

1257

1880

1880

1880

27-08
90-00-00
27-08
6 27 50 20

MICROFILMED

DEC 22 1964

Disc returned 8/18/75 7/18/79 M.H.

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CITY OF SAN DIEGO,
CALIFORNIA.

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Bliss
Halbeck
Jacobson
0/6/45
Bliss, Top Work
0/6/45 to Garnet

X. Sections Pendleton St Pacific
Beach from the S line of Garnet to
the N line of Pacific -

80's
20' obs
10' 45

1.29

14.7
37.29

EW
36.05

0100: S. Line Garnet

W	1.7	35.6
+5	1.9	35.4
+6	2.7	34.6
+19	4.0	33.3
cb	4.7	32.6
+2	5.0	32.3
+9	5.2	32.1
+5	4.4	32.9
1/4	4.4	32.9
E	4.4	32.9
1/4	4.5	32.8
cb	4.7	32.6
+10	5.5	31.8
+14	4.9	32.4
E	3.2	34.1
	05'S	
E	3.3	34.0
+5	5.2	32.1
+10	5.7	31.6
cb	5.2	32.1
1/4	4.8	32.5
E	4.6	32.7
1/4	4.4	32.9
+L	4.5	32.8

Plotted - 6-28-28 - C.B.H.

37.29

+7	5.2	32.1
cb	5.2	32.1
+1	5.0	32.3
+2	4.1	33.2
W	3.5	33.8
	25' South	
W	4.4	32.9
+17	4.6	32.7
+19	4.3	33.0
cb	5.5	31.8
+2	5.0	32.3
1/4	5.5	31.8
E	5.5	31.8
1/4	5.8	31.5
cb	5.9	31.4
+10	6.4	30.9
F18	6.4	30.9
E	5.2	32.1
	50'S	
E	6.3	31.0
+5	6.8	30.5
+10	7.1	30.2
cb	6.6	30.7
1/4	6.2	31.1
E	6.0	31.3
1/4	6.0	31.3

3729

cb	5.7	31.6
W	5.2	32.1
	0+72	<i>N line of Grandon</i>
W	6.1	31.2
+17	6.1	31.2
+18	6.5	30.8
cb	6.1	31.2
+8	6.4	30.9
1/4	7.0	30.3
¢	6.7	30.6
1/4	6.8	30.5
cb	7.0	30.3
+10	7.5	29.8
E	7.1	30.2
	1+01	33
E	8.5	28.8
cb	7.9	29.4
1/4	7.7	29.6
¢	7.5	29.8
+9	7.8	29.5
1/4	7.3	30.0
cb	6.6	30.7
+1	7.0	30.3
W	6.8	30.8
	1+25	
W	7.2	30.1

3729

2

cb	7.5	29.8
1/4	7.6	29.7
+2	8.2	29.1
¢	7.8	29.5
1/4	8.3	29.0
cb	8.5	28.8
+7	8.7	28.6
+9	9.4	27.9
+11	8.7	28.6
E	8.7	28.6
	1+50	
E	8.4	28.9
cb	8.6	28.7
1/4	8.6	28.7
¢	8.3	29.0
1/4	8.0	29.3
cb	7.7	29.6
W	7.6	29.7
	1+75	
W	7.6	29.7
+14	7.7	29.6
+18	8.7	28.6
cb	8.4	28.9
1/4	8.5	28.8
¢	8.5	28.8
1/4	8.9	28.4

37.29

+5	9.4	27.9
+8	9.1	28.2
cb	9.1	28.2
+8	9.5	27.8
+9	13.0	24.3
+11	13.0	24.3
+11.5	9.6	27.7
E	9.3	28.0
	1+9.4	
E	8.9	28.4
+6	8.7	28.6
+7	12.5	24.8
+13	11.8	25.5
+15	10.0	27.3
cb	9.9	27.4
1/4	9.6	27.7
ϕ	9.3	28.0
1/4	9.1	28.2
cb	9.0	28.3
+2	9.2	28.1
+4	10.2	27.1
+7	8.3	29.0
W	8.4	28.9
	2+0.0	
W	8.5	28.8
F14	9.0	28.3

37.29

3

+16	11.5	25.8
+18	11.3	26.0
+19	9.3	28.0
cb	9.2	28.1
1/4	9.4	27.9
ϕ	9.5	27.8
1/4	10.0	27.3
cb	10.2	27.1
+8	10.6	26.7
+10	12.3	25.0
E	14.0	23.3
	2+0.7	1/2 S Line Grand on East
E	12.5	26.8
cb	10.9	26.4
1/4	10.4	26.9
ϕ	9.8	27.5
1/4	9.6	27.7
cb	9.4	27.9
+3	9.8	27.5
+4	11.5	25.8
+6	11.4	25.9
+8	8.9	28.4
W	8.6	28.7
TP	2.63	30.36
	9.56	27.73
	2+2.9	53 S Line Grand on West
W	0.9	29.5

7
3036

+13	2.6	27.8
+15	5.1	25.3
+17	4.5	25.9
cb	4.2	26.2
1/4	4.6	25.8
E	4.9	25.5
1/4	5.3	25.1
+6	6.0	24.4
cb	5.9	24.5
E	7.0	23.4
	24.0	
E	7.0	23.4
cb	6.4	24.0
+3	6.6	23.8
1/4	6.1	24.3
E	5.7	24.7
1/4	5.7	24.7
+1	5.3	25.1
cb	5.0	25.4
+2	5.3	25.1
W	4.6	25.8
	27.4 ²⁵	N. D. of Horn blends
W	5.1	25.3
+15	5.8	24.6
cb	5.8	24.6
+8	6.0	24.4
1/4	6.4	24.0

7
3036

4

E	6.2	24.2
1/4	6.6	23.8
cb	6.7	23.7
E	7.4	23.0
	N. C. B.	
E	7.2	23.2
+8	6.8	23.6
+10	7.2	23.2
cb	6.9	23.5
+2	7.2	23.2
1/4	6.7	23.7
E	6.5	23.9
1/4	6.7	23.7
+1	6.9	23.5
E	6.3	24.1
cb	6.1	24.3
+7	6.2	24.2
W	5.5	24.9
	N. 1/4	
W	5.5	24.9
	6.0	23.4
+12	6.3	24.1
+13	6.3	24.1
cb	6.1	24.3
+8	6.4	24.0
+9	6.8	23.6
1/4	6.8	23.6

7
30.36

6	6.6	23.8
1/4	6.8	23.6
+8	7.3	23.1
+9	7.0	23.4
cb	7.0	23.4
+11	7.3	23.1
+12	6.8	23.6
E	7.3	23.1
E	7.5	22.9
+7	6.9	23.5
+9	7.4	23.0
cb	7.1	23.3
1/4	6.9	23.5
6	6.7	23.7
1/4	6.8	23.6
+12	7.0	23.4
+3	6.5	23.9
cb	6.3	24.1
+7	6.4	24.0
+8	6.0	24.4
W	5.6	24.8
	5 1/4	
14	5.6	24.8
+12	6.0	24.4
+13	6.6	23.8

7
30.36

5

cb	6.9	24.0
+7	6.5	23.9
+8	7.0	23.4
1/4	6.9	23.5
6	6.9	23.5
1/4	7.0	23.4
+8	7.6	22.8
+9	7.0	23.4
cb	7.3	23.1
+10	7.7	22.7
+12	6.9	23.5
E	7.6	22.8
	5cb	
E	7.8	22.6
+8	7.7	22.7
+10	7.9	22.5
cb	7.4	23.0
+1	7.7	22.7
1/4	7.3	23.1
6	7.1	23.3
1/4	7.2	23.2
+1	7.4	23.0
+12	6.8	23.6
cb	6.5	23.9
+7	6.7	23.7
+8	6.1	24.3

30.36

W	5.7	24.7
	S Line Hornblende = 00	
W	6.1	24.3
+11	6.0	24.4
+12	7.0	23.4
c6	6.8	23.6
+7	7.2	23.2
+8	7.5	22.9
1/4	7.4	23.0
ϕ	7.4	23.0
1/4	7.6	22.8
+8	7.9	22.5
c6	7.7	22.7
+10	8.1	22.3
E	8.2	22.2
	0+20	
E	8.6	21.8
+8	8.0	22.4
+10	8.7	21.7
c6	7.8	22.6
+1	8.1	21.3
1/4	7.5	22.9
ϕ	7.3	23.1
1/4	7.2	23.2
+2	7.4	23.0
+3	7.0	23.4

π
30.36

6

c6	6.7	23.7
+5	6.7	23.7
+7	7.5	22.9
+9	6.2	24.2
W	5.9	24.5
	0+95	
W	6.4	24.0
+11	6.4	24.0
+12	8.2	22.2
+13	7.5	22.9
c6	7.0	23.4
+7	7.2	23.2
+8	7.7	22.7
1/4	7.5	22.9
ϕ	7.5	22.9
1/4	7.9	22.5
+7	8.3	21.9
+8	8.1	22.3
c6	8.2	22.2
+10	9.0	21.4
+13	8.1	22.3
E	8.9	21.5
	0+95	
E	9.9	20.5
+8	9.2	21.2
+10	10.3	20.1

30.36

cb	9.3	21.1
+2	9.2	21.2
+3	9.7	20.7
1/4	9.0	21.4
6	8.8	21.6
1/4	8.5	21.9
+3	9.0	21.4
+4	8.4	22.0
cb	8.4	22.0
+7	8.8	21.6
+10	7.9	22.5
W	8.1	22.3
	1+26	
W	8.6	21.8
+10	8.3	22.1
+12	9.2	21.2
cb	8.9	21.5
+6	9.0	21.4
+7	9.5	20.9
1/4	9.2	21.2
6	9.4	21.0
1/4	9.6	20.8
+7	10.3	20.1
+9	9.8	20.6
cb	9.9	20.5
+10	10.6	19.8

30.36

+12	9.7	20.7
6	10.2	20.2
	1+95	
5	10.9	19.5
+8	10.3	20.1
+10	11.6	18.8
+12	11.0	19.4
cb	10.5	19.9
+2	10.5	19.9
+3	11.0	19.4
1/4	10.4	20.0
6	10.1	20.3
1/4	9.9	20.5
+3	10.1	20.3
+4	9.8	20.6
cb	9.8	20.6
+8	10.5	19.9
+10	9.8	20.6
W	9.5	20.9
TP:	2.02	20.95 11.93
W		1+95 1.3 19.7
+10		1.3 19.7
+11		1.5 19.5
cb		1.7 19.3
+5		1.6 19.4
+6		2.0 19.0

7

18.93

X
2095

1/4	1.7	19.3
£	1.9	19.1
1/4	2.2	18.8
+7	3.0	18.0
+9	2.7	18.6
cb	2.4	18.6
+10	3.3	17.7
+11	2.5	18.5
E	3.0	18.0

2+95

5	3.9	17.1
+8	3.0	18.0
+10	3.8	17.2
cb	3.3	17.7
+~	3.5	17.5
1/4	3.0	18.0
£	2.8	18.2
1/4	2.7	18.3
+4	3.0	18.0
+5	2.5	18.5
cb	2.4	18.6
+8	2.9	18.1
+9	2.2	18.8
W	1.9	19.1

2+72 N line of I-14

W	2.5	18.5
---	-----	------

X
2095

8

+10	2.7	18.6
+12	3.4	17.6
cb	2.9	18.1
+6	3.3	17.7
1/4	3.1	17.9
£	3.1	17.9
1/4	3.3	17.7
+8	3.9	17.1
+9	3.4	17.6
cb	3.4	17.6
+10	4.2	16.8
+11	3.9	17.6
E	4.0	17.0

N:cb

E	4.5	16.5
+7	4.0	17.0
+10	5.2	15.8
cb	4.2	16.8
+1	4.7	16.3
1/4	4.0	17.0
£	3.7	17.3
1/4	3.6	17.4
+4	4.0	17.0
+5	3.5	17.5
cb	3.4	17.6
+8	3.8	17.2

X
20.95

+9	3.9	17.6
W	2.9	18.1
	N 1/4	
W	3.2	17.8
+11	3.6	17.4
+12	4.4	16.6
cb	3.8	17.2
+5	4.0	17.0
+6	4.3	16.7
1/4	4.2	16.8
E	4.2	16.8
1/4	4.6	16.4
cb	5.3	15.7
+1	4.8	16.2
+10	5.3	15.7
+13	4.9	16.1
E	5.2	15.8
	N 1/4 +12	
E	5.4	15.6
+7	5.1	15.9
+10	5.7	15.3
cb	5.3	15.7
+1	5.8	15.2
1/4	5.0	16.0
E	4.7	16.3
1/4	4.7	16.3

X
20.95

9

+5	4.9	16.1
+6	4.4	16.6
cb	4.4	16.6
+8	4.9	16.1
+10	4.2	16.8
W	3.4	17.6
	E	
N	4.7	16.3
+10	4.6	16.4
+12	5.2	15.8
cb	4.7	16.3
+5	4.9	16.1
+6	5.2	15.8
1/4	5.0	16.0
E	5.1	15.9
1/4	5.3	15.7
cb	6.0	15.0
+1	5.7	15.3
+10	5.8	15.2
+13	5.6	15.4
E	6.2	14.8
	S 1/4	
E	6.2	14.8
+10	6.4	14.6
cb	6.0	15.0
1/4	5.8	15.2

20.95

E	5.7	15.3
1/4	5.5	15.5
cb	5.2	15.8
+7	5.3	15.7
W	5.2	15.8
	S. cb	
W	9.4	16.6
cb	5.1	15.9
1/4	5.4	15.6
E	5.7	15.3
1/4	6.1	14.9
cb	6.5	14.5
E	7.1	13.9
	S. Line of ILY = 00	
E	7.3	13.7
cb	6.6	14.4
1/4	6.2	14.8
E	5.8	15.2
1/4	5.4	15.6
cb	5.1	15.9
W	4.6	16.4
	0+20	
Set BMSW Prop H. 6	4.66	16.29
W	4.7	16.3
+10	5.1	15.9
+11	5.7	15.3

20.95

10

cb	5.3	15.7
+3	5.3	15.7
+4	5.8	15.2
1/4	5.7	15.3
E	5.7	15.3
1/4	6.2	14.8
+8	6.9	14.1
+9	6.6	14.4
cb	6.7	14.3
+10	7.6	13.4
+12	7.0	14.0
E	7.3	13.7
	0+70	
E	8.0	13.0
+8	7.7	13.3
+10	8.4	12.6
cb	7.2	13.8
+2	7.0	14.0
+3	7.5	13.4
1/4	6.9	14.1
E	6.6	14.4
1/4	6.6	14.4
+6	6.9	14.1
+7	6.4	14.6
cb	6.3	14.7
+10	7.1	13.9

π
20.95

7 11	6.2	14.8
VV	6.0	15.0
	1+20.	
W	7.9	13.6
+9	7.6	13.4
+10	8.2	12.8
cb	7.8	13.2
+2	7.9	13.1
+3	8.3	12.7
1/4	8.0	13.0
1/8	8.0	13.0
1/4	8.4	12.6
+7	9.2	11.8
+8	8.7	12.3
cb	8.9	12.1
+10	9.9	11.1
+11	9.1	11.9
E	9.3	11.7
	1+70	
E	10.4	10.6
7.9	10.5	10.5
+10	11.1	9.9
cb	10.1	10.9
+2	10.0	11.0
+3	10.4	10.6
1/4	9.8	11.2

π
20.95

1/2	9.9	11.6
1/4	9.9	11.6
+7	9.7	11.3
+8	9.2	11.8
cb	9.2	11.8
+10	9.8	11.2
+11	9.0	12.0
W	8.8	12.2
	2+20	
W	10.5	10.5
+9	10.6	10.4
+10	11.2	9.8
cb	10.8	10.2
+2	10.8	10.2
+3	11.2	9.8
1/4	10.9	10.1
1/2	10.8	10.2
1/4	11.1	9.9
+8	11.7	9.3
cb	11.3	9.7
+5	11.3	9.7
+10	12.2	8.8
+12	11.5	9.5
E	11.6	9.4
T.P	11.2~	10.60
	11.57	9.38
	4.92	5.68

B.M.S.W.
Set Prop. H. b.
Thomas +
Pendleton

11

π
1060

2770 N line of Thomas 51045

80.5
20.45

E	3.0	7.6
+9	3.0	7.6
+10	3.6	7.0
cb	2.9	7.7
+2	2.9	7.7
+3	3.2	7.4
1/4	2.7	7.9
ϕ	2.9	8.2
1/4	2.3	8.3
+6	2.6	8.0
+8	2.1	8.5
cb	2.0	8.6
+10	2.4	8.2
+9	1.7	8.9
W	2.5	9.1
N cb	2.5	8.1
VV-	2.5	8.1
cb	2.9	7.7
1/4	3.1	7.5
ϕ	3.0	7.6
1/4	3.4	7.2
cb	3.4	7.2
E	3.6	7.0
N 1/4	3.8	6.8
E	3.8	6.8
cb	3.5	7.1

π
1060

1/4	3.9	7.2
ϕ	3.3	7.3
1/4	3.2	7.4
cb	3.1	7.5
+10	3.3	7.3
W	2.8	7.8
ϕ	2.8	7.8
W	2.8	7.8
+10	3.4	7.2
cb	3.4	7.2
1/4	3.5	7.1
ϕ	3.4	7.2
1/4	3.6	7.0
cb	3.8	6.8
E	3.9	6.7
5 1/2	4.5	6.1
E	4.5	6.1
cb	4.2	6.4
1/4	4.0	6.6
ϕ	3.8	6.8
1/4	3.8	6.8
cb	3.7	6.9
+10	3.8	6.8
W	3.6	7.0
5 cb	4.0	6.6
W	4.0	6.6

↑
10.60

+10	4.3	6.3
cb	4.2	6.4
1/4	4.3	6.3
2	4.4	6.2
1/4	4.5	6.1
cb	4.6	6.0
+10	5.0	5.6
E	4.8	5.8

S. Line of Thomas = 00

E	5.3	5.3
+9	5.3	5.3
+10	5.8	4.8
cb	5.4	5.2
+12	5.5	5.1
1/4	5.3	5.3
2	5.2	5.4
1/4	5.3	5.3
+7	5.7	4.9
+8	5.3	5.3
cb	5.3	5.3
+9	5.7	4.9
+10	5.2	5.4
W	4.9	5.7
	0450	
W	7.0	3.6
+10	7.4	3.2

↑
10.60

+11	8.0	2.6
cb	7.5	3.1
+2	7.5	3.1
+3	7.9	2.7
1/4	7.6	3.0
2	7.5	3.0
1/4	7.7	2.9
+8	8.2	2.4
cb	7.7	2.9
+10	8.2	2.4
+11	7.7	2.9
E	7.5	3.1

1400

E	9.3	1.3
+8	9.3	1.3
+9	9.9	0.7
cb	9.3	1.3
1/4	9.1	1.5
2	8.7	1.9
1/4	8.7	1.9
+8	9.1	1.5
+9	8.6	2.0
cb	8.6	2.0
+10	9.0	1.6
+11	8.3	2.3
W	8.1	2.5

13

10.60

1+25 N Line of Alley

W	8.7	1.9
+10	9.0	1.6
11	9.7	0.9
cb	9.2	1.4
+2	9.2	1.4
+3	9.6	1.0
14	9.3	1.3
⊥	9.4	1.2
14	9.7	0.9
+9	10.2	0.4
cb	9.9	0.7
+11	10.4	0.2
+12	10.0	0.6
E	10.1	0.5

1+95 E Line of Alley

E	10.3	0.3
+8	10.3	0.3
+9	10.7	-0.1
cb	10.3	0.3
+2	10.5	0.1
14	10.1	0.5
⊥	9.6	1.0
14	9.8	0.8
+7	10.1	0.5
+8	9.7	0.9
cb	9.6	1.0

10.60

14

+10	10.3	0.3
+11	9.9	1.2
W	9.2	1.4

1+75'

W	10.0	0.6
+10	10.5	0.7
cb	10.3	0.3
+2	10.6	0.0
14	10.3	0.3
⊥	10.0	0.6
14	10.4	0.4
+7	10.7	-0.1
cb	10.4	0.2
+10	11.0	-0.4
+12	10.5	0.1
E	10.4	0.2

2+00

E	10.4	0.2
+8	10.4	0.2
+10	11.1	-0.5
cb	10.4	0.2
14	10.3	0.3
⊥	10.2	0.4
14	10.4	0.2
+6	10.8	-0.2
+7	10.4	0.2

1060

cb	10.5	0.1
+10	10.6	0.0
W	10.6	0.0
	+50	
W	10.6	0.0
+10	10.8	-0.2
cb	10.6	0.0
+2	10.6	0.0
+3	11.0	-0.4
1/4	10.6	0.0
E	10.4	0.2
1/4	10.7	-0.1
cb	10.6	0.0
+11	11.0	-0.4
+12	10.4	0.2
E	10.3	0.3
	2770 ²⁰	2 = Read over
2	10.6	0.0
+8	10.6	0.0
+10	11.0	-0.4
cb	10.7	-0.1
1/4	10.6	0.0
E	10.5	0.1
1/4	10.8	-0.2
+7	11.1	-0.5
+8	10.8	-0.2

1060

15

cb		10.8	-0.2
+10		10.6	0.0
W		10.6	0.0
TP	9.37	9.31	10.66
		N:cb	
W		4.6	-0.3
cb		4.5	-0.2
1/4		4.5	-0.2
E		4.5	-0.2
1/4		4.5	-0.2
cb		4.5	-0.2
E		4.4	-0.1
		N:1/4	
E		4.4	-0.1
cb		4.5	-0.2
1/4		4.4	-0.1
E		4.3	0.0
1/4		4.5	-0.2
cb		4.5	-0.2
W		4.5	-0.2
		E	
W		4.5	-0.2
cb		4.5	-0.2
1/4		4.4	-0.1
E		4.5	-0.2
1/4		4.5	-0.2

7
431

cb	44	-0.1
E	4.3	-0.0
	5 1/4	
E	4.6	-0.3
cb	4.5	-0.2
1/4	4.5	-0.2
2	4.4	-0.1
1/4	4.5	-0.2
cb	4.5	-0.2
W	4.6	-0.3
	S cb	
W	4.7	-0.4
+10	5.1	-0.8
cb	4.5	-0.2
1/4	4.5	"
2	4.5	"
1/4	4.5	"
cb	4.5	"
E	4.6	-0.3
	S. line of road = 20	
E	4.9	-0.6
+8	4.9	-0.6
+10.	5.3	-1.0
cb	4.6	-0.3
+1	4.9	-0.6
1/4	4.4	-0.1

2
1/4
+7
+8
cb
+10
+11
W
set BM-NW
Prop. Hub. Reed
pendleton

W

+9

+10

cb

+2

+3

1/4

2

1/4

+9

cb

+11

+12

E

2

431

4.4	-0.1
4.5	-0.2
4.9	-0.6
4.5	-0.2
4.5	-0.2
5.3	-1.0
4.7	-0.4
4.7	-0.4
4.37	-0.06
0+50	
5.0	-0.7
4.9	-0.6
5.3	-1.0
4.9	-0.6
4.8	-0.5
5.3	-1.0
4.9	-0.6
4.9	-0.6
5.0	-0.7
5.3	-1.0
5.0	-0.7
5.5	-1.2
4.7	-0.4
4.7	-0.4
4.9	-0.6

1400

16

7
931

+8	51	-0.8
+9	55	-1.2
cb	50	-0.7
+1	54	-1.1
1/4	51	-0.8
2	49	-0.6
1/4	50	-0.7
+7	54	-1.1
+8	51	-0.8
cb	52	-0.9
+10	56	-1.3
+12	51	-0.8
W	52	-0.9

1125 N. Linné Alley

W	51	-0.8
+8	51	-0.8
+10	57	-1.4
cb	50	-0.7
+2	50	-0.7
+3	55	-1.2
1/4	49	-0.6
2	49	-0.6
1/4	52	-0.9
+8	55	-1.2
cb	51	-0.8
+12	54	-1.1

7
931

17

E	4.9	-0.6
	1495	
E	4.7	-0.4
+7	47	-0.4
+8	54	-1.1
cb	50	-0.7
+1	59	-1.1
1/4	51	-0.8
2	50	-0.7
1/4	51	-0.8
+7	56	-1.3
+8	52	-0.9
cb	52	-0.9
+10	56	-1.3
+11	52	-0.9
W	50	-0.7
	2100	
W	48	-0.5
+9	49	-0.6
+10	56	-1.3
cb	49	-0.6
+2	48	-0.5
+3	51	-0.8
1/4	48	-0.5
2	49	-0.1
1/4	47	-0.4

π
4.31

+9	5.2	-0.9
cb	4.9	-0.6
+11	5.7	-1.4
+12	5.0	-0.7
E	4.9	-0.6
2+50		
E	5.1	-0.8
+8	4.8	-0.5
cb	5.1	-0.8
1/4	4.9	-0.6
⊥	4.8	-0.5
1/4	5.1	-0.8
+7	5.4	-1.1
cb	5.2	-0.9
+8.10	5.2	-0.9
+10	5.8	-1.5
+11	5.2	-0.9
W	5.2	-0.9
2+70 N. Lorie Oliver		
W	5.2	-0.9
+9	5.3	-1.0
+10	5.6	-1.3
cb	5.2	-0.9
+3	5.5	-1.2
1/4	5.1	-0.8
⊥	5.1	-0.8

π
4.31

18

1/4	5.0	-0.7
+9	5.5	-1.2
cb	5.1	-0.8
+12	5.6	-1.3
+13	5.0	-0.7
E	5.2	-0.9
N. cb		
E	5.1	-0.8
cb	5.1	-0.8
1/4	5.2	-0.9
⊥	5.1	-0.8
1/4	5.2	-0.9
cb	5.2	-0.9
W	5.1	-0.8
N. 1/4		
W	5.1	-0.8
cb	5.3	-1.0
1/4	5.2	-0.9
⊥	5.2	-
1/4	5.2	-
cb	5.1	-0.8
E	5.1	-
⊥		
E	5.0	-0.7
cb	5.1	-0.8
1/4	5.1	-

x
4:31

5.51

2	5.1	-0.8
1/2	5.2	-0.9
cb	5.3	-1.0
W	5.1	-0.8
	5 1/2	
W	5.2	-0.9
cb	5.3	-1.0
1/4	5.2	-0.9
2	5.1	-0.8
1/4	5.2	-0.9
cb	5.1	-0.8
E	5.1	✓
	5cb	
E	4.9	-0.6
cb	5.1	-0.8
1/4	5.2	-0.9
2	5.1	-0.8
1/4	5.2	-0.9
cb	5.3	-1.0
W	5.1	-0.8
	5. line of observer = 00	
W	5.2	-0.9
cb	5.3	-1.0
1/4	5.3	-1.0
2	4.8	-0.5
1/4	5.0	-0.7

4:31

19

2b	5.0	-0.7
E	5.0	-0.7
	5.51	-1.20
	0.50	
E	5.0	-0.7
cb	5.0	-0.7
1/4	5.0	-0.7
2	4.9	-0.6
1/4	5.0	-0.7
cb	5.0	-0.7
W	5.2	-0.9
	1.00	
W	5.1	-0.8
cb	5.1	-0.8
1/4	5.0	-0.7
2	4.9	-0.6
1/4	5.0	-0.7
cb	5.0	✓
+7	5.0	✓
+11	5.9	-1.6
+14	5.1	-0.8
E	5.0	-0.7
	1.25	
E	5.1	-0.8
+8	5.2	-0.9
+9	6.2	-1.9

43.1

+13	5.2	-0.9
cb	5.0	-0.7
1/4	5.0	-
2	5.0	-
1/4	5.1	-0.8
cb	5.1	-0.8
+7	5.3	-1.0
+11	5.7	-1.4
+12	5.2	-0.9
W	5.0	-0.7
	1795	
W	5.2	-0.9
+8	5.2	-0.9
+9	5.7	-1.4
+12	5.2	-0.9
cb	5.1	-0.8
1/4	5.0	-0.7
2	4.9	-0.6
1/4	4.9	-0.6
cb	5.1	-0.8
+7	5.3	-1.0
cb +11	6.0	-1.7
+14	5.6	-1.3
F	5.5	-1.2
	2700	
1/4	6.1	-1.8

43.1

20

+8	6.9	-2.1
+12	6.0	-1.7
cb	5.6	-1.3
1/4	5.6	-1.3
2	5.3	-1.0
1/4	5.3	-1.0
cb	5.3	-1.0
+7	5.3	-1.0
+11	5.7	-1.4
+12	5.1	-0.8
W	5.0	-0.7
	2725	
W	5.9	-1.1
cb	5.6	-1.3
1/4	5.6	-1.3
2	6.0	-1.7
1/4	6.1	-1.8
cb	6.1	-1.8
E	6.8	-2.5
	2750 N. Line of Pacific	
E	6.0	-1.7
cb	6.3	-2.0
1/4	6.5	-2.2
2	6.4	-2.1
1/4	6.4	-2.1
cb	6.3	-2.0

4.31

79

6.4 - 2.1

711

6.7 - 2.4

712

6.2 - 1.9

71

5.9 - 1.6

21

Bias
Stops
BMSV Top
Walk Pendleton
- Garnet

X-sections Quincy Street Pacific
Beach from the line of Garnet to S. line of 1st

41
26-88

22

	1.91	37.46		36.05
TP	2.40	26.88	12.98	24.98
		0+00	S. line of Garnet	10'46
W			2.1	24.8
cb			2.6	24.3
1/4			2.9	24.0
1/2			3.2	23.7
1/4			3.4	23.5
cb			3.7	23.2
E			4.3	22.6
		0+07		
E-10			5.0	21.9
E			4.2	22.7
cb			4.2	22.7
1/4			3.9	23.0
1/2			3.9	23.0
+5			3.7	23.2
1/4			3.4	23.5
cb			3.1	23.8
W			2.7	24.2
		0+22		
W			3.0	23.9
+5			4.0	22.9
cb			4.7	22.2
+6			5.1	21.8
1/4			6.3	20.6

Plotted 6-29-28 - CBK

+2				6.8	20.1
+5				5.0	21.9
1/2				5.0	21.9
1/4				5.1	21.8
cb				5.4	21.5
E				5.6	21.3
E+10				7.4	19.5
				0+33	
E-10				8.5	18.4
E				8.0	18.9
+5				6.5	20.4
cb				6.4	20.5
1/4				6.0	20.9
1/2				5.9	21.0
+7				5.6	21.3
1/4				6.8	20.1
+5				8.1	18.8
cb				8.0	18.9
+8				9.6	22.9
W				4.4	22.5
					19.64
W+17				7.24	19.42
				7.46	
				0+35	
W-10				8.1	18.8
W				8.0	18.9
+1				6.3	20.6
cb				8.3	18.6

End of flow line of 22 Drain
carrying water under ground
off beach

H.I.
26.88

1/4	7.9	19.0
+6	6.2	20.7
£	6.2	20.7
1/4	6.2	20.7
cb	6.7	20.2
+3	6.7	20.2
E	8.9	18.5
+10	8.8	18.1

0+42.23

E-10	9.5	17.4
E	9.3	17.6
+3	8.0	18.9
cb	7.2	19.7
1/4	6.8	20.1
+5	6.7	20.2
£	7.1	19.8
+2	7.1	19.8
+6	8.3	18.6
1/4	8.6	18.3
cb	8.5	18.4
W	8.3	18.6
+10	8.1	18.8

0+68

W-10	8.8	18.1
W	9.4	17.5
cb	9.5	17.4

H.I.
26.88

23

1/4	9.5	17.4
£	9.2	17.7
1/4	9.0	17.9
cb	9.4	17.5
+3	9.3	17.6
+5	9.8	17.1
E	10.1	16.8
+10	10.8	16.1

0+77

E-10	12.0	14.9
E	10.9	16.0
+3	11.4	15.5
+5	9.9	17.0
+7	9.8	17.1
+8	10.1	16.8
cb	10.0	16.9
1/4	9.7	17.2
£	9.7	17.2
1/4	9.7	17.2
+7	9.9	17.5
cb	7.0	19.9
+7	6.0	20.9
W	5.0	21.9
W+10	2.7	24.2
W-10	2.6	24.3

0+83.70

H.I.
26.88

W-2	2.6	24.3
W	3.8	23.1
cb	7.4	19.5
+5	9.3	17.6
1/4	9.7	17.2
¢	9.8	17.1
1/4	10.0	16.9
cb	10.4	16.5
+2	10.5	16.4
+3	10.1	16.8
E	11.0	15.9
E+10	12.5	14.4
	0+95	
E-10	13.0	13.9
-5	11.7	15.2
E	11.2	15.7
cb	10.9	16.0
1/4	10.5	16.4
¢	10.0	16.9
1/4	10.0	16.9
+5	9.7	17.2
cb	8.8	18.1
+5	8.6	18.3
W	7.9	19.0
W+10	7.4	19.5

H.I.
26.88

24

	1425	
W	10.6	16.3
cb	10.7	16.2
1/4	10.6	16.3
¢	10.9	16.5
1/4	11.0	15.9
cb	11.7	15.2
E	11.8	15.1
E+5	12.0	14.3
+10	14.0	12.9
	1+65	
E-10	13.2	13.7
E	12.3	14.6
+8	11.7	15.2
+9	12.1	14.8
cb	12.1	14.8
1/4	11.9	15.5
¢	11.0	15.9
1/4	11.0	15.9
cb	11.5	15.4
+8	11.1	15.8
W	10.6	16.3
	2+00	
W	10.6	16.3
+2	11.3	15.6
cb	11.7	15.2

π
26.88

1/4			11.6	14.3
ε			11.5	15.4
1/4			12.0	14.9
cb			12.9	14.5
+2			12.0	14.9
E			12.2	14.7
T.P.	3.95	18.35	11.98	14.90
		2150		
E			9.2	14.2
+8			3.9	14.5
cb			4.6	13.8
1/4			4.1	14.3
ε			3.4	15.0
1/4			3.6	14.8
cb			3.8	14.6
+1			3.9	15.0
+7			3.9	15.0
N			2.3	16.1
		2+75 50		
N			2.3	16.1
+2			3.4	15.0
+9			3.7	14.7
cb			4.1	14.3
1/4			3.7	14.7
ε			3.9	14.5
1/4			4.4	14.0

HZ
18.35

cb			5.0	13.4
+1			4.3	14.1
E			4.5	13.9
			N cb	
E			5.9	13.0
cb			5.9	13.0
+5			4.8	13.6
1/4			4.6	13.8
ε			4.1	14.3
+5			4.2	14.2
1/4			4.1	14.3
cb			4.4	14.0
+1			3.8	14.6
+7			3.6	14.8
N			2.2	16.2
			N 1/4	
N			2.6	15.8
+2			3.6	14.8
cb			4.0	14.4
+2			4.5	13.9
1/4			4.2	14.2
ε			4.1	14.3
1/4			4.6	13.8
cb			5.1	13.3
E			5.3	13.1

25

10/4
80' of
20' obs
N. line of Hornblende

H3
18.35

⊕

E	5.5	12.9
cb	5.1	13.3
1/4	4.8	13.6
⊕	4.3	14.1
1/4	4.3	14.1
cb	4.5	13.9
N	3.8	14.6
	5.14	
N	2.7	15.7
+3	4.0	14.4
cb	4.3	14.1
1/4	4.5	13.9
⊕	4.9	14.0
1/4	4.9	13.5
cb	5.3	13.1
E	5.7	12.7
	5.06	
E	5.9	13.0
cb	5.5	12.9
1/4	5.0	13.4
⊕	4.7	13.7
1/4	4.7	13.7
cb	4.8	13.6
+1	4.3	14.1
+8	3.8	14.6
N	2.9	15.5

H5
18.35

S. line of Horobkade 26

N	3.9	15.0
cb	4.7	13.7
+1	5.2	13.2
1/4	5.0	13.4
⊕	5.0	13.4
1/4	5.2	13.2
cb	5.5	12.9
+1	5.0	13.4
E	5.9	13.0
	0.50	
E	6.6	11.8
cb	6.6	11.8
1/4	6.2	12.2
⊕	6.0	12.4
1/4	6.2	12.2
cb	6.4	12.0
+7	5.7	12.7
N	4.3	14.1
	1.00	
N	5.9	13.0
+3	6.1	12.3
+9	6.6	11.8
cb	7.2	11.2
1/4	7.0	11.4
⊕	7.0	11.4
1/4	7.2	11.2

1835

cb	7.3	11.1
E	7.7	10.7
	1750	
E	8.7	9.7
cb	8.3	10.1
+1	8.6	9.8
1/4	8.3	10.1
E	7.9	10.5
1/4	7.9	10.5
cb	8.4	10.0
+1	7.9	10.4
N	6.8	11.6
	2100	
N	8.0	10.4
+3	8.6	9.8
cb	9.0	9.4
+1	9.3	9.1
1/4	9.2	9.2
E	9.1	9.3
1/4	9.6	9.8
+9	10.0	8.4
cb	9.6	8.8
E	9.6	8.8
	2+27	
E	10.9	8.0
cb	10.0	8.4

18.35

77

27

+1	10.8	7.6
1/4	10.3	8.1
E	9.8	8.6
1/4	9.9	8.5
+6	10.1	8.3
cb	9.7	8.7
+7	9.6	8.8
N	8.7	9.7
	2+50	
N	10.0	8.4
cb	10.0	8.4
1/4	10.1	8.3
E	10.2	8.2
1/4	10.7	7.7
cb	11.0	7.4
E	11.2	7.2
	2+71.50	
E	11.4	7.0
cb	11.1	7.3
1/4	10.7	7.7
E	10.3	8.1
1/4	10.2	8.2
cb	10.1	8.3
N	10.3	8.1
	N.C.B.	
N	10.4	8.0

125' 57
20' 65
21' 57/4

18.35

cb		10.3	8.1
1/4		10.2	8.2
ϕ		10.3	8.1
1/4		10.9	7.5
cb		11.0	7.4
+4		11.9	7.0
E		11.5	6.9
T.P.	6.85	19.26	10.94
		N. 1/4	
E		7.6	6.7
cb		6.7	7.6
1/4		6.7	2.6
ϕ		6.5	7.8
1/4		6.3	8.0
cb		6.6	7.7
W		6.9	7.9
		ϕ	
W		5.6	8.7
+9		5.6	8.7
cb		6.0	8.3
1/4		5.9	8.4
ϕ		6.1	8.2
+5		6.5	7.8
1/4		6.6	7.7
+9		6.8	7.5
cb		6.9	7.9

7.91

14.26

E		6.6	7.7
	ϕ+7		
E		6.0	8.3
+9		5.8	8.5
cb		6.9	7.4
1/4		6.7	7.6
ϕ		6.1	8.2
+5		5.8	8.5
1/4		5.7	8.6
cb		5.9	8.4
+1		5.3	9.0
W		5.1	9.2
	5/4		
W		6.5	7.8
+7		6.8	7.5
cb		7.0	7.3
1/4		6.7	7.6
ϕ		6.9	7.4
1/4		7.2	7.1
cb		7.0	7.3
E		6.8	7.5
	5/4+9		
E		7.0	7.3
cb		7.2	7.1
1/4		7.2	7.1
ϕ		7.1	7.2

28

π
1926

1/4	7.2	7.1
cb	7.7	6.6
W	7.6	6.7
S/A + 8		
W	7.6	6.7
cb	7.7	6.6
1/4	7.6	6.7
⊕	7.4	6.9
1/4	7.4	6.9
cb	7.6	6.7
+1	7.6	6.7
+3	8.6	5.7
E	8.7	5.6
S.cb		
E	9.2	5.1
+8	9.0	5.3
cb	8.0	6.3
1/4	7.9	6.4
⊕	7.9	6.4
1/4	8.0	6.3
cb	7.9	6.4
W	7.8	6.5
S. line of Ivy		
W	7.9	6.4
cb	8.2	6.1
1/4	8.3	6.0

π
1926

⊕		8.9	5.9	29
1/4		8.5	5.8	
cb		8.8	5.5	
E		9.4	4.9	
TP	8.97	22.17	1.06	13.20
check on 8m SW				15.20
244 - find later			5.93	16.29
				0.00

Bliss
Holbein
Jacobson
81 1/2 W. Proptlet
Thomas Fendley

X Section Thomas Street Pacific Beach
from the E Line of Olney to the W. Line
of Quincy HZ.

13.15 18.83

5.68

0+00. E Line

S	3.3	15.5
+10	3.2	15.6
+11	3.7	15.1
cb	3.3	15.5
1/4	3.0	15.8
1/2	2.9	16.4
1/4	2.1	16.7
cb	2.1	16.7
+8	1.8	17.0
+10	2.0	16.8
+11	1.5	17.3
N	1.3	17.5
	0+25	16.3
X	2.7	16.1
+9	2.7	16.1
+10	3.0	15.8
cb	2.8	16.0
1/4	2.9	15.9
1/2	3.2	15.6
1/4	3.9	14.9
cb	4.2	14.6
+10	5.0	13.8
+11	4.6	14.2
S	4.6	14.2

Platted - 6-29-28 - CBH

HJ
1883

0+50

S	5.1	13.7
+9	4.9	13.9
+10	5.9	13.4
cb	4.6	14.2
1/4	4.3	14.5
1/2	3.6	15.2
1/4	3.3	15.5
cb	3.1	15.7
+8	3.2	15.6
+11	3.3	15.5
+12	2.9	15.9
N	2.9	16.4
	1+00	
N	2.9	15.9
+8	3.4	15.4
+9	3.9	14.9
+12	3.6	15.2
cb	3.7	15.1
1/4	4.1	14.7
1/2	4.5	14.3
1/4	5.2	13.6
cb	5.6	13.2
+10	6.3	12.5
+11	5.6	13.2
S	6.0	12.8

30

H2
1883

1750

S	5.1	13.7
+9	5.2	13.6
+10	5.8	13.0
cb	5.1	13.7
1/4	4.7	14.1
2	3.8	15.0
1/4	3.9	14.9
cb	3.6	15.2
+11	3.9	14.9
+12	3.4	15.4
N	3.1	15.7

2400

N	3.2	15.6
+8	3.7	15.1
+9	4.2	14.6
cb	4.0	14.8
1/4	4.1	14.7
2	4.0	14.8
1/4	4.5	14.3
cb	5.1	13.7
+11	5.9	12.9
+12	5.4	13.4
S	5.8	13.0

2735

S	6.0	12.8
+8	5.8	13.0

X
1883

31

+9	6.4	12.4
cb	5.7	13.1
1/4	5.3	13.5
2	4.7	14.1
1/4	4.9	13.9
cb	4.8	14.0
+8	4.9	13.9
+11	5.2	13.6
+12	4.6	14.2
N	4.4	14.4

2450

N	4.7	14.1
+8	5.0	13.8
+9	5.6	13.2
+12	5.2	13.6
cb	5.2	13.6
1/4	5.3	13.5
2	5.1	13.7
1/4	5.7	13.1
cb	6.1	12.7
+11	6.7	12.1
+12	6.2	12.6
S	6.3	12.5

3400

S	7.6	11.2
+8	7.5	11.3

7
18.83

+9	7.9	10.9
ob	7.3	11.5
1/4	7.0	11.8
¢	6.8	12.0
1/4	6.6	12.2
ob	6.3	12.5
+9	6.4	12.4
+11	6.7	12.1
+12	6.0	12.8
N	5.6	13.2
	3750	
N	6.8	12.0
+9	7.2	11.6
+10	7.8	11.0
+12	7.5	11.3
ob	7.4	11.4
1/4	7.7	11.1
¢	7.9	10.9
1/4	8.3	10.5
ob	8.6	10.3
+8	9.0	9.8
+11	9.5	9.3
+12	8.9	9.9
S	9.0	9.8
	9700	
S	10.3	8.5

7
18.83

+8	10.0	8.8
+9	10.5	8.3
+12	10.2	8.6
ob	9.9	8.9
1/4	9.5	9.3
¢	9.0	9.8
1/4	8.9	9.9
ob	8.6	10.2
+8	8.6	10.2
+11	9.0	9.8
+12	8.9	10.4
N	7.8	11.0
	4450	
N	8.9	9.9
+8	9.9	9.4
+9	10.0	8.8
+12	9.8	9.0
ob	9.8	9.0
1/4	10.1	8.7
¢	10.2	8.6
1/4	10.8	8.0
ob	11.2	7.6
+8	11.7	7.1
+11	12.0	6.8
+12	11.9	7.4
S	11.6	7.2

32

18.83

568

T.P. 566 11.39 13.15 568

5+00 W. line of Pendleton

S. 5.7 5.6
 +8 5.2 6.1
 +9 5.6 5.7
 +12 5.2 6.1
 ob 4.8 6.5
 1/4 4.4 6.9
 1/4 3.6 7.7
 1/4 3.6 7.7
 ob 3.3 8.0
 +8 3.4 7.9
 +11 3.2 7.9
 +12 2.9 8.4
 N 2.9 8.9

E. line of Pendleton = 00

N 3.8 7.5
 +8 4.2 7.1
 +9 4.7 6.6
 +12 4.6 6.7
 ob 4.4 6.9
 1/4 4.6 6.7
 1/4 4.7 6.6
 1/4 5.3 6.0
 ob 5.6 5.7
 +8 6.1 5.2

11.34

+11 6.4 4.9
 +12 6.0 5.3
 S. 6.2 5.1
 : 0450
 S 7.1 4.2
 +8 6.8 4.5
 +9 7.4 3.9
 +12 7.1 4.2
 ob 6.6 4.7
 1/4 6.1 5.2
 1/4 5.5 5.8
 1/4 5.3 6.0
 ob 5.3 6.0
 +12 5.5 5.8
 +13 4.9 6.4
 N 4.3 7.0

H00

N 5.1 6.2
 +8 5.5 5.8
 +9 6.3 5.0
 +12 6.0 5.3
 ob 6.0 5.3
 1/4 6.1 5.2
 1/4 6.0 5.3
 1/4 6.6 4.7
 ob 7.3 4.0

33

11.34

+ 4	82	3.1
+12	76	3.7
S	80	3.3
	1450	
S	9.0	2.3
+8	8.6	2.7
+9	9.0	2.3
+12	8.6	2.7
cb	8.2	3.1
1/4	7.6	3.7
£	7.0	4.3
1/4	7.0	4.3
cb	7.0	4.3
+8	7.1	4.2
+11	7.1	4.2
+12	6.5	4.8
N	6.1	5.2
	1170	
N	6.9	4.4
+8	7.1	4.2
+9	8.1	3.2
+12	7.9	3.4
cb	7.5	3.8
1/4	7.5	3.8
£	7.9	3.9
1/4	8.2	3.1

11.34

cb	8.7	2.6
+8	9.1	2.2
+11	9.3	2.0
+12	9.0	2.3
S	9.3	2.0
	2100	
S	9.7	1.6
+8	9.6	1.7
+9	10.0	1.3
+12	9.6	1.7
cb	9.3	2.0
1/4	9.2	2.1
+8	8.8	2.5
£	8.5	2.8
1/4	8.9	2.9
cb	8.3	3.0
+8	8.6	2.7
+11	8.8	2.5
+12	8.1	3.2
N	7.8	3.5
	2130	
N	8.9	2.9
+8	8.5	2.5
+9	7.9	1.9
+12	7.1	2.2
cb	8.8	2.5
1/4	7.0	2.3

34

11.34

9.1	2.2
9.6	1.7
9.8	1.5
10.0	1.3
10.2	1.1
10.3	1.0
10.4	0.9

2+50

10.1	1.2
10.1	1.2
10.2	1.1
10.1	1.2
9.9	1.4
9.6	1.7
9.9	1.9
9.1	2.2
9.5	1.8
9.2	2.1
8.9	2.4

2+98 35 W. line of Quincy

9.6	1.7
9.5	1.8
9.9	1.4
9.7	1.6
9.8	1.5
9.6	1.7
9.9	1.4

11.34

9.9	1.4
10.0	1.3
10.0	1.3

35

BHSS
6/14/08

B.M. NW Prop. Hub.
Reed Foundation

X Sections of Reed Street
Pacific Beach from the E Line of Olney to the
W Line of Quincy or West End Elev

H.I.
17.61

36

T.P

9.84 17.61 1.81 7.77

N

6.3

11.3

Set B.M. S. Corner
Prop. Reed

9.09 13.52

N

9.0

8.6

0+00 E line of Olney

cb

9.2

8.4

N

9.0 13.6

+1

9.6

8.0

cb

3.5 13.8

1/4

9.9

8.2

+2

9.4 13.2

1/2

9.2

8.4

+4

9.2 13.4

3/4

9.7

8.9

1/2

4.3 13.3

+8

10.1

7.5

1/4

4.1 13.5

+9

9.7

7.9

+8

4.3 13.3

cb

9.8

7.8

+9

4.4 13.2

S.

9.8

7.8

cb

4.1 13.5

0+70

12.0

5.6

S

4.1 13.5

cb

12.0

5.6

S

6.8 10.8

+2

12.2

5.4

cb

6.7 10.9

1/4

11.7

5.9

+1

6.7 10.9

1/2

11.2

6.4

+2

7.1 10.5

+7

11.3

6.3

+6

6.9 10.7

cb

11.9

6.2

1/4

6.9 10.7

N

11.0

6.6

1/2

6.7 10.9

11.0

10.8

6.8

1/4

6.7 10.9

N

11.7

5.9

+9

6.8 10.8

cb

12.2

5.4

cb

6.9 11.2

+1

12.5

5.1

Plotted 6-29-28 - C.B.H.

HZ
1751

1/4			12.9	5.2
ϕ			12.9	5.2
1/4			12.9	4.7
+8			13.3	4.3
+9			12.9	4.7
cb			13.1	4.5
S.			13.5	4.1
T.P	1.90	7.83	11.68	5.93
			+50	
S			5.2	2.6
cb			9.9	3.4
+2			9.6	3.2
1/4			9.0	3.8
+4			3.8	4.0
ϕ			3.0	4.8
1/4			3.2	4.6
+8			3.9	4.4
cb			3.1	4.7
N			2.7	5.1
			+72	
N			2.8	5.0
cb			3.3	4.5
+2			3.7	4.1
1/4			3.8	4.0
+5			3.6	4.2
ϕ			3.6	4.2

HZ
783

						3.6	4.2
				+9		4.2	3.6
				1/4		4.3	3.5
				+8		5.0	2.8
				+9		4.7	3.1
				cb		4.7	3.1
				+10		5.3	2.5
				+13		6.3	1.5
				S		6.2	1.6
						2+00	
				S-10		7.0	0.8
				S		6.9	1.4
				cb		6.0	1.8
				+8		6.1	1.7
				1/4		5.1	2.7
				ϕ		4.0	3.8
				1/4		4.1	3.7
				+8		4.1	3.7
				+9		3.6	4.2
				cb		3.7	4.1
				N		3.2	4.6
						2+25	
				N		3.9	4.4
				cb		4.0	3.8
				+1		4.0	3.8
				+2		4.5	3.3

37

42
783

1/4	4.6	3.2
ϕ	4.7	3.1
+5	5.5	2.3
1/4	6.0	1.8
cb	6.6	1.2
S	7.2	0.6
.2+50		
S	7.0	0.8
cb	6.5	1.3
1/4	6.0	1.8
ϕ	5.9	2.4
1/4	5.4	2.4
+8	5.5	2.3
+9	5.0	2.8
cb	4.9	2.9
+10	4.9	2.9
+11	4.3	3.5
N	3.8	4.0
2+90		
N	4.8	3.0
+9	5.2	2.6
+10	5.7	2.1
cb	5.5	2.3
+1	5.5	2.3
+2	5.9	1.9
1/4	5.9	1.9

7
783

38

ϕ	5.7	2.1
1/4	6.2	1.6
+8	7.0	0.8
+9	6.7	1.1
cb	6.9	0.9
S	7.6	0.2
3+25		
S	8.1	-0.3
cb	7.7	0.1
+2	7.9	-0.1
1/4	7.2	0.6
ϕ	6.8	1.0
1/4	6.5	1.3
cb	6.2	1.6
+10	6.4	1.4
+11	6.0	1.8
N	5.7	2.1
3+50		
N	6.6	1.2
+9	6.2	1.6
+10	6.9	0.9
cb	6.7	1.1
1/4	6.9	0.9
ϕ	6.9	0.9
1/4	7.6	0.2
+8	8.2	-0.4

7
7.83

+9	8.0	-0.2
cb	8.0	-0.2
S	8.2	-0.4
	4+00	
S	8.3	-0.5
cb	8.3	-0.5
1/4	8.0	-0.2
ϕ	7.9	-0.1
1/4	7.7	0.1
cb	7.6	0.2
+10	7.9	-0.1
+11	7.9	0.4
N	7.1	0.7
	4+50	
N	8.0	-0.2
+9	8.1	-0.3
+10	8.5	-0.7
cb	8.0	-0.2
1/4	8.0	-0.2
ϕ	7.9	-0.1
1/4	8.0	-0.2
cb	8.1	-0.3
S	8.2	-0.4
	5.00	
S	8.9	-0.6
cb	8.3	-0.5

W.L. Pan

7
7.83

39

1/4	8.2	-0.4
ϕ	8.1	-0.3
1/4	8.1	-0.3
cb	7.9	-0.1
N	7.9	-0.1
TP 8M	5.19	5.09
	7.88	-0.05
	E Line of Pendleton = 0.0	
N	5.1	0.0
cb	5.1	0.0
+1	5.4	-0.3
+5	5.1	0.0
1/4	5.1	0.0
ϕ	5.2	-0.1
1/4	5.2	-0.1
+5	5.5	-0.4
+1	5.9	-0.8
cb	5.5	-0.4
S	5.6	-0.5
	0+20	
S	5.6	-0.5
cb	5.2	-0.1
+1	5.7	-0.6
+5	5.2	-0.1
1/4	5.1	0.0
ϕ	4.9	0.2
1/4	5.0	0.1

5.09

+5	5.1	0.0
+9	5.9	-0.3
cb	5.0	0.1
N	5.0	0.1
	0+50	
N	5.1	0.0
cb	5.3	-0.2
+1	5.7	-0.6
+5	5.3	-0.2
1/4	5.3	-0.2
8	5.3	-0.2
1/4	5.5	-0.4
+5	5.6	-0.5
+9	6.1	-1.0
cb	5.6	-0.5
S	5.5	-0.4
	1+00	
S	5.3	-0.2
cb	5.4	-0.3
+1	5.9	-0.8
+5	5.9	-0.3
1/4	5.4	-0.3
8	5.9	✓
1/4	5.9	✓
+5	5.9	✓
+9	5.7	-0.6

5.09

40

cb	5.4	-0.3		
N	5.3	-0.2		
TP	4.99	4.94	5.14	-0.05
		4.50		
N	4.6	0.3		
+8	4.6	0.3		
+9	5.2	-0.3		
+13	4.9	0.0		
cb	4.9	0.0		
1/4	5.0	-0.1		
8	4.8	0.1		
1/4	4.8	0.1		
cb	4.9	0.0		
+8	4.9	0.0		
+12	5.3	-0.4		
+13	4.8	0.1		
S	4.8	0.1		
	2+00			
S	5.0	-0.1		
+8	5.0	-0.1		
+9	5.3	-0.4		
+12	5.0	-0.1		
cb	5.0	-0.1		
1/4	4.9	0.0		
8	4.9	0.0		
1/4	4.9	0.0		

	↑ 990		
cb		48	0.1
+7		48	0.1
+11		51	-0.2
+12		49	0.0
N		48	0.1

2+50

N		47	0.2
+8		47	0.2
+9		5.0	-0.1
+12		4.7	0.2
cb		4.7	✓
1/4		4.7	✓
2		4.7	✓
1/4		4.7	✓
cb		4.8	0.1
S		4.9	0.0

2+98⁵⁰ W. line of W. End

S		4.8	0.1
+9		4.6	0.3
+10		4.6	✓
+13		4.6	✓
cb		4.5	0.4
2		4.4	0.5
1/4		4.7	0.2
cb		4.7	0.2
+8		4.9	0.0

	↑	↑	-	Elev
+11		4.94		4.4
N				4.2
TP	4.63	4.74	4.83	0.11

41

Note Used this
TP 1/4 sec of
Oliver

Bliss
Holbeck
Jacobson
6/16/28
Used T.P. From
Boon. See Page

X Sections of Oliver St. Pacific Beach
from the W. line of West End St. to E. line of
Olney St.

#3
4.74

42

Platted 6-29-28 - C.B.H.

	H.I.		Elev			
	4.63	4.74	0.11	+14	5.6	
				06	5.7	
				1/4	5.6	
N		5.4	-0.7	2	5.7	-1.0
+12		5.7		1/4	5.8	
06		5.2		06	5.6	
1/4		5.2		0	5.5	-0.8
2		5.2	-0.5		0775	
1/4		5.4		5	5.9	-1.2
06		5.5		06	5.9	
0		5.6	-0.9	1/4	5.5	
		0730		2	5.3	-0.6
5		5.3	-0.6	1/4	5.4	
+9		5.3		06	5.6	
+10		5.7		+5	5.6	
+13		5.4		+9	5.9	
06		5.3		+10	5.6	
1/4		5.3		N	5.2	-0.5
2		5.5	-0.8		1700	
1/4		5.6		N	4.8	-0.1
+8		6.0		+9	5.2	
+9		5.6		+10	5.5	
N		5.6	-0.9	06	5.1	
		0750		1/4	5.3	
N		5.5	-0.8	2	5.5	-0.8
+10		5.6		1/4	5.7	
+11		5.8				

H2.
4.74

c6	5.6	
+7	5.5	
+11	5.9	
+12	5.5	
S	5.6	-0.9
	1+7.5	
S	6.0	-1.3
+8	5.8	
+9	6.2	
+13	5.8	
c6	5.6	
1/4	5.3	
Φ	5.0	-0.3
1/4	4.9	
c6	4.9	
+6	5.1	
+10	5.5	
+11	5.0	
N	5.0	-0.3
	1+5.0	
N	5.0	-0.3
+9	5.0	
+10	5.6	
+15	5.0	
c6	4.9	
1/4	4.9	

H1.
4.74

13

Φ	4.8	-0.1
1/4	4.9	
c6	5.1	
+6	5.3	
+11	5.8	
+12	5.4	
S	5.6	-0.9
	2+0.0	
S	5.2	-0.5
+8	5.1	
+9	5.6	
+15	5.1	
c6	5.0	
1/4	5.0	
Φ	5.0	-0.3
1/4	5.1	
c6	5.1	
+7	5.3	
+11	5.6	
+12	5.1	
N	5.1	-0.4
	2+5.0	
N	5.9	-0.7
+8	5.4	
+9	5.9	
+14	5.5	

H.I.
9.74

06	5.9	
1/4	5.9	
2	5.1	-0.4
1/4	5.1	
06	5.1	
+8	5.9	
+11	5.8	
+12	5.4	
S	5.3	-0.6

2+99 EL Pen

S	5.4	-0.7
+8	5.4	
+9	5.9	
+14	5.5	
06	5.4	
1/4	5.5	
2	5.9	-0.7
1/4	5.5	
06	5.5	
N	5.4	-0.7

Wlime Pendleton = 00 W L Pen

N	5.5	-0.8
+9	5.4	
+10	5.9	
+14	5.6	
06	5.5	

H.I.
9.74

44

1/4	5.5	
2	5.5	-0.8
1/4	5.6	
06	5.7	
+7	5.7	
+11	6.2	
+12	5.6	
S	5.7	-1.0

0+50

S	5.7	-1.0
+7	5.6	
+8	6.3	
+15	5.6	
06	5.6	
1/4	5.6	
2	5.5	-0.8
1/4	5.5	
06	5.6	
+5	5.7	
+11	6.1	
+12	5.7	
N	5.6	-0.9

1+00

N	5.6	-0.9
+8	5.5	
+9	6.1	

#1.
979

cb		5.6	
1/4		5.6	
ϕ		5.6	-0.9
1/4		5.7	
cb		5.7	
+1		5.7	
+12		6.4	
+13		5.8	
S		5.8	-1.1
TP	9.33	8.89	5.18
		11.50	-0.44
S		10.0	-1.1
+8		10.0	
+9		10.5	
+15		10.0	
cb		9.9	
1/4		9.9	
ϕ		9.9	-1.0
1/4		9.8	
cb		9.7	
+4		9.7	
+10		10.4	
+11		9.7	
N		9.7	-0.8
		2100	
N		10.1	-1.2

#1.
8.89

45

+8		10.2	
+9		10.5	
+15		10.1	
cb		10.0	
1/4		9.9	
ϕ		9.9	-1.0
1/4		9.9	
cb		10.0	
+6		10.0	
+12		10.6	
+13		10.0	
S		10.0	-1.1
		2140	
S		10.1	-1.2
+8		10.2	
+9		10.6	
+13		10.3	
cb		10.1	
1/4		10.0	
ϕ		9.9	-1.0
1/4		10.1	
cb		10.3	
N		10.9	-1.5
		2150	
N		11.2	-2.3
+10		11.4	

HI
8.89

cb	10.8	
1/4	10.8	
¢	10.5	-1.6
1/4	10.6	
cb	10.5	
+5	10.5	
+10	10.9	
+11	10.2	
S	10.1	-1.2
	2+60	
S	10.9	-2.0
+9	11.0	
+10	11.5	
cb	11.0	
1/4	11.2	
¢	11.3	-2.4
1/4	11.2	
cb	11.1	
+10	11.4	
N	11.2	-2.3
	2+70	
N	10.0	-1.1
+10	10.4	
cb	10.4	
1/4	10.5	
¢	10.7	-1.8

HI
8.89

46

1/4	10.8	
cb	11.1	
+9	11.6	
S	11.6	-2.7
	2+80	
S	11.4	-2.5
+10	10.8	
cb	10.1	
1/4	9.4	
¢	9.2	-0.3
1/4	9.0	
cb	9.0	
+10	9.0	
+11	8.7	
N	8.6	0.3
	3+00	
N	5.5	3.4
+8	5.5	
+9	6.1	
+15	5.4	
cb	5.4	
1/4	5.3	
¢	5.7	3.2
1/4	6.0	
cb	6.7	
+5	7.0	

H.I.
8.89

+10			7.6	
+11			7.1	
+17			7.7	
S			8.1	0.8
S+10			9.1	
		3+20		
S-10			5.2	
S			4.3	4.6
+8			3.9	
+9			4.1	
cb			3.6	
1/4			3.1	
ϕ			2.7	6.2
1/4			2.5	
cb			2.6	
N			2.5	6.4
T.P.	6.52	15.02	0.39	8.50
		3+35		
N			6.5	5.5
cb			6.6	
1/4			6.9	
ϕ			6.6	8.4
1/4			6.9	
cb			7.3	
+8			8.0	
S			8.6	6.4

15.02

47

S+15			10.2	
		3+50		
S-15			9.0	
S-8			7.9	
S			6.5	8.5
+13			6.1	
cb			5.5	
1/4			5.3	
ϕ			5.2	9.8
1/4			5.3	
+7			5.7	
cb			5.6	
N			6.1	8.9
T.P.	1.85	12.12	9.75	10.27
		3+64		
N			3.0	9.1
cb			2.1	
1/4			1.9	
ϕ			1.9	10.2
1/4			2.0	
cb			2.2	
+17			2.2	
S			2.0	10.1
S+9			3.0	
+15			5.0	

#2
12.12

377.9

S-15	5.2	
-6	2.9	
S	2.5	9.6
+8	2.5	
cb	2.0	
1/4	1.7	
♀	1.6	10.5
1/4	1.6	
cb	1.8	
N	2.7	9.4
N+15	3.8	

378.7

N	4.5	7.6
+9	6.7	
+10	7.6	
cb	7.3	
1/4	7.0	
♀	5.5	6.3
+6	2.0	
1/4	1.8	
cb	3.1	
S	4.2	7.5
+15	8.0	

379.5

S-15	12.3
-9	10.8

#2
12.12

S	9.6	2.5
+10	8.5	
+18	9.2	
cb	8.4	
+3	7.5	
1/4	8.2	
12	7.8	
♀	8.8	3.3
1/4	10.4	
+5	10.6	
cb	10.2	
N	9.8	2.3

410.7

N	11.8	0.3
+12	12.1	
cb	11.9	
1/4	12.1	
♀	12.8	-0.3
+9	9.1	11.31
1/4	5.8	-1.7
cb	6.4	
+16	6.2	
S	6.8	-2.7

3.32

413.0

S	7.0	-2.9
cb	7.0	

48

12.12
11.31
0.81
3.32
4.13

H.I.
9.14

1/4	7.0	
£	8.2	- 4.1
1/4	7.7	
cb	7.3	
N	6.8	- 2.7
	4732	channel crosses N line
N	8.7	- 4.6
cb	8.7	
1/4	8.7	
£	8.6	- 4.5
1/4	7.3	
cb	7.1	
S	7.1	- 3.0
	4745	channel crosses S line
S	8.5	- 4.4
cb	8.7	
1/4	8.6	
£	8.7	- 4.6
1/4	8.6	
cb	8.7	
N	8.7	- 4.6
	4752	channel N line
N	8.6	- 4.5
cb	8.7	
1/4	8.7	
£	8.7	- 4.6

H.I.
9.19

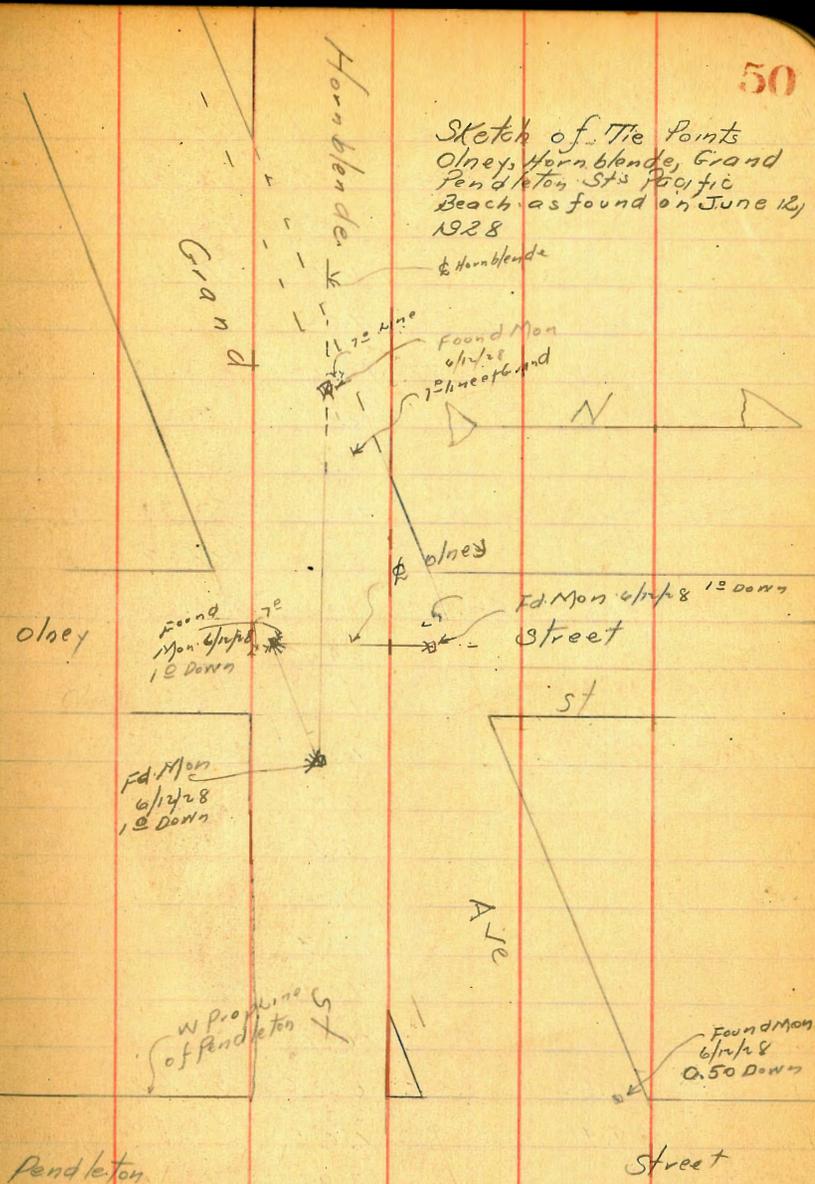
49

1/4	8.7	
cb	8.7	
S	8.7	- 4.6
	4755	
S	8.7	- 4.6
cb	8.7	
1/4	8.7	
£	8.7	- 4.6
+5	8.6	
+6	6.8	
1/4	6.8	
cb	6.7	
N	6.7	- 2.6
	4767	channel S line
N	6.5	- 2.4
cb	6.5	
1/4	6.5	
£	6.7	- 2.6
1/4	6.5	
cb	6.5	
+15	7.2	
+16	8.6	
S	8.7	- 4.6
	4769	
S	6.7	- 3.6
cb	6.6	

H.I.
7.14

50

1/4			6.5	
2			6.6	-2.5
1/4			6.5	
CB			6.5	
N			6.5	-2.4
		4499 W	Line of Olney	
N			6.8	-2.7
CB			6.9	
1/4			6.7	
2			6.7	-2.6
1/4			6.5	
CB			6.5	
S			6.5	-2.4
TP	12.11	15.49	0.76	3.38
TP	12.23	27.01	0.71	14.78
TP	13.12	39.92	0.21	26.80
TP	6.74	45.38	1.28	38.64
check on BM NW Olney + Corner			0.20	45.19

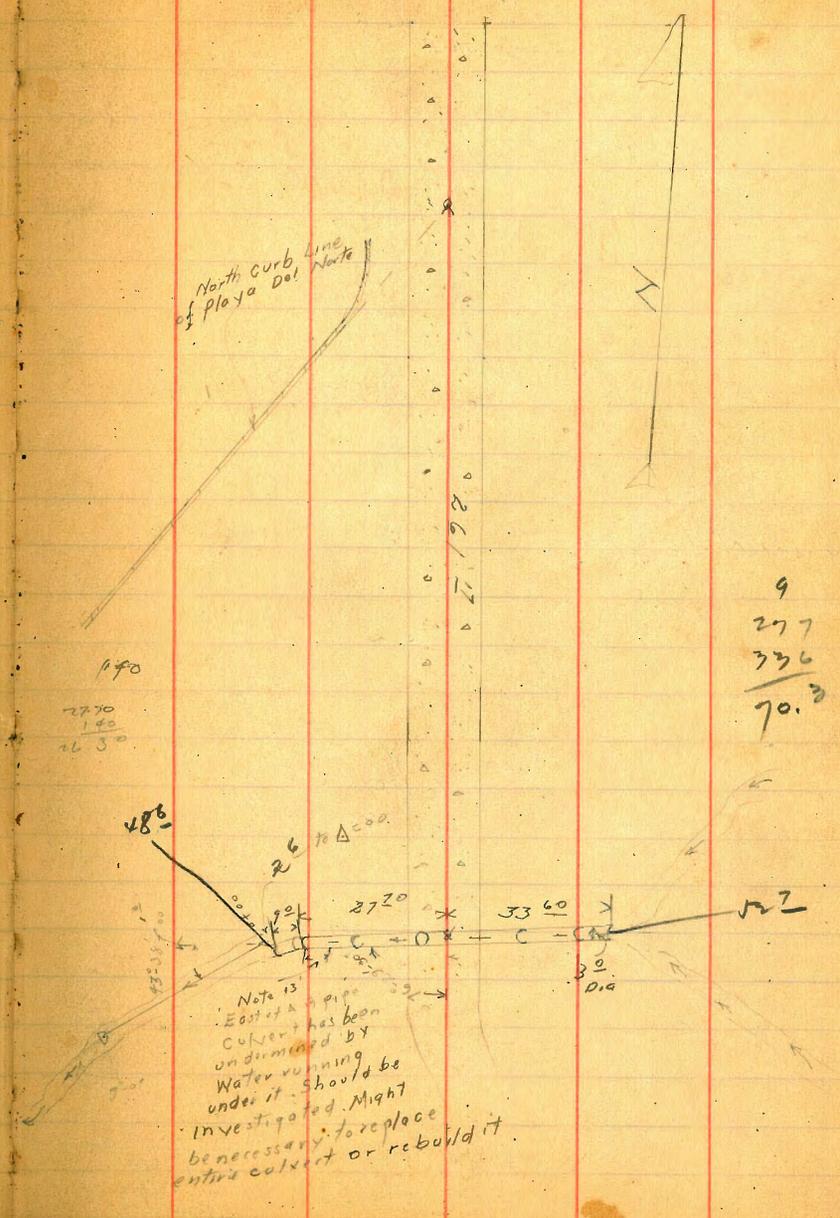


Location of and levels for Culvert
Across La Jolla Blvd Between Playa del Sur

Blk 5
Dw 1007
No 1007
7006304
4/12/48

BMNEBP + Playa Del Norte
Center La Jolla Blvd 4.33 74.16 - Elev 69.83

T.P.	7.23	76.54	9.85	69.31
T.P.	7.73	83.90	0.37	76.17
T.P.	2.85	80.98	6.77	77.13
T.P.	2.00	71.36	11.62	69.36
T.P.	2.08	62.77	10.67	60.69
0+00	25' East of culvert		8.1	54.7
0+10			8.3	54.47
0+25	Flow Line of Existing culvert Dia 3.0'		10.06	57.71
T.P.	4.61	65.30	2.08	60.69
T.P.	4.91	56.98	13.23	52.07
Flow Line of existing culvert of Dia 2.6'			8.92	58.56
Δ Ahead of Flow Line	43° 38' 00"		10.1	46.9
0+24			10.2	46.8
0+29			9.0	48.0
0+43			9.6	47.4
0+48			9.2	47.8
0+53			10.3	46.7
0+63			10.6	46.4
0+72			10.9	46.1
T.P.	11.62	68.24	0.36	56.62
T.P.	9.91	76.00	1.65	66.59
check on BM on 300' on Air + La Jolla Blvd.			3.90	72.10
			72.01	72.01
			0.09	0.09



Bliss
Warbeck
Jacobson

X Sections of Fern Glen from the
W. line of La Jolla Blvd to 100' West.

BM NEBP Center of La Jolla Blvd	3.22	73.05	Elev 69.83
TP	6.95	76.19	3.81 69.24

0+00 W. line of La Jolla Blvd

N	5.2
+7	7.5
+17	8.0
+25	6.9
+30	5.0
+40	5.6
+45	6.0
+46	5.3
+55	4.9
+65	5.0
N	7.0
+6	10.3
+22	10.1
+31	5.2
+40	6.0
+50	5.6
+55	5.2
+65	5.1
N	6.4
+10	10.5
+26	9.7
+30	6.3
+34	5.8

0+05

0+15

Belvedere Street

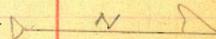
110'

90.55

La Jolla

B. l. y d

Fern Glen Street



Used N Line
of Fern Glen for
baseline

1+00

0+75

0+50

0+25

0+15

0+05

0+00

HZ.
76-19

+39	6.5	
+55	57	
+65	53	
	0+25	
N	6.3	
+5	7.0	
+12	10.4	
+26	9.8	
+30	7.9	
+35	6.9	
+45	6.8	
+48	8.0	
+51	6.1	
+55	6.2	
+65	5.6	
	0+35	
N	6.5	
+6	6.8	
+13	10.6	
+27	10.5	
+33	7.6	
+49	6.8	69.4
+49.5	9.9	
+52	9.8	
+52 Top	6.6	
+55	6.6	
+59	6.5	

HZ.
76-19

54

+60	5.9
+65	5.9
	0+50
N	7.0
+10	7.0
+14	7.9
+18	11.1
+31	11.0
+33	10.0
+35	10.7
+52	10.3
+53	6.9
+55	6.7
+65	6.9
	0+63
N	7.5
+10	7.3
+15	7.6
+20	8.7
+24	10.1
+31	11.3
+44	10.9
0+98	8.5
+55	7.2
+59	7.3
+60	6.8

HZ
76-19

55

+65	6.6
	0+75
N	8.0
+12	8.0
+17	8.5
+23	10.2
+30	12.0
+39	12.9
+44	10.7
+50	8.0
+55	7.2
+60	7.6
+65	7.1

1+00

N	9.6
+6	9.6
+11	10.1
+26	13.8
+39	13.6
+42	11.7
+48	9.1
+55	8.5
+65	8.2
check back on BM	6.41

69.78 ✓

Levels for Proposed Drain

59.4

H.I.
59.37

59.4

56

BM Flow Line
of existing Pipe

	+	+	-	Elev
	10.81	59.37		48.56
		Line A	see sketch Page 52	
0+00			11.7	47.7
0+03			12.6	46.8
0+15			12.4	47.0
+17			11.3	48.1
+18			11.2	48.2
+20			10.0	49.4
+30			7.8	51.6
0+30 5'S			9.7	49.7
0+30 10'S			11.3	48.1
0+39			5.8	53.6
0+46			9.8	54.6
0+46 5'S			6.8	52.6
0+46 9'S			7.9	51.5
0+51			5.0	54.4
0+52			7.2	52.2
0+69			8.0	51.4
0+67			5.4	54.0
0+67 7'S			8.3	51.1
0+67 8'S			12.1	47.3
0+74			3.5	55.9
0+84			2.0	57.4
0+84 9'S			3.0	56.4
0+89 10'S			7.0	52.4
H.I.			1.2	58.2

1+12 5'S

1.8 57.6

1+12 6'S

3.1 56.3

1+12 15'S

4.0 55.4

1+34

2.7 56.7

TP

0.23

54.81

2.79 56.58

1+34 13'S

2.3 54.5

1+55 4'

2.7 54.1

1+55 10'S

3.9 52.9

1+55 15'S

5.0 51.8

1+74

5.6 51.2

10'S

7.2 49.6

15'S

7.7 49.1

1+92

8.4 48.4

10'S

9.6 47.2

2+00

10.1 46.7

6'S

11.0 45.8

10'S

13.7 43.1

F.I. Bottom

2+08

11.6 45.2

2+12

15.0 41.8

2+45 2' Δ

15.3 44.07

56.8

Line "B"

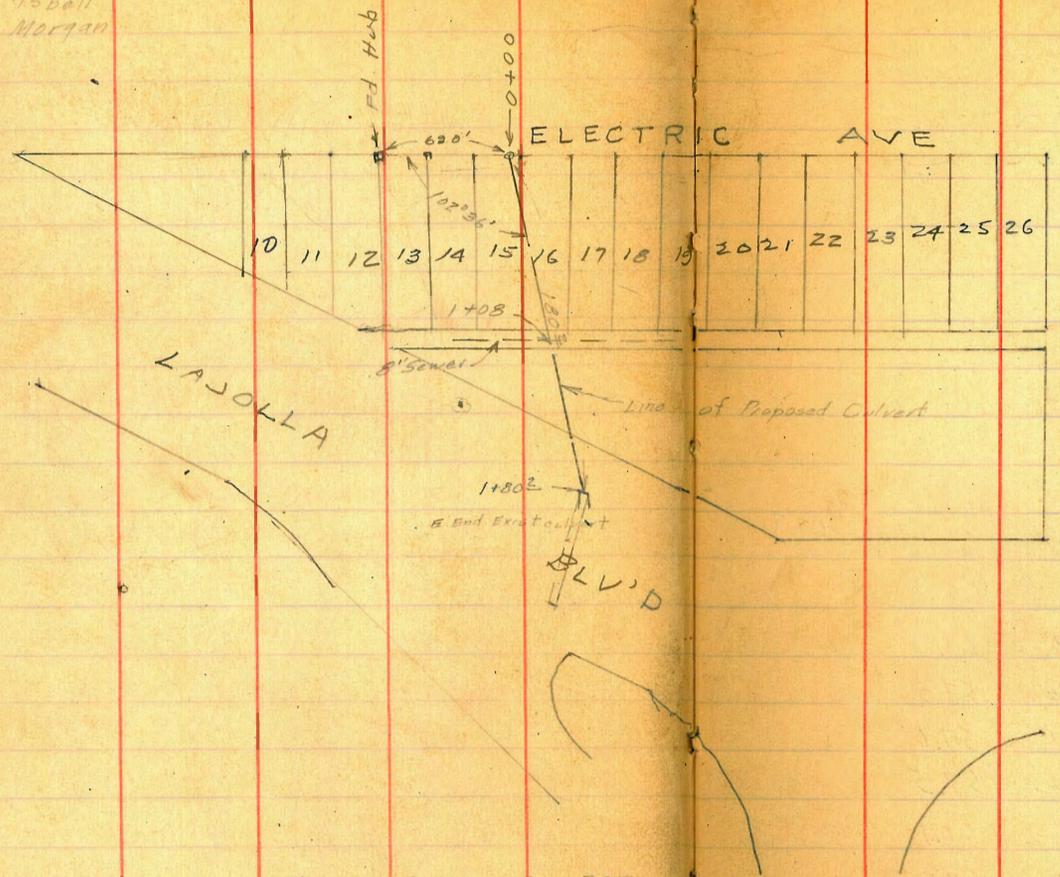
51.4

BM Flow line of existing culvert	288	51.44		98.56
0100			3.7	47.7
0403			4.8	46.6
0450			4.9	46.5
+55			9.9	46.5
+63			4.6	46.8
+75			4.6	46.8
+80			5.1	46.3
+80			5.7	45.7
+125			7.1	44.3
+144 ²⁰ TP Δ	62.9	50.09	7.69	43.75
+147			6.4	43.6
+152			5.0	45.0
+157			4.3	45.7
+166			5.3	44.7
+174			5.8	44.2
+176			6.4	43.6
+181 ⁷ TP Δ	3.90	97.95	6.53	42.51
+189			4.9	42.5
+209 ²⁰ Δ			5.3	43.1
+243 ²⁰ Δ	Endline		5.85	41.60

50.0

57

Oct 25-28
Loudon
Isbell
Morgan



SKETCH SHOWING LINE FOR
PROPOSED STORM DRAIN FROM
ELECTRIC AVE THRU LAJOLLA BLVD.

0+35-28
London.

Profile of Proposed Drain shown
on P. 58

SP NE
Center
La Jolla Blvd

B.M.	3.19	73.02		69.83
T.P.	7.90	78.02	2.90	70.12
T.P.	6.45	84.02	0.45	77.57
T.P.	1.81	79.59	6.24	77.78
NE Cor Jet 13 Hub	3.21	73.99	8.81	70.78
0+00	at cor W. Electric Ave		9.6	74.4
T.P.	2.77	67.66	9.10	64.89
0+20			3.9	63.8
0+30			4.7	63.0
0+35			4.8	62.9
0+45			3.8	63.9
0+50			4.1	63.6
0+65			4.6	63.1
0+73			5.8	61.9
0+90			10.2	57.5
1+00			10.1	57.6
1+05			9.2	58.5
1+08	top pipe sewer		7.62	60.1
1+14			8.8	58.9
1+25			10.5	57.2
1+37			11.7	55.8
1+46			12.6	55.1
1+55			12.9	54.8
1+58			12.6	55.1
1+63			12.7	55.0
1+70			12.7	55.0
1+80	FL End of Alvert.		15.0	52.66

67.7

Stadia Topog of Channel
See P 58 For control.

Area From Electric Ave to Ocean

60

Sta	Az	Stadia	Vert L	Rod	Hor. dist	diff.	H.I	EI.
Ht. inst = 5.2 7"	Inst. at NE cor Lot 13		Lat 13	oriented w/ Electric Ave	20.73		75.98	70.78 ✓
1	131°-24'	1.49	+2°-02'		149.0	5.3		76.1
2	126°-15'	1.50	+2°-10'		150.0	5.7		76.5
3	33°-01'	1.44		0.8	144.0			75.2
4	24°-17'	1.70		1.3	170.0			74.7
5	4°-28'	2.42		1.6	242.0			74.4
6	1°-32'	1.20		6.0	120.0			70.0
7	333°-57'	1.51		6.7	151.0			69.3
8	300°-36'	0.86		13.1	86.0			62.9
9	283°-40'	1.22		10.3	122.0			65.7
10	279°-17'	0.90	-6°-53'		89.8	10.7		60.1
11	242°-12'	1.04	-7°-22'		102.0	13.2		57.6
12	245°-58'	1.30	-6°-22'		128.0	14.3		56.5
13	259°-36'	1.54		11.7	154.0			64.3
14	241°-06'	2.18		13.0	218.0			63.0
15	234°-00'	1.84	-3°-39'	up 3.3 9.0	184.0	15.6		55.2
16	221°-24'	1.69	-2°-59'	11.0	169.0	14.5		56.3
17	225°-01'	1.52	-4°-04'		151.0	10.7		60.1
18	207°-03'	1.37	-1°-48'	12.0	137.0	10.7		60.1
19	211°-04'	1.44	-1°-08'	8.0	144.0	5.6		65.2
20	207°-26'	1.05	-0°-56'	13.0	105.0	9.5		61.3
21	183°-27'	2.18	-0°-03'	10.0	218.0	5.1		65.7
22	179°-49'	1.70	+0°-19'		170.0	1.0		69.8
23	166°-33'	0.70		10.0	70.0			66.0
24	142°-13'	0.73		1.1	73.0			74.9

Head of Draw

Bottom of Draw

Bottom of Draw

52.4 ✓

Sta.	Az	Stadia	Vert. L	Rod.	Hor. Dist.	Diff.	75.98 H.I.	70.78 Elev.
25	177°-57'	3.45	+8°-49'		345.0	5.0		75.8
26	184°-42'	2.52	+0°-19'		252.0	1.3		72.1
27	207°-58'	2.12		6.9	212.0			69.1
28	224°-36'	2.12		9.0	212.0			69.0
29	229°-10'	2.18	-2°-23'		218.0	9.0		61.8
30	236°-08'	2.50		13.1	250.0			62.9
31	218°-26'	0.69		9.7	69.0			66.3
32	2°-49'	0.40		3.0	40.0			73.0
33	48°-14'	0.72		3.0	72.0			73.0
34	102°-12'	0.25		7.2	25.0			68.8
"B"	251°-57'	3.75 ⁵	-1°-57'		375.0	12.7		58.1
Inst. at "B" oriented on "A"								
H.I. inst. 5.2							63.3	58.1
A		3.75	+1°-56'					
1	59°-27'	1.90	+1°-52'		190.0	6.2		64.3
2	79°-57'	1.39	+2°-25'		225.0	9.4		67.5
3	65°-46'	1.55	-0°-07'	Up 3.0	155.0	3.3		54.8
4	77°-11'	1.09	-5°-54'		109.0	11.1		47.0
5	140°-02'	0.42	-17°-53'		38.6	12.3		45.8
6	201°-29'	0.62	-8°-52'	Up 3.0	60.0	12.4		45.7
7	255°-01'	1.99	-7°-12'	Up 2.0	198.0	26.7		31.9
8	266°-32'	1.67	-5°-44'	Up 3.0	167.0	19.6		38.5
9	256°-27'	1.98	-4°-16'	Up 6.0	198.0	20.7		37.4
10	258°-29'	2.06	-3°-25'	Up 6.0	266.0	21.7		36.4
11	253°-09'	2.63	-1°-26'		263.0	6.6		51.5
12	250°-30'	1.90		9.8	190.0			53.5

Edge of Road.

51.8 ✓
42.7 ✓
29.4 ✓
35.5 ✓
31.4 ✓
30.4 ✓

Sta.	Az.	Stadia	Vert. L	Rod	Hor. Dist.	Diff.	63.3 H.I.	58.1 Elev.	
13	234°-24'	1.02		6.7	102.0			56.6	
14	175°-05'	0.88	+2°-11'		88.0	3.3		61.4	
15	108°-46'	1.10	+0°-31'		110.0	1.0		59.1	
26	62°-30'	0.81		2.4	81.0			60.9	
17	273°-42'	0.91		8.3	91.0			55.0	
18	272°-49'	1.77		11.4	177.0			51.9	
19	260°-38'	2.42	-2°-15'		242.0	9.4		48.7	
"C"	264°-05'	5.25	-1°-47'		525.0	16.5	46.8	41.6 ✓	
Inst. at "C" oriented on "B"									
Ht. Inst. 5.2									
"B"		5.23	+1°-49'						
1	78°-07'	1.97	+1°-51'		197.0	6.3		47.9	
2	87°-42'	1.85		5.8	185.0			41.0 ✓	
3	93°-44'	1.76	+1°-28'	1/2 p. 12.0	176.0	7.5		34.1 37.1 ✓	
4	70°-46'	1.35	-3°-45'		135.0	8.8		32.8	
5	73°-03'	0.55	-10°-50'		53.0	10.2		31.4	
6	169°-05'	0.44	-16°-04'		40.0	11.7		29.9	
7	216°-43'	1.10	-7°-00'	1/2 p. 1.0	109.0	14.3		27.3 26.3 ✓	
8	250°-44'	1.32	-7°-08'	1/2 p. 1.0	130.0	17.2		24.4 23.4 ✓	
9	264°-47'	2.32	-4°-24'	1/2 p. 2.0	232.0	19.7		21.9 19.9 ✓	
10	277°-37'	2.64	-4°-15'	1/2 p. 5.0	263.0	24.5		17.1 12.1 ✓	
11	277°-38'	2.67	-3°-46'		267.0	17.5		24.1	
12	265°-04'	2.41	-2°-56'	1/2 p. 4.0	241.0	16.3		25.3 21.3 ✓	
13	247°-05'	1.66	-4°-14'		166.0	12.2		29.4	
14	241°-46'	1.56	-4°-53'		156.0	13.2		28.4	
15	225°-30'	1.30	-6°-04'	1/2 p. 1.0	132.0	14.7		26.9 25.9 ✓	

Cor. N.W. #1
Shack 10'x12'
N.E. cor. #2
Shack 10'x12'
N.W. cor. #3
Shack 20'x12'

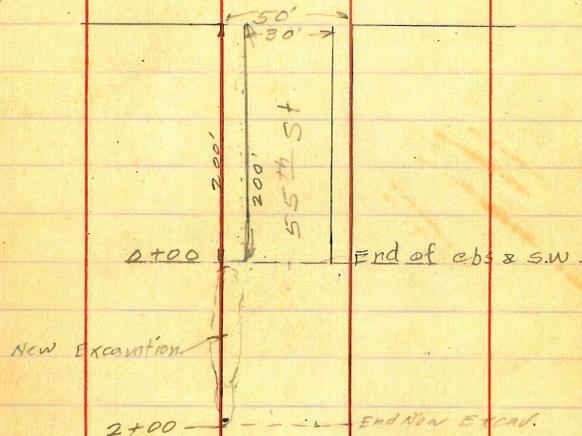
Sta	H ₃	Stadia	Vert. L	Rod.	Hor. Dist	Diff.	H.I.	Elev.	
16	190°-50'	1.00		7.7	100.00		46.8	39.1	
17	121°-25'	0.79		2.0	79.00			44.8	
18	96°-03'	1.32	+2°-32'		131.00	5.83		52.63 47.4 ✓	
19	104°-40'	1.95	+2°-12'		194.00	7.49		54.29 49.1 ✓	
20	63°-09'	1.38	-2°-06'		137.00	4.82		41.98 37.8 ✓	
21	55°-40'	0.61		2.7	61.00			44.1	
22	242°-38'	0.59		9.1	59.00			37.7	
23	216°-44'	0.93	-6°-30'	1/2 p. 3.0	92.00	10.53		33.2 28.1 ✓	
24	259°-44'	0.91		10.4	91.00			36.4	
25	266°-46'	2.00	-3°-25'		199.00	11.92		34.88 29.7 ✓	
26	266°-09'	2.24	-4°-06'		223.00	12.02		34.8 29.6 ✓	
27	277°-43'	2.60	-3°-45'		259.00	17.00		29.8 24.6 ✓	
"D"	278°-23'	4.27	-3°-07'		426.00	23.19	23.7	23.61 18.4 ✓	
Inst. at "D" oriented on "C"									
H.I. Inst. 5.3									
"C"		4.30	+3°-07'		429.00	23.35	23.7		
1	53°-38'	1.36		11.0	136.00			12.7	
2	321°-36'	0.50	-11°-26'	1/2 p. 1.0	49.00	9.91		7.5	
3	312°-28'	1.34	-5°-49'		133.00	12.57		5.8	
4	288°-00'	1.35	-8°-08'		133.00	19.10		-1.7	
5	353°-55'	0.89		6.7	89.00			17.0	
6	23°-14'	1.30	+4°-38'		129.00	10.49		28.9	
7	45°-45'	1.66	+5°-12'		165.00	15.04		33.4 ✓	
8	111°-14'	1.85	+1°-05'		185.00	3.49		21.9 ✓	
9	130°-35'	1.01	+4°-16'		101.00	7.51		29.4 ✓	
10	65°-55'	0.98		2.4	98.00			21.3	

N.E. cor.
Bldg.
N.W. cor.
Bldg.

Sta.	A.3	Stadia	Vert. L.	Rod.	Hor. Dist	Diff.	H. I.	Elev.
11	311°-48'	0.37		7.2	37.00		27.7	16.5



Madison St.



3/28/09
 London Rd - X sec 55th St from 200' S of
 Madison thru New Excavation
 50' wide 30' roadway

65

B.M.	5 63	427.94		427.31
T.P.	8.11	429.07	6.98	420.96
	0+00			
w.L.			9.9	419.2
cb	top cb		9.95	419.12
cut			10.9	418.7
'4			10.0	419.1
±			9.7	419.4
'4			9.5	419.6
cut			9.9	419.2
cb	top cb		9.46	419.61
E.L.			7.8	421.3
	0+05			
E.L.			4.0	425.1
+5			4.7	424.4
cb			8.8	420.3
'4			9.0	420.1
±			9.3	419.8
'4			9.61	419.5
cb			10.2	418.9
+4			9.4	419.7
w.L.			9.9	419.2

New for deep required from 100 to 100
 3/29/09
 C.B. Jones

429.07

0+21

w.L.	7.3	421.8
+2	7.7	421.4
cb	9.4	419.7
1/4	8.9	420.2
±	8.9	420.2
1/4	8.7	420.4
+6	8.6	420.5
cb	7.0	422.1
+2	4.0	425.1
E.L.	3.2	425.9

0+30

E.L.	2.9	426.2
+6	3.1	426.0
cb	6.7	422.4
+1 ⁵	8.1	421.0
1/4	8.6	420.5
±	8.7	420.4
1/4	8.7	420.4
cb	9.4	419.7
+6	9.2	419.9
w.L.	6.9	422.2

429.07

66

0+32

w.L.	7.2	421.9
+4	9.0	420.1
cb	9.4	419.7
1/4	8.7	420.4
±	8.6	420.5
1/4	8.5	420.6
+6	8.1	421.0
cb	7.5	421.6
E.L.	5.9	423.2

0+39

E.L.	5.9	423.2
cb	8.0	421.1
1/4	8.6	420.5
±	8.5	420.6
1/4	8.7	420.4
cb	9.3	419.8
+9	8.2	420.9
w.L.	7.0	422.1

429.07

0+45

w.L	6.7	422.4
+2	8.7	420.4
cb	9.0	420.1
1/4	8.7	420.4
±	8.5	420.6
1/4	8.3	420.8
+6	8.1	421.0
cb	5.4	423.7
+3	2.5	426.6
EL	2.4	426.7

0+75

EL	1.5	427.6
+8	2.1	427.0
cb	5.9	423.2
+15	8.1	421.0
1/4	8.1	421.0
±	8.1	421.0
1/4	8.2	420.9
cb	8.2	420.9
w.L	7.9	421.2

429.07

67

1+00

w.L	2.1	422.0
+2	7.8	421.3
cb	7.8	421.3
1/4	7.5	421.6
±	7.8	421.3
1/4	7.7	421.4
+6	7.8	421.3
cb	3.7	425.4
+1	2.0	427.1
EL	1.1	428.0

1+25

EL	2.3	426.8
+8	2.8	426.3
cb	6.0	423.1
+15	7.5	421.6
1/4	7.6	421.5
±	7.4	421.7
1/4	7.5	421.6
cb	7.7	421.4
+8	7.8	421.3
w.L	6.8	422.3

429.07

1+50

w.l	6.4	422.7
+2	8.4	420.7
cb	7.9	421.2
1/4	7.6	421.5
E	2.4	421.7
1/4	7.5	421.6
+6	7.3	421.8
cb	6.0	423.1
+2	4.5	424.6
E.L	4.1	425.0

1+7.5

E.L	5.9	423.7
+8	5.9	423.2
cb	6.7	422.4
+3	7.4	421.7
1/4	7.5	421.6
E	7.4	421.7
1/4	7.7	421.4
cb	8.4	420.7
+6	7.9	421.2
w.l	7.2	421.9

2+00

429.07

w.l	7.5	421.6
+6	7.5	421.6
+8	8.8	420.3
cb	8.5	420.6
1/4	8.0	421.1
E	7.8	421.3
1/4	7.8	421.3
cb	7.3	421.8
+3	6.5	422.6
EL	6.3	422.8

SE Allen H. 6 on 550 N. 27 E 1/2 1/4 on
B.M.

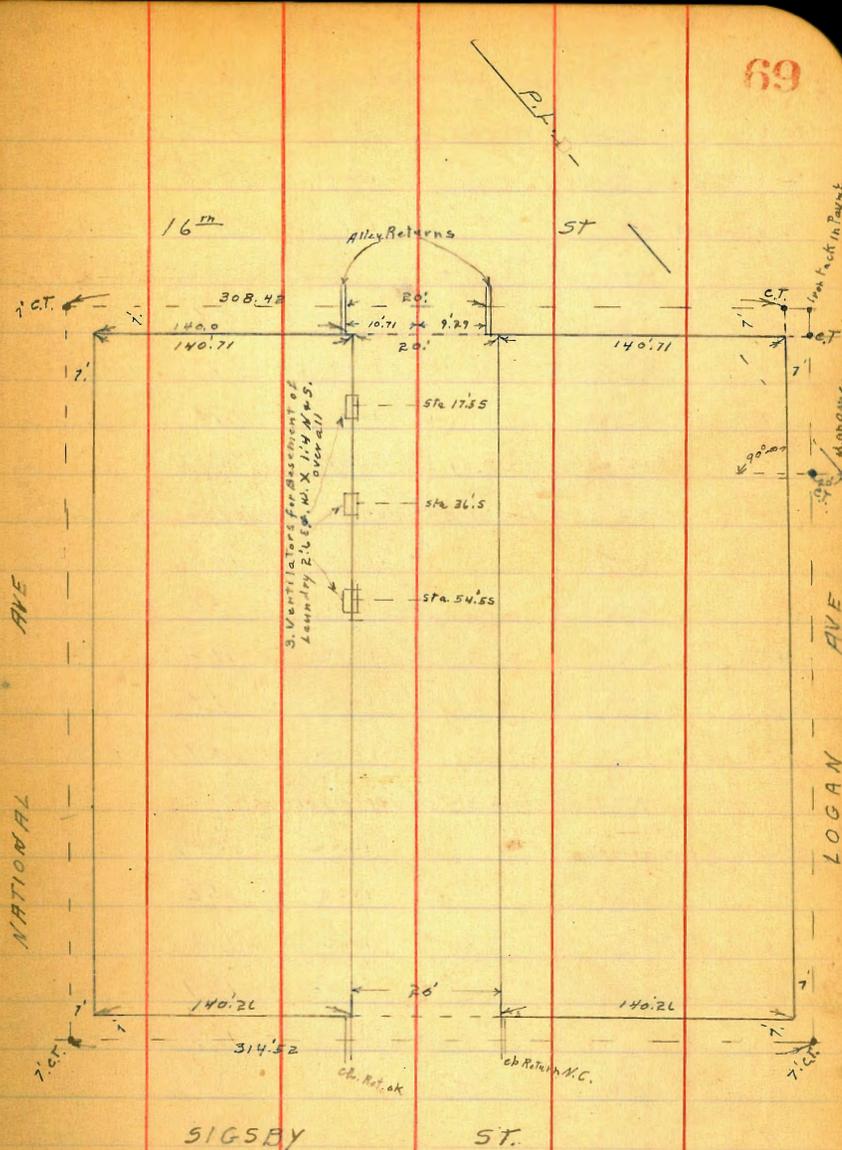
12.12 416.99 (417.00)

68

20' wide X Sec. Alley BIK 138 Man. + Schiller 4-25-29
 16th to Sigby Bet National & Logan
 mile

BM	7.79	11.59	3.80	N.W. 16 th + National.
	00 = E. line 16 th St			
S - 0.71 = d. Ret		4.48	7.11	ground Pavmt + d. Ret.
S. line Alley		4.54	7.05	pavmt
⊕		4.62	6.97	"
C + 9.29 = N. d. Ret		4.19	7.40	curb + Pavmt.
N. line Alley		4.2	7.4	ground.
P.H.E. doorway on S. Bldg. o'g Buek				
N ₂		4.3	7.3	
⊕		4.1	7.5	
S		3.9	7.9	
+ 0.6		3.57	8.02	doorstep
inside of Bldg.		3.70	7.89	floor laundry
→ 17.5 s Ventilator on S. N. Edge o'g 14 th Alley				
Top grating		4.02	7.57	
36.0 s Ventilator on S. N. Edge o'g 14 th Alley				
		3.63	7.96	
54.5 s Ventilator on S. N. Edge o'g 14 th Alley				
S on ventilator		3.11	8.48	
S ground		3.3	8.3	
⊕		3.6	8.0	
N		3.9	7.7	
100' E				
N		2.7	8.9	
L		2.5	9.1	
S		2.1	9.5	

plotted
 5-2-29
 J.C.



11.59
108'.E Entrance into Laundry on W.

15'-2.4 Floor of Laundry	3.40	8.19
S-0.7 on sill	1.00	10.59
S. ground	2.1	9.49

135'.E

S	2.0	9.6
C	1.9	9.7
N.	1.9	9.7
T.P.	12.57	23.21
	0.95	10.64

182'.E = N. Line ent. drive into Laundry Garage on S.

N	12.0	11.2
C	12.1	11.1
+8	12.0	11.2
S	12.2	11.0
+1.0 = ent. drive	12.24	10.97

193'.E = E. line ent. drive to garage on S.

S-1.0 = ent. drive	12.22	10.99
S	12.0	11.2
+2	11.6	11.6
E.	11.3	11.9
N.	11.3	11.9

200'.E

N	10.5	12.7
E	11.0	12.2
S	10.5	12.7

on ent. walk

23.21

Alley BIK. 138 N. + S.

210'.E.

70

S	10.3	12.9
E	10.3	12.9
N	9.8	13.4

230'.E

N	8.6	14.6
E	8.8	14.4
S	7.6	15.6

247'.E

S	4.4	18.8
+3	4.5	18.7
+6	6.3	16.9
E	6.0	17.2
+5	5.9	17.3
N	7.1	16.1
+4	7.5	15.7

House

250'.E

-4	7.1	16.1
N.	6.7	16.5
+1	4.0	19.2

+3 Pepper Tree Stump 2.0 Diam.

+5	4.0	19.2
+7	5.4	17.8
E	5.4	17.8
+4	5.6	17.6
+7	3.6	19.6
S	3.2	20.0

R3.21
251'E

S	3.0	20.2
+3	3.3	19.9
+4	5.4	17.8
⊥	5.2	18.0
+3	5.2	18.0
+7	3.2	20.0
N	3.1	20.1

267'E

N	1.7	21.5
+8	1.9	21.3
⊥	2.4	20.8
+5	2.6	20.6
S	1.2	22.0

T.P. 7.63 30.33 ✓ 0.51 22.70

295'E

S	7.5	22.8
C	7.6	22.7
N	6.7	23.6

R99'E, 7.5 N. of ⊥ = Pepper Tree stump 2' Diam

307' garage on S. cnt. floor 2'3 Back

N	6.3	24.0
C	7.0	23.3
S	6.9	23.4

+0.4: cnt. Apron 7.02 23.31

+2.3 floor 6.58 23.75

30.33
323'E

Alley Bk/38 N.+S.

71

S-0.6 End cnt. walk to House	6.19	24.14
S	6.5	23.8
C	6.6	23.7
N	6.4	23.9

331.2 E = M.H.

R. N. of ⊥ on M.H. 6.39 23.94

360'E.

N	5.7	24.6
C	6.1	24.2
S	6.0	24.3

409'E. garage on N. dirt floor 3'3 Back

S	5.5	24.8
C	5.3	25.0
N	5.1	25.2

+3.3

5.1 25.2 floor

433'E garage on S. dirt floor on line

N	4.9	25.4
C	5.2	25.1
S	5.3	25.0

470'E.

S	4.9	25.4
⊥	5.0	25.3
N	4.6	25.7

30.33

518' E garage on s. Wood floor 1.4 Back

N		4.2	26.1	
E		4.6	25.7	
S		4.6	25.7	floor

532' E. garage on s. line dirt floor

S		4.4	25.9	floor
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538' E. double garage on dirt floors 3.2 Back

S		4.1	26.2	
E		4.1	26.2	
N		3.8	26.5	
+3.2		3.4	26.5	floor

570' E

N		3.5	26.8	
E		3.8	26.5	
S		3.7	26.6	

595' E

S		3.5	26.8	
E		3.7	26.6	
+6		3.6	26.7	
N.		2.6	27.7	

600' E. = W. line Sigby St.

N		4.83	25.50	ent. cl. ret + ground
+8		4.30	26.03	Top M.H
E		4.5	25.8	ground
S		4.60	25.7	ent. cl. Ret. + ground.
T.R	601	30.86	5.48	24.85
chk on B.M.		6.95	23.71	23.94 + Sigby.

N.E. National

10-30-29
 J.C. Bliss
 Lynn Diebert
 Chuck Bauer

X-section Alley Block 214 Univer. Hqs
 10' to Vermont - between Essex +
 Robinson - 20' wide

Σ 292.37

73

B.M. J.W.B.P. Essex + Vermont 287.98

+439

Σ 292.37

W.G. Essex = 0.100 - Existing paving

N Top cb	4.67	287.70
G	4.80	287.57
E	5.02	287.35
G	4.86	287.51
S Top cb	4.72	287.65
	0+25	
S	4.4	288.0
E	4.5	287.9
N	4.7	287.7
	0+50	
N	4.8	287.6
E	4.5	287.9
S	4.6	287.8
	0+75	
S	4.8	287.6
E	4.6	287.8
N	4.7	287.7
	0+96	
E Garage 6' Back S.L. Concrete Floor	4.74	287.63 ✓

Plotted 11/4/29 - C.B.H.

	1+00			
N	5.1	287.3		
E	4.9	287.5		
S	4.9	287.5		
	1+20			
E 8' Garage 1' Back N.L. Dirt Floor	5.3	287.1 ✓		
	1+25			
S	5.3	287.1		
E	5.1	287.3		
N	5.6	286.8		
	1+31			
E 7' Concrete Drive 3.5' Back S.L.	5.58	286.79 ✓		
E 8' Garage at N.L. Dirt Floor	5.7	286.7 ✓		
	1+40			
E 8' Garage at N.L. Dirt Floor	5.8	286.6 ✓		
	1+49			
E 8' Garage at N.L. Dirt Floor	5.8	286.6 ✓		
	1+50			
N	5.8	286.6		
E	5.7	286.7		
S	6.0	286.4		
	1+51			
E 26' Concrete Double Garage Apron 8' in alley from S.L. East end.	5.20	286.47 ↓		
Garage floor 6' Back S.L. East end	5.76	286.61 ↓		
" " " " West end	5.95	286.42 ↓		
	6.31	286.06 ↓		

Σ 292.37

1475

S	6.2	2862
E	6.1	2863
N	6.2	2862

1470

12" Eucalyptus tree 3' in alley from N.W. ✓

1485

£8' Garage 3' Back S.L. Dirt Floor 6.2 2862 ✓

1498

£8' Garage 3' Back S.L. Dirt Floor 6.4 2860 ✓

2400

N 6.4 2860

E 6.3 2861

S 6.4 2860

2408

£8' Garage 3' Back S.L. Dirt Floor 6.4 2860 ✓

£8' " 2' " N.L. " " 6.4 2860 ✓

2418

£8' Garage 2' Back N.W. Dirt Floor 6.3 2861 ✓

T.P.

6.58 285.79

2.53

Σ 288.37

2425

S 2.8 2855

E 2.5 2858

N 2.3 2860

Σ 288.37

2435

£8' Garage 2.3' Back N.W. Dirt Floor 2.5 2858 ✓

2445

£8' Garage 2.3' Back N.W. Dirt Floor 2.7 2856 ✓

2450

N 2.7 2856

E 2.7 2856

S 2.4 2859

2475

S 3.3 2850

E 2.8 2855

N 2.8 2855

2478

£8' Garage 1' Back N.W. Wood Floor 2.5 2858 ✓

3400

N 3.1 2852

E 2.9 2854

S 3.1 2852

3420

£12 Concrete Apron 1' Back N.W.

East end 3.11 2852.1 ✓

West 3.13 2851.9 ✓

3425

S 3.4 2849

E 3.1 2852

N 3.2 2851

288.32

3+33

\$8 Garage 3' Back N.W. Int Floor 3.4 284.9 ✓

3+50

N 3.7 284.6

E 3.5 284.8

S 3.6 284.7

3+67

\$6 Concrete Double Garage Apron 1' in alley from S.W.

Garages are on S.W. Apron & Floors are here!

East end 3.33 284.99 ✓

West " 3.42 284.90 ✓

3+75

S 3.5 284.8

E 3.8 284.5

N 3.8 284.5

3+88

\$21 Concrete Double Garage Apron 1.6' in alley from S.W.

Garages are on S.W.

East end edge apron 3.78 284.54 ✓

Garage Floor 3.67 284.65 ✓

West end edge apron 4.11 284.21 ✓

Garage Floor 3.70 284.62 ✓

4+00

N 4.2 284.1

E 3.8 284.5

S 4.3 284.0

288.32

4+01

\$6 Concrete Double Garage Apron 1.5' Back N.W.

East end 4.08 284.24 ✓

West " 4.37 283.95 ✓

4+04

\$8 Concrete Driveway at S.W. 4.30 284.02 ✓

4+25

S 4.5 283.8

E 4.2 284.1

N 4.7 283.6

4+46 = Beginning 2' Concrete Walk at S.W. ✓

N 4.4 283.9

E 4.3 284.0

S 4.5 283.8

Edge Walk 4.20 284.12

4+80.5 = El. 10th St. = Existing paving ✓

Edge Walk 4.58 283.74

G 5.41 282.91

E 5.40 282.92

G 5.34 282.98

N Typo 5.08 283.24

B.M. S.E. B.P. 10th & Robinson 628 282.04

Correct 282.01

75

78

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 1/2 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body

of table in same row and column gives distance from side stake to slope stake. If ground is not

level, the side stake and slope stake, lower target by this amount if cut, otherwise add this amount.

To cut or fill and find distance in table. Set up rod at this point and level should cut tangent.

necessary.

TABLE No. 2.

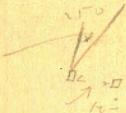
To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent (or external), opposite I by given tangent (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

270
80
196.50
125
250

80 Thomas
270 Reed
870
800
170
112



53.88

ENGINEERING DEPARTMENT
CITY OF SAN DIEGO
CALIFORNIA

69°-13'-00
28 10
35°55' 2)99.05

100
95.25
50.75

146.8
.3
143.8

277.5
5.5
272.0

45.25 55

83.52
17.3
85.25

32.50

1432.2

179.60'-00
102.46'-00
77.14'-00

102°-46'-00

343.87

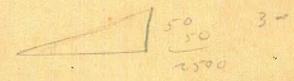
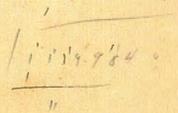
35.55
20.51
15.04

270
80
270
125
270

80
270
80
250
1695

620
10.75
380
14.25

119.82



50.2
7
43.9

44.3

100

20