

1258



FIELD BOOK

NO. 1258

MICROFILMED

DEC 22 1964

16-18 inside

65-14
32-37
16-18-30

3220
272
1140

ENGINEERING DEPARTMENT,
CITY OF SAN DIEGO,
CALIFORNIA.

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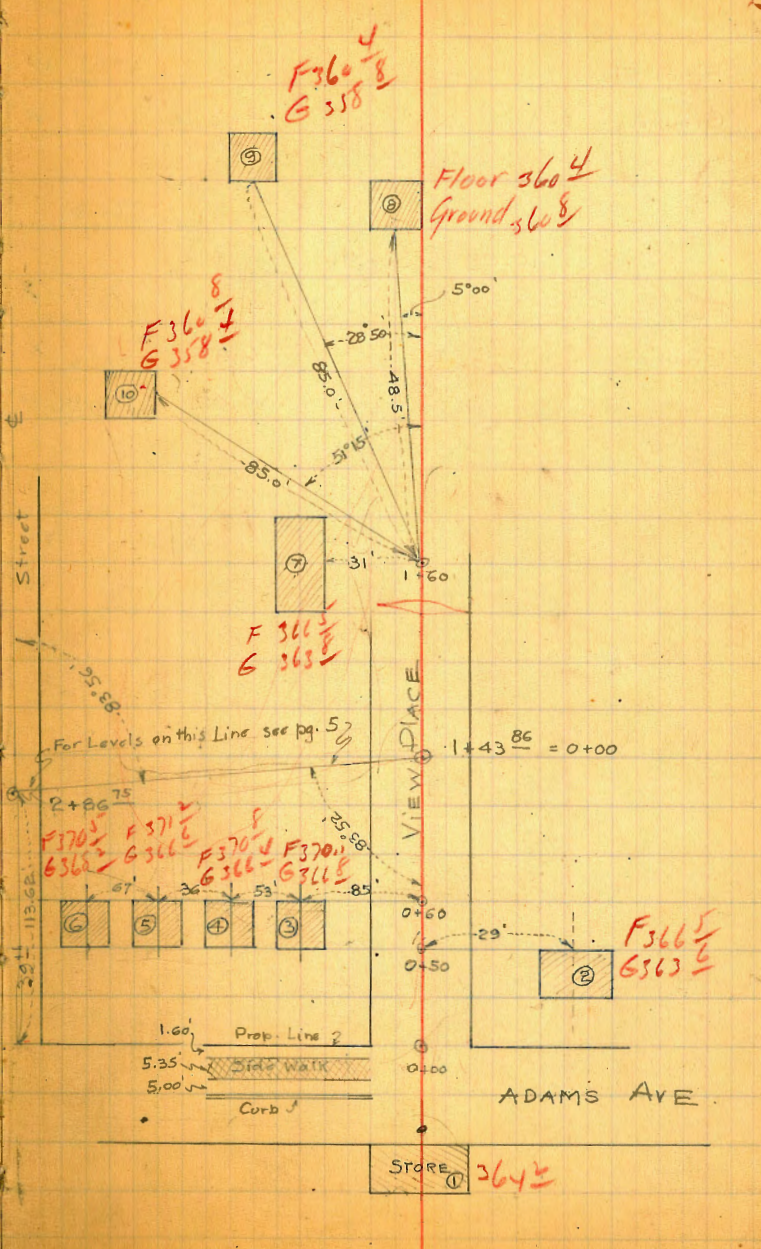
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ENGINEERING DEPARTMENT
CITY OF
SAN DIEGO,
CALIFORNIA.

Sewer Levels View Place & Vicinity

JAEGER }
Bailey } June 8th 1918
Clarett }

STA	+ H.I.	-	Elev.
B.M. S.E. B.P. 39 th & Adams			370.87
	0.42	371.29	
①		7.17	364.12 ✓
0+00		7.44	363.9 ✓
0+50		6.26	365.0 ✓
+60		6.40	364.89 ✓
1+60		8.07	363.2 ✓
T.P.		6.47	364.82 ✓
	6.70	371.52	
③ Floor Elev.		321.5	370.1 ✓
Ground		4.65	366.8 ✓
④ Floor Elev.		0.71	370.9 ✓
Ground		5.05	366.1 ✓
⑤ Floor Elev.		0.25	371.2 ✓
Ground		4.93	366.6 ✓
	2.82	367.64	
⑦ Floor Elev.		367.6	366.5 ✓
Ground		3.80	362.8 ✓
⑧ Floor Elev.		5.67	361.9 ✓
Ground		6.80	360.84 ✓
⑨ Floor Elev.		7.23	360.4 ✓
Ground		8.80	358.84 ✓
⑩ Floor Elev.		6.77	360.8 ✓
Ground		9.20	358.2 ✓



STA	+	H.I.	Elev.
(2) Floor Elev.		$\frac{367.8}{1.10}$	366.5 ✓
Ground		4.00	363.6 ✓
			364.82 ✓
(6) Floor El.	10.09	374.91	$\frac{374.9}{4.49}$ 370.5 ✓
Ground		6.65	368.2 ✓
		4.02	370.89 ✓

Check on B.M. SE. B.P. 39th & Adams 370.87

Sewer Levels & Alleys Bk. 45 & 44 Normal Hts.
 from W.L. 39th to E.L. Cherokee

STA.	+	H.I.	-	Elev.
P.M. SE. B.P. 39 th & Adams				370.87
	5.11	375.98		
Intersection of Alley & 39 th		376.4 4.95		3711 X
0+00 W.L. 39 th		4.69		3714 X
+50		3.60		3724 X
1+00		2.80		3732 X
+50		2.30		3737 X
2+00		1.60		3744 X
+50		1.80		3742 X
+87 ⁵⁰ E.L. Mountain View Dr.		3.41		3726 X
T.P.		3.19		372.79 X
	10.09	382.88		
? 3+27 ²⁰ Intersection of Alley Bk. 45 & E Mountain View Dr.		382.9 10.15		3728 X
0+00 W.L. Mountain View Dr.		9.33		3726 X
+50		7.80		3751 X
1+00		7.20		3757 X
+50		7.15		3757 X
2+00		6.70		3762 X
+50		5.95		3770 X
3+00		4.90		3780 X
+50		3.50		3794 X
4+00		1.70		3817 X
+50		0.15		3827 X
T.P.		0.60		382.28 X

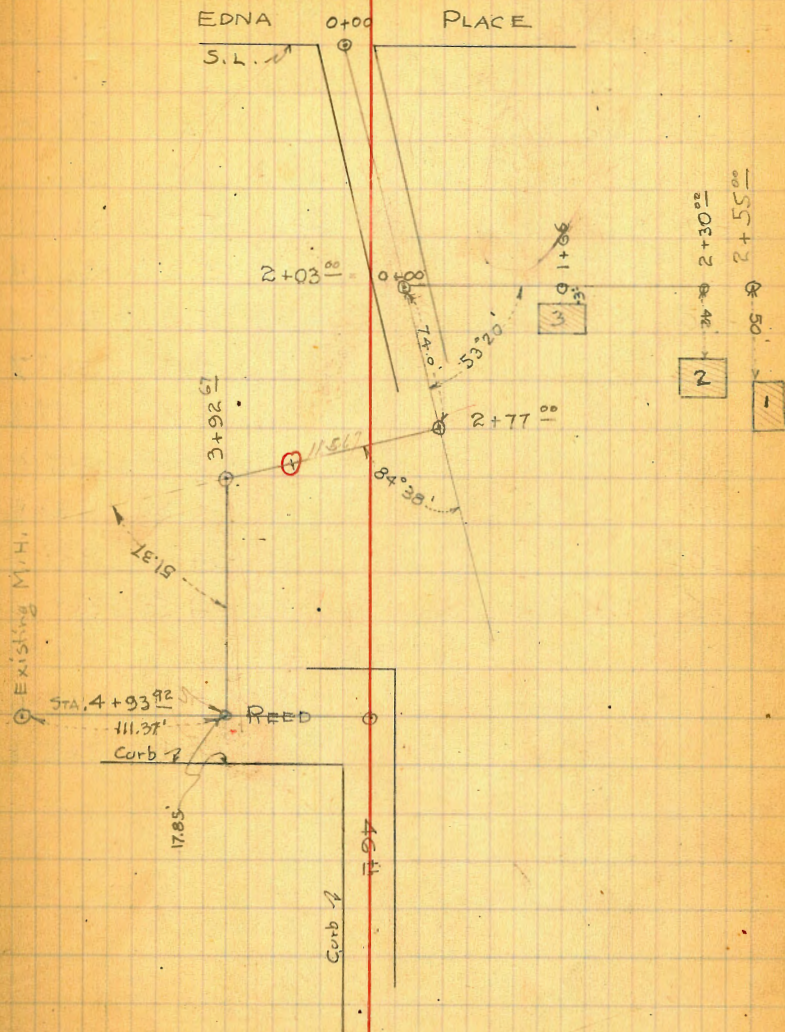
STA	+	H.I.	-	Elev.
	8.02	390.30		
4+98 ⁰⁶	E.W. Cherokee	590.3	4.52	3858 X
Intersection of Alley & Cherokee			4.40	3859 X

Levels from STA. 1+43⁸⁶ = 0+00 to 2+86⁷⁵
See Sketch Page 2

	T.P. see Page 2			
	2.54	367.36		364.82
0+00 = 1+43 ⁸⁶		367.3	3.56	3639 X
+50			2.50	3642 X
1+00			5.50	3619 X
+50			9.00	3584 X
2+00			7.80	3596 X
+23			6.90	3605 X
+28			2.00	3654 X
+63 ⁶⁰			1.45	3660 X
2+86 ⁷⁵ at 39th Str.			1.30	3661 X

Ward. Road
Sewer Levels from S.L. Edna Pl. to Intersection
of Reed Place & 46th Str.

STA	+	H.I.	-	Elev.
BM. SE. B.P. 39 th & Adams				370.87
	4.00	374.87		
T.P.			5.68	369.19
	1.22	370.41		
		<u>370.41</u>		
0+00		1.60		368.8 X
+50			2.70	367.2 X
1+00			3.20	367.2 X
+50			3.90	366.5 X
2+00			4.40	366.0 X
+50			5.20	365.2 X
2+77° Δ			6.10	364.3 X
3+00			6.00	364.2 X
+50			8.20	362.2 X
+60			10.20	360.2 X
+92.9 ⁹² Δ			7.60	362.8 X
T.P.			7.49	362.92 X
	4.87	367.79	8	
4+50		<u>367.50</u>		367.3 X
+93.9 ⁹²			3.60	364.2 X
Intersection Reed Place & 46 th			3.85	363.9 X



Sewer Levels from Sta. 2+03⁰⁰ (Ward Rd.) -

0+00 East to STA. 2+55⁰⁰
+ H.I.

- Elev.

Elev. 3+92⁶⁷ Sec Page 6

362.80

9.80 372.60

2+03⁰⁰ = 0+00

6.6 366.0

0+09

7.5 365.1

+17

5.5 367.1

+50

5.2 367.4

1+00

5.6 367.0

+50

4.9 367.7

+66

4.8 367.8

+66

3.6 369.0

2+00

4.80 367.8

+30⁰⁰

4.40 368.2

+55 T.P.

4.50 368.10 ✓

5.30 373.40

4.80 368.6

5.30 368.1

JAEGER } June 30th 1918
Bailey
Clarke

Floor Level House #3

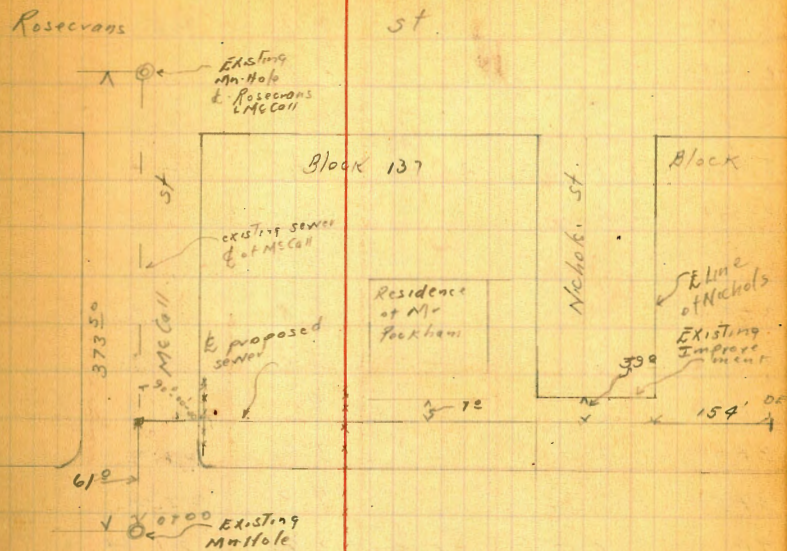
Ground Floor House #1

" " " #2

Bliss Due-mit Jacobson Krieman 7/2/28 B.M. NW BP Mo. Call. + Rosecrans		Location of and Levels for		Sewer across Blocks
137-153 La Playa				Elev
	3.85	41.99	-	38.14
Flow Line of Existing Man. Hole of Rosecrans & McColl		9.70		32.29
TP.	2.02	37.07	6.94	35.05
TP	0.15	29.49	12.73	29.34
TP	0.37	12.85 12.70	12.01	12.83
Rim of Existing Man. Hole of McColl		9.18		3.67
Flow Line ...		19.90		-1.55
TP	8.92	12.44 ⁵⁹	9.18	3.52 ⁶⁷
at 00 in Man. Hole		8.92		3.67
at 24		8.18		4.41
at 61 Δ 90°00'-00P		4.65		7.94
at 73.5 Gutter		5.50		7.09
at 73.5 Top of		4.82		7.77
at 78		3.8		8.77
at 84 E. Line of McColl		4.2		8.39
at 91 $\frac{1}{2}$ Cross-fence		4.5		8.09
100		5.3		7.79
112.5		6.1		6.59
113.5		5.5		7.09
1150		2.9		9.69
1155		1.7		10.89
1162		0.2		12.4
1166		0.1		12.5
1168		2.5		10.1
1170		3.8		8.8
2700		3.2		9.4

Sketch of proposed Private
Sewer Across Blocks 137-153
La Playa.

8



40

		759 12.94		
414			1.3	11.3
218			2.8	9.8
2125			2.4	10.2
2131			1.9	10.7
T.P.	13.23	47 25.32	0.35	12.29
2137 ^E	crosses fence		12.1	13.40
2138			10.3	15.2
2146			6.8	18.7
2150			5.8	19.7
2170			4.2	21.3
3100			3.8	21.7
3150			4.3	21.2
T.P.	4.11	60 25.95	3.98	21.39
3180			4.8	20.8
3182			5.4	20.2
3186	W line of Nichols		5.1	20.2
4100			6.2	19.4
4111	E Nichols		6.0	19.6
4125			2.3	19.3
4136	E line of Nichols		6.7	18.9
4150			5.8	19.8
5100			5.8	19.8
5150			5.2	20.4
5186			4.2	21.4
5190 ⁴⁰	End of line		4.1	21.5
T.P.	11.70	91 36.76	0.39	25.21

TP 8.91 45.11
~~44.96~~ 70
 36.55
 38.14
 27.99

check on starting BM N.W. Mc Coye Rosecrans
 6.97

Notes
 N. L. Juniper
 8-26-20

Cross Section CALIFORNIA ST
 From N.L. Juniper to N.L. Chokras
 7.5' wide
 12.75' 4.5'

5.12 22.12 17.00

Exit
 Note. as face on Prop. Lines

N.L. Juniper = 0+00

E. top cb.	5.90	16.22
E. Gut. on Paring	6.64	15.48
" 1/4 " "	6.23	15.89
E top Rail	6.00	16.12
" " "	6.00	16.12
E " Rail.	6.25	15.87
" 1/4 on Par.	6.55	15.57
" cb " "	6.98	15.14
" Gut. on Par.	7.75	14.37
" top cb.	7.10	15.02

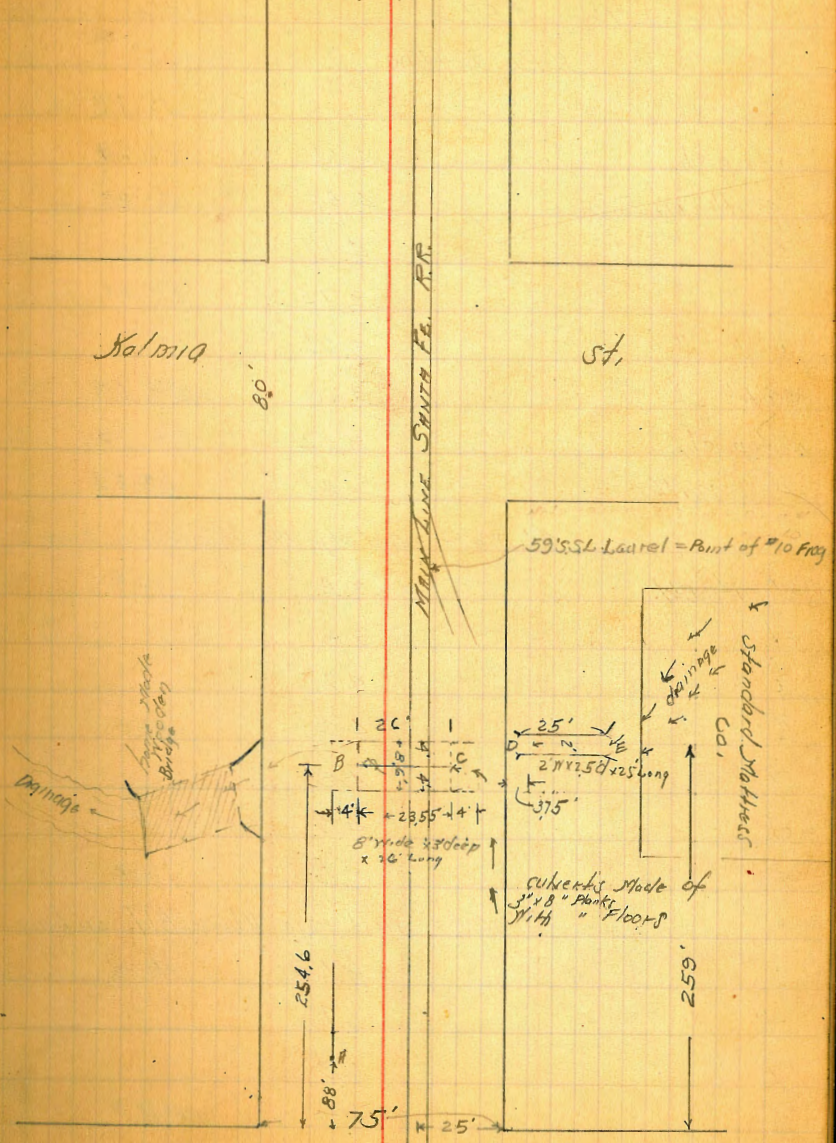
Con. Floor R= 4.00 18.12
 0+32 = Doorway to Macaroni Factory 254' back

0+50

-5	8.8	13.3
"	8.8	13.3
cb.	8.1	14.0
1/2	8.6	
E.	8.5	13.6
+7	7.0	
West Rail	6.14	15.98
1/4 "	6.6	
E Rail	6.11	16.01
+6	6.6	
cb.	7.1	

Cont. on Page 46

Continuation of sketch
 on Page 46



Kalmia

80'

St.

59' S.S.L. Laurel = Point of 10' frog



JUNIPER

Walker
Ruppel
Shaw
8-22-28

X. Section LAUREL St 80' wide 14' cbs
From N.L. Kettner Bld. to E.L. California

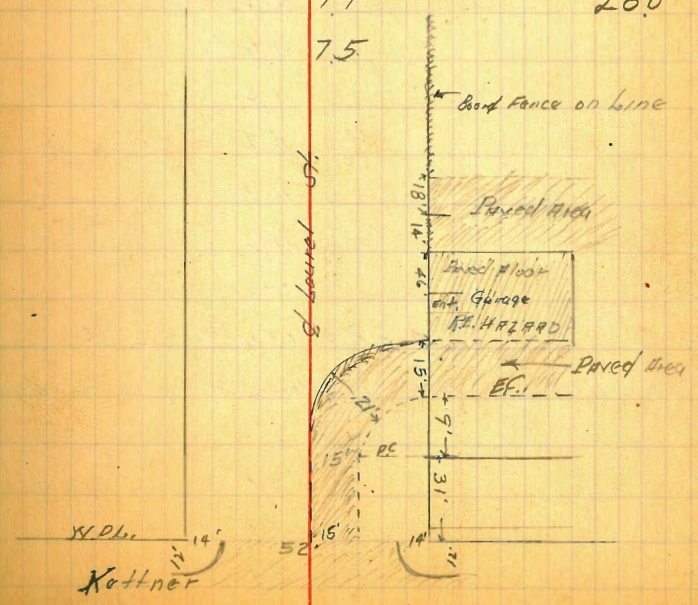
35.75

11

SE. BP	2.78	35.75	32.97
Laurel & Kettner			
	N.L. Kettner Bld - 0+00		
S	3.56	32.19	
S top cb.	4.11	31.64	
S Gutter on Paving	4.50	31.25	
1/4 " " "	4.11		
1/2 " " "	3.74	32.01	
1/4 " " "	3.66		
N Gut " " "	3.68	32.07	
N top cb.	3.02	32.73	
N " Walk	2.51	33.24	
	6' West = East edge Bld. on North on line		
N of Bld.	2.4	33.3	
cb.	3.8		
1/4	4.2		
1/2	4.2	31.5	
1/4	4.3		
cb	4.2		
S	3.5	32.2	
	31' West = West edge Above Bld. on line		
S	6.7	29.0	
cb.	6.7		
1/4	6.3		
1/2	6.4	29.3	
+2 on Paving (South edge)	6.25		

Plotted 9-11-28 - C.B.H.

1/2 on Paving	6.55	
+5 " (North edge)	6.87	
cb.	7.0	
N of Bld.	6.3	29.4
40' N = E.C. Paving	see sketch	
(N-10') on Paving	9.14	
N on Paving	8.41	27.34
cb " "	8.00	
1/4 " "	7.21	
+11 " = S. edge	6.93	
1/2	7.3	28.4
1/4	7.1	
cb	7.5	
S	7.7	28.0
+5	7.5	



35.75

	55' West = West edge	aving	on North Side East edge Bld. on line	
-5		7.2		
S		7.2	26.5	
cb.		9.4		
$\frac{1}{4}$		7.2		
$\frac{1}{4}$		8.9	26.8	
$\frac{1}{4}$		8.6		
+3 on paving		8.40		
cb " "		8.60		
N " "		8.80	26.95	
+10 " "		7.5		
	81' West = $\frac{1}{2}$ Above Bld. = 2' DIVE WAY			
N on paving		11.40	24.35	
cb.		11.5		
$\frac{1}{4}$		11.6		
$\frac{1}{4}$		11.3	24.4	
$\frac{1}{4}$		11.7		
cb.		11.8		
S		11.3	24.4	
+5		11.0		
TP	2.14	24.88	13.01	22.74
	101' N = West edge Above Bld. on North on line			
-5		3.0		
S		3.1	21.8	
cb.		3.5		
$\frac{1}{4}$		3.1		
$\frac{1}{4}$		2.7	22.2	

24.88

LAUREL ST.
X. Section

12

$\frac{1}{4}$		2.8	
cb.		3.0	
N at Bld.		1.7	23.2
	115' N = East edge Aving on N on line		
-10		4.60	
N		4.60	20.3
cb.		4.0	
$\frac{1}{4}$		4.2	
$\frac{1}{4}$		4.2	20.7
$\frac{1}{4}$		4.3	
cb.		4.5	
S		4.5	20.4
+10		4.2	
	133' N = West edge Aving on North		
-5		5.2	
S		5.2	19.7
cb.		5.4	
$\frac{1}{4}$		5.3	
$\frac{1}{4}$		5.2	19.7
$\frac{1}{4}$		5.1	
cb.		5.3	
N on paving		5.05	19.63
+10 " "		5.0	
	175' N		
-10		6.4	
N		6.4	18.5

2488

640 E. L. St.
X. Section

Duplicate 13

cb.	6.7	
$\frac{1}{4}$	6.8	
L	7.1	17.8
$\frac{1}{4}$	7.4	
cb	7.3	
S	8.2	16.7
+10	8.5	

300' West - E. L. California St.

-10'	9.5	
S	9.3	15.6
cb.	9.1	
$\frac{1}{4}$	9.0	
L	7.4	17.5
$\frac{1}{4}$	7.2	
cb.	7.1	
N	7.1	17.8
+10	7.2	
	7.88	17.00

T.P. on 3 Nails ^{10 Bolt} N.Y. California + hours!

Cont. in Book 1272-63

Cross Section MAPLE St. 80' wide
From N.L. Kettner to E.L. Cal.

#414
44.73

13

N.L. Kettner

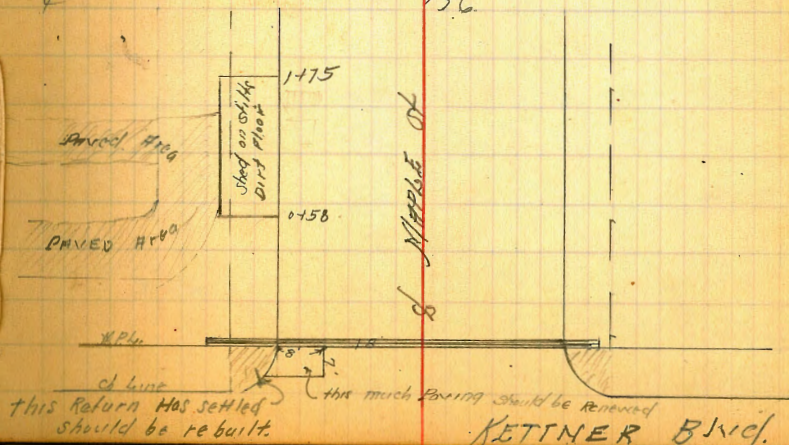
Maple & Kettner

	44.73	42.11 OK.	
Maple & Kettner	2.62	44.14	41.52 = This is wrong Fire Hdr. moved
N.L. Kettner Blvd = 0+00			
N	5.9	38.8	
N top Cb.	6.60	38.13 ✓	
" Gutter on Br.	7.20		
1/4 " "	7.00		
1/2 " "	7.13	37.60	
+5 " "	7.34		
3/4	10.5		
+4	8.0		
S Gutter on Grating	9.00		
S top Cb.	8.05	35.68 ✓	
S	8.00		
+5	8.2		
0.5' W - 1/2 10" Con Wall Parallel With Kettner			
-5	9.2		
S	9.0		
+9 - beginning Con. Wall	8.10	36.63	
cb.	8.05		
1/4	7.30		
1/2	6.64	38.09	
3/4	6.32		
cb.	6.10		
+5 = END of WALL	6.05	37.68	
N	6.0		

Plotted 9728-CBH

1.5' W = Section Base of Con. Ret. Wall

N	6.7	38.5
-9	8.0	
cb.	8.5	
1/2	8.8	
1/4	9.0	35.7
+10	9.9	
1/4	13.2	
cb.	15.7	
+5	12.5	
S	8.9	35.8
+5	9.0	
4' W.		
-10	12.2	
S	12.2	32.5
+11	13.4	
cb.	15.5	
1/4	13.6	



~~44.14~~
44.73

MAPLE ST.
X-Section

1/4 +3		10.3	
1/2		9.7	35.5
1/4		8.6	
cb.		8.2	
N		7.4	37.3
T.P.	(minus Ref) 31.71 -0.30 31.42	12.72	32.01 31.42
	10' NY	0.1	
-15		0.1	
N		2.2	29.5
cb.		2.3	
1/4		1.6	
1/2		2.1	29.6
1/2		2.2	
+8		4.0	
cb.		6.3	
+4		3.0	
S		4.1	27.6
+15		3.6	
	14' NY		
-15		8.4	
S		7.7	24.0
cb.		6.8	
1/2		5.0	
1/2		5.3	26.4
1/4		4.2	
cb.		3.6	

31.72
31.71

14

N		3.1	28.6
+15		1.7	
	21' NY		
-25'		9.6	
N		9.6	22.1
cb.		9.4	
1/4		9.4	
1/2		9.2	22.5
1/4		8.4	
cb.		8.8	
S		9.4	22.3
+25		9.4	
	Garage 0+58 = East edge shed on South 14' 1/2" st		shed is on stilts
-20' on Porch		10.37	
-1' " " N. edge		10.21	
S		10.0	21.7
cb.		10.0	
1/4		9.4	
1/2		9.6	22.1
1/2		9.9	
cb.		10.0	
N		10.0	21.7
+20		10.0	
	1+0.0		
-15		11.1	
N		11.0	20.7

3112
3171

MAPLE St.
X Section

cb.		11.2	
1/4		11.2	
1/2		11.0	20.7
3/4		11.0	
cb.		11.0	
S		11.0	20.7
+15		11.3	
T.P.	3.17	23.14	19.97
		22.55	19.38
		11.74	

Note: bet. 0+58 + 1+75 there is 11,000' of 10" Cast Iron
Pipe in St. bet N 1/2 + South cb.
Also 6,000 12" Iron Pipe (cast)

1+50

-10		3.5	
N		3.5	19.6
cb.		3.6	
1/4		3.4	
cb.		3.5	19.6
1/4		3.5	
cb.		3.6	
S		3.7	19.4
+10		3.7	

1+75 = West edge Garage shed on S 14' in St.

-10		4.8	
S		4.7	18.4
cb.		4.3	
1/4		4.1	
1/2		4.2	18.9

2255
2314

15

1/2		4.4	
cb.		4.5	
N		4.2	18.9
+10		4.3	
1+94 = E Rail of Santa Fe siding Rtd to Maple			
N on top of Rail		4.33	18.81
S " " " "		4.70	18.44
1+98.72 = West Rail			

S		4.70	18.44
N		4.33	18.81
2+00			

N		4.8	18.9
cb.		4.8	
1/2		4.9	
1/2		4.9	18.2
1/2		5.0	
cb.		5.1	
S		5.2	17.9
Cal. + MAPLE			
T.P. 3 Nails in SW Pole		4.58	18.56 see Page 6)
			+7.9.7

26' Ker
Rupliger
Shard
Shell

Cross Section NUTMEG St. 80' wide
Bet. Kettner Blvd. & California St.
14' cbs
13' 1/2 S

47.42
48.01

16

NE. top Hndth Maple & Kettner	48.01 47.42	42.11 41.52	80' wide 14' cbs 13' 1/2 S	cb. 1/4 1/2 1/4 cb. N +10 +20 -20 -10 N +12 cb. 1/4 1/2 1/2 cb. +7 S +25 -25 S cb. 1/2	5.9 5.3 4.8 4.9 3.9 4.6 9.1 9.5 12.1 12.1 10.3 10.0 8.0 8.2 8.6 9.7 13.7 14.8 17.8 19.9 22.2 20.4 18.4 16.8	43.2 43.4 37.7 39.4 30.2 27.6
S	3.32					
S top cb.	3.94	44.07				
S Gutter on Brink X X X X	4.52	43.49				
1/2 " "	3.56					
1/2 " "	2.92	45.09		0+35		
1/4 " "	2.63					
N " " "	2.73					
N top cb.	2.14	45.87				
N " Salt	1.58	46.43				
	0+05					
N	1.9	46.1				
cb.	2.6					
1/4	2.9					
1/2	3.2	44.8				
1/4	3.5					
cb.	4.5					
+5	5.2					
S	6.3	41.8				
+5	6.2					
	0+15					
-20	14.8					
S	13.9	34.1				

Plotted 9-7-28 - C.B.H.

0+53 = End cut at 10' S. side
0+53 = 8 Con. steps on North 20' Beck. of line
(Steps to office Home Title Co.)

		47.42 +8.01 +	Rods	Ground Elev.		35.60 36.19	Nutmeg St. X. Section	17
6			14.4	33.6	6	8.3	27.9	
7			12.4		7	7.3		
cb.			12.6		cb.	7.1		
+40N	14" Corrug. Iron pipe Floor Line		16.0		N	6.6	29.6	
+8			13.9		+15	6.0		
N			14.7	33.3				
+20			13.2		-15	6.4		
+20	on top Bottom step		12.13	35.88	N	7.3	28.9	
+25	" " con. step		11.00		cb.	8.1		
T.P.		36.19	12.96	35.25	7	9.0		
Note: Dist Drive Way on South		35.60		34.46	8	10.0	26.2	
8+0+53+0+70	0+70 = East edge			Machine Shop				
25			2.8		9	10.6		
N			4.2	32.0	cb.	11.3		
+8			5.2		S at Bld.	12.0	24.2	
cb.			3.8					
7			3.9		1+21 = East edge South Foundry	13.1 at Bld.		
6			5.6	30.6	1+35 = " " Acme tile Co.'s	Bld. on North on line		
5			7.4		S = base Foundry Bld.	14.3	21.9	
cb.			8.3		cb.	13.4		
S at base of Bld.			9.0	27.2	7	12.5		
+20			10.4		6	12.2	24.0	
	↓ Wooden Floor (8' doorway) Door to Machine Shop		8.55	27.54	5	10.3		
	0+95				cb.	9.7		
S at Bld.			10.8	25.4	N at Bld.	9.0	27.2	
cb.			10.0		+15	8.8		
7			9.0		on South on line			
					1+41 = 1/2 Doorway to Foundry	13.8	22.4	
					1+68			

3560
3619

Nutmeg St.
X-Section

N of Bld.		9.2	27.0
+ 8		12.6	
cb.		13.5	
$\frac{1}{4}$		14.4	
$\frac{1}{2}$		14.5	21.7
$\frac{1}{4}$		14.6	
cb.		15.2	
S = at Base Foundry Bld.		15.6	20.6
T.P.	2.05	26.46	24.41
		25.87	23.82

Note: bet. Sta. 1+00 + 2+00 there is in the st. the following Articles:
 2 - Galv. Iron tanks 10' x 8' 1/2"
 3 - Wooden Platforms 4' x 8' x 8' sq.

Also several Piles of Forms for Foundry Work

1+75 = West edge Foundry on South, and West edge Bld. on North

S - Base of Foundry Bld.		6.6	19.9
cb.		6.1	
$\frac{1}{4}$		5.6	
$\frac{1}{2}$		5.7	20.8
$\frac{1}{4}$		5.4	
cb.		4.4	
N		1.2	25.3

1+90

-10		5.2	
N		5.5	21.0
cb.		6.0	
$\frac{1}{4}$		6.3	
$\frac{1}{2}$		6.2	20.3

2587
2642

18

$\frac{1}{4}$		6.3	
cb.		6.5	
S		7.3	19.2
2+00 = E.L. CALIFORNIA ST.			
S		8.1	18.4
cb.		7.3	
$\frac{1}{4}$		6.2	
$\frac{1}{2}$		5.8	20.7
$\frac{1}{4}$		5.6	
cb.		5.7	
N		5.4	21.1
T.P. 3 rails in NE. Tol. Pole		4.20	21.26 See Page 66 21.67 For chkt.

N		5.2	
cb.		5.5	
$\frac{1}{4}$		5.5	
$\frac{1}{2}$		5.6	
$\frac{1}{4}$		5.9	
cb.		6.5	
		6.8	

Note: for X-Section West Calif St see Book 1272-68

3/4 NW 1/4
8-23-28

Cross Section OLIVE st 50' wide
Bet Kettner Blvd. & Cal. St. 14' cb S
13' 4/8

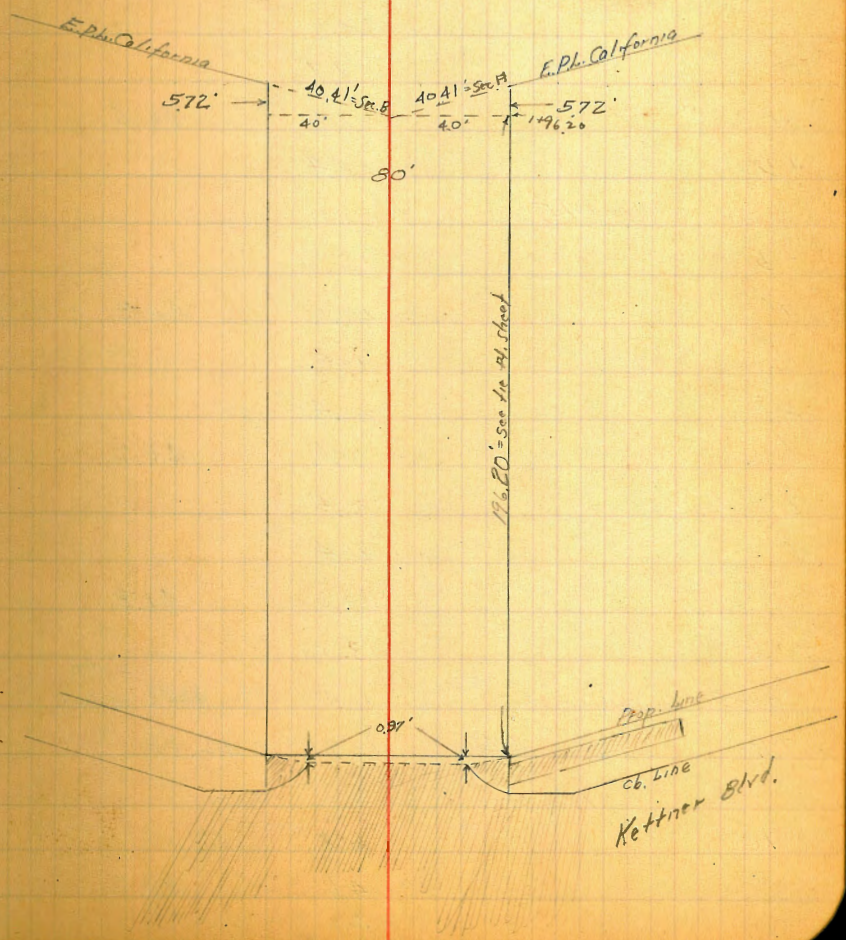
B.M. NW 1/4			
B.P. Olive & Kettner 0.62	54.33	53.71	
Top Walk			
	M.L. Kettner Blvd = 0+00		
N top Walk	1.04	53.29	
" " cb.	1.51	52.82	
" Gut on Parap	2.11		
" 1/4 " "	2.02		
1/2 " "	2.16	52.17	
1/4 " "	2.61		
S Gut " "	3.40		
S top cb.	2.98	51.35	
S " Walk	2.60	51.73	
	0+05		
S	3.00	51.3	
cb.	3.0		
1/2	3.2		
1/4	2.7	51.6	
1/4	2.7		
cb	2.9		
N	3.5	50.8	
+5	3.5		
	0+25		
S	5.5		
N	5.5	48.8	
cb.	4.8		
1/2	5.0		

Plotted 9-7-28
CBH

54.33

19

1/2	4.8	49.5
1/2	5.1	
cb.	5.2	
S	6.3	48.0
+10	7.8	
0+42 = 1/2 Euc. Tree on S 1 Back	8.7	12" dia.



5433

0+50 = $\frac{1}{2}$ Euc tree on S. 5" dia. on line

-10	10.7	
S = at tree	9.6	44.7
+4	8.2	
cb.	8.3	
$\frac{1}{4}$	8.4	
$\frac{1}{2}$	8.1	46.2
$\frac{3}{4}$	8.0	
cb.	7.7	
N	7.8	46.5
+5	7.4	

0+75

-5	10.0	
N	10.0	44.3
cb.	10.4	
$\frac{1}{4}$	10.4	
$\frac{1}{2}$	10.6	43.7
$\frac{3}{4}$	10.5	
cb.	11.4	
S	13.0	41.3
+10	13.8	

0+85 = 5' con. walk on North

T.P.	2.19	44.31	12.21	42.12	2' wide 2' back.
------	------	-------	-------	-------	---------------------

1+00

-10	6.8	
S	4.7	39.6
cb.	4.0	

4431

olive st.

X. Section

20

$\frac{1}{2}$	3.6	
$\frac{3}{4}$	3.0	41.3
$\frac{1}{4}$	2.8	
cb.	2.7	
N	1.6	42.7

1+25

N	3.8	40.5
cb.	4.0	
$\frac{1}{4}$	4.6	
$\frac{1}{2}$	5.2	39.1
$\frac{3}{4}$	5.5	
cb.	6.5	
S	7.9	36.4
+10	8.3	

1+41 = $\frac{1}{2}$ Garage on N dirt floor 4.8 ✓2' back
39.5 8' wide

1+50

-10	10.0	
S	8.9	35.4
cb.	8.2	
$\frac{1}{4}$	7.4	
$\frac{1}{2}$	6.7	37.6
$\frac{3}{4}$	6.8	
cb.	6.5	
N	5.7	38.6

1+75

N	7.8	36.5
---	-----	------

cont. on Page 26

Walker
Res. 1/2
S. 22-28

Cross Section Pair of 80' wide 14' cbs
13' 45"
Bet. Kettner Blvd & Co. 1. st

62.39

21

NY 89
Oliver Kettner 8.68 62.39 53.71

W.L. Kettner Blvd = 0+00

Note: det. bet. cbs on W.L. Kettner = 51.4
x. Section for 52' Rel. Way

S on Walk	5.73	56.66
S top cb.	6.06	56.33
S Gut. on Boring	6.75	55.64
S 1/4 " "	6.73	56.16
E " "	5.97	56.42
N 1/4 " "	5.95	56.44
N Gut " "	6.25	56.14
N top cb	5.52	56.87
N " Walk	5.14	57.25
0+01		
N	3.3	59.1
cb.	2.9	59.5
+1	3.7	58.4
1/2	4.4	58.0
E	4.4	58.0
+10	3.9	58.5
1/2	5.7	56.7
cb.	6.1	56.3
+2	3.4	59.0
S	2.8	59.6
0+25		
S	5.3	57.1
cb.	5.3	57.1

Plotted 9-7-28- G.B.H.

1/4	54	57.0
1/2	4.8	57.6
1/4	4.6	57.8
cb.	4.7	57.7
N	4.6	57.8
0+50		
N	7.9	54.5
cb.	7.4	55.0
1/4	7.2	55.2
E	7.4	55.0
1/4	8.3	54.1
cb.	8.0	54.4
S	8.6	53.8
+5	9.0	53.4
TP 407		
53.78 12.68		49.71
0+77		
-5	3.0	50.8
S	2.7	51.1
cb.	2.4	51.4
+3	1.3	52.5
1/4	1.1	52.7
1/2	1.5	52.3
1/4	1.5	52.3
cb.	1.6	52.2
N	1.8	52.0
+5	1.8	52.0

5378

1+95

N	4.0	49.8
cb.	4.0	49.8
$\frac{1}{2}$	4.4	49.4
$\frac{1}{4}$	4.6	49.2
$\frac{1}{4}$	4.8	49.0
cb.	5.2	48.6
S	5.4	48.4
+5	5.5	48.3

1+04 = 2 Pepper tree on N 8' in st	4.4	10" dia.
1+14 = " " " " " " " "	5.3	6" "
+22 = " " " " " " " "	6.9	5" "
+32 = " " " " " " " "	7.8	6" "
+39 = " " " " " " " "	8.6	6" "
1+47 = " " " " " " " "	9.2	6" "
+52 = " " " " " " " "	10.1	4" "
1+52 = " " " " " on line	10.4	5" "

1+15

-5'	8.0	45.8
S	7.8	46.0
cb.	8.0	45.8
$\frac{1}{4}$	7.0	46.8
$\frac{1}{2}$	6.7	47.1
$\frac{1}{2}$	6.1	47.7
cb.	5.6	48.2
N	5.4	48.4

5378

1+50

N	10.1	43.7
cb.	11.1	42.7
$\frac{1}{2}$	11.0	42.8
$\frac{1}{4}$	11.1	42.7
$\frac{1}{4}$	10.9	42.9
cb.	11.2	42.6
S	11.8	42.0
+5	12.0	41.8

TP 123 42.79 1222 41.56

1+86

S	4.3	37.5
cb.	4.0	38.8
$\frac{1}{2}$	3.9	38.9
$\frac{1}{4}$	4.0	38.8
$\frac{1}{4}$	3.6	37.8
cb.	3.2	39.6
N	2.8	40.0

1+92

N	5.2	37.6
cb.	5.5	36.3
$\frac{1}{4}$	5.5	36.3
$\frac{1}{2}$	5.6	37.2
$\frac{1}{2}$	5.9	36.9
cb.	6.5	36.3
S	6.8	36.0

22

1497

S	5.2	37.6
cb	4.9	37.9
$\frac{1}{2}$	4.6	38.2
$\frac{1}{4}$	4.5	38.3
$\frac{1}{4}$	4.1	38.7
cb.	3.4	39.4
N	3.3	39.5

2+00 = E.L. CALIFORNIA

N	3.9	38.9
cb.	4.0	38.8
$\frac{1}{4}$	4.7	38.1
E on cen Monument	5.16	37.63
$\frac{1}{4}$	5.0	37.8
cb.	5.5	37.3
S	5.7	37.1

For Ch. Sec
Page 75

Note: Cross sections cont. Book 1272-70

Walker
Rip
Shed
P. 23-28

Cross Section QUINCE 80' wide
Bet Kettner + Col. St.
14' cl
13' 1/2 S

6249

24

M. Kettner = 0400

NE top Hyd.	0.74	62.49	61.75
N on top Walk		3.81	58.68
N " " cb		4.03	58.46
N Gut. on Pav.		4.58	57.91
" 1/4 " "		4.07	
1/2 " "		3.93	58.56
S 1/4 " "		4.13	
S Gut " "		4.56	57.93
S top cb.		4.01	58.48
S " Walk		3.73	58.76
0+11 = Pepper tree on S 12' 10" st.		5.1	10" dia
+23 = " " " " " " " "		6.1	6" "
+36 = " " " " " " " "		6.9	8" "
+47 = " " " " " " " "		7.5	
	0+50		
S		8.2	54.3
cb.		8.0	
1/4		8.0	
1/2		7.9	54.6
1/4		7.9	
cb.		8.1	
N		7.1	55.4
	0+86		
N		11.6	50.9

Plotted 9-7-28-CBH

cb.		11.8	
1/4		11.5	
1/2		11.8	50.7
1/4		12.2	
cb		12.2	
S		12.4	50.1
		12.4	50.1 ^{10' wide}
	0+91 = Garage on South side dirt floor		
	0+94 = " " " N " " " ✓	12.3	50.2 ^{10' wide}
	1+01		
S		13.2	49.3
cb.		13.4	
1/4		14.1	
1/2		14.0	48.5
1/4		14.0	
cb.		14.3	
N		14.4	48.1
	TR 083	50.94	12.38
	1+34		50.11
N		5.0	45.9
cb.		4.9	
1/4		5.1	
1/2		5.5	45.4
1/4		5.4	
cb.		5.2	
S		5.2	45.7
	1+70 = Garage on S dirt floor	9.9	41.0

5094

1+74

S		10.0	40.9
cb.		10.2	
$\frac{1}{4}$		10.5	
$\frac{1}{2}$		11.0	39.9
$\frac{3}{4}$		10.7	
cb.		10.9	
N		10.9	40.0

1+82

N		11.7	39.2
cb.		11.3	
$\frac{1}{4}$		11.5	
$\frac{1}{2}$		11.6	39.3
$\frac{3}{4}$		11.5	
cb.		12.1	
S		12.0	38.9

1+88

S		11.5	39.4
cb.		11.7	
$\frac{1}{4}$		12.1	
$\frac{1}{2}$		11.7	39.2
$\frac{3}{4}$		12.3	
cb.		12.3	
N		12.6	38.3

2+00 = E.L. CALIFORNIA

N		15.3	35.6
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5094

QUINCE ST
T. Section 25

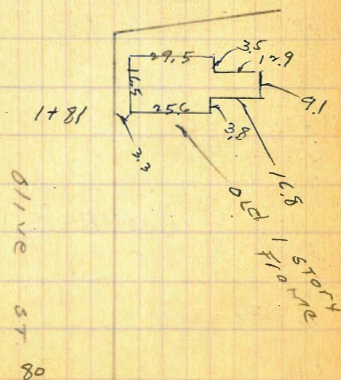
cb.		14.2	
$\frac{1}{4}$		14.4	
La on Con. Mon. N. Calif. + Quince		14.64	36.30
$\frac{3}{4}$		14.6	
cb.		14.1	
S		14.4	36.5

For ch. see
Book 1272-3Note: For X-sections West of Calif. St.
See Book 1272-73Place location & levels on house
8-6-41 NE Cor Olive + Calif.Com. Mon. 11.81 40.83 299⁰⁰ Olive Calif

1+81 N.W. ground 4.6

Floor elev. 1.27

Calif.



0+00

KETTNER

4431 olive st. X Section
Cont. from Page 20

1725

cb.	7.8	
1/4	8.6	
1/2	8.6	35.7
3/4	9.3	
cb.	9.8	
5	10.6	33.7
710	11.7	
1796.20 See sketch p-19		
5	13.4	30.9
cb.	12.6	
1/4	11.8	
1/2	11.0	33.3
3/4	9.6	
cb.	9.0	
N	8.7	35.6
Section A		
N	10.2	34.1
cb.	9.4	
1/4	10.1	
1/2	11.0	33.3
Sec B		
1/2	11.0	33.3
3/4	11.9	
cb.	13.3	
5	14.1	30.2

T.P. on E Mon. 25' x Calif. and on olive 13.66 30.65
Note see Page 69 For chk. on this Mon.

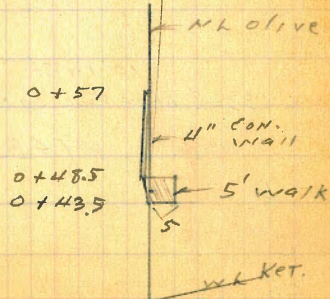
Moore Add. Levels on Olive bet.
8-4-x1 Kettner & Calif.

26

NWGP					olive
Top wall	2.24	55.95		53.71	Kettner
0+43.5	Top walk	8.36	47.59		North on line
0+48.5	" walk & wall	8.45	47.50		N + 0.5
0+57	" wall	8.25	47.30		N + 0.7
0+85	" 2' walk	12.07	43.93		N - 2
T.P. 119	X 4.36	12.78	43.17		
1720 1/2 4'	CON walk	3.23	41.13		N - 1.5
1741 1/2	Singer dirt floor	4.8	39.56		N - 8.3
T.P. 7.15	38.14	8.37	35.99		
on Mon 25' x Calif.	olive	9.17	29.07		30.65
T.P. 11.22	47.21	2.15	35.99		
T.P. 10.39	56.52	10.8	46.13		
orig. B.M.		2.81	53.71		

See p 25 for house Elev.

Mon. has been lowered to 29.07



Walker
Ruplinger
Shaw
Shaw 8-23-28

Cross Section Redwood St. 80' wide
Bet. Kettner Blvd. & Cal. St. 14' chs
13' #1

62.17

27

0.42	62.17	61.75
W. Kettner -0+00		
S top Walk	4.46	57.71
" " cb	5.00	57.17
" Gutter Parap	5.73	
" 1/2 " "	5.40	
" " "	5.31	56.86
N 1/2 " "	5.52	
" Gut " "	5.92	
" top cb.	5.25	56.92
" " Walk	4.68	57.49
0+22		
N	6.40	55.8
cb.	6.6	
1/2	6.6	
1/2	6.3	55.9
1/2	6.3	
cb.	5.8	
S	5.7	56.5
0+33 = 10' in st. olive tree on it ✓	7.3	54.9
0+48		
-5	8.3	
S	8.2	54.0
cb.	8.2	
1/4	7.6	

Plotted 9-7-28 - C.B.H.

2	8.0	54.2
1/4	8.4	
cb.	8.9	
N	9.5	52.7
+5	10.0	
0+85		
-5	13.0	
N	13.1	49.1
cb.	13.0	
1/4	11.6	
1/2	11.0	51.2
1/2	11.4	
cb.	12.5	
S	12.1	50.1
15	12.0	
TP 0.83	12.54	49.63
50.66		
1+20		
S-5	4.0	
S	4.0	46.5
cb.	2.7	
1/4	2.5	
1/2	2.7	47.8
1/4	3.5	
cb.	4.8	
14' at olive tree 8" dia. ✓	4.5	46.0
N	5.2	45.3

5046

1+27 = 2 olive trees on N 10' inst	6.4 ✓	44.1	8" dia.
+47 = " " " " " "	8.6 ✓	41.9	" "
+67 = " " " " " "	10.7 ✓	39.8	" "
1+30			
N	6.0	44.5	
cb.	6.0		
$\frac{1}{4}$	5.8		
$\frac{1}{2}$	5.4	45.1	
$\frac{1}{4}$	4.5		
cb.	4.8		
S	5.0	45.5	
+10	5.4		
1+45			
S	7.3	43.2	
cb.	7.2		
$\frac{1}{4}$	7.5		
$\frac{1}{2}$	7.7	42.8	
$\frac{1}{4}$	8.1		
cb.	8.0		
N	8.0	42.5	
1+78			
N	10.9	39.6	
cb.	10.6		
$\frac{1}{4}$	10.8		
$\frac{1}{2}$	11.0	39.5	
$\frac{1}{4}$	10.8		

5046

REDWOOD ST.
Y. SECTION

28

cb.	10.8	
S	11.1	39.4
		1+86
S	12.4	38.1
cb.	12.3	
$\frac{1}{4}$	12.3	
$\frac{1}{2}$	12.1	38.4
$\frac{1}{4}$	12.2	
cb.	11.2	
N	11.7	38.8
		2+00 = E.L. CALIFORNIA
N	13.1	37.4
cb.	13.1	
$\frac{1}{4}$	13.0	
$\frac{1}{2}$ on Con. Mon.	13.84	36.62
$\frac{1}{4}$	13.0	
+5	16.6	
+10	13.3	
cb.	13.7	
S	12.8	37.7

Note: For Cross Sections West of Calif. St.
See Book 1272-76

See Book
1272-12
For Chk.

Plotter
R.P. Johnson
Shaw
8-23-28

Cross Section Spruce st 80' wide
Bet. Kettner Blvd. & Col. St. 14' dbh
13' 1/2 S

5678

N.E. Bolt top depth	0.00	56.78	56.78
Kettner + Spruce	0.00	56.78	56.78
N top walk	5.02	51.76	
" " cb.	5.51	51.27	
" Gutter on Paring	6.19		
" 1/4 " "	5.27		
1/2 " "	4.76	52.02	
S 1/4 " "	4.63		
S Gut. " "	4.64		
S top cb.	4.03	52.75	
S " Split	3.57	53.21	
	0+10		
-10	8.5		
S	6.0	50.8	
+3	4.3		
cb.	4.6		
1/2	4.9		
1/4	5.0	51.8	
1/4	5.0		
cb.	5.2		
+5	5.7		
N	9.3	47.5	
+10	9.3		
	0+20		
-10	7.6		

Plotted 9-7-28
C.B.H.

N	9.5	47.3	29
+10	8.7		
cb.	6.2		
1/2	4.9		
1/4	4.8	52.0	
1/4	4.7		
cb.	4.2		
+5	3.8		
S	2.6	47.2	
+10	9.7		
	0+45		
-10	11.0		
S	11.0	45.7	
+10	5.3		
cb.	4.6		
1/4	5.1		
1/2	5.0	51.8	
+5	6.2		
1/4	10.8		
cb.	12.3		
N	12.0	44.8	
+10	12.3		
	0+55		
-10	12.8		
N	12.8	44.0	
cb.	12.8		

5678

1/2		130	
1/2		124	44.4
1/2		122	
cb.		120	
S		121	44.7
+10		121	
	0+95		
T.P.	066 4516	1228	44.50
-10		22	
S		22	43.0
cb.		30	
1/2		34	
1/2		34	41.8
1/2		37	
cb.		37	
N		37	41.5
+10		37	
	1+25		
-5		60	
N		60	39.2
cb.		48	
1/2		60	
+3		60	
1/2		78	37.4
+5		62	
1/2		60	

4516 SPRUCE ST.
X. Section

30

cb.		58	
S		47	40.5
+5		43	
	1+47		
S		67	38.5
cb.		74	
1/2		73	
+8		76	
1/2		97	35.5
+5		107	
1/2		76	
cb.		76	
N		80	37.2
	1+68		
N		90	36.2
cb.		90	
1/2		97	
+8		98	
1/2		120	33.2
1/2		87	
cb.		78	
S		73	37.9
	1+76		
S		100	35.2
+10		104	
cb.		117	

4516

Spruce st.
X. Section

1/4	14.3	
+10	15.0	
1/2	10.3	34.9
3/4	10.2	
cb.	10.2	
N	9.8	35.4
	1+83	
N	10.4	34.8
cb.	8.8	
1/4	9.6	
1/2	11.2	34.0
+5	14.7	
1/4	16.2	
cb.	12.7	
+2	8.4	
S	8.0	37.2
	1+89	
S	11.0	34.2
+10	11.6	
cb.	12.8	
1/4	16.9	
+5	15.6	
1/2	14.3	30.9
+10	14.2	
1/4	12.3	
+7	9.9	

4516

Spruce st.
X. Section 31

cb	9.5	
N	10.2	35.0
	1+95	
N	9.7	35.4
cb	9.5	
1/4	14.2	
1/2	15.0	30.2
1/4	17.2	
cb.	14.6	
+4	10.5	
S	8.0	37.2
	2+00 = E.L. CALIFORNIA	
S	9.9	35.9
+5	9.6	
cb.	15.3	
1/4	17.5	
1/2	14.6	30.6
1/4	14.4	
cb.	13.5	
N	11.1	34.1
TP	Spruce + California 3 Nails NE Pole	9.18
	35.98	

Note: For X Sections West of Calif st. See Book 1280-1

See Book
1272-21
for chs.

Walker
8-24-28

Cross Section SASSAFRAS ST 80' wide
Bet. Kettner + Col. St.
14' c/s
13' s/s

47.94
49.01

32

BM NE top Hydt.		50.23		43.96	
Thorne + Kettner	6.27	49.16		42.89 = this found wrong	
		49.01		48.26	
T.P.	0.75	47.94	1.97	47.19	
					on line
M.L. Kettner	= 0+00	= East Edge	Bld on N		
S top Walk		0.75		48.26	
" " cb.		1.41		47.60	
S Gut on Spring		2.10			
" 1/4 " "		2.08			
L " "		2.19		46.82	
N 1/2 " "		2.71			
N Gut " "		3.56			
N top cb.		2.86		46.15	
N " Walk		2.24		46.77	
	0+10				
N at Bld		4.3		44.7	
+4		4.2			
cb.		4.4			
1/4		3.5			
L		3.4		45.6	
1/4		3.2			
cb.		3.3			
+3		4.8			
+6		3.6			
S		4.5		44.5	
+10		4.4			

Plotted 9-7-28 - C.B.H.

0+50 = West edge Above Bld.

Note: Above Bld.

-10		8.2			
S		8.7			40.3
cb.		8.9			
1/4		9.0			
L		9.1			39.9
1/4		9.7			
cb.		10.2			
N at Bld		9.6			39.4
					33.71 outer edge 15' 4" in St.
0+90 = Gas Pump					on line on North
					R = 15.30
					1+00 = 1/2 M.H. in 2 SASSAFRAS ST
					36.54
					36.03
					35.47 12.98
T.P. 0.51					34.96
-5		4.4			
N		4.0			32.5
cb.		3.7			
1/4		3.4			
L on Rim M.H.		2.41			34.13
1/4		2.4			
cb.		1.4			
S		1.1			35.4
+10		1.1			
					R = 5.4
1+11 = East edge					36.00 311
					Plaining Mill Bld. on North on line. Master floor
1+37 = 1/2 Door way					Above Bld.
-10		5.5			
S		5.0			31.5
cb.		4.9			

3547
36.54

$\frac{1}{4}$	4.9	
$\frac{1}{2}$	5.0	31.5
$\frac{1}{4}$	5.4	
cb	5.4	
N = on floor 2 doorway	5.41	31.13
	✓ 1+65 = West edge Phinney Mill Bld.	
N = of BH	6.6	29.9
cb.	6.3	
$\frac{1}{4}$	6.1	
$\frac{1}{2}$	5.4	31.1
$\frac{1}{4}$	5.4	
cb.	5.8	
S	6.4	30.1
	1+75	
-10	7.5	
S	7.4	29.1
cb.	7.2	
$\frac{1}{4}$	5.6	
$\frac{1}{2}$	6.0	30.5
$\frac{1}{4}$	7.0	
cb.	7.0	
N	6.7	29.8
	1+86	
-10	9.2	
N	8.8	27.7
cb.	8.0	

Wooden
Floor

SASSAFRAS ST,
X. Section

3547
36.54

33

$\frac{1}{4}$	8.0	
$\frac{1}{2}$	8.3	28.2
$\frac{1}{4}$	9.0	
cb.	8.5	
S	8.1	28.4
+10	8.2	
	1+94	
-10	9.1	
S	9.2	27.3
cb.	9.4	
$\frac{1}{4}$	9.7	
$\frac{1}{2}$	10.5	26.0
$\frac{1}{4}$	10.1	
cb.	10.3	
N	10.8	25.7
+5	10.9	
	2+00 = E.L. CALIFORNIA	
N	10.7	25.8
cb.	10.5	
$\frac{1}{4}$	10.5	
$\frac{1}{2}$	10.6	25.9
$\frac{1}{4}$	10.2	
cb.	9.7	
S	9.4	27.1
T.P. SE. SPK. SASSAFRAS & Cal.	7.36	29.18 For chk. 28.11 See Book 1272-27

Note: For X. Sections West of Calif. See Book 1280-5

Cross Section THORNE ST. 80' wide
Bet. Kettner Blvd & Calif. St.

43.11
44.18

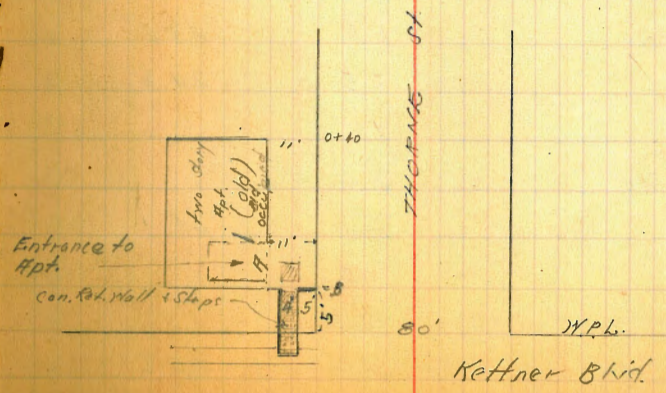
34

Walker
Rud. 11/11/11
S. 8-28-28

Top of top of Apt.	44.18	43.96
Thorne & Kettner 0.22	43.71	42.89 = THIS B.M. X 100%
W. Kettner = 0+00		
N Top Walk	3.50	40.68
" " cb.	4.18	40.00
" Gut. on Paring	4.67	39.51
" " "	4.24	
" " "	3.77	40.41
S 1/4 " "	3.89	
S Gut " "	4.30	39.88
" top cb.	3.68	40.50
" " Walk	3.06	41.02
0+07 = Entrance to Apt. - A	8.70	35.48
0+05 = top con. Wall = B	3.09	41.09
0+05		
S = Start of Above Wall	9.0	35.2
+2	5.7	
cb.	6.0	
1/4	3.3	
1/2	3.7	40.5
1/4	4.0	
cb.	5.3	
N	7.2	37.0
+10	9.8	
+20	10.0	
0+14		

Plotted 9-7-28-
CBM

-25	13.3	
N	12.0	32.2
cb.	11.0	
1/4	8.0	
1/2	7.6	36.6
+12	7.3	
1/4	9.0	
+9	10.9	
cb.	10.9	
S	10.8	33.4
+11' = at Base of Apt.	11.3	32.9
2' back line		2' dia
0+17 = 2' back of tree on S	11.0	33.2 10' High.
T.P. 0.67	32.13	31.46
	31.06	30.39
0+10 = West edge Apt.	1.5	30.6
0+49		
-10	3.8	
S	3.6	29.5



31.06
32.13

cb.	4.3	
$\frac{1}{4}$	3.6	
2	3.6	28.5
$\frac{1}{4}$	2.6	
cb.	2.8	
N	2.8	29.3
+20	3.0	
	0+6.6	
-20	5.8	
N	7.0	25.1
cb.	6.2	
$\frac{1}{4}$	6.5	
2	6.1	26.0
$\frac{1}{4}$	6.2	
cb.	6.0	
S	5.3	26.8
+20	5.0	
0+79	= Garage on S dirt floor 36' Back	
-36 = 9+ Garage	6.6	25.5
S	7.5	24.6
cb.	7.6	
$\frac{1}{4}$	8.0	
2	8.0	24.1
$\frac{1}{4}$	8.4	
cb.	8.5	
N	8.5	23.6

31.06
32.13

THORNE ST.
X. Section

35

+20	8.8	
	1+02	
-20	10.5	
N	10.2	21.9
cb.	10.1	
$\frac{1}{4}$	10.0	
2	10.0	22.1
$\frac{1}{4}$	9.6	
cb.	8.9	
S	9.3	22.8
+25	8.7	
	1+27	
-25	11.7	
S	12.0	20.1
cb.	12.2	
$\frac{1}{4}$	12.2	
2	12.5	19.6
$\frac{1}{4}$	13.0	
cb.	13.3	
N	13.2	18.9
+25	12.5	
TP 266	22.61 21.54	19.95 18.88
	1+60	
-20	5.4	
N	5.3	16.3
cb.	5.1	

2154
2261

1/2	52	
1/4	6.0	16.6
1/4	6.2	
cb.	5.0	
S	5.1	17.5
+25	4.0	
		17.70
-25	6.8	
S	8.1	14.5
cb.	7.9	
1/4	7.6	
1/4	7.9	14.7
1/2	8.1	
cb.	8.4	
N	8.7	13.9
+25	9.0	
		17.95 = 8 MH in 2 Thorne st.
-25	11.0	
N	10.3	12.3
cb.	9.2	
1/4	8.7	
1/2 on Rim MH	7.70	14.91
1/4	8.2	
cb.	8.4	
S	8.1	14.5
+25	7.7	

2154
2261

THORNE ST
X. Section

36

2400 = E.L. CALIFORNIA

-25	5.7	
S	6.2	16.4
cb.	6.7	
1/2	7.2	
1/2 on Con. Mon.	8.58	14.03 12.96
1/4	6.6	See Book 1272-32 For chkt.
cb.	7.1	
N	8.0	14.6
+20	12.4	
+25	10.6	

Note: For X. Sections West of Calif. st. See Book 1286-8

Walker
8-24-28

Cross Section UPHS st. 80' wide
14' CBS
Bel. Kettner + CALIFORNIA st. 13' 1/2 S

43.59
44.66

37

8th N.E. Top Walk	44.66	43.96	
Thorne + Kettner 0.70	43.59	42.89 = this 8th N.W. corner	
ML Kettner Blvd. = 0+00			
S Top Walk	4.98	39.68	
" " cb	5.30	39.36	
" Gut. on Dr.	5.96	38.70	
" 1/2 " "	5.62	39.04	
1/2 " "	5.58	39.08	
N 1/4 " "	5.73	38.93	
N Gut " "	6.23	38.43	
N Top cb.	5.56	39.10	
N " Walk	5.21	39.45	
0+05			
-5	6.1	38.6	
N	6.0	38.7	
cb.	5.8	38.9	
1/4	5.8	38.9	
1/2	6.2	38.5	
1/4	6.4	38.3	
cb.	7.0	37.7	
S	7.3	37.4	
+10	8.1	36.6	
0+50			
-10	12.0	32.7	
S	11.2	33.5	
cb.	11.2	33.5	

Plotted 9-7-28
C.B.H.

1/4	11.0	33.7
1/2	11.0	33.6
1/4	10.0	34.7
cb.	10.0	34.7
N	10.3	34.4
+5	10.2	34.5
0+78		
T.P. 179	33.81 32.74	32.02 30.95
12.64		
-5	2.5	31.3
N	2.6	31.2
cb.	2.0	31.8
1/4	1.9	31.9
1/2	2.5	31.9
1/4	2.7	31.1
cb.	3.2	30.6
S	3.6	30.2
+10	3.6	30.2
0+89		
-10	4.9	28.9
S	4.9	28.9
cb.	4.1	29.7
1/4	4.0	29.8
1/2	3.5	30.3
1/4	3.8	30.0
cb.	3.1	30.7
N	2.8	31.0
+5	2.8	31.0

3274
3381

0+96 = Garage on South dirt floor.

-10	5.7	28.1
N	5.6	28.2
cb.	4.8	29.0
$\frac{1}{4}$	4.7	29.1
$\frac{1}{2}$	4.1	29.7
$\frac{3}{4}$	4.6	29.2
cb.	4.5	29.3
S = 9 + Garage	5.2	28.6

1+00 = West edge Above Garage = East edge Garage below

S of Garages	5.2	28.6
cb	5.3	28.5
$\frac{1}{4}$	5.2	28.6
$\frac{1}{2}$	4.7	29.1
$\frac{3}{4}$	5.2	28.6
cb.	5.4	28.4
N.	5.3	28.5
+5	5.4	28.4

1+10 = West edge Above Garage

1+17	5.6	28.7
-10	7.1	26.7
N	7.0	26.8
cb.	6.6	27.2
$\frac{1}{4}$	6.4	27.4
$\frac{1}{2}$	5.5	28.3
$\frac{3}{4}$	5.5	28.3

3274
3381

Lipas st.
X. Section

38

cb.	6.4	27.4
S	6.2	27.6
1+36		
S	8.8	25.0
cb.	8.6	25.2
$\frac{1}{4}$	7.8	26.0
$\frac{1}{2}$	7.4	26.4
$\frac{3}{4}$	7.5	26.3
cb.	8.7	25.1
N	9.2	24.6
+10	8.3	25.5
1+50		
-10	10.3	23.5
N	10.1	23.7
cb.	9.0	24.8
$\frac{1}{4}$	9.5	24.3
$\frac{1}{2}$	9.3	24.5
$\frac{3}{4}$	9.3	24.5
cb.	9.3	24.5
S.	9.4	24.4
+10	9.2	24.6
1+62		
-10	9.7	24.1
S	9.7	24.1
cb.	9.9	23.9
$\frac{1}{4}$	9.7	24.1

2274
3381

L	10.0	23.8
$\frac{1}{4}$	9.7	24.1
cb.	9.7	24.1
N	10.3	23.5
+10	11.0	22.8
	1+87	
-10	13.3	20.5
N	12.9	20.9
cb.	12.5	21.3
$\frac{1}{4}$	12.7	21.6
L	12.0	21.8
$\frac{1}{4}$	11.4	22.4
cb.	11.6	22.2
S	11.6	22.2
+10	11.5	22.3
TP	5.80	27.25 26.18
	1+95	
-10	9.5	17.7
S	9.2	18.1
cb.	9.0	18.2
$\frac{1}{4}$	8.7	18.5
L	8.6	18.7
$\frac{1}{4}$	8.6	18.6
cb.	8.5	18.7
N	8.8	18.5
+10	8.5	18.7

2618
27.25

Upos st.
X Section

39

	2+00	
-10	8.7	18.5
N	8.7	18.6
cb.	8.8	18.4
$\frac{1}{4}$	9.0	18.2
$\frac{1}{4}$ on Ground	9.0	18.2
$\frac{1}{4}$ on Can. Mon.	10.02	17.23
$\frac{1}{4}$	9.2	18.0
cb.	9.3	17.9
S	9.4	17.9
+10	9.6	17.6

18.2 For chik. see
Book 1272-38

Walker
8-24-28

Cross Section VINE ST. 80' wide
Bet Kettner & Calif. St. 14' chs
13' as.

40-38
41.45

40

NE. BM. top Hctt. 44.36
Thorne & Kettner 0.40 42.29
VINE + Kettner 41.45
T.P. on NET' hctt 1.39 40.38

43.96
42.89 = this BM. wrong
40.06
38.99

M.L. KETTNER BLVD. = 0+00

N top Walk 2.68 38.77
" " cb. 3.07 38.38
" Gut. on Pav. 3.75 37.70
" 1/4 " " 3.43 38.02
" 1/2 " " 3.37 38.08
S 1/4 " " 3.56 37.89
S Gut " 4.21 37.24
S top cb. 3.23 38.22
S " Walk 2.96 38.49

0+05

S 3.2 38.2
cb. 3.6 37.8
1/2 3.4 38.0
1/2 3.5 38.0
1/2 3.5 37.9
cb. 3.2 38.2
N 2.8 38.7
N 3.1 38.4
cb. 3.3 38.1
1/4 3.5 37.9
1/2 3.6 37.9

0+13 = End Drain on South

0+13 = 1/2 DIRT DR. to oil Pumps on N

1/2 38 37.6
-10 38 37.6
cb 37 35.7
+3 = Flow Line 16" Con Pipe 7.7 33.7
+13 9.5 31.9
5 6.0 35.5
+10 7.8 33.6
-10 8.3 33.1
-5 9.8 31.6
S 9.0 32.5
+11 on Flow drain 8.4 33.1
cb. 4.6 36.8
1/2 4.6 36.8
1/2 4.0 37.5
1/2 3.5 37.9
cb. 3.6 37.8
N = Level with oil station Drive 3.2 38.3
0+23
N 3.2 38.3
cb. 3.6 37.8
1/2 3.5 37.9
1/2 4.0 37.5
1/2 4.6 36.8
cb. 4.6 36.8
S 5.9 35.6

0+21 = End Drain

Note: bet 0+13 + 0+21
Section 112 DRAIN IS GONE

Plotted 9-8-28 - CBH

4038
41.45

+5	9.9	31.5
+10	8.4	33.0
-10	7.8	33.6
5	6.1	35.4
cb.	5.8	35.6
$\frac{1}{4}$	5.0	36.4
$\frac{1}{2}$	5.0	36.5
$\frac{1}{4}$	4.4	37.0
cb.	4.1	37.3
N	3.5	38.0
0+50		
N	4.1	37.4
cb.	4.4	37.0
$\frac{1}{4}$	4.8	36.6
$\frac{1}{2}$	5.8	35.7
$\frac{1}{4}$	6.1	35.3
cb.	6.4	35.0
5	6.9	34.6
+5	7.2	34.2
0+68		
-10	8.9	32.5
5	9.3	32.2
cb.	10.3	31.1
$\frac{1}{4}$	7.8	33.6
$\frac{1}{2}$	7.0	34.4

0+39 = $\frac{1}{2}$ Dirt Dr. to oil Pump in N

4038
41.45

VINE ST
X. Section 41

$\frac{1}{2}$	7.1	34.4
+5	5.4	34.3
+10	6.7	34.7
$\frac{1}{2}$	6.6	34.8
cb.	4.6	36.8
N	4.5	37.0
0+77		
N	4.7	36.8
+5	4.9	36.5
cb.	7.5	33.9
+7	9.0	32.4
$\frac{1}{4}$	7.7	33.7
+3	7.3	34.1
+5	6.2	35.2
+10	7.3	34.1
$\frac{1}{2}$	7.3	34.2
$\frac{1}{2}$	7.4	34.0
cb.	7.4	34.0
5	9.0	32.5
+10	9.0	32.4
1+00		
-10	12.2	29.2
5	10.3	31.2
cb.	9.0	32.4
$\frac{1}{4}$	8.1	32.7
+5	8.6	32.8

4038
41.45

+10	7.2	34.2
L	8.8	32.7
+3	8.1	33.3
+5	9.4	32.0
$\frac{1}{4}$	9.5	31.9
+4	10.0	31.4
+6	12.9	28.5
+8	9.6	31.8
cb.	9.6	31.8
+8.	9.2	32.2
N	6.6	34.9
	1401	
N	6.6	34.9
+6	9.2	32.2
cb	9.6	31.8
+5	9.6	31.8
+7	12.9	28.5
+9	10.0	31.4
$\frac{1}{2}$	9.5	31.9
+8	9.4	32.0
+10	8.1	33.3
L	8.8	32.7
+3	7.2	34.2
+5	8.6	32.8
$\frac{1}{4}$	8.7	32.7
+6	8.7	32.7

4038
41.45

VINE ST.
X. Section

42

+7	13.0	28.4
+12	13.0	28.4
cb.	9.0	32.4
S	10.3	31.2
+10	12.7	29.2
	1718	
-10	12.7	29.2
S	11.0	30.5
+1	13.7	27.7
cb.	13.7	28.2
+3	10.0	31.4
$\frac{1}{4}$	10.0	31.4
+7	9.8	31.6
+9	8.5	32.9
L	9.4	32.1
+3	9.1	32.3
+4	10.7	30.7
$\frac{1}{4}$	10.5	30.9
+3	11.1	30.3
+4	11.3	27.1
+7	11.0	30.4
cb.	10.5	30.9
+12	10.1	30.6
N	9.7	31.8
+5	7.3	34.1
	1729	
	1+29	

40.38
41.45

-10	11.4	30.0
N	12.2	29.3
cb.	11.2	30.2
+7	11.4	30.0
+8	14.1	27.3
+10	11.5	29.9
1/4	11.1	30.3
+8	11.4	30.0
+10	9.9	31.5
1/2	10.4	31.1
+3	9.2	32.2
+5	10.6	30.8
1/4	10.9	30.5
cb.	11.2	30.2
+10	11.3	30.1
+11	14.1	27.3
S	13.8	27.7
+10	12.3	29.1
T.P.	149	29.59
		28.52
	1750	
-10	3.7	27.4
S	3.0	28.1
cb.	2.0	29.1
1/2	1.8	29.3
+5	1.5	29.6
+7	0.0	31.1

3001
3108

VINE ST.
X. Section 43

+9	14	29.7
1/2	1.8	29.3
1/4	1.8	29.3
+3	1.9	29.2
+1	4.3	26.8
+7	1.9	29.2
cb.	1.9	29.2
+10	2.5	28.6
N	3.4	27.7
+5	3.4	27.7
	2+00 - E. L. Calif. St.	
-10	5.7	25.4
N	5.4	25.7
cb.	5.1	26.0
+6	5.2	25.9
+8	6.8	24.3
+10	4.8	26.3
1/2	4.7	26.4
1/4	4.6	26.5
1/4	5.0	26.1
cb.	4.6	26.5
S	7.7	23.9
+5	7.6	23.5
	3/2 col. & S 1/2 Vine St	
	T.P. 3 Nails IN TEL. Pole	
	670	24.38 For chh. See
		23.71 Book 1272-43
	Note: For X. Sections West Calif. St. See Book 1280-10	

Walker
8-28-28

Cross Section WALNUT ST
bet. Kettner Blvd. and Calif. St.
80' wide
14' cbs
13' 7/8

42.06
43.13

44

BNE 7' hach.
Page 80

3.07, 43.13, 40.06, 38.99

on line

0+00 Kettner Blvd - East edge Blvd on North

s top walk	2.86	40.27
" " cb	3.06	40.07
" Gut on Pav.	3.70	39.43
" 1/4 " "	3.00	
" 1/2 " "	2.64	40.49
" 3/4 " "	2.57	
" Gut "	2.81	40.32
N top cb	2.08	41.05
" " Walk	2.0 ±	41.1

cb	4.8	
1/4	4.2	
1/2	4.5	38.6
3/4	4.4	
cb	4.2	
N-at Bld.	4.0	
0+40 = East edge Blvd. on North		39.1
N-at Bld. on Ground	5.6	37.5
cb	5.6	
1/4	5.5	
1/2	5.7	37.4
3/4	5.3	

Con. Floor
Planing Mill

Plotted 38-28 - CB.H.

0+05

N	2.2	40.9
cb	2.8	
1/4	3.2	
1/2	3.4	39.7
3/4	3.0	
cb	3.6	
+8	4.5	
S	6.3	36.8
+10	6.8	

cb	5.4	
+8	5.8	
S	7.7	35.4
+10	8.1	

0+62 = 12' Doorway Above Blvd. on N

0+20 = West edge Above Blvd. on N on Line		
-10	7.4	
S	7.7	35.9
+6	9.4	

-10	9.3	
S	9.2	33.9
+6	7.4	
cb	6.3	
1/2	6.3	
1/4	7.0	36.1
1/2	6.8	
cb	6.9	
+8	6.8	

4206
43.13

N on Con. Floor Planing Mill 7.70 35.43

0+84 = $\frac{1}{2}$ Doorway #2 on N 8.00 35.2 on bill

1+00 = West edge Above Bld

H of Bld. on Ground. ✓ 9.0 34.1

cb. 9.3

$\frac{1}{4}$ 9.2

$\frac{1}{2}$ 8.2 34.9

$\frac{1}{4}$ 8.8

cb. 9.5

S 10.7 32.4

+10 11.0

1+05

-10 10.5

S 10.5 32.6

cb. 9.6

$\frac{1}{4}$ 9.2

$\frac{1}{2}$ 8.8 34.3

$\frac{1}{4}$ 9.2

cb. 9.8

N 9.9 33.2

1+25

N 10.7 32.4

cb. 10.6

$\frac{1}{4}$ 10.5

$\frac{1}{2}$ 10.4 32.7

4206
43.13

WALNUT ST.
Cross Sections

45

$\frac{1}{4}$ 10.0

cb. 10.3

S 11.8 31.3

+10 11.7

TP. 2.59 34.77 33.70 10.95 34.18 34.11

1+53

-10 5.0

S 5.5 29.3

cb. 4.1

$\frac{1}{4}$ 3.6

$\frac{1}{2}$ 3.5 31.3

$\frac{1}{4}$ 3.9

cb. 2.9

N 2.8 32.0

2+00 = E.L. CALIFORNIA

N 5.9 28.9

cb. 6.0

$\frac{1}{4}$ 6.4

$\frac{1}{2}$ 6.7 28.1

$\frac{1}{4}$ 6.4

cb. 6.6

S 6.9

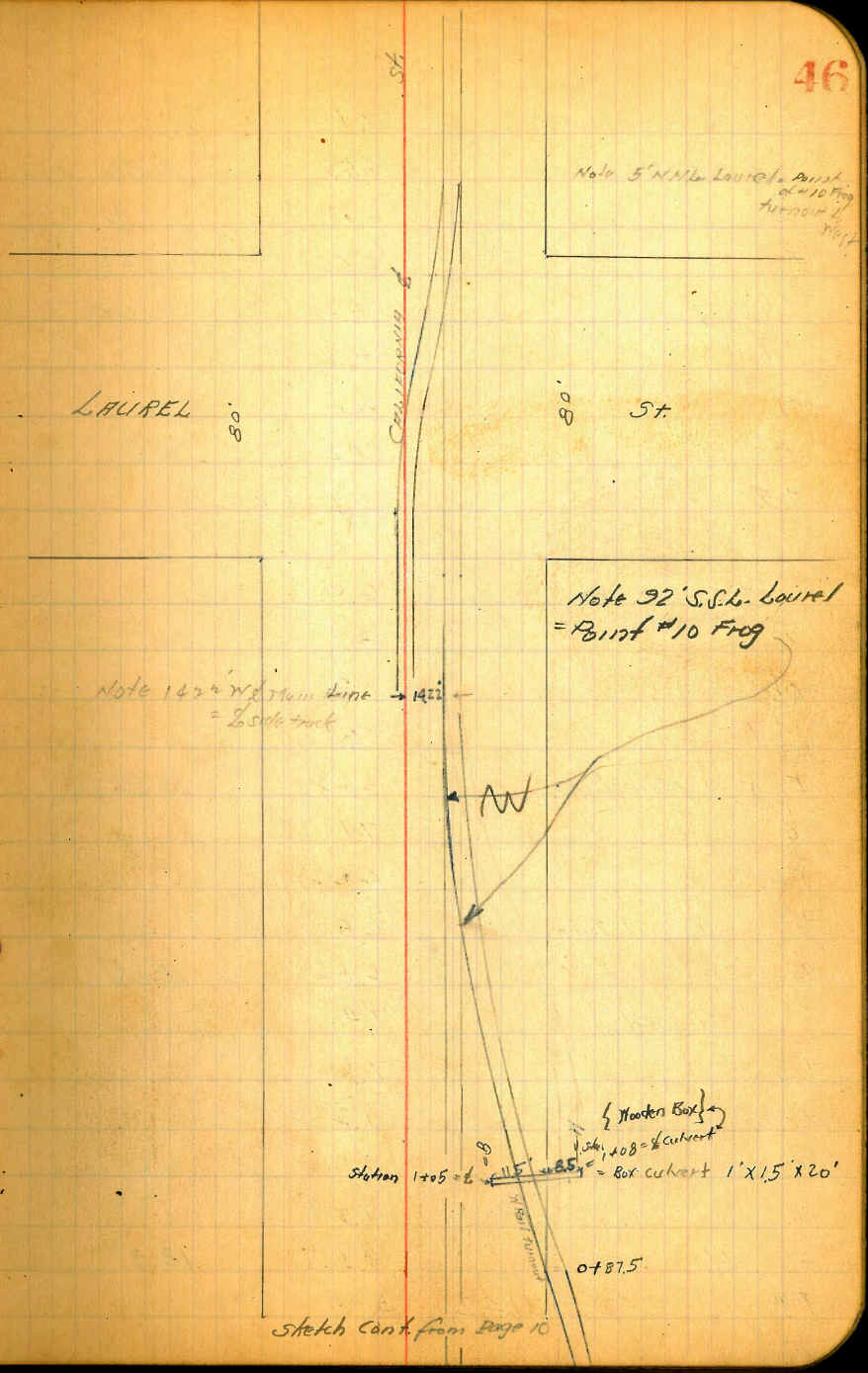
TP. on Con Mon $\frac{1}{2}$ Walnut And 25' West of East Line Calif. 8.38 26.39 27.9 For ch. see Book 1272+46

Walker
8-24-28

CALIFORNIA St. X. Sections
Cont. from Page 10

75' wide
12' cbs.
12.75' x 5

E	22.12	67	15.4
+5		5.6	
		R = 8.60	13.52
0+88 = End side track at R. & track = 131.5' W of St.			
	1+00		
-5		6.3	
E		7.1	15.0
cb		7.5	
+7		7.0	
E Rail		6.37	15.75
$\frac{1}{4}$		6.9	
W top Rail		6.36	15.76
+6		7.0	
+10		7.9	
$\frac{1}{4}$		8.3	13.8
$\frac{1}{4}$		8.7	
cb.		8.4	
W + 1 = Lumber shed		8.8	13.3
	1+50		
W - 4' = Lumber shed on ground		8.5	
W		8.5	13.6
cb.		8.6	
$\frac{1}{4}$		8.7	
+3 on West Rail of side track		7.78	14.34
" " "		7.83	
$\frac{1}{4}$		8.3	13.8
+3		8.3	



Note 5' N.N.W. Laurel Point of #10 Frog turned right

Note 92' S. S. Ch. Laurel = Point #10 Frog

Note 142' W of main line = 1/2 side track

Station 1+05 = 1+85 = Box culvert 1' x 1.5' x 20'

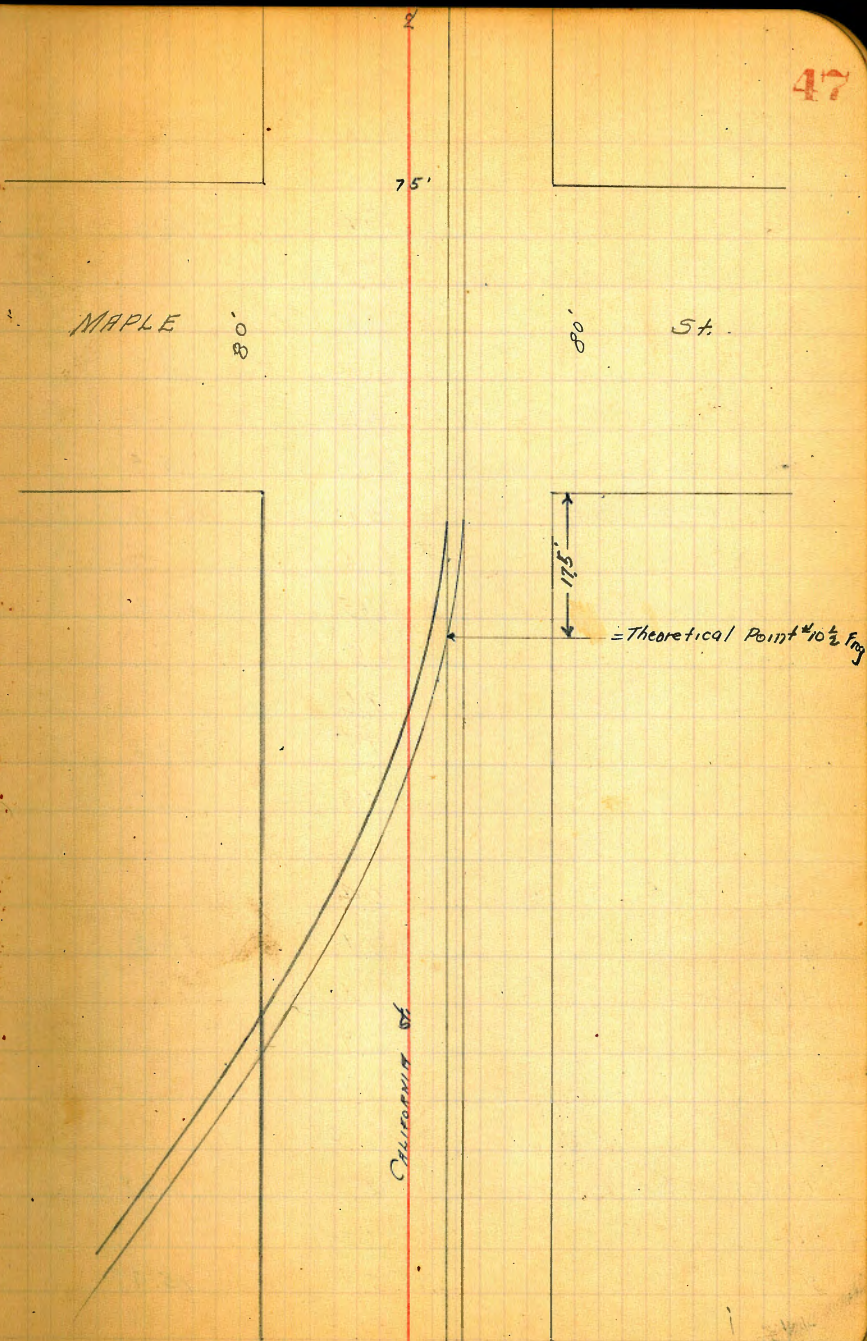
Sketch cont. from Page 10

22.12

CALIFORNIA ST.
X. Section

47

+7		7.1	
West. Rail Main Line		6.53	15.59
$\frac{1}{4}$		6.98	
E " " "		6.53	15.59
+6		7.2	
+9		7.6	
cb.		8.0	
E		7.2	14.9
+5		5.9	
	2+00		
-5		6.0	
E		8.0	14.1
cb.		8.3	
+7		7.1	
E Rail Main Line		6.62	15.50
$\frac{1}{4}$		7.1	
W " " "		6.62	15.50
+8 on E Rail Turnout		6.80	
$\frac{1}{2}$ " " "		6.86	15.26
" on Ground		7.4	
+3		7.6	
+8		9.2	
$\frac{1}{4}$		9.1	
cb.		9.2	
X = Bld.		8.9	13.3
TP	4.42 21.42	5.12	17.00

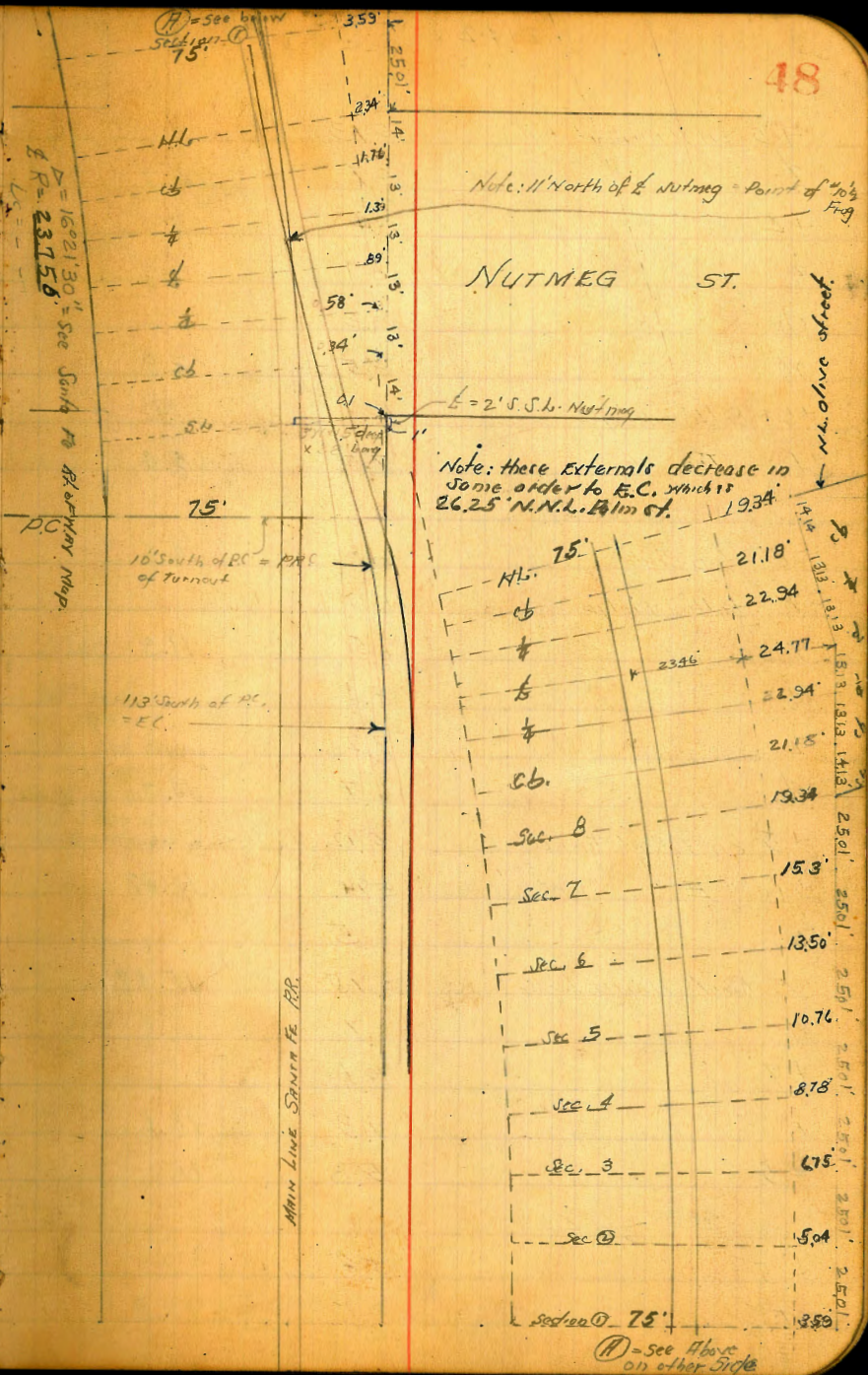


2142

CALIFORNIA ST.
X Section

2118

-5	7.4	
X	7.4	14.0
cb	6.8	
$\frac{1}{4}$	7.0	
L	6.5	14.9
+3 LOP Rail	5.95	15.47
+8 "E Rail	5.90	15.52
+10 = X Rail Main Line	5.93	15.49
$\frac{1}{2}$	6.4	
E Rail main Line	5.93	15.49
$\frac{1}{4}$ +6	6.5	
cb	7.6	
L	7.9	13.5
+5	4.8	
2432		
-5	5.4	
L	9.1	12.3
+5	9.6	
+6	7.9	
cb	7.3	
+7	6.4	
E Rail Main Line	5.95	15.47
$\frac{1}{4}$	6.4	
X " " "	5.95	15.47
+1 " East on turnout Rail	5.93	



+5 on X turnout Rail	593	
6	67	14.7
+4	84	
7	87	
cb	88	
X	85	12.9
+6 = Bottom Bridge	10.1	
+7 = Top "	7.0	14.4

2+37

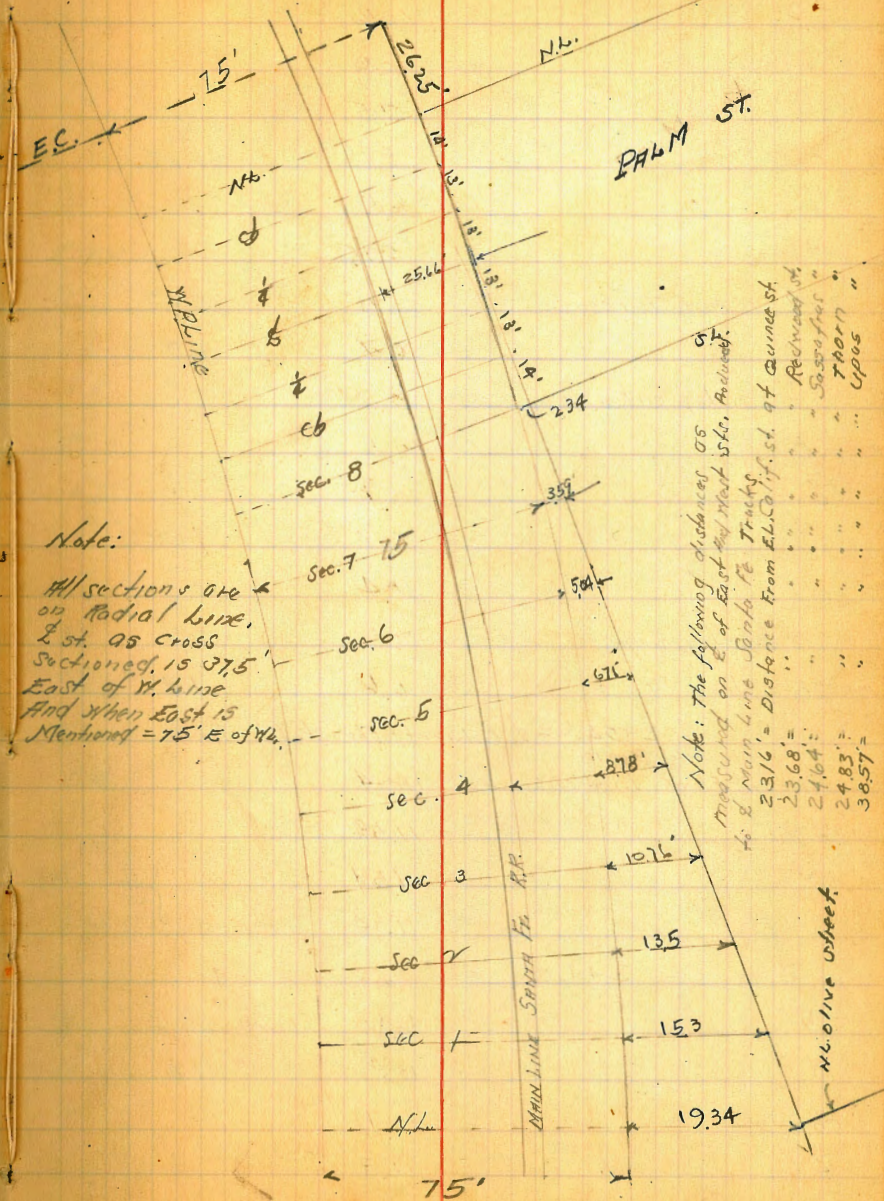
- 8' = top Bridge	6.8	14.6
- 8 = Bottom Bridge	11.0	
X	9.5	11.9
cb	8.1	
7	7.2	
6	6.7	14.7

+5 on X Rail turnout	592	
+10 " E " = Frog = X Rail Main line	595	15.47
7	6.5	
E Rail drain Line	595	15.47
cb	6.7	
7	8.1	
E	9.3	12.1
+5	5.8	

2+48

- 5	5.4	
E	8.5	12.9

CALIFORNIA ST.
Cross Section



2142

+2	10.6	
+6	9.0	
cb.	7.5	
E Rail main line	595	1547
$\frac{1}{2}$	6.5	
N " " "	595	
$\frac{1}{2}$ +7 = N Rail Turnout	595	1547
$\frac{1}{2}$	6.7	14.1
+3 on top culvert	8.0	
+8	10.5	
$\frac{1}{2}$	10.9	
cb	11.1	
N	11.4	10.0
+8 = Bottom Bridge	11.8	
+8 = top "	6.6	14.8
2+54.6 = $\frac{1}{2}$ culvert see sketch P-10 see sketch Page 10		
B - on Flood Line culvert	11.64	
C = " " " "	11.56	
D = " " " "	9.57	
E = " " " "	9.24	
2+60		
-5	6.9	
N	10.4	11.0
cb.	10.7	
$\frac{1}{2}$	11.3	
+5	7.6	

2142

CALIFORNIA ST.
Cross Sections 50

+10	7.9	
$\frac{1}{2}$	6.5	14.9
$\frac{1}{2}$ +7 on Rail turnout	5.91	
N Mainline Rail	592	15.50
$\frac{1}{2}$	6.5	
E main " "	595	15.47
+10	7.5	
cb	18.3	
+3	10.5	
E	10.2	11.2
+5	6.5	
2+63		
5	5.6	
E	9.2	12.2
+8	10.1	
cb.	6.9	
E Rail M Line	596	15.46
$\frac{1}{2}$	6.4	
N " " "	593	15.49
$\frac{1}{2}$ +6 N Rail turnout	592	15.50
$\frac{1}{2}$	6.6	14.8
$\frac{1}{2}$	7.2	
cb.	8.1	
N	7.0	14.4
+5	6.9	
2+70		

} Sta. = 2+59

2142

-5	7.4	
N	7.4	14.0
cb.	8.5	
$\frac{1}{4}$	8.0	
$\frac{1}{2}$	6.8	14.6
+7 on W Rail Turnout	5.89	
" " " " " " " " " " " "	5.93	15.49
$\frac{1}{2}$	6.4	
E " " "	5.94	15.48
$\frac{1}{4}+10$	6.8	
cb.	9.4	
E	8.0	13.4
+5	4.7	

2+75

-5	5.1	
E	8.1	13.3
cb.	8.1	
$\frac{1}{4}$	6.4	
+9	6.5	
$\frac{1}{4}$	8.5	12.9
$\frac{1}{2}$	9.6	
cb.	8.5	
N	7.6	13.8
+5	6.7	

3+00. 37 = S.W. Kalmia 14' cbs 13' 25

-5 7.0

2142

CALIFORNIA ST.
X. Section

51

N	7.2	14.2
cb.	7.0	
$\frac{1}{4}$	8.2	
$\frac{1}{2}$	8.5	12.9
+5	6.4	
+9 on W Rail Turnout	5.90	
" " " " " " " " " " " "	5.90	15.52
$\frac{1}{4}$	6.4	
" E " "	5.90	15.52
$\frac{1}{4}+5$	6.5	
+10	7.6	
cb.	7.9	
+4	8.3	
E	6.7	14.7
+5	5.3	
S. cb. Kalmia		
-5	5.3	
E	6.8	14.6
+7	8.4	
cb.	7.3	
+5	7.2	
+8	6.5	
$\frac{1}{2}$	6.4	
$\frac{1}{4}$	6.4	15.0
$\frac{1}{4}$	7.0	
cb.	7.1	

2142

W	7.0	14.4
+5	6.7	
	5.93	
S cb. + 7' = Σ upright switch		
S $\frac{1}{4}$		
-5	6.1	
W	6.1	15.3
cb.	5.9	
$\frac{1}{4}$	5.3	
+7	5.2	
Σ	6.2	15.2
$\frac{1}{4}$	6.4	
+5	6.4	
+7	7.0	
cb.	8.0	
E	6.3	15.1
+5	4.6	
Σ		
-5	4.9	
E	6.4	15.0
cb.	8.0	
+6	7.1	
+8	6.4	
on E Rail Main Line	5.92	15.50
$\frac{1}{4}$	6.5	
W " " "	5.94	15.48
$\frac{1}{4}$	6.1	15.3

2142

CALIF. ST.
Cross Section 52

+3	4.8	
$\frac{1}{4}$	4.7	
cb.	6.2	
W	5.7	15.7
+5	5.7	
N $\frac{1}{4}$		
-5	5.7	
W	5.0	16.4
cb.	5.0	
$\frac{1}{4}$	4.3	
+10	4.3	
Σ	5.2	16.2
+3	6.3	
$\frac{1}{4}$	6.5	
+5	6.5	
+7	7.3	
cb.	8.0	
E	6.4	15.0
+5	5.6	
N cb.		
-5	5.4	
E	6.2	15.2
cb.	8.0	
+8	6.5	
$\frac{1}{4}$	6.4	
Σ	6.3	15.1

1/2	4.8	
cb.	5.8	
W	6.2	15.2
+5	6.3	
N.L. KALMIA = 0+00		
-5	7.3	
W	7.3	14.1
+10	7.5	
+11	5.7	
cb.	5.7	
1/2	5.8	
+7	5.1	
E	7.9	13.5
+6	6.4	
on W Rail Main line		
1/4	5.7	15.45
	6.4	
" E " " "	5.95	15.57
1/4 +5	6.5	
+7	7.6	
cb.	8.0	
E	6.3	15.1
+5	5.2	
0-40		
-5	5.3	
E	6.2	15.2
cb.	7.8	

+4	7.3	
+7	6.7	
Main		
on Rail E line		
1/2	6.01	15.41
	6.5	
on W Rail M line		
1/2 +6	5.99	15.43
	6.5	
+10	7.4	
1/2	5.7	15.7
+7	5.3	
+9	6.9	
1/2	6.0	
cb.	7.2	
W	9.4	12.0
+5	9.6	
0+45		
-5	9.6	
W	9.4	13.0
cb.	9.0	
+2	7.3	
1/2	6.0	
+4	6.9	
+6	5.3	
1/2	5.7	15.7
+3	7.4	
+7	6.5	
1/2	6.5	

2142

+6	6.4	
+9	7.3	
cb.	7.8	
E	6.2	15.2
+5	5.3	

Notes: bet 0+40 & 75 bet. E. Cal. + N. Cal. there is 110 ft. Four
Concrete Piers 2.5' wide + base 1.5' at top by 5' out of ground. Old Bridge Piers
Also 3 Bridge Timbers 10" x 16" x 35' Also 3 timbers 12" x 12" x 12'

7 = 532

0+87.5 = Intersection N. Rail turnout N. Cal. E. Cal.

1+08

-8.5 = Flow line station 1+08 = 7.20 14.22

1+05

-5 6.1

-1 = top E Rail turnout 5.51

E 6.0 15.4

+4.72 " " " " 5.56 15.86

E + 11.5 = Flow Line ^{Page 41} see sketch = 7.47 13.95

cb. 7.5

+5 6.9

+7 6.4

E Rail Main line 5.99 15.43

$\frac{1}{4}$ 6.4

N " " " 5.95 15.47

$\frac{1}{2}$ +7 6.5

+10 7.4

$\frac{1}{2}$ 6.4 15.0

+8 6.1

2142

CALIFORNIA ST.
Cross Section 54

$\frac{1}{2}$	8.3	
cb.	8.6	
+3	9.4	
N	10.5	10.9
+10	10.7	

1+25 = E. Cal. Bld. on Line on Mud Sills

W = E. Cal. Bld on West 23' wide

W = at Bld on Ground 9.6 11.8

+9 9.2

+5 8.3

cb. 7.9

$\frac{1}{2}$ 5.5

+10 6.0

E " 7.5 13.9

+7 6.6

W Rail - M-Line 5.96 15.46

$\frac{1}{2}$ 6.4

E Rail - M-Line 5.97 15.45

$\frac{1}{2}$ +5 6.5

+8 7.0

cb. 6.8

+3 on W Rail turnout 5.71

+7.72 " " " 5.66

E 6.5 14.8

+5 6.7

2142

1+50

-5	5.6	
-1	5.8	
E	7.3	14.1
+9 on E Rail turnout	5.91	15.51
cb	6.4	
" " "	5.90	15.52
E Rail main line	5.98	15.44
$\frac{1}{4}$	6.40	
" " "	5.95	15.57
+6	6.6	
+10	7.4	
$\frac{1}{4}$	6.5	14.9
$\frac{1}{4}$	8.7	
cb	8.1	
W at Big	10.1	11.3

1+75

W " "	10.8	10.6
cb	9.6	
+1	10.2	
$\frac{1}{4}$	10.6	
+5	10.5	
$\frac{1}{4}$	7.2	14.2
W Rail Main line	5.96	15.46
$\frac{1}{4}$	6.5	
E " " "	5.97	15.45

2142

CALIF. ST.
Cross Section
55

+5 on W. Rail turnout	6.00	
+972 " E " "	6.03	
cb	6.5	
+4	6.7	
+7	7.1	
+9	5.6	
E	5.4	16.0
+5	5.6	
1+93 = South end turnout West of $\frac{1}{4}$		
-5	5.6	
E	5.7	15.7
+5	5.5	
+6	7.0	
+10	6.6	
cb	6.5	
+3 on E Rail turnout	5.98	
+772 " W " "	5.95	
E Rail Main line	5.95	15.47
$\frac{1}{4}$	6.4	
W " " "	5.92	15.50
+6	6.5	
+10	8.2	
$\frac{1}{4}$ on E Rail turnout	8.95	12.47
+4.71 W " "	8.85	
+8	10.4	
$\frac{1}{4}$	11.1	

2142

cb.		9.9	
W		10.2	11.2
+5		11.0	
+10		11.9	
T.P.	0.72	17.72	442
	1+95		1700
-15		13.2	
W		11.3	6.4
cb.		9.0	
$\frac{1}{4}$		7.3	
+8 on W Rail turnout		5.2	
$\frac{1}{4}$ " E " "		5.2	12.5
+8		2.8	
$\frac{1}{4}$		2.7	
cb.		2.8	
+4		3.5	
+6		1.8	
E		2.0	15.7
+5		2.0	
	2+50		
-5		2.4	
E		2.5	15.2
+8		2.3	
+10		3.2	
cb.		2.5	
+9 on E Rail turnout		2.09	

1772

CALIFORNIA ST.
Cross Section

56

on E Rail main line	209	
$\frac{1}{4}$	2.6	
on W " " "	209	15.63
$\frac{1}{4}+6$	2.8	
$\frac{1}{4}$ on E Rail turnout	480	1292
+471 W " "	485	
$\frac{1}{4}$	0.4	
+7	7.0	
cb.	9.6	
W	15.5	2.2
+10	16.8	
+20	19.3	
	2+60	
-20	18.7	
-10	18.2	
W	16.2	1.5
cb.	8.5	
+4	6.4	
$\frac{1}{4}$	5.7	
+8 on W R turnout	4.67	
$\frac{1}{4}$ " E " "	4.66	3.06
+2	4.3	
+6	3.7	
W Rail main line	2.10	15.62
$\frac{1}{4}$	3.6	
E " " "	2.07	15.65
$\frac{1}{4}+3$ E R turnout	2.07	

1772

cb.		3.0	14.7
L		2.2	15.5
+5		2.2	15.5
	2+80		
-5		2.5	15.2
E		2.5	15.2
cb.		2.4	15.3
$\frac{1}{4}$		2.6	15.1
+5		2.8	14.9
L		4.1	13.6
$\frac{1}{4}$		4.4	13.3
cb.		3.3	14.4
X		2.1	15.6
+20		3.1	14.6
	2+88 = Upright Switch 7.35' East of E Main track		
T.P	568 2268	0.72	17.00
	3+60.52 S.L. LAUREL ST 14' cbs 13' $\frac{1}{4}$ s		
X-5		8.0	14.7
X		8.3	14.4
cb.		8.2	14.5
$\frac{1}{4}$		8.4	14.3
+9 on West Rail Turnout		7.95	14.73
$\frac{1}{4}$		8.0	14.7
" " Main line		6.95	15.73
$\frac{1}{4}$		7.5	15.2
" E " " "		6.97	15.71

2268

CALIFORNIA ST

X. Section

57

cb.		7.1	15.6
E		7.1	15.6
	S ch Laurel		
E		6.9	15.8
cb.		7.2	15.5
$\frac{1}{4}$		7.3	15.4
+10 = E Rail Turnout		7.30	15.38
X " "		7.28	15.40
$\frac{1}{4}$		7.5	14.2
$\frac{1}{4}$		7.8	14.9
cb.		8.3	14.4
X		8.6	14.1
+5		8.1	14.3
	S $\frac{1}{4}$ LAUREL		
-5		9.5	14.2
X		8.5	14.2
cb.		8.3	14.4
$\frac{1}{4}$		7.9	14.8
+11 on X Rail Turnout		7.08	15.60
$\frac{1}{4}$		7.1	15.6
" E " " "		7.08	15.60
" X Rail Main Line		6.86	15.82
$\frac{1}{4}$		7.0	15.7
" E " " "		6.87	15.81
cb.		7.1	15.6
E		6.8	15.9

22.68

E Laurel

E	5.3	17.4
cb.	5.9	16.8
+3	7.5	15.2
$\frac{1}{4}$	7.3	15.4
+8 on E Rail turnout	7.00	15.68
" W " "	7.03	15.65
$\frac{1}{2}$	7.1	15.6
$\frac{1}{4}$	7.9	14.8
cb.	8.1	14.6
W	8.2	14.5
N $\frac{1}{2}$		
W	7.5	15.2
cb.	7.7	15.0
$\frac{1}{4}$	7.7	15.0
$\frac{1}{2}$	7.4	15.3
+2 on W Rail Turnout	6.96	15.72
" E " "	6.90	15.78
$\frac{1}{2}$	7.3	15.4
+10	7.4	15.3
cb.	5.5	17.2
E	5.0	17.7
N cb.		
E	4.9	17.8
+10	5.3	17.4
cb.	6.2	16.5

22.68

CALIFORNIA ST.
Cross Section

58

+2	7.4	15.3
$\frac{1}{4}$	7.2	15.5
+5 = E Rail turnout	6.75	15.93
" " "	6.79	15.89
$\frac{1}{2}$	7.3	14.4
$\frac{1}{4}$	7.6	15.1
cb.	7.7	15.0
W	7.5	15.2
N.L. LAUREL = 0+00		
W	7.5	15.2
cb.	7.7	15.0
$\frac{1}{2}$	7.4	15.3
$\frac{1}{2}$	7.4	15.3
+5 on W Rail turnout	6.66	16.02
" E " " = W Rail main line	6.71	15.97
$\frac{1}{4}$	7.2	15.5
+10	7.4	15.3
cb.	5.2	17.5
E	4.9	17.8
0+50		
E	5.0	17.7
+10	5.3	17.4
cb.	7.2	15.5
E Rail main line	6.57	16.11
$\frac{1}{4}$	7.0	15.7
W " " "	6.57	16.11

2268

+4 = W Rail turnout	6.50	16.18
$\frac{1}{2}$	7.2	15.5
$\frac{1}{2}$	7.2	15.5
cb.	7.5	15.2
W	9.6	13.1
+5	9.5	12.2
0+80		
-5	8.8	13.9
W	8.8	13.9
cb.	8.6	14.1
+5	5.8	16.9
$\frac{1}{4}$	6.5	16.2
$\frac{1}{2}$	6.8	15.9
on W Rail main line	6.44	16.24
$\frac{1}{2}$	7.0	15.7
"E" " "	6.44	16.24
$\frac{1}{2}+10$	7.0	15.7
cb.	5.3	17.4
E	5.0	17.7
0+85 = Upright switch & side main line		
E	5.0	17.7
cb.	4.8	17.9
+3	6.8	15.9
$\frac{1}{4}$	6.8	15.9
of switch.	6.9	15.8
$\frac{1}{2}$	7.1	15.6

2268

CALIF. ST.
Cross Section

59

$\frac{1}{2}$	7.1	15.6
cb.	8.9	13.8
W	8.6	14.1
+5	8.3	14.4
+6 on E Rail turnout	9.17	13.51
1+00		
-5 = W Rail turnout	9.14	13.54
W = E " "	8.87	13.81
cb.	8.8	13.9
$\frac{1}{4}$	7.7	15.0
$\frac{1}{2}$	7.4	15.3
W Rail main line	6.32	16.36
$\frac{1}{2}$	6.8	15.9
E " " "	6.30	16.38
$\frac{1}{2}+11$	6.8	15.9
cb.	4.8	17.9
E	5.0	17.7
1+40		
-10	4.8	17.9
E	4.7	18.0
cb.	5.0	17.7
+3	7.1	15.6
E Rail main line	6.07	16.61
$\frac{1}{4}$	6.6	16.1
W " " "	6.10	16.58
$\frac{1}{2}$	7.3	15.4

$\frac{1}{4}$	8.0	14.7
+10 = E Rail turnout	8.20	14.48
cb.	8.4	14.3
= M " "	8.40	14.28
M	8.7	14.0
+5	9.0	13.7
2+00		
-5	8.2	14.5
M	7.9	14.8
cb.	7.5	15.2
$\frac{1}{4}$	7.0	15.7
+3 on M Rail Turnout	6.77	15.91
" E " "	6.64	16.04
L	6.8	15.9
M Rail main line	5.70	16.98
$\frac{1}{4}$	6.2	16.5
E " " "	5.70	16.98
+10	6.5	16.2
cb.	5.2	17.5
+9	4.8	17.9
+9.2	1.1	21.6
E	1.3	21.4
+10	1.3	21.4
+10.2	4.4	18.3
2+02		
E -0.5 = M Rail turnout	4.92	17.76

cb.	5.2	17.5
+3	6.6	16.1
$\frac{1}{4}$	6.2	16.5
L	6.8	15.7
$\frac{1}{2}$	7.0	15.7
cb.	7.5	15.2
M	7.7	14.0
-5	8.0	14.7
2+50		
-5	6.0	16.7
M	6.2	16.5
cb.	6.1	16.6
$\frac{1}{4}$	6.8	15.9
+10	6.8	15.9
L = M Rail turnout	5.43	17.25
E " "	5.37	17.31
M " main line	5.33	17.35
L	5.8	16.9
E " " "	5.30	17.38
$\frac{1}{4}+10$	6.3	16.4
cb.	4.8	17.9
E = top M Rail turnout	4.64	18.04
3+00.51 = St. MAPLE 14'cb. 13'45		
E = M Rail Turnout	4.32	18.36
+10	4.4	18.3
cb.	6.0	16.7

22.68

E Rail main line	4.94	17.74
$\frac{1}{2}$	5.5	17.2
+2 = E Rail Turnout	4.90	17.78
W " main line	4.94	17.74
" " Turnout	4.88	17.80
$\frac{1}{4}$	6.0	16.7
$\frac{1}{4}$	6.0	16.7
cb.	6.1	16.6
W	6.0	16.7
+5	6.4	16.3
South cb.		
-5	6.9	15.8
W	6.5	16.2
cb.	6.0	16.7
$\frac{1}{4}$	5.7	17.0
$\frac{1}{4}$	5.6	17.1
+8 = W Rail turnout	4.81	17.87
" " main line	4.86	17.82
$\frac{1}{4}$	5.3	17.4
E " " "	4.86	17.82
$\frac{1}{4}$ +10	5.8	16.9
cb.	4.7	18.0
E = W Rail Turnout	4.25	18.43
5 $\frac{1}{4}$		
E = W Rail Turnout	4.25	18.43
cb.	4.2	18.5

22.68

CALIF. ST.
Cross Section

61

+3	5.9	16.8	22.68 = K
$\frac{1}{2}$	5.3	17.4	+1.8 =
+4 = W Rail Turnout	4.72	17.96	18.50
$\frac{1}{4}$	5.5	17.2	18.56
$\frac{1}{4}$	5.4	17.3	0.06 = E10
cb.	5.8	16.9	
W	6.2	16.5	
+5	6.3	16.4	
			chk on BM Maple & Cal. Page 15
-5	6.6	16.1	
W	6.3	16.4	
cb.	6.0	16.7	
$\frac{1}{2}$	5.7	17.0	
$\frac{1}{4}$	5.3	17.4	
+9 = W Rail turnout	4.66	18.02	
$\frac{1}{4}$	5.1	17.6	
+10	5.6	17.1	
cb.	4.7	18.0	
E = W Rail Turnout.	4.19	18.49	
E = W Rail Turnout	4.16	18.52	
+10	4.6	18.1	
cb.	4.7	18.0	
+3	5.5	17.2	
$\frac{1}{4}$	5.2	17.5	
$\frac{1}{4}$	5.3	17.4	

MAPLE

2268

4	55	17.2
cb.	5.8	16.9
W	6.2	16.5
+5	5.8	16.9
	N.Cb.	
-5	6.2	16.5
W	6.0	16.7
cb.	5.8	16.9
1/2	5.3	17.4
1/4	5.0	17.7
+10	5.5	17.2
cb.	4.9	17.8
E = W Rail Turnout	4.05	18.63
	N. L. MARKS - 0+00	
E = W Rail main line	3.93	18.75
cb.	4.7	18.0
+3	5.5	17.2
E Rail main line	4.37	18.31
1/4	4.8	17.9
W " " "	4.38	18.30
1/2	5.1	17.6
1/4	5.4	17.3
cb.	5.9	16.8
W	5.9	16.8
+5	6.0	16.7

Note. 3' N.C. Maple = 1/2 upright. Switch Turnout to South West.
N.L. ?

2268

CALIF. ST.
CR 69. Section

69

0+150 = 1/2 Frame cement shed 9'x12'x9' high. 2 bid. = 22' East N.L.

-5	5.3	17.4
W	5.5	17.2
cb.	5.5	17.2
1/2	5.1	17.6
1/4	4.4	16.3
+7	5.2	17.5
+9	4.6	18.1
W Rail main line	4.00	18.18
1/4	4.5	18.2
E " " "	4.00	18.68
cb.	4.5	18.2
E = top W Rail Turnout	3.68	19.00
	1+00	
E = Top W Rail Turnout	3.04	19.64
cb.	3.6	19.1
+8	4.5	18.2
+9	4.0	18.7
E Rail N.L.	3.6	19.22
1/4	4.0	18.7
W " " "	3.16	19.22
1/4+7	4.0	18.7
+9	4.5	18.2
1/2	4.5	18.2
1/4	4.9	17.8
W	4.9	17.8
+5	4.9	17.8

22.68

7.P	11.20	30.04	3.84	18.84
	1+50			
-5			11.1	18.9
W			11.0	19.0
cb.			11.0	19.0
$\frac{1}{4}$			10.8	19.2
$\frac{1}{2}$			11.2	18.8
W Rail main Line			10.33	19.71
$\frac{1}{4}$			10.8	19.2
E " " "			10.28	19.76
cb.			10.9	19.1
E = top W Rail turnout			10.10	19.94
	2+00			
E			10.5	19.5
+1 = top W Rail			9.95	20.09
cb.			10.8	19.2
* E Rail main Line			9.78	20.26
$\frac{1}{4}$			10.3	19.7
W " " "			9.79	20.25
$\frac{1}{4} + 7$			10.4	19.6
+9			11.0	19.0
$\frac{1}{2}$			10.6	19.4
+8			12.1	17.9
$\frac{1}{2}$			11.9	18.1
cb.			10.8	19.2
W			11.6	18.4

3004

CALIFORNIA ST.
Cross Section

63

+5			11.6	18.4
	2+50			
-5			10.5	19.5
W			10.5	19.5
cb.			10.1	19.9
$\frac{1}{4}$			10.7	19.3
$\frac{1}{2}$			10.1	19.9
W Rail main Line			9.20	20.84
$\frac{1}{4}$			9.7	20.3
E " " "			9.14	20.90
cb.			10.3	19.7
+6 = W Rail turnout			9.18	20.86
E			9.8	20.2
+5			10.1	19.9
+10			12.6	17.4
+15			12.6	17.4
	2+74.21 = P.C.			
				was Per. Sketch Page 48 in Curve to E.C. 24.25' N.W. 1/4 P. 100
-15			12.6	17.4
-10			12.4	17.6
E			9.7	20.3
+6 = E Rail turnout			8.87	21.17
W " " "			8.90	21.14
cb.			9.7	20.3
E Rail main Line			8.85	21.19
$\frac{1}{4}$			9.4	20.6
W " " "			8.90	21.14

30.04

+7	9.4	20.6
$\frac{1}{4}$	11.0	19.0
$\frac{1}{4}$	10.8	19.2
cb.	10.6	19.4
X	10.9	19.1
+5	11.1	18.9
21.25' North of P.C.		
-5	11.3	18.7
X	11.1	18.9
cb.	11.2	18.8
$\frac{1}{4}$	11.6	18.4
+10	11.0	19.0
$\frac{1}{4}$	10.6	19.4
+5	9.3	20.7
X Rail main line	8.68	21.36
$\frac{1}{4}$	9.1	20.9
E " " "	8.62	21.42
$\frac{1}{4} + 10 = X$ Rail turnout	8.60	21.44
cb.	9.2	20.8
E Rail turnout	8.65	21.39
cb +5	9.2	20.8
E	11.7	18.3
	12.2	17.8
Note: 2' S.S. Nutmeg = 2 Box Culvert ✓		
E -1 = Flow line	13.59	16.45
E	11.7	18.3

30.04

CALIF. ST.
GROSS SECTION 64

+7	9.0	21.0
+10 = E Rail Turnout	8.62	21.42
cb.	9.14	20.90
X " " "	8.60	21.44
$\frac{1}{4}$	9.1	20.9
+7	9.4	20.6
$\frac{1}{4}$	11.3	18.7
+2	12.3	17.7
+3 on Flow Line = End of Exist. Culvert	14.09	15.95
$\frac{1}{4}$	13.6	16.4
cb.	14.0	16.0
X	14.0	16.0
+25 in ditch	13.5	16.5
S.S. Nutmeg sections on Radial line		
-10	11.8	18.2
X	11.2	18.8
cb.	10.9	19.1
$\frac{1}{4}$	11.4	18.6
$\frac{1}{4}$	11.0	19.0
+6	9.2	20.8
$\frac{1}{4}$	9.1	20.9
cb.	9.1	20.9
+5	9.1	20.9
E	11.2	18.8
5 cb.		
E	10.8	19.2

30.04

+5	10.5	19.5
+10	8.7	21.3
cb.	8.7	21.3
$\frac{1}{4}$	8.9	21.1
+6	9.0	21.0
$\frac{1}{2}$	11.1	18.9
+2	12.1	17.9
+5	10.4	19.6
$\frac{1}{4}$	10.8	19.2
cb.	10.9	19.1
$\frac{1}{2}$	11.1	18.9
+5	11.2	18.8

5 $\frac{1}{4}$

-5	10.6	19.4
$\frac{1}{2}$	10.4	19.6
cb.	10.4	19.6
$\frac{1}{4}$	10.2	19.8
+6	10.1	19.9
+10	12.2	17.8
$\frac{1}{2}$	11.4	18.6
+5	9.0	21.0
$\frac{1}{4}$	8.8	21.2
cb.	8.6	21.4
+3	9.7	20.3
E	9.8	20.2

 $\frac{1}{2}$

30.04

C#61F. St.
Cross Section 65

E	9.4	20.6
+5	8.9	21.1
+10	10.2	19.8
cb.	8.4	21.6
$\frac{1}{4}$	8.6	21.4
+8	8.8	21.2
$\frac{1}{2}$	11.2	18.8
+3	11.7	18.3
$\frac{1}{2}$	10.1	19.9
cb.	10.3	19.7
$\frac{1}{2}$	10.8	19.2
+5	11.1	18.9

N $\frac{1}{2}$

-5	10.6	19.4
$\frac{1}{2}$	11.1	18.9
cb.	10.4	19.6
$\frac{1}{4}$	10.7	19.3
+8	11.7	18.3
$\frac{1}{2}$	11.3	18.7
+5	8.6	21.4
$\frac{1}{2}$	8.5	21.5
+10	8.2	21.8
cb.	9.2	20.8
+2	10.0	20.0
+5	8.5	21.5
E	9.2	20.8

N cb.

E	9.4	20.6
+8	8.3	21.7
+10	9.7	20.3
cb.	9.0	21.0
+5	8.1	21.9
$\frac{1}{4}$	8.3	21.7
+9	8.6	21.4
$\frac{1}{2}$	11.2	18.8
+8	10.4	19.6
$\frac{1}{2}$	10.8	19.2
cb.	11.0	19.0
N	10.8	19.2
+5	10.8	19.2
N.L. Nutmeg		
-5	11.0	19.0
N	11.0	19.0
cb.	11.4	18.6
$\frac{1}{4}$	11.1	18.9
+10	10.6	19.4
$\frac{1}{2}$	9.6	20.4
+3	8.5	21.5
+5 = W Rail main line	7.65	22.39
$\frac{1}{4}$ on W " turnout	7.58	22.46
" E " main line	7.49	22.55
" " turnout	7.41	22.63
$\frac{1}{4}+8$	7.9	

+11	8.8	21.2
cb.	7.6	20.4
+4	8.4	21.6
E	8.8	21.2
Section ①		
E-10	7.9	22.1
E	8.0	22.0
+10	8.2	21.8
cb.	9.4	20.6
+5	7.6	22.4
+8 = E Rail Turnout	7.14	22.90
+9 = " " main line	7.19	22.85
$\frac{1}{4}$ W " turnout	7.32	22.72
" " main line	7.34	22.70
$\frac{1}{4}+7$	8.2	21.8
$\frac{1}{2}$	10.4	19.6
$\frac{1}{2}$	10.4	19.6
cb.	10.2	19.8
N	10.7	19.3
+10	10.7	19.3
Section ② - $\frac{1}{2}$ upright switch turnout to SE. - From Main Line		
+10	10.8	19.2
N	10.3	19.7
cb.	7.8	20.2
$\frac{1}{4}$	7.8	20.2
$\frac{1}{2}$	7.6	20.4

3004 = π
 7.82 -
 25.72
 22.26 - 8M.
 004

Chk on B.M. NE. 806 Nutmeg & Cal. Page 18

30.04

$\frac{1}{2} + 4$	7.7	22.3
+11 = Y Rail main line	7.04	23.00
E " " "	6.88	23.16
$\frac{1}{2}$	7.4	22.6
+7	7.5	22.5
cb.	9.0	21.0
+2	7.8	22.2
E	8.0	22.0
+10	7.8	22.2
		✓ ARE on Main Line
Section ③	Note: All Radon Rafts From Here	
-5	6.6	23.4
E	7.0	23.0
+10	7.4	22.6
cb.	7.3	22.7
+3	8.6	21.4
+8	7.0	23.0
+11 = E Rail	6.60	23.44
$\frac{1}{4}$	7.1	22.9
Y "	6.78	23.26
$\frac{1}{4} + 7$	7.5	22.5
Z	9.6	20.4
+3	7.8	22.2
+8	9.2	20.8
$\frac{1}{4}$	9.8	20.2
cb.	9.7	20.3
Y	9.9	20.1
+10	10.4	19.6

3004

CAL. ST.
Cross Section 37

Section ④

-10	9.9	20.1
W	9.7	20.3
cb.	9.3	20.7
$\frac{1}{4}$	9.1	20.9
+7	8.5	21.5
+10	7.2	22.8
Z	8.2	21.8
+2	9.3	20.7
+8	7.2	22.8
Y Rail	6.49	23.55
$\frac{1}{2}$	6.9	23.1
E Rail	6.33	23.71
$\frac{1}{4} + 7$	6.7	23.3
$\frac{1}{4} + 10$	8.5	21.5
cb.	7.4	22.6
+2	6.0	24.0
E	6.0	24.0
+10	5.3	24.7
		Section ⑤
-10	4.0	26.0
E	5.1	24.9
+5	4.1	25.9
cb.	6.7	23.3
+2	8.2	21.8
+8	6.5	23.5

3004

E Rail	6.08	23.96
$\frac{1}{4}$	6.5	23.5
Y "	6.25	23.79
$\frac{1}{4} + 6$	7.0	23.0
L	8.9	21.1
+3	6.9	23.1
+8	8.4	21.6
$\frac{1}{4}$	8.7	21.3
cb	8.5	21.5
Y	9.3	20.7
+10	9.6	20.4
section 12 (6)		
-10	9.0	21.0
Y	8.4	21.6
cb	8.3	21.7
$\frac{1}{4}$	8.3	21.7
+7	7.8	22.2
+10	6.7	23.3
L	7.6	22.4
+3	8.6	21.4
+8	6.6	23.4
Y Rail	5.96	24.08
$\frac{1}{4}$	6.40	23.64
E "	5.79	24.25
+6	6.2	23.8
+10	7.8	22.2

3004

CALIFORNIA ST.
CROSS SECTION 68

cb	6.7	23.3
+7	3.2	26.8
E	4.1	25.9
+10	3.2	26.8
+13.50	3.3	26.7
-15.30	1.5	28.5
-10	1.8	28.2
E	3.2	26.8
+5	1.8	28.2
cb	6.5	23.5
+2	7.7	22.3
+8	6.0	24.0
E Rail	5.52	24.52
$\frac{1}{4}$	6.0	24.0
Y "	5.69	24.35
+6	6.1	23.6
+10	8.3	21.7
L	6.8	23.2
+2	6.4	23.6
+7	7.8	22.2
$\frac{1}{4}$	8.0	22.0
cb	8.7	21.3
Y	9.0	21.0
+10	10.5	19.5
section 8 - Sta. Olive St. see sketch P. 48		
-10	10.2	19.8
Y	9.8	20.2

30.04

cb	9.7	20.3	
$\frac{1}{4}$	9.0	21.0	
+6	8.6	21.4	
+10	6.2	23.8	
$\frac{1}{2}$	7.2	22.8	
+2	8.1	21.9	
+8	6.1	23.9	
W Rail	5.45	24.59	
$\frac{1}{4}$	5.8	24.2	
E "	5.26	24.78	
$\frac{1}{4}+5$	5.7	24.3	
+10	7.3	22.7	
cb	6.2	23.8	
+4	5.1	24.9	
+8	0.5	29.5	
E	0.9	29.1	
+19.3A	+0.2	30.2	
T.P. 700	36.67	0.37	29.67
Chk. on BM. Con. Mon. 2nd 5' WEL	6.07	36.72	30.60
	S cb.		30.65 = Elev. Mon. P. 26 0.05 = error
			30.65 = Above B.M. 100
-21.18	5.7	21.0	
-10	7.0	19.7	
E	6.7	30.0	
$\frac{1}{4}$	6.3	30.4	

36.72

CALIFORNIA ST,
Goss Section 69

+7	10.0	26.7
cb.	12.4	24.3
+2	13.9	22.8
+7	12.4	24.3
E Rail	11.77	24.95
$\frac{1}{4}$	12.3	24.4
W "	11.95	24.77
$\frac{1}{2}+5$	12.6	24.1
+10	14.8	21.9
$\frac{1}{2}$	13.8	22.9
$\frac{1}{4}$	15.2	21.5
cb.	15.9	20.8
W	16.3	20.4
+10	16.4	20.3
		5 $\frac{1}{4}$
-10	17.0	19.7
W	16.2	20.5
cb.	15.5	21.2
$\frac{1}{4}$	15.3	21.4
+10	13.8	22.9
$\frac{1}{2}$	15.2	21.5
+8	12.5	24.2
W Rail	11.85	24.87
$\frac{1}{2}$	12.2	24.5
E "	11.69	25.03
$\frac{1}{2}+6$	12.1	24.6

36.72

cb.	13.7	23.5
+10	10.5	26.2
E	6.0	30.7
+15	6.0	30.7
+22.94	4.4	32.3
-24.77	3.5	33.2
-15	5.6	31.1
E	6.1	30.6
+5	6.2	30.5
+7	11.0	25.7
cb.	13.0	23.7
+5	12.0	24.7
E Rail	11.51	25.21
$\frac{1}{2}$	12.0	24.7
N "	11.69	25.03
$\frac{1}{2}$ +5	12.3	24.4
+10	14.4	22.3
$\frac{1}{2}$	12.6	24.1
+8	14.2	22.5
$\frac{1}{2}$	14.7	22.0
cb.	15.2	21.5
N	15.0	21.7
+10	15.5	21.2
-10	15.8	20.9

N $\frac{1}{2}$

36.72

CALIF. ST.
Cross Section

N	15.3	21.4
cb.	14.9	21.8
$\frac{1}{2}$	13.8	22.9
+8	13.2	23.5
+10	11.8	24.9
$\frac{1}{2}$	14.1	22.6
+8	12.1	24.6
N Rail	11.58	25.14
$\frac{1}{2}$	12.0	24.7
E Rail	11.41	25.31
$\frac{1}{2}$ +5	11.8	24.9
cb.	13.3	23.4
+5	10.6	26.1
+8	6.0	30.7
E	5.0	31.7
+15	5.6	31.1
+22.94	3.2	33.5
N cb.		
-21.18	1.8	24.9
-15	4.7	32.0
E	4.7	32.0
+5	5.2	31.5
+7	10.8	25.9
cb.	12.2	24.5
+2	13.4	23.3
+7	11.7	25.0

36.72

E Rail	11.28	25.44
$\frac{1}{4}$	11.8	24.9
W "	11.45	25.27
$\frac{1}{2} + 5$	12.0	24.7
$\frac{3}{8}$	13.0	23.7
+4	11.1	25.6
+8	13.3	23.4
$\frac{1}{4}$	14.1	22.6
cb.	14.9	21.8
W	15.0	21.7
+10	15.7	21.0
597	36.62	6.07
N.L. olive	Sections on Road of Line	
-10	15.1	21.5
W	14.2	22.4
$\frac{3}{8}$	13.5	23.1
$\frac{1}{4}$	13.5	23.1
+7	13.0	23.6
+10	11.0	25.6
$\frac{1}{2}$	12.7	24.4
+2	13.4	23.2
+7	11.8	24.8
W Rail	11.21	25.41
$\frac{1}{4}$	11.7	24.9
E Rail	11.05	25.57
$\frac{1}{4} + 7$	11.6	25.0

36.62

CALIF. ST.
Cross Section 71

cb	13.0	23.6
+4	10.5	26.7
+8	4.2	32.4
E	4.1	33.5
+10	3.0	33.6
+15	4.1	32.5
+19.34	1.5	35.1
Section ①		
-15.3	1.8	34.8
-10	1.8	34.8
E	3.6	33.0
+5	4.8	31.8
+7	10.3	26.3
cb.	12.7	23.9
+6	11.2	25.4
E Rail	10.78	25.84
$\frac{1}{2}$	11.5	25.1
W Rail	10.95	25.67
+5	11.5	25.1
+10	13.4	23.2
$\frac{1}{2}$	11.4	25.2
+4	12.3	24.3
$\frac{1}{4}$	13.5	23.2
cb.	13.4	23.2
W	14.5	22.1
+10	15.3	21.3

36.62

Section 2

-10	14.7	21.9
W	14.7	21.9
cb	13.4	23.2
$\frac{1}{4}$	13.3	23.3
+7	12.4	24.2
+10	10.8	25.8
$\frac{1}{2}$	12.0	24.6
+2	13.1	23.5
+7	11.3	25.3
WEST Rail	10.70	25.92
$\frac{1}{4}$	11.2	25.4
E	10.54	26.08
$\frac{1}{4}+6$	11.0	25.6
cb	12.5	24.1
+2	10.0	26.6
+4	9.9	26.7
+7	4.1	32.5
E	3.4	33.2
+5	14	35.2
+13.5	1.7	34.9

Section 3

-10.76	1.3	35.3
E	2.0	34.6
+5	3.7	32.9
+8	10.0	26.6

36.62

CALIF. ST.
GASS Section

72

cb.	12.3	24.3
+7	10.7	25.9
E Rail	10.28	26.34
$\frac{1}{4}$	10.9	25.7
W "	10.45	26.17
+5	11.1	25.5
+10	12.7	23.9
$\frac{1}{2}$	11.3	25.3
+1	10.3	26.3
+5	12.4	24.2
$\frac{1}{4}$	12.9	23.7
cb.	13.6	23.0
W	14.0	22.6
+10	14.6	22.0

Section 4

-10	13.6	23.0
W	13.2	23.4
cb.	12.8	23.8
$\frac{1}{4}$	12.4	24.2
+7	11.7	24.9
+10	10.1	26.5
$\frac{1}{2}$	10.8	25.8
+3	12.4	24.2
+8	10.9	25.7
W Rail	10.18	26.44
$\frac{1}{4}$	10.7	25.9
E "	10.00	26.6

36.62

$\frac{1}{4}+6$	10.5	26.1
+10	12.0	24.6
cb.	10.8	25.8
+4	9.3	27.3
+7	1.6	34.0
E	1.6	35.0
+10.78	1.0	35.6
Section 5		
-6.75	^{plus Rail} +0.2	36.8
E	0.7	35.9
+4	1.3	35.3
+7	9.0	27.6
cb.	11.7	24.9
+6	10.2	26.4
E Rail	9.78	26.84
$\frac{1}{4}$	10.4	26.2
N Rail	9.96	26.66
$\frac{1}{4}+3$	10.5	26.1
+5	11.6	25.0
+8	11.7	24.9
L	9.0	27.6
+8	10.0	26.6
$\frac{1}{4}$	11.7	24.9
cb.	12.3	24.3
N	13.0	23.6
+10	14.7	21.9

36.62

CALIF. ST.
GASS SECTION 73

(Section 5) +7'		
-10	12.6	24.0
N	11.5	25.1
cb.	10.0	26.6
$\frac{1}{4}$	8.6	18.0
L	7.2	29.4
+2	10.7	25.9
+3	11.8	24.8
+9	10.5	26.1
N Rail	9.86	26.76
$\frac{1}{4}$	10.3	26.3
E Rail	9.68	26.98
$\frac{1}{4}+8$	10.1	26.5
cb.	11.6	25.0
+4	8.6	28.0
+9	1.0	25.6
E	0.9	35.7
+5	0.0	36.6
(Section 5) +9'		
-5	0.0	36.6
E	1.0	35.6
+4	1.0	35.6
+9	8.6	28.0
cb.	11.6	25.0
+5	10.1	26.5
$\frac{1}{4}$	10.3	26.3
+4	10.4	26.2

36.62

+10	11.8	24.8
+11	10.7	25.9
$\frac{1}{2}$	3.8	32.8
$\frac{1}{2}$	4.0	32.6
cb.	3.0	33.6
W	5.3	31.3
+10	6.4	30.2
-10	6.6	30.0
W	4.0	32.6
cb.	3.2	33.4
$\frac{1}{2}$	4.6	32.0
+10	4.4	32.2
$\frac{1}{2}$	10.0	26.6
+5	11.6	25.0
+9	10.2	26.4
W Rail	9.68	26.94
$\frac{1}{4}$	10.2	26.4
E "	9.49	27.13
+7	10.0	26.6
cb.	11.2	25.4
+4	8.5	28.1
+7	2.8	34.3
E	1.3	35.3
+5.04	0.3	36.3

Section 6

Section 7

36.62

CALIFORNIA ST.
ROSS Section 74

-3.59	0.4	36.2
E	1.1	35.5
+5	1.9	34.7
+7	7.8	28.8
cb.	11.3	25.3
+5	9.8	26.8
E Rail	9.27	27.35
$\frac{1}{2}$	10.0	26.6
W "	9.44	27.18
$\frac{1}{2}$ +4	10.3	26.3
+9	11.2	25.4
$\frac{1}{2}$	10.2	26.4
+2	4.3	32.3
$\frac{1}{2}$	4.3	32.3
cb.	4.7	31.9
W	6.0	30.6
+10	7.5	29.1
-10	7.2	29.4
W	5.4	31.2
cb.	4.4	32.2
$\frac{1}{4}$	4.0	32.6
$\frac{1}{2}$	3.4	33.2
+7	9.2	27.4
+5	7.3	29.3
+8	10.0	26.6

Section 8

3662

W Rail		9.24	27.38
$\frac{1}{4}$		9.7	26.9
E "		9.07	27.55
$\frac{1}{4}+7$		9.6	27.0
+10		11.1	25.5
cb.		9.0	27.6
+8		7.8	28.8
+5		7.2	29.4
+8		0.5	36.1
E		0.0	36.6
+234		+0.5	37.1
TD	3.12	38.75	0.99
	5 cb.		35.63
E-176		1.2	37.6
E		1.5	37.3
+4		1.8	37.0
+6		9.7	29.1
cb.		13.0	25.8
+5		11.6	27.2
E Rail		11.04	27.71
$\frac{1}{4}$		11.6	27.2
W "		11.22	27.53
+4		11.9	26.9
+7		13.3	25.5
$\frac{1}{4}$		11.4	27.3
+2		5.6	33.2

3875 CALIFORNIA ST. Cross Section 75

$\frac{1}{4}$		6.1	32.7
cb.		7.4	31.4
W		8.6	30.2
+10		9.4	29.4
	5 $\frac{1}{4}$		
+10		9.8	29.0
W		9.0	29.8
cb.		6.7	32.1
$\frac{1}{4}$		5.8	33.0
+10		5.0	33.8
$\frac{1}{4}$		11.6	27.2
+5		13.1	25.7
+10		11.8	27.0
W Rail		11.10	27.65
$\frac{1}{4}$		11.7	27.1
E "		10.95	27.80
$\frac{1}{4}+7$		11.5	27.3
cb.		13.0	25.8
+5		10.3	28.5
E		1.0	37.7
+13		0.8	38.0
	$\frac{1}{4}$		
	-0.89 on Con. Mon.	1.08	37.67 See P-23
	E	1.1	37.7
	+2	1.4	37.4
	+6	10.1	28.7

38.75

cb.	130	25.8
+7	11.4	27.4
$\frac{1}{2}$	11.4	27.4
+3	11.4	27.4
+5	13.0	25.8
+10	10.5	28.3
cb	10.5	28.3
+2	4.4	34.4
$\frac{1}{4}$	6.3	32.5
cb.	7.3	31.5
N	8.7	30.1
+10	9.6	29.2
	N $\frac{1}{2}$	
-10	8.0	30.8
N	6.5	32.3
+11	6.4	32.4
cb	5.0	33.8
$\frac{1}{4}$	5.2	33.6
+10	4.8	34.0
L	11.6	27.2
+4	13.0	25.8
+9	11.5	27.3
$\frac{1}{4}$	11.3	27.5
+7	11.2	27.6
cb.	13.0	25.8
+8	9.4	29.4

38.75

CALIF. ST.
Cross, Section 76

E	0.8	38.0
	N. Gb	38.0
E	0.1	38.7
+4	9.4	29.4
cb.	12.8	26.0
+7	11.0	27.8
$\frac{1}{4}$	11.2	27.6
+4	11.4	27.4
+7	12.8	26.0
L	9.8	29.0
+2	4.3	34.5
$\frac{1}{4}$	4.7	34.1
cb.	2.6	36.2
+2	5.5	33.3
N	6.4	32.4
+10	6.5	32.3
	N. L. Palm	
N at Base Cal. House ✓	6.4	32.4
+10	6.0	32.8
cb.	2.5	36.3
$\frac{1}{4}$	4.3	34.5
+10	4.0	34.8
L	10.3	28.4
+2	12.4	26.4
+9	11.3	27.5
N Rail	10.72	28.03

3875

1/2	11.2	27.6
E Rail	10.53	28.22
1/4 + 8	11.0	27.8
cb.	12.7	26.1
+ 8	8.2	30.6
E	2.5	36.3
+ 3	0.8	38.0
26.25' N.N.W. PALM = E.C. = 0+00		
- 5	0.3	38.5
E	4.6	33.2
+ 4	9.5	29.3
cb.	12.6	26.2
+ 9	10.8	28.0
E Rail	10.32	28.43
1/2	11.0	27.8
W	10.46	28.29
1/4 + 5	11.1	27.7
+ 8	12.4	26.6
1/2	9.8	29.0
+ 2	3.5	35.3
1/4	3.8	35.0
± b	2.1	36.7
+ 2	6.0	32.8
W at	6.2	32.6
+ 1.5 = at House	6.2	32.6
4.00	41.63	1.08
		37.67

use this BM.
37.63 - Elev. 1100. P. 23

4163

CALIF ST.
Cross Section 77

↓ 0+15 E. Cal. House (stack) on W 4' in st 10' side.

0+20

W	9.5	32.1
cb	8.8	32.8
+ 1	6.7	34.9
1/2	6.7	34.9
+ 10	6.2	35.4
+ 11	12.8	28.8
1/2	13.0	28.6
- 5	15.0	26.6
+ 9	13.9	27.7
W Rail	13.25	28.38
1/2	13.9	27.7
E Rail	13.08	28.55
1/4 + 7	14.6	27.0
cb.	15.3	26.3
E	7.0	34.6
+ 5 = top Bank	2.7	38.9
0+39		
- 5 = top Bank	3.3	38.3
E	8.0	33.6
cb	15.3	26.3
+ 5	8.6	28.0
1/4	13.6	28.0
+ 3	13.6	28.0
+ 7	15.0	26.6

4163

d	13.0	28.6
+2	7.0	34.6
$\frac{1}{4}$	7.2	34.4
+5	6.6	35.0
cb.	9.0	32.6
X	12.2	29.4
+10	13.2	28.4
	0+59	
-10	13.4	28.2
X	11.6	30.0
cb.	9.8	31.8
$\frac{1}{4}$	8.7	32.9
+10	7.6	34.0
+11	11.6	30.0
d	13.5	28.1
+5	15.0	26.6
+9	13.6	28.0
X Rail	12.85	28.78
$\frac{1}{4}$	13.4	28.2
E "	12.75	28.88
$\frac{1}{4}+7$	13.4	28.2
cb.	15.1	26.5
E	9.5	32.1
+7 = top Bank	4.1	37.5
	0+74	
-6 = top Bank	4.5	37.1

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CALIFORNIA

Cross Section 78

E	9.2	32.4
cb.	15.0	26.6
+5	13.3	28.3
$\frac{1}{4}$	13.3	28.3
+3	13.3	28.3
+7	14.6	27.0
$\frac{1}{4}$	12.7	28.9
+2	8.3	33.3
$\frac{1}{4}$	8.9	32.7
+10	4.0	37.6
cb.	7.4	34.2
X	12.5	29.4
+10	14.4	27.2

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Note: Cross Sections Cont. in Book 1272

" for chk. out for Above H.I. See continuation of Levels in Book 1272

67
202
57 2
196 28

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body

of table in same row and column gives distance from side stake to slope stake. If ground is not the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point and line of sight should cut target.
necessarily.

**IMPROVED TABLES
AND
INFORMATION**

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add connection found in column of connections. Degree of curve with a given T may be found by dividing tangent (or external), opposite T by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

TABLE X.
MIDDLE ORDINATES OF RAILS
Length of Rail (feet)

C	R	30	28	26	24	22	20	C	R	30	28	26	24	22	20
o /	Feet	Inch	Inch	Inch	Inch	Inch	Inch	o	Feet	Inch	Inch	Inch	Inch	Inch	Inch
0-20	17189	.08	.07	.06	.05	.04	.03	8	716.8	1.88	1.64	1.42	1.20	1.01	.84
0-40	8594	.16	.14	.12	.10	.08	.07	9	637.3	2.12	1.84	1.60	1.35	1.14	.94
1-0	5730	.24	.20	.18	.15	.13	.10	10	573.7	2.36	2.05	1.78	1.50	1.27	1.04
1-20	4297	.31	.27	.23	.20	.17	.13	11	521.7	2.59	2.26	1.95	1.65	1.39	1.15
1-40	3438	.39	.34	.29	.25	.21	.17	12	478.3	3.83	2.47	2.15	1.81	1.54	1.26
2-0	2865	.47	.41	.35	.30	.25	.20	13	441.7	3.05	2.66	2.30	1.96	1.66	1.36
2-20	2456	.55	.48	.41	.35	.29	.23	14	410.3	3.30	2.87	2.48	2.10	1.78	1.46
2-40	2149	.63	.55	.47	.40	.33	.27	15	383.1	3.54	3.08	2.68	2.26	1.91	1.57
3-0	1910	.71	.62	.53	.45	.38	.31	16	359.3	3.76	3.28	2.83	2.40	2.04	1.67
3-20	1719	.78	.68	.59	.50	.42	.35	17	338.3	4.00	3.48	3.02	2.57	2.16	1.78
3-40	1563	.86	.75	.65	.55	.46	.38	18	319.6	4.21	3.67	3.18	2.70	2.28	1.87
4-0	1433	.94	.82	.71	.60	.50	.42	19	302.9	4.45	3.89	3.36	2.86	2.41	1.98
4-20	1323	1.02	.89	.77	.65	.55	.45	20	287.9	4.70	4.09	3.55	3.00	2.54	2.09
4-40	1228	1.10	.96	.83	.70	.59	.48	22	262.0	5.16	4.44	3.84	3.30	2.80	2.29
5	1146	1.18	1.03	.89	.75	.63	.52	24	240.5	5.64	4.92	4.20	3.59	3.04	2.50
6	955.3	1.41	1.23	1.06	.90	.76	.62	26	222.3	6.07	5.29	4.58	3.88	3.29	2.70
7	819.0	1.65	1.44	1.24	1.05	.89	.73								

TABLE XI.
SHORT RADIUS CURVES

Radius Feet	Chord Feet	Central Angle	Deflection Angle	Deflection for 1 Foot
35	10	16-26	8-13	49.3
45	10	12-46	6-23	38.3
50	15	17-16	8-38	34.5
60	15	14-22	7-11	28.8
75	15	11-30	5-45	23.0
100	20	11-30	5-45	17.3
120	20	9-34	4-47	14.3
150	20	7-39	3-49	11.5
190	25	7-32	3-46	9.15
200	25	7-10	3-35	8.6
225	25	6-25	3-12	7.7
240	25	5-58	2-59	7.2
250	25	5-44	2-52	6.9
275	25	5-12	2-36	6.2
288	50	9-58	4-59	6.0
300	50	9-32	4-46	5.7
350	50	8-12	4-06	4.9
376	50	7-40	3-50	4.6
400	50	7-10	3-35	4.3
410	50	7-00	3-30	4.2

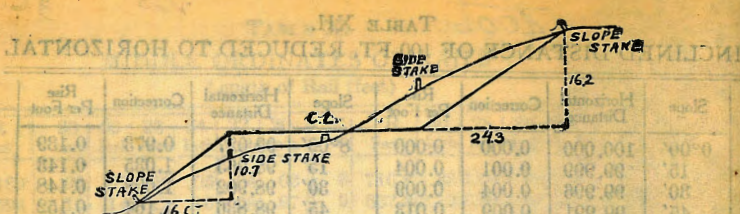
To find length of curve divide angle from P. C. to P. T. by central angle of chord and multiply by length of chord.

3899
107
1006
311
46
265
301
26
36
TABLE XII.
INCLINED DISTANCE OF 100 FT. REDUCED TO HORIZONTAL

Slope	Horizontal Distance	Correction	Rise Per Foot	Slope	Horizontal Distance	Correction	Rise Per Foot
0°00'	100.000	0.000	0.000	8°00'	99.027	0.973	0.139
15'	99.999	0.001	0.004	15'	98.965	1.035	0.143
30'	99.996	0.004	0.009	30'	98.902	1.098	0.148
45'	99.991	0.009	0.013	45'	98.836	1.164	0.152
1 00	99.985	0.015	0.017	9 00	98.769	1.231	0.156
15	99.976	0.024	0.022	15	98.700	1.300	0.161
30	99.966	0.034	0.026	30	98.629	1.371	0.165
45	99.953	0.047	0.031	45	98.556	1.444	0.169
2 00	99.939	0.061	0.035	10 00	98.481	1.519	0.174
15	99.923	0.077	0.039	15	98.404	1.596	0.178
30	99.905	0.095	0.044	30	98.325	1.675	0.182
45	99.885	0.115	0.048	45	98.245	1.755	0.187
3 00	99.863	0.137	0.052	11 00	98.163	1.837	0.191
15	99.839	0.161	0.057	15	98.079	1.921	0.195
30	99.813	0.187	0.061	30	97.992	2.008	0.199
45	99.786	0.214	0.065	45	97.905	2.095	0.204
4 00	99.756	0.244	0.070	12 00	97.815	2.185	0.208
15	99.725	0.275	0.074	15	97.723	2.277	0.212
30	99.692	0.308	0.078	30	97.630	2.370	0.216
45	99.657	0.343	0.083	45	97.534	2.466	0.221
5 00	99.619	0.381	0.087	13 00	97.437	2.563	0.225
15	99.580	0.420	0.092	15	97.338	2.662	0.229
30	99.540	0.460	0.096	30	97.237	2.763	0.233
45	99.497	0.503	0.100	45	97.134	2.866	0.238
6 00	99.452	0.548	0.105	14 00	97.030	2.970	0.242
15	99.406	0.594	0.109	15	96.923	3.077	0.246
30	99.357	0.643	0.113	30	96.815	3.185	0.250
45	99.307	0.693	0.118	45	96.705	3.295	0.255
7 00	99.255	0.745	0.122	15 00	96.593	3.407	0.259
15	99.200	0.800	0.126	15	96.479	3.521	0.263
30	99.144	0.856	0.131	30	96.363	3.637	0.267
45	99.087	0.913	0.135	45	96.246	3.754	0.271

TABLE XIII.
MINUTES IN DECIMALS OF A DEGREE.

0 30"	.00833	10' 30"	.17500	20' 30"	.34167	30' 10"	.50833	40' 30"	.67500	50' 10"	.84167
1 00	.01667	11 00	.18333	21 00	.35000	31 00	.51667	41 00	.68333	51 00	.85000
30	.02500	30	.19167	30	.35833	30	.52500	30	.69167	30	.85833
2 00	.03333	12 00	.20000	22 00	.36667	32 00	.53333	42 00	.70000	52 00	.86667
30	.04167	30	.20833	30	.37500	30	.54167	30	.70833	30	.87500
3 00	.05000	13 00	.21667	23 00	.38333	33 00	.55000	43 00	.71667	53 00	.88333
30	.05833	30	.22500	30	.39167	30	.55833	30	.72500	30	.89167
4 00	.06667	14 00	.23333	24 00	.40000	34 00	.56667	44 00	.73333	54 00	.90000
30	.07500	30	.24167	30	.40833	30	.57500	30	.74167	30	.90833
5 00	.08333	15 00	.25000	25 00	.41667	35 00	.58333	45 00	.75000	55 00	.91667
30	.09167	30	.25833	30	.42500	30	.59167	30	.75833	30	.92500
6 00	.10000	16 00	.26667	26 00	.43333	36 00	.60000	46 00	.76667	56 00	.93333
30	.10833	30	.27500	30	.44167	30	.60833	30	.77500	30	.94167
7 00	.11667	17 00	.28333	27 00	.45000	37 00	.61667	47 00	.78333	57 00	.95000
30	.12500	30	.29167	30	.45833	30	.62500	30	.79167	30	.95833
8 00	.13333	18 00	.30000	28 00	.46667	38 00	.63333	48 00	.80000	58 00	.96667
30	.14167	30	.30833	30	.47500	30	.64167	30	.80833	30	.97500
9 00	.15000	19 00	.31667	29 00	.48333	39 00	.65000	49 00	.81667	59 00	.98333
30	.15833	30	.32500	30	.49167	30	.65833	30	.82500	30	.99167
10 00	.16667	20 00	.33333	30 00	.50000	40 00	.66667	50 00	.83333	60 00	1.00000



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/4 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

3547
283
4747
3264
1530

1175
184
1359

380.46
80
300.46
2621
274.21

5371
028
5399
1188
4211
4152
59

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CALIFORNIA.

439
756
23
44
23
23
153
25
308
3080
70
68.64

23.16 = dist. from stan to 2 tracks
23.68 = " " " " " " Redwood.

148
120
168
208
208
330

15
22
30
33
33.6
198
330

75.00
52.40
22.60

37.5
12.75
50.25

12.75
24.75
37.50
12.75
50.25
63.00

935 204 93
63
11.52/600/102
146
4

593

4 110102
28.25
96.20
121.45
707
129.52

320
180
130
87
1011
870
184
10.59
10.11

5025
273
1375
1550
233
13.15
82
95
472
14.22

172

1065
87
1005
195

105.0
175
875

12.75
210
10.65
87
275

0.85 - 1040
1011.65
2' wide

371.29
6.47
364.82
6.70
371.52

160
16.14
143.86

40.8
40
36.2

3547
736
28.11 = opt

2268
118
1860
1897
53

364.82
7.82
367.64

2268
418
1850

2 87.50
39.70
327.20

364.82
10.09
374.91
4.02
370.89

374.87
5.68
369.19
1.22
370.41
7.49
362.92
4.87
367.79

263.60
23.15
286.75

392.67
277.00
115.67
1.0102
70714

33
37
40
53
72
98 = 1

364.82
2.54
367.36

38' 4" x 6"
4' wide
3' deep
26' long

10.8
12.75
23.55

1275
87
1222
180
1409

3004
782
2222
5
21.77