.7 303.6

+8 4.2 304.1

w.l. 4.4 303.9

3' W 5.2 303.1

8' W 7.5 300.8

Garage Figure 7.6H
Checked garages 6-27-28
G.B.H.

308.26

0+38		
10' W	8.0	300.3
0+56		
10' W	8.5	299.8
7' W	7.8	300.5
W.L.	4.9	303.4
+3	4.4	303.9
⊕	4.8	303.5
+4	4.7	303.6
+7	5.3	303.0
E.L.	5.8	302.5
5' E	6.6	301.7
10' E	7.5	300.8
0+65		
10' E	7.8	300.5
7' E	6.9	301.4
E.L.	6.3	302.0
+5	5.2	303.1
⊕	5.0	303.3
W.L.	5.4	302.9
8' W	8.1	300.2
10' W	8.3	300.0

308.26

50

0+87² = L on E

10' W	8.6	299.7
4' W	8.1	300.2
W.L.	6.3	302.0
+3	6.1	302.2
+5	5.2	303.1
⊕	5.2	303.1
+9	4.6	302.7
E.L.	5.3	303.0
2' E	6.4	301.9
8' E	6.8	301.5
10' E	7.3	301.0
0+90 ¹⁶ = 6 on W Sec A		
E.L.	5.3	303.0
+1	4.8	303.5
⊕	5.1	303.2
+7	5.3	303.0
W.L.	7.0	301.3
0+92 ⁴² = c on E		
W.L.	7.1	301.2
+2	6.3	302.0
+5	5.2	303.1
⊕	5.1	303.2
+7	4.7	303.6
E.L.	5.3	303.0

1+20	308.26		
5'E	5.5	3028	
3'E	4.9	3034	
E.L.	4.7	303.6	
⊕	4.2	304.1	
+4	4.2	304.1	
+9	5.5	3028	
W.L.	5.8	302.5	
5'W	6.5	3018	
1+34			
5'W	5.6	3027	
W.L.	4.9	3034	
+2	4.6	3037	
+6	3.1	3052	
⊕	3.6	3047	
+1	4.0	3043	
E.L.	3.7	304.6	
5'E	4.4	3039	
1+44			
5'E	4.3	3040	
E.L.	3.9	3044	
+9	3.7	3046	
⊕	3.2	3051	
+2	3.2	3051	
+6	4.1	3042	
W.L.	4.3	304.0	
5'W	4.7	303.6	

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1+60	308.26		
5'W	4.0	304.2	
W.L.	3.7	304.6	
+7	3.2	3051	
⊕	3.5	304.8	
+3	3.8	304.5	
E.L.	4.0	304.3	
1+73			
E.L.	3.1	305.2	
+4	2.8	305.5	
⊕	2.8	305.5	
+3	2.8	305.5	
W.L.	3.1	305.2	
1+85 = ⊕	Single garage on W.L. earth floor		
	2.7	305.6	
2+00			
W.L.	2.1	306.2	
⊕	1.7	306.6	
+7	2.2	306.1	
E.L.	2.2	306.1	
TP 10.20	318.80	1.66	308.60

316.80

2+14 = send 6 car garage 0.2'E earth floor X
 8.7 308.1

2+48 = Φ same garage on E.L.
 8.6 308.2

2+87 = N end same garage 0.2' in Alley X
 7.2 309.6

2+41 = send 4 car garage 0.2' W earth floor X
 9.2 307.6

2+81 = N end same garage 0.2' in Alley X
 8.2 308.6

2+30

E.L. 9.0 307.8
 Φ 9.4 307.4
 +7 9.8 307.0
 W.L. 9.7 307.1

2+65

W.L. 8.7 308.1
 +3 8.6 308.2
 Φ 9.2 309.6
 +3 8.1 309.7
 E.L. 7.7 309.1

3+00

E.L. 6.1 310.7
 +5 6.6 310.2
 Φ 6.8 310.0

3+00

316.80

Φ +5 7.1
 W.L. 7.1 309.7
 (2+87 = send 2 car garage on W.L. X
 7.07 309.73 X
 3+15 = N end same garage 0.4' W X
 7.01 309.79 X
 (3+11 = send 4 car garage 2'E earth floor X
 5.6 311.2 X
 3+55 = N end same garage 75 E X
 5.1 311.7 X
 3+35 = fence 0.7' in Alley on W X

W.L. 6.3 310.5
 +1 5.9 310.9
 +9 6.2 310.6
 Φ 5.9 310.9
 +6 5.9 310.9
 E.L. 5.6 311.2

3+56 = fence 1.6' in alley on W X

E.L. 5.3 311.5
 +5 5.3 311.5
 Φ 5.0 311.8
 +5 5.0 311.8
 +8 4.7 312.1
 W.L. 5.9 310.9

316.80
 3+66 Fence 2.8' in Alley on W. *
 W.L. 5.7 311.1
 +2 4.3 312.5
 +3 4.4 312.4
 +4 4.6 312.2
 ♀ 4.7 312.1
 +5 4.7 311.9
 E.L. 5.0 311.8

3+74
 E.L. 4.7 312.1
 +5 4.7 312.1
 ♀ 4.4 312.4
 +6 4.3 312.5
 +9 3.3 313.5
 W.L. 3.3 313.5

4+00
 W.L. 3.1 313.7
 ♀ 3.7 313.1
 +5 3.9 312.9
 E.L. 3.9 312.9

4+06 = ♀ Single garage 5' E earth floor *
 3.6 313.2

4+15 = ♀ Single garage 1.1' W earth floor *
 3.1 313.7

316.80

4+18 = S end 2 car garage 13.6' E earth floor *
 2.5 314.3
 4+35 N end same garage 16' E *
 2.3 314.5
 4+35 = S end 2 car garage 16' E *
 1.4 315.4
 4+50 = N end same garage 20' E *
 1.3 315.5
 4+50 = ♀ Single garage 8' W Porch floor *
 2.73 314.07

4+25
 E.L. 3.2 313.6
 +5 3.3 313.5
 ♀ 3.2 313.6
 +5 3.1 313.7
 W.L. 2.9 313.9

4+50
 W.L. 2.3 314.5
 +5 2.5 314.7
 ♀ 2.4 314.7
 +5 2.4 314.4
 E.L. 2.1 314.7

4+80 316.80
 E.L. 0.9 315.9
 +5 1.0 315.8
 6 0.9 315.9
 +6 1.3 315.5
 w.L. 0.8 316.0

4+78 = S end 2 car garage 2.5 W earth floor
 0.6 316.2

4+95 = N end Same garage 2.6 W
 0.5 316.3

4+82 = 1/2 Single garage 2' E earth floor
 0.8 316.0

T.P. 12.59 328.75 0.64 316.16

5+30
 w.L. 11.4 317.3
 +4 11.6 317.2
 +5 11.5 317.3
 6 11.4 317.4
 +5 11.6 317.2
 E.L. 11.3 317.4

5+35 = 1/2 Single garage 3' E. Pone floor
 10.91 317.84

5+44
 w.L. 10.7 318.1
 +5 11.0 317.8
 6 11.0 317.8

5+44 328.75
 4+5 11.2
 E.L. 10.6 318.2
 5+47 = S end 2 car garage 0.2' W earth floor
 9.7 319.1
 5+73 = N end Same garage 0.2' W Pone floor
 9.46 319.29

5+48
 E.L. 10.3 318.5
 +5 10.9 317.9
 6 10.8 318.0
 +6 10.8 318.0
 w.L. 9.7 319.1

5+66 = 1/2 Single garage 5' E earth floor
 8.7 320.1

5+86
 w.L. 8.8 320.0
 +5 9.1 319.7
 6 8.9 319.9
 +5 8.9 319.9
 E.L. 7.9 320.9

6+00
 E.L. 6.8 322.0
 +6 7.3 321.5
 6 7.4 321.9
 +7 7.8 321.0
 w.L. 7.5 321.3

328.75

6+20		
w.L.	6.4	322.4
+6	6.4	322.4
±	6.3	322.5
+6	5.9	322.9
+7	5.5	322.3
E.L.	5.6	323.2

{ 6+25 = S end 1 car garage on E.L. Conc floor. 6+94⁵ = S.L. Lincoln on E.

4.38 324.37 X

{ 6+44 = Head same garage on E. X

4.22 324.53

6+40

E.L.	4.4	324.4
+5	4.5	324.3
±	5.2	323.6
+8	5.6	323.2
w.L.	5.9	322.9

6+48

w.L.	5.2	323.6
±	4.7	324.1
+3	4.1	324.7
+6	3.9	324.9
E.L.	3.9	324.9

M.H. at 6+75 as Foot ± (F.L.) 9.62 319.13 X

top of M.H. 2.27 326.48 X

328.75

65

6+75	328.75	
E.L.	1.1	327.7
+6	2.0	326.8
±	2.4	326.4
+2	3.0	325.8
+5	3.1	325.7
w.L.	3.1	325.7

w.L.	1.1	327.7
+5	0.9	327.9
±	1.0	327.8
+5	0.7	329.1
E.L.	0.3	328.5

End Section on S.L. Lincoln.

top E cb	0.13	328.62
E.L. Pav	0.45	328.30
± Pav	0.90	327.85
w.L. pav	0.63	328.12
top w cb	0.57	328.18
S cb line Lincoln.		
top e b w ret	0.82	327.93
gut at w.L.	1.30	
gut at ±	1.16	
gut at E.L.	0.91	
top cb E ret	0.46	328.29

~~332.75~~~~T.P. 1.45 325.00 9.20 323.55~~~~T.P. 1.57 313.54 13.03 311.97~~~~T.P. 5.16 313.26 5.44 308.10~~~~B.M. 5.40 307.66~~

TOP MH 0.96 327.44 326.48

T.P. 1.44 317.32 11.46 315.98

MH 335⁰⁰ South

TOP 6.55 310.77

F.L. 11.37 305.95

Profile for Storm Drain
at end 35th St.

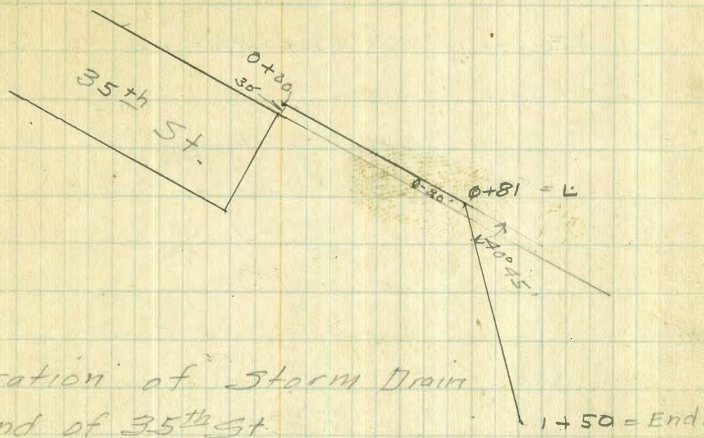
B.M.	2.16	
0+00		5.1
0+06		7.2
0+15		12.9
T.P.	0.50	12.81
0+23		4.8
0+33		7.8
0+49		13.1
0+66		19.3
0+81 = L		22.7
0+96		26.6
1+09		30.3
1+17		32.6
1+23		34.5
1+35		37.3
1+38		39.5
1+41		40.6
1+42		39.7
1+47		40.2
1+47 $\frac{1}{2}$		42.7
1+48 $\frac{1}{2}$		42.9
1+49		44.7
1+50		45.0

Jun 26-28

London
Fahll
Max 9.17.

B.P. SE 35th St

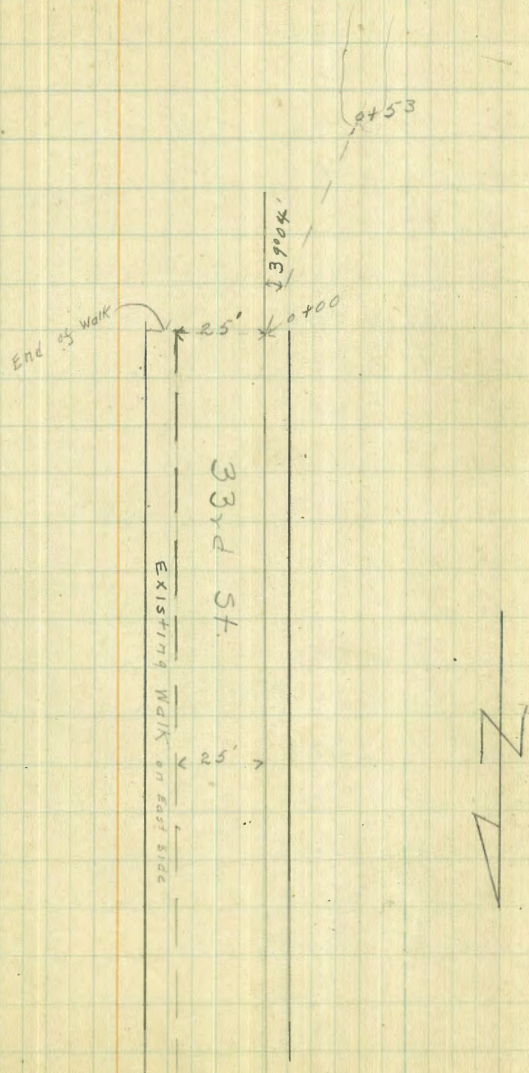
37



8-2-28
 30.8155
 Flood
 Rooney

Levels for culvert at 33rd + Hawthorne

Sta	+	Red	-
B.M. B.P. N.E. corner walk 33rd + Hawthorn			257.84
	+2.65		
		Σ 260.49	
0+00 ^{sec sketch}		4.7	255.6
+11		10.2	250.3
T.P.			-12.85 247.64
	+0.47		
		Σ 248.11	
0+20		4.7	243.7
0+30		11.0	237.1
T.P.			-12.57 235.54
	+12.3		
		Σ 236.77	
0+43		6.9	229.9
0+52		15.1	219.7
0+53: bottom of ravine		19.4	217.4
T.P.			-0.35 236.42
	+12.86	249.28	
			-0.80 248.48
	+10.95	259.43	
			-1.61 257.82
B.M. N.E.B.P. 33rd + Hawthorne			257.84



Profile of Alley between Santa Cruz
 & Coronado from 50'E of Santa Barbara to
 300' W of Froude.

P.M.	11.00	<u>251.17</u>		240.17
0+00			6.0	2550 245.2
0+10			5.5	2555 245.7
0+20			4.3	2567 246.9
0+35			3.7	2571 247.3
0+48			4.1	2569 247.1
0+50 = EL. Santa Barbara			4.3	2567 246.9
0+60			5.8	2552 245.4
0+70			5.1	2559 246.1
+ 80 = E Santa Barbara			4.9	2561 246.3
+ 90			4.9	2561 246.3
+ 97			5.4	2556 245.8
1+00			5.3	2557 245.9
+ 20			3.0	2580 248.2
+ 30			2.5	2585 248.7
+ 50			0.0	2610 251.2
TP	4.80	255.80	0.17	251.00
		265.63		260.83
4+75			4.0	2616 251.8
2+00			3.5	2621 252.3
2+25			3.3	2623 252.5
2+50			3.6	2620 252.2
2+75			4.0	2616 251.8
3+00			5.0	2606 250.8
3+25			6.2	2594 249.6
+ 50			7.7	2577 248.1
+ 75			9.2	2564 246.6

Aug. 25-28
 Louisa
 Moran
 Isbell.

		255.80		
		265.63		
3+85			9.7	246.1 255.9
4+00			9.6	246.2 256.0
4+25			11.2	244.6 254.4
4+50			12.9	242.9 252.7
4+75			14.7	241.1 250.9
TR 10.25	243.04	252.87	13.01	242.79
				252.62
5+00			3.8	239.2 249.1
5+25			5.4	237.6 247.5
5+50			6.9	236.1 246.0
5+75			8.1	234.9 244.8
6+00			9.8	233.2 243.1
6+25			11.3	231.7 241.6
6+50			12.9	230.1 240.0
TR 1.65	232.00	241.83	12.69	230.35
				240.18
6+75			3.4	228.6 238.4
7+10 = EL. Guizot			5.7	226.3 236.1
7+21			5.8	226.2 236.0
7+45			7.3	224.7 234.5
7+2.6			8.5	223.5 233.3
7+29.			15.4	216.6 226.4
7+33			15.7	216.8 226.6
7+36			12.3	219.7 227.5
7+40 = E Guizot			12.4	219.6 227.4
7+49.			12.8	219.2 227.0
7+52			8.8	223.2 233.0

all of 101

232.00

~~241.92~~

7+60		8.5	233.3	223.5
7+70 = mL Guizot.		9.0	232.8	223.0
8+00		10.7	231.1	221.3
8+25		12.0	229.8	220.0
T.P.	1.17	12.88	228.75	219.12
				220.29
8+55		1.6	228.5	218.7
8+75		2.5	227.6	217.8
9+00		3.4	226.7	216.9
9+10		3.6	226.5	216.7
9+25		4.3	225.8	216.0
9+50		4.9	225.2	215.4
9+75		5.4	224.7	214.9
10+00		6.1	224.0	214.2
10+25		6.5	223.5	213.8
10+50		7.0	223.1	213.3
10+75		8.0	222.1	212.3
11+00		9.4	220.7	210.9
11+25		11.3	219.8	209.0
11+42		13.2	216.9	207.1
T.P.	0.04	12.26	217.26	207.53
				207.57
11+53		11.3	215.6	205.8
11+57		8.5	208.9	199.1
T.P.	0.28	12.59	207.81	194.98
				195.26
11+59		3.4	204.6	191.9
11+64		3.9	201.2	191.4

195.26

~~205.09~~

11+75		11.0	184.3	194.1
11+93		14.1	181.2	191.0
11+94		15.4	179.9	189.7
12+00		16.3	179.0	188.8
12+37		19.2	175.5	185.3
12+60		20.8	174.5	184.3
12+85		15.5	179.8	189.6
12+90		15.7	179.6	189.4
13+00		18.1	177.2	187.0
13+49		17.7	177.6	187.4
13+30		16.3	179.0	188.8
13+37		16.4	178.9	188.7
13+50		18.8	176.5	186.3
13+58		18.9	176.4	186.2
13+70 = EL Froude.		15.9	179.4	189.2
13+75		14.5	180.8	190.6
	1.07			185.39
B.M. 35 Alley H. 6		9.87		195.26
13+95		11.1	175.4	194.0
14+10		12.6	173.9	192.5
				175.02
T.P. 1.35		12.79		184.85
				173.67
14+20		5.6	169.4	179.30
100.00 at 14+20		14.4	160.6	170.5
14+30 = mL Froude		6.5	168.5	178.4
14+53		9.0	166.0	175.9
14+65		9.3	165.7	175.6

70

all off 10/1

	175.02			
	184.85			
14+93		9.8	175.1	165.2
15+00		10.5	174.4	164.5
100' N at 15+00		25.3	159.6	149.7
15+10		10.8	174.7	164.2
15+25		11.3	173.6	163.7
15+38		12.9	172.0	162.1
T.P.	0.04	162.16	162.12	
		171.99	171.95	
15+50		2.1	169.9	160.1
15+62		6.2	165.8	156.0
15+63		7.5	164.5	154.7
15+66		8.3	163.7	153.9
+67		9.3	162.7	152.9
+80		12.6	159.4	149.6
+85		13.7	158.5	148.5
+90		15.8	156.2	146.4
100' N at 15+90		23.0	149.6	139.2
15+95		12.9	158.1	148.3
16+05		12.7	159.8	149.5
16+23		12.1	159.9	150.1
16+35		13.8	158.2	148.4
T.P.	0.62	150.15	149.51	
		159.93	159.51	
16+60		5.2	154.8	145.0
16+80		8.3	151.7	141.9
17+13		14.8	145.2	135.4
T.P.	0.40	137.60	137.20	
		147.43	147.03	

Aug 26-28

Loudon
Tobell
Morgan.

137.60

~~147.43~~

17+29 = M.H.

F.L. 13.36 124.24 134.07

top 4.58 133.03 142.85

100' N of M.H.

Profile of E. M.H. w of Froude to 50' E of Santa Barbara
Alley Between Coronado & Delmar

BM 317 188.56 185.39

~~178.59~~ 175.22

14+63 = M.H. w of Froude.

top 9.48 179.08 188.71

F.L. 18.54 170.02 179.85

14+45 6.8 181.8 191.6

14+30 = w of Froude 6.2 182.4 192.2

14+20 6.2 182.4 192.2

14+15 6.9 181.7 191.5

14+00 = E Froude 6.0 182.6 192.4

13+88 6.1 182.5 192.3

13+84 6.7 181.9 191.7

13+81 5.5 183.1 192.9

13+71 5.1 183.5 193.3

13+50 1.1 187.5 197.3

T.P. 9.90 196.86 187.96

~~206.69~~ 0.60 ~~197.79~~

13+67 7.3 189.6 200.4

13+62 6.5 190.4 201.2

13+40 5.3 191.6 202.4

13+30 4.9 192.0 202.8

13+20 5.7 191.2 202.0

all off 10' per sec

196.86
~~206.67~~

13+10	5.1	202.6	191.8
12+85	4.4	203.3	192.5
12+75	3.2	204.5	193.7
12+71	4.4	203.3	192.5
12+64	3.8	203.9	193.1
12+55	5.0	202.7	191.9
12+50	3.9	203.8	193.0
95'S at 12+50	10.7	196.3	186.2
125'S at 12+50	25.5	192.2	171.4
12+49	3.7	204.0	193.2
12+48	1.9	205.1	195.0
12+36	2.0	205.7	194.9
12+30	6.5	201.2	190.4
12+18	12.0	195.7	184.9
12+10	12.9	194.1	184.0
T.P. 11.52	188.38 198.21	183.86 193.67	
11+90	12.2	186.0	176.2
11+78	15.2	183.0	173.2
11+60	16.5	181.7	171.9
11+40	16.2	182.0	172.2
70'S at 11+40	17.0	181.2	171.4
105'S at 11+40	10.0	188.2	178.4
11+10	15.8	182.4	172.6
10+85	14.6	183.6	173.8
10+73	12.1	186.1	176.3

188.38
~~198.21~~

10+60	11.5	176.9	166.7
10+39	5.0	183.4	193.2
10+25	3.1	185.3	195.1
10+00	0.4	188.0	197.8
T.P. 12.62	200.94 210.77	0.06	188.32 198.15
9+75	7.3	191.6	201.5
9+50	5.4	195.5	205.4
9+25	0.3	200.6	210.5
T.P. 12.46	213.19 223.02	0.21	200.73 210.56
9+00	9.5	203.7	218.5
8+75	7.1	206.1	215.9
8+65	5.9	207.3	217.7
8+50	1.2	212.0	221.8
T.P. 12.84	225.99 235.82	0.04	213.15 222.98
8+38	10.7	215.3	225.1
8+25	9.8	216.2	226.0
8+00	8.0	218.0	227.8
7+70 = w.L. Guizat.	4.0	220.0	231.8
7+60	4.0	222.0	231.8
7+59	5.0	221.0	230.8
7+40 = E. Guizat	3.8	222.2	232.0
7+25	3.9	222.1	231.9
7+26	4.5	221.5	231.3
7+20	4.2	221.8	231.6
7+20	3.4	222.6	232.4
7+12	2.6	223.4	233.2

all off 10

		225.99		
7+10 = EL Guizo +	1.8	234.0	224.2	
TR 13.06		238.82	225.76	
	0.23	248.65	225.51	
7+07	11.4	237.3	227.4	
6+87	6.4	242.3	232.4	
6+81	7.8	240.9	231.0	
6+75	3.9	244.7	234.9	
100' S. at 6+75	12.4	236.3	226.4	
6+67	3.4	245.3	235.4	
6+66	5.3	243.4	233.5	
6+60	3.0	245.7	235.8	
6+57	4.1	244.6	234.7	
6+54	2.7	246.0	236.1	
6+50	4.6	244.1	234.2	
6+40	2.9	245.8	235.9	
6+25	2.7	246.0	236.1	
6+17	3.5	245.2	235.3	
6+00	2.6	246.1	236.2	
100' S. at 6+00	8.0	240.7	230.8	
5+75 11.31	0.27	249.86	238.55	
		259.65	248.34	
5+47	8.0	251.7	241.9	
5+44	3.3	256.4	246.6	
5+40	1.9	257.8	248.0	
5+37	4.7	253.0	245.2	
5+33	4.7	255.0	245.2	
5+31	1.8	257.9	248.1	

		249.86		
		254.69		
		261.15		249.33
TP 11+82	0.53	270.78		259.16
5+25	11.1		250.1	259.9
5+00	9.3		251.9	261.7
4+75	7.7		253.5	263.3
4+50	6.2		255.0	264.8
4+25	5.1		256.1	265.9
4+00	4.0		257.2	267.0
3+75	3.0		258.2	268.0
3+50	2.3		258.9	268.7
TP 3.71		262.50		258.74
		272.33	2.36	268.62
3+25	3.5		259.0	268.8
3+00	3.8		258.7	268.5
2+75	4.5		258.0	267.8
2+50	5.7		256.8	266.6
2+25	7.2		255.3	265.1
2+00	9.0		253.5	263.3
1+75	10.9		251.6	261.4
1+68	13.0		249.5	259.3
TP 1.87		251.92		250.05
		261.75	12.45	259.88
1+50	4.2		247.7	257.6
1+35	5.2		246.7	256.6
1+10 = W. L. Santa Barbara	7.4		244.5	254.4
1+05	7.7		244.2	254.1
1+00	9.0		242.9	252.8
0+80 = E. Santa Barbara	9.0		242.9	252.8
0+60	9.9		242.0	251.9

01710

251.92

~~251.95~~

0+50 - E.L. Santa Barbara	8.9	252.9	243.0
0+25	7.9	251.9	242.0
0+00 = 50' E of Santa Barbara	11.2	250.6	240.7
B.M. Beginning	11.68	240.24	240.24
profile of Alley between Del Mar's Orchard.			
SW Santa Barbara 50' E of Santa Barbara to NW. W of Forder.			
B.M.	11.68	251.85	240.17
		261.68	250.0
TP	9.61	259.91	250.30
		269.74	260.13
0+00 = 50' E of Santa Barb.	9.4	260.3	250.5
0+20	8.0	261.7	251.9
0+40	7.1	262.6	252.8
0+50 = E.L. Santa Barb.	7.0	262.7	252.9
0+60	7.1	262.6	252.8
0+80 = E Santa Barbara	6.6	263.1	253.3
1+00	6.2	263.5	253.7
1+04	6.1	263.6	253.8
1+05 walk	5.57	264.17	254.34
1+10 = W.L. Santa Barbara	5.5	264.2	254.4
1+50	3.8	265.9	256.1
1+60	1.9	267.8	258.0
1+75	3.7	266.0	256.2
2+00	4.7	265.0	255.2
2+25	5.6	264.1	254.3
2+38	7.4	262.3	252.5
2+50	7.6	262.1	252.3
2+60	8.0	261.7	251.9

259.91

~~259.94~~

2+75	10.2	249.7	259.9
3+00	12.6	247.3	257.1
TP 0.27		247.83	247.56
		257.66	257.39
3+25	3.0	244.8	254.7
3+35	3.8	244.0	253.9
3+50	5.8	242.0	251.9
3+75	8.6	239.2	249.1
4+00	10.2	237.6	247.5
4+25	13.0	234.8	244.7
TP 0.06		235.20	235.14
		245.03	244.97
4+50	3.8	231.4	241.2
4+75	4.6	230.6	240.4
4+90	6.7	228.5	238.3
5+00	9.5	225.7	235.5
5+25	16.1	219.1	228.9
TP 0.17		222.32	222.15
		232.15	231.9
5+40	8.7	213.6	223.5
5+50	9.5	212.8	222.7
5+75	12.6	209.7	219.6
5+85	13.5	208.8	218.7
5+92	13.0	209.3	219.2
6+00	13.8	208.5	218.4
TP 0.11		209.46	209.35
		217.29	217.18
6+25	4.6	204.9	214.7
6+50	7.7	201.8	211.6
6+75	11.8	197.7	207.5

74

101
100

	209.46		196.82
	197.76		206.65
T.P. 0.94	12.64		
B.M. 20th at 7+00	1.78	205.81	195.98
7+00	3.9	203.7	193.9
7+08	5.8	201.8	192.0
7+10 = EL. Guizot	8.8	198.8	189.0
7+22	9.5	198.1	188.3
7+23	10.2	197.4	187.6
7+40 = 4 Guizot	10.2	197.4	187.6
7+58	11.0	196.6	186.8
7+59	10.5	197.1	187.3
7+70 = w.L. Guizot	10.7	196.9	187.1
T.P. 0.26	12.67		
7+81	3.8	191.4	181.6
8+15	6.9	188.3	178.5
8+45	8.8	186.4	176.6
8+61	9.2	186.0	176.2
8+75	10.2	185.0	175.2
9+00	11.0	184.2	174.4
9+25	10.2	185.0	175.2
9+50	9.0	186.2	176.4
9+75	10.9	184.3	174.5
10+00	13.2	182.0	172.2
T.P. 0.74	13.02		
10+25	1.6	180.4	171.5
10+50	1.6	180.4	171.5
100's. at 10+50	6.3	176.7	166.8

	173.12		
	182.95		
10+59	2.5	170.6	180.5
10+68	6.8	166.3	176.2
10+83	13.3	159.8	169.7
10+93	15.4	157.7	167.6
11+00	16.5	156.6	166.5
11+27	15.2	157.9	167.8
11+58	10.6	162.5	172.4
11+68	7.5	165.6	175.5
11+77	3.6	169.5	179.4
11+83	2.3	170.8	180.7
50's. at 11+83	9.8	163.3	173.2
185's. ✓ ✓	23.6	149.5	159.4
100's. ✓ ✓	24.2	148.9	158.8
12+00	2.0	171.1	181.0
T.P. 1.05	5.90		
12+40	2.0	166.3	176.1
12+65	5.0	163.3	173.1
13+00	8.5	159.8	169.6
13+20	9.9	158.4	168.2
100's. at 13+20	18.7	149.6	159.4
13+45	10.6	157.7	167.5
13+66	11.4	156.9	166.7
13+70 = EL. Froude	12.6	155.7	165.5
13+71	16.8	151.5	161.3
T.P. 0.48	12.19		

101767

Oct 16-28

London

Profile of Proposed Drain

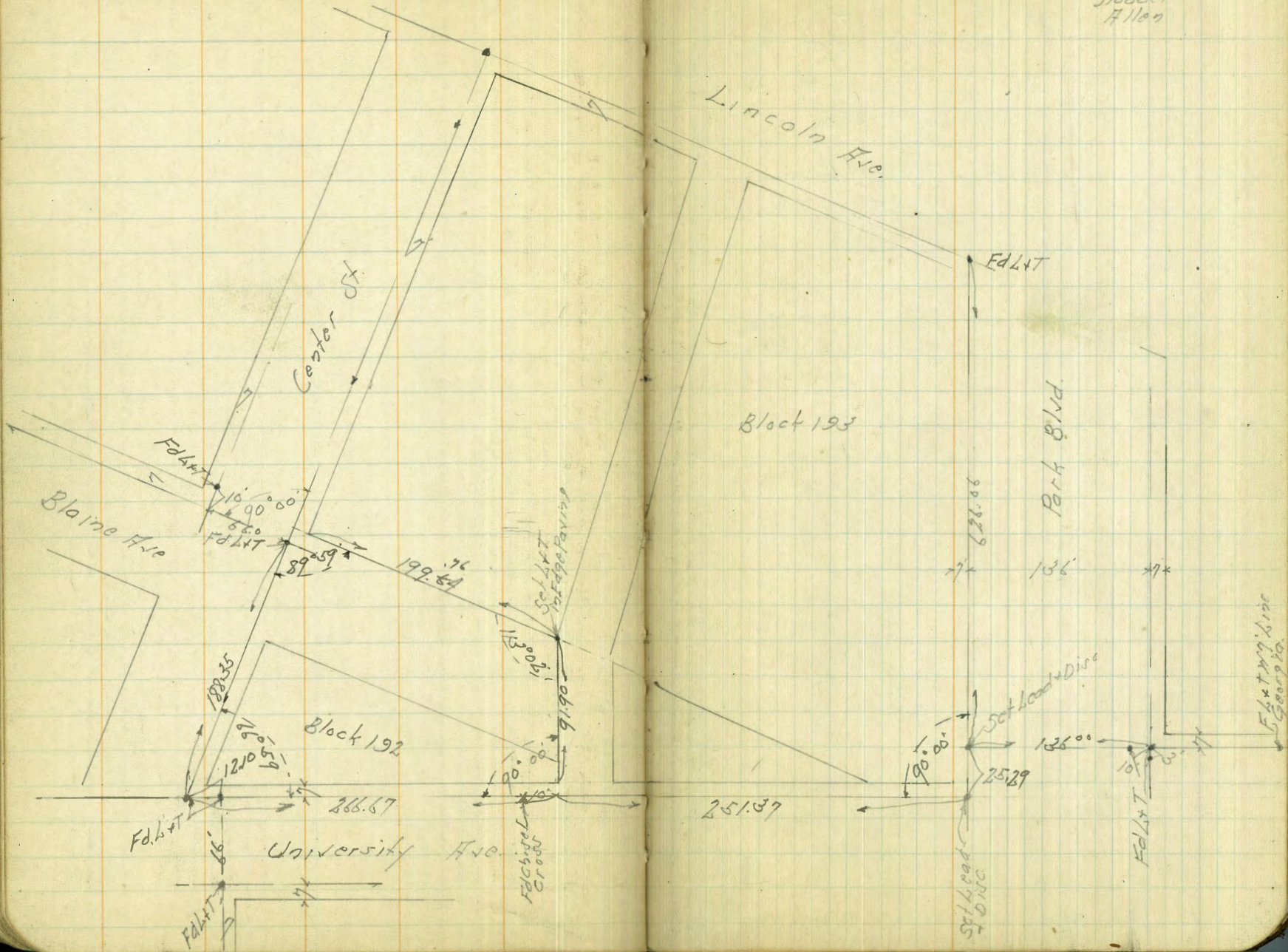
Line shown on P. 76

M.H.	0.21	310.98		310.77	706 Middle of alley.
0+00			10.6	300.38	
0+06			9.1	301.88	
0+08			9.2	301.78	
0+17			7.6	303.38	
0+22			8.1	302.88	
0+29			7.8	303.18	
0+36			11.1	299.88	
0+40			11.5	299.98	
0+60			11.7	299.28	
T.P.	2.82	301.82	11.98	299.00	
0+80			3.9	297.92	
1+00			4.7	297.1	
1+15			5.7	296.1	
1+16			5.2	296.6	
1+17 ²⁵ Δ			5.1	296.7	
1+38			6.2	295.6	
1+47			6.4	295.4	
1+62 ²⁵ FL. Univ Ave Culvert.		8.86		292.96	

Tie Points North of University Ave
West of Park Blvd.

Oct. 14. 16
Sisson
McCoy
Stoddell
Allen

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DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

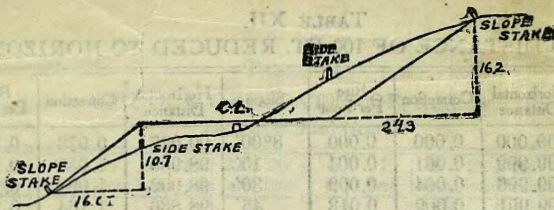
Distance of slope stake from side of shoulder
take for any width roadway, slope 1 1/2 to 1.
If ground is nearly level, the cut or fill at side
stake is located by the double entry method in
left column and top row. The number in body
of table is same row and column gives distance
from side stake to slope stake. If ground is not

IMPROVED TABLES
AND
INFORMATION

TABLE No. 2.

To find Tangent and External for curve of
any other degree, divide by degree of curve and
add correction found in column of corrections.
Degree of curve with a given T may be found
by dividing tangent (or external) or point P by
given tangent (or external).
The distance from a point on the tangent to
the curve is very nearly the square of the tangent
length divided by twice the radius.

46-30
47-00
1-33-30
47-00
2-20-30
47
3 0 1 30



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/4 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 05	1 20	1 35	1 50	1 65	1 80	1 95	2 10	2 25	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

7.05
7.65
7.11

ENGINEERING DEPARTMENT,
CITY OF SAN DIEGO,
CALIFORNIA.

109
110
2-19
1-10
3-29
1-10
4-39

0-43
0-43
1-26
48

0-53
48

4-18
10
4-28

1-36
114.59
52.68
167.27

8+10.93

46+47.90
34.550
591.79

5/5.55
1.11
7.71

11.1
7.8
18.9
7.8
26.7
7.8
34.5
7.8
42.3

5/5.8
1.16
5.7
20.3

1.16
7.8
5.80
8.96

61.34
31
50.30

28.40
0.67
59.07

550
24.935
36.74
611.67

450
20.31
24.87
504.20

194
8.3
52.7
83
320.43
152.13
168.30

114.17
52.68
167.27

67.5
11.2
56.3
11.2
45.1
11.2
33.9
11.2
22.7
11.2
11.5

5/5.5.8
1.11

58.85
23.09
35.85

23.0 L
28.7 R
51.7

58.85
40.00
18.85
58.85
28.70
87.55