

1251

1951

1951

1951

ENGINEERING DEPARTMENT,
CITY OF SAN DIEGO,
CALIFORNIA.

Our Leather Bound Engineers Note Books are carried in the following rulings:

- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
- No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.
- No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.
- No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

We also carry the Note Books listed above, bound in extra strong Fabri-Hide (otherwise the same quality of book), which can be furnished at a somewhat lower price.

In ordering Fabri-Hide covered books, add the letter "F" to catalog number.

THE FREDERICK POST CO.
ENGINEERING and DRAFTING SUPPLIES
IRVING PARK STATION
CHICAGO, ILL.

MICROFILMED

DEC 22 1964

No. 385 Bpp Co 7/1/30 H.H.

	from	To	
Ebers	Voltaire	Pescadero	1-26
Keating	Columbia	Torrence	27-43
Eads	Silverado	S. end	44-65

Drain levels Cooper St. to Nite St. 67

Canon line 71

Eads Ave. Silverado to Prospect 73

No. 1000 4/13/30

Moore
 5/10/48
 Cross Section of EBERS ST
 VOLTAIRE to Pascardero
 EBERS = 60' wide 10' curbs
 + 10' 1/4" Voltaire to Brighton (30.12)
 Voltaire + Ebers 5.2 35.30 30.06 SW90

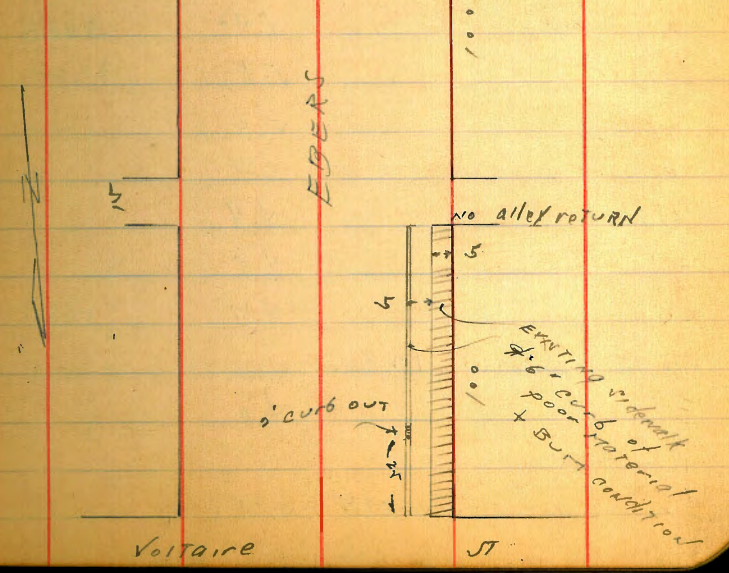
N.L. Voltaire = 00
 w/ mudo algo core work 4.9
 + 7 = Eucalyptus 1.3 diam
 curb top cement 5.7 30.18
 gutter on paving 5.2 29.55
 1/4 " " 5.4
 " " " 5.25
 1/4 " " 5.3
 gutter " " 5.48 29.82
 Top curb 1.5 30.5
 E 4.4

0 + 5
 E 4.1
 + 6.5 = Eucalyptus 1.4 diam
 + 9 4.1
 6 5.1 30.2
 1/4 5.0
 " 5.0
 1/4 5.2
 gutter 5.6
 Top curb 4.9 30.4
 + 3 Eucalyptus 1.0 diam
 w/ 1.6

35.30
 1

0 + 5
 w/ 4.5
 + 8 Eucalyptus 1.1 diam
 Top curb 5.7 30.58
 gutter 5.6
 1/4 5.4
 " 4.9
 1/4 5.0
 + 9 gutter 5.1
 curb 1.4 30.9
 + 4 Eucalyptus 1.0 diam
 E 1.4
 M/R Excepted HVE.

Note! all trees should be removed!



0+75

1+17

E		4.5	
+8 Eucalyptus	1.0 diam	4.4	
cb		4.1	30.9
+1		5.2	
1/4		4.9	
e		4.9	
1/4		5.3	
gutter		5.4	
Top cam curb		4.65	30.62
+7 Eucalyptus	1.0 diam	4.4	
w		4.4	

E		4.2	
+8 Eucalyptus	1.3 diam		
cb		4.2	31.1
+1		4.8	
1/4		4.7	
c		4.6	
1/4		5.0	
+9		5.4	
cb		4.5	30.8
+7 Eucalyptus	1.2 diam	4.0	
w		4.6	

0+99

1+35

w		4.4	
+8 Eucalyptus	1.3 diam		
ent. cb		4.4	30.88
gutter		5.1	30.2
1/4		5.0	
e		4.7	
1/4		4.9	
+9		4.8	
cb		4.1	31.2

w		4.6	
+8 Eucalyptus	1.4 diam		
cb		4.5	30.8
+1		5.3	
1/4		4.8	
c		4.5	
1/4		4.6	
+9		4.8	
cb		4.1	31.2

+7 Eucalyptus 1.2 diam

+7 Eucalyptus 1.4 diam

E		4.0	
1+975			
d of alley and ST = ^{Top} Jena M.H.		4.55	

E		4.0	
1+64			
E		3.9	

		35.30	
E + 8	Eucalyptus 1.4 diam		
cb		4.0	31.3
+1		4.8	
1/4		4.6	
c		4.4	
1/4		4.7	
+9		5.4	
cb		4.4	30.9
+ 4.5	Eucalyptus 2.0 diam		
W		4.5	
	2+15 = NL MUR ST.		
W		4.0	
Top CMT curb		4.27	31.03
Gutter on paving		4.87	30.43
1/4	" "	4.64	
c	" "	4.4	
1/4	" "	4.35	
Gutter	" "	4.58	30.72
Top CMT curb		3.80	31.50
E		3.50	
	SL MUR = 00		
E		3.4	
Top CMT curb		3.74	31.56
Gutter ON paving		4.5	
1/4		4.4	
c		4.4	
1/4		4.68	

		35.30	Ebens
Gutter on paving		4.94	
Top CMT curb		4.30	31.00
W		4.1	
T.P. 5.7W		36.15	30.43
	0+25		
W		5.0	
+ 8	Eucalyptus 1.0 diam		
cb		5.1	31.0
+1		6.0	
1/4		5.5	
c		5.1	
1/4		5.1	
Gutter		5.1	
Top CMT cb.		4.51	31.64
E		4.2	
	0+50		
E		4.2	
Top CMT cb		4.40	31.75
Gutter		5.1	
1/4		5.0	
c		5.0	
1/4		5.4	
+9		5.8	
cb		5.0	31.1
+W	Eucalyptus 1.3 diam		
W		5.1	

Note: 8" curb + 5" sidewalk in D.K. on East side EBENS ST.
 between Mur + Long Street
 inside edge of sidewalk 2.5' from pt.

3615

	0+75		
w/		5.0	
+ 8 Eucalyptus 1.0 diam			
cb		4.9	31.3
+1		5.7	
1/4		5.2	
c		4.8	
1/4		4.8	
Gutter		4.9	
Top cmt cb		4.30	31.85
E		5.0	
	1+00 = NL alley		
E	Top curb of E	3.9	
cb	Top alley return	4.16	32.00
Gutter		4.8	
1/4		4.5	
c		4.8	
1/4		5.2	
+9		5.5	
cb		4.8	31.4
+ w Eucalyptus 1.1 diam			
w/		4.7	
	1+07.5		
♀ alley 4.5 = sewer 14 H		5.1	
	1+15 = SL alley		
w		4.8	

E60ns

4

+ 8 Eucalyptus 1.5 diam			
cb		4.8	31.4
+1		5.5	
1/4		5.2	
c		4.7	
1/4		4.6	
Gutter		4.6	
cb Top cmt.		4.11	32.04
E " alley return		4.78	
	1+64		
E		4.7	
cb Top cmt		4.57	32.23
Gutter		4.6	
1/4		4.5	
c		4.5	
1/4		4.9	
+9		5.1	
cb		4.3	31.9
+ 7.5 Eucalyptus 1.7 diam		4.0	
w		4.6	
	1+90 = w/L + 8 Eucalyptus 1.6 diam		
	2+0.5 = P.C. of 20' curb return = 20' R		
w		4.3	
cb		4.5	31.7
+1		4.7	
1/4		4.4	

36.15

C	4.0	
1/4	4.1	
gutter	4.1	
nb Top curv	3.63	32.52
E	3.6	
0 + 15 = NL Long Branch Ave		
E	3.4	
+ 7.3 Top curv curv	3.6	32.55
gutter on paving	4.33	
curb / line	4.3	
1/4	4.17	
c	4.23	
1/4	4.23	
curb line	4.67	
gutter	4.74	
+ 2.8 Top curv curv	4.15	32.00
W	4.1	
TP 6.47	38.85	34.58
SL Long Branch = 00		
W	6.3	
+ 7.1 = Top curv cb	6.47	32.58
gutter on paving	6.93	
cb line	6.87	
1/4	6.66	
c	6.57	
1/2	6.50	

38.85

KBONS 5

ob line on paving	6.64	
gutter	6.64	
+ 2.7 Top curv curv	5.87	32.98
E	5.7	
0 + 0.8 = PC of curb return		
E	5.5	
cb	5.7	33.1
+ 1	6.4	
1/4	6.1	
c	6.4	
1/4	6.5	
+ 9	7.1	
cb	6.5	32.3
W	6.3	
0 + 2.5		
WL + 8 Eucalyptus	1.4 diam	
EL - 8	1.0	
0 + 1.0		
W	6.0	
+ 8 eucalyptus	1.4 diam	
cb	6.0	32.9
+ 1	6.3	
1/4	6.4	
c	5.9	
1/4	5.8	
+ 9	6.0	

3885

cb 5.4 33.4

+ n.5 eucalyptus 1.0 diam

E 5.2

0+75

WL + n.5 eucalyptus 1.5 diam

EL - 7.5 " 1.5 "

1+00

E 5.5

+ 8 eucalyptus 8" diam

cb 5.5 34.5

+1 5.4

1/4 5.3

c 5.2

1/4 5.4

+9 6.0

cb 5.8 33.0

wl 5.5

1+38

wl 5.2

+ 8 eucalyptus 1.4 diam

cb 5.9 34.0

+1 5.4

1/4 5.1

c 5.6

1/4 5.6

+9 5.7

3885

Ebons

6

cb 4.0 34.9

+ n.5 eucalyptus 1.7 diam

E 3.9

1+07.5 Baked up

fall of + JT = top ^{sewer} Mt. 4.93

1+63

WL + eucalyptus 1.7 diam

EL - 7.5 " 0.7 diam

1+18

E 3.4

cb 3.4 35.5

+1 4.3

1/4 4.2

c 4.2

1/4 4.6

+9 5.3

cb 4.8 34.1

+ eucalyptus 1.4 diam 4.6

wl

2+15 = all Brighton = Excepted

wl 4.1

cb Top cmr. 4.30 34.55

quarter expansion 4.87

1/4 " 4.37

c " 3.97

1/4 " 3.90

quarter " 3.96

3885

cb Topcmt.	3.23	3562
E	3.1	
T.P. 6.07	40.59	36.57
SL Driveway = 00		
E	4.0	
cb Topcmt.	5.00	35.6
gutter on paving	5.75	
1/4 " "	5.70	
" " "	5.77	
1/2 " "	6.15	
gutter	6.60	
cb Topcmt	6.07	34.52
W	5.66	
0+50		
W	4.9	
+V	5.2	
+3	5.7	
cb	5.8	34.8
+1	6.45	
1/4	6.0	
c	5.5	
1/4	5.4	
+8	5.6	
cb	4.8	35.8
+10	4.4	
+11	2.7	
E	2.7	

NOTE 1
 EBERS 60' wide
 12' curbs
 9' / 11'
 Brighton to Pescadero

40.59

Ebers 7

1400		
E	3.2	
+1	3.3	
+V	4.3	
cb	4.8	35.8
+1	5.4	
1/4	5.4	
c	5.0	
1/4	5.8	
+8	6.0	
cb	5.4	
+95 = both fence	5.2	
W	5.2	
1+40 both fence	2.5 in street	
1+50		
W	5.6	
cb	5.6	35.0
+1	5.8	
1/4	5.3	
c = To S Sewer	4.6	
1/4	4.8	
+8	4.8	
cb	4.5	36.1
E	4.1	
2+00		
E	4.1	

34.2
 Ladybug
 shame on you

EV. 35.10

4/0.59

cb	4.4	36.2
+1	5.0	
1/4	4.6	
c	4.6	
1/4	5.2	
+8	5.9	
cb	5.0	35.6
w	5.3	
2+50		
w	5.2	
cb	5.0	35.6
+1	5.6	
1/4	5.1	
c	4.4	
1/4	5.5	
+8	4.8	
cb	4.0	36.6
E	3.7	
3+00 = NL Cape May = Excepted		
E = BM	3.73	37.36 37.36
cb Top CMT.	3.61	36.98
+1	4.5	
1/4	4.6	
c	4.7	
1/4	4.9	
+8	5.3	

2/0.59

Ebers

8

cb	Top CMT.	4.55	35.94
w		4.7	
5L Cape May = 00			
w		3.7	
cb	Top CEMENT	3.61	36.98
+1		4.3	
1/4		3.7	
c		3.4	
1/4		3.3	
+8		3.4	
cb	Top CMT.	2.64	37.97
E		2.7	
0+50			
E		1.7	
cb		1.8	38.8
+1		2.5	
1/4		2.4	
c		2.3	
1/4		2.7	
+8		3.2	
cb		2.4	38.2
w		2.7	
1+00			
w		1.6	
cb		1.6	39.0
+1		2.3	

		2/0.59		
W	1/4		1.6	
C			1.2	
	1/4		1.3	
	+8		1.5	
	cb		0.7	39.9
	E		0.7	
T.P.	10.84	50.57	0.86	39.73
	1+50			
	E		9.0	
	cb		9.4	41.2
	+1		10.2	
	1/4		10.2	
	C = Sewer M.H. R.I.M		10.0	
	1/4		10.5	
	+8		11.1	
	cb		10.7	39.8
	W		10.7	
	2+00			
	W		9.3	
	cb		9.4	41.2
	+1		10.0	
	1/4		9.4	
	C		9.0	
	1/4		9.1	
	+8		9.3	
	cb		8.7	41.9
	E		8.3	

		50.57	Elevs	9
	2+50			
	E		7.3	
	cb		8.0	42.6
	+1		8.2	
	1/4		8.0	
	C		8.0	
	1/4		8.3	
	+8		8.9	
	cb		8.5	42.1
	W		8.4	
	3+00 = L Saratoga = excepted			
	W		7.3	
	cb Top cmt		7.58	42.99
	+1		8.1	
	1/4		7.8	
	C		7.1	
	1/4		7.0	
	+8		7.1	
	cb Top cmt		6.6	43.95
	E		5.8	
	5+00 = L Saratoga = .00			
	E		5.4	
	cb Top cmt.		5.59	44.98
	+1		5.8	
	1/4		6.1	
	C		6.1	

50.57

1/4		6.5	
+8		7.1	
cb	Top crst.	6.57	44.00
w		6.00	
	0+50		
w		6.0	
cb		6.0	44.6
+1		6.6	
1/4		5.9	
c		5.6	
1/4		5.4	
+5		5.7	
cb		5.4	45.4
E		4.7	
	1+00		
E		4.4	
cb		4.5	46.1
+1		5.0	
1/4		4.5	
c		4.9	
1/4		5.3	
+8		6.0	
cb		5.4	45.2
w		5.4	
	1+50		
w		4.4	

50.57

Ebars 10

cb		5.0	45.6
+1		5.4	
1/4		4.8	
c	Jewer MH Rim	4.6	
1/4		4.2	
+9		4.4	
cb		4.0	46.6
E		3.7	
	2+00		
E		3.1	
cb		3.2	47.2
+1		4.4	
1/4		2.9	
c		4.1	
1/4		4.5	
+8		5.1	
cb		4.5	46.1
w		4.5	
	2+50		
w		4.3	
cb		4.3	46.3
+1		4.7	
1/4		4.1	
c		3.8	
1/4		3.6	
+8		3.9	

50.57

cb 3.1 47.5

E 2.7

3400 = N. SANTA MONICA - Excepted

E 2.1

cb Top cmt 2.50 48.07

qut Top paving 3.25

1/4 " " 3.20

c " " 3.00

1/4 " " 3.00

qut " " 3.90

cb Top cmt. 3.47 47.10

W 3.5

T.P. exp. back 49.99 3.57 49.00

S. L. SANTA MONICA = 00

S. L. SANTA MONICA
FLOORS

W 3.0

cb Top cmt 3.01 46.96

qut paving 3.34

1/4 " " 2.85

c " " 2.53

1/4 " " 2.49

qut " " 2.69

cb Top cmt 2.01 47.98

E 1.7

0 + 50

E 2.3

cb 2.7 47.3

49.97

+1 3.3

1/4 3.2

c 3.3

1/4 3.7

+8 4.3

Cb 4.6 46.4

W 3.4

1700

W 3.9

Cb 4.0 46.0

+1 4.6

1/4 4.0

c 3.6

1/4 3.5

+8 3.5

Cb 3.0 47.0

E 2.8

+50

E 2.8

Cb 3.6 46.4

+1 3.8

1/4 4.0

C = Sewer M.H.R.M. 3.97

1/4 4.5

+8 4.7

Cb 4.5 45.5

W 4.5

5000 Ebons

11

49.97

50.00

	2+00		
W		5.1	
cb		5.1	44.9
+1		5.5	
1/4		5.0	
c		4.5	
1/4		4.6	
+8		4.6	
cb		4.2	45.8
E		3.9	
	0+50		
E		4.3	
cb		4.8	45.2
+1		5.2	
1/4		5.3	
c		5.1	
1/4		5.6	
+8		5.9	
cb		5.8	44.2
W		5.6	

3+00 = W L New port = excepted

W		6.3	
cb	Top CMT	6.00	43.97
qut	paving	6.67	
1/4	"	6.28	
c	"	5.88	

49.97

Ebons

50.00

12

1/4		5.66	
qut		5.67	
cb	Top CMT	4.95	45.02
E		4.7	
	SL New port = 00		
E		4.7	
cb	Top CMT	5.00	44.97
qut	paving	5.68	
1/4	"	5.65	
c	"	5.77	
1/4	"	6.15	
qut	"	6.67	
cb	Top CMT	6.00	43.97
W		5.9	
	0+50		
W		4.6	
cb		4.9	45.1
+1		5.5	
1/4		4.9	
c		4.5	
1/4		4.3	
+8		4.4	
cb		3.8	46.2
E		3.5	
	1+00		
E		2.8	
cb		2.8	47.2

11997

50.00

E cb +1	3.5	
1/4	3.5	
c	3.3	
1/4	3.7	
+05	4.4	
cb	3.7	463
W	4.0	
	1750	
W	3.0	
cb	2.6	474
+1	3.3	
1/4	2.6	
c M.M. here to be built up	2.3	
1/4	2.2	
+8	2.3	
cb	1.8	48.2
E	1.5	
	2400	
E	0.1	
cb	0.2	49.7
+1	1.0	
1/4	1.0	
c	1.0	
1/4	1.5	
+8	2.1	
cb	1.5	48.5
W	2.0	

11997

Ebans

13

T.P.	219	56.77	0.89	49.08
	2450			
W			6.6	
cb			6.5	49.8
+1			7.2	
1/4			6.5	
c			6.0	
1/4			6.1	
+8			6.3	
cb			5.4	50.9
E			5.3	
	3400 = St Niagara			EXCEPTED
E			4.1	
cb Top cmt			4.7	52.00
90T			5.4	
1/4			4.8	
c			4.7	
1/4			5.4	
90T			6.0	
cb Top cmt			6.45	50.02
W			6.4	
TP	10.03	67.86	3.44	52.83
	00 = St Niagara			
W			11.4	
cb Top cmt.			10.83	52.03
90T			11.8	

6286

1/4	11.1	
c	10.5	
1/4	10.2	
gut	10.2	
cb Top amt	9.88	52.98
E	9.4	
		0+50
E	8.6	
cb	8.7	54.1
gut	9.3	
1/4	9.3	
c	9.4	
1/4	9.6	
gut	10.4	
cb	9.7	53.2
w	9.6	
		1+00
w	8.4	
cb	8.3	54.6
gut	8.5	
1/4	8.3	
c	7.8	
1/4	7.9	
gut	8.1	
cb	7.4	55.5
E	7.1	

6286

Ebens

14

			1+50	
E	5.5			
cb	6.4	56.7		
gut	6.9			
1/4	6.3			
c	6.8		Lower = 1/4	on rim
1/4	7.1			
gut	7.4			
cb	7.0	55.9		
w	7.1			
			2+00	
w	5.7			
cb	5.7	57.2		
gut	6.4			
1/4	5.6			
c	5.1			
1/4	5.1			
gut	5.3			
cb	5.5	58.4		
E	4.4			
			2+50	
E	2.8			
cb	3.4	59.7		
gut	3.7			
1/4	4.0			
c	4.1			

62.86

1/4		4.4	
gut		4.9	
cb		5.5	58.5
w		4.3	
34000 NI Narr - excepted			
w		3.2	
cb	Top cmt.	2.86	60.00
gut	on paving	3.47	
1/4	" "	3.06	
c	" "	2.75	
1/4	" "	2.61	
gut	" "	2.64	
cb	Top cmt.	1.80	61.06
E		0.6	
T.P. ^{no}	11.23	72.29	61.06
00=SL Narr			
E		9.7	
cb	Top cmt	10.30	61.99
gut	on paving	10.97	
1/4	" "	11.0	
c	" "	11.24	
1/4	" "	11.53	
gut	" "	11.94	
cb	Top cmt.	11.31	60.98
w		11.8	

72.29

E6005

15

0750			
w		9.7	
cb		13.0	62.3
gut		10.0	Washed out
1/4		9.3	
c		9.2	
1/4		9.2	
gut		9.3	
cb		8.9	63.4
E		8.1	
1400			
E		7.1	
cb		7.2	65.1
gut		8.2	
1/4		7.8	
c		2.9	
1/4		8.3	
gut		8.5	63.8
cb		8.2	
w			
1450			
ST & alley	Per M. Sewer M.H.	6.17	
1460=81 alley			
w	Top alley return	5.83	
cb	cmt.	6.02	66.27
gut		6.5	
1/4		6.4	

NOTE: 1460' curb & sidewalk in O.K.
 old West side on
 Lot mt B/K/S/O.D.B.

74.29

c	6.0	
1/4	5.9	
cb	5.6	66.7
E	5.3	
2+00		
E	4.5	
cb	4.2	67.9
gUT	4.8	
1/4	4.5	
c	4.2	
1/4	4.9	
gUT	5.2	
cb Top CMT	4.84	67.45
+8.5 = inside edge of 5' wide	4.64	Sidewalk
2+50		
W +3.5 = inside edge of " "	3.2	"
cb Top CMT	3.36	68.93
gUT	3.5	
1/4	3.6	
c	3.2	
1/4	3.4	
gUT	3.5	
cb	3.0	69.3
E	2.8	

74.29

3+00 = NL Del Monte = except prod		
E	0.9	
cb Top CMT	1.37	70.97
gUT on paving	2.25	
1/4	2.01	
c	2.00	
1/4	2.22	
gUT	2.28	
cb Top CMT	1.86	70.43
+8.5 = inside edge of 5' wide	1.50	
T.P. S.W.C.T. 11.87	8 3.13	1.03
71.26		Del Monte Ebens
00 = S.L. Del Monte		
W	11.5	
cb Top CMT	11.58	71.55
gUT on paving	12.12	
1/4 " "	11.83	
c " "	11.67	
1/4 " "	11.65	
gUT " "	11.90	
cb Top CMT	11.09	72.04
E	11.0	
0+50		
E	6.8	
cb	7.2	75.9
gUT	8.1	
1/4	2.7	

Ebens 16

8313

C		7.5	
1/4		8.0	
gut		8.5	
cb		7.6	75.4
w		8.1	
	1+00		
w		3.7	
cb		3.6	80.5
gut		4.3	
1/4		3.5	
C		3.4	
1/4		3.4	
gut		3.5	
cb		2.8	80.3
E		2.6	
T.P.	1260	9.5.73	0.00 8313
	1+50		
C	4 ft alley = sewer M.H. rim	12.09	
	1+60 = BREAK = grade change see profile		
E		10.9	
cb		11.4	84.5
gut		11.8	
1/4		11.4	
C		11.4	
1/4		11.8	
gut		12.4	

95.73

E602 17

cb		12.0	83.7
w		11.4	
	2+00		
w		9.7	
cb		9.4	86.3
gut		10.1	
1/4		9.4	
C		8.7	
1/4		8.7	
gut		9.1	
cb		8.4	87.5
E		8.1	
	2+50		
E		4.9	
cb		5.3	90.4
gut		5.9	
1/4		5.8	
C		5.8	
1/4		6.3	
gut		6.9	
cb		6.4	89.3
w		6.7	
	3+00 = ALL SANTA CRUZ = 20 curves 10' 1/2 S		
w		3.4	
cb		3.4	92.3
gut		4.1	

95.73

1/4			3.2	
c			3.0	
1/4			3.1	
gut			3.3	
cb			2.1	93.6
E			2.1	
T.P.	10.56	106.29	0.00	95.73
	N curb			
E			12.4	
cb			12.7	93.6
1/4			12.8	
c			12.7	
1/4			13.2	
gut			13.6	
cb			13.2	93.1
w			13.7	
	N 1/4			
w			12.9	
cb			13.1	93.2
1/4			13.0	
c			12.4	
1/4			12.5	
cb			12.2	94.1
E			11.3	
E			10.9	

106.79

Ebers 18

cb			12.0	94.3
1/4			12.1	
c			12.1	
1/4			12.7	
cb			12.7	93.6
w			12.4	
	S 1/4			
w			12.1	
cb			12.4	93.9
1/4			12.3	
c			12.0	
1/4			12.0	
cb			11.9	94.4
E			11.3	
	S cb			
E			11.4	
cb			11.8	94.5
1/4			11.8	
c			11.7	
1/4			12.2	
cb			12.3	94.0
w			12.2	
	00 = S2 Santa Cruz			
w			11.3	
cb			11.1	95.0 should be 94.00
gut			11.8	

Most of the road graded to top of 1.0' cut grade on curve line. It was completed without a check up.

10629

1/4		11.4	
e		10.9	
1/4		11.2	
cb		11.2	95.1
E		10.7	
	0+50		
E		8.3	
cb		8.5	97.8
quT		9.1	
1/4		8.9	
c		8.7	
1/4		9.3	
quT		9.8	
cb		9.2	97.1
w		9.3	
	1+00		
w		7.0	
cb		6.8	99.5
quT		7.4	
1/4		6.7	
c		6.2	
1/4		6.2	
quT		6.6	
cb		6.0	100.3
E		5.6	

10629

Eber 19

1+40 = BREAK = Change from proposed grade
See profile

E		3.5	
cb		3.8	102.5
quT		4.8	
1/4		4.6	
c		4.6	
1/4		4.9	
quT		5.8	
cb		4.8	101.5
w		4.8	

1+50

c d Alley = Low M.H.R.M 3.96

2+00

w		3.5	
cb		3.4	102.9
quT		4.0	
1/4		3.4	
c		2.9	
1/4		2.9	
quT		3.1	
cb		2.3	104.0
E		2.3	
T.P.	5.69	109.95	2.03 104.26
	2+50		
E		5.0	104.9
cb		5.0	104.9

109.95

110.00

109.95

110.00 Ebers

20

E qut

5.7

N curb

1/4

5.5

w/

5.6

c

5.5

cb

4.7

105.3

1/4

6.1

1/4

4.1

qut

6.7

c

3.8

cb

6.1

103.9

1/4

3.5

w/

6.1

cb

3.5

106.5

3400 = NL Coronado to WEST = 20' cbs 10' 1/4"

w/

5.0

E

2.9

cb

4.8

105.2

E

2.7

qut

5.2

cb

3.2

106.8

1/4

4.7

1/4

3.5

c

4.2

c

3.7

1/4

4.3

1/4

4.0

qut

4.1

cb

4.4

105.8

cb

3.8

106.2

w/

4.9

E

3.5

E

NL + 10 = NL Coronado to EAST = 10' cbs 10' 1/4"

E

2.8

w/

4.8

cb

3.8

106.2

cb

4.2

105.8

1/4

3.9

1/4

3.9

c

4.0

c

3.5

1/4

4.7

1/4

3.4

cb

5.1

104.9

cb

3.2

106.8

w/

4.9

E

2.8

E

2.8

20' R
RETURNED

N 1/4

E

S 1/4

10995

110.00

E cb	3.5	106.5
1/4	3.5	
C	3.5	
1/4	4.0	
cb	4.1	105.6
w	5.2	
∫ cb		
w	5.4	
cb	4.6	105.4
1/4	4.1	
C	3.7	
1/4	3.7	
cb	3.8	106.2
E	2.9	
∫ cb + 10 = SL Coronado to east		
E	3.0	
cb	3.5	106.5
gut	4.7	
1/4	4.6	
C	3.9	
1/4	4.4	
cb	5.1	104.9
w	5.0	
+ 10 = SL Coronado to west = 00		
w	5.2	
cb	4.7	104.3

10995

Egans 21

110.00

gut	5.6	
1/4	5.0	
e	4.5	
1/4	4.4	
+ 2	5.2	
gut	5.3	
cb	4.0	106.0
+ 10 = Top of bank		
T.P. ^{Mod} NW	2.97	108.98
0.450		
E + 3 = Top Bank		
cb	6.2	102.1
gut	7.0	
1/4	6.7	
C	6.6	
1/4	7.1	
gut	7.7	
cb	7.0	101.3
w	7.1	
+ 100		
w	10.4	
cb	10.8	97.5
gut	11.5	
1/4	10.6	
e	10.4	
1/4	10.5	

Coronado
28 bars
104.3

Note! Bank on east side of Egans
between Coronado + Del Mar to remain as is

10878

gut			10.5	
cb			9.9	98.4
+ 9.5	Toe Bank		9.4	
	+50			
E + 3	Toe Bank		12.7	
cb			13.4	95.1
T.P.	0.05	95.31	13.0	95.76
gut			1.1	
1/4			1.0	
C = M.H. R.M.			0.8	
1/4			1.4	
gut			2.2	
cb			1.6	93.7
W			1.6	
	+100			
W			4.7	
cb			4.6	90.7
gut			5.4	
1/4			5.0	
C			4.4	
1/4			4.6	
gut			4.5	
cb			4.0	91.3
+ 10.5 = Toe Bank			3.6	
	+50			
E + 2.5 = Toe Bank			6.9	

9531

EGBK

22

cb			7.7	876		
gut			8.7			
1/4			8.3			
C			8.3			
1/4			8.9			
gut			9.5			
cb			8.6	867		
W			8.6			
Short Block	2 + 77.6 =	NH Del Mar =	50' wide	20' curbs	10 1/4	30' R Returns
W			13.0			
cb			14.6	82.7		
gut			13.0			
1/4			12.9			
C			12.0			
1/4			11.6			
gut			11.4			
cb			11.1	84.2		
E	Toe Bank		10.5			
T.P.	2.53	84.87	12.97	87.34		
	Ncb					
E			0.5			
cb			1.4	83.5		
1/4			1.7			
C			1.8			
1/4			2.6			
cb			3.4	81.5		

84.87

w/		5.3	
	n 1/4		
w/		4.6	
cb.		3.6	81.3
1/4		3.1	
c		2.4	
1/4		2.0	
cb.		1.4	83.5
E		0.5	
	201 Mar		
E		0.5	
cb.		1.6	83.3
1/4		3.1	
c		2.6	
1/4		3.3	
cb		3.9	81.0
w/		4.7	
	1/4		
w/		5.2	
cb		4.1	80.8
1/4		4.6	
c		3.0	
1/4		2.6	
cb		2.1	82.8
E		1.1	

84.87

EDERS

23

	Sob		
E		1.3	
cb		2.3	82.6
1/4		2.9	
c		3.3	
1/4		3.9	
cb		4.5	80.4
w/		5.1	
	00 = SL 10/14/18		
w/		4.8	
cb		4.5	80.4
PUT		5.0	
1/4		4.4	
c		4.0	
1/4		3.9	
PUT		3.4	
cb		3.3	81.6
E		2.3	
	0+50		
E		4.4	
cb		5.1	79.8
PUT		5.9	
1/4		5.9	
c		5.9	
1/4		6.4	
PUT		6.9	

8487

cb		6.5	78.4
w		6.9	
	1+00		
w		8.8	
cb		8.4	76.5
gut		8.8	
1/4		8.3	
c		7.9	
1/4		7.8	
gut		7.9	
cb		7.5	77.4
E		7.0	
	1+50		
E		8.8	
cb		8.8	76.1
gut		9.8	
1/4		9.6	
⊙ Sewer MH here	but 1' below grade	9.7	
1/4		10.2	
gut		10.7	
cb		10.2	74.7
w		10.4	
	2+00		
w		12.6	
cb		12.1	72.8
gut		12.6	

8487

EDERS

24

1/4			12.1	
c			11.6	
1/4			11.6	
gut			11.8	
cb			11.1	73.8
E			11.3	
	2+50			
E			12.2	
cb			12.9	72.0
gut			13.8	
1/4			13.3	
c			13.3	
1/4			13.8	
gut			14.4	
cb			14.0	70.9
w			14.2	
T.P.	0.96	72.79	13.02	71.83
	3+00 = NL Orchard		50' wide	20' cbs 10' 1/2 20' cbs
w			3.8	
cb			3.7	69.1
gut			4.0	
1/4			3.4	
c			3.4	
1/4			3.4	
gut			3.4	
cb			3.1	69.7
E			2.7	

72.79

72.79

EBERS

25

	Neb		
E		2.8	
cb		3.5	69.3
1/4		3.6	
c		3.8	
1/4		4.0	
cb		4.4	68.4
w		4.9	
	N 1/4		
w		5.2	
cb		4.4	68.4
1/4		4.2	
c		3.9	
1/4		3.7	
cb		3.3	69.5
E		3.2	
	E		
E		3.0	
cb		3.6	69.2
1/4		3.8	
c		4.0	
1/4		4.4	
cb		4.6	69.2
w		5.7	
	S 1/4		
w		6.0	

cb		4.9	67.9
1/4		4.4	
c		4.3	
1/4		4.1	
cb		3.7	69.1
E		3.0	
	S cb		
E		3.5	
cb		4.3	68.5
1/4		4.7	
c		4.7	
1/4		4.9	
cb		5.2	67.6
w		5.8	
	00 = SL Orchard		
w		6.2	
cb		5.7	67.1
quT		6.3	
1/4		5.9	
e		5.6	
1/4		5.3	
quT		5.0	
cb		4.8	67.0
E		4.4	
	0+50		
E		7.5	

7279

cb	7.9	64.9
gut	8.4	
1/4	8.2	
c	8.5	
1/4	8.9	
gut	9.0	
cb	8.5	64.3
w	8.4	

+100

w	10.0	
cb	11.7	61.1
gut	12.0	
1/4	11.5	
c	11.1	
1/4	11.2	
gut	11.0	
cb	10.9	61.9
E	10.4	

+100 = NL a ley = BREAK grade changed. see profile

E	12.2	
cb	12.8	60.0
gut	13.2	
1/4	12.8	
c	13.0	
1/4	13.3	
gut	13.9	

7279

cb		13.2	59.6
w		13.7	
T.P.	247	64.32	14.94
1450 = \$ JT and w/ley =			
Sewer M.H. R.M.			
2500			

w		5.3	
cb		5.0	57.3
gut		5.3	
1/4		4.9	
c		4.4	
1/4		4.6	
gut		4.7	
cb		4.3	58.0
E		3.9	

2500

E		5.2	
cb		5.5	56.8
gut		6.1	
1/4		6.2	
c		6.0	
1/4		6.2	
gut		7.1	
cb		6.5	55.8
w		6.8	

26

Should be 59.0
sand washed
in here

643ⁿ

EBERS 36 1/2

3400 = N. Pescadero

w/		7.8		
cb	Top cement cb	7.2 ⁿ	54.50	
qut	" paving	8.39		
1/4	" "	7.94		
c	" "	7.67		
1/4	" "	7.48		
qut	" "	7.49		
cb	" Cem cb	6.84	55.48	
E		6.6		
check to BM	NEC or Mon.	4.69	57.63	57.6 ⁿ = AM.

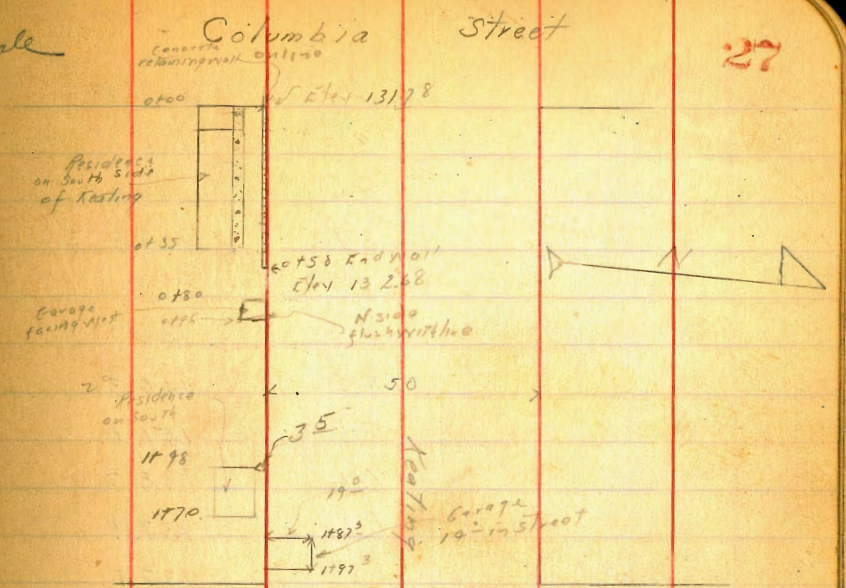
Bliss
Overmit
J. I. Beck
Jacobson
4/17/28
B.M. S.E. Top
Wall Pringle Keller
X. Sections of Keating Street
Middletown Addition from the E line
of Columbia. to the E line of Torrence & Reale

10.89	110.11	51.4	50.57
		99.22	10.65
			7.5 1/4
T.P.	12.60	122.20	0.51
T.P.	11.15	133.12	0.23
T.P.	6.85	137.91	2.06
T.P. <small>S.E. Top of Columbia & Keating</small>	12.89	145.88	9.87

0+00 E line of Columbia

N	11.4	134.5
+2	8.6	137.3
cb	9.1	136.8
1/4	9.9	136.0
1/4	10.8	135.1
1/4	10.8	135.1
+5	10.6	135.3
cb	11.9	134.0
+3	12.8	133.1
S on Top Wall	14.1	131.8
S on Ground	16.3	129.6
S + 5" concrete walk around House	16.4	129.5
S + 9" House on S. floor Porch	16.8	129.7
	0+0.3	
S on Ground	16.5	129.4
S on Top Wall	14.0	131.9
S + 8	12.5	133.4
cb	11.7	134.2
+3	10.3	135.6
1/4	10.5	135.4

Plotted 8-4-28
C.B.M.



Lin Wood Street

Street

4 I
145.88

ϕ	10.9	135.5
1/4	9.3	136.6
cb	8.6	137.3
N	8.1	137.8
	0725	
N	5.2	140.7
cb	5.6	140.3
+5	5.9	140.0
1/4	7.2	138.7
ϕ	8.8	137.1
1/4	8.8	137.1
+3	8.8	137.1
cb	11.0	134.9
+7	12.6	133.3
S on Top Wall	13.6	132.3
S on Ground	16.3	129.6
S+5.5 Edge Walk around House	16.0	129.9
S+10 House on South		1327
	0750	
S-14 Walk on South	16.1	129.8
S on Ground	16.2	129.7
S on Top Wall	13.2	132.7
+8	11.0	134.9
cb	9.9	136.0
+5	7.7	138.2
1/4	7.9	138.0

145.88
at 35 End House
at 40 End Wall 16-1

108

28

ϕ	7.2	138.3
+2	7.5	138.4
1/4	5.8	140.1
+5	3.9	142.0
cb	3.8	142.1
N	2.6	143.3
	0775	
N	1.2	144.7
cb	2.6	143.3
1/4	5.2	140.7
+5	6.8	139.1
1/4	7.3	138.6
+3	8.3	137.6
cb	10.2	135.7
S on Top	12.8	133.1
S Bottom	15.0	130.9
S+15	16.8	129.1
	0792	
S-15	18.5	127.4
S-5	16.0	126.9
S	15.2	130.7
+1	13.2	132.7
cb	10.8	135.1
+6	7.5	138.4
1/4	7.5	138.4
ϕ	7.9	138.5

at 35 End House
at 40 End Wall 16-1
1313 ✓

145.88

79		6.9	139.0
19		6.0	139.9
cb		2.8	143.1
N		0.2	145.7
TR	6.29	151.24	144.95
		14.05	
N		3.7	147.5
+05		5.8	145.4
cb		8.0	143.2
+05		10.7	140.5
1/4		11.4	139.8
£		12.9	138.3
1/4		13.0	138.2
+02		13.2	138.0
cb		15.9	135.3
+09		19.1	132.1
S		20.6	130.6
5-06		21.6	129.6
5-15		23.8	127.4
		14.6	£ Walk on North
	Step on Prop	3.81	147.43
	N+11 Bottom Step	9.22	142.02
5-20		24.4	126.8
5-11		29.0	127.2
5-05		21.9	129.3
S		21.3	129.9

151.24

29

S+03		21.0	130.3
+04		19.2	132.0
+07		18.9	132.3
cb		17.3	133.9
+06		13.9	137.3
1/4		13.8	137.4
£		14.0	137.2
+04		13.5	137.7
1/4		12.5	138.7
cb		8.9	142.3
N		3.7	147.5
		14.50	
N		6.2	145.0
+5		9.2	142.0
+8		10.0	141.2
+9		11.2	140.0
cb		11.6	139.6
TR	9.99	143.18	138.24
1/4		5.8	137.4
+3		6.8	136.4
£		7.2	136.0
1/4		7.0	136.2
+1		7.1	136.1
cb		10.4	132.8
S		13.5	129.7
5-3.5	Residence on South floor	13.00	130.2

HZ
193.18

End of P. Walling	Pos on floor	13.7°	129.48
	1775		
S-15	17.9	125.3	
S	14.6	128.6	
cb	11.9	131.3	
1/4	8.9	134.8	
⊥	8.6	134.6	
1/4	8.0	135.2	
+3	7.9	135.3	
cb	5.9	137.3	
+4	3.4	139.8	
N	1.9	141.3	
	1794		
N	3.1	140.1	
+6	4.6	138.6	
cb	6.9	136.3	
+4	8.4	134.8	
1/4	8.8	134.4	
⊥	9.2	134.0	
1/4	9.3	133.9	
+5	11.5	131.7	
cb	10.5	130.7	
S	15.1	128.1	
+4	16.0	127.2	
+15	19.4	123.8	

X
193.18

50.5°

2400 W line of fir wood	30
15.3	127.9
13.6	129.6
12.8	130.4
9.7	133.5
9.4	133.8
8.8	134.4
6.0	137.2
3.5	139.7
⊥ line of fir wood	
9.5	138.7
7.8	135.4
8.9	134.3
9.5	133.7
9.9	133.3
10.2	133.0
10.6	132.6
13.3	129.9
16.6	126.6
E line of fir wood = 00	
21.3	121.9
17.3	125.9
14.4	128.8
12.9	130.3
11.0	132.2
9.9	133.3
9.9	133.3

π
143.18

1/4	9.5	133.7
+6	8.2	135.0
cb	7.6	135.6
N	5.2	138.0
	0+25	
N	4.9	138.3
+7	7.9	135.3
cb	8.3	134.9
1/4	10.2	133.0
⊕	10.5	132.7
+5	11.0	132.2
1/4	12.0	131.2
cb	14.5	128.7
S	18.2	125.0
S+15	23.0	120.2
S+25	25.3	117.9
	0+50	
S-25	28.2	117.0
S-15	23.4	119.8
1/4	19.0	124.2
S	14.6	128.6
cb	11.9	131.3
1/4	10.6	132.5
+2	10.5	132.7
⊕	10.5	132.7
+6	10.1	133.1
1/4	9.7	133.5

H.I.
143.18

31

+3	9.4	133.8
cb	8.2	135.0
+3	7.7	135.5
N	4.5	138.7
T.P.	7.88	140.97
	10.09	133.09
	0+67	
N	2.7	138.3
+3	3.0	138.0
+6	5.0	136.0
cb	5.2	135.8
+5	7.6	133.4
1/4	7.9	133.1
⊕	8.4	132.6
+3	8.6	132.4
1/4	10.5	130.5
cb	12.9	128.1
S	16.8	124.2
S+15	21.9	119.1
S+25	25.1	115.9
	0+79	
S-25	26.2	114.8
S-15	22.5	118.5
S	16.1	124.9
cb	14.4	126.6
+6	12.1	128.9
1/4	11.2	129.8

H.I.
190.97

+5	8.8	132.2
ϕ	8.6	132.4
1/4	8.2	132.8
+2	7.8	133.2
+4	6.2	134.8
cb	5.3	135.7
+5	5.3	135.7
+8	3.2	137.8
N	2.9	138.1
	1700	
N	3.0	138.0
cb	6.3	134.7
1/4	8.0	133.0
ϕ	8.4	132.6
+1	8.4	132.6
+5	10.0	131.0
1/4	11.5	129.5
cb	14.7	126.3
S	17.7	123.3
S+8	21.0	119.9
+15	23.0	118.0
+25	25.3	115.7
	1725	
S-25	29.0	117.0
S-15	22.0	119.0
-5	20.8	120.2

H.I.
190.97

11.0

32

S	19.0	122.0
cb	15.0	126.0
1/4	11.7	129.3
ϕ	8.1	132.9
1/4	8.0	133.0
+5	7.7	133.3
cb	6.9	134.1
N	2.8	138.2
	1750	
N	1.8	139.2
+2	2.9	138.1
cb	5.9	135.1
+3	7.1	133.9
1/4	7.8	133.2
ϕ	7.7	133.3
+1	7.8	133.2
1/4	11.1	129.9
+3	12.3	128.7
cb	13.6	127.4
+6	15.6	125.4
S	16.5	124.5
+7	18.6	122.4
+15	20.0	121.0
+25	22.2	118.8
	1775	
S-25	19.5	121.5

H.I.
140.97

S-	14.3	126.7
cb	10.9	130.1
+3	10.5	130.5
1/4	9.2	131.8
+6	6.9	134.1
ϕ	6.7	134.3
1/4	6.7	134.3
cb	5.5	135.5
+5	4.1	136.9
N	1.8	139.2
2400 W Line of Guy ^{50st}		
N	2.1	138.9
cb	4.8	136.2
1/4	5.3	135.7
ϕ	5.6	135.4
+1	5.5	135.5
1/4	7.3	133.7
cb	9.4	131.6
S	12.8	128.2
S+25	19.4	121.6
ϕ		
S-25	20.3	120.7
S	12.2	128.8
cb	8.8	132.2
1/4	6.9	134.1
+5	5.3	135.7

140.97

33

ϕ	9.9	136.6
1/4	3.8	137.2
cb	2.4	138.6
+8	0.9	140.1
TP	4.39	143.93
N	1.93	137.54
	3.0	140.9
E Line of Guy = 00		
N	2.1	141.8
+4	2.8	141.1
+8	4.3	139.6
cb	4.7	139.2
1/4	5.5	138.4
ϕ	6.1	137.8
1/4	9.1	134.8
cb	11.8	132.1
S	16.0	127.9
+10	19.2	124.7
+25	23.5	120.4
O+25		
S-25	23.0	120.9
S-8	18.5	125.4
S	16.0	127.9
cb	13.0	130.9
1/4	10.3	133.6
+3	8.9	135.0
ϕ	6.3	137.6

H.I.
143.93

+2	5.2	138.7
1/4	5.1	138.8
cb	4.6	139.3
+2	3.8	140.1
+7	2.1	141.8
N	1.1	142.8
	0450	
N	0.3	143.6
cb	4.3	139.6
1/4	5.0	138.9
+3	5.0	138.9
£	6.4	137.5
+4	7.0	134.9
1/4	10.1	133.8
cb	12.0	131.9
S	14.7	129.2
S+8	17.6	126.3
S+20	20.4	123.5
S+25	21.0	122.9
	0475	
S-25	20.0	123.9
S	14.4	129.5
cb	10.9	133.0
1/4	8.8	135.1
£	6.0	137.9
+3	4.4	138.5

H.I.
143.93

34

1/4	4.7	139.2
cb	4.0	139.9
N	1.4	142.5
	1100	
N	0.6	143.3
+5	3.2	140.7
cb	3.8	140.1
1/4	4.1	139.8
£	4.4	139.5
1/4	4.0	139.9
+1	5.8	138.1
cb	9.2	134.7
S	13.2	130.7
S+25	19.4	124.5
	1107 Stone steps on North ✓	
	online Bottom step etc 2.89	141.04
	+14 £ Single Garage on North	
	on line dirt floor etc 3.3	140.6 ✓
	1117	
S-25	19.0	124.9
S	12.3	131.6
cb	8.8	135.1
+5	6.2	137.7
1/4	5.2	138.7
£	3.7	140.2
1/4	3.8	140.1

193.93

cb		3.2	140.7
N		2.7	141.2
Tp	7.01	147.20	3.19
		140.79	
		142.5	
N		2.7	145.1
+7		6.9	141.4
cb		7.0	140.8
1/4		7.3	140.5
2		7.7	140.1
+5		9.5	138.3
1/4		9.8	138.0
cb		12.6	135.2
S		15.8	132.0
S+25		22.8	125.0
		145.0	
S-25		22.3	125.5
S-15		19.0	128.8
S		15.5	132.3
f7		13.4	134.4
cb		13.0	134.8
1/4		10.6	137.2
2		7.5	140.3
+2		6.8	141.0
1/4		6.8	141.0
cb		6.2	141.6
+7		5.9	142.4

197.80

		2.8	145.0
		1.7	146.1
		145.2	
		1.7	146.1
cb		5.8	142.0
+2		6.4	141.4
1/4		6.9	140.9
+6		6.8	141.0
2		7.9	140.4
1/4		10.7	137.1
+5		12.3	135.5
cb		13.3	134.5
S		15.5	132.3
		147.5	
S-35		30.0	117.8
S-28		29.5	123.3
S-20		26.0	125.8
S 7		18.1	129.7
S		15.3	132.5
cb		13.3	134.5
1/4		11.3	136.5
2		8.1	139.7
+2		7.2	140.6
1/4		6.8	141.0
cb		5.6	142.2
+5		3.8	144.0

H.I.
147.80

N	1.8	146.0
	2101 W. Line of Paterbaugh	
N	1.7	146.1
+5	3.8	144.0
cb	5.7	142.1
1/4	7.0	140.8
+5	7.4	140.4
ϕ	8.6	139.2
1/4	11.8	136.0
cb	14.5	133.3
S	17.5	130.3
S+25	25.0	122.8
S+28	26.2	121.6
	ϕ	
S-25	28.0	119.8
S	18.3	129.5
cb	14.5	133.3
1/4	11.8	136.0
ϕ	8.7	139.1
+3	7.2	140.6
1/4	7.4	140.4
cb	6.6	141.2
+8	4.3	143.5
N	3.3	144.5
	E Line of Paterbaugh = 00	
N	2.0	145.8

H.I.
147.80

11.0

35

+1	3.9	143.9
cb	6.9	141.4
1/4	6.9	140.9
+4	7.1	140.7
ϕ	8.9	139.4
1/4	12.2	135.6
cb	14.7	133.1
S	18.3	129.5
S+25	25.0	122.8
	0+25	
S-25	24.7	123.1
S-10	21.0	126.8
S	18.0	129.8
cb	14.8	133.0
1/4	12.6	135.2
ϕ	9.6	138.2
+5	6.8	141.0
1/4	5.8	142.0
cb	4.9	143.4
N	2.8	145.0
TP	9.18	155.98
	1.50	196.30
	0+39	Single Garage on North
	24° Back	Basement of Building
	5.09	150.39
	0+50	
N	9.9	146.1
cb	11.0	144.5

H.I.
155.98

1/4	126	142.9
¢	17.0	138.5
1/4	20.0	135.5
cb	22.0	133.5
S	24.9	130.6
S+25	33.0	122.5
	0+80	
S-40	38.5	117.0
S-5	34.4	121.1
S-20	31.6	123.9
S	24.4	131.1
cb	20.4	135.1
1/4	17.8	137.7
¢	15.7	139.8
+4	13.9	141.6
1/4	11.6	143.9
cb	10.4	145.1
N	9.0	146.5
	0+91	
N	8.7	146.8
cb	9.9	145.6
+5	10.5	145.0
1/4	11.3	144.2
¢	14.9	140.6
+4	16.3	139.2
1/4	18.7	136.8

H.I.
155.98

36

cb	22.7	132.8
S	28.5	127.0
S+25	34.8	120.7
S+90	38.7	116.8
	1+0	
S-40	38.0	117.5
S-25	33.6	121.9
S	29.6	125.9
cb	26.0	129.5
1/4	22.3	133.2
¢	17.0	138.5
1/4	14.8	143.7
+5	9.~	146.3
cb	9.0	146.5
N	8.3	147.2
	1+11	
N	7.7	147.8
cb	7.4	148.1
+4	8.8	146.7
+6	10.7	144.8
1/4	12.7	142.8
¢	17.4	138.1
1/4	22.3	133.2
cb	26.0	129.5
+6	27.7	127.8
S	28.5	127.0

HZ
155.98

120

S+25	31.9	123.6
+90	373	118.2
	1+17	
S	258	129.7
S+3	265	129.0
+6	270	128.5
+8	252	130.3
cb	245	131.0
1/4	218	133.7
1/4	195	136.0
1/4	147	140.8
+5	126	142.9
+6	8.1	147.4
cb	7.9	147.6
N.	7.3	148.2
	1+25	
N	6.7	148.8
+6	6.5	149.0
cb	8.4	147.1
+5	12.3	143.2
1/4	12.2	143.3
1/4	16.1	139.4
1/4	20.0	135.5
+2	22.0	133.5
+6	22.0	133.5
2b	22.0	133.5

X
155.98

37

S	21.5	134.0
S+10	24.0	131.5
S+25	29.2	126.3
	1+40	
S-50	36.0	119.5
S-25	28.0	127.5
S	16.6	138.9
cb	12.4	143.1
+5	10.9	144.6
1/4	11.1	144.4
+2	11.9	143.6
1/4	12.1	143.4
+5	9.8	145.7
1/4	8.5	147.0
+3	7.1	148.4
+4	5.8	149.7
cb	4.9	150.6
+4	5.6	149.9
+7	5.1	150.4
N	5.2	150.3
	1+54	
N	3.0	152.5
cb	3.3	152.2
1/4	2.9	152.6
+3	3.6	151.9
1/4	4.0	151.5

	HI			
	155.98			
1/4		6.1	149.4	
cb		8.6	146.9	
S		14.4	141.1	
S+10		20.3	135.2	
S+5		26.6	128.9	
S+35		30.0	125.5	
		17.71		
S-35		28.0	127.5	
S		12.8	142.7	
cb		6.8	148.7	
1/4		3.5	152.0	
⊕		1.5	154.0	
+4		0.1	155.4	
1/4		1.3	154.2	
+2		0.4	155.1	
cb		0.3	155.2	
+3		0.2	155.3	
+4		1.2	154.3	
+5		1.1	154.4	
T.P.	10.53	165.53	0.99	154.99
N			8.0	155.5
			17.89	
N			3.2	162.3
+6			6.9	158.6
cb			7.7	157.8
1/4			7.9	157.6

	HI			
	165.52			
				38
				157.9
				156.8
				153.9
				151.9
				148.2
				146.6
				152.1
				130.8
				128.0
				27° 00' 90" W Line Torrence 50' S
				130.5
				140.6
				149.1
				152.0
				153.8
				156.2
				157.5
				158.9
				159.8
				159.8
				159.9
				159.3
				164.3
				175.16
				163.92
				168.5

175.16

+5	86	166.6
+8	11.0	164.2
cb	11.2	164.0
1/4	11.3	163.9
ϕ	10.9	164.3
1/4	14.6	160.6
cb	18.5	156.7
s	23.5	151.7
St 25	32.0	142.8
St 40	38.4	136.8
E line of Torrence = 00		
S-40	34.5	140.7
S-8	19.8	155.4
S	16.5	158.7
cb	12.9	162.8
1/4	9.7	165.5
+4	8.0	167.2
ϕ	7.9	167.3
1/4	8.3	166.8
cb	8.5	166.7
+4	8.5	166.7
+7	6.2	169.0
N	4.4	170.8
O+25		
N	0.0	175.2
+2	1.0	174.2

13.0

25.3

12.0

13.0

175.16

+3	4.1	171.1
+6	5.4	169.8
cb	5.7	169.5
+1	4.8	170.4
1/4	4.8	170.4
ϕ	4.8	170.6
+6	5.2	170.0
1/4	5.7	169.5
cb	8.4	166.8
S	13.1	162.1
St 10	18.7	156.5
St 20	24.1	151.1
St 35	30.0	145.2
O+43		
S-40	33.4	141.8
S-30	29.7	145.5
S-20	26.4	148.8
S-8	20.0	155.2
S	12.7	162.5
+5	9.6	165.6
cb	7.6	168.6
1/4	4.1	171.1
+3	2.6	172.6
ϕ	2.5	172.7
1/4	3.7	172.5
cb	2.4	172.8

39

	H.I. 175.6		12.0 11.0		H.I. 186.30		12.5 12.5		40
+6		1.8	173.4	1/4		11.4	174.9		
+7		0.2	175.0	cb		11.6	174.7		
T.P.	11.38	186.30	0.24	174.92	+7	10.9	175.4		
+9		10.2	176.1	N		8.0	178.3		
N		8.5	177.8		0+70				
		0+50		N		7.9	178.4		
N		9.2	177.1	+3		10.1	176.2		
+4		11.7	174.6	cb		10.0	176.3		
cb		12.7	173.6	1/4		9.7	176.6		
1/4		12.5	173.8	2		9.8	176.5		
2		12.9	173.9	1/4		15.0	171.3		
+5		13.3	173.0	cb		21.6	164.7		
1/4		14.9	171.4	S		23.0	163.3		
+2		18.0	168.3	S+18		26.0	160.3		
cb		19.2	167.1	S+30		29.5	156.8		
S		26.1	160.2	S+40		34.0	152.3		
+7		32.5	153.8	TP	1.58	184.56	3.32	182.98	
		0+58				0+88			
S-40		38.5	147.8	S-40		23.0	161.6		
S-23		34.7	151.6	S-30		20.4	164.2		
S-8		32.5	153.8	S-15		16.6	168.0		
S		29.9	156.4	S		11.9	172.7		
cb		22.7	163.6	cb		9.8	174.8		
+3		21.0	165.3	+6		7.8	176.8		
1/4		16.0	170.3	1/4		7.5	177.1		
2		11.0	175.3	2		5.8	178.8		

HZ
184.56

1/4	6.0	178.6
cb	6.5	178.1
+6	6.2	178.4
+7	5.2	179.4
N	4.3	180.3
	1700	
N	2.5	182.1
ts	5.1	179.5
cb	5.5	179.1
+3	5.6	179.0
+4	4.8	179.8
1/4	4.4	180.2
ts	4.5	180.1
1/4	6.1	178.5
cb	7.0	177.6
S	9.6	175.0
S+16	10.2	174.4
S+26	13.9	170.7
S+40	20.5	164.1
	1725	
S-40	19.0	165.6
S-24	7.3	176.3
S	6.2	178.4
cb	4.7	179.9
+5	4.0	180.6
1/4	3.2	181.4

HZ
189.56

HZ
194.56
41

+6	1.0	183.6
ts	0.9	183.7
1/4	0.7	183.9
cb	1.7	182.9
TP	11.55	194.53
+8	8.9	185.6
N	7.3	187.2
	1750	
N	4.1	190.4
+2	5.3	189.2
cb	7.2	187.3
1/4	7.8	186.7
ts	7.6	186.9
1/4	9.2	185.3
cb	10.7	183.8
S	12.6	181.9
S+20	16.0	178.5
S+30	24.0	170.5
S+40	30.2	164.3
	1775	
S-40	24.2	170.3
S-25	21.5	173.0
S-10	14.8	179.7
S	10.4	184.1
+4	7.6	186.9
+9	5.6	188.9

HI
194.53

1 CB	5.5	189.0
1/4	5.2	189.3
+ 1/4	5.3	189.2
+ 1/4	5.0	189.5
+ 1/4	5.1	189.4
CB	4.0	190.5
N	2.0	192.5
N	0.0	194.5
2400 W. Line of Neale 50' St		
+ N	0.0	194.5
+ 1/4	2.3	192.2
1 CB	3.4	191.1
1/4	3.5	191.0
1/4	3.7	190.8
1/4	3.4	191.1
CB	3.7	190.8
+ 1/4	4.8	189.7
S	6.5	188.0
+ 1/4	11.6	182.9
+ 20	16.0	178.5
+ 40	24.0	170.5
W. Line + 2		
S-40	24.0	170.5
- 9	11.6	182.9
S	6.5	188.2
CB	3.6	190.9

HI
194.53

80

42

1/4	3.4	191.1
1/4	3.7	190.8
1/4	3.5	191.0
CB	3.4	191.1
N	2.7	191.8
W. Line of Neale		
N	1.6	192.9
CB	2.2	192.3
1/4	2.4	192.1
1/4	2.5	192.0
1/4	2.8	191.7
CB	3.0	191.5
+ 1/4	2.6	191.9
S	9.0	190.5
+ 10	10.2	184.3
+ 19	11.7	182.8
+ 32	17.8	176.7
S+40	21.0	173.5
E. Line of Neale		
S-40	21.0	173.5
S-18	12.0	182.5
S	2.1	192.4
+ 4	0.1	194.4
T.P.	10.03	202.60
10.03 202.60	1.96	192.57
CB	7.8	194.8
1/4	8.9	193.7

Note: Keating has been 250' from Neale to S. 1/4.

43
20260

2			9.0	193.6
1/4			9.4	193.2
cb			9.1	193.5
N			8.7	193.9
Rod on Existing cb SE end of Neale & Keating			9.39	193.21
T.P.	12.60	214.87	0.33	202.27
T.P.	12.29	227.03	0.13	214.74
TP	13.06	239.88	0.21	226.82
TP	13.14	252.95	0.07	239.81
TP	12.17	264.97	0.65	252.30
TP	6.71	269.86	1.32	263.15
check on BM F.W.B.F.	Pringle & Washington		4.76	265.10
				265.07
				.03

43

Bliss
Quernit
Holbein
Jacobson
6/21/28
on NW BP
Silverado &
Eads

X. Sections Eads Street La Jolla
from Silverado to S. End

80.57
14' obs
18' 1/2 S

+	HZ	-	Elev
7.85	99.80		91.95

0100 = Skine of Silverado

on having
same as Ground

W. Topcb		6.73	93.07
G		7.29	92.80
1/4		6.70	93.10
1/4		6.36	93.44
1/4		6.22	93.58
G		6.33	93.47
E Topcb		5.73	94.07
0150			
E Topcb		5.13	94.67
G		6.1	93.7
1/4		5.7	94.1
1/4		5.6	94.2
1/4		6.1	93.7
G		6.9	92.9
W Topcb		6.10	93.70
1700			
W Topcb		5.91	94.39
G		6.3	93.5
1/4		5.5	94.3
1/4		4.9	94.9
1/4		5.0	94.8
G		5.5	94.3
E Topcb		4.43	95.37

99.80

1750

E Topcb	3.83	95.87
G	4.6	95.2
1/4	4.4	95.4
1/4	4.3	95.5
1/4	4.9	94.9
G	5.7	94.1
W Topcb	4.82	94.98
2100		
W Topcb	4.17	95.64
G	5.0	94.8
1/4	4.4	95.4
1/4	3.8	96.0
1/4	3.8	96.0
G	3.7	96.1
E Topcb	3.20	96.60
2150		
E Topcb	2.70	97.10
G	3.3	96.5
1/4	3.3	96.5
1/4	3.2	96.6
1/4	3.8	96.0
G	4.4	95.4
W Topcb	3.66	96.14
3100		
W Topcb	3.52	96.28
G	4.2	95.6

44

H.I.
99.80

1/4	3.8	96.0
1/4	3.1	96.7
1/4	3.2	96.6
G	3.9	96.7
E Topcb	2.61	99.29
3790 Brk. Cb. E. side		
E Topcb	2.71	97.09
G	3.5	96.3
1/4	3.7	96.1
1/4	3.6	96.2
1/4	4.1	95.7
G	4.8	95.0
W Topcb	3.73	96.07
4100		
W Topcb	5.37	94.73
G	6.3	93.5
1/4	5.8	94.0
1/4	5.2	94.6
1/4	5.3	94.5
G	5.7	94.1
E Topcb	4.7.6	95.04
4450		
E Topcb	6.53	93.27
G	7.4	92.7
1/4	6.9	92.9
1/4	6.8	93.0

H.I.
99.80

45

1/4	7.2	92.6
T.P.	196	99.60
G	7.16	92.64
G	2.9	92.2
W Topcb	1.69	92.96
5700 50° N. line of Kline St		
W Topcb	3.01	91.59
G	3.7	90.9
1/4	3.3	91.3
1/4	2.8	91.8
1/4	3.2	91.4
G	3.6	91.0
E Topcb	3.04	91.56
N.C.S.		
E on Topcb	3.10	91.50
E on Ground	3.9	90.7
Cb	3.6	91.0
1/4	3.4	91.2
1/4	3.1	91.5
1/4	3.4	91.2
Cb	3.8	90.8
W on Ground	3.9	90.7
W on Topcb	3.06	91.54
N. 1/4		
W	4.0	90.60
Cb	3.9	90.7
1/4	3.7	90.9

80° 57'
19' 00"
13' 19"

HZ.
99.60

ϕ	3.5	91.1
1/4	3.7	90.9
cb	3.8	90.8
E	3.9	90.7
ϕ		
E	3.9	90.7
cb	4.0	90.6
1/4	4.0	90.6
ϕ	3.5	90.7
1/4	4.0	90.6
cb	4.1	90.5
W	4.0	90.6
	5/4	
W	4.6	90.0
cb	4.6	90.0
1/4	4.4	90.2
ϕ	4.3	90.3
1/4	4.4	90.2
cb	4.6	90.0
E	4.6	90.0
	S cb	
E on Top cb	4.99	90.1
E on Ground	5.3	89.3
cb	5.1	89.5
1/4	4.0	90.0
ϕ	4.6	90.0

HZ
99.60

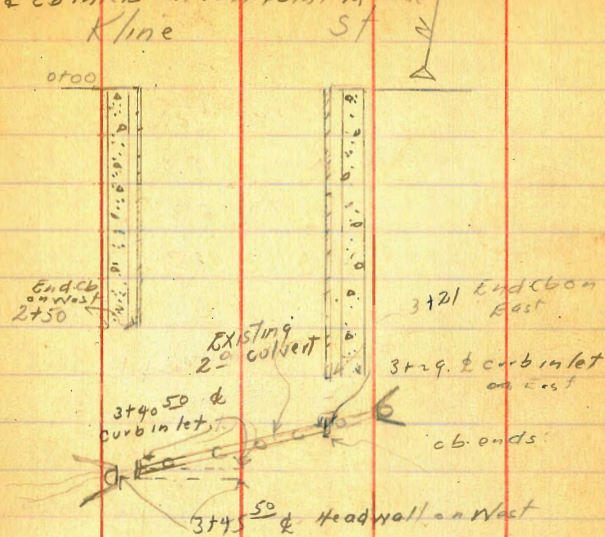
16

1/4	4.7	89.9
cb	5.1	89.5
W on Ground	5.2	89.4
W on Top cb	4.97	90.1
	S. line of Khie = 00	
W. Top cb	4.52	90.08
E	5.5	89.1
1/4	5.2	89.4
ϕ	5.0	89.6
1/4	5.0	89.6
E	5.3	89.3
E Top cb	4.46	90.14
	0+50	
E Top cb	6.65	87.95
E	7.2	87.2
1/4	7.0	87.6
ϕ	7.1	87.5
1/4	7.4	87.2
E	7.6	87.0
W. Top cb	6.98	87.62
	1+00	
W. Top cb	9.54	85.06
E	10.0	84.6
1/4	9.7	84.9
ϕ	9.4	85.2
1/4	9.2	85.4

#1
99.60

G		9.5	85.1
E Top cb		8.77	85.83
		17.50	
E		10.93	83.67
G		11.6	83.0
1/4		11.5	83.1
E		11.8	82.8
1/4		12.2	82.4
G		12.6	82.0
W Top cb		12.09	82.56
T.P.	1.39	84.08	11.91
		21.00	
W Top cb		3.95	80.13
G		4.5	79.6
1/4		4.0	80.1
E		3.4	80.7
1/4		2.9	81.2
G		3.2	80.9
E Top cb		2.99	81.64
		21.50	
E Top cb		4.32	79.86
E		5.0	79.1
1/4		5.0	79.1
E		5.4	78.7
1/4		6.0	78.1
E		6.3	77.8

Sketch of Eads Street to Jolla
between the S line of Kline & the
N line of Silver showing location of
existing cb & cb inlets at low point in grade



Silver Street

HZ
89.08

W Topcb	5.98	78.10
W	5.5	78.6
	2+97	B.K. in cb Grade on East
W	5.5	78.6
+4	6.3	77.8
+11	6.3	77.8
cb	7.1	77.0
+5	7.7	76.4
1/4	7.2	76.9
±	6.6	77.5
1/4	6.3	77.8
G	6.3	77.8
E Topcb	5.98	78.10
	3+21	End. cb on East
E	5.7	78.4
E Topcb	6.14	77.84
G	7.3	76.8
+3	6.9	77.2
1/4	7.0	77.1
±	7.2	76.9
1/4	7.7	76.4
+9	8.4	75.7
cb	7.2	76.9
+2	6.0	78.1
W	5.6	78.5

3+29 ± catch Basin on E

HZ
89.08

99.4

48

Rod Topcb	6.07	78.01
Rod on curb entrance	7.06	77.02
	3+35	
W	6.1	78.0
+6	6.2	77.9
+13	7.1	77.0
cb	8.0	76.1
1/4	7.7	76.4
±	7.2	76.9
1/4	6.9	77.2
+7	6.9	77.2
cb	6.0	78.1
E	5.4	78.7
	3+40 ±	± catch Basin on W
Topcb	8.08	76.0
Rod on curb entrance	9.07	75.01
	3+45	± E. West of Proplon R. Headwall and outlet
Top Headwall	8.62	75.46
Flow line of Outlet	11.94	73.14
W	8.2	75.9
+2	7.3	76.9
+6	7.4	76.7
+13	7.5	76.6
cb	8.8	75.3
+2	8.4	75.7
1/4	7.7	76.4

H.I.
89.08

ϕ	7.2	76.9
1/4	6.9	77.2
+10	7.0	77.1
cb	6.4	77.7
+6	5.8	78.3
E	5.6	78.5
	3763	
E	5.7	78.4
+7	6.1	78.0
+11	6.0	78.1
cb	6.5	77.6
1/4	6.8	77.3
ϕ	7.1	77.0
3/4	7.5	76.8
+10	8.1	76.0
cb	8.0	76.1
W	7.8	76.3
	3776	
W	7.2	76.9
+12	6.9	77.2
cb	7.3	76.8
+4	7.8	76.3
1/4	7.3	76.8
ϕ	6.8	77.3
1/4	6.7	77.4
+10	6.7	77.4

H.I.
89.08

49

cb	6.1	78.0
+4	5.8	78.3
E	5.4	78.7
	4700	
E	5.1	79.0
+12	5.4	78.7
cb	5.9	78.2
+4	6.6	77.5
1/4	6.3	77.8
ϕ	6.4	77.7
1/4	6.9	77.2
+10	7.3	76.8
cb	6.9	77.2
W	6.8	77.3
	4700	
W	6.2	77.9
cb	6.5	77.6
+4	7.1	77.0
1/4	6.4	77.7
ϕ	6.2	77.9
1/4	6.1	78.0
+10	6.5	77.6
cb	5.3	78.8
+12	5.0	79.0
E	4.5	79.6

H.I.
84.08

9150

E	3.5	80.6
+13	4.2	79.9
cb	4.6	79.5
+2	5.3	79.8
1/4	5.2	79.9
¢	5.1	79.0
1/4	5.5	79.6
+10	6.0	79.1
+12	6.0	79.1
cb	5.5	79.6
+2	5.1	79.0
W	5.1	79.0

9180

W	3.8	80.3
cb	4.2	79.9
+2	5.4	79.7
+4	5.1	79.0
1/4	4.5	79.6
¢	4.1	80.0
1/4	4.9	79.7
G	4.1	80.0
E Topcb	3.39	80.7
E	2.9	81.2
E Topcb	2.91	81.2
G	3.9	80.2

80.57
1900s 13 1/2
N. line of Silver

H.I.
84.08

50

1/4	3.8	80.3
¢	3.4	80.7
1/4	3.7	80.4
+7	4.3	79.8
+9	4.7	79.9
cb	3.7	80.4
+2	2.9	81.2
W	3.0	81.1
TP	7.67	88.90
	2.85	81.23
	N cb	
W	8.3	80.6
cb	8.8	80.1
1/4	8.1	80.8
¢	7.8	81.1
1/4	8.2	80.7
G	8.2	80.7
E Topcb	7.39	81.51
	N 1/4	
Topcb	7.06	81.84
G	7.7	81.2
1/4	7.8	81.1
¢	7.5	81.4
1/4	7.7	81.2
cb	8.0	80.9
W	8.0	80.9

H.I.
8890

W	7.0	81.9
cb	7.2	81.3
1/4	7.3	81.6
ϕ	6.9	82.0
1/4	7.4	81.5
G	7.4	81.5
E Topcb	6.75	82.15
	3 1/4	
Topcb	6.44	82.46
G	7.2	81.7
1/4	7.1	81.8
ϕ	6.7	82.2
1/4	7.0	81.9
cb	7.1	81.8
W	6.9	82.0
	5cb	
W or Topcb	5.74	83.16
W or Ground	6.7	82.2
cb	7.0	81.9
1/4	6.8	82.1
ϕ	6.4	82.5
1/4	6.7	82.2
G	6.8	82.1
E Topcb	6.13	82.97
	S. Line of Silver = 00	
E Topcb	5.71	83.19

H.I.
8890

51

G	6.3	82.6
1/4	6.3	82.6
ϕ	6.0	82.9
1/4	6.4	82.5
G	6.4	82.5
N Topcb	5.72	83.70
	0.50	
W Topcb	4.10	84.80
G	4.8	84.1
1/4	4.5	84.4
ϕ	4.4	84.5
1/4	4.6	84.3
G	4.6	84.3
E Topcb	4.00	84.90
	1.00	
E Topcb	2.33	86.57
G	3.0	85.9
1/4	2.8	86.1
ϕ	2.7	86.2
1/4	2.9	86.0
G	3.2	85.7
W Topcb	2.52	86.98
	1.50	
Topcb	0.87	88.03
G	1.6	87.3
1/4	1.3	87.6

H.I.
88.90

£		1.0	87.9
1/4		1.1	87.8
G		1.1	87.8
E Topcb		0.58	88.32
T.P.	10:34	98.66	0.58
		2+00	
E Topcb		8.65	90.01
£		9.2	89.4
1/4		9.1	89.5
£		9.0	89.6
1/4		9.3	89.3
G		9.5	89.1
W Topcb		8.92	89.74
		2+50	
W Topcb		7.29	91.37
G		7.9	90.7
1/4		7.5	91.0
£		7.4	91.2
1/4		7.3	91.3
G		7.5	91.1
E Topcb		6.83	91.83
		3+00	
E Topcb		5.11	93.55
G		5.9	92.7
1/4		5.6	93.0
£		5.6	93.0

H.I.
98.66

52

1/4		5.8	92.8
£		6.0	92.6
W Topcb		5.68	92.88
		3+50	
W Topcb		9.03	94.83
G		9.5	94.1
1/4		9.1	94.6
£		3.9	94.7
1/4		9.0	94.6
£		9.0	94.6
E Topcb		3.23	95.43
		9+00	
E Topcb		1.59	97.07
£		2.1	96.5
1/4		2.2	96.4
£		2.3	96.3
1/4		2.5	96.1
G		3.0	95.6
W Topcb		2.39	96.27
		9+50	
W Topcb		0.67	97.99
£		1.3	97.3
1/4		1.0	97.6
£		0.6	98.0
1/4		0.9	98.2
£		0.9	98.2

H.I.
98.66

T.P.	9.22	107.32	0.56	98.10
E Topcb			8.50	98.82
			4+70	
E Topcb			7.98	99.84
G			8.1	99.2
1/4			8.0	99.3
¢			8.1	99.2
1/4			8.3	99.0
G			8.8	98.5
W Top Cb			8.32	99.00

5400 N. line of Pearl
on Paving

W Topcb			7.70	99.42
G			8.21	99.11
1/4			7.77	
¢			7.36	99.96
1/4			7.32	
G			7.39	99.93
E Topcb			6.74	100.58

see sketch page 62
S line of Pearl = 00
on Paving

E Topcb			5.29	102.08
G			5.82	101.50
1/4			5.59	
¢			5.60	101.72
1/4			6.05	
G			6.62	100.70
W Topcb			6.15	101.17

H.I.
107.32

0+05

W Topcb			6.01	101.31
G			6.5	100.8
1/4			5.9	101.4
¢			5.4	101.9
1/4			5.5	101.8
+11			5.5	101.8
cb			5.0	102.3
E			4.5	102.7
7.95	111.70	3.07		104.25

See sketch page 62
Hydant Pearl
+ 20.5

0+50

E			7.9	103.8
+11			8.1	103.7
cb			8.3	103.4
+4			9.3	102.4
1/4			9.0	102.7
¢			8.8	102.9
1/4			9.3	102.4
E			9.6	103.1
W Topcb			9.13	102.57

1400

W			7.66	104.04
G			8.3	103.4
1/4			5.0	103.7
¢			7.4	104.3
1/4			7.5	104.2
+9			7.9	103.8

53

HZ
111.70

cb	6.7	105.0
E	6.0	105.7
	1750	
E	5.0	106.7
cb	5.9	106.3
+3	6.5	105.2
1/4	6.2	105.5
⊕	6.0	105.1
1/4	6.5	105.2
G	6.9	104.8
W Topcb	6.20	105.50
	2100	
W Topcb	9.80	106.90
G	5.4	106.3
1/4	5.0	106.7
⊕	9.6	107.1
1/4	4.8	106.9
E +11	5.3	106.4
cb	4.1	107.6
E +1	3.8	107.9
G E	3.4	108.3
	2450	
E	1.7	110.0
1/4 +1	2.0	109.7
G +13	2.4	108.3
W cb	2.9	108.8

HZ
111.70

54

+2	3.7	108.0
1/4	3.1	108.6
⊕	3.2	108.5
1/4	3.7	108.0
E	4.0	107.7
W Topcb	3.19	108.51
	3400	
W Topcb	1.77	109.93
⊕	2.5	109.2
1/4	2.2	109.5
⊕	1.8	109.9
1/4	1.9	109.8
+9	2.3	109.4
26	1.0	110.7
+13	0.6	111.1
E	0.1	111.6
T P	10.98	120.91
	3750	
E	7.9	113.0
+2	8.4	112.5
cb	9.3	111.6
H	10.2	110.7
1/4	9.7	111.2
⊕	9.5	111.4
1/4	10.0	110.9
G	10.3	110.6

H.I.
120.91

W Top Cb	9.78	111.13
	9+00	
W Top Cb	8.31	112.41
G	8.9	112.0
1/4	8.6	112.3
⊕	8.2	112.7
1/4	8.4	112.5
G	8.4	112.5
E Top Cb	7.34	113.57
E	6.5	114.4
	4+50	
E Top Cb	6.10	114.81
G	7.0	113.9
1/4	7.0	113.9
⊕	6.9	114.0
1/4	7.4	113.4
G	7.7	113.2
W Top Cb	7.01	113.91
	5+00	
W Top Cb	5.78	115.13
G	6.4	114.5
1/4	6.2	114.7
⊕	5.6	115.3
1/4	5.6	115.3
G	5.7	115.2
E Top Cb	4.92	115.99

H.I.
120.91

55

	5+50	
E Top Cb	3.68	117.23
G	4.5	116.4
1/4	4.5	116.4
⊕	4.3	116.6
1/4	5.0	115.9
G	5.3	115.6
W Top Cb	9.63	116.28
	6+00	
W Top Cb	3.41	117.50
G	4.0	116.9
1/4	3.9	117.0
⊕	3.2	117.7
1/4	3.3	117.6
G	3.5	117.4
E Top Cb	2.42	118.49
	6+50	
E Top Cb	1.16	119.75
G	2.3	118.6
1/4	2.2	118.7
⊕	2.0	118.9
1/4	2.5	118.4
G	2.9	118.0
W Top Cb	2.19	118.72
	7+00	
W Top Cb	0.93	119.99
G	1.5	119.4

H.I.
120.91

1/4		1.1	119.8
¢		0.7	120.2
1/4		0.8	120.1
G		0.7	120.2
E Top cb		0.00	120.91
TP	9.11	129.72	0.30 120.61
		7+50	
E Top cb		7.57	122.15
G		8.3	121.4
1/4		8.5	121.2
¢		8.4	121.3
1/4		8.7	121.0
G		9.3	120.4
W Top cb		8.55	121.17
		8+00	
W Top cb		7.33	122.39
G		7.8	121.9
1/4		7.5	122.2
¢		7.1	122.6
1/4		7.3	122.4
G		7.0	122.7
E Top cb		6.35	123.37
		8+50	
E Top cb		5.19	124.58
G		5.9	123.8
1/4		6.0	123.7

H.I.
129.72

56

¢		5.9	123.8
1/4		6.3	123.4
G		6.7	123.0
A Top cb		6.07	123.45
		9+00	
W Top cb		4.81	124.91
G		5.6	124.1
1/4		5.0	124.7
¢		4.5	125.2
1/4		4.7	125.0
G		4.5	125.2
E Top cb		3.81	125.91
		9+50	
E Top cb		2.61	127.11
G		3.3	126.4
1/4		3.2	126.5
¢		3.3	126.4
1/4		3.7	126.0
G		4.2	125.5
W Top cb		3.60	126.12
		10+00	
W Top cb		2.37	127.35
G		3.1	126.6
1/4		2.6	127.1
¢		2.2	127.5
1/4		2.2	127.5

H.I.
129.72

G		1.9	127.8
E Topcb		1.41	128.31
T.P.	7.58	136.55	0.75
		107.50	
E Topcb		6.99	129.66
G		7.7	128.8
1/4		7.7	128.8
⊥		7.8	128.7
1/4		8.3	128.2
G		8.8	127.7
W Topcb		8.09	128.51
	on page 107	75	N. Line of Center
W Topcb		7.93	129.25
G		8.02	128.52
1/4		7.48	
⊥		7.10	129.45
1/4		6.99	
G		7.09	129.76
E Topcb		6.90	130.25
		S. Line of Center	30.00
E Topcb		5.93	130.62
G		6.55	130.00
1/4		6.47	130.1
⊥		6.60	129.95
1/4		6.98	129.6
G		7.50	129.05

H.I.
136.55

57

W Topcb		6.93	129.62
-W		6.6	130.0
		0.10	
W		7.1	129.5
Cb		7.1	129.5
1/4		6.7	129.9
⊥		6.9	130.2
1/4		6.9	130.2
G		6.3	130.3
E Topcb		5.86	136.89
		0.150	136.9
E Topcb		5.99	131.06
G		5.9	130.7
1/4		6.1	130.5
⊥		6.0	130.6
1/4		6.7	129.9
1/8		7.2	129.4
Cb		6.7	129.9
W		6.3	130.3
		1.00	
W		6.0	130.6
Cb		6.4	130.2
1/3		6.8	129.8
1/4		6.2	130.4
⊥		5.6	131.0
1/4		5.5	131.1

HZ
136.55

E	5.6	131.0
E Top cb	5.06	131.49
	1+35	
E Top cb	4.78	131.87
G	5.4	131.2
1/4	5.3	131.3
E	5.3	131.3
1/4	6.0	130.6
G	6.5	130.1
W Top cb	5.86	130.69
W	5.8	130.8
	1+85	
W	5.0	131.6
W Top cb	5.45	131.10
G	6.1	130.5
1/4	5.6	131.0
E	5.0	131.6
1/4	5.0	131.6
E	5.1	131.5
E Top cb	4.37	132.78
	2+00	
E Top cb	4.18	132.87
G	4.8	131.8
1/4	4.9	131.7
E	4.9	131.7
1/4	5.5	131.1

HZ
136.55

x11	6.0	130.6
cb	5.6	131.0
+3	5.0	131.6
W Line	4.8	131.8
	2+30	
W Line	4.7	131.9
cb	5.2	131.4
+2	5.7	130.9
1/4	5.1	131.5
E	4.6	132.0
1/4	4.5	132.1
G	4.7	131.9
E Top cb	3.87	132.78
	3+00	
E Line	2.9	133.7
+4	3.6	133.0
E Top cb	3.07	132.78
G	4.5	132.1
1/4	4.5	132.1
E	4.5	132.1
1/4	5.1	131.5
+11	5.5	131.1
cb	5.4	131.2
+5	4.9	131.7
W Line	4.8	131.8

58

H.Z.
136.55

3+50

W. Line	4.7	131.9
+7	4.8	131.8
cb	5.1	131.2
+2	5.7	130.9
1/4	5.2	131.4
E	4.6	132.0
1/4	4.6	132.0
+12	4.6	132.0
cb	4.3	132.3
+3	4.0	132.6
E. Line	3.2	133.4

4+50

E. Line	3.8	132.8
E. Top cb	4.42	132.43
6	5.0	131.6
1/4	4.9	131.7
E	5.0	131.6
1/4	5.6	131.0
6	6.1	130.5
W. Top cb	5.51	131.14
W. Line	5.1	131.5

4+50

W. Line	5.3	131.3
W. Top cb	5.92	130.63
6	6.5	130.1
1/4	6.2	130.4

H.Z.
136.55

59

4	5.5	131.1
1/4	5.6	131.0
E	5.5	131.1
E Top cb	9.95	131.60
5+60 N. Line of Pulville		
E	5.0	131.6
E Top cb	5.43	131.44
E	6.0	130.6
1/4	6.0	130.6
E	5.9	130.7
1/4	6.5	130.1
+10	7.0	129.6
cb	6.5	130.1
W.	5.7	130.9
T.P	3.05	134.17
5.43		131.12
N. cb		
W	3.5	130.7
cb	4.4	129.8
1/4	4.1	130.1
E	3.5	130.7
1/4	3.7	130.5
cb	3.5	130.7
+13	2.9	131.3
E	1.0	133.2
N. 1/4		
E	3.2	131.0

60.57
10.16
10.45

HZ
139.17

cb	3.6	130.6
+9	3.7	130.5
1/4	3.5	130.7
ϕ	3.6	130.6
1/4	4.2	130.0
cb	4.5	129.7
W	4.1	130.1
	ϕ	
W	3.9	130.3
+10	4.4	129.8
cb	4.6	129.6
+5	4.7	129.5
1/4	4.3	129.9
ϕ	3.7	130.5
1/4	3.7	130.5
cb	3.7	130.5
E	2.9	131.3
	5/4	
E	2.7	131.5
cb	3.8	130.4
1/4	3.7	130.5
ϕ	3.8	130.4
1/4	4.5	129.7
+9	4.7	129.5
+5	5.1	128.5
+8	5.6	128.6

HZ
139.17

+9	4.8	129.4
cb	4.5	129.7
W	4.1	130.1
	S cb	
W	3.8	130.4
cb	4.8	129.4
+6	5.1	129.1
+7	6.0	128.2
+8	5.6	128.6
+9	4.8	129.4
1/4	4.6	129.6
ϕ	3.9	130.3
1/4	3.9	130.3
+10	4.3	129.9
cb	3.9	130.3
+4	3.7	130.5
+13	3.3	130.9
E	1.9	132.8
	S 4.10	
E	3.2	131.0
+12	4.1	130.1
cb	4.7	129.5
+5	4.9	129.3
1/4	4.2	130.0
ϕ	4.1	130.1
1/4	4.8	129.4

60

H.I.
134.17

+3	4.9	129.3
+4	6.3	127.9
+7	6.5	127.7
+8	5.5	128.7
cb	5.3	128.9
+3	4.9	129.3
W	4.5	129.7
	0+30	
W	5.6	128.6
+5	5.9	128.3
cb	6.2	128.0
+2	7.1	127.1
+9	7.5	126.7
+10	6.6	127.6
1/4	6.3	127.9
E	5.3	128.9
1/4	5.5	128.6
+10	6.1	128.1
cb	5.8	128.4
+9	5.2	129.0
E	4.7	129.5
	0+50	
E	5.4	128.8
cb	6.0	128.2
+6	6.6	127.6
1/4	6.0	128.2

H.I.
134.17

61

E	5.9	128.3
1/4	6.7	127.5
+11	7.8	126.4
cb	6.8	127.4
+3	6.5	127.7
W	6.3	127.9
	1+00	
W	7.7	128.5
cb	8.1	126.1
+5	9.2	125.0
1/4	8.1	126.1
E	7.5	124.7
1/4	7.5	126.7
+10	8.3	125.9
cb	7.5	126.7
+11	7.0	127.2
E	6.8	127.4
	1+50	
E	8.4	125.8
cb	8.9	125.3
+7	9.1	125.1
1/4	8.8	125.4
E	8.6	125.6
1/4	9.4	124.8
+5	9.8	124.4
cb	9.8	124.4

H.I.
139.17

W	9.3	124.9
	1+90	
W	10.8	123.4
cb	10.3	123.9
1/4	10.2	124.0
ϕ	9.9	124.3
1/4	9.8	124.4
cb	9.1	125.1
E	8.8	125.4
	1+92	
E	8.7	125.5
cb	9.1	125.1
+11	10.2	124.0
1/4	10.0	124.2
ϕ	10.7	123.5
+2	12.1	122.1
1/4	12.6	121.6
+11	12.9	121.3
cb	10.8	123.4
W	10.8	123.4
	1+95	
W	10.8	123.4
+7	10.7	123.5
+10	13.3	120.9
cb.	13.2	121.0
1/4	12.6	121.6

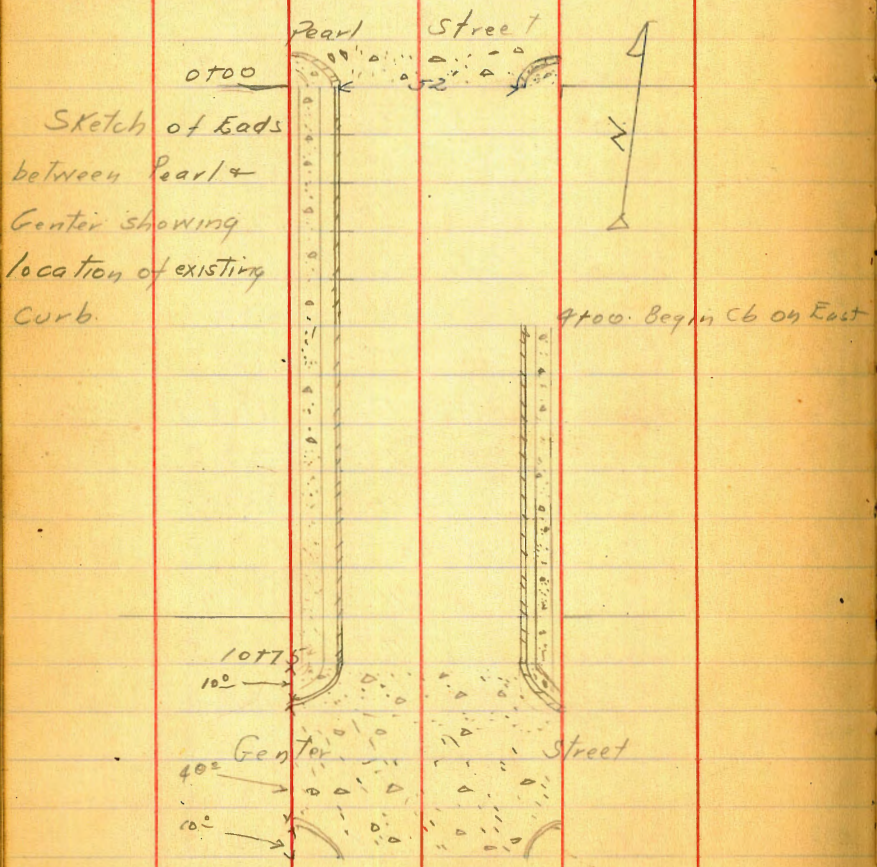
H.I.
139.17

62

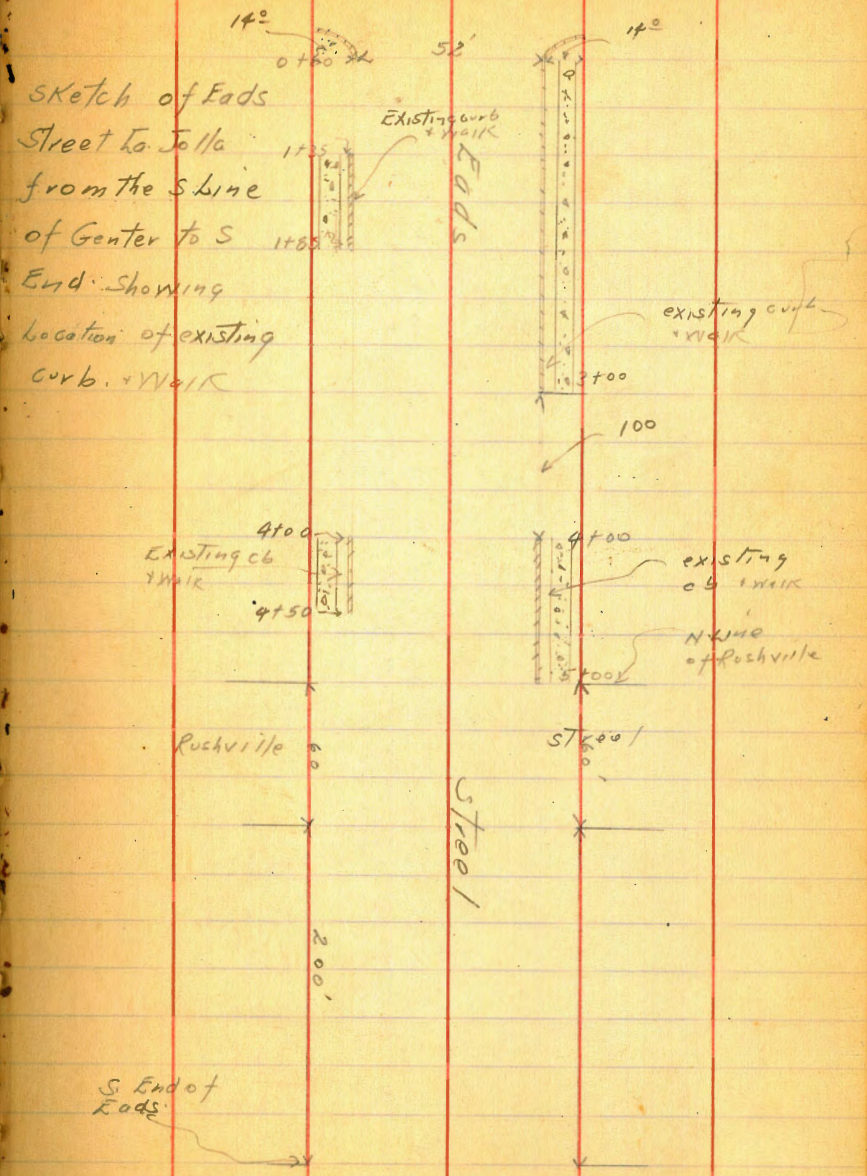
+3	10.5	123.7
ϕ	10.8	123.4
1/4	10.0	124.2
cb	8.9	125.3
E	8.5	125.7
	1+96	
E	8.5	125.9
cb	9.0	125.2
1/4	9.8	124.4
ϕ	10.5	123.7
1/4	10.4	123.8
cb	11.1	123.1
+1	13.2	121.0
+6	13.3	120.9
+7	10.7	123.5
W	10.8	123.4
	2+00	
W	11.3	122.9
+5	11.7	122.5
+6	13.8	120.4
+8	13.6	120.6
+9	11.1	123.1
cb	10.9	123.3
1/4	9.7	124.5
ϕ	10.1	124.1
1/4	9.9	124.8

H.I.
139.17

Cb			8.9	125.3
E			2.5	125.7
T.P.	1.87	123.02	13.02	121.15
T.P.	2.51	113.08	12.95	110.57
Check on SW RP P.M. Draper + Center			6.60	106.48 ✓



Genter St



Bliss
Hobbs
Jacobson
4/6/18
BM N.E. Top of
Pushville
Eads

Additional sections of Eads
Street South of Pushville

80.51
19 cbs
13 1/45

133.9

64

2.79 133.86 131.12

Continuation from Page 63

2 + 05

E	7.9	126.0
cb	8.3	125.6
1/4	8.0	125.9
+5	8.6	125.3
⊕	9.9	124.5
1/4	9.7	124.2
+8	9.7	124.2
+11	11.4	122.5
cb	11.9	122.0
+10	13.2	120.7
X	12.7	121.2
	2 + 09 35 = 2709 20	
X	13.9	120.5
+9	13.6	120.3
+7	11.0	122.9
+10	11.9	122.0
cb	11.4	122.5
+9	11.1	122.8
+11	8.8	125.1
1/4	9.4	124.5
+6	9.3	124.6
+10	8.2	125.7
⊕	8.7	125.2

+7

1/4

cb

+5

+11

E

Set BM
light pole
SW at Edge of Eads

7.8 126.1

6.5 127.4

6.1 127.8

6.1 127.8

6.8 127.1

6.5 127.4

9.9 123.87

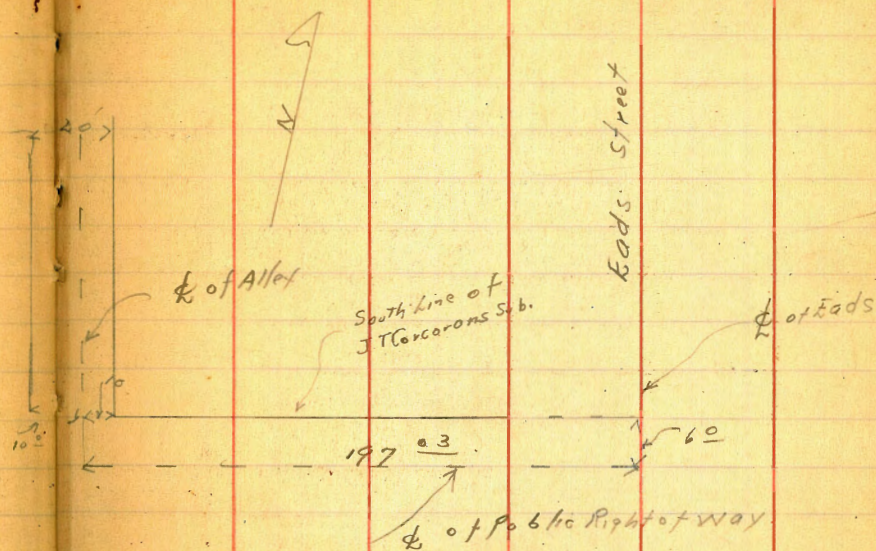
12510

Bliss
Holbeck
Jacobson

7/6/28

Sewer Levels on the Public Right of Way
6' South of the South End of Eads from the
E of Eads West to E of Alley West of Eads

	3.69	127.56	123.87
0+00 E of Eads	0.9	126.7	
0+07	2.7	124.9	
0+10	2.9	124.7	
0+14	1.6	126.0	
0+18	4.9	123.2	
0+25	0.6	127.0	
0+27	0.7	126.9	
0+38	6.8	120.8	
0+40 W Line of Eads	6.9	120.7	
1+00	8.9	118.7	
1+50	10.0	117.6	
1+85	9.9	117.7	
1+97 E of Alley	10.9	117.2	



Bliss
7/6/08

Levels to determine the Elevation
of floor line in Sewer Man Hole 228³⁵ South
of the S line of Kline St La Jolla

B.M. S.E. B.P.
Kline + Fay

1.46 97.95 95.99

T.P.

1.72 89.11 10.06 87.39

Rod on rim
of Man Hole

9.33

Rod on floor of Man Hole

15.01

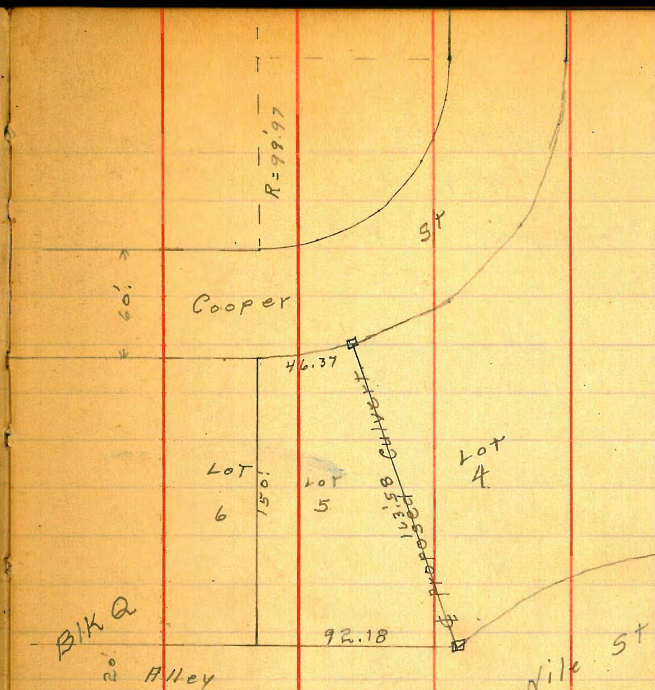
Levels for Drain Cooper St to Nile Bet Lots 4 & 5 BIK & Montclair

8-20-28
mills

π 290.85

00 = W. Line Cooper St			+ 1.5	292.3
0 + 10 E			0.1	290.7
+ 15			2.1	288.8
+ 20			2.2	288.7
+ 30			2.2	288.7
+ 40			4.7	286.2
+ 50			6.3	284.6
+ 60 = E. Line Cooper = 0100			9.0	281.9
0 + 10			11.2	279.7
0 + 20			15.3	275.6
T.P.	0.80	278.96	12.69	278.16
T.P.	0.13	266.21	12.88	266.08
0 + 46			6.5	259.7
0 + 50			10.4	255.8
T.P.	0.10	253.30	13.01	253.20
0 + 75			9.4	243.9
0 + 84			13.2	240.1
T.P.	0.47	241.01	12.76	240.54
0 + 91			7.2	233.8
1 + 00			9.7	231.3
T.P.	0.17	228.50	12.68	228.33
1 + 15			4.5	224.0
1 + 40			13.4	215.1
T.P.	0.65	216.32	12.93	215.57
1 + 63 ^{SE} = W. Line Alley			3.64	212.62

Continued Next Page.



continued
 π 216.22

1 + 92

6.8

2 + 02

8.9

2 + 20

11.4

2 + 23

13.3

Wash.

67

Saw ev Levels & All 45 in
 BIKs P + Q Montclair
 + BIKs U + T City Hts.

8-20-28
 miller

BLK. P.

301.79

0+00 = Existing DE. 190's of S. Line Cooper St.	2.5	299.3
+50	3.3	298.5
1+00	4.4	297.4
+50	5.1	296.7
2+00	5.8	296.0
+50	6.7	295.1
3+00	7.1	294.7
+50	7.9	293.9
4+00	9.0	292.8
4+30 = N. Line Maple St	9.8	292.0
4+60 = " " "	10.8	291.0
4+90 = S. Line " "	11.7	290.1
+50	13.1	288.7
T.P.	0.38	289.53
5+50	7.8	287.7
6+00	3.7	285.8
+50	6.7	282.8
+75	7.8	281.7
7+00	9.8	279.7
+60	13.5	276.0
+44	15.8	273.7
+68	15.4	274.1
+76	17.8	271.7
+81	15.3	274.2

289.53

68

T.P.	0.35	276.98	12.90	276.63
8+00			2.9	274.1
+50			6.4	270.6
9+00			10.4	266.6
+50			16.1	260.9
T.P.	0.53	264.88	12.63	264.35
9+85			9.5	255.4
T.P.	3.12	260.80	7.20	257.68
9+97			11.8	249.0
10+00			9.6	251.2
10+10			8.8	252.0
10+25			11.4	249.4
+50			14.6	246.2
+90			15.2	245.6
11+10 = N. Line Kalmia			12.7	248.1
T.P.	7.20	264.88	3.12	257.68
T.P.	12.43	276.68	0.63	264.25
				BIK T.
☉ Kalmia St.			2.3	274.4
N. line Kalmia St = 0+00			1.7	275.0
T.P.	8.32	283.36	1.64	275.04
0+50			7.4	276.0
1+00			7.6	275.8
+50			7.3	276.1
2+00			4.6	276.8
2+50			6.4	277.0

BIKT. City H.B.

283.36

3+00			6.1	277.3
+50			5.2	278.0
4+00			4.7	278.7
+50			5.2	278.2
5+00			5.2	278.2
+50			5.6	277.8
6+00			7.0	276.4
6+20 = S. line Maple St.			8.6	274.8
+30			9.6	273.8
+34			11.4	272.0
+50 = E. Maple St			13.0	270.4
6+60			15.0	268.4
T.P.	0.01	270.51	12.86	270.50
6+65			3.4	267.1
6+80 = N. line Maple St			10.7	259.8
T.P.	0.04	258.18	12.37	258.14
7+03			10.5	247.7
T.P.	3.89	251.75	10.31	247.87
7+10 M.H. 200. canyon line $\Delta 45^{\circ} 00' L$			9.71	242.04
7+16			12.7	239.1
+20			10.9	240.9
+30			5.5	246.3
T.P.	12.78	263.97	0.56	251.19
+45			12.0	252.0
+80			1.8	262.2
8+10			0.6	263.4
+30			5.4	258.6

Plat Page 71.

on H46

wash

263.97

8+85			4.6	259.4
+50			5.6	258.4
+70			4.6	259.4
+77			3.0	261.0
T.P.	12.44	273.71	2.70	261.27
+91			11.1	262.6
9+10			11.8	261.9
+33			8.8	264.9
+50			7.7	266.0
+65			4.5	269.2
10+10			4.2	269.5
+33			4.4	269.3
+50			6.0	267.7
+75			12.3	267.4
T.P.	0.64	261.24	13.11	260.60
11+05			14.5	246.7
T.P.	0.19	248.55	12.88	248.36
11+31			4.0	244.6
+46			7.3	241.3
+52			9.6	239.0
+79			15.5	233.0
T.P.	0.53	235.98	13.10	235.45
+99			10.3	225.7
12+01			12.9	223.1
T.P.	0.33	223.49	12.82	223.16
12+25			4.7	218.8

69

Alley BIK, Q. Montclair

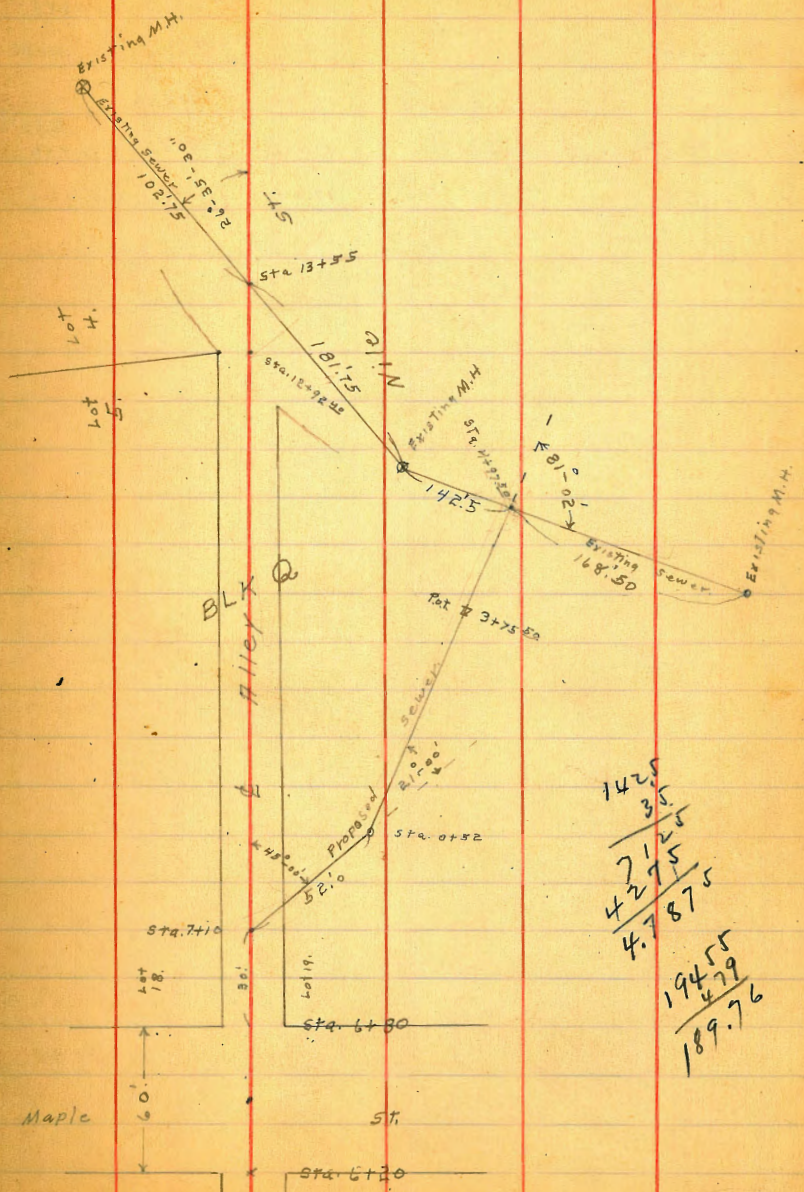
223.49

70

12+33			4.4	219.1	
12+70			9.6	213.9	
12+92.40 = 90° from	four BIK Lots 4+5		11.8	211.7	
T.P. ch. on Hub.	BIK Q. Montclair	1.21	213.83	10.87	212.62 = 212.62 Page 67
13+00			2.8	211.0	
+25			4.5	209.3	
+26			5.9	207.9	
+39			4.9	208.9	
13+55 P.I. with Existing Sewer			7.00	206.8	on stub
Existing M.H.			9.21	204.62	Flow Line
" "			19.17	194.66	" "
T.P.			13.01	200.82	

Center Line

6' Alley BLK Q	0.43	242.47	242.04	00 =
0+00 = 7+10				9+10
0+10		4.5	238.0	Wash. +10
0+37		7.0	235.5	Wash. 9+47
0+52 M.H. 21' 00" L		7.18	235.3	on Hub 9+62
above				
4' E. of A in wash		8.3 X	234.2	
T.P.	1.85	235.58	8.74	233.73
0+92		1.9	233.7	10+02
8' E. of above in wash		5.2 X	230.4	
1+10		6.8	228.8	Wash 10+20
1+50		9.2	226.4	10+60
6' W. of above in wash		10.1 X	225.5	
1+66		9.5	226.1	10+76
7' W. of above in wash		11.6 X	224.0	
2+00		13.0	222.6	11+10
6' W. of above in wash		14.2 X	221.4	
T.P.	0.68	223.42	12.84	222.74
2+22		1.4	222.0	11+32
9' W. of above in wash		3.6 X	219.8	
2+40		4.4	219.0	11+50
3+00		9.6	213.8	Wash 12+10
3+35		11.6	211.8	12+45
T.P.	0.45	210.93	12.94	210.48
3+75.50 P.O.T.		2.51	208.42	12+65.2 = W. Hub V.M. Conn 12+85.5 on Hub
4+00		4.7	206.2	13+10
4+62		11.8	199.1	13+72
4+7		13.1	197.8	13+77



142.5
 + 3.5

 146.0
 + 212.5

 358.5
 + 47.5

 406.0
 + 194.5

 600.5
 - 410.7

 189.8

 189.76

210.93

CHK of T.P. Page 70
210.93
10.11
200.82 = 200.82

72

4+72			12.3	198.6	13+82
4+90			14.6	196.3	14+00
T.P.	1.90	201.63	11.80	199.13	
4+97.50 P.E. with Existing sewer			4.02	197.0	14+07.5 on Hub
Existing M.H.			17.00	184.0	Flow Line

B.M. H.W.B.P.

Silverado + Eads +

H.I. — Elev
91.95

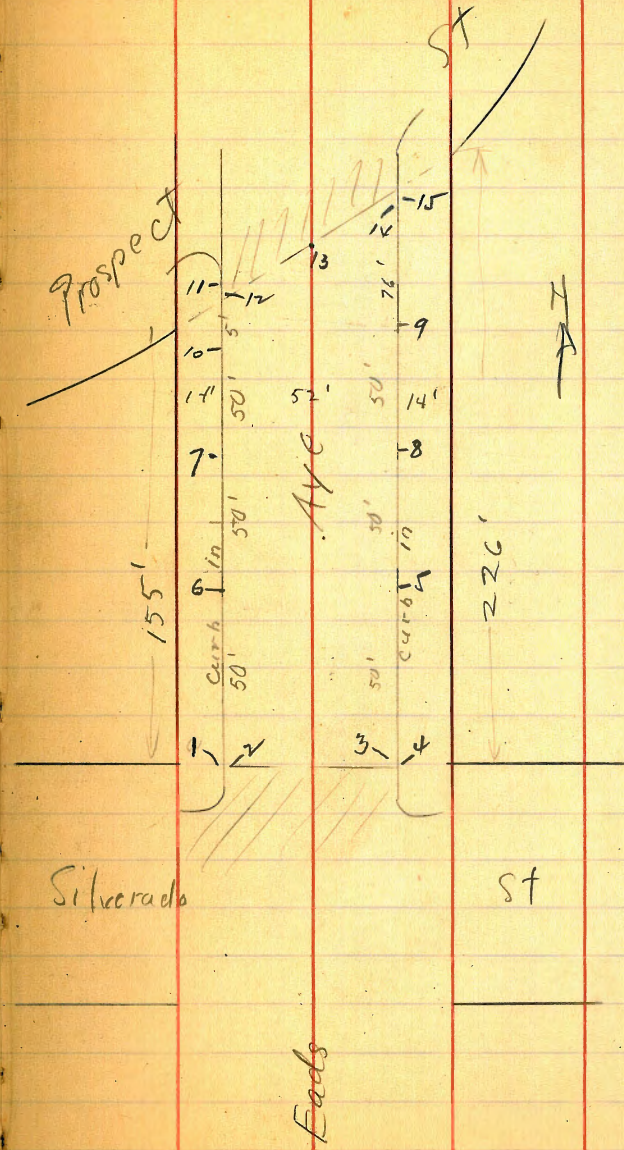
6.50 98.75

6.68	92.07	1
7.20	91.55	2
6.37	92.38	3
5.71	93.04	4
6.85	91.90	5
8.04	90.71	6
9.25	89.50	7
7.75	91.00	8
8.20	90.05	9
10.60	88.15	10
10.70	88.05	11
11.28	87.47	12
10.30	88.45	13
10.74	88.01	14
9.96	88.79	15

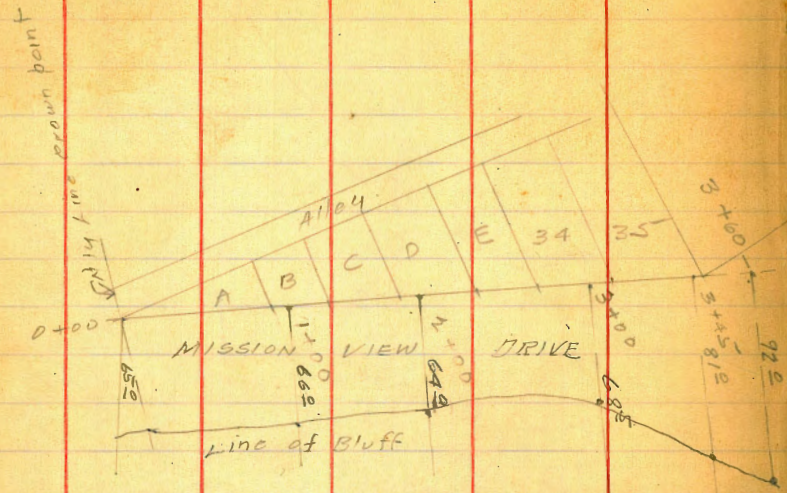
Diff
Cassm
9/20/28

X-sec. Eads Ave.
Silverado - Prospect

73

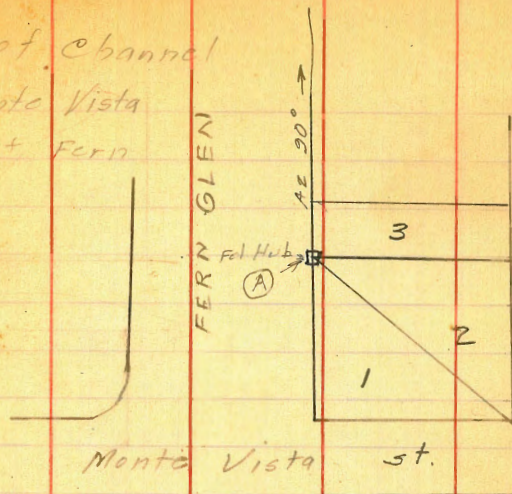


Oct 26-28
London



Location of Bluff From N¹4
Line of Crown point to Shasta St

To top of Channel
From Monte Vista
to Sea at Fern
Glenn



Beginning Point of stadia survey

Nail Pole				
B.M.	6.34	84.62		77.78
B.M.	0.15	77.40	7.37	77.25
T.P.	0.01	65.67	11.74	65.66
Hub NE cor. Lot 1			5.79	59.88

F.H. S.W.
S. L. S. Co.
Alameda, Cal.

74

Oct 27-28

London

Isbell

Morgan

Topog of channel

75

sta	Az	stadia	vert L	Red	Hor dist	diff	H.I	Elev.
Inst at A								59.88
B	311° 52'	2.64	-3° 08'		264.0	14.4		45.5
Inst at B							50.6	45.5 ✓
A		2.64	+3° 10'					
	167° 37'	1.99	+3° 21'		199.0	11.6		57.1
	175° 36'	1.62	+3° 54'		162.0	11.0		56.5
	199° 18'	0.92	+4° 35'		91.0	7.3		52.8
	265° 43'	0.42		5.8	42.0			44.8
	226° 40'	0.28		12.3	28.0			38.3
	187° 00'	0.76		6.9	76.0			43.7
	169° 04'	1.63		5.4	163.0			47.2
	158° 00'	1.62	+3° 31'		162.0	9.9		55.4
	150° 12'	0.73		0.4	73.0			50.2
	126° 30'	0.30		2.6	30.0			48.0
	87° 10'	0.35		13.2	35.0			37.4
	42° 46'	0.53		3.5	53.0			47.1
	350° 44'	0.54		8.8	54.0			41.8
	306° 58'	1.30	-4° 03'		129.0	9.1		36.4
	313° 25'	2.18	-3° 03'		218.0	11.5		34.0
	297° 37'	3.00	-2° 56'		300.0	15.3		30.2
	306° 18'	2.25	-4° 57'	UP 2	223.0	21.3		24.2
	297° 44'	1.34	-5° 20'	UP 5	133.0	17.4		28.1
	307° 36'	0.99	-9° 41'		96.0	16.4		29.1
	306° 35'	0.54	-13° 19'		51.0	12.1		33.4
	285° 20'	0.62		5.7	62.0			44.9

N.W. cor Monte Vista
 Surveyors place
 S.W. cor House
 Facing Monte Vista

Topog. of

Spann

76

Sta	Az	Stadia	Vert L	Rod	Hor. Dist	Dist	H.T.	Elev.	
	289° 37'	1.24		11.7	124.0		50.6	38.9	
	299° 07'	2.30	-2° 51'		230.0	11.4		34.1	
	284° 13'	2.82		8.4	282.0			42.2	
	285° 42'	3.95		11.1	395.0			39.5	
"C"	290° 39'	5.31	-1° 36'		531.0	14.0		31.5	
	Inst. at "C" oriented on "B"								
	44.1157	5.2					36.7	31.5v	
"B"		5.31	+1° 38'						
	84° 23'	1.25		6.7	125.0			30.0	
	109° 44'	2.25	-1° 35'	4.5	225.0	10.7		20.8	
	103° 22'	1.80	-4° 03'		179.0	12.6		18.9	
	87° 52'	1.84		6.0	184.0			30.7	
	78° 10'	1.83	-3° 09'		183.0	10.1		21.4	
	72° 00'	1.82		7.2	182.0			29.5	
	53° 48'	0.90	-6° 26'		89.0	10.0		21.5	
	67° 10'	1.00	-8° 15'		98.0	14.2		17.3	
	67° 56'	0.65	-16° 10'		60.0	17.3		14.2	
	99° 37'	0.80	-10° 19'		77.0	14.1		17.4	
	30° 47'	0.71	-15° 42'		66.0	18.5		13.0	
	23° 10'	1.09		11.7	109.0			25.0	
	237° 27'	0.80	-8° 47'		78.0	12.1		19.4	
	309° 45'	1.04	-8° 56'		101.0	16.0		15.5	
	305° 34'	1.82	-6° 25'		180.0	20.1		11.4	
	313° 24'	2.29	-5° 42'		226.0	22.6		8.9	
	311° 57'	2.30	-6° 55'	4.1	226.0	28.4		3.1	
	299° 33'	2.04	-8° 21'		200.0	30.0		1.5	

8

DIRECTIONS FOR USE OF TABLES

TABLE No. 1

Distance of slope stake from side or shoulder
stake for any width roadway, slope 1 1/2 to 1.
If ground is nearly level, the cut or fill at side
stake is located by the double entry method in
left column and top row. The number in body

of table in same row and column gives distance

from side stake to slope stake. If ground is not

level, the side stake and slope stake, lower target by this

amount if cut, else by this amount. Add this amount

to cut or fill and find distance in table. Set up

rod at this point and line of sight should cut

target.

TABLE No. 2

To find Tangent and External for curve of

any other degree, divide by degree of curve and

add correction found in column of corrections.

Degree of curve with a given T may be found

by dividing tangent (or external), opposite T by

given tangent (or external).

The distance from a point on the tangent to

the curve is very nearly the square of the tangent

length divided by twice the radius.

**IMPROVED TABLES
AND
INFORMATION**

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=10°	I	T	E	I=20°	I	T	E	I=30°
1°	50.00	.218	+	11°	551.70	26.500	+	21°	1061.9	97.577	+
10'	58.34	.297		10'	560.11	27.313	5° C	10'	1070.6	99.155	5° C
20'	66.67	.388	5° C.	20'	568.53	28.137		20'	1079.2	100.75	5° C.
30'	75.01	.491	T	30'	576.95	28.974	T	30'	1087.8	102.35	T
40'	83.34	.606	.03	40'	585.36	29.824	.06	40'	1096.4	103.97	.10
50'	91.68	.733	E	50'	593.79	30.686	E	50'	1105.1	105.60	E
2°	100.01	.873	.001	12°	602.21	31.561	.006	22°	1113.7	107.24	.013
10'	108.35	1.024		10'	610.64	32.447		10'	1122.4	108.90	
20'	116.68	1.188		20'	619.07	33.347		20'	1131.0	110.57	
30'	125.02	1.364		30'	627.50	34.259		30'	1139.7	112.25	
40'	133.36	1.552		40'	635.93	35.183		40'	1148.4	113.95	
50'	141.70	1.752		50'	644.37	36.120		50'	1157.0	115.66	
3°	150.04	1.964	10° C.	13°	652.81	37.070	10° C.	23°	1165.7	117.38	10° C.
10'	158.38	2.188	T	10'	661.25	38.031	T	10'	1174.4	119.12	T
20'	166.72	2.425	.06	20'	669.70	39.006	.13	20'	1183.1	120.87	.19
30'	175.06	2.674	E	30'	678.15	39.993	E	30'	1191.8	122.63	E
40'	183.40	2.934	.003	40'	686.60	40.992	.011	40'	1200.5	124.41	.025
50'	191.74	3.207	T	50'	695.06	42.004	T	50'	1209.2	126.20	T
4°	200.08	3.492	15° C.	14°	703.51	43.029	15° C.	24°	1217.9	128.00	15° C.
10'	208.43	3.790	T	10'	711.97	44.066	T	10'	1226.6	129.82	T
20'	216.77	4.099		20'	720.44	45.116		20'	1235.3	131.65	
30'	225.12	4.421		30'	728.90	46.178		30'	1244.0	133.50	
40'	233.47	4.755		40'	737.37	47.253		40'	1252.8	135.35	
50'	241.81	5.100	T	50'	745.85	48.341	T	50'	1261.5	137.23	T
5°	250.16	5.459	.09	15°	754.32	49.441	.19	25°	1270.2	139.11	.29
10'	258.51	5.829	E	10'	762.80	50.554	E	10'	1279.0	141.01	E
20'	266.86	6.211	.004	20'	771.29	51.679	.017	20'	1287.7	142.93	.038
30'	275.21	6.606	T	30'	779.77	52.818	T	30'	1296.5	144.85	T
40'	283.57	7.013		40'	788.26	53.969		40'	1305.3	146.79	
50'	291.92	7.432	E	50'	796.75	55.132	E	50'	1314.0	148.75	E
6°	300.28	7.863	20° C.	16°	805.25	56.309	20° C.	26°	1322.8	150.71	20° C.
10'	308.64	8.307	T	10'	813.75	57.498	T	10'	1331.6	152.69	T
20'	316.99	8.762	.13	20'	822.25	58.699	.26	20'	1340.4	154.69	.39
30'	325.35	9.230	E	30'	830.76	59.914	E	30'	1349.2	156.70	E
40'	333.71	9.710	.006	40'	839.27	61.141	.022	40'	1358.0	158.72	.051
50'	342.08	10.202	T	50'	847.78	62.381	T	50'	1366.8	160.76	T
7°	350.44	10.707	.16	17°	856.30	63.634	.32	27°	1375.6	162.81	.49
10'	358.81	11.224	E	10'	864.82	64.900	E	10'	1384.4	164.86	E
20'	367.17	11.753	.006	20'	873.35	66.178	.028	20'	1393.2	166.95	.065
30'	375.54	12.294	T	30'	881.88	67.470	T	30'	1402.0	169.04	T
40'	383.91	12.847		40'	890.41	68.774		40'	1410.9	171.15	
50'	392.28	13.413	E	50'	898.95	70.091	E	50'	1419.7	173.27	E
8°	400.66	13.991	25° C.	18°	907.49	71.421	25° C.	28°	1428.6	175.41	25° C.
10'	409.03	14.582	T	10'	916.03	72.764	T	10'	1437.4	177.55	T
20'	417.41	15.184	.16	20'	924.58	74.119	.32	20'	1446.3	179.72	.49
30'	425.79	15.799	E	30'	933.13	75.488	E	30'	1455.1	181.89	E
40'	434.17	16.426	.007	40'	941.69	76.869	.028	40'	1464.0	184.08	.065
50'	442.55	17.065	T	50'	950.25	78.264	T	50'	1472.9	186.29	T
9°	450.93	17.717	30° C.	19°	958.81	79.671	30° C.	29°	1481.8	188.51	30° C.
10'	459.32	18.381	T	10'	967.38	81.092	T	10'	1490.7	190.74	T
20'	467.71	19.058	.19	20'	975.96	82.525	.39	20'	1499.6	192.99	.59
30'	476.10	19.746	E	30'	984.53	83.972	E	30'	1508.5	195.25	E
40'	484.49	20.447	.008	40'	993.12	85.431	.034	40'	1517.4	197.53	.078
50'	492.88	21.161	T	50'	1001.7	86.904	T	50'	1526.3	199.82	T
10°	501.28	21.887	30° C.	20°	1010.3	88.389	30° C.	30°	1535.3	202.12	30° C.
10'	509.68	22.624	T	10'	1018.9	89.888	T	10'	1544.2	204.44	T
20'	518.08	23.375	.19	20'	1027.5	91.399	.39	20'	1553.1	206.77	.59
30'	526.48	24.138	E	30'	1036.1	92.924	E	30'	1562.1	209.12	E
40'	534.89	24.913	.008	40'	1044.7	94.462	.034	40'	1571.0	211.48	.078
50'	543.29	25.700	T	50'	1053.3	96.013	T	50'	1580.0	213.86	T

T = R tan ½ I

E = R exsec ½ I

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

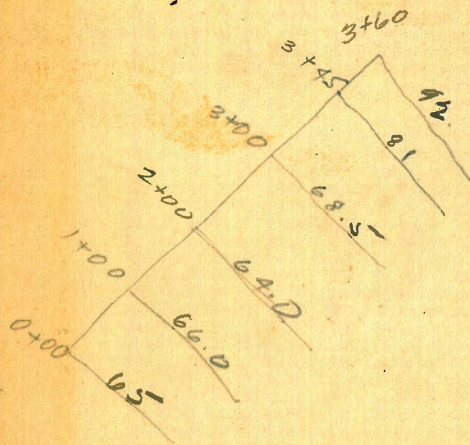
I	T	E	I=40°	I	T	E	I=50°	I	T	E	I=60°
31°	1589.0	216.3	+	41°	2142.2	387.4	+	51°	2732.9	618.4	+
10'	1598.0	218.7	5° C.	10'	2151.7	390.7	5° C.	10'	2743.1	622.8	5° C.
20'	1606.9	221.1		20'	2161.2	394.1		20'	2753.4	627.2	
30'	1615.9	223.5	T	30'	2170.8	397.4	T	30'	2763.7	631.7	T
40'	1624.9	226.0	.13	40'	2180.3	400.8	.17	40'	2773.9	636.2	.21
50'	1633.9	228.4	E	50'	2189.9	404.2	E	50'	2784.2	640.7	E
32°	1643.0	230.9	.023	42°	2199.4	407.6	.037	52°	2794.5	645.2	.056
10'	1652.0	233.4		10'	2209.0	411.1		10'	2804.9	649.7	
20'	1661.0	235.9		20'	2218.6	414.5		20'	2815.2	654.3	
30'	1670.0	238.4		30'	2228.1	418.0		30'	2825.6	658.8	
40'	1679.1	241.0		40'	2237.7	421.4		40'	2835.9	663.4	
50'	1688.1	243.5	E	50'	2247.3	425.0	E	50'	2846.3	668.0	E
33°	1697.2	246.1	10° C.	43°	2257.0	428.5	10° C.	53°	2856.7	672.7	10° C.
10'	1706.3	248.7	T	10'	2266.6	432.0	T	10'	2867.1	677.3	T
20'	1715.3	251.3	.26	20'	2276.2	435.6	.34	20'	2877.5	682.0	.42
30'	1724.4	253.9	E	30'	2285.9	439.2	E	30'	2888.0	686.7	E
40'	1733.5	256.5	.048	40'	2295.6	442.8	.075	40'	2898.4	691.4	.112
50'	1742.6	259.1	T	50'	2305.2	446.4	T	50'	2908.9	696.1	T
34°	1751.7	261.8	15° C.	44°	2314.9	450.0	15° C.	54°	2919.4	700.9	15° C.
10'	1760.8	264.5	T	10'	2324.6	453.6	T	10'	2929.9	705.7	T
20'	1770.0	267.2	.40	20'	2334.3	457.3	.51	20'	2940.4	710.5	.63
30'	1779.1	269.9	E	30'	2344.1	461.0	E	30'	2951.0	715.3	E
40'	1788.2	272.6	.070	40'	2353.8	464.6	.116	40'	2961.5	720.1	.168
50'	1797.4	275.3	T	50'	2363.5	468.4	T	50'	2972.1	725.0	T
35°	1806.6	278.1	20° C.	45°	2373.3	472.1	20° C.	55°	2982.7	729.9	20° C.
10'	1815.7	280.8	T	10'	2383.1	475.8	T	10'	2993.3	734.8	T
20'	1824.9	283.6	.53	20'	2392.8	479.6	.68	20'	3003.9	739.7	.84
30'	1834.1	286.4	E	30'	2402.6	483.4	E	30'	3014.5	744.6	E
40'	1843.3	289.2	.093	40'	2412.4	487.2	.151	40'	3025.2	749.6	.225
50'	1852.5	292.0	T	50'	2422.3	491.0	T	50'	3035.8	754.6	T
36°	1861.7	294.9	25° C.	46°	2432.1	494.8	25° C.	56°	3046.5	759.6	25° C.
10'	1870.9	297.7	T	10'	2441.9	498.7	T	10'	3057.2	764.6	T
20'	1880.1	300.6	.39	20'	2451.8	502.5	.68	20'	3067.9	769.7	.84
30'	1889.4	303.5	E	30'	2461.7	506.4	E	30'	3078.7	774.7	E
40'	1898.6	306.4	.065	40'	2471.5	510.3	.189	40'	3089.4	779.8	.283
50'	1907.9	309.3	T	50'	2481.4	514.3	T	50'	3100.2	784.9	T
37°	1917.1	312.2	30° C.	47°	2491.3	518.2	30° C.	57°	3110.9	790.1	30° C.
10'	1926.4	315.2	T	10'	2501.2	522.2	T	10'	3121.7	795.2	T
20'	1935.7	318.1	.093	20'	2511.2	526.1	.151	20'	3132.6	800.4	.225
30'	1945.0	321.1	E	30'	2521.1	530.1	E	30'	3143.4	805.6	E
40'	1954.3	324.1	.117	40'	2531.1	534.2	.189	40'	3154.2	810.9	.283
50'	1963.6	327.1	T	50'	2541.0	538.2	T	50'	3165.1	816.1	T
38°	1972.9	330.2	35° C.	48°	2551.0	542.2	35° C.	58°	3176.0	821.4	35° C.
10'	1982.2	333.2	T	10'	2561.0	546.3	T	10'	3186.9	826.7	T
20'	1991.5	336.3	.67	20'	2571.0	550.4	.85	20'	3197.8	832.0	.84
30'	2000.9	339.3	E	30'	2581.0	554.5	E	30'	3208.8	837.3	E
40'	2010.2	342.4	.065	40'	2591.0	558.6	.189	40'	3219.7	842.7	.283
50'	2019.6	345.5	T	50'	2601.1	562.8	T	50'	3230.7	848.1	T
39°	2029.0	348.6	40° C.	49°	2611.2	566.9	40° C.	59°	3241.7	853.5	40° C.
10'	2038.4	351.8	T	10'	2621.2	571.1	T	10'	3252.7	858.9	T

79.29
184
70.57
5762 NE

Proffert

ENGINEERING DEPARTMENT
CITY OF CALIFORNIA
SAN DIEGO

Delivered to St. Peter's
To St. Center -



1.8
125
18
70.7
8.91
890
1730
865

97.25
741
87.84

89.84

90.10
89.54
0.30

933
568
1501

N 73-51-40 E
N 57-15-40 E
16-36-20

N 57-15-40 E
40-05-10
17-10-30

N 39-64-70 E
N 40-05-70 E
18-12-40
21-52-30

16-36-26
17-10-30

33-46-50
21-52-30

55-39-40
20