

1249

PAST

LEVEL 100A

No. 350F

ENGINEERING DEPARTMENT,
CITY OF ⁵⁵³ SAN DIEGO,
³⁴ CALIFORNIA.

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No. 380 381 382 384 385

X sec.	Page
X sec. Herbert St. Robinson South	1
X sec Franklin 46 th to 47 th	3
X sec East St. Imp. to Woolman	9
X sec Texas Madison to Adams	22
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X sec Alley Blk D. Altadena	30
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" " Cherokee El Cajon to Madison	33-40
" " Quarry on Rose Canyon Rd	41-43
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X sec Wightman from Herman to Boundary	46-48
" " POLK, Idaho to Boundary	49-53
" " 33 rd Ash to H	54-57
" " H 3 rd to 34 th	58-72
" " Alley Blk 72 Ocean Beach	73-76

5/9/28

X-SECTION HERBERT St. from Robinson to South End of Recent Fill

B.M. 294.05

STA + H.I. - Elev.

294.05

3.66 297.71

0+00

Prop. 5.50 292.21

Curb 5.76 291.95

W/4 6.04 291.67

¢ 5.70 292.01

E/4 5.49 292.22

Curb 4.69 293.02

Prop. 4.52 293.19

+ 25

Prop. 3.55 294.16

Curb 4.41 293.30

E/4 4.51 293.20

¢ 4.48 293.23

W/4 4.90 292.81

Curb 5.30 292.41

Prop. 5.16 292.55

0+50

Prop. 5.40 292.31

Curb 5.45 292.26

W/4 5.60 292.11

Plotted
5-10-28
T.G.H.
Yardage

JABBER } May 4th 1928
Bailey
Clarett

1

B.R. N.E. Herbert & Robinson.

S.L. Robinson

Cement

"

"

"

"

"

"

STA.	+	H.I.	-	Elev.
¢			5.35	292.36
E 1/4			4.40	293.31
Curb				Garage in Place
Prop.			4.62	293.09
T.P.			5.08	292.63
	1.69	294.32		
0+75				
Prop.			1.70	292.62
Curb			1.90	292.42
E 1/4			1.90	292.42
¢			2.06	292.26
W 1/4			3.07	291.25
Curb			4.20	290.12
Prop.			6.15	288.17
T.P.			12.48	281.84
	7.96	289.80		
1+00				
Prop.			10.20	279.60
Curb			13.20	276.60
W 1/4			12.20	277.60
¢			11.10	278.70
E 1/4			8.30	281.50
Curb			4.00	285.80
Prop.			0.40	289.40

End of Recent Fill

X - Sections East St. betw. Imperial to Woolman, Franklin Ave. between 46th & 47th

JAEGER } May 5th 1928
Bailey }
Clarett }

3

STA. + H.I. - Elev.

~~12.35 50.61 38.26~~

~~Spike in Pole # 75827 SW. Cor. 45th & Woolman~~

~~0.87 49.74~~

~~Curb SE. Cor. 46th & Woolman~~

~~6.74 56.48~~

T.P.

~~1.49 54.99~~

~~12.30 67.29~~

T.P.

~~0.56 66.73~~

~~7.24 73.97~~

~~3.05 70.92~~

~~Cemen SW Cor. 47th & Woolman~~

~~1.22 72.75~~

~~Spike in Pole # 75820, B.M. 118.56 & 124.55~~

Woolman & 47th SW. Cor. 116.49 Brass Plug

X - Sections on Franklin from W.L. 47th to E.L. 46th

" & East SW. Cor. 101.94 Spike in Pole

116.49

SW. Cor. Woolman & 47th Brass Plug

1.00 117.49

T.P.

7.70 109.79

Plotted 5/9/28
T.G.H.

3.12 112.91

0+00

West Line 47th

N.P. 3.71 109.20

C 4.02 108.89

N/4 4.70 108.21

1/2 4.84 108.07

3/4 5.05 107.86

on Cement

10

See Book 1615 & 2015 page 40

STA	+	H.I.	-	Elev.	
C			4.50	108.41	} on Cement
S.P.			4.12	108.79	
0+50					
S.P.			4.30	108.61	
C			5.10	107.81	
S $\frac{1}{4}$			6.3	106.6	
¢			5.8	107.1	
N $\frac{1}{4}$			5.5	107.4	
C			2.9	110.0	
N.P.			2.6	110.3	
1+00					
N.P.			6.6	106.3	
C			6.4	106.5	
N $\frac{1}{4}$			7.8	105.1	
¢			7.8	105.1	
S $\frac{1}{4}$			8.4	104.5	
C			6.5	106.4	
S.P.			6.2	106.7	
1+25					E.L. Alley
S.P.			7.5	105.4	
C			8.2	104.7	
S $\frac{1}{4}$			9.1	103.8	
¢			8.9	104.0	
N $\frac{1}{4}$			9.0	103.9	

112.91

5

STA.	+	H.I.	-	Elev.
C			10.6	102.3
N.P.			10.6	102.3
1+35				¢ Alley
N.P.			11.30	101.61
C			10.6	102.3
N¼			9.5	103.4
¢			9.4	103.5
S¼			9.7	103.2
C			9.3	103.6
S.P.			9.3	103.6
1+45				W.L. Alley
S.P.			9.8	103.1
C			10.0	102.9
S¼			9.7	103.2
¢			9.9	103.0
N¼			10.4	102.5
C			10.7	102.2
N.P.			10.2	102.7
2+00			10.5	102.4
C			10.9	102.0
N¼			12.5	100.4
¢			12.4	100.5
S¼			12.6	100.3
C			15.0	97.9
S.P.			15.6	97.3

112.91

6

STA.	+	H.I.	-	Elev.
T.P.			12.58	100.33

	5.25	105.58		
--	------	--------	--	--

2+70				E.L. EAST STREET
------	--	--	--	------------------

S.P.			9.2	96.4
------	--	--	-----	------

C			9.0	96.6
---	--	--	-----	------

S $\frac{1}{4}$			7.1	98.5
-----------------	--	--	-----	------

¢			7.0	98.6
---	--	--	-----	------

N $\frac{1}{4}$			6.7	98.9
-----------------	--	--	-----	------

C			4.8	100.8
---	--	--	-----	-------

N.P.			4.0	101.6
------	--	--	-----	-------

3+30				W.L. EAST STREET
------	--	--	--	------------------

N.P.			4.0	101.6
------	--	--	-----	-------

C			5.9	99.7
---	--	--	-----	------

N $\frac{1}{4}$			6.3	99.3
-----------------	--	--	-----	------

¢			6.6	99.0
---	--	--	-----	------

S $\frac{1}{4}$			6.6	99.0
-----------------	--	--	-----	------

C			9.1	96.5
---	--	--	-----	------

S.P.			12.1	93.5
------	--	--	------	------

3+50

S.P.			7.6	98.0
------	--	--	-----	------

C			7.1	98.5
---	--	--	-----	------

S $\frac{1}{4}$			6.2	99.4
-----------------	--	--	-----	------

¢			6.0	99.6
---	--	--	-----	------

N $\frac{1}{4}$			5.7	99.9
-----------------	--	--	-----	------

C			4.7	100.9
---	--	--	-----	-------

105.58

7

STA.	+	H.I.	-	Elev.
N.P.			3.8	101.8
4+00				
N.P.			2.8	102.8
C			4.2	101.4
N $\frac{1}{4}$			4.3	101.3
¢			4.7	100.9
S $\frac{1}{4}$			4.9	100.7
C			4.1	101.5
S.P.			3.7	101.9
4+55				
S.P.			3.8	101.8
C			4.0	101.6
S $\frac{1}{4}$			4.3	101.3
¢			4.1	101.5
N $\frac{1}{4}$			4.0	101.6
C			3.3	102.3
N.P.			2.9	102.7
4+65				
N.P.			3.2	102.4
C			3.5	102.1
N $\frac{1}{4}$			4.0	101.6
¢			4.2	101.4
S $\frac{1}{4}$			4.2	101.4
C			4.4	101.2
S.P.			4.4	101.2

E.L. Alley

¢ Alley

105.58

8

STA.	+	H.I.	-	Elev.
4+75				
SP.			4.5	101.1
C			4.6	101.0
S $\frac{1}{4}$			4.3	101.3
¢			4.2	101.4
N $\frac{1}{4}$			4.10	101.48
C			3.70	101.88
N.P.			3.3	102.3
5+00				
N.P.			3.9	101.7
C			4.0	101.6
N $\frac{1}{4}$			4.4	101.2
¢			4.6	101.0
S $\frac{1}{4}$			4.7	100.9
C			5.4	100.2
S.P.			5.7	99.9
5+50				
S.P.			5.7	99.9
C			5.5	100.1
S $\frac{1}{4}$			5.1	100.5
¢			4.7	100.9
N $\frac{1}{4}$			4.7	100.9
C			4.0	101.6
N.P.			3.8	101.8

W. L. Alley

STA	+	H.I.	-	Elev.
6+00 ⁷⁵				
N.P.			3.1	102.5
C			3.6	102.0
N $\frac{1}{4}$			4:10	101.48
¢			4.3	101.3
S $\frac{1}{4}$			4.6	101.0
C			5.5	100.1
S.P.			5.8	99.8

East St.

EAST STREET South from ¢ Franklin St.

0+00				
W.P.			6.6	99.0
C			6.8	98.8
W $\frac{1}{4}$			7.0	98.6
¢			7.2	98.4
E $\frac{1}{4}$			7.1	98.5
C			7.1	98.5
E.P.			7.0	98.6
0+10				
E.P.			7.1	98.5
C			7.4	98.2
E $\frac{1}{4}$			7.8	97.8
¢			7.8	97.8
W $\frac{1}{4}$			7.5	98.1
C			7.0	98.6
W.P.			6.6	99.0

E.L. 46TH STREET.

$$\begin{array}{r} 61.00 \\ 3.50 \\ \hline 27.50 \end{array}$$

¢ Franklin STREET

East

105.58

ST

10

STA.	+	H.I.	-	Elev.
0+20				
W.P.			9.2	96.4
C			9.9	95.8
W $\frac{1}{4}$			8.3	97.3
¢			8.6	97.0
E $\frac{1}{4}$			8.5	97.1
C			8.7	96.9
E.P.			8.7	96.9
0+30				
W.P.			11.6	94.0
C			11.7	93.9
W $\frac{1}{4}$			9.2	95.4
¢			8.9	96.7
E $\frac{1}{4}$			8.9	96.7
C			9.7	95.9
E.P.			9.3	96.3
0+50				
W.P.			12.5	93.1
C			11.9	93.7
W $\frac{1}{4}$			9.6	96.0
¢			9.4	96.2
E $\frac{1}{4}$			9.8	95.8
C			9.0	96.6
E.P.			8.4	97.2

S. L. Franklin

STA.	+	H.I.	-	Elev.
1+00				
E.P.			5.8	99.8
C			6.9	98.7
E'4			9.7	95.9
¢			9.9	95.7
W'4			10.3	94.3
C			11.2	94.4
W.P.			14.0	91.6
T.P.			11.45	94.13

5.75 99.88

1+50				
W.P.			8.9	91.0
C			7.2	92.7
W'4			5.6	94.3
¢			5.4	94.5
E'4			4.8	95.1
C			1.7	98.2
E.P.			0.4	99.5

2+00				
E.P.			6.5	93.4
C			7.8	92.1
E'4			7.7	92.2
¢			7.8	92.1
W'4			8.2	91.7
C			10.4	89.5
W.P.			12.7	87.2

99.85

12

STA. + H.I. - Elev.

2+50

STA.	+	H.I.	-	Elev.
W.P.			13.3	86.6
C			9.9	90.0
W $\frac{1}{4}$			6.5	93.4
¢			5.6	94.3
E $\frac{1}{4}$			5.2	94.7
C			1.9	98.0
E.P.			1.0	98.9

3+00

STA.	+	H.I.	-	Elev.	Notes
E.P.				100.9	Hand Level
C				100.9	" "
E $\frac{1}{4}$			2.9	97.0	
¢			3.0	96.9	
W $\frac{1}{4}$			3.8	96.1	
C			2.4	97.5	
W.P.			1.1	98.8	
T.P.			3.04	96.84	

7.09 103.93

STA.	+	H.I.	-	Elev.
3+50 W.P.			5.2	98.7
C			5.0	98.9
W $\frac{1}{4}$			6.6	97.3
¢			7.0	96.9
E $\frac{1}{4}$			7.2	96.7
C			6.1	97.8
E.P.			6.1	97.8

103.93

13

STA.	+	H.I.	-	Elev
4+00				
E.P.			8.8	95.1
C			9.0	94.9
E $\frac{1}{4}$			9.0	94.9
¢			8.5	95.4
W $\frac{1}{4}$			8.4	95.5
C			7.2	96.7
W.P.			6.4	97.5
4+50				
W.P.			8.9	95.0
C			9.2	94.7
W $\frac{1}{4}$			9.0	94.9
¢			8.2	95.7
E $\frac{1}{4}$			7.8	96.1
C			5.4	98.5
E.P.			5.3	98.6
5+00				
E.P.			4.8	99.1
C			5.0	98.9
E $\frac{1}{4}$			6.2	97.7
¢			6.2	97.7
W $\frac{1}{4}$			6.5	97.4
C			6.7	97.2
W.P.			7.0	96.9

103.93

14

ST.A.	+	H.I.	-	Elev.
S+50				
W.P.			5.8	98.1
C			5.9	98.0
W $\frac{1}{4}$			6.0	97.9
¢			5.4	98.5
E $\frac{1}{4}$			5.2	98.7
C			4.6	99.3
E.P.			4.0	99.9
G+00				
E.P.			3.7	100.2
C			4.2	99.7
E $\frac{1}{4}$			4.5	99.4
¢			4.5	99.4
W $\frac{1}{4}$			4.6	99.3
C			4.5	99.4
W.P.			4.6	99.3
G+35 ⁸⁹				
W.P.			3.4	100.5
C			3.6	100.3
W $\frac{1}{4}$			3.8	100.1
¢			3.3	100.6
E $\frac{1}{4}$			3.4	100.5
C			2.5	101.4
E.P.			2.5	101.4

N.H. Woolman

East

103.93

ST.

15

STA.	+	H.I.	-	Elev.
G+57 ⁸⁹				
E.P.			2.85	101.08
C			3.14	100.79
E 1/4			3.44	100.49
¢			3.60	100.33
W 1/4			3.85	100.08
C			4.05	99.88
W.P.			4.28	99.65

North Hetter Board on Woolman

T.P.

12.51 115.59

1.07 114.52

116.49

5.89 120.41

4.24 116.17

EAST STREET North from ¢ Franklin

0+00

98.89 ?

10.57 109.46

0+10

W.P.			10.0	99.5
C			10.10	99.36
W 1/4			10.50	98.96
¢			10.60	98.66
E 1/4			10.90	98.56
C			10.90	98.66
E.P.			10.70	98.76

East

109.46

st

STA. + H.I. - Elev.

0+20

E.P.	8.9	100.6
C.	9.1	100.4
E 1/4	10.4	99.1
☐	10.2	99.3
W 1/4	9.8	99.7
C	9.5	100.0
W.P.	8.9	100.6

N.L. Franklin

0+30

W.P.	8.6	100.9
C	9.3	100.2
W 1/4	9.6	99.9
☐	9.7	99.8
E 1/4	9.2	100.3
C	8.6	100.9
E.P.	8.0	101.5

Yardage
 Det. Franklin & Imperial
 figured T.G.H.
 5/21/28

0+50

E.P.	7.4	102.1
C	7.8	101.7
E 1/4	8.3	101.2
☐	8.7	100.8
W 1/4	8.8	100.7
C	7.9	101.6
W.P.	7.6	101.9

109.46

17

STA.	+	H.I.	-	Elev.
1+00				
W.P.			6.9	102.6
C			7.3	102.2
W ¹ / ₄			6.8	102.7
ϕ			6.8	102.7
E ¹ / ₄			6.5	103.0
C			6.4	103.1
E.P.			6.2	103.3
1+50				
E.P.			4.8	104.7
C			5.7	103.8
E ¹ / ₄			5.6	103.9
ϕ			5.8	103.7
W ¹ / ₄			5.9	103.6
C			6.0	103.5
W.P.			5.7	103.8
2+00				
W.P.			5.5	104.0
C			5.8	103.7
W ¹ / ₄			5.4	104.1
ϕ			5.10	104.36
E ¹ / ₄			5.0	104.5
C			5.1	104.4
E.P.			4.4	105.1

109.46

19

STA.	+	H.I.	-	Elev.
4+00				
W.P.			6.6	102.9
C			6.0	103.5
W ¹ / ₄			5.2	104.3
☒			5.2	104.3
E ¹ / ₄			5.0	104.5
C			5.2	104.3
E.P.			4.8	104.7
4+50				
E.P.			5.1	104.4
C			5.6	103.9
E ¹ / ₄			5.2	104.3
☒			5.7	103.8
W ¹ / ₄			6.0	103.5
C			6.7	102.8
W.P.			7.0	102.5
5+00				
W.P.			7.2	102.3
C			6.9	102.6
W ¹ / ₄			6.3	103.2
☒			6.0	103.5
E ¹ / ₄			5.9	103.6
C			5.7	103.8
E.P.			5.3	104.2

109.46

20

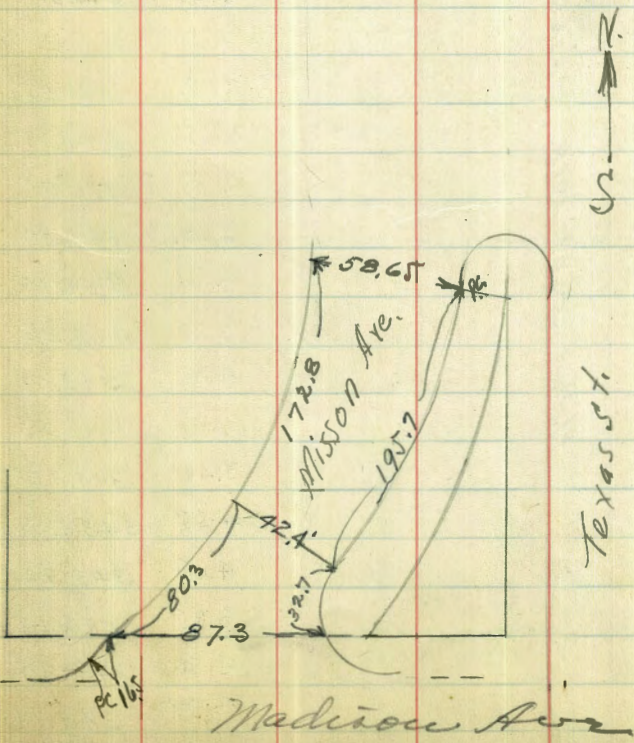
STA.	+	H.I.	-	Elev.
5+50				
E.P.			5.4	104.1
C			5.4	104.1
E ¹ / ₄			6.3	103.2
ϕ			6.4	103.1
W ¹ / ₄			6.7	102.8
C			6.3	103.2
W.P.			6.5	103.0
6+00				
W.P.			6.8	102.9
C			7.1	102.4
W ¹ / ₄			7.4	102.1
ϕ			7.3	102.2
E ¹ / ₄			7.2	102.3
C			6.2	103.3
E.P.			6.7	102.8
6+35 ⁸⁹				
E.P.			7.9	101.6
C			7.7	101.8
E ¹ / ₄			7.1	102.4
ϕ			8.0	101.5
W ¹ / ₄			8.4	101.1
C			8.8	100.7
W.P.			7.9	101.6

Sta. Imp.

109.H6

STA.	T.P.	+	H.I.	-	Elev.
		4.04	107.64	5.86	103.60
6+56 ⁸⁹				7.11	100.53
W.P.				6.82	100.82
C				6.53	101.11
W ¹ / ₄				6.26	101.38
¢				5.96	101.68
E ¹ / ₄				5.61	102.03
C				5.33	102.31
E.P.					

South Edge of Pavement on Imperial



X-Sections Texas from Madison to Adams

Mission Ave. " " " "

STA.	+	H.I.	-	Elev.
	B.M. Brass Plug	SE. Cor. Texas & Madison		346.03
	1.77	347.80		
0+00	Intersection	E.L. Texas & N.L. Madison	(NE. Cor. Texas & Madison)	
	Curb Top +14		1.92	345.88
	" Bottom +14		2.65	345.15
	E 1/4 +27		2.40	345.40
	¢ +40		2.60	345.20
	W 1/4 +53		3.10	344.70
	Curb Top +66		2.70	345.10
	" Bott. +66		3.50	344.30
0+50				
	C-Top		2.65	345.15
	C-Bott.		3.65	344.15
	E 1/4		3.25	344.55
	¢		3.00	344.80
	W 1/4		3.70	344.10
	C-Top		3.55	344.25
	C-Bott.		4.10	343.70
1+00				
	C-Top		3.48	344.32
	C-Bott.		4.55	343.25
	E 1/4		4.05	343.75
	¢		3.65	344.15
	W 1/4		4.55	343.25
	C-Top		4.06	343.74
	C-Bott.		5.10	342.70

Plotted 5-22-1928 C.E.H. 694

JAEGER
Bailey
Claert

Mag 11th 1928. May 12th

STA.	+	H.I.	-	Elev.
		347.80		
1+50				
	C-Top		4.34	343.46
	C-Bott.		5.20	342.60
	E 1/4		4.85	342.95
	¢		4.60	343.20
	W 1/4		5.20	342.60
	C-Top		4.67	343.13
	C-Bott.		5.40	342.40
2+00				
	C-Top		5.02	342.78
	C-Bott.		5.45	342.35
	E 1/4		5.20	342.60
	¢		5.25	342.55
	W 1/4		5.60	342.20
	C-Top		5.07	342.73
	C-Bott.		5.95	341.85
2+25	Termination of Curb & Side Walk on E.L. Texas			
	C-Top		5.35	342.45
	C-Bott.		6.05	341.75
	E 1/4		5.90	341.90
	¢		5.95	341.85
	W 1/4		5.95	341.85
	+ 100		5.80	342.00
	Top C +163'		3.12	344.68
	Bot. C		3.90	343.90

See page 78

+ 162 ft.

347.80

347.80

23

Sta.	+	H.I.	-	Elev.	Sta.	+	H.I.	-	Elev.
2+50					3+00				
E.L.			4.6	343.2	E.L.			10.1	337.7
+14			7.4	340.4	+13			10.05	337.75
+27			7.15	340.65	+14			11.05	336.75
+40			7.45	340.35	+27			10.4	337.4
+53			7.20	340.60	+40			10.65	337.15
+100			5.70	342.10	+68			9.90	337.90
+147			5.00	342.80	+87			9.35	338.45
Top Curb + 161	← 160 ft	W. Curb	3.03	344.77	+94			4.85	342.95
Bot. "		Mission Ave.	3.70	344.10	+100			3.85	343.95
2+75					+114			3.20	344.60
E.L.			7.05	340.75	+117			5.35	342.45
+12			7.90	339.90	Bot. C + 154	↙		3.60	344.20
+14			9.00	338.80	Coner. Driveway				
+27			8.90	338.90	3+25				
+40			9.10	338.70	E.L.			12.1	335.7
+53			8.70	339.10	+10			12.35	335.45
+66			7.95	339.85	+11			13.2	333.6
+100			7.00	340.80	+14			12.5	335.3
+114			7.00	340.00	+27			12.5	335.3
+121			4.75	343.05	+40			12.95	334.85
Top C + 157	✓ 156 ft	H.	2.90	345.90	+53			12.55	335.35
Bot. C			3.45	344.35	+62			12.55	335.35
					+68			9.15	338.65
					+83			7.70	340.10
					+100			3.95	343.85

34780

STA.	+	H.I.	-	Elev.
+121			2.9	344.9
+124			4.1	343.7
Top C +152	✓		3.30	344.50
Bot. C			4.10	343.70
	T.P.		12.25	335.55
	1.63	337.18		
3+50				
E.L.			2.5	334.7
+9			2.5	334.7
+11			3.85	333.33
+14			3.20	333.98
+27	40' to Ctr. Road		4.60	332.58
+33	Center Existing Road		4.45	332.73
+38			4.65	332.53
+40			4.00	333.18
+48			5.50	332.68
+51			3.75	333.43
+66			3.10	334.08
+83			4.25	332.93
	T.P.		1.27	335.91
	Hand Level 13.0	348.91		
+100			8.3	340.6
+107			5.7	343.2
Top C +149	148' St. to cl.		4.4	344.5
Bot. C			5.4	343.5

STA.	+	H.I.	-	Elev.
	Instr.	337.18		
T.P.			11.83	325.35
Hand Level	1.70	327.05		
3+75				
+40	East of E. h. Texas		4.20	322.85
+20	" " " "		6.20	320.85
	Instr.	337.18		
0			10.2	327.0
+12			5.5	331.7
+33	40' to Ctr. Road		7.15	330.03
	Center Exist. Road			
+44			7.40	329.78
+47			8.45	328.73
+51			5.30	331.88
+96			5.30	331.88
	T.P.		0.12	337.66
	Hand Level 11.60	348.66		
+122			5.40	343.26
Top-C +146.5	145' to cl.		4.50	344.16
Bot. C			5.30	343.36
	Instr.	337.18		
	T.P.		12.42	324.76
	1.90	326.66		
	T.P.		11.10	315.56
	Hand Level 6.90	322.46		

24
Elev.

322.46

330.59

25

STA.	+	H.I.	-	Elev.	STA.	+	H.I.	-	Elev.
+17	East of E.L. Texas		14.0	308.5	+40	<u>46° to Ctr Road</u> Center Ex. Rd.		5.3	325.3
4+00 - 0			3.6	318.9	+52			6.5	324.1
	T.P.		1.30	321.16	+54			4.7	325.9
		13.0	334.16		+88			1.0	329.6
+15			5.30	328.86		T.P.		0.4	330.19
+34	<u>42' to ctr. Road</u> Center Existing Rd.		6.80	327.36			12.40	342.59	
+47			7.40	326.76	+92			11.9	330.7
+50			6.00	328.16	+97			12.5	330.1
+68			4.20	329.96		T.P.		0.6	341.99
+96			4.10	330.06			6.50	348.47	
	T.P.		0.00	334.16	+123			5.7	343.8
		11.10	345.26		+170			3.0	345.5
+117			2.40	342.86				324.25	
Top. C + 145	<u>1425' to dl.</u> Termination of Curb + Sidewalk		1.10	344.16		T.P.		9.30	314.95
Bot. C			1.40	343.86		Hand Level	0.00	314.95	315.0
	Instr.		326.66		+6	East of E.L. Texas		14.3	300.7
	T.P.		9.57	317.09	4+50 - 0			11.5	303.5
		7.16	324.25					324.25	
			8.46	315.79	+31			0.25	324.00
	Hand Level	1.8	317.59		+46	<u>5247' to Road</u> Center Exist. Rd.		1.75	322.50
+11	East of E.L. Texas		11.7	305.9	+58			3.15	321.10
4+25 0			5.4	312.2	+61			1.45	322.80
	T.P.		0.1	317.49		T.P.		0.00	324.25
		13.10	330.59		Hand Level	10.60	334.85		
+22			2.70		+66			6.80	328.05

334.85

346.35

26

STA.	+	H.I.	-	Elev.	STA.	+	H.I.	-	Elev.
+95			5.10	329.75	+ 196			1.7	344.7
	T.P.		0.0	334.85			<u>324.25</u>		
	11.2	346.05			T.P.			13.0	311.15
+105			6.9	339.2	Hand Level	0.0	311.15		
+120			3.2	342.9	S+00			12.0	299.3
+170			0.6	345.5	+13			17.5	293.8
		<u>324.25</u>					<u>324.25</u>		
	T.P.		10.28	313.97	+58			8.5	315.8
	Hand Level	0.0	313.97		+68	to to Q Road Center Ex. Rd.		9.6	314.7
	T.P.		13.30	300.67	+78			10.0	314.25
	4.00	304.67			T.P.			0.0	324.25
A+75			5.5	299.2	Hand Level	13.0	337.25		
	T.P.		1.1	303.57	T.P.			0.0	337.25
	12.60	316.17				11.5	348.75		
	T.P.		1.4	314.77	+122			9.10	339.65
		<u>324.25</u>			+148			3.90	344.85
+50			5.85	318.40	+162			4.5	344.3
+60	59 to Q Road Center Exist. Road		6.65	317.60			<u>324.25</u>		
+71			7.65	316.60	T.P.			13.20	311.05
	T.P.		0.0	324.25	Hand Level	0.3	311.35		
	Hand Level	13.10	337.35		S+25			10.5	300.9
+117			6.8	330.6	+18			20.2	291.2
	T.P.		0.0	337.35			<u>324.25</u>		
	9.0	346.35			+70			12.0	312.3
+151			5.5	340.9	+80	73 to Q Road Center Ex. Rd.		13.0	311.3

STA.		+	H.I.	-	Elev.	STA.		+	H.I.	-	Elev.
			324.25								27
+90				13.7	310.6			11.30	348.25		
	T.P.			0.0	324.25	+150				6.7	341.6
	Hand Level	13.20	335.45 311.95			+177				5.3	343.0
	T.P.			0.0	335.45 311.05				324.25		
		10.20	345.65 321.25			T.P.				13.0	311.25 ✓
+133				7.8	337.9	Hand Level	0.20	311.45			
+161				4.6	341.1	S+75				4.8	306.7
			324.25			T.P.				13.0	298.45
	T.P.			13.65	311.20		1.30	299.75			
	Hand Level	1.0	312.20			+30				12.2	287.6
S+50				7.0	305.2	T.P.					311.25 ✓
	T.P.			13.0	299.20		3.90	315.15			
		2.0	301.20			+85				8.10	307.05
+20				12.3	298.9	+95	88' to to Road			9.0	306.2
			324.25			+105				9.6	305.6
	T.P.			13.05	311.20				324.25		
	Hand Level	5.20	316.40			+120				0.0	324.25
+75				6.5	309.9	Hand Level	13.20	337.95			
+85	to Road	81' to to Road		7.5	308.9	+135	T.P.			1.40	336.05
+95				9.2	307.2		11.60	347.65			
			324.25			+145				9.6	338.1
+115	T.P.			0.0	324.25	T.P.					311.25 ✓
	Hand Level	12.70	336.95				0.0	311.25			
+135	T.P.			0.0	336.95	G+00				7.8	303.5

349.31

349.31

29

STA.	+	H.I.	-	Elev.	STA.	+	H.I.	-
0+25	Width	43.70'			1+00	Width	49.27'	
W. Curb Top			5.46	343.85	E. Curb Top		5.7	343.6
" Bott.			6.10	343.21	" Bott.		6.6	342.7
W 1/4			5.8	343.5	E 1/4		6.0	343.3
ϕ			5.5	343.8	ϕ		5.6	343.7
E 1/4			5.7	343.6	W 1/4		5.3	344.0
E. Curb Top			5.36	343.95	W. Curb Top		5.01	344.30
" Bott.			6.2	343.1	" Bott.		5.6	343.7
0+50	Width	45.50'			1+25	Width	51.50	
E. Curb Top			5.41	343.90	W. Curb Top		4.89	344.42
" Bott.			6.3	343.0	" Bott.		5.70	343.61
E 1/4			5.9	343.4	W 1/4		5.40	343.91
ϕ			5.4	343.9	ϕ		5.40	343.91
W 1/4			5.5	343.8	E 1/4		5.80	343.51
W. Curb Top			5.33	343.98	E. Curb Top		5.85	343.46
" Bott.			6.1	343.2	" Bott.		6.80	342.51
0+75	Width	47.65'			1+50	Width	53.95	
W. Curb Top			5.15	344.16	E. Curb Top		5.96	343.35
" Bott.			5.6	343.7	" Bott.		6.90	342.41
W 1/4			5.6	343.7	E 1/4		6.40	342.91
ϕ			5.3	344.0	ϕ		5.80	343.51
E 1/4			5.8	343.5	W 1/4		5.40	343.91
E. Curb Top			5.54	343.77	W. Curb Top		4.70	344.61
" Bott.			6.3	343.0	" Bott.		5.60	343.71

349.31

JAEGER - Bailey - Clavert, May 14th 1928.

X - Section Alley - Block D - Alhadena between
Felton & Gregory from Upas to Thorn

30

STA.	+	H.I.	-	Elev.
1+75	Width	56.35'		
W. Curb Top			4.55	344.76
" Bot.			5.60	343.71
W/4			5.40	343.91
¢			5.60	343.71
E/4			6.20	343.11
E. Curb Top			6.15	343.16
" Bot.			7.0	342.3
1+95 ⁷⁰	P.R.C. E. Curb Line	Mission Ave.	Width	58.65'
E. Curb Top			6.2	343.1
" Bot.			7.10	342.21
E/4			6.3	343.0
¢			5.8	343.5
W/4			5.5	343.8
W. Curb Top			4.45	344.86
" Bot.			5.10	344.21

STA.	+	H.I.	-	Elev.
SE. Cor. 32nd & Upas. N. Curb Line				325.00
	1.32	326.32		
T.P.			8.37	317.95
	2.26	320.21		
T.P. on Garage Drive Way			7.62	312.59
	12.38	324.97		
T.P. on 0+00 & Alley			5.91	319.06
	6.78	325.84		
0+00 E.L. Cement = N.L. Thorn			6.60	319.2
¢			6.78	319.0
W.L.			6.66	319.1
0+49				
+4' from W.L. & Garage Cement Floor			5.47	320.3
W.L.			5.65	320.1
¢			5.90	319.9
E.L.			6.0	319.8
1+00				
E.L.			5.7	320.1
¢			5.5	320.3
W.L.			5.7	320.1
1+28				
W.L.			5.4	320.4
¢			5.4	320.4
E.L.			5.5	320.3
+ 5.2' for E.L. & Garage Cement Floor			5.26	320.5

STA.	+	H.I.	-	Elev.	STA.	+	H.I.	-	Elev.
1+50		325.84			3+00		325.26		
W.L.			5.10	320.7	W.L.			3.7	321.6
φ			5.20	320.6	φ			3.7	321.6
E.L.			5.30	320.5	E.L.			3.9	321.4
2+00					3+50				
W.L.			4.2	321.6	+8.3 from E.L. φ Garage, Conc. Floor			4.13	321.1
φ			4.9	320.9	E.L.			4.10	321.2
E.L.			4.8	321.0	φ			3.90	321.4
2+12					W.L.			3.90	321.4
+ 10.8 from E.L. φ Garage, Concrete Floor			4.51	321.3	3+81				
E.L.			4.8	321.0	W.L.			4.30	321.0
φ			4.7	321.1	φ			4.40	320.9
W.L.			4.6	321.2	E.L. φ Garage Conc. Floor			4.80	320.5
2+50					4+14				
W.L.			4.4	321.4	+ 7.8 from E.L. φ Garage, Conc. Floor			5.72	319.6
φ			4.6	321.2	E.L.			5.60	319.7
E.L.			4.7	321.1	φ			5.30	320.0
T.P.			4.48	321.36	W.L.			5.10	320.2
	3.90	325.26			4+32				
2+88					+3.4 from W.L. φ Garage, Board Floor			4.60	320.7
+ 13.3 from E.L. φ Garage, Conc. Floor			3.84	321.4	W.L.			5.60	319.7
E.L.			3.9	321.3	φ			5.90	319.4
φ			3.7	321.5	E.L.			6.20	319.1
W.L.			3.7	321.5					

STA.	+	H.I.	-	Elev.
4+49		325.26		
E.L.			6.8	318.5
ϕ			6.4	318.9
W.L.			6.0	319.3
+1.7	from W.L. ϕ Garage, Conc. Floor		5.88	319.4
4+86				
+1.7	from W.L. ϕ Garage, Conc. Floor		7.00	318.3
W.L.			7.30	318.0
ϕ			8.0	317.3
E.L.			8.3	317.0
5+00				
E.L.			9.0	316.3
ϕ			8.7	316.6
W.L.			7.6	317.7
5+53				
+1.20	from W.L. ϕ Garage, Conc. Floor		10.79	314.5
W.L.			11.20	314.1
ϕ			11.90	313.4
E.L.			12.80	312.5
T.P.			13.17	312.09
	3.33	315.42		
5+90				
E.L.			5.6	309.8
ϕ			4.8	310.6
W.L.			4.3	311.1

STA.	+	H.I.	-	Elev.
6+00		315.42		
W.L.			4.50	310.9
ϕ			5.20	310.2
E.L.			5.40	310.0

X-Section Cherokee - El Cajon to Madison
36' Between Curbs

JAEGER
Bailey
Clareit } May 15th 1928.

33

STA.	+	H.I.	-	Elev.
B.M. Tr. Pl.	SW. Cor. El Cajon & 36 th			377.94
	4.51	382.45		
	T.P.			
0+00	N.L. El Cajon	8.03	385.56	
W.C. Top		8.64	376.92	
" Bott. Cement		9.21	376.35	
W ¹ / ₄		9.0	376.56	
ϕ		8.83	376.73	
E ¹ / ₄		9.09	376.47	
E.C. Top		9.0	376.56	
" Bott.		9.53	376.03	
0+50				
E.C. Top		8.50	377.06	
" Bott.		9.2	376.4	
E ¹ / ₄		8.6	377.0	
ϕ		8.3	377.3	
W ¹ / ₄		8.5	377.1	
W.C. Top		8.06	377.50	
" Bott.		8.80	376.76	

Here notes are all

done

at

the

end

STA.	+	H.I.	-	Elev.
1+00		385.56		
W.C. Top		7.55	378.01	
" Bott.		8.3	377.3	
W ¹ / ₄		7.9	377.7	
ϕ		7.7	377.9	
E ¹ / ₄		8.0	377.6	
E.C. Bott.		8.6	377.0	
" Top		7.81	377.75	
1+42 ⁵⁰	S.L. Alley			
E.C. Top		7.26	378.30	
" Bott.		7.5	378.1	
E ¹ / ₄		7.3	378.3	
ϕ		7.1	378.5	
W ¹ / ₄		7.2	378.4	
W.C. Bott.		7.6	378.0	
" Top		6.92	378.64	
1+57 ⁵⁰	N.L. Alley			
W.C. Top		6.71	378.84	
" Bott.		7.4	378.2	
W ¹ / ₄		7.1	378.5	
ϕ		7.1	378.5	
E ¹ / ₄		7.2	378.4	
E.C. Bott.		7.3	378.3	
" Top		7.85	377.71	

STA.	+	H.I.	-	Elev.	STA.	+	H.I.	-	Elev.
2+00		385.56			3+50		385.56		
E.C. Top			6.52	379.04	W.C. Top			4.19	381.37
" Bott.			7.3	378.3	" Bott.			5.1	380.5
E 1/4			6.6	379.0	W 1/4			4.5	381.1
ϕ			6.6	379.0	ϕ			4.6	381.0
W 1/4			6.6	379.0	E 1/4			4.7	380.9
W.C. Bott.			7.1	378.5	E.C. Bott.			5.3	380.3
" Top			6.16	379.40	" Top			4.69	380.82
2+50					4+00				
W.C. Top			5.57	379.99	E.C. Top			3.85	381.71
" Bott.			6.5	379.1	" Bott.			4.50	381.06
W 1/4			5.8	379.8	E 1/4			4.0	381.6
ϕ			5.6	380.0	ϕ			3.6	382.0
E 1/4			5.9	379.7	W 1/4			3.9	381.7
E.C. Bott.			6.5	379.1	W.C. Bott.			4.3	381.3
" Top			5.8	379.8	" Top			3.51	382.05
3+00					4+50				
E.C. Top			5.30	380.25	W.C. Top			2.84	382.72
" Bott.			6.0	379.6	" Bott.			3.6	382.0
E 1/4			5.4	380.2	W 1/4			3.1	382.5
ϕ			5.3	380.3	ϕ			3.0	382.6
W 1/4			5.3	380.3	E 1/4			3.0	382.6
W.C. Bott.			5.5	380.1	E.C. Bott.			3.8	381.8
" Top			4.92	380.64	" Top			3.15	382.41

STA.	+	H.I.	-	Elev.	STA.	+	H.I.	-	Elev.
S+00		385.56			T.P.			0.88	384.68
E.C. Top			2.45	383.11		4.02	388.70		
" Bott.			3.0	382.6	6+07 ⁵⁵	S.L. Mead Ave. (olive)			
E 1/4			2.4	383.2	E.C. Top			4.02	384.68
¢			2.2	383.4	" Bott.			4.3	384.3
W 1/4			2.3	383.3	E 1/4			3.9	384.8
W.C. Bott.			2.8	382.8	¢			3.6	385.1
" Top			2.08	383.48	W 1/4			3.8	384.9
S+50					W.C. Bott.			4.1	384.6
W.C. Top			1.28	384.28	" Top			3.59	385.11
" Bott.			2.00	383.56	T.P.			4.92	383.78
W 1/4			1.55	384.01		5.29	389.07		
¢			1.6	383.96	0+00	N.L. Mead (olive)			
E 1/4			1.65	383.91	W.C. Top			5.35	383.72
E.C. Bott.			2.3	383.26	" Bott.			6.12	382.95
" Top			1.67	383.89	W 1/4			5.6	383.5
G+00					¢			5.1	384.0
E.C. Top			0.98	384.58	E 1/4			5.6	383.5
" Bott.			1.50	384.06	E.C. Bott.			6.4	382.7
E 1/4			0.9	384.66	" Top			5.78	383.29
¢			0.7	384.86	0+50				
W 1/4			0.7	384.86	E.C. Top			5.63	383.44
W.C. Bott.			1.1	384.46	" Bott.			6.1	383.0
" Top			0.6	384.96	E 1/4			5.6	383.5
					¢			5.4	383.7

STA	+	H.I.	-	Elev.	STA	+	H.I.	-	Elev.
W/4		389.07	5.4	383.7	E.C. Bott.			5.6	383.5
W.C. Bott.			5.9	383.2	" Top			5.02	384.05
" Top			5.17	383.90	2+50				
1+00					E.C. Top				
W.C. Top			5.03	384.04	" Bott.	Driveway		5.31	383.76
" Bott.			5.7	383.4	E/4			4.8	384.3
W/4			5.4	383.7	☐			4.5	384.6
☐			5.2	383.9	W/4			4.7	384.4
E/4			5.5	383.6	W.C. Bott.			5.4	383.7
E.C. Bott.			6.0	383.1	" Top			4.60	384.47
" Top			5.39	383.68	3+00				
1+50					W.C. Top			4.21	384.86
E.C. Top			5.23	383.84	" Bott.			5.1	384.0
" Bott.			5.9	383.2	W/4			4.5	384.6
E/4			5.3	383.8	☐			4.3	384.8
☐			5.0	384.1	E/4			4.5	384.6
W/4			5.2	383.9	E.C. Bott.			5.3	383.8
W.C. Bott.			5.5	383.6	" Top			4.68	384.39
" Top			4.73	384.34	3+50				
2+00					E.C. Top			4.37	384.70
W.C. Top			4.83	384.24	" Bott.			5.0	384.1
" Bott.			5.4	383.7	E/4			4.2	384.9
W/4			5.1	384.0	☐			4.0	385.1
☐			4.9	384.2	W/4			4.0	385.1
E/4			5.2	383.9	W.C. Bott.			4.6	384.5
					" Top			3.92	385.15

STA	+	H.I.	-	E.I.
4+00		389.07		
W.C. Top			3.54	385.53
" Bott.			4.2	384.9
W ¹ / ₄			3.9	385.2
☐			3.7	385.4
E ¹ / ₄			4.0	385.1
E.C. Bott.			4.4	384.7
" Top			3.80	385.27

4+50				
E.C. Top			3.41	385.66
" Bott.			4.2	384.9
E ¹ / ₄			3.7	385.4
☐			3.4	385.7
W ¹ / ₄			3.6	385.5
W.C. Bott.			3.9	385.2
" Top			3.25	385.82

5+00				
W.C. Top			2.85	386.22
" Bott.			3.4	385.7
W ¹ / ₄			3.3	385.8
☐			3.1	386.0
E ¹ / ₄			3.3	385.8
E.C. Bott.			3.8	385.3
" Top			3.20	385.87

STA	+	H.I.	-	Elev.
5+50		389.07		
E.C. Top			2.90	386.17
" Bott.			3.5	385.6
E ¹ / ₄			3.0	386.1
☐			2.8	386.3
W ¹ / ₄			2.9	386.2
W.C. Bott.			3.2	385.9
" Top			2.52	386.55

6+00 ⁸⁵				S.L. Monroe
W.C. Top			2.16	386.91
" Bott.			2.7	386.4
W ¹ / ₄			2.7	386.4
☐			2.5	386.6
E ¹ / ₄			2.6	386.5
E.C. Bott.			2.8	386.5
" Top			2.58	386.49

			3.24	389.73
6+00				W.C. Top N.L. Monroe
W.C. Top			3.24	386.49
" Bott.			3.70	386.03
W ¹ / ₄			3.7	386.0
☐			3.5	386.2
E ¹ / ₄			3.6	386.1
E.C. Bott.			3.9	385.8
" Top			3.61	386.12

STA.	+	H.I.	-	Elev.
0+50		389.73		
E.C. Top			3.86	385.87
" Bott.			4.3	385.4
E'4			4.0	385.7
☼			3.6	386.1
W'4			4.0	385.7
W.C. Bott.			4.4	385.3
" Top			3.66	386.07
1+00				
W.C. Top			3.94	385.79
" Bott.			4.8	384.9
W'4			4.3	385.4
☼			4.0	385.7
E'4			4.3	385.4
E.C. Bott.			4.5	385.2
" Top			4.11	385.62
1+50				
E.C. Top			4.35	385.38
" Bott.			5.0	384.7
E'4			4.6	385.1
☼			4.4	385.3
W'4			4.5	385.2
W.C. Bott.			4.9	384.8
" Top			4.26	385.47

STA.	+	H.I.	-	Elev.
2+00		389.73		38
W.C. Top			4.52	385.21
" Bott.			5.2	384.5
W'4			4.6	385.1
☼			4.5	385.2
E'4			4.8	384.9
E.C. Bott.			5.1	384.6
" Top			4.52	385.21
2+50				
E.C. Top			4.68	385.05
" Bott.			5.1	384.6
E'4			4.9	384.7
☼			4.6	385.1
W'4			4.8	384.9
W.C. Bott.			5.4	384.3
" Top			4.65	385.08
3+00				
W.C. Top			4.86	384.87
" Bott.			5.4	384.3
W'4			5.0	384.7
☼			4.7	385.0
E'4			5.0	384.7
E.C. Bott.			5.4	384.3
" Top			4.84	384.89
T.P.			4.86	384.87

STA.	+	H.I.	-	Elev.	STA.	+	H.I.	-	Elev.
	4.0 ^v	388.89			S+00		388.89		
3+50					W.C. Top			4.88	384.01
E.C. Top			4.0 ^v	384.87	" Bott.			5.4	383.5
" Bott.			4.6	384.3	W/4			5.0	383.9
E'4			4.2	384.7	ϕ			4.6	384.3
ϕ			4.0	384.9	E'4			4.7	384.2
W'4			4.2	384.7	E.C. Bott.			5.0	383.9
W.C. Bott.			4.7	384.2	" Top			4.62	384.27
" Top			4.10	384.79	S+50				
4+00					E.C. Top			4.69	384.20
W.C. Top			4.44	384.45	" Bott.			5.3	383.6
" Bott.			5.0	383.9	E'4			5.0	383.9
W'4			4.6	384.3	ϕ			4.8	384.1
ϕ			4.4	384.5	W'4			5.2	383.7
E'4			4.5	384.4	W.C. Bott.			5.4	383.5
E.C. Bott.			4.6	384.3	" Top			5.09	383.80
" Top			4.33	384.56	6+00				
4+50					W.C. Top			5.26	383.63
E.C. Top			4.5 ^v	384.37	" Bott.			5.6	383.3
" Bott.			5.1	383.8	+10			5.4	383.5
E'4			4.7	384.2	+20			4.95	383.94
ϕ			4.5	384.4	+30			4.85	384.04
W'4			4.8	384.1	+40			4.85	384.04
W.C. Bott.			5.2	383.7	+50			4.9	384.0
" Top			4.65	384.24	+60			5.0	383.9

STA.	+	H.I.	-	Elev.	
+70		388.89	5.0	383.89	
+80			5.15	383.74	
+90			5.4	383.49	
+100			5.8	383.09	
+ 108	Bot. Curb	NE. Curb	Mission Drive	6.05	382.84
	Top	"	"	5.53	383.36
G+42 ⁷⁰	S.L. Madison				
W.C. Top			5.29	383.60	
" Bot.			5.3	383.59	
+10			5.15	383.74	
+20			5.15	383.74	
+30			5.2	383.7	
+40			5.2	383.7	
+50			5.1	383.8	
+60			5.3	383.6	
+70			5.65	383.24	
+80			6.05	382.84	
+ 83 ⁵⁰	Bot. NE. Curb	Mission Drive	6.25	382.64	
	Top	"	"	5.83	383.06

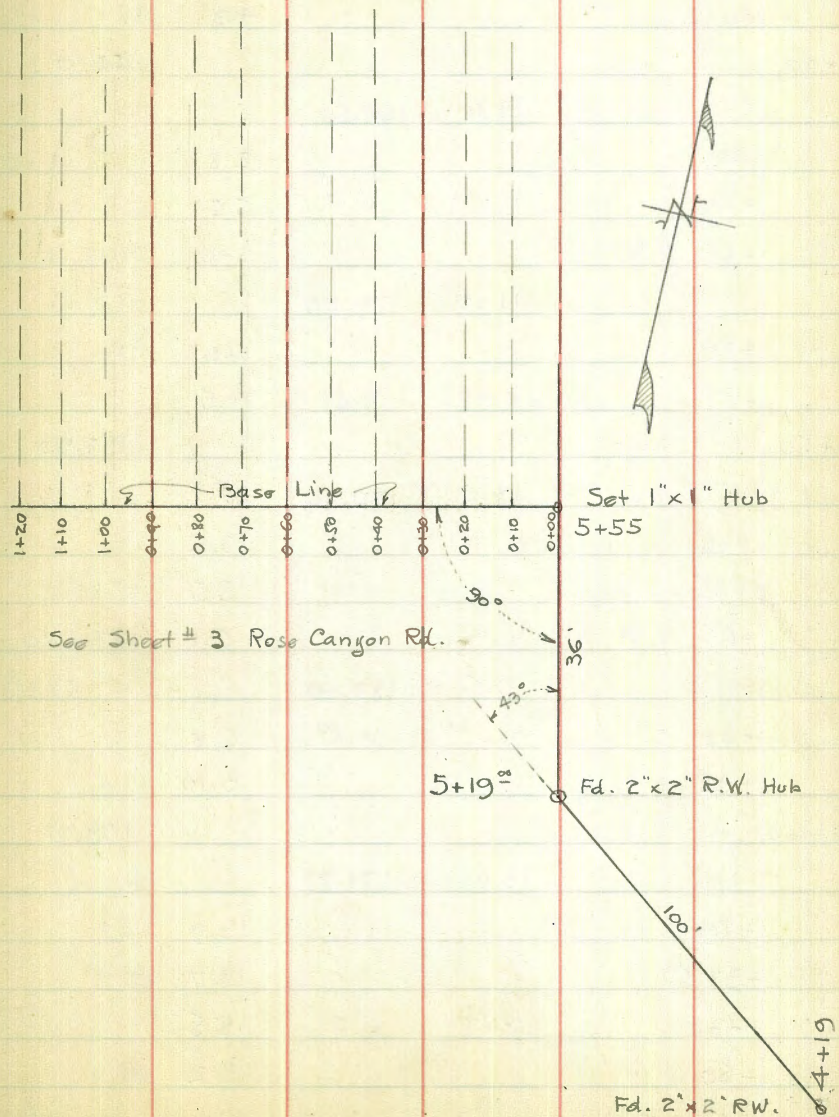
X - Sections of Quarry on Rose Canyon Rd.

JAEGER }
Bailey }
Claret }

May 24th 1928

41

STA	+	H.I.	-	Elev.
B.M. Spike in Pole # 4213				152.64
	6.81	159.45		
5+55 = 0+00 on Base Line			4.07	155.38
0+10	"		3.47	155.98
0+20			3.27	156.18
0+50			1.55	157.90
	6.94	164.84		
0+30			8.21	156.63
0+40			8.34	156.50
0+60			6.07	158.77
0+70			5.08	159.76
0+80			4.52	160.32
0+90			3.51	161.33
1+00			2.43	162.41
0+20	Base Line			156.18
	11.00	167.18		
+78			11.10	
+81			9.1	
+91			1.70	
0+30				156.63
	13.00	169.63		
+48			13.2	
+62			5.4	
+90			0.6	



STA	+	H.I.	-	Elev.	STA	+	H.I.	-	Elev.
	6.60					11.9	183.57		42 Elev.
+ 100			4.3		+78			7.0	
0+40				156.50	+93			3.6	
	13.0	169.50			+100			1.6	
+40			12.8		0+70				159.76
+49			5.5			7.0	166.76		
+65 T.P.			1.40	168.10	+18			7.0	
	11.10	179.20			+24			6.3	
+82			6.6		+32 T.P.			0.0	166.76
+97			4.5			13.0	179.76		
0+50				157.90	+46			6.8	
	13.0	170.90			+65 T.P.			0.4	179.36
+36			13.8		+6	12.5	191.86		
+45			5.5		+71			9.5	
+65 T.P.			0.1	170.80	+85			4.4	
	11.5	182.40			0+80				160.32
+83			6.8			13.10	173.42		
+92			3.10		+17			11.8	
0+60				158.77	+18			9.5	
	13.00	171.77			+23			11.2	
+29			13.9		+36			4.5	
+33.5			10.7		+39 T.P.			0.0	173.42
+43			8.5			12.6	186.02		
+50			3.2		+64			9.2	
+60 T.P.			0.1	171.67					

STA	+	H.I.	-	Elev.
+65			3.5	
+71			0.9	
0+90				161.33
	13.1	174.43		
+10			12.3	
+22			3.7	
+24			6.4	
+34			4.3	
+36 T.P.			1.1	173.33
	13.2	186.53		
+43			9.6	
+57			5.0	
+65			1.2	
1+00				162.41
	13.25	175.66		
+17			5.7	
+31 T.P.			0.0	175.66
	13.20	188.86		
+48			8.6	
+49			7.1	
+61			2.0	
				162.41
	13.25	175.66		
1+10			13.0	

STA	+	H.I.	-	
+6			11.5	
+26 T.P.			0.8	174.86
	12.5	187.36		
+39			7.6	
+40			6.3	
+49			2.4	
				162.41
	13.20	175.61		
			12.40	
			10.1	
			4.2	
			0.6	175.01
	12.70	187.71		
			10.4	
			7.1	
			0.9	

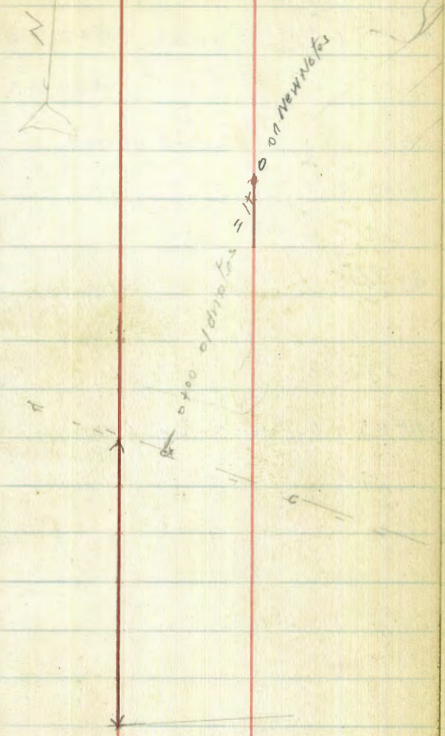
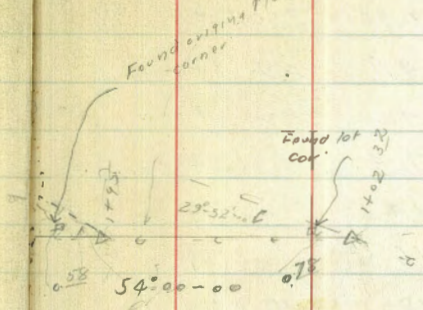
8/15
6/1/28
Location and Levels for Culvert on 55th St
North of El Cajon

BM 12.78 cut West of Meador St	H.I.	Elev
1118	437.45	423.27
T.P.	6.80	438.82
Set BM set top Fire Hydrant El Cajon = 56.72	2.43	432.02
T.P.	0.58	426.30
	1.12	437.70
	43.10	425.72

Line "A" = old line extended East.

0+00		6.2	420.1
0+10		8.1	418.2
0+33		11.0	415.3
0+45		12.6	413.7
T.P.	2.24	417.07	11.47
0+69		6.7	410.87
0+83		8.8	408.27
1+00 = 00 old notes		9.5	407.57
T.P.	1.16	405.70	12.53
1+28	old notes. West unchanged	5.1	400.6
1+32		5.1	400.6
1+35		7.4	398.3
1+54		9.4	396.3
1+70		10.2	395.7
1+85		11.3	394.4
1+89		11.3	394.4
1+95 Δ	54°00'-00" R.	9.6	396.1
2+05		11.4	394.3
2+07		12.3	393.4
2+25 End of line		12.8	392.9

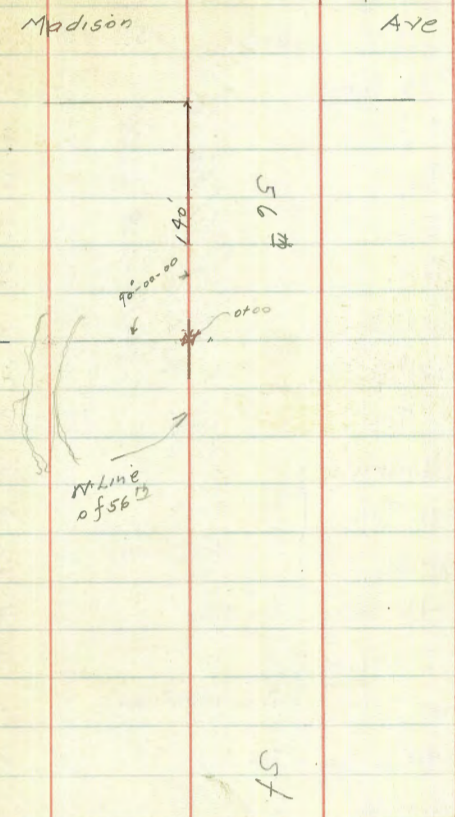
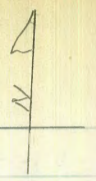
Sketch of Proposed Drain
Across 55th Between El Cajon
Blvd & Madison Ave.



8153
6/7/28

Location & Levels for Proposed Drain
crossing Lot 2 Block B Redlands Gardens West
of 56th St Between El Cajon & Madison

BM. SE Top Hydrot 56 th El Cajon	10.49	448.19		437.70
T.P.	2.27	441.69	8.77	439.42
0+00	on Hub flush with Ground		0.96	440.53
0+10			4.9	436.79
0+20			7.2	434.49
0+32			11.4	430.29
0+33			14.5	427.19
0+42			16.6	425.09
0+45	Bottom Natural Drain		18.2	423.49



X-Section Wightman St. from Herman to Boundary

JAEGER
Bailey
Clavert

July 14th 1928

352.40

46

STA	+	H.I.	-	Elev.
BM. B.P. SW. Wightman & 32 nd				346.40
	6.00	352.40		
0+00 E.L. Herman				
S. Curb Top			3.43	348.97
" Bott.			3.89	348.51
N. " Top			2.95	349.45
" Bott.			3.35	349.04
+50				
N. Curb Top			3.39	349.01
S. " Top			3.87	348.53
+95 W.L. Driveway				
N. Curb Top			4.44	347.96
+99 ⁸⁰ Apron &			5.05	347.35
1+04 ³⁰ E.L. Driveway			4.47	347.93
1+05 ⁵⁰ W.L. Driveway			3.90	348.50
1+15 ²⁰ Apron &			4.48	347.92
1+25 ⁸⁰ E.L. Driveway			4.22	348.18
1+25 ⁸⁰ W.L. Alley				
S. Curb Top			4.62	347.78
1+41 ³⁰ E.L. Alley				
S. Curb Top			4.82	347.78
N. " Top			4.44	347.96
1+44 ⁸⁰ W.L. Driveway			4.48	347.92
+49 ⁸⁰ Apron &			5.08	347.32
55 ³⁰ E.L. Driveway			4.53	347.87

Chkd as to E.L. grade
 on Profile
 7-19-28 CBH

STA	+	H.I.	-	Elev.
1+50 ⁶⁰ W.L. Driveway			4.91	347.49
1+57 ²⁰ Apron &			5.52	346.88
+63 ³⁰ E.L. Driveway			5.03	347.37
2+00				
S. Curb Top			5.36	347.04
N. " "			4.96	347.44
2+50				
S. Curb Top			5.86	346.54
N. " "			5.40	347.00
2+67 ²⁰ W.L. 32 nd				
S. Curb Top			5.88	346.52
" Bott.			6.47	345.93
N. " Top			5.47	346.93
" Bott.			6.07	346.33
0+00 E.L. 32 nd				
S. Curb Top			6.43	345.97
" Bott.			6.78	345.62
N. " Top			5.83	346.57
" Bott.			6.38	346.02
+50				
S. Curb Top			6.63	345.77
N. Curb Top			6.09	346.31

S.L.
 Wightman

STA	+	H.I.	-	Elev.
0+68 ²⁰	W.L. Driveway	Curb Top	6.69	345.71
+74 ²⁰	Apron	♀	S.L. Wightman	7.37
+80 ⁸⁰	E.L.	" " "		6.75
0+85 ⁵⁰	W.L. Driveway	Curb Top		6.21
+91 ⁰⁰	Apron	♀	N.L. Wightman	6.82
+97 ⁵⁰	E.L.	" " "		6.24
1+00				
	S. Curb Top		6.84	345.56
	N. " Top		6.27	346.13
1+25	W.L. Alley			
	S. Curb Top		6.85	345.55
	N. " Top		6.33	346.07
1+40	E.L. Alley			
	S. Curb Top		6.85	345.55
	N. " Top		6.47	345.93
1+45	W.L. Driveway	Curb Top	6.98	345.42
+50 ⁶⁰	Apron	♀	S.L. Wightman	7.61
+55 ⁸⁰	E.L. Driveway	" " "		7.03
2+00				
	S. Curb Top		7.22	345.18
	N. " Top		6.80	345.60
2+50				
	S. Curb Top		7.43	344.97
	N. " Top		6.91	345.49

STA	+	H.I.	-	Elev.
2+65 ²⁵	W.L. Bancroft			
	S. Curb Top		7.43	344.97
	" Bott.		7.96	344.44
	N. " Top		6.95	345.45
	" Bott.		7.46	344.94
	T.P.		7.26	345.14
		2.36		347.50
0+00	E.L. Bancroft			
	S. Curb Top		2.55	344.95
	" Bott.		2.96	344.54
	N. " Top		2.07	345.43
	" Bott.		2.61	344.89
+50				
	S. Curb Top		2.87	344.63
	N. " Top		2.68	344.82
0+63 ⁰⁰	W.L. Driveway	Curb Top	2.86	344.64
+67 ⁰⁰	Apron	♀	N.L. Wightman	3.51
+72 ³⁰	E.L. Driveway	Curb Top		2.97
+76 ⁰⁰	W.L.	" " "	N.L. Wightman	2.98
+81 ⁹⁰	Apron	♀		3.68
+87 ⁸⁰	E.L.	" " "		3.26
+76 ⁷⁰	W.L.	" " "	S.L. Wightman	3.05
+82 ⁰⁰	Apron	♀		3.74
+86 ²⁰	E.L.	" " "		3.25

352.40

352.40

47

Elev.

STA	+	H.I.	-	Elev.	STA	+	H.I.	-	Elev.
		347.50							48
1+00									
S. Curb Top			3.74	343.76	T.P.			1.95	335.52
N. " Top			3.86	343.64		11.78	347.30		
1+25 W.L. Alleg					T.P.			2.15	345.15
S. Curb Top			4.42	343.08		5.25	350.40		
N. " "			4.83	342.67	B.M. SW. Wightman & 32nd			3.99	346.41
1+40 E.L. Alleg									
S. Curb Top			4.96	342.54					
N. " Top			5.36	342.14					
1+50									
S. Curb Top			5.90	341.60					
N. " Top			6.19	341.31					
2+00									
S. Curb Top			11.59	335.91					
N. " Top			12.04	335.46					
T.P.			11.98	335.50					
	1.95	337.47							
2+50									
S. Curb Top			7.31	330.16					
N. " Top			7.70	329.77					
2+66 W.L. Boundary									
S. Curb Top			9.09	328.38					
N. " Top			9.60	327.87					

80' wide
14' cbs

Polk Ave X Sec Idaho to Boundary 7-23-28
miller

					373.77			
					220' E			
B.M. B.P.	3.81	373.77	369.96	se. Idaho & Polk	s. cl	5.19	368.58	49
		00 = E. Line Idaho Paved			N. cl	4.83	368.84	
s. cl		3.78	369.99	Top cl		235' E		
" "		4.33	369.44	pavmt	N. cl	4.90	368.87	
¢		3.85	369.92	"	s. cl	5.26	368.51	
N. cl		4.26	369.51	pavmt		250' E		
" "		3.72	370.05	Top cl	s. cl	5.37	368.40	
		50' E			N. cl	5.03	368.74	
N. cl		3.86	369.91			280' E		
s. cl		4.11	369.66		N. cl	5.27	368.50	
		100' E			s. cl	5.52	368.25	
s. cl		4.37	369.40			300' E = W. Line Utah Paved		
N. cl		4.14	369.61		s. cl	5.70	368.07	
		140' E = N. Alley			s. gutter	6.06	367.71	pavmt
N. Line		4.09	369.68	Alley Ret	¢	5.49	368.28	"
N. cl		4.35	369.42		N. gutter	5.84	367.93	"
s. cl		4.63	369.14		N. cl	5.29	368.48	
S. Line		4.36	369.41	Alley Ret	In block bet. Idaho + Utah cont. Curbs including Alley Returns are in on both sides. 5' cont. Walk 5' from curb face in on N.			
		160' E = E. Alley			entire BIK. No walk on S.			
s. Line		4.69	369.08	Alley Ret	00 = E. Line Utah.			
s. cl		4.78	368.99					
N. cl		4.44	369.33		N. cl	5.15	368.62	
N. Line		4.31	369.46	Alley Ret	N. gutter	5.76	368.81	pavmt
		200' E			¢	5.41	368.36	"
N. cl		4.57	369.20		s. gutter	6.12	367.65	"
s. cl		4.96	368.81		s. cl	5.61	368.16	

373.77

373.34
300' E = W Line Kansas ST. Paved

50

T.P.	5.04	373.34	5.47	368.30
		45' E		
S. cl			4.96	368.38
N. cl			4.73	368.61
		100' E		
N. cl			4.64	368.70
S. cl			4.77	368.57
		140' E = W. Line Alley		
S. Line			4.49	368.85 Alley Ret
S. cl			4.83	368.51
N. cl			4.49	368.85
N. Line			4.38	368.96 Alley Ret
		160' E = E. Line Alley		
N. Line			4.36	368.98 Alley Ret
N. cl			4.43	368.91
S. cl			4.54	368.80
S. Line			4.42	368.92 Alley Ret
		174' E		
S. cl			4.62	368.72
N. cl			4.40	368.94
		200' E		
N. cl			4.50	368.84
S. cl			4.56	368.78
		250' E		
S. cl			4.44	368.90
N. cl			4.37	368.97

N. cl			4.35	369.01
N gutter			4.70	368.64 pavmt
⊕			4.50	368.84 "
S. gutter			4.71	368.63 "
S. cl			4.21	367.13
		314' Bet Utah & Kansas cmt. curb, walks		
		Returns + curb returns all in 5' walk - 5' from curb face		
		00 = E. Line Kansas		
S. cl			4.24	369.06
S. gutter			4.92	368.42
⊕			4.32	369.02
N. gutter			4.92	368.42
N. cl			4.31	369.03
		50' E		
N. cl			5.10	368.24
S. cl			5.24	368.10
T.P.	2.96	370.92	5.38	367.96
		107' E		
S. cl			3.74	367.18
N. cl			3.59	367.33
		140' E = W. Alley		
N. Line			4.00	366.92 Alley Ret
N. cl			4.06	366.86
S. cl			4.31	366.61
S. Line			4.14	366.78

370.92
160'E = E. Line Alley

S. Line 4.64 366.28 Alley Ret

S. cl 4.75 366.17

N. cl 4.55 366.34

N. Line 4.32 366.60 Alley Ret

-200'E

N. cl 5.31 365.61

S. cl 5.52 365.40

250'E

S. cl 6.35 364.57

N. cl 5.98 364.94

300'E = W. Line 30th St (Paved.)

N. cl 6.89 364.03

N. gutter 7.59 363.33

⊥ 7.37 363.55

S. gutter 7.89 363.03

S. cl 7.31 363.61

All cont. ed. walk Returns + Alley Ret. Bk. Kansas to 30th St.
5' walk 45' front Race Cup

T.P. 3.08 368.72 5.28 365.64

00 = E. Line 30th St.

S. cl 5.68 363.04

S. gutter 6.16 362.56 pavmt

N. " 5.87 362.85 "

N. cl 5.24 363.48

50'E

N. cl 4.82 363.90

S. cl 5.22 363.50

368.72
100'E

S. cl 4.82 363.90

N. cl 4.80 364.22

140'E = W. Alley

N. Line 4.02 364.70

N. cl 4.26 364.46

S. cl 4.55 364.17

S. Line 4.50 364.22

" " Alley Pavmt 5.01 363.72

S. Line Alley Pavmt 160'E = E. Alley 4.90 363.82

S. Line 4.21 364.51

S. cl 4.29 364.43

N. cl 4.04 364.68

N. Line 3.82 364.90

200'E

N. cl 3.76 364.96

S. cl 4.05 364.67

250'E

S. cl 3.58 365.14

S. cl 3.45 365.27

300'E = W. Line 30th St (Paved)

N. cl 3.15 365.57

N. gutter 3.76 364.96 pavmt

⊥ 3.03 365.69 "

S. gutter 3.63 365.09 "

S. cl 3.24 365.46

368.72

T.P. RM 5.60

371.58

2.74

365.98

Polk & Ohio

S. cl

4.83

366.75

Polk Ave

52

00 = E. line Ohio

N. cl

4.73

366.85

S. cl

5.52

366.07

300' E = W. line Illinois (Paved)

S. gutter

5.95

365.63

N. cl

4.59

366.99

♀

5.29

366.29

N. gutter

5.02

366.56

Paymt

N. gutter

5.94

365.64

♀

4.38

367.20

"

N. cl

5.63

366.09

S. gutter

5.04

366.54

"

50' E

S. cl

4.60

366.98

N. cl

5.41

366.17

B/K Bet Ohio & Illinois ent walk, cl, Returns

S. cl

5.29

366.29

& Alley Returns in 5' walks 45' from face cl.

100' E

00 = E. line Illinois

S. cl

5.14

366.44

S. cl

5.14

366.44

N. cl

5.22

366.36

S. gutter

5.61

365.97

Paymt

140' E = W. Alley

♀

4.88

366.70

N. line

4.95

366.63

Alley Ret

N. gutter

5.62

365.96

N. cl

5.10

366.48

N. cl

5.15

366.43

S. cl

5.11

366.47

T.P.

1.72

367.56

5.74

365.84

S. line

4.64

366.90

Alley Ret

50' E

S. " Alley Pavmt

4.82

366.76

N. cl

2.75

364.81

S. line Alley Pavmt

160' E = E. Alley

4.83

366.75

S. cl

2.53

365.03

S. line Alley Ret

4.73

366.85

Alley Ret

S. cl

4.93

366.65

100' E

N. cl

5.07

366.51

S. cl

4.00

363.56

N. line

4.85

366.73

N. cl

4.30

363.26

200' E

N. cl

4.92

366.66

S. cl

4.97

366.71

367.56
140' E = W. Line Alley

N. Line	5.34	362.20	Alley Ret
N. "	5.97	361.59	" Pavmt
N. cl	5.47	362.09	
S. cl	5.05	362.51	
S. Line	4.85	362.71	Alley Ret
" "	5.14	362.42	" Pavmt

160' E = E. Line Alley

S. Line	5.45	362.11	Alley Pavmt
" "	5.33	362.23	" Ret
S. cl	5.63	361.93	
N. cl	6.16	361.40	
N. Line	5.87	361.69	Alley Ret
" "	6.33	361.23	" Pavmt

200' E.

N. cl	7.46	360.10	
S. cl	6.80	360.76	

250' E

S. cl	8.20	359.36	
N. cl	9.04	358.52	

300' E = W. Line Iowa (Paved)

N. cl	10.61	356.95	
N. gutter	10.96	356.60	
φ	10.08	357.48	
S. gutter	10.06	357.50	
S. cl	9.58	357.98	

BK bet Illinois + Iowa cmt cl - Returns - Alley Returns All in
5' cmt walk 4.5' from cl. in on N. + E. 140' on S. 140' on S. N. in

353.04 SE Polk + 32

367.56

Polk Ave

T.P.	2.70	359.73	10.53	357.03
T.P. on B.M. B.P.	2.06	355.16	6.63	353.10

BK bet Iowa + 32nd curbed, walk + Paved.

00 = E. Line 32nd (Intersection Paved)

S. cl	2.00	
S. gutter	2.62	Pavmt

φ 2.10

N. gutter	2.83
-----------	------

N. cl	2.16
-------	------

50' E

N. cl	4.75
-------	------

S. cl	4.20
-------	------

90' E.

S. cl	6.03
-------	------

N. cl	7.03
-------	------

116.7 E = W. end C.B. Opening P.C. Return

N. cl	7.99	Top cl.
-------	------	---------

N. gutter	9.02	Q.B. inlet
-----------	------	------------

135' E = P.T. S. cl Polk + W. Line Boundary

S. cl	8.00
-------	------

141.6 E = W. end C.B. Opening

S. cl	8.06	Top cl
-------	------	--------

S. gutter	9.04
-----------	------

119.5 E. on N. cl. Polk = W. Line Boundary

N. cl	8.01
-------	------

In BK bet. 32nd + Boundary cmt. Walk + cl. all in.

53

SE Polk

353.04 + 32nd

8-25-28
 J. C. Bliss
 Drebert
 Pauner

X section 33rd St. Ash St.
 To A St. 60' wide
 10' cbs
 10' 1/2"

B. M. N. E. Mon. 33rd & Ash

192.85

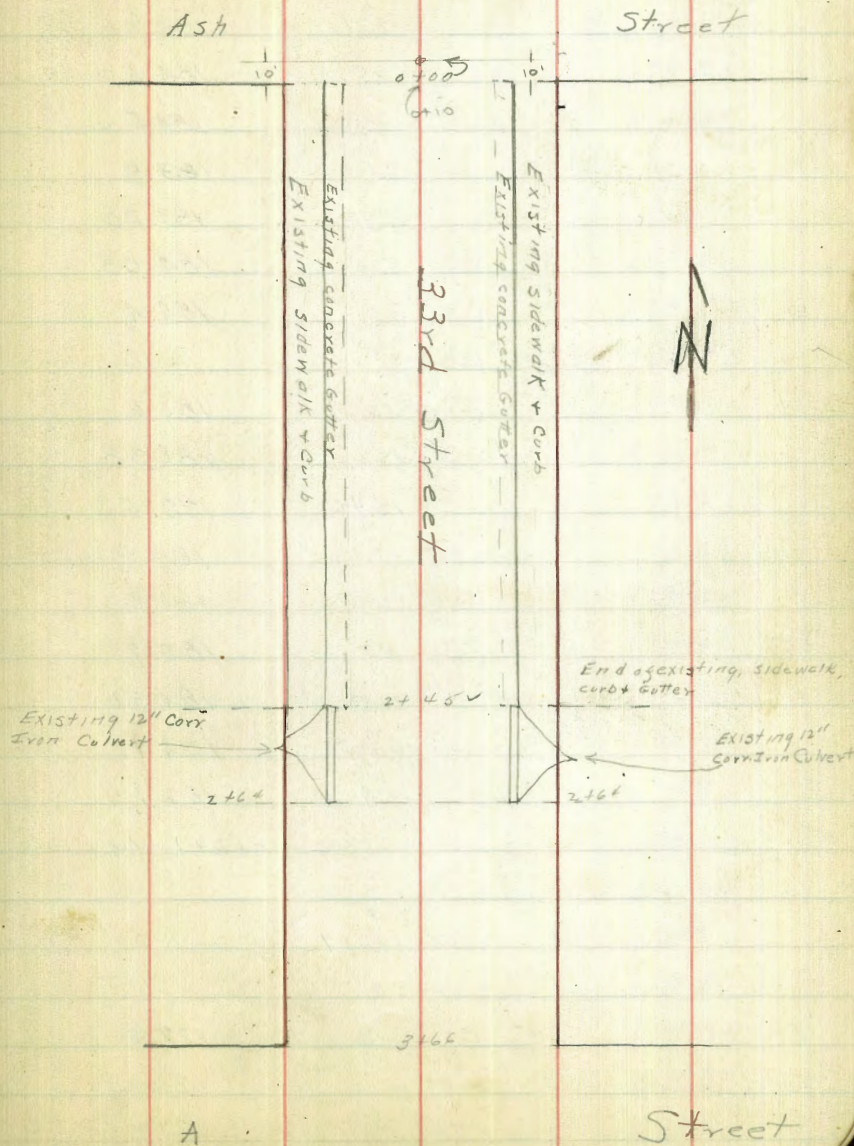
+018.

+193.03
 10' N of S Line Ash
 0+60 = South Line Ash St.

E	47	188.3
Tree	5.01	185.02
Concrete Gutter	5.71	187.32
1/4"	5.4	187.6
&	5.5	187.5
1/4"	6.2	186.8
Concrete Gutter	6.81	186.32
Tree	6.00	187.03
W	5.8	187.2
	0+10 = S.L. Ash.	
W	5.8	187.2
Tree	6.00	187.03
Con. G.	6.97	186.06
1/4"	6.6	186.4
&	5.8	187.2
1/4"	5.8	187.2
Con. Gut.	5.82	187.21
Tree	5.01	188.02
E	4.9	188.1
	0+50	
E	7.9	185.1

Platted 8-31-28
 C.B.H.

54



π 19303

Tp cb	8.05	184.98
Con Gut.	8.87	184.06
1/4	8.5	184.5
⊥	8.5	184.5
1/2	9.1	183.9
Con Gut.	9.83	183.20
Tpcb	8.95	184.08
W	8.6	184.4
1400		
W	12.4	180.6
Tpcb	12.65	180.38
Con Gut	13.46	179.57
1/4	12.7	180.3
⊥	12.0	181.0
1/4	12.3	180.7
Con Gut.	12.75	180.30
Tpcb	11.92	181.11
E	11.9	182.1
T.P.		-12.77 180.26
+0.41		
π 180.67		
1450		
E	3.2	177.5
Con Gutter-Downward	4.32	176.35
1/4	3.7	177.0

π 180.67

55

⊥	3.4	177.3
1/4	4.1	176.6
Con Gut.	4.83	175.84
Tpcb	4.02	176.65
W	3.6	177.1
2400		
W	7.3	173.4
Tpcb	7.68	172.99
Con Gut.	8.43	172.24
1/4	7.7	173.0
⊥	7.2	173.5
1/4	7.4	173.3
Con Gut.	8.05	172.62
Tpcb	7.22	173.45
E	7.0	173.7
2445 on West + 2445 on East = Endog. existing cb. + Gutter		
E	10.5	170.2
Tpcb	10.73	169.94
Gutter's Flowline of 12" Corr Iron Culvert	12.85	168.32
1/4	10.6	170.1
⊥	11.0	169.7
1/4	10.9	169.8
Gutter's Flowline of 12" Corr Iron Culvert	12.79	167.88
Tpcb	11.06	169.61
W	10.6	170.1

$\pi 180.67$

168.16

56

T	T.P.		-12.61	168.06	1/4	10.0	158.2
	+0.10				cb	9.6	158.6
		$\pi 168.16$			E	9.3	158.9
		2+50					
		0.0	168.2			3+00	
		1.8	166.4	E	11.5		156.6
		0.1	168.0	cb	12.9		155.3
		0.0	166.2	1/4	12.3		155.9
		0.4	167.8	2	13.2		155.0
		1.4	166.8	+2	13.9		154.3
		2.0	166.2	+3	11.9		156.3
		0.5	167.7	1/4	9.0		159.2
		2+64		cb	6.8		161.4
		7.1	161.1	W	5.0		163.2
		7.60	160.56			3+25	
		6.9	161.3	W	7.1		161.1
		4.6	160.6	cb	8.9		159.3
		7.1	161.1	1/4	10.1		158.1
		7.80	160.36	2	13.0		155.2
		4.7	163.5	T.P.			-13.18 154.98
		2+75				15.77	
		4.2	164.0			$\pi 160.75$	
		8.1	160.1	+6	8.1		152.6
		9.0	159.2	1/4	8.0		152.7
		10.9	157.3	cb	8.5		152.2
		10.6	157.6	+8	8.0		152.7

160.75

57

E 64 154.3

3+50

E 10.7 150.0

C6 11.3 149.4

+3 13.2 147.5

114 8.6 152.1

E 7.1 153.6

114 4.6 156.1

C6 3.0 157.7

W 1.4 159.3

3+66 = North line A St.

W 2.5 158.2

C6 4.3 156.4

114 6.4 154.3

E 8.6 152.1

114 10.0 150.7

C6 14.2 146.5

+4 13.0 147.7

E 11.6 149.1

F.P. Rock on A St Near West Curb -6.25 154.50

T.P. -0.79 159.96

+12.96 172.92

-0.14 172.78

+13.12 185.90

-1.51 184.39

+889 193.28

B.M. N.E. Mo. Ash + 33 yd.

-0.43 192.85

192.85

8-27-28 Cross-section of A Street
 J.C. Bliss 80' wide
 Brebert 14' cbs
 Rauner 13' 1/2"

179.32

58

B.M. S.W.B.P. Edgemont & A.	22.737	cb	8.7	170.6
+1.62	228.77	S	10.5	168.8
T.P.	-12.99	216.00	W 1/4 32nd St	
+0.21	216.21	S	12.0	167.3
T.P.	-13.13	203.09	cb	11.4
+1.16	204.24	1/4	11.1	168.2
T.P.	-13.17	191.07	♀	12.0
+0.64	191.71	T.P.		167.3
T.P.	-12.68	179.03	+5.84	-13.11
+0.29	179.32			166.21
	T 179.32		T 172.05	
West Line 32nd Street	60' wide	1/4	6.8	165.2
	10' cbs	cb	8.4	163.6
S	7.3	172.3	N	10.4
cb	6.0	173.3	♀ 32nd St.	
1/4	6.0	173.3	N	13.2
♀	6.6	172.7	cb	10.8
1/4	7.6	171.7	1/4	9.8
cb	9.0	170.3	♀	8.2
N	11.0	168.3	1/4	6.8
West cb 32nd St.		cb	5.9	165.2
N	14.9	164.4	S	5.7
cb	13.0	166.3	East 1/4 32nd	
1/4	11.8	167.5	S	8.7
♀	10.8	168.5	cb	10.1
1/4	8.9	170.4	1/4	11.2
				163.3
				161.9
				160.8

Plotted 9-1-28
C.B.H.

172.05

Q	12.5	159.5
1/4	14.2	157.8
cb	14.3	157.7
N	17.3	154.7
E C b 32nd St		
N	20.2	151.8
cb	18.4	153.6
1/4	16.9	155.1
Q	16.2	155.8
1/4	15.8	156.2
cb	14.0	158.0
4 9	12.6	159.4
S	8.6	163.4
E Line 32nd St. = 0+00		
S	11.4	160.6
T.P.		-13.16 158.89
+0.22		
159.11		
+10	4.3	154.8
cb	4.7	154.4
1/4	4.8	154.3
Q	6.3	152.8
1/4	7.7	151.4
cb	7.0	150.1
N	9.4	149.7

159.11

59

0+25		
N	14.5	144.6
cb	14.5	144.6
1/4	14.3	144.8
Q	14.0	145.1
1/4	13.5	145.6
cb	13.2	145.9
S	12.2	146.9
T.P.		-12.53 146.58
+0.28		
146.86		
0+50		
S	5.3	141.5
cb	5.4	141.4
1/4	6.6	140.2
Q	6.9	140.0
1/4	6.8	140.0
cb	6.6	140.2
1	6.6	140.2
0+75		
N	9.4	137.5
cb	9.7	137.2
1/4	10.1	136.8
Q	10.4	136.4
1/4	10.7	136.1
cb	10.5	136.3

π 146.86

S	10.5	136.3
		-13.01 133.85

+0.22

π 137.07

1400

S	2.2	131.9
cb	2.7	131.4
114	2.3	131.8
♀	1.3	132.8
114	0.5	133.6
cb	0.0	134.1
N	0.0	134.1
Out 20	6.5	127.6
N	6.8	127.3
cb	5.5	128.6
114	6.5	127.6
♀	7.0	127.1
114	7.4	126.7
cb	8.0	126.1
S	8.4	125.7
Out 20	9.4	124.7
	1450	
Out 20	12.6	121.5
S	12.4	121.7
cb	11.8	122.3

π 134.07

60

114	10.5	123.6
♀	9.5	124.6
114	9.2	124.9
cb	9.3	124.8
N	9.3	124.8
Out 20	8.4	125.7
	1454	
Out 20	8.7	125.4
N	9.2	124.9
cb	10.3	123.8
114	10.3	123.8
♀	10.1	124.0
114	11.8	122.3
+1	14.8	119.3
cb	14.9	119.2
S	15.0	119.1
Out 20	15.5	118.6
	1467	
Out 20	11.8	122.3
S	11.2	122.9
cb	11.1	123.0
114	11.0	123.1
♀	11.0	123.1
114	10.8	123.3
cb	11.3	122.8

134.07

+1	13.4	120.7
N	13.2	120.9
out 9	13.0	121.1
Out 4	10.9	123.2
Out 20	10.1	124.0

1+65 on ϕ of A St. Man Held 1.8.16

Shot on Flowline 16.91

Line of levels for culvert in Natural Drain

crossing the North Line of A at 1+67 and the South Line

at 1+54 0+00 of drain levels = 15' North of North Line

0+00	12.6
0+15 - North Line	13.3
0+48	13.4
0+55	12.4
0+70	12.9
0+80	14.5
0+97 = South Line	15.0
1+12	15.4

1+75

Out 20	12.5	121.6
0+16	12.9	121.2
Out 15	10.8	123.3
N	10.0	124.1
cb	9.8	124.3
1+4	10.1	124.0

134.07

61

ϕ	10.5	123.6
1+4	10.6	123.5
cb	11.1	123.0
S	11.5	122.6
Out 20	12.1	122.0

2+00

Out 20	11.6	122.5
--------	------	-------

S	11.6	122.5
---	------	-------

cb	11.2	122.9
----	------	-------

1+4	10.7	123.4
-----	------	-------

ϕ	9.9	124.2
--------	-----	-------

1+4	9.8	124.3
-----	-----	-------

cb	9.1	125.0
----	-----	-------

N	7.7	126.4
---	-----	-------

Out 20	6.3	127.8
--------	-----	-------

2+25

Out 20	6.4	133.7
--------	-----	-------

N	2.2	131.9
---	-----	-------

cb	4.9	129.2
----	-----	-------

1+4	6.7	127.4
-----	-----	-------

ϕ	7.8	126.3
--------	-----	-------

1+4	8.1	126.0
-----	-----	-------

cb	8.8	125.3
----	-----	-------

S	8.2	125.9
---	-----	-------

Out 20	7.3	126.8
--------	-----	-------

X 13407

2+34 = Man Hole on E of Ast.

Shot on Floorline 1046 123.61
T.P. - 0.20 133.81

+1322

X 148.09

²⁺⁵⁰
10.5

136.6

Out 20

S

10.0

137.1

cb

10.7

136.4

14

10.9

136.2

+7.79

Q

10.8

136.3

14

9.0

138.1

cb

6.8

140.3

N

4.2

142.9

Out 20

4.0

143.1

T.P.

-0.09 147.00

+1240

X 159.40

²⁺¹⁵
6.7

152.7

N

7.4

152.0

cb

8.7

150.7

14

10.4

149.0

Q

12.7

146.7

14

15.4

144.0

cb

17.4

142.0

S

X 159.40

62

3+00

10.3

149.1

S

8.5

150.9

cb

7.0

152.4

14

Q

5.8

153.6

14

4.5

154.9

cb

3.0

156.4

N

1.7

157.7

-0.38 159.02

X 166.81

³⁺²⁵
6.1

160.7

N

6.9

159.9

cb

14

8.1

158.7

Q

9.1

157.7

14

10.2

156.6

cb

10.7

156.1

S

10.9

155.9

3+50

9.7

157.1

S

cb

8.7

158.1

14

7.7

159.1

Q

6.9

159.9

14

6.0

160.8

cb

5.0

161.8

N

3.9

162.9

T 166.81

3775

N	1.9	164.9
cb	3.3	163.5
1/4	4.5	162.3
¢	5.2	161.6
1/4	6.1	160.7
cb	7.2	159.6
S	7.8	159.0

4400

S	7.3	159.5
cb	6.3	160.5
1/4	5.4	161.4
¢	4.9	161.9
1/4	4.4	162.4
cb	3.1	163.7
N	1.9	164.9

4425

N	2.6	164.2
cb	4.1	162.7
1/4	5.2	161.6
¢	6.0	140.8
1/4	6.8	160.0
cb	7.5	159.3
S	7.6	159.2

T 166.81

4450

S	10.9	155.9
cb	9.7	156.9
1/4	9.0	157.8
¢	8.0	158.8
1/4	7.0	159.8
cb	5.4	161.4
N	4.1	162.7

4475

N	8.0	158.8
cb	10.4	156.4
1/4	12.3	154.5
¢	12.8	154.0
1/4	12.6	154.2
cb	12.9	153.9
S	13.6	153.2

T.P.

13.82 T 15 7.38

4484 = West Line 33rd North of A.

S	5.5	151.9
cb	4.6	152.8
1/4	5.0	152.4
¢	4.7	152.7
1/4	5.0	152.4
cb	3.2	154.2
N	0.0	157.4

T 15738

Check on T.P. at 33rd & A → -2.84 → 154.54
 → 154.50

4794 = West cb. 33rd st. N of A

N	1.0	156.4
cb	3.8	153.6
1/4	7.1	150.3
£	7.8	149.6
1/4	6.7	150.7
cb	7.0	150.4
S	7.3	150.1
Out 20	7.9	149.5

5104 = W. 1/4 33rd N of A

Out 20	9.5	147.9
S	8.4	149.0
cb	8.2	149.2
1/4	9.0	148.4
£	9.2	148.2
1/4	8.0	149.4
cb	4.7	152.7
N	2.9	154.5

5114 = £ of 33rd N of A

N	5.1	152.3
cb	7.0	150.4
1/4	10.1	147.3
+ 4	12.9	144.5

T 15738

1214
420

64

£	14.1	143.3
1/4	12.2	145.2
cb	12.1	145.3
S	12.0	145.4
Out 20	11.4	146.0

5119 = £ 33rd + S

Out 20	12.6	144.8
S	12.0	145.4
cb	12.7	144.7
1/6	14.4	143.0
1/4	14.8	142.6

£	13.9	143.5
+ 1	12.7	144.7
+ 9	11.3	146.1
+ 10	13.0	144.4
1/4	13.1	144.3
+ 3	10.5	146.9
cb	7.8	147.6
N	5.9	151.5

Manhole at Intersection of £ S of A + 33rd

On Flow Line 16.49

5124 = E 1/4 33rd st. N of A

N	6.4	151.0
cb	8.2	149.2
+ 6	9.8	147.6

π 157.38

+7	12.2	145.2
1/4	10.3	147.1
¢	11.1	146.3
1/4	12.1	145.3
+9	12.6	144.8
+10	15.1	142.3
cb	15.2	142.2
+4	13.3	144.1
5	14.3	143.1
Out 20	15.4	142.0

5+34 = ECB 33rd St. N of A

Out 20	15.0	142.4
5	12.2	145.2
cb	10.5	146.9
1/4	9.0	148.4
¢	8.0	149.4
1/4	7.8	149.6
+7	9.3	148.1
cb	10.0	147.4
+1	11.7	145.7
N	11.0	146.4

5+44 = E Line 33rd N of A

N	8.2	149.2
+20	7.7	149.7
cb	6.1	151.3

π 157.38

65

1/4	5.5	151.9
¢	6.4	151.0
1/4	7.7	149.7
cb	8.7	148.7
5	10.5	146.9
Out 20	12.2	145.2
5+75		
Out 20	5.3	152.1
5	4.6	152.8
cb	2.7	154.7
1/4	0.8	156.6

T.P.

-0.05 157.33

+ 11.45

π 168.78

¢	10.4	158.4
1/4	8.0	160.8
cb	6.3	162.5
X	6.2	162.6

6+00 = West Line 33rd South of A

N	16	167.2
cb	3.0	165.8
1/4	4.6	164.2
¢	6.3	162.5
1/4	8.3	160.5
cb	10.6	158.2

T 168.78

S 12.5 156.3
 T.R. -0.13 168.65

+11.08

T 179.73

East Line A St. South of A. St. = 0+00

S 15.0 164.7
 cb 12.4 167.3
 1/4 9.9 169.8
 ♀ 7.6 172.1
 1/4 5.4 174.3
 cb 3.5 176.2
 N 2.2 177.5

0+25

N 0.8 178.9
 cb 2.2 177.5
 1/4 3.7 176.0
 ♀ 5.4 174.3
 1/4 8.1 171.6
 cb 10.0 169.7
 S 14.2 165.5
 0+15 18.8 160.9

0+50

0+15 16.8 162.9
 S 13.9 165.8
 cb 10.2 169.5

T 179.13

1/4 7.8 171.9
 ♀ 5.5 174.2
 1/4 4.0 175.7
 cb 2.8 176.9
 N 1.9 177.8

Section in Bottom of Ditch that crosses A Line
 A at 0+50 and S Line at 0+75. Ditch is Approx.

4' wide and banks are level with each other

N-Top ^{1.6} 178.1
 Top ^{2.5} 177.4
 cb - Bottom ^{3.6} 176.1

Top Bank 2.7 177.0
 1/4 - Bottom 5.8 173.9
 - Top 4.3 175.4

+8 - Bottom 6.9 172.8
 Top 6.0 173.7

+9 Bottom 1.7 170.0
 Top 6.0 173.7

♀ Bottom 9.7 170.0
 Top 6.5 173.2

1/4 Bot 11.4 168.3
 Top 8.3 171.4

cb Bot 13.2 166.5
 Top 9.9 169.8

S Bot 14.5 165.2
 Top 11.7 168.0

66

π 179.73

0+75

0+15	13.0	166.7	
5	11.7	168.0	
cb	10.0	169.7	
14	8.3	171.4	
♀	5.3	174.4	
14	3.5	176.7	
cb	1.9	177.8	
N	0.7	179.0	
T.P.		-0.45	179.28

+1104

π 190.32

0+98

N	8.1	182.2	
+10	9.8	180.5	
+11	12.6	177.7	
+13	10.7	179.6	
cb	10.7	179.6	
14	12.1	178.2	
♀	13.3	177.0	
14	15.4	174.9	
cb	16.0	174.3	
5	18.6	171.7	

1+00

5	18.3	172.0	
cb	15.7	174.6	

π 190.32

67

14	15.0	175.3	
♀	13.0	177.3	
14	11.8	178.5	
cb	10.6	179.7	
+3	10.4	179.9	
+5	12.2	178.1	
N	10.1	180.2	

1+08

N	8.4	181.9	
cb	9.7	180.6	
14	11.3	179.0	
♀	11.6	178.7	
14	12.9	177.4	
cb	14.0	176.3	
5	15.5	174.8	

1+25

5	11.7	178.6	
cb	10.8	179.5	
14	10.0	180.3	
♀	8.9	181.4	
14	7.8	182.5	
cb	7.5	182.8	
N	6.1	184.2	

1+20 M.H. ♀ + 54

On Flowline	14.60	175.7	
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19032

1450

N	44	185.9
cb	51	185.7
114	53	185.0
¢	56	184.7
114	66	183.7
cb	78	182.5
S	92	181.1

1475

S	60	184.3
cb	53	185.0
114	48	185.5
¢	45	185.8
114	40	186.3
cb	30	187.3
N	34	186.9

2400

N	24	189.9
cb	28	189.5
114	16	188.7
¢	20	188.3
114	28	187.5
cb	35	186.8
S	42	186.1
J.P.		-1.40 188.92

1473

193.65

19365

2425

J	53	188.3
cb	45	189.2
114	41	187.6
¢	37	190.0
114	31	190.6
cb	25	191.2
N	23	191.3

2450

N	20	191.6
cb	25	191.2
114	30	190.7
¢	35	190.2
114	39	189.8
cb	41	189.6
S	45	189.1

2475

S	51	188.5
cb	49	
114	49	
¢	48	
114	45	
cb	41	
N	33	190.3

3400

N

6.2

187.4

68

∑ 193.65

cb	6.7	
114	7.5	
2	7.6	
114	7.8	
cb	7.5	
5	7.3	186.3

3+25

5	10.4	183.2
cb	11.2	
114	11.6	
2	11.1	
114	10.3	
cb	9.8	
1	9.2	184.4

3+50

1	12.8	180.8
cb	14.0	
114	14.7	
2	14.6	
114	14.5	
cb	14.2	
5	13.1	180.5

-13.02 180.63

T.P.

+1.37

∑ 182.00

∑ 182.00

69

3+75

5	4.9	177.1
cb	5.5	
114	5.7	
2	5.9	
114	6.6	
cb	5.4	
1	5.0	177.0

4+00

1	7.9	174.1
cb	8.8	
114	9.7	
2	9.5	
114	8.8	
cb	7.6	
5	6.6	175.4

4+25

5	9.1	172.9
cb	12.8	
114	12.8	
2	14.4	
114	14.9	
cb	13.9	
1	12.5	169.5

T.P.

+6.62

∑ 175.84

-12.78 169.22

17584

4450

X	13.3	162.5
cb	17.0	
1/4	15.6	
♀	12.3	
1/4	8.4	
cb	6.0	
S	4.0	171.8

4475

S	3.9	171.9
cb	7.3	
1/4	10.7	
♀	14.8	
1/4	18.1	
cb	21.0	
N	25.2	150.6
out 10	20.6	

5400

out 10	25.4	
N	28.0	147.8
cb	23.6	
1/4	20.0	
♀	15.3	
1/4	11.4	
cb	7.9	
S	4.1	171.7

17584

5425

S	5.1	170.7
cb	8.9	
1/4	12.2	
♀	15.5	
1/4	19.6	
cb	24.6	
N	28.4	147.4
out 10	31.4	
out 20	26.9	

5450

out 10	32.7	
N	35.0	140.8
cb	27.4	
1/4	22.3	
♀	17.6	
1/4	13.0	
cb	9.7	
S	6.5	169.3

5475

S	8.1	167.7
cb	11.7	
1/4	14.7	
♀	20.4	
1/4	25.0	
cb	29.8	

70

π 175.84

N	35.2	140.6
Out 10	38.1	
Out 20	34.4	
Out 20	39.2	
Out 10	42.0	
N	37.1	138.7
cb	32.0	
1/4	27.4	
⊕	22.5	
1/4	17.1	
cb	13.2	
S	9.5	166.3
S	10.2	165.6
cb	13.8	
1/4	17.7	
⊕	22.7	
1/4	28.0	
cb	33.1	
N	38.5	137.3
Out 15	45.0	
Out 25	42.0	
Out 30	45.3	

6 + 00 = West Line 34th

60' wide
10' 00"
10' 00"

West cb 34th

⊕ 34th

π 175.84

71

Out 20	49.9	
N	39.0	136.8
cb	33.6	
1/4	28.7	
⊕	24.0	
1/4	19.2	
cb	15.1	
S	11.3	164.5
S	12.5	163.3
cb	16.2	
1/4	20.4	
⊕	24.5	
1/4	29.8	
cb	35.9	
N	41.0	134.8
Out 20	51.3	
Out 30	47.6	
Out 30	50.1	
Out 20	53.0	
N	42.7	133.1
cb	37.9	
1/4	30.0	
⊕	25.4	

East cb. 34th

East Line 34th

117584

72

114		208		
Cb		167		
S.		144	161.4	
T.P.			-105	174.71
	+12.92	187.71		
			-1.09	186.62
	+12.68	199.30		
			-0.66	198.64
	+8.02	206.66		
B.M. Felton & Ash			-4.59	202.07
				201.99

Walker
Ruppinger
Stack
book
10-15-28

Cross Section East West 20' Alley
B/H. 72 Ocean Beach
Bet NIAGARA and NEWPORT.

16.27

73

6.24 17.29

11.05 NE BP
Newport Bacon

0-12' = N.Y. C. Line Bacon

N on Paving	5.61	11.68
S " "	5.55	11.74
S " " Bacon = East edge Bld. on S 0.2' Back. Con Foundation	5.52	11.77
N.Y. Bacon = 0+00 = East edge Bld. on N on Line		
S top cb	4.61	12.68
" Gut on Paving	4.79	12.50
S " "	5.24	12.05
N Gut on "	5.00	12.29
N top cb	4.82	12.47
0+40 = West edge Bld. on N on Line		
N at Bld. on Ground	5.6	11.7
S on Ground	5.5	11.8
S " Con Foundation on Line	5.0	12.3
0+50 = West edge Bld. on S	4.71	12.58
0+51 = East edge " on N 0.2' in St.	4.7	12.0
T.P. 4.76	16.27	5.78
0+66 = East edge 4 Garages on South	4.43	11.84
+82 = West " First 2 Garages on S	4.46	11.81
+82 = East " 2nd Pair " " S	4.7	11.6
1+00 = " " " " "		
-2.5 on Garage Floor	4.8	11.5
S	4.9	10.4

Plotted 10-20-28
HRS
5

do	5.0	11.3
N	4.8	11.5
4.9	11.4	
1+25 = East edge Stack on N on Line wood Foundation		
1+27 = east edge triple Garage on South	2.2' Back	11.7
1+50 = " " " " "	" " "	11.7
-2.2' on dirt Floor	4.7	11.6
S	5.0	11.3
S	5.1	11.2
+6	5.1	11.2
N	5.4	10.9
1+55.5 = S Garage on N on Line	5.8	10.5
+65.5 = " " " " "	5.8	10.5
+75 = " " " " "	6.0	10.3
1+81		
N	5.4	10.9
S	5.4	10.9
S	4.7	11.6
2+06 = S Garage on S 7.5' back	4.6	11.7
2+30		
S	5.5	10.8
S	5.7	10.6
N	5.9	10.4
2+68 = S Garage on N Con Floor		
-3 on Floor Garage	5.44	10.83
N	5.6	10.7
S	5.6	10.7

dirt floors
1+30 also =
west edge
Stack on

12' wide

12' wide
3' back

16.27

S			5.2	11.1
	3+00			
S			4.6	11.7
L			5.0	11.3
N			5.2	11.1
	3+50			
N			3.6	12.7
L			3.6	12.7
S			3.1	13.2
T.P.	10.80	24.70	2.37	13.90
	4+00			
S			8.9	15.8
+7			9.0	15.7
L			9.2	15.5
N			9.3	15.4
	4+25 = Entrance	North and South Alley		
N			9.0	15.7
L			8.4	16.3
S			8.0	16.7
chk. on T.P. in Past.			6.24	18.46

Book 1252-76
For ch.

Walker
Reupling
Shoxy
Lecky
10+15-20

20' Cross Section North and South
Alley Bk. 72 Ocean Beach

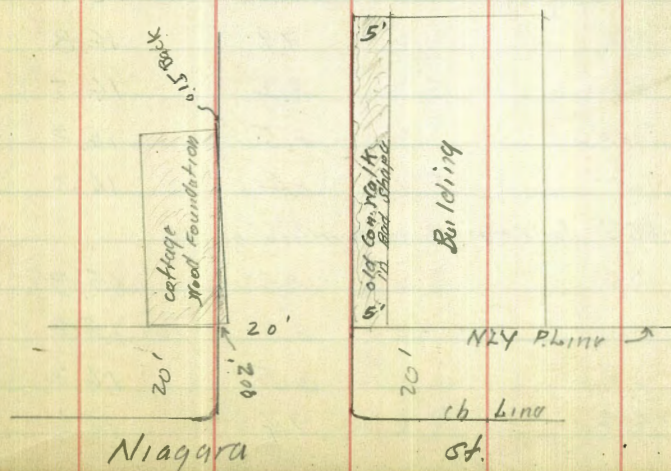
74

24.70 Ht. from Page 73

N.Y. Line NIAGARA St. = 4+00

N top ch.	0.25	24.25
" Gut on Paring	0.95	23.75
L " "	1.58	23.12
E " " "	1.48	23.22
E top ch.	1.30	23.40
0+18 = 1/2 Cottage on Walk on N.Y. 1.5		23.2
0+37.5 = 1/2 on Walk on N		
- 0.25 on top Walk	1.88	22.82
N	2.7	22.0
L	3.4	21.3
E	3.2	21.5
E on old con Walk		

Entrance
Niagara St.



2470

E-5 at Bld. on Walk	4.66	20.04
E	5.1	19.6
S	5.0	19.7
N	4.5	20.2
1+25 = S Garage on N. Very Poor Con. Cen Floor. ↓		
-2 on Floor	6.7	18.0
N	6.7	18.0
S	7.2	17.5
E	7.1	17.6
1+40 = Shine East + West #115		
E	8.0	16.7
S	8.0	16.7
W	7.5	17.2
1+50		
-6	12.5	12.2
-5	8.5	16.2
-2	7.9	16.8
W	7.9	16.8
+3	8.2	16.5
S	8.5	16.2
E	8.4	16.3
1+55 = South edge Dance Pavilion on N.		
E	8.8	15.9
S	8.8	15.9
+8	8.5	16.2
N	9.1	15.6

2470

75

+2	12.0	12.7
+5 at Bld. on Ground	13.3	11.4
2+00		
-5 at Bld. on Ground	13.1	11.6
-2	12.5	12.2
N	11.3	13.4
+2	10.4	14.3
S	10.9	13.8
E	10.9	13.8
T.P.	2.52	15.15
	12.07	12.63
2+50		
E	3.4	11.8
S	3.7	11.5
N	3.7	11.5
+3	4.1	11.1
+5 at Bld. on Ground	4.6	10.6
2+69 = South edge shack on East		
-5 at Bld	5.5	9.7
-3	4.8	10.4
N	4.7	10.5
S	5.0	10.2
E	4.8	10.4
+0.8 at shack on Ground	4.8	10.4
2+95		
E	6.6	8.6
S	6.9	8.3

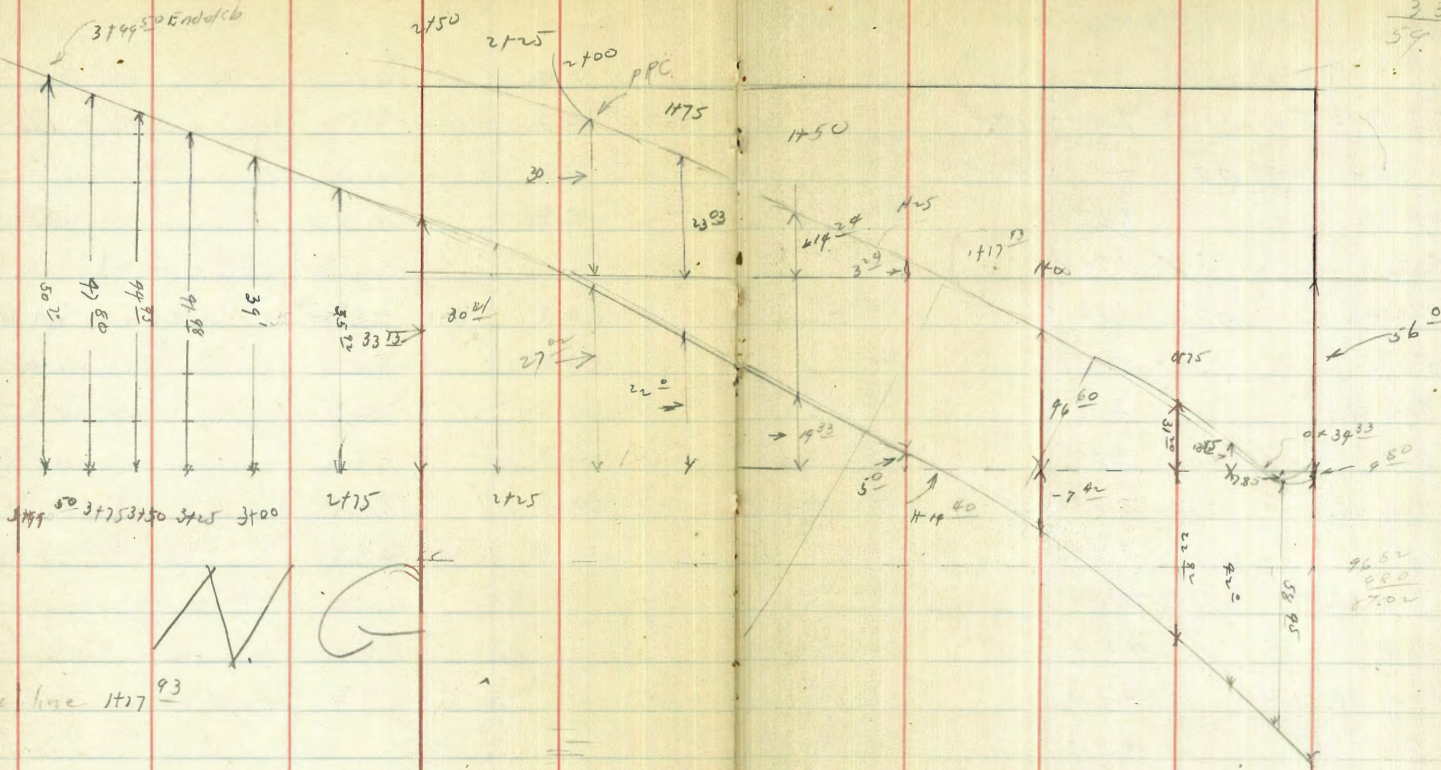
L+6	6.6	8.6
Y	6.4	8.8
+3	6.6	8.6
+5 at Bld.	7.0	8.2

3+00 = 5'6" Len

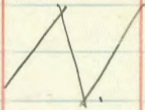
-5 at Bld. on long Walk	7.30	7.85
X on top ch.	7.24	7.91
" " Gut on Pav.	7.40	7.75
Q " "	7.70	7.45
E " " "	7.18	7.97
E top ch.	7.04	8.11
T.P. 6.96 14.91	7.20	7.95
T.P. 3.57 15.57	7.91	12.00
chk. on B.M. Newport & Bacon	4.52	11.05

$$\frac{11.05}{0.00} = \text{B.M.}$$

56
334
 59 34 17



3149.50 3175 3150 3125 3100
 2175 2125



Parallel line 1177 93

49.80

96.52
350
 87.02

66.30
135
 58.75

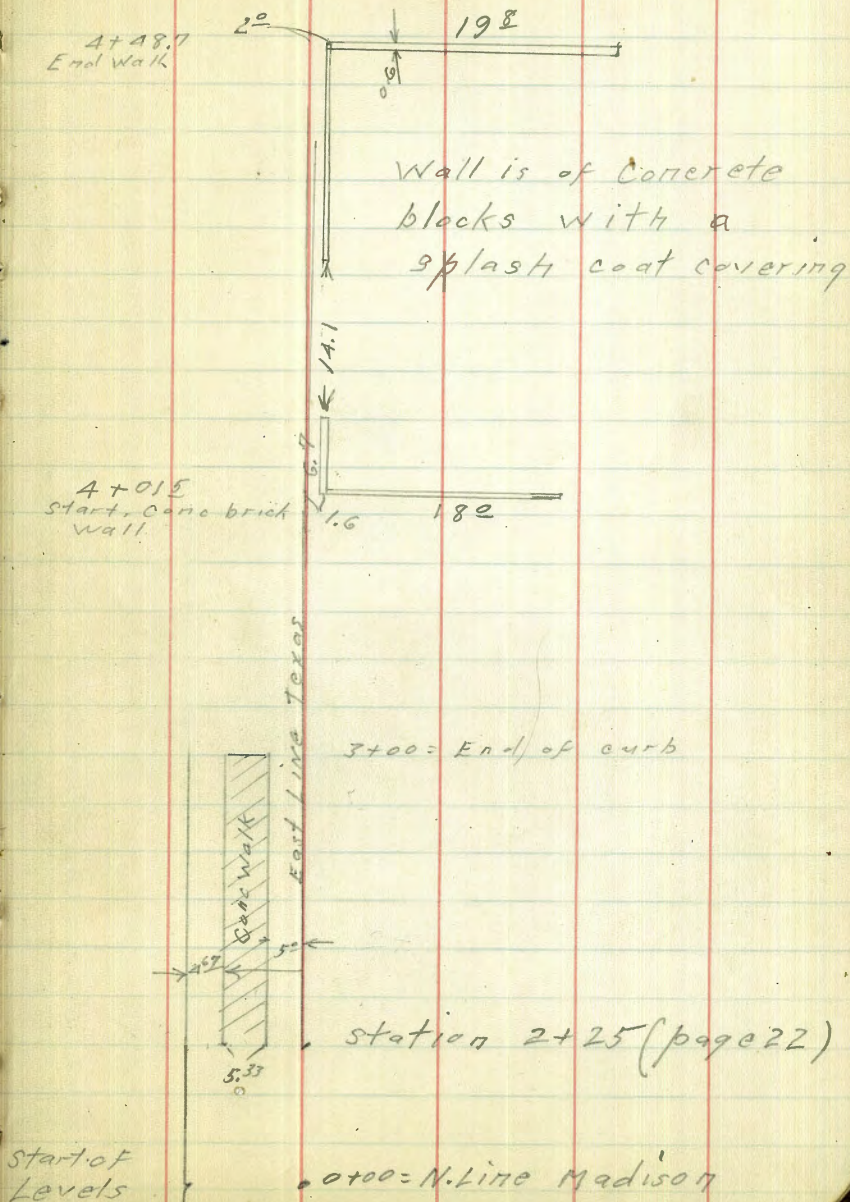
W.O. 237

Additional Curb

Levels TEXAS. St.
North of Madison

2-10-47
Spattermeier
W. Moore 78
Green

B.M. =	S.E.B.P.	Texas	& Madison	
	1.06	<u>347.09</u>	—	346.03
0+00	Top. ch.		1.17	345.9
"	Out.		1.70	345.4
+50	Top. ch.		1.82	345.27
"	Out.		2.49	344.6
+100	Top. ch.		2.58	344.51
"	Out.		3.27	343.82
+150	Top. ch.		3.35	343.74
"	Out.		3.91	343.18
+200	Top. ch.		4.01	343.08
"	Out.		4.64	342.45
+25	Top. ch.		4.34	342.75
"	Out.		4.94	342.15
+50	Top. ch.		5.47	341.62
"	Out.		6.05	341.04
+75	Top. ch.		7.22	339.87
"	Out.		7.85	339.24
3+00	End of curb. Top. ch.		9.58	337.51
"	Out.		10.25	336.84
4+01.5	15' Back of E. Line Bot. of wall		12.43	336.66
"	Ground (Bottom of Wall)		15.0	332.09
4+487	End of wall (Top of Wall) 2' East of prop. Line		12.93	334.16
"	Ground		15.6	331.39
2x2 Δ	Back 1757 P. 5	4.56	342.53	Should be 342.54



Start of Levels

DIRECTIONS FOR USE OF TABLES

TABLE No. 1

Distance of slope stake from side or shoulder stake for any width roadway, slope 1/2 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level, the side stake and slope stake lower target by this amount if cut elevations are used. Add this amount to cut or fill and find distance in table. Set up rod at side stake and find distance to cut or fill target.

TABLE No. 2

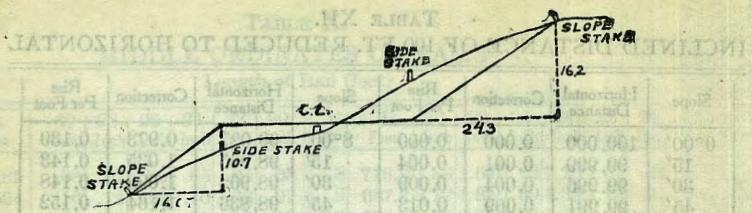
To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given L may be found by dividing tangent (or external), opposite L by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

TABLE No. 3

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given L may be found by dividing tangent (or external), opposite L by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

S+00	13'	Bottom Canyon
	58'	Edge Road
	68'	q Rd
	79'	Edge Rd
	129'	Top of Bluff
Slope S+25	18'	Bottom Canyon
	70'	Edge Road
	80'	q Rd
	90'	Edge
	139'	Top of Bluff
S+50	20'	Bottom Canyon
	75'	Edge of Road
S+75	30'	Bottom Canyon
	85'	Edge Road
600	30'	Botl. Can.
	95'	Edge Road



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

519
36
555

47
17
64

19.88
 $- 0.7$

 19.2
 $+ 7.4$

 106.6

38
 14

 52
 14

 66

$- 5.7$

 100.9

ENGINEERING DEPARTMENT
CITY OF SAN DIEGO,
CALIFORNIA.

339.65
 314.25

 25.40

50×50
 2500
 645

 $1855 = 44$
 16

 $255 = 8$

25.40×25.40
 5080
 12700

 161600

 6451600

$7 \overline{) 170.5} = 2$
 14

 30

$25 \overline{) 195.70} = 7$
 175

 20.70

$195.70 : 170.5 =$
 25.0
 3.6

 21.4

195.70
 170.50

 $25.20 = 3.6$
 21

 4.2

21.4×7
 149.8

 170.5

 20.7

4
 18

 65

21.4
 21.4
 21.4
 21.4
 21.4
 21.4
 21.4
 21.4

 20.7

 170.5

53
 18

 71
 65

 18

 85

 20.7

 195.7

Louisiana + Madison S.E BP 342.31
 Texas S.E BP 346.03