

1262

PASTS

FIELD BOOK

No. 365 F

ENGINEERING DEPARTMENT,
CITY OF SAN DIEGO,
CALIFORNIA.

MICROFILMED

DEC 22 1964

ENGINEERING DEPARTMENT,
CITY OF SAN DIEGO,
CALIFORNIA.

Our Leather Bound Engineers Note Books are carried in the following rulings:

- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
- No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.
- No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.
- No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

We also carry the Note Books listed above, bound in extra strong Fabri-Hide (otherwise the same quality of book), which can be furnished at a somewhat lower price.

In ordering Fabri-Hide covered books, add the letter "F" to catalog number.

THE FREDERICK POST CO.
ENGINEERING and DRAFTING SUPPLIES
IRVING PARK STATION
CHICAGO, ILL.

Index

PAGE

X sec. Boundary St.	1-8
X Sec. Vancouver Ave	9-30
X Sec. Alley BIK 3 Crittenden's	31-36
Sub.	2 44
X Sec. Alley BIK 242	
S.D. Land & Town	37-44
X sec. Haller St.	45-55
" Howard Ave	56-63
" 36th St Woolman to Kth	64-79

ENGINEERING DEPARTMENT,
CITY OF SAN DIEGO,
CALIFORNIA.

Cross-Section Boundary St.

	³⁵ 295.35 <u>295.70</u>	
4+75		
10'E	12.0	
E.L.	10.5	285.2
cb	9.9	
1/4	9.6	
+	9.3	286.4
1/4	9.2	
cb	9.1	
w.L.	8.9	286.8
4+50		
w.L.	9.6	286.1
cb	9.7	
1/4	9.9	
+	10.0	285.7
1/4	10.3	
cb	10.6	
+3	11.0	
E.L.	11.6	284.1
10'E	12.1	
4+75		
8'E	12.8	
10'E	14.1	
E.L.	12.1	283.6
+2	11.7	
cb	11.4	
+3	11.0	

Plotted 7-18-28 - C.B.H.

The Original H.I. is "Check" Elev. are Reduced .35 to Height.

Cont From Book 1242 P. 77

	⁷⁰ 295.35	
4+75		
E 1/4	10.9	
+	10.7	285.0
1/4	10.7	
cb	10.5	
w.L.	10.4	285.3
B.M. Can. Mon SL Laurel w.L. Boundary	^{5.88} 289.47 <u>289.82</u> - OK	
T.P. 0.96	³⁵ 284.87 <u>285.24</u>	11.42 283.93
5+00		
w.L.	0.7	284.5
cb	0.8	
1/4	0.7	
+1	1.0	
+	0.9	284.3
+2	1.1	
1/4	1.4	
+2	1.5	
cb	1.9	
E.L.	2.3	282.9
10'E	3.8	
5+25		
10'E	4.4	
E.L.	3.3	281.9
cb	2.6	
1/4	2.2	
+3	2.0	

	285.24		
5+25	287.89		
¢	1.8	283.4	
+1	1.6		
¼	1.6		
cb	1.5		
w.l.	1.5	283.7	
5+50			
w.l.	2.1	283.1	
cb	2.1		
¼	2.2		
+3	2.2		
¢	2.4	282.8	
+3	2.5		
¢	2.7		
cb	3.3		
+2	3.5		
EL	3.9	281.3	
10'E	5.3		
5+75			
10'E	5.9		
EL	4.4	280.8	
cb	3.9		
¼	3.3		
¢	3.0	282.2	
¼	2.9		
cb	2.7		
w.l.	2.8	282.4	

Boundary St. 2

	285.24		
6+00	244.89		
w.l.	3.6	281.6	
cb	3.5		
¼	3.6		
+3	3.7		
¢	3.8	281.4	
+1	3.9		
¼	4.1		
cb	4.5		
EL	5.1	280.1	
6'E	5.8		
10'E	6.5		
6+20 = N.L. Kalmlia			
10'E	7.5		
5'E	6.4		
EL	5.9	279.3	
cb	5.3		
¼	5.1		
¢	4.9	280.3	
¼	4.7		
+3	4.5		
cb	4.4		
w.l.	4.4	280.8	

285.24

~~284.89~~

Ncb line Kalmia

w.L.	4.9	280.3
cb	5.0	
1/4	5.2	
1/2	5.4	279.8
+3	5.3	
1/4	5.5	
cb	5.8	
E.L.	6.5	278.7
5'E	7.0	
10'E	7.9	
N 1/4 line Kalmia		
10'E	6.2	
E.L.	6.8	278.4
cb	6.3	
1/4	6.0	
+2	5.8	
1/2	5.8	279.4
1/4	5.7	
cb	5.5	
w.L.	5.4	279.8

Boundary St

285.24

~~284.89~~

1/2 Kalmia

w.L.	5.8	279.4
cb	5.9	
1/4	6.1	
1/2	6.2	279.0
1/4	6.2	
cb	6.6	
E.L.	7.3	277.9
10'E	8.5	
S 1/4 line Kalmia		
10'E	9.3	
E.L.	8.0	277.2
+3	7.7	
cb	7.1	
1/4	7.0	
1/2	6.8	278.4
1/4	6.6	
cb	6.4	
w.L.	6.5	278.7
Scb line Kalmia		
w.L.	6.5	278.7
cb	6.9	
1/4	7.2	
1/2	7.5	277.7
+3	7.6	
1/4	7.7	
cb	7.3	

3

285.24

~~284.89~~

S cb line Kalmia

Ecb + 2	7.6	
E.L.	9.5	276.7
10'E	9.9	
0 + 00 = S.L. Kalmia		
10'E	10.2	
5'E	9.6	
E.L.	8.8	276.4
cb	8.5	
+3	8.5	
1/4	8.3	
1/4	8.0	277.2
1/4	7.6	
cb	7.4	
w.L.	7.3	277.9
0 + 25		
w.L.	9.8	275.4
cb	9.6	
+4	9.3	
1/4	9.3	
1/4	9.4	275.8
1/4	9.5	
cb	9.8	
+3	10.4	
E.L.	10.6	274.6
10'E	11.4	
walk 1'E at 0+20	10.89	274.35 ✓

Boundary St.

4

285.24

~~284.89~~

0 + 50		
10'E		13.2
3'E		12.5
2.5E		12.5
E.L.		12.1
		273.2
cb		12.0
1/4		11.7
1/4		11.7
		273.5
1/4		12.0
+3		12.0
cb		12.2
w.L.		12.6
		272.6
10'w		13.3
	273.35	272.0
T.P. 1.15	273.00	271.85
0 + 75		
10'w		3.5
w.L.		3.0
		270.4
cb		2.8
1/4		2.7
1/4		2.6
		270.8
1/4		2.5
cb		2.5
E.L.		2.7
		270.7
10'E		3.4
floor house ^{22'E} 9+0+80		2.89
		270.46 ✓

1+00	273.35	
10'E	5.5	
5'E	5.1	
E.L.	5.0	268.4
cb	4.8	
1/4	4.7	
±	4.7	268.7
+3	4.9	
1/4	4.9	
+3	5.0	
cb	5.1	
+1	5.3	
w.L.	5.8	267.6
8'w.	5.7	
10'w	7.2	
floor	7.85	265.50
at sta 1+09 house 20'w		
1+25		
10'w	11.2	
5'w	10.9	
4'w	9.6	
w.L.	9.6	263.8
cb	8.5	
1/4	8.2	
±	8.0	265.4
+3	8.0	
1/4	7.8	

Boundary St.

5

1+25	273.35	
Ecb	7.6	
E.L.	7.7	265.7
10'E	8.7	
1+50		
10'E	12.0	
E.L.	11.6	261.8
cb	11.6	
+2	11.6	
1/4	12.2	
±	12.4	261.0
1/4	13.0	
+3	13.3	
cb	13.7	
w.L.	14.7	258.7
4'w	15.9	
10'w	16.9	260.91
J.P.	0.14	260.30
		12.44
		260.36
1+75		
10'w	9.2	
6'w	7.6	
w.L.	6.2	254.8
cb	5.0	
1/4	4.3	
±	3.8	257.2
1/4	3.3	
cb	2.9	

261.05

1475		
E.L.	5.7	258.3
5'E	2.9	
10'E	2.6	
2+00		
10'E	5.9	
E.L.	6.3	254.8
cb	6.7	
+3	7.2	
1/4	9.8	
1/4	8.5	252.6
1/4	9.5	
+2	8.9	
cb	10.5	
+3	11.4	
w.L.	12.3	248.8
4'w	13.2	
10'w	13.5	
2+25		
10'w	17.7	
1'w	16.9	
w.L.	16.4	244.7
+3	15.0	
cb	15.8	
+4	15.1	
1/4	14.5	
1/4	13.7	247.4

Boundary St.

261.05

~~260.70~~

6

2+25		
E'W		12.8
cb		12.4
+4		11.9
E.L.		11.4
4'E		10.7
10'E		11.5
T.P. e.o.l	248.06 35 247.71	13.00
2+50		
10'E		6.8
E.L.		6.9
cb		7.0
1/4		7.1
1/4		7.2
1/4		7.6
+3		7.7
cb		7.5
w.L.		8.0
5'w		8.2
10'w		9.2
2+67		
10'w		12.8
7'w		11.9
w.L.		10.9
cb		10.3
+1		10.8
1/4		10.3

249.7

248.05
~~247.70~~

241.2

240.8

240.0

237.2

2+67	248.06	
	247.71	
+1	10.1	
¢	10.0	238.1
¼	9.7	
cb	9.5	
E.L.	9.4	238.7
10'E	9.5	
2+75		
10E	10.5	
E.L.	10.4	237.7
cb	10.6	
¼	11.3	
¢	12.1	236.0
¼	11.8	
cb	12.7	
w.L.	13.5	234.6
5'w	14.3	
10'w	15.4	
T.P. 0.07	235.09 234.74	235.02 234.69
2+90	13.04	
15'w	9.7	
10'w	8.7	
5'w	7.5	
w.L.	6.2	228.9
cb	5.7	
+3	4.6	
¼	3.8	

Boundary est. 7

2+90	235.09	
	234.74	
¢	3.3	231.8
¼	1.5	
cb	1.1	
+3	0.3	
E.L.	0.0	235.1
3+00		
E.L.	3.4	231.7
cb	4.5	
¼	5.8	
¢	6.8	228.3
¼	8.2	
cb	9.9	
+3	10.1	
w.L.	10.7	224.4
6'w	12.2	
10'w	12.6	
15'w	13.3	
3+17		
20'w	22.0	
15'w	20.5	
w.L.	18.7	216.4
cb	16.6	
¼	14.9	
¢	13.8	221.3
¼	13.0	
cb	12.0	✓

3+17	235.09		
	234.74		
E.L.	10.2	224.9	
10'E	7.6		
3+35			
10'E	14.6		
T.P. 0.68	222.85	222.63	
	222.50	221.82	
2'E	4.1		
E.L.	5.3	217.5	
cb	7.0		
1/4	8.7		
⊕	11.2	211.6	
+4	12.5		
1/4	13.4		
cb	14.6		
w.l.	15.3	207.5	
7'w	16.1		
10'w	16.9		
20'w	17.8		
25'w	19.1		
30'w	19.3		
3+55			
30'w	19.5		
w.l.	22.3	200.5	
cb	23.1		
+3	21.2		
1/4	19.6		
⊕	17.4	205.4	

Boundary St. 8

3+55	222.85		
E/L	14.3		
+2	13.8		
cb	12.8		
+3	11.8		
E.L.	10.8	212.0	
5'E	8.1		
15'E	5.8		
3+75			
20'E	11.0		
10'E	12.9		
T.P. 0.90	210.97	210.97	
	210.62	12.78	209.72
E.L.	5.5	205.5	
cb	6.9		
1/4	8.5		
⊕	9.9	201.1	
+4	11.4		
1/4	12.1		
+3	12.2		
cb	11.7		
w.l.	8.9	202.1	
5'w	6.8		
12'w	4.8		
20'w	1.5		

.97
~~210.62~~

3+92⁴ = end. - w side.

15' W	1.8	
12' W	3.5	
5' W	5.6	
W.L.	7.2	203.8
Cb	8.7	
1/4	9.8	
2	11.4	199.6
1/4	12.7	
+2	13.2	
+3	13.6	
+4	13.9	
Cb	13.2	
E.L.	11.6	199.4
6'E	8.9	
10'E	7.6	
20'E	5.3	
End Section		
20'E	10.7	
13'E	11.3	
5'E	12.1	
E.L.	13.5	197.5
+3	14.5	
Cb	11.7	
1/4	12.2	
2	11.1	199.9
1/4	9.4	

Boundary St.

Jun 9-25

Louton
Morgan
Zsbell.

End Sec 210.62⁹⁷

Web	8.2	
W.L.	7.1	203.9
4' W	5.8	
13' W	2.8	
T.P. 12.49	222.27	0.84 209.78
T.P. 12.23	234.21	0.29 221.98
T.P. 8.60	242.06	0.75 233.46
B.M. Nail Pole sand Cooper	0.71	241.35

This is on Low Datum
which is what we wish
to use.

X section Vancouver From s.l. Maple

to southerly termination

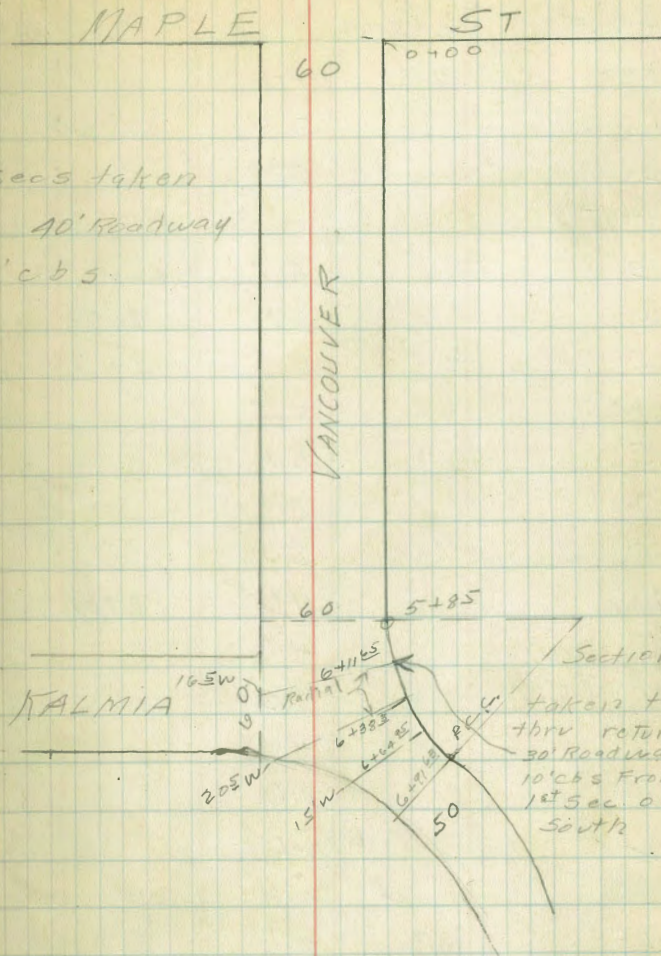
Loudon
Isbell
Morgan.

9

B.M.	3.90	275.29	271.39	Hub N.E. Vancouver & Maple
0+00 = s.l. Maple				
E.L.		4.7	270.6	
cb		4.2		
+5		4.1		
1/4		3.8		
1/2		3.5	271.8	
+6		3.3		
3/4		3.3		
+8		3.1		
cb		3.1		
+4		2.9		
w.l.		2.8	272.5	
0+25				
w.l.		2.8	272.5	
+7		3.1		
+8		3.4		
cb		3.4		
+5		3.4		
1/4		3.7		
+4		3.9		
+7		3.9		
1/2		4.0	271.3	
3/4		4.4		
+4		4.4		
+5		4.6		

Plotted 7-19-28 - C.B.H.

This is one low bottom valley is Okla.



Secs taken
for 40' Roadway
10' cbs.

Sections
taken thru
return
30' Roadway
10' cbs from
1st sec. on ret.
South

Vancouver

0+25	275.29	
E.L.	4.8	
E.L.	5.3	270.0
10'E	5.7	
0+50	6.9	
10'E	6.9	2204
E.L.	6.1	269.2
+5	5.8	
cb	5.5	
+5	5.4	
+7	5.1	
1/4	5.1	
E	4.6	270.7
+5	4.3	
1/4	4.2	
+4	4.1	
cb	3.6	
+2	3.6	
+3	3.3	
W.L.	3.1	272.2
0+95		
W.L.	3.5	271.8
+6	3.7	
+8	4.3	
cb	4.3	
+5	4.7	
1/4	4.9	

0+75	275.29	
E	5.4	269.9
+5	5.7	
1/4	6.0	
+4	6.3	
+5	6.6	
cb	7.0	
+6	7.3	
E.L.	7.9	267.4
15'E	9.0	266.5
1+00	12.9	
15'E	12.9	624
E.L.	10.4	264.9
+4	9.6	
cb	8.8	
+5	7.9	
1/4	7.3	
+7	6.7	
E	6.3	269.0
+6	5.8	
1/4	5.6	
+7	5.1	
cb	4.9	
+3	4.8	
+5	4.2	
W.L.	3.9	271.4

Vancouver:

12.2
11.8

11

1+18	275.29	
w.l.	4.0	271.3
+4	4.3	
+6	4.9	
cb	5.1	
+4	5.4	
1/4	5.6	
2	6.3	269.0
+6	6.7	
1/4	7.7	
+3	7.8	
cb	9.1	
+1	9.4	
+6	10.3	
E.L.	12.9	2624
16'E	21.1	254.2
20'E	22.1	
1+25		
20'E	25.8	
16'E	22.9	252.4
7'E	18.1	
E.L.	14.8	260.5
+6	12.6	
+7	11.1	
cb	9.6	
+6	8.9	
+8	9.4	

1+25	275.29	
E 1/4	7.1	
+5	6.8	
2	6.3	269.0
1/4	5.7	
cb	5.3	
+4	4.9	
+6	4.3	
w.l.	4.1	271.2
1+38		
w.l.	4.1	271.2
+4	4.3	
+7	5.0	
cb	5.1	
+3	5.4	
1/4	5.7	
2	6.4	2689
+5	7.2	
1/4	10.0	
+5	13.2	
cb	14.1	
+6	18.0	
E.L.	19.0	256.3
15'E	22.2	253.1
20'E	23.2	

Vancouver

1+55

275.29

15'E	14.9	2604
6'E	12.1	
FL	11.0	264.3
+5	9.7	
cb	9.0	
+6	8.0	
1/4	8.1	
+4	7.2	
±	6.8	268.5
1/4	5.9	
+4	5.5	
+7	5.4	
cb	5.0	
+4	4.9	
+6	4.2	
incl.	4.0	271.3
1+86		
w.l.	4.4	270.9
+3	4.6	
+5	5.4	
cb	5.4	
+2	5.7	
+5	5.8	
1/4	6.4	
±	6.9	268.4
1/4	8.0	

12.1

12

1+86

275.29

E 1/4 + 1	8.6	
+6	8.6	
cb	9.4	
EL	10.8	264.5
15'E	13.2	262.1
2+07		
20'E	20.7	
12'E	22.7	252.6
FL	22.5	252.8
cb	17.5	
1/4	13.0	
±	7.2	268.1
1/4	6.6	
+9	6.3	
cb	6.0	
+6	5.7	
+8	5.2	
incl.	4.9	270.4
2+16		
w.l.	5.0	270.3
+2	5.8	
+8	6.0	
cb	6.3	
1/4	6.8	
+8	7.3	

11.3
Vancouver

2+16	275.29	
ϕ	7.7	267.6
+8	12.0	
1/4	13.0	
+4	14.1	
cb	17.7	
E.L.	20.8	254.5
2'E	21.9	
11'E	27.8	
20'E	27.5	249.8
2+26		
2.5'E	36.0	
20'E	31.7	243.6
15'E	31.7	
8'E	26.8	
E.L.	25.0	250.3
cb	19.3	
1/4	13.9	
+6	7.6	
ϕ	7.4	267.9
1/4	6.7	
+5	6.2	
cb	6.0	
+3	5.7	
+5	5.8	
+8	5.5	
w.L.	4.6	270.7

13.0
1.8

13

2+38	275.29	
w.L.	4.4	270.9
+2	5.0	
+6	5.4	
+8	5.2	
cb	5.6	
+2	5.7	
+5	6.2	
1/4	6.5	
ϕ	7.2	268.1
+6	9.1	
1/4	10.5	
cb	13.2	
E.L.	17.5	257.8
5'E	19.3	
10'E	22.3	
15'E	25.6	249.7
25'E	31.0	
2+52		
25'E	31.7	
13'E	24.0	250.7
11'E	22.6	
E.L.	14.4	260.9
cb	11.4	
+8	9.5	
1/4	9.4	

Vancouver

275.29

2+52		
E/A +6	8.8	
±	7.2	268.1
+5	6.6	
1/4	6.1	
+2	6.2	
+6	5.6	
cb	5.4	
+3	4.9	
+8	4.3	
w.L.	3.7	271.6
2+75		
w.L.	3.2	272.1
+2	4.0	
+7	4.3	
cb	4.6	
+2	4.6	
1/4	5.3	
+5	5.9	
±	6.3	269.0
+5	6.7	
1/4	7.5	
+7	8.5	
cb	9.4	
+5	10.7	
E.L.	11.6	263.7

13.0

275.29

14

2+75		
13'E	14.2	
16'E	16.2	259.1
19'E	19.5	
25'E	23.0	
3+00		
20'E	13.9	261.9
E.L.	10.0	265.3
cb	8.1	
+6	7.1	
1/4	7.0	
+3	6.6	
+5	6.2	
±	5.7	269.6
1/4	4.9	
+8	4.3	
cb	4.2	
+4	4.1	
w.L.	3.5	271.8
3+25		
w.L.	3.6	271.7
+5	3.9	
cb	4.1	
1/4	4.5	
±	4.9	270.4
1/4	6.1	
+6	6.4	

Vancouver

275.29

3+25		
ECB	7.1	
E.L.	8.6	266.7
20'E	12.3	263.0
3+50		
15'E	10.2	265.1
E.L.	7.6	267.7
cb	6.4	
+6	5.5	
1/4	5.3	
1/4	4.4	270.9
1/4	4.0	
cb	3.6	
+9	3.3	
w.L.	2.9	272.4
3+75		
w.L.	3.0	272.8
+2	3.6	
cb	3.6	
1/4	4.0	
1/4	4.5	270.8
1/4	4.9	
+3	5.0	
cb	6.0	
E.L.	7.0	268.3
15'E	9.0	266.3

15

275.29

T.P. 0.19

273.14 2.34 272.95

4+00

w.L.	0.8	272.3
+1	1.4	
+7	1.4	
cb	1.5	
1/4	1.8	
1/4	2.5	270.6
1/4	2.8	
+2	2.7	
+4	3.0	
+6	2.9	
cb	3.6	
E.L.	4.6	268.5
15'E	6.1	269.2
4+25		
20'E	7.1	268.2
E.L.	4.8	268.3
cb	3.5	
1/4	3.0	
1/4	2.5	270.6
1/4	2.6	
+7	1.7	
cb	1.7	
+9	1.4	
w.L.	1.2	271.9

Vancouver^{11.2}

16

4+34	273.14	
w.L.	1.3	271.8
+1	1.6	
cb	1.9	
+5	2.0	
1/4	2.2	
♀	2.7	270.4
1/4	3.0	
+3	3.1	
+5	3.0	
cb	3.7	
+5	4.5	
E.L.	5.1	268.0
9'E	6.2	
16'E	7.9	
20'E	9.4	263.7
4+50		
25'E	16.9	
14'E	15.4	257.7
7'E	12.6	
E.L.	9.4	264.9
+5	5.3	
+9	4.0	
cb	4.0	
+5	3.3	
1/4	3.3	
♀	2.8	270.3

4+50	273.14	
♀+4	2.5	
1/4	2.5	1
cb	2.1	
+4	1.9	
+7	1.9	
w.L.	1.7	271.4
4+60		
w.L.	1.7	271.4
+1	2.1	
cb	2.4	
+3	2.3	
1/4	2.6	
+5	2.8	
♀	3.1	270.0
1/4	3.4	
+5	3.5	
cb	4.5	
+4	5.2	
+7	5.9	
+8	7.4	
E.L.	8.0	265.1
13'E	14.7	258.4
17'E	17.6	247.0
25'E	22.0	255.5

Vancouver⁴_{9.0}15.5
2.5
7.8

7.7

17

4+75

273.14

4+87

273.14

25'E	24.2	
14'E	16.8	563
E.L.	9.0	264.1
42	7.4	
cb	5.0	
+5	3.9	
1/4	3.6	
+7	3.3	
4	3.4	269.7
+5	3.5	
1/4	3.5	
cb	4.1	
+5	4.1	
+9	3.7	
w.L.	3.3	269.8
4+87		
w.L.	3.8	269.3
+1	4.5	
+6	5.0	
cb	5.0	
+7	4.8	
1/4	5.0	
+5	5.3	
4	5.1	268.0
1/4	4.6	
+7	5.0	

Ecb	5.6	
+7	7.3	
E.L.	8.6	264.5
13'E	14.9	258.2
25'E	21.4	
5+00		
25'E	23.9	
14'E	18.5	546
E.L.	13.0	260.1
+3	11.6	
cb	10.1	
1/4	9.1	
4	9.2	263.9
+5	10.1	
1/4	8.2	
+6	5.7	
cb	5.4	
+5	5.3	
+9	4.9	
w.L.	4.2	268.9

Vancouver.

5+13	273.14	
w.L.	5.0	268.1
cb	5.6	
+3	5.9	
1/4	10.0	
ϕ	14.8	258.3
1/4	14.5	
cb	15.4	
E.L.	17.6	255.5
25'E	26.6	246.5
5+26		
25"E	29.6	
16'E	28.3	244.8
E.L.	23.9	249.2
cb	20.5	
1/4	19.4	
+7	16.0	
ϕ	16.1	257.0
1/4	9.6	
+6	6.0	
cb	5.7	
w.L.	5.1	268.0

11.6

18

5+50	273.14	
w.L.	3.1	270.0
+4	4.6	
cb	4.9	
1/4	5.4	
ϕ	8.6	264.5
1/4	11.0	
cb	12.4	
E.L.	13.2	259.9
10'E	14.2	58.9
20'E	15.1	58.1
5+70		
15'E	7.1	266.0
E.L.	6.1	267.0
cb	4.8	
+3	4.3	
+5	4.4	
+9	4.0	
1/4	4.1	
ϕ	4.4	268.7
+5	4.3	
1/4	4.0	
+6	3.6	
+8	3.7	
cb	3.4	
+2	3.2	
+5	2.3	

Vancouver

6+70	273.14	
w.l.	2.1	271.0
5+85 = B.C. return on E.		
w.l.	2.3	270.8
+4	2.3	
+8	2.7	
cb	3.1	
1/4	3.4	
+3	3.4	
±	3.8	269.8
+5	3.8	
1/4	4.1	
+7	3.8	
cb	4.0	
E.L.	4.6	268.5
10'E	5.0	
Return A equal parts Secs for 30' roadway		
10' cbs		
6+11 65		
10'E	5.0	
E.L.	4.8	268.3
cb	4.5	
1/4	4.8	
±	4.5	268.6
+3	4.4	
1/4	4.1	
cb	4.2	

6+11 65	273.14	
+4	4.0	
w.l.	3.6	269.5
165w Int.	2.9	
6+38 30		
205'w Int	3.9	
14'w	4.3	
25'w	4.5	
w.l.	4.7	268.4
cb	5.1	
1/4	5.2	
+3	5.4	
±	5.5	267.6
1/4	5.8	
cb	5.8	
E.L.	5.9	267.2
10'E	5.9	
6+64 95		
10'E	7.1	
E.L.	7.4	265.7
cb	7.5	
+5	7.5	
1/4	7.8	

ENGINEERING DEPARTMENT,
CITY OF SAN DIEGO,
CALIFORNIA.

Vancouver

20

6+64⁹⁵

273.14

+5	7.4	
±	7.5	265.6
+2	7.5	
+5	7.8	
1/4	7.3	
+4	7.2	
cb	7.5	
+8	6.8	
w.L.	6.8	266.3
10'w	6.9	
15'w Int.	6.8	
T.P. 5.20	270.85	7.49 265.65

6+91⁶⁸ = P.R.C. stationed on outside 10 equal ft.

10'w	9.6	
w.L.	9.1	261.7
cb	7.8	
1/4	6.7	
±	6.7	264.1
1/4	6.8	
cb	6.7	
E.L.	6.0	264.9

7+14

270.85

E.L.	6.3	264.6
+5	6.9	
cb	6.9	
1/4	7.3	
+4	6.8	
+7	7.0	
±	7.0	263.9
1/4	7.0	
+3	7.0	
cb	7.9	
w.L.	10.3	260.6
10'w	10.9	
7+36 ³²		
10'w	10.7	
w.L.	10.4	260.5
+4	10.2	
cb	8.1	
+3	7.1	
1/4	6.9	
±	7.2	263.7
+3	6.9	
1/4	7.0	
+3	7.0	
cb	6.5	
+5	6.8	
+8	4.3	

Vancouver.

7+36³²

270.85

E.L.	4.1	266.8
7+58 ²⁴		
E.L.	4.2	266.7
+7	4.4	
cb	5.5	
+4	6.0	
1/4	6.4	
1/4	6.6	264.3
1/4	6.8	
+4	7.1	
cb	7.6	
+5	9.6	
w.L.	10.3	260.6
10'w	11.8	
7+81 ¹⁴		
10'w	10.7	
w.L.	9.7	261.2
cb	7.2	
1/4	6.4	
1/4	6.1	264.8
1/4	5.4	
cb	4.7	
+2	4.4	
+5	3.6	
E.L.	3.6	267.3

21

6+03⁴⁸

270.85

10'E	4.5	
E.L.	4.2	266.7
+8	4.1	
cb	4.2	
+3	4.6	
1/4	4.8	
1/4	5.6	265.3
+3	5.8	
1/4	6.0	
+5	6.2	
cb	6.7	
w.L.	8.5	262.4
10'w	10.2	
8+25 ⁸⁵		
10'w	9.1	
w.L.	7.4	263.5
cb	5.7	
+3	5.3	
+6	5.5	
1/4	5.5	
1/4	5.1	265.8
1/4	4.7	
cb	4.3	
+5	4.4	
E.L.	4.8	266.1
10'E	5.8	

Vancouver

22

8+48²²

270.85

10'E	7.5	
5'E	6.6	
E.L.	5.8	265.1
+7	5.2	
cb	4.9	
+5	4.7	
1/4	5.0	
±	5.0	265.9
+3	5.1	
1/4	5.2	
+5	5.1	
cb	5.3	
w.l.	6.4	264.5
10'w	8.0	
8+70 ⁵⁹		
10'w	7.2	
w.l.	6.1	264.8
+8	5.3	
cb	5.5	
1/4	5.4	
±	5.3	265.6
1/4	5.5	
+3	5.3	
+5	5.7	
cb	5.6	
E.L.	7.1	263.8

8+70⁵⁷

270.85

10'E	8.9	
8+92 ²⁵		
10'E	9.7	
E.L.	7.9	263.0
+5	6.8	
cb	6.4	
1/4	5.6	
±	5.4	265.5
1/4	5.5	
+3	5.6	
cb	5.6	
+2	5.5	
w.l.	6.2	264.7
10'w	7.0	
9+15 ³⁷ E.C.		
10'w	7.1	
w.l.	6.2	264.7
+7	5.6	
cb	5.6	
1/4	5.5	
+5	5.4	
±	5.4	265.5
1/4	5.9	
+2	5.9	
cb	6.6	

Vancouver

23

9+15³² E.C. 270.85

+5	7.3	
E.L.	8.3	262.6
10'E	10.0	
9+40		
10'E	9.5	
E.L.	7.8	263.1
+8	6.8	
cb	6.6	
+5	5.9	
1/4	6.0	
+6	5.5	
±	5.6	265.3
+5	5.6	
1/4	5.6	
cb	5.5	
+3	5.4	
w.L.	6.1	264.8
10'w	7.0	
9+75		
10'w	6.8	
w.L.	6.0	264.9
+7	5.2	
cb	5.3	
1/4	5.4	
±	5.4	265.5
1/4	5.5	

9+75⁻ 270.85

E 1/4 +3	5.7	
cb	5.8	
+5	6.7	
E.L.	7.2	263.6
10'E	8.9	
10+05 ³⁷ B.C. stationed on outside. 6 = parts		
10'E	8.3	
E.L.	6.8	264.1
+6	6.0	
cb	5.6	
1/4	5.1	
±	4.7	266.0
1/4	5.0	
cb	5.0	
w.L.	5.5	265.4
10'w	6.2	
10+36 ¹⁶		
10'w	5.7	
w.L.	5.2	265.7
cb	4.7	
1/4	4.5	
±	4.6	266.3
1/4	4.9	
cb	5.2	
E.L.	6.4	264.5
10'E	7.7	

VANCOUVER

270.85

floor house 12' East 10+49 ✓

6.08 263.77

10+66⁹⁵

10'E 7.0

E.L. 6.2 264.7

cb 5.1

1/4 4.5

1/4 4.5 266.4

1/4 4.4

1/4 4.6

w.L. 4.8 266.1

10'W 4.8

floor house 21'W 4.38 266.47 ✓

10+97²⁴

10'W 5.0

w.L. 5.3 265.6

cb 4.8

1/4 4.4

1/4 4.4 266.5

1/4 4.4

+5 4.6

cb 4.7

+5 5.3

E.L. 5.9 265.0

10'E 7.3

24

270.85

TP 1.51 267.84 4.52 266.33

11+28⁵³

10'E 4.0

E.L. 2.5 265.3

cb 1.6

1/4 1.3

1/4 1.5 266.3

1/4 1.6

cb 1.9

w.L. 2.3 265.5

10'W 3.2

11+59³²

10'W 3.9

w.L. 3.0 264.8

cb 2.6

1/4 2.2

1/4 2.0 265.8

1/4 1.7

+4 1.7

cb 1.8

E.L. 2.1 265.7

10'E 2.5

Vancouver

25

11+90 ⁴	E.C. 267.84		
10'E		2.6	
E.L.		2.5	265.3
cb		2.5	
+5		2.4	
1/4		2.6	
1/4		2.9	264.9
1/4		3.0	
+3	1	3.0	
cb		3.3	
w.L.		3.8	264.0
10'w		4.6	
12+20			
10'w		5.4	
w.L.		4.8	263.0
+4		4.8	
cb		4.5	
1/4		4.3	
1/4		4.2	263.6
1/4		4.0	
cb		3.4	
E.L.		3.2	264.6
10'E		3.0	

12+50	267.84		
10'E		3.9	
E.L.		4.0	263.8
cb		4.5	
1/4		4.8	
1/4		4.9	262.9
1/4		5.1	
+3		4.9	
+5		5.1	
cb		5.2	
w.L.		5.5	262.3
10'w		6.0	
12+75			
10'w		6.1	
w.L.		5.7	262.1
cb		5.4	
1/4		5.4	
1/4		5.1	262.7
+5		5.2	
1/4		5.2	
+3		5.1	
cb		5.1	
E.L.		4.7	263.1

Vancouver

26

13+00

267.84

E.L.	5.4	2624
cb	5.6	
+6	5.5	
1/4	5.5	
⊥	5.6	2622
1/4	5.6	
+5	5.5	
cb	5.7	
w.L.	5.9	2619
10'w	6.2	
13+25		
10'w	5.9	
w.L.	5.8	2620
cb	5.9	
1/4	5.9	
⊥	5.8	2620
1/4	5.8	
cb	5.8	
E.L.	5.8	2620
10'E	6.0	

13+50

267.84

10'E	6.2	
E.L.	5.9	2619
+6	5.9	
cb	6.2	
+4	5.9	
1/4	5.9	
⊥	5.8	2620
1/4	5.8	
cb	5.7	
+5	5.5	
w.L.	5.3	2625
10'w	5.2	
13+75		
10'w	4.2	
w.L.	4.4	2634
cb	5.0	
1/4	5.3	
⊥	5.5	2623
1/4	5.6	
cb	6.3	
E.L.	6.4	2614
10'E	6.8	

Vancouver

14+00	267.84	
10E	7.3	
E.L.	6.7	261.1
cb	6.3	.
+3	6.1	
1/4	5.6	
1/2	5.1	2627
1/4	4.8	
cb	4.6	
+7	4.2	
w.L.	4.2	2636
10'w	4.1	
14+2924 = End on E.		
10'w	4.4	
w.L.	4.4	2634
+6	4.5	
cb	4.6	
1/4	4.7	
1/2	5.0	2628
1/4	5.5	
+5	6.0	
cb	6.0	
E.L.	6.7	261.1
10'E	7.6	

end section

10' E	267.84	7.4
E.L.		6.7
		261.1
+8		6.0
cb		6.0
1/4		5.6
1/2		5.1
		2627
1/4		4.9
cb		4.8
+4		4.4
w.L.		4.7
		263.1
10'w		4.8
T.P. 0.01	256.40	11.45
		256.39
B.M. sent Cooper.		15.12
		241.28 (241.34)

X Section Vancouver From N.L.

B.M	3.11	274.50	271.39
0+00 = N.L.	Maple		
E.L.	3.1	271.4	
cb	3.0		
+5	3.1		
1/4	2.9		
+5	2.6		
±	2.6	271.9	
1/4	2.7		
cb	2.7		
w.l.	3.1	271.4	
10'w	3.6		
0+25			
10'w	4.6		
w.l.	3.8	270.7	
cb	3.3		
+5	3.4		
1/4	2.9		
±	2.8	271.7	
1/4	2.8		
+5	2.9		
+7	2.7		
cb	2.7		
E.L.	2.7	271.8	

Maple to Canyon North.

Jun 12-28
Loudon. 28

0+50	274.50	
E.L.	2.5	272.0
cb	2.6	
+3	2.7	
+5	3.0	
1/4	3.0	
+7	3.0	
±	3.3	271.2
+7	3.4	
1/4	3.7	
+6	4.1	
+8	3.9	
cb	4.1	
w.l.	5.2	269.3
10'w	6.6	
0+75		
15'w	12.4	
5'w	9.6	
w.l.	7.6	266.9
cb	5.8	
1/4	4.9	
±	4.0	270.5
+3	3.8	
1/4	3.6	
+5	3.5	
+7	3.3	

Vancouver

29

0+75	274.50	
Ecb	3.1	
E.L.	2.8	271.7
10'E	2.7	
1+00		
10'E	3.8	
E.L.	3.6	270.9
+5	3.6	
cb	3.9	
+3	4.0	
+5	4.4	
1/4	4.4	
±	5.1	269.4
1/4	6.2	
cb	7.9	
w.L.	10.5	264.0
15'w	15.0	
1+17		
15'w	15.5	
w.L.	12.3	262.2
cb	9.4	
+5	8.9	
1/4	7.9	
±	6.5	268.0
+4	6.0	
1/4	5.3	
+3	5.4	

1+17	274.50	
Ecb	4.7	
E.L.	4.7	269.8
10'E	4.9	
1+35		
15'E	6.6	
E.L.	6.9	267.6
+4	6.5	
+5	6.7	
cb	7.2	
+2	7.3	
+4	7.6	
1/4	7.8	
±	9.1	265.4
+6	10.4	
1/4	11.3	
cb	13.1	
w.L.	14.4	260.1
20'w	17.4	
1+58		
20'w	19.9	
15'w	18.2	
w.L.	16.2	258.3
cb	15.7	
1/4	14.8	
±	13.8	260.7

VANCOUVER

30

1+58	274.50		
E 1/4	12.6		
+8	11.7		
cb	11.8		
+3	11.3		
+6	11.3		
E.L.	10.8	263.7	
15'E	10.0		
T.P. 0.33	262.09	12.74	261.76
1+73			
15'E	0.3		
E.L.	1.6	260.5	
+2	2.0		
cb	2.5		
1/4	2.8		
4	3.3	258.8	
+5	3.7		
1/4	3.7		
cb	4.3		
+5	4.7		
w.L.	5.4	256.7	
10'w	8.0		
20'w	11.6		

1+83	262.09		
25'w	15.9		
18'w	13.0		
10'w	10.7		
w.L.	7.7	254.4	
cb	5.4		
1/4	4.2		
4	3.8	258.3	
1/4	3.6		
cb	3.8		
+4	3.7		
E.L.	3.2	258.9	
20'E	3.1		
2+00 = Canyon			
20'E	3.8		
7'E	3.6		
3E	4.7		
E.L.	5.0	257.1	
cb	5.2		
1/4	5.5		
4	6.8	255.3	
1/4	8.3		
cb	11.2		
w.L.	14.1	248.0	
25'w	20.5		

X sec Alleg BK 3 Crittendens
Sub.

Jun 14-28
Loudon
Isbell
Morgan.

31

B.M. 296 289.82 286.86 ^{n.w. 6th} & Penna.

Subline Penna.

web 5.78
gut 6.36
gut at ϕ 6.72
gut at E.L. 6.99
Ecb 6.59

O+00 = S.L. Penna.

~~top~~ Ecb 6.33 283.5

E.L. Pav 6.36 283.4

ϕ Pav 6.40 283.4

w.L. Pav 5.87 284.0

top web 5.51 284.3

O+07 3.8 286.0

w.L. 4.1 285.7

+1 4.8 285.0

+2 4.7 285.1

+4 4.7 285.1

+6 4.8 285.0

ϕ 4.8 285.0

+2 4.8 285.0

+4 5.1 284.7

+8 5.1 284.7

E.L. 5.4 284.4

289.82

O+16

E.L. 4.8 285.0
+5 4.6 285.2
+9 4.3 285.8
 ϕ 4.4 285.4
+1 4.5 285.3
+2 4.3 285.5
+3 4.5 285.3
+7 4.6 285.2
+8 3.6 286.2
w.L. 3.5 286.3

O+30

w.L. 3.8 286.0
+2 4.1 285.7
+3 4.4 285.4
+5 4.5 285.3
 ϕ 4.3 285.5
+3 4.4 285.4
+6 4.6 285.2
+7 4.5 285.3
E.L. 4.6 285.2

Plotted 6-25-28
TSH

0+50		289.49		
E.L.			4.8	285.0
+3			4.6	285.2
⊕			4.2	285.6
+5			4.3	285.5
+6			4.6	285.2
+7			4.0	285.8
W.L.			3.8	286.0
T.P.	5.36	290.87	4.31	285.51
0+75				
W.L.			4.7	286.2
+5			4.6	286.3
+6			5.2	285.7
⊕			5.4	285.5
+1			5.2	285.7
+4			5.6	285.3
+6			5.4	285.5
E.L.			5.5	285.4
1+00				
E.L.			4.8	286.1
+4			4.8	286.1
+5			5.0	285.9
+8			4.7	286.2
⊕			4.9	286.0
+1			4.9	286.0
+3			4.5	286.4

Brdg on W. side in Alley
0+36 to 0+112

0.9' in Alley
at 1+12 on W. side at 1+50

1+00		290.87		
+6			4.0	286.9
W.L.			4.0	286.9
Garage	at 1+15 facing South on E.L. earth floor			
			5.3	285.6
1+25				
W.L.			4.2	286.7
+5			4.5	286.4
+9			4.8	286.1
⊕			4.7	286.2
+1			4.7	286.2
+3			4.9	286.0
+6			4.8	286.1
E.L.			5.2	285.7
0+50				
E.L.			5.3	285.6
+5			4.9	286.0
+7			5.1	285.8
⊕			5.0	285.9
+1			4.9	286.0
+5			4.4	286.5
W.L.			4.1	286.8
1+52	N end 2 ear garage 15E earth floor			
			5.14	285.7
1+69	S end same garage 15E			
			5.2	285.7

1470	29087		
w.l.	4.7	2862	
+5	4.9	2860	
+9	5.3	2856	
⊕	5.3	2856	
+2	5.2	2857	
+6	5.2	2857	
E.L.	5.3	2856	
1490			
E.L.	5.5	2854	
+5	5.5	2854	
+6	5.6	2853	
+8	5.5	2854	
⊕	5.7	2852	
+1	5.8	2851	
+5	5.3	2856	
w.l.	5.1	2858	
2404	⊕ Single garage 4.2' E Conc. floor		
	5.91	2850	
2405	⊕ Single garage 0.2 w Conc. floor.		
	4.86	2860	
2415			
w.l.	5.6	2853	
+5	6.1	2848	
+9	6.6	2843	
⊕	6.5	2844	

2415	29087		
⊕ +3	6.8	2841	
+3	6.6	2843	
E.L.	6.5	2844	
2430			
E.L.	7.2	2837	
+5	7.3	2836	
+7	7.4	2835	
⊕	7.3	2836	
+4	6.8	2841	
w.l.	6.4	2845	
2443	⊕ Single garage 1.25' E. Conc. floor		
	7.74	2831	
2443			
w.l.	7.1	2838	
+8	7.8	2831	
⊕	7.7	2832	
+3	7.9	2830	
+6	7.8	2831	
E.L.	7.7	2832	
2465			
E.L.	8.5	2824	
+8	8.6	2823	
⊕	8.8	2821	
+6	8.2	2827	
w.l.	7.8	2821	

2+90	290.87		
w.L.	8.7	2822	
+6	9.4	2815	
+7	9.4	2815	
♀	9.7	2813	
+8	9.4	2815	
E.L.	9.2	2817	
2+95	♀ Single garage 4' w Conc floor	8.34	2825
3+07	♀ Single garage 0.1 in Alley on E.	10.04	280.83
3+04	N end 4 car garage 4.9' w Conc floor	9.20	281.7
		10.47	280.40
3+46	S end same garage 4.9' w		
3+15			
E.L.	10.0	2809	
+5	10.3	2806	
♀	10.2	2807	
+3	9.9	2810	
w.L.	9.8	281.7	

3+50	290.87		
w.L.	10.3	2806	
+2	10.9	2800	
+6	11.0	2799	
♀	11.2	2797	
+2	11.3	2796	
+6	11.7	2792	
E.L.	11.1	2798	
3+57	♀ single garage 3.2' E wood floor	11.13	2798
3+75			
E.L.	12.3	2786	
+3	12.5	2784	
+6	12.8	2781	
♀	12.3	2786	
w.L.	10.6	270.3	
3+82	♀ single garage 2' w Conc floor	10.57	2803
4+00	♀ single garage 2' w Conc floor	11.00	279.9
4+05			
w.L.	12.0	278.9	
+5	12.7	278.2	
♀	13.3	277.6	
+4	13.5	277.4	
E.L.	13.1	277.8	
T.P.	13.05	277.82	

T.P.	3.14	280.96	277.82
H+10			
E.L.	3.6	2774	
+6	3.8	2772	
+8	3.5	2775	
±	3.3	2777	
w.L.	2.4	2786	
H+13	± Single garage 0.8' w earth floor		
	2.5	2785	
H+35			
w.L.	2.4	2786	
+8	4.0	2770	
±	4.1	2769	
+3	4.4	2766	
+6	4.2	2768	
E.L.	4.5	2765	
H+50			
E.L.	5.1	2759	
+6	4.8	2762	
+8	5.2	2758	
±	4.8	2762	
+5	4.0	2770	
w.L.	3.1	2779	

H+75	280.96	
w.L.	4.4	2766
+4	5.1	2759
+8	5.6	2753
±	6.1	2749
+3	5.8	2752
+8	5.6	2754
E.L.	5.8	2752
H+100		
E.L.	6.7	2743
+6	6.6	2744
±	6.7	2743
+2	7.0	2740
+3	7.0	2740
w.L.	6.4	2746
H+115		
w.L.	7.4	2736
±	7.6	2734
+5	7.6	2734
E.L.	7.5	2735
H+127		
E.L.	8.7	2723
+4	8.8	2722
±	8.6	2724
w.L.	8.6	2726

Chicken yard across Alley at 5+15

280.96
5+38 = edge Canyon

W.L.		10.7	270.3
±		10.5	270.5
E.L.		11.8	269.2
T.P.	8.84	289.80	0.00 280.96
BM	Benjamin 0179	2.94	286.86 ✓
average	0.98	281.81	280.83
T.P.	1.01	270.63	12.19 269.62

5+40

E.L.		2.7	267.9
+4		3.1	267.5
+6		2.3	268.3
±		0.9	269.7
+6		0.8	269.8
W.L.		1.6	269.0

5+47

10' W		4.6	2660
6 W		4.6	2660
5 W		5.3	2653
W.L.		5.2	2654
+5		5.8	2648
±		5.6	2650
+5		5.8	2648
+7		6.4	2642
E.L.		7.0	2636
5'E		7.0	2636
10'E		7.6	2630

5+52 270.63

10'E		10.2	2604
5'E		9.8	2608
E.L.		9.2	2614
+5		7.8	2628
+8		8.1	2625
±		9.1	2615
+2		8.9	2617
+7		7.0	2636
W.L.		6.4	2642
6' W		6.7	2639
10' W		7.4	2632

5+67

20' W		12.4	2582
10' W		13.0	2576
W.L.		13.8	2568
+7		14.7	2559
±		14.9	2557
T.P.	0.30	259.28	11.65 258.98
+3		3.4	2561
+7		3.7	2558
E.L.		5.1	2542
10'E		6.2	2531
20'E		6.3	2530

See P. 44 For Continuation

X Sec. Alley Blk 242 S.D. Land & Town.

Jun 14-28
London

87.15

87

BM	0.10	87.15	87.05	N.W. Sicard & Herrick
Web line	Sicard			
N ret	top ob	5.07		
S ret	top ob	5.73		
0+00 =	N.L. Sicard			
top ob		5.41	81.74	
S.L.		5.2	82.0	
+3		5.3	81.9	
+6		5.5	81.7	
±		5.4	81.8	
+1		5.3	81.9	
+3		5.5	81.7	
+8		5.1	82.1	
N.L.		4.6	82.6	
top N ob		4.77	82.38	
0+10				
N.L.		3.6	83.6	
+5		4.7	82.5	
+6		4.7	82.5	
+7		4.5	82.7	
±		4.4	82.8	
+1		4.6	82.6	
+4		4.6	82.6	
+7		4.1	83.1	
S.L.		4.0	83.2	
0+55	± Single garage 0.2 in Alley on S.	3.80		wood floor

82-52-7
7541

0+21⁵ ± Single garage 0.2 in Alley on S. wood floor

		3.38	
0+22			
S.L.		3.5	837
+4		3.5	837
+5		3.8	834
±		3.7	835
+3		3.7	835
+5		3.7	835
+6		4.0	832
+8		3.9	833
N.L.		3.0	84.2
0+32	± Single garage 0.2 in Alley on S. wood floor		
		2.46	84.7
0+38			
N.L.		2.9	84.3
+3		3.6	83.6
+5		3.4	83.8
+7		3.6	83.6
±		3.3	83.9
+2		3.6	83.6
+8		3.2	84.0
S.L.		3.2	84.0
0+42 ⁵	± Single garage 4.9' N Conc floor	1.87	85.3

87.15

earth floor

0+55 & Single garage 0-3' in on 5

3.60 836

0+57

S.L. 3.7 835

+4 3.6 836

+7 3.2 840

± 3.3 839

+3 3.4 838

+6 3.3 839

+9 3.0 842

N.L. 3.0 842

0+69 & Single garage 44' 5 earth floor

3.54 836

0+72

N.L. 3.0 842

+3 3.0 842

+5 3.1 841

+7 3.1 841

± 3.0 842

+3 3.2 840

+6 3.5 837

S.L. 3.7 835

~~0+80 & Single garage 4.6' 5 wood floor~~

T.P. 5.81 89.70 3.26 83.89

H.I.

8970

38

0+80 & Single garage 4.6' 5 wood floor

5.66 840

0+84⁵ & Single garage 1' N Conc floor

5.27 844

+089 & Single garage 4.3' 5 wood floor

5.90 838

0+94 & Single garage 3.5' N Conc floor

4.99 847

1+00

S.L. 5.8 839

+1 5.7 840

+3 5.8 839

+6 5.6 841

± 5.3 844

+1 5.3 844

+3 5.5 842

+7 5.4 843

N.L. 5.3 844

1+04 & Single garage 4.5' 5 earth floor

5.80 839

1+20

N.L. 5.0 847

+2 5.1 846

+3 5.4 843

+5 5.2 845

+8 5.0 847

	H. 16		
1+20	89.20		
⊕		5.0	847
+3		5.2	845
+8		5.8	839
S.L.		5.6	841
1+35			
S.L.		5.4	843
+1		5.5	842
+4		5.7	840
+6		5.2	845
⊕		4.9	848
+3		4.8	849
+6		5.0	847
+7		5.3	844
+8		4.9	848
N.L.		4.9	849
1+43 ⊕ Single garage 0.4' N cart floor		4.83	849
1+60			
N.L.		4.7	850
+2		4.7	850
+4		5.2	845
+6		5.1	846
⊕		5.1	846
+5		5.2	845
+7		5.6	841
S.L.		5.4	842

	89.70	39
1+63 ⊕ Single garage 2.5's. earth floor		
		5.2
0+76 ⊕ Single garage 0.15' N Porc floor		
		4.47
		85.2
1+80		
S.L.		4.4
		85.3
+4		5.0
		84.7
+6		4.8
		84.9
+8		4.9
		84.8
⊕		4.7
		85.0
+3		4.9
		84.8
+5		5.0
		84.7
N.L.		4.4
		85.3
0+89 ⊕ Single garage on N.L. Wood floor		
		4.02
		85.7
1+92 End 2 car garage 0.4's wood floor		
		4.29
		85.4
2+12 w end same garage 0.4's Conc floor		
		4.21
		85.5
2+00		
N.L.		4.1
		85.6
+5		4.6
		85.1
+6		4.3
		85.4
+7		4.4
		85.3
+9		4.2
		85.5
⊕		4.2
		85.5

2+00	89.70		
4+2		4.3	85.4
+3		4.3	85.4
+6		4.4	85.3
S.L.		4.3	85.4
2+25			
S.L.		3.6	86.1
+5		4.1	85.6
+6		3.9	85.8
+8		4.0	85.7
4		3.8	85.9
+3		4.0	85.7
+5		4.1	85.6
N.L.		3.9	85.8
2+35 4 Single garage 0.4' s. earth floor		3.75	85.9
{ 2+31 Eend near garage 4.7' N Conc. floor		3.26	86.4
{ 2+50 w. end same garage 5.0' N.		3.26	86.4
2+50			
N.L.		3.7	86.0
+3		3.9	85.8
+5		3.6	86.1
4		3.4	86.3
+3		3.5	86.2
+5		3.7	86.0

2+50	89.7		
S.L.		3.3	86.4
2+45 4 Single garage 0.4' s. earth floor		3.5	86.2
2+7.5			
S.L.		2.9	86.8
+2		2.9	86.8
+3		3.4	86.3
+5		3.4	86.3
+6		3.1	86.5
+8		3.1	86.5
4		3.0	86.7
+3		3.1	86.6
+5		3.0	86.7
+7		3.6	86.1
+8		2.8	86.9
N.L.		2.6	87.1
3+00			
N.L.		3.2	86.5
+4		3.3	86.4
4		3.0	86.7
+7		3.2	86.5
S.L.		3.1	86.6
3+06 4 Single garage 3' s. Conc. floor		3.10	86.6
3+07 4 Single garage 3.5' N Conc. floor		3.07	86.6

3+25

89.70

S.L.	3.0	867
+4	3.1	866
±	3.0	867
+4	3.1	866
+6	3.2	865
N.L.	3.0	867

3+34 Door Bldg o A'N Conc floor

3.00 867

3+37 Walk (Conc) 2' wide 1' S

2.72 870

3+46 ± Single garage 3.85 earth floor

2.85 868

3+50

N.L.	2.9	868
+2	2.9	867
+4	3.1	866
± top M.H.	2.45	872
+5	2.8	869
+7	3.0	867
S.L.	3.1	866

3+72 Conc walk 3' wide 1' S

2.77 869

3+75

S.L.	3.0	867
+4	2.9	868

3+75

89.70

S.L. + 7	2.6	871
±	2.6	871
+2	2.6	871
+6	2.9	868
N.L.	2.9	868

4+00

N.L. 2.8 869

+4 2.8 869

+8 2.6 871

± 2.6 871

+2 2.7 870

+5 3.0 867

S.L. 3.0 867

T.P. 7.00 94.13 2.57 87.13

4+08 ± Single garage 2.3's earth floor

7.1 870

4+25

S.L. 7.2 869

+2 7.1 870

+4 7.4 867

+6 7.2 869

+7 7.4 867

+9 7.1 870

± 7.1 870

+2 7.0 871

+3 7.1 870

41

4+25	94.13	7.0	87.1
N.L.			
4+50			
N.L.		6.7	87.4
+3		7.1	87.0
+6		7.1	87.0
+8		6.9	87.2
⊘		6.9	87.2
+2		7.1	87.0
+5		6.9	87.2
S.L.		6.9	87.2

4+50 E end 2 car garage 0.1 in on s earth floor

6.9 87.2

4+62 W end Same garage 0.2 5

6.9 87.2

4+57 ⊘ Single garage 6.5' N Conc floor

6.54 87.6

4+75			
S.L.		6.8	87.3
+8		6.7	87.4
⊘		6.5	87.2
+3		6.7	87.4
+5		6.8	87.3
+7		6.8	87.3
N.L.		6.4	87.7

42

5+00	94.13		
N.L.		5.9	88.2
+3		6.3	87.8
+7		6.3	87.8
⊘		6.0	88.1
+3		6.2	87.9
+5		6.0	88.1
+7		6.3	87.9
+8		5.9	88.2
S.L.		6.0	88.1

5+21 ⊘ Single garage 0.3' s earth floor

5.5 88.6

5+25

S.L. 5.5 88.6

+4 5.5 88.6

+6 5.4 88.7

+8 5.5 88.6

⊘ 5.3 88.8

+3 5.5 88.6

+7 5.5 88.6

N.L. 5.0 89.1

5+50

N.L. 4.3 89.8

+4 4.7 89.4

+7 4.7 89.4

+9 4.5 89.6

⊘ 4.6 89.5

	94.13		
5+50			
♀ +2	4.8	893	
+6	4.6	895	
S.L.	4.4	897	
5+91			
♀ single garage e. h. in on S. Conc. floor			
	3.99	901	
5+95			
S.L.	4.0	901	
+9	3.9	902	
+8	4.0	901	
♀	3.8	903	
+2	3.8	903	
+5E	3.9	902	
N.L.	3.6	905	
5+80			
N.L.	3.6	905	
+2	3.6	905	
+4	3.7	904	
+7	3.7	904	
♀	3.8	903	
+2	4.0	901	
+3	3.8	903	
S.L.	3.7	904	

	94.13		
5+88			
S.L.	3.7	904	
+5	3.5	906	
+8	4.0	901	
♀	3.8	903	
+2	3.6	905	
+6	3.7	904	
N.L.	3.3	908	
5+98			
N.L.	3.3	908	
+4	4.0	901	
♀	3.9	902	
+3	4.0	901	
+6	3.8	903	
S.L.	3.6	905	
6+00 = E.L. Jamison			
Top scb	3.95	9020	
S.L.	4.0	901	
+6	4.2	899	
+8	4.0	901	
♀	4.1	900	
+1	4.2	899	
+4	3.9	902	
+6	4.1	903	
N.L.	3.6	905	
top Ncb	3.58	906	

9A.13

Ech line Jamson
 Top N ret. 3.86
 Top S ret. 4.19
 T.P. 0.77 87.56 7.34 86.79
 B.M. Beginning 0.36 89.20

X sec Alley Blk 3 Crittenton's

Sub Cont From P 36

259.28

5+70
 20'E 12.3 247.0
 10'E 12.1 247.2
 E.L. 11.0 248.3
 +3 10.1 249.2
 +8 9.5 249.9
 ♀ 9.3 250.0
 +5 9.6 249.7
 W.L. 9.0 250.3
 20'W 8.8 250.5
 T.P. 0.08 247.61 11.75 247.53

44

5+85 247.61
 20'W 4.1 243.5
 W.L. 4.6 243.0
 +4 5.0 242.6
 ♀ 5.5 242.1
 +3 5.4 242.2
 +7 6.0 241.6
 E.L. 5.9 241.7
 20'E 6.4 241.2

6+00 = N.L. Brookes

20'E 12.4 235.2
 E.L. 12.1 235.5
 ♀ 11.8 235.8
 W.L. 11.1 236.5
 12'W 11.2 236.9
 20'W 10.1 237.5

X Section Haller St From Banjo
North of Maple to Wabash Ave

Jun 15-20
London

B.M.	5.57	281.04	275.47
0-30 = \pm Maple			
E.L.	5.2	275.8	
+8	5.4	275.6	
cb	5.5	275.5	
$\frac{1}{4}$	5.6	275.4	
$\frac{1}{2}$	5.7	275.3	
$\frac{3}{4}$	5.8	275.2	
cb	6.0	275.0	
W.L.	6.1	274.9	
0-60 = N.L. Maple			
W.L.	5.6	275.4	
+8	5.5	275.5	
cb	5.6	275.4	
+2	5.8	275.2	
$\frac{1}{4}$	5.5	275.5	
$\frac{1}{2}$	5.2	275.8	
$\frac{3}{4}$	5.0	276.0	
+6	5.1	275.9	
cb	5.1	275.9	
+3	4.9	276.1	
E.L.	4.9	276.1	
0-95			
E.L.	4.5	276.5	
cb	4.7	276.3	
$\frac{1}{4}$	4.7	276.3	

H.S. N.W.
Haller & Maple

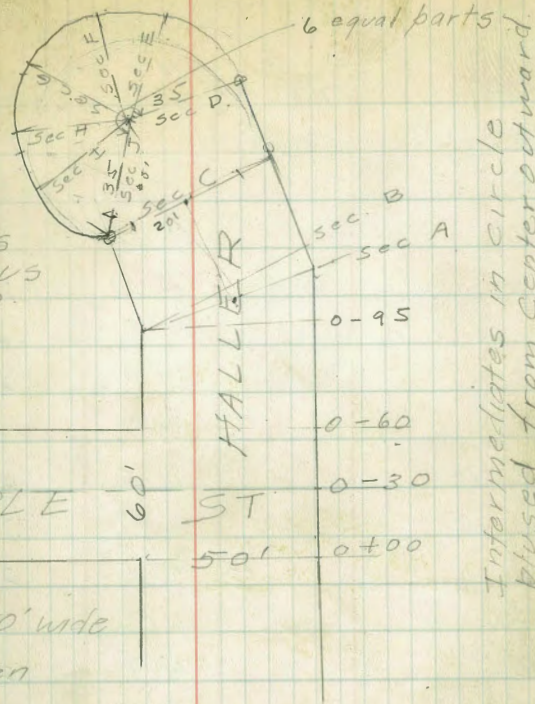
Plotted 8-7-28
C.B.H.

Sections
taken thus
on Banjo.

MAPLE 60' ST
50' 0+00

Haller 50' wide
Sec's taken
to 30' Roadway 10' cbs.

0-95	281.04		
\pm	4.9	276.1	
$\frac{1}{4}$	5.0	276.0	
cb	5.2	275.8	
+4	5.1	275.9	
W.L.	5.3	275.7	



Intermediates in circle
plotted from center outward.

Sec A	281.04		
w.l.		5.3	275.7
+5		5.2	275.8
cb		5.2	275.8
1/4		5.0	276.0
ϕ		4.8	276.2
1/4		4.7	276.3
cb		4.7	276.3
EL. L		4.5	276.5
Sec B			
EL		4.5	276.5
cb		4.7	276.3
1/4		4.7	276.3
ϕ		4.8	276.2
1/4		5.0	276.0
cb		5.2	275.8
w.l.		5.3	275.7
Sec C			
w.l.		5.0	276.0
+5		5.1	275.9
cb		4.9	276.1
1/4		4.7	276.3
ϕ		4.6	276.4
1/4		4.5	276.5
cb		4.6	276.4
EL		4.4	276.6

Sec D	281.04		
c		4.8	276.2
+65		4.6	276.4
+25		4.8	276.2
Line		4.4	276.6
Sec E			
c		4.8	276.2
+26		4.9	276.1
Line		4.7	276.3
Sec F			
c			
+10		5.0	276.0
+20		5.0	276.0
line		5.2	275.8
Sec G			
c			
+15		5.0	276.0
+25		5.5	275.5
line		5.5	275.5
Sec H			
c			
+14		5.1	275.9
+25		5.5	275.5
+30		5.3	275.7
line		5.5	275.5

Sec I	281.04		
c			
+25	5.4	275.6	
+27	5.0	276.0	
line	5.2	275.8	

Sec J			
c			
+10	4.9	276.1	
+25	5.1	275.9	
+30	4.9	276.1	
line	5.0	276.0	

0+00 = S.V. Maple			
w.L	6.9	274.1	
+5	6.8	274.2	
cb	6.8	274.2	
1/4	6.6	274.4	
ϕ	6.4	274.6	
1/4	6.2	276.8	
cb	6.2	276.8	
+3	6.0	275.0	
E.L.	5.7	275.3	

0+25			
E.L.	6.2	274.8	
+8	6.5	274.5	
cb	6.8	274.2	
1/4	6.5	274.5	
ϕ	6.9	274.1	

Haller

47

0+25	281.04		
w/4		7.2	273.8
cb		7.4	273.6
+1		7.2	273.8
w.L.		7.5	273.5

0+50			
w.L.		8.1	272.9
+6		8.0	273.0
cb		8.1	272.9
1/4		7.6	273.4
+3		7.4	273.6
ϕ		7.4	273.6
1/4		7.2	273.8
cb		7.2	273.8
+2		6.9	274.1
E.L.		6.7	274.3

0+75			
E.L.		7.1	273.9
+8		7.3	273.7
cb		7.7	273.3
1/4		7.7	273.3
ϕ		8.0	273.0
1/4		8.2	272.8
cb		8.8	272.2
+2		8.6	272.4
w.L.		8.8	272.2

1+00

281.04

w.L.	9.6	271.4
+8	9.0	272.0
cb.	9.2	271.8
1/4	8.7	272.3
1/4	8.7	272.3
1/4	8.5	272.5
cb	8.5	272.5
+2	8.1	272.9
E.L.	7.9	273.1

1+25

E.L.	8.7	272.3
+8	8.9	272.1
cb	9.1	271.9
1/4	9.0	272.0
+7	9.3	271.7
1/4	9.5	271.5
1/4	9.8	271.2
cb	10.2	270.8
w.L.	10.6	270.4

1+50

w.L.	11.6	269.4
+8	11.3	269.7
cb	11.4	269.6
+3	11.0	270.0
1/4	10.9	270.1

1+50

281.04

1/4	10.4	270.6
1/4	10.0	271.0
cb	10.2	270.8
+2	9.6	271.4
E.L.	9.4	271.6

1+75

E.L.	10.4	270.6
+9	10.7	270.1
cb	11.2	269.8
1/4	11.1	269.9
1/4	11.4	269.6
1/4	12.0	269.0
+6	12.2	268.8
cb	12.3	268.7
w.L.	12.8	268.7
T.P. 181	271.41	11.44 269.60

2+00

w.L.	4.3	267.1
cb	3.8	267.6
1/4	3.4	268.0
1/4	2.8	268.6
1/4	2.5	268.9
cb	2.4	269.0
+1	2.1	269.3
E.L.	1.6	269.8

2+25	271.41		
2 E.L.		2.3	269.1
cb		3.0	268.4
1/4		3.3	268.1
1/4		3.7	267.7
1/4		4.4	267.0
cb		5.0	266.4
+7		5.5	265.9
w.L.		6.2	265.2
2+50			
w.L.			
10'w		12.8	258.6
6'w		11.0	260.4
w.L.		8.2	263.2
+6		7.3	264.1
cb		6.1	265.3
1/4		5.5	265.9
1/4		4.9	266.5
1/4		4.3	267.1
cb		4.0	267.4
+1		3.6	267.8
E.L.		2.8	268.6

2+75	271.41		
E.L.		4.0	267.4
cb		4.9	266.5
1/4		5.2	266.2
1/4		5.9	265.5
+5		6.8	264.6
1/4		7.0	264.4
+5		7.4	264.0
cb		8.0	263.4
+3		8.6	262.8
+8		9.4	262.0
w.L.		10.2	261.2
10'w		15.0	256.4
3+00			
10'w		15.2	256.2
w.L.		12.2	259.2
+3		11.4	260.0
cb		9.9	261.5
1/4		8.3	263.1
1/4		7.2	264.2
1/4		6.2	265.2
cb		5.7	265.7
+5		5.1	266.3
E.L.		4.7	266.7

271.41 $\Delta 28^{\circ} 14' 10''$
 3 + 22¹⁶ = B.C. Curve Stations on outside
 15 equal parts

E.L.	5.5	265.9
cb	6.8	264.6
1/4	7.7	263.7
1/2	8.5	262.9
3/4	9.6	261.8
cb	12.1	259.3
w.L.	14.9	256.5
10' w	17.4	254.0
3 + 49 ²⁵		
25' w	24.5	246.9
20' w	22.6	248.8
5' w	19.0	252.4
4' w	18.4	253.0
w.L.	17.5	253.9
+2	16.0	255.4
cb	14.8	256.6
1/4	13.3	258.1
1/2	11.3	260.1
3/4	9.7	261.7
cb	8.5	262.9
E.L.	6.8	264.6

3 + 77²⁴ 271.41

E.L.	8.7	262.7
cb	10.5	260.9
1/4	12.3	258.1
1/2	14.6	256.8
3/4	16.9	254.5
cb	18.7	252.7
w.L.	22.7	248.7
12' w	28.6	242.8
14' w	30.2	241.2
26' w	36.0	235.4
30' w	38.2	233.2
T.P. 1.40	259.91	12.90 258.51
4 + 04 ⁹³		
35' w	36.5	223.4
30' w	32.6	227.3
w.L.	20.4	239.5
cb	15.8	244.1
1/4	12.7	247.2
1/2	8.7	251.2
+3	6.9	253.0
1/4	5.6	254.3
+4	4.7	255.2
cb	2.9	257.0
+5	1.5	258.4
E.L.	0.0	259.9

4+3252

259.91

10'E	2.2	257.7
E.L.	5.0	257.9
cb	8.8	251.1
1/4	12.1	247.8
1/2	16.0	243.9
3/4	19.1	250.8
cb	23.0	236.9
w.L.	28.0	231.9
16'w	34.8	225.1
31'w	44.9	215.0
T.P.	0.47	247.29
	13.09	246.82

4+60¹¹

24'w	36.3	211.0
6'w	24.0	223.3
w.L.	21.8	225.6
cb	17.9	229.6
1/4	14.0	233.3
1/2	9.5	237.8
3/4	6.7	240.6
cb	3.4	243.9
E.L.	+0.2	247.5
20'E	+9.8	265.1

Haller

51

4+8720

247.29

20'E	+1.3	248.6
E.L.	5.9	241.4
cb	11.1	236.2
1/4	14.6	232.7
1/2	18.5	228.8
3/4	22.3	225.0
cb	25.3	222.0
w.L.	29.8	217.6
24'w	41.7	205.6
50'w	56.1	191.2
T.P.	0.59	238.73
	7.15	238.14
5+15.29		
50'w	50.5	188.2
47'w	51.7	187.0
40'w	51.2	187.5
25'w	42.4	196.3
15'w	35.8	202.9
w.L.	28.17	210.6
cb	20.7	218.0
1/4	17.7	221.0
1/2	14.4	224.3
3/4	11.2	227.5
cb	6.7	232.0
E.L.	1.4	237.3
15'E	+5.2	243.9
25'E	+9.8	246.5

5+92⁸⁸ 238.73

20'E	+4.2	242.9
E.L.	5.7	233.0
cb	10.4	228.3
1/4	14.0	224.7
1/4	18.2	220.5
1/4	27.8	216.9
cb	27.3	211.4
w.l.	31.7	207.0
20'w	42.8	195.9
35'w	53.2	185.5
40'w	53.9	184.8
50'w	51.2	187.5
5+70 ²⁴		
50'w	49.1	189.6
35'w	56.6	182.1
30'w	55.4	183.3
20'w	47.8	190.9
w.l.	35.7	203.0
cb	29.1	209.6
1/4	44.6	214.1
1/4	19.1	219.6
1/4	14.5	224.2
cb	10.7	228.0
E.L.	5.6	233.1
11'E	+0.3	239.0
15'E	+3.1	241.8

Haller 52

5+70²⁴ 238.73

20'E	+4.3	243.0
5+98 ⁰⁶		
20'E	+2.1	240.8
10'E	1.4	237.3
T.P. 5.44	236.86	7.31
E.L.	4.8	232.0
cb	9.8	227.0
1/4	13.6	223.2
1/4	17.6	219.2
1/4	21.7	215.1
cb	25.9	211.0
w.l.	32.6	204.3
15'w	43.1	193.8
30'w	54.6	182.3
40'w	55.4	181.5
50'w	52.4	184.4
T.P. 1.71	233.13	
6+25 ⁶⁵		
50'w	57.7	175.4
43'w	54.9	178.2
25'w	37.4	195.7
w.l.	30.7	202.4
cb	24.7	208.4
1/4	20.8	212.3
1/4	17.2	215.9

6+25 ⁶⁵	233.13		
E 1/4	12.9	220.2	
cb	9.1	224.0	
E.L.	4.9	228.2	
20'E	+4.7	237.8	
T.P. 3.29	229.73	6.69	226.44 ✓
6+53 ²⁴			
20'E	+6.8	236.5	
E.L.	5.0	224.7	
cb	10.2	219.5	
1/4	14.7	215.0	
1/2	17.7	212.0	
1/4	23.9	205.9	
cb	28.2	201.5	
w.L.	33.7	196.0	
25'W	41.1	188.6	
35'W	53.1	176.6	
40'W	53.4	176.3	
50'W	50.4	179.3	
T.P. 0.22	226.66		226.44

6+80 ⁸³	226.66		
50'W	48.6	178.0	
30'W	52.9	173.7	
20'W	49.4	177.3	
w.L.	36.4	190.2	
cb	30.2	196.4	
1/4	25.6	201.0	
1/2	20.6	206.0	
1/4	15.7	211.0	
cb	10.9	215.8	
E.L.	4.5	222.1	
14'E	+3.5	230.2	
20'E	+7.7	234.4	
T.P. 1.26	227.70		226.44
7+08 ⁴²			
20'E	+6.3	234.0	
15'E	+4.5	232.2	
E.L.	4.7	223.0	
cb	10.7	217.0	
1/4	15.1	212.6	
1/2	20.0	207.7	
1/4	24.5	203.2	
cb	29.3	198.4	
w.L.	35.4	192.3	
20'W	48.6	179.1	
35'W	55.5	172.2	

7+08 ⁴²	227.20		
50'W	52.0	175.7	
T.P. 4.70	229.17	3.23	224.47
7+36 ¹²	P.C.C.	Curve station	outside
50'W	59.5	169.7	
45'W	59.7	169.5	
25'W	42.1	187.1	
13'W	39.7	189.5	
W.L.	32.4	196.8	
cb	26.3	202.9	
1/4	21.4	207.8	
ϕ	17.1	212.1	
1/4	13.2	216.0	
cb	9.6	219.6	
E.L.	4.9	224.3	
10'E	+0.4	229.6	
20'E	+3.9	233.1	
T.P. 4.35	230.58	2.94	226.23
7+62 ²⁸			
20'	+1.5	232.1	
10'E	0.5	230.1	
E.L.	4.6	226.0	
cb	9.7	220.9	
1/4	13.3	217.3	
ϕ	17.1	213.5	
1/4	21.0	209.6	

Haller

54

7+62 ²⁸	230.58		
cb	25.1	205.6	
W.L.	30.3	200.3	
20'W	41.8	188.8	
40'W	54.5	176.1	
50'W	60.0	170.6	
60'W	63.5	167.1	
T.P. 4.30	232.53		226.23 x
7+88 ⁴⁴			
60'W	59.1	173.4	
50'W	53.0	189.5	
30'W	42.4	190.1	
10'W	31.8	200.7	
W.L.	26.9	205.6	
cb	21.8	210.7	
1/4	18.3	214.2	
ϕ	15.2	217.3	
1/4	11.6	220.9	
cb	8.6	223.9	
+6	5.9	226.6	
E.L.	5.2	227.3	
10'E	3.4	229.3	
20'E	1.9	230.7	

8 + 14 ⁶⁰	232.53	
20'E	2.3	230.2
E.L.	5.6	226.9
cb	7.6	224.9
1/4	9.7	222.8
1/4	11.9	220.6
1/4	15.2	217.3
cb	18.3	214.2
w.L.	20.5	212.0
10'W	24.5	208.0
30'W	36.4	196.1
70'W	42.1	190.4
8 + 40 ²²		
30'W	39.5	193.0
18'W	33.5	199.0
w.L.	27.4	205.4
cb	22.6	209.9
1/4	20.3	212.2
1/4	17.7	214.8
1/4	14.7	217.8
cb	12.5	220.0
E.L.	9.8	222.7
20'E	4.6	227.9

Haller

232.53

55

8 + 66 ⁹³	P.R.C near Wabash	
20'E	7.6	224.9
10'E	11.8	220.7
E.L.	15.8	216.7
cb	20.2	212.3
1/4	22.3	210.2
+3	22.9	209.6
1/4	25.1	217.4
1/4	28.1	204.4
cb	31.9	200.6
w.L.	36.7	195.8
20'W	44.2	188.3
30'W	49.7	182.8
T.P. 12.98	245.11 0.20	232.33
T.P. 11.52	256.34 0.29	244.82
T.P. 12.99	268.99 0.34	256.00
T.P. 8.93	277.67 0.05	268.94
B.M Beginning	2.25	275.42

X-Sections Howard Str. from E.L. Arizona to
W.L. Oregon.

STA.	+	H.I.	-	Elev.
S.E. Curb B.P.				331.51
	13.24	344.75		
0+00 E.L. Arizona				
S. Curb Top			13.23	331.52
" Bot.			13.80	330.95
N. " Top			12.70	332.05
" Bot.			13.42	331.33
0+50				
S. Curb Top			8.71	336.04
N. " Top			8.12	336.63
1+00				
S. Curb Top			4.14	340.61
N. " Top			3.34	341.41
T.P.			0.33	344.42
	12.90	357.32		
1+40 W.L. Alley				
S. Curb Top			13.03	344.29
N. " Top			12.19	345.13
1+60 E.L. Alley				
N. Curb Top			10.09	347.23
S. " Top			10.95	346.37
2+00				
S. Curb Top			7.40	349.92
N. " Top			6.48	350.84

Plotted 7-27-28
C.B.H.

JAEGER } July 21st 1928.
Bailey }
Clavert }

357.32

56

STA.	+	H.I.	-	Elev.
2+50				
S. Curb Top			2.96	354.36
N. " Top			1.96	355.36
T.P.			0.81	356.51
	13.24	369.75		
3+10 W.L. Hamilton				
N. Curb Top			8.48	361.27
S. " Top			9.75	360.00
0+00 E.L. Hamilton				
S. Curb Top			8.11	361.64
N. " Top			6.72	363.03
0+50				
S. Curb Top			5.76	363.99
N. " Top			4.50	365.25
1+00				
S. Curb Top			3.35	366.40
N. " Top			2.35	367.40
1+50 W.L. Alley				
S. Curb Top			1.02	368.73
N. " Top			0.22	369.53
T.P.			0.39	369.36
	7.78	377.14		
1+70 E.L. Alley				
S. Curb Top			7.39	369.75
N. " Top			6.70	370.44

377.14

STA.	+	H.I.	-	Elev.
2+00				
S. Curb Top			6.53	370.61
N. " Top			5.88	371.26
2+50				
S. Curb Top			4.96	372.18
N. " Top			4.63	372.51
3+10 W.L. Oregon				
N. Curb Top			3.15	373.99
✓ Bott.			3.81	373.33
S. " Top			3.12	374.02
✓ Bott.			3.75	373.39
Howard from W.L. Arizona to E.L. Texas				
SE. Curb B.P.				331.51
	0.13	331.64		
S. Curb Howard				
0+00 W.L. Arizona				
Curb Top			2.15	329.49
" Bott.			2.82	328.82
0+50 Curb Top			4.06	327.58
+80 " "			5.27	326.37
+90 " "			5.75	325.89
1+10 " "			6.32	325.32
+40 E.L. Alley Curb Top			7.40	324.24
S.L. Arizona			7.23	324.41

331.64

57

STA	+	H.I.	-	Elev.
1+60 W.L. Alley				
S.L. Arizona Curb Top	8.02			323.62
S. Curb Top	8.18			323.46
2+00 Curb Top	9.80			321.84
2+50 "	11.69			319.95
3+00 Curb + Street E.L. Texas	13.56			318.08
North Curb Howard				
0+00 W.L. Arizona				
Curb Top	1.63			330.01
" Bott.	2.42			329.22
0+05 Curb Top	1.80			329.84
+37 " "	3.13			328.51
+50 " "	3.93			327.71
+80 " "	5.07			326.57
+96 " "	6.05			325.59
1+06 " "	5.92			325.72
1+40 E.L. Alley				
N. Curb Top	7.09			324.55
N.L. Arizona Curb Top	6.67			324.97
1+60 W.L. Alley				
N.L. Arizona Curb Top	7.71			323.93
N. Curb Top	8.04			323.60
2+00 Curb Top	9.72			321.92
+50 " "	11.65			319.99
3+00 Curb + Street E.L. Texas	13.61			318.03

Curb very bad
condition

7-25-28
S.C. Bliss
Flood
Route

Howard St. x sections - West Line Texas
west

STA	+	H.I.	-	Elev.
B.M. S.E. B.P. Texas + Howard				318.04
	+4.80			
				Σ 322.84
				0+00 = West Line Texas
North Top curb		6.82		316.02
Gutter		8.08		14.76
South Top curb		6.84		316.00
Gutter		7.90		314.94
				0+60
North Top curb		7.75		315.09
G		8.60		314.24
South Top curb		7.46		315.38
G		8.21		314.63
				0+79.40 - Over grading at Inlet on South
S Top curb		7.43		315.41
G		8.28		14.56
				0+89.30 - Over grading at inlet on North
N Top curb		7.88		314.96
G		8.72		314.12
				1+06
N Top curb		7.78		315.06
G		8.53		314.31
S Top curb		7.30		315.54
G		8.13		314.71

Note - Concrete gutter
on both sides of
Howard extends 160'
West to West Line of Alley

Σ 322.84

58

STA	+	H.I.	-	Elev.
				1+25
N Top curb				7.22
G				8.16
S Top curb				6.75
G				7.62
				1+40 - East Line Alley
N Top curb				6.61
G				7.45
S Top curb				6.13
G				6.97
				1+60 - West Line Alley
N Top curb				4.92
G				5.93
S Top curb				4.63
G				5.53
				1+95
N Top curb				1.82
S " "				1.76
T.R.				-0.40
				Σ 322.44
				1+920
				Σ 331.64
				2+50
N Top curb				5.37
S Top curb				5.84

π 33164

STA	+	H.I.	-	Elev.
3+00 = East Line Louisiana				
N Tp cb		0.66		330.98
G		1.36		330.29
S Tp cb		1.68		329.96
G		2.20		329.44
0+00 = West Line Louisiana				
N Tp cb		0.63		331.01
G		1.32		330.32
S Tp cb		0.66		330.98
G		1.34		330.30
0+50				
N Tp cb		2.66		328.98
S Tp cb		2.86		328.78
1+00				
N Tp cb		4.63		327.01
S Tp cb		5.05		326.59
1+40 = East Line Alley				
N Tp cb		6.04		325.60
S Tp cb		6.71		324.93
1+60 = West Line Alley				
N Tp cb		7.10		324.54
S Tp cb		7.76		323.88
2+00				
N Tp cb		8.68		322.96
S Tp cb		9.33		322.31

π 33164

59

STA	+	H.I.	-	Elev.
2+50				
N Tp cb		10.64		321.00
S Tp cb		11.52		320.12
Tp.		3100 =	-12.55	319.09
		+0.35		
π 319.44				
3+00 = East Line Mississippi				
N Tp cb		0.41		319.03
S Tp cb		1.43		318.01
0+00 = West Line Mississippi				
N Tp cb		2.49		316.95
S Tp cb		3.57		315.87
0+50				
N Tp cb		6.46		312.98
S Tp cb		7.68		311.76
1+00				
N Tp cb		10.51		308.93
S Tp cb		11.78		307.66
Tp.			-13.22	306.22
		+0.98		
π 307.20				
1+40 = East Line Alley				
N Tp cb		1.31		305.89
S Tp cb		2.78		304.42

π 307.20

1+60 = West Line Alley

N T p c b 3.19 304.01

S T p c b 4.60 302.60

2+00

N T p c b 6.26 300.94

S T p c b 7.83 299.37

2+50

N T p c b 10.22 296.98

S T p c b 11.93 295.27

T.P. -12.93 294.27

+1.56

π 295.83

3+00 = East Line Alabama

N T p c b 2.77 293.06

G 3.58 292.25

S T p c b 4.70 291.13

G 5.32 290.51

0+00 = West Line Alabama

N T p c b 3.81 292.02

G 4.61 291.22

S T p c b 5.80 290.03

G 6.52 289.31

0+50

N T p c b 4.22 291.61

S T p c b 6.06 289.77

π 295.83

60

1+00

N T p c b 4.70 291.13

S T p c b 6.36 289.47

1+40 = East Line Alley

N T p c b 4.92 290.91

S T p c b 6.51 289.32

1+60 = West Line Alley

N T p c b 5.23 290.60

S T p c b 6.32 289.51

2+00

N T p c b π 280.27 7.90 290.37

S T p c b 11.24 289.03

T.P. Spike in pole sta 2+50 -6.63 289.20

+11.07

π 300.27

2+50

N T p c b 10.30 289.97

S T p c b 11.60 288.67

3+10 = East Line Florida

N T p c b 10.68 289.59

Concrete gutter on N.E. cor 11.51 288.76

S T p c b 11.76 288.51

S.E. cb. inlet grating 12.52 287.75

0+00 = West Line Florida

N T p c b 9.78 290.49

S-concrete 10.53 289.64

S T p c b 10.75 289.52

G 11.53 288.74

Note: Concrete gutter
on both sides between
Florida & Georgia ✓

Σ 300.27

0750

N Tp cb	6.37	293.90
G	7.22	293.08
S Tp cb	6.33	293.94
G	7.14	293.13

1100

N Tp cb	2.91	297.36
G	3.73	296.54
S Tp cb	2.08	298.19
G	2.91	297.38

1115 BxK

N Tp cb	1.87	298.40
G	2.65	297.62
S. G. in Driveway	1.57	298.70
T.P.		-0.20 300.07

+12.04

Σ 312.11

1150 = East Line Alley

N Tp cb	10.62	301.49
G	11.42	300.69
S Tp cb	9.65	302.46
G	10.42	301.69

1170 = West Line Alley

N Tp cb	8.66	303.45
G	9.48	302.63
S Tp cb	7.61	304.50
G	8.49	303.62

Σ 312.11

61

1190

N Tp cb	6.96	305.15
G	7.74	304.37
S Tp cb	5.91	306.20
G	6.73	305.38

2125

N Tp cb	3.39	308.72
G	4.19	307.92
S Tp cb	2.51	309.60
G	3.30	308.81

2143

N Tp cb	1.36	310.75
G	2.16	309.95
S Tp cb	0.42	311.69
G	1.21	310.90

T.P.

-0.25 311.86

+13.11

Σ 324.97

2175

N Tp	10.62	314.35
G	11.42	1355
S Tp cb	9.72	315.25
G	10.48	1449

Note:
 Paving on
 Georgia is 15'
 short of property line
 on south side

π 324.97

Note - Concrete
 gutter from
 Georgia to Park Blvd

3410 = East Line Georgia St

N T p c b	675	318.22
G	7.58	317.39
S T p c b	5.74	319.23
G	6.53	318.44

0400 = West Line Georgia

N T p c b	5.20	319.87
G	5.66	319.31
S T p c b	4.13	320.84
G	4.83	320.04

0750

N T p c b	186	323.11
G	2.69	322.28
S T p c b	0.92	324.05
G	1.74	323.23

T.P.

-0.11 324.86

+11.80

π 336.66

1400

N T p c b	1023	326.43
G	11.06	325.60
S T p c b	7.45	327.21
G	10.26	326.40

1440.30 = East Line Alley on North

N T p c b	7.49	329.17
G	8.25	328.41

π 336.66

62

1439.80 = East Line Alley on South

S T p c b	7.05	329.61
G	7.85	328.81

1459.80 = West Line Alley on South

S T p c b	5.56	331.10
G	6.32	330.34

1460.30 = West Line Alley on North

N T p c b	6.03	330.63
G	6.85	329.81

2400

N T p c b	3.48	333.18
G	4.33	332.33

S T p c b	3.24	333.42
G	4.05	332.61

T.P.

-1.08 335.58

+9.32

π 344.90

2450

N T p c b	8.30	336.52
-----------	------	--------

G	9.18	335.72
---	------	--------

S T p c b	8.37	336.43
-----------	------	--------

G	9.20	335.7
---	------	-------

3400 = East Line Park Blvd

N T p c b	5.01	339.89
-----------	------	--------

G	5.60	339.21
---	------	--------

S T p c b	5.16	339.74
-----------	------	--------

G	5.70	339.20
---	------	--------

T 344.90

T.P.

- 3.96 340.94

+4.86 345.80

-6.30 339.50

+2.70 342.20

O.K. B.M. N.W. B.P. Polk Georgia -5.28 336.92

B.M. Elev 337.01

Paving Elevations @ Howard Park Blvd to Oregon

E Line Park Blvd

T 342.37 from Curb Notes Page 62 ^{Does not chk B.M. S.P. (N.W. Howard Georgia) 0.00 L.S.}

N. ch 2.48 339.89 chK

@ Howard 2.48 339.89 Payment

I.A. 0.49 329.93 12.93 329.44

W. Line Georgia

S. ch 9.09 320.84 chK

@ Howard 9.59 320.34 Payment

E Line Georgia

N. ch 11.70 318.23 = 318.22

@ Howard 11.50 318.45 Payment

B.M. B.P. 4.81 295.40 290.59

295.38 Taken from ch. Elev's Page 60

W. Line Alabama

N. ch 3.36 292.02 chK

@ Howard 4.46 290.92 Payment

E Line Alabama

N. ch 2.32 293.06 chK

@ Howard 3.37 292.01 Payment

W. Line Louisiana
T 335.02 From ch. Elev's Page 59

N. ch 4.01 331.01 chK

@ Howard 4.24 330.79 Payment

E. Line Louisiana

N. ch 4.04 330.98 chK

@ Howard 4.58 330.44 Payment

B.M. B.P. 2.68 W. Line Texas
X 320.69

N. ch 4.69 316.00 chK

@ Howard 4.60 316.09 Payment

E. Line Texas

S. ch 2.61 318.08 chK

@ Howard 2.59 318.10 Payment

B.M. 2.38 N. Line Arizona
T 323.89

N. ch 3.88 330.01 chK

@ Howard 4.15 329.74 Payment

E. Line Arizona

N. ch 1.84 332.05 chK

@ Howard 2.01 331.88 Payment

10' W of W. Line Hamilton = Wend Payment.
367.86 from ch. Elev's Page 56

S. Top ch 8.78 359.09

S. gutter 9.45 358.41 Payment

@ Howard 8.34 359.52 "

N. gutter 8.24 359.62 "

N. Top ch. 7.55 360.36

Continued on Page 77

36th St. Cross Sections
Woolman to National

60 H. de
10 Cb
10 Qls

64.93

8.32
Ston
No Hush
Piled
Leaky

64

BM	all	64.93	64.87	SF Top Hyd Woolman to 36th		62.5	62.4
		SL Woolman				8.3	
F		3.5	61.4			8.2	
Cb Top		3.07	61.89		150.5	1.7	63.2
Gutter on Pav		3.66				2.8	62.1
H		3.00				3.5	
S		2.70	62.23			3.1	
H		2.55				3.7	
Gutter on Pav		2.74				3.3	61.6
Cb on Top		2.06	62.87			3.4	
H		1.7	63.2			3.4	
		12.54 of SL Woolman				3.5	61.4
H		1.7	63.2		100.5		
Cb		2.1				4.1	60.3
H		2.5				5.1	
S		2.6	62.3			5.5	
H		2.6				5.7	59.2
Cb		2.7				5.8	
H		3.3				6.0	
F		3.5	61.4			6.6	58.3
		150.5			150.5		
F		3.2	61.7			9.6	55.7
H		2.1				8.1	
Cb		1.8				8.8	
H		2.4				8.8	56.1

Plotted 8-29-28
C.B.H.

6493

1/4		8.4	
cb		7.8	
F		7.4	57.5
	183'S		
F		11.8	53.1
cb		11.3	
1/4		11.9	
z		11.1	53.8
1/4		10.9	
cb		10.8	
H		10.3	54.6
	200'S		
H		11.5	53.4
cb		12.3	
1/4		12.5	
z		12.3	52.6
1/4		12.4	
cb		12.9	
F		14.2	50.7
+10		15.2	
TP	0.37	12.46	52.17
	225'		
-10		7.7	
F		5.7	47.1
cb		5.6	
1/4		3.1	

5281

65

z		2.7	50.1
1/4		2.5	
cb		2.3	
+7		1.9	
H		1.2	51.6
	250'S		
H		2.1	50.2
+3		3.6	
cb		3.9	
1/4		4.4	
z		4.9	47.9
1/4		5.3	
cb		6.5	
F		8.8	44.0
+10		10.8	
	275'S		
-10		11.5	
F		10.2	42.5
+7		8.8	
cb		8.4	
1/4		7.4	
z		6.7	46.1
1/4		5.8	
cb		5.0	
+7		4.4	
H		3.4	49.4

5287

300'S

N	3.3	49.5
cb	6.0	
1/4	7.1	
1/2	8.3	44.5
3/4	9.3	
cb	9.9	
1.5	10.2	
F	12.9	39.9
11.0	12.5	

325'S

-1.0	13.3	
F	13.7	39.1
1.5	12.4	
cb	12.0	
1/4	11.5	
1/2	10.9	41.9
3/4	9.5	
cb	8.9	
N	6.0	46.8

350'S

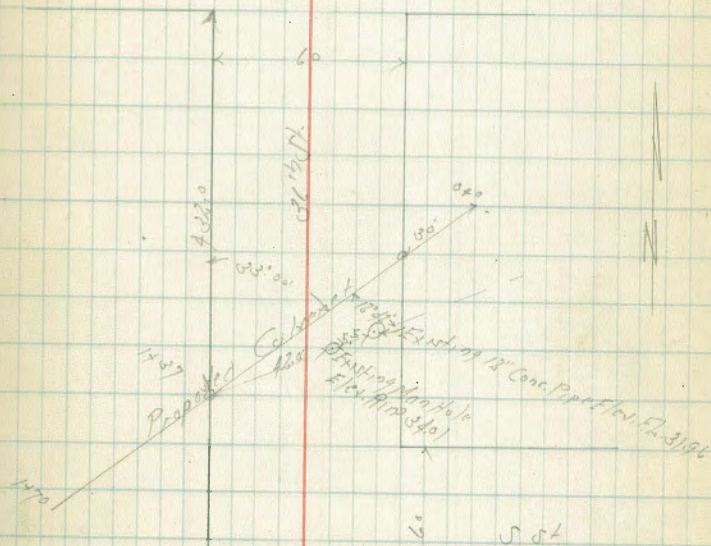
N	9.9	42.9
cb	12.4	
1/4	13.0	
1/2	14.0	37.8
3/4	14.3	

5284

66

cb	14.1	
1.5	14.0	
F	16.1	36.7
11.0	14.1	
TP	13.5	41.22
		12.97
		39.87

Proposed Culvert 36th St + S of
Hosmer Ave



361657

41.22

Levels For Proposed Drain

070	1.2
+30 - 5231 ^{1/2}	2.9
+50	3.1
+80	5.3
+10	7.8
+25	7.1
+37 1/2 X 236 ^{1/2}	10.2
+70	10.5

375 S of S 2 X 10/1007

-10	1.9	
F	2.7	38.5
+3	4.3	
cb	4.2	
1/4	4.2	
2	4.7	36.5
1/4	4.8	
cb	4.6	
+5	4.2	
X	2.7	38.5
+10	11	

400 S

-10	4.7	
X	5.4	35.8
cb	6.2	
1/4	7.3	

41.22

67

+6	7.7	
+8	9.2	
2	9.6	31.6
+3	9.1	
+8	5.7	
1/4	4.9	
cb	4.6	
+8	4.3	
F	3.0	38.2
+10	1.4	

428 S

-10	0.0	
F	1.3	39.9
+3	2.9	
cb	3.6	
1/4	3.9	
+2	4.2	
2	6.9	34.3
1/4	7.3	
+7	8.0	
cb	9.3	
+8	10.1	
X	7.3	33.9
+15	7.5	

4334 S - N 2 S 1/4 From E on

-20	7.8	
-----	-----	--

-13		7.5	
-8		10.3	
-2		9.7	
H		8.0	33.2
cb		7.1	
1/4		7.1	
+5		6.2	
2		5.0	36.2
+7		2.8	
1/4		2.1	
cb		2.1	
18		1.3	
F		0.4	40.8
P	359	0.20	41.02
	X Cb of S W		
F or Cb Top End		1.72	42.89
cb		4.2	
1/4		5.0	
2		7.1	36.5
1/4		10.3	
cb		11.1	
H		10.7	32.9
+9		11.0	
+12		13.7	
+20		12.1	
+25		11.3	

S of 60' high
10 Cb
10.24

2551			
-20		11.6	
H		11.2	33.4
cb		9.3	
1/4		8.0	
2		5.4	39.2
1/4		3.1	
cb		2.3	
F		1.0	43.6
	S Cb of S W		
F or F or Cb		0.82	43.79
cb		1.9	
1/4		2.7	
2		4.3	40.3
1/4		6.7	
cb		8.8	
H		10.2	34.4
-120		12.1	
	S-L 50'		
-20		12.4	
H		10.3	34.3
cb		8.4	
1/4		6.2	
2		4.0	40.6
1/4		2.9	
cb		2.1	

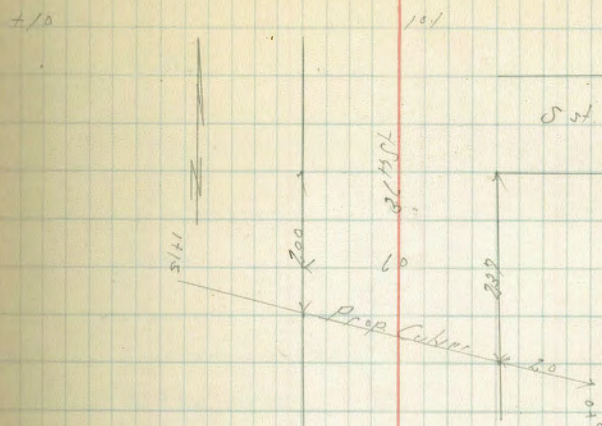
✓ Fixing M.H.
2.26 + 19.50
17.25
0.67 = 37.97

F	0.7	43.9
250 g / 5.2.0.51		
F	1.8	42.8
L	2.8	
cb	3.3	
1/4	3.9	
L	5.2	39.9
1/4	7.0	
cb	8.5	
H	9.4	35.2
+20	12.8	
50.5		
-20	7.2	
-5	7.1	
H	8.6	36.0
+5	8.5	
+5	6.3	
cb	6.8	
1/4	6.1	
L	5.7	38.9
1/4	4.0	
cb	3.1	
F	2.2	42.4
75.5		
F	0.7	43.9
+8	2.1	

cb		2.3	
1/4		2.6	
L		3.3	41.3
1/4		3.8	
cb		3.8	
H		4.3	40.3
+10		4.8	
TP	277	47.26	5.02
100.5			
H		4.8	42.6
cb		4.3	
1/4		3.5	
L		2.8	44.6
1/4		2.2	
cb		2.1	
+8		1.9	
F		0.7	46.7
125.5			
F		2.4	45.0
cb		2.8	
1/4		3.4	
L		4.2	43.2
1/4		4.9	
cb		5.8	
H		6.5	40.9
150.5			

on 10/1/63
1+3.2
11.5

-10		11.0	
H		10.5	36.8
cb		9.6	
1/4		8.8	
3/8		8.0	39.4
1/2		6.8	
cb		6.2	
F		6.1	41.3
	175°S		
F		9.1	38.3
cb		9.5	
1/4		10.0	
3/8		11.0	36.4
1/2		12.8	
cb		13.0	
H		14.0	33.4
+10		14.6	
	200°S		
-20		19.4	
H		17.2	30.2
cb		17.2	
1/4		16.8	
3/8		16.5	30.9
1/2		13.0	
cb		11.8	
F		11.0	36.4



Levels For Prepared Culvert

0 x 0	14.8
+10	13.1
+20 = F.L. of 36' 1/2" S	14.0
+30	11.8
+50	13.3
+90 = H.L. of 36' 1/2" S	17.3
+115	17.9

225°S

-10	12.1	
F	12.3	35.1
+8	12.9	
cb	15.3	
+5	12.1	
1/4	12.0	
3/8	12.1	35.3
1/2	11.3	

36.65

77.36

Cb	11.4	
X	11.4	36.0
+10	11.4	
	250.5	
-10	5.0	
X	4.8	42.6
Cb	5.5	
1/4	6.7	
1/2	8.4	39.0
1/4	9.2	
Cb	9.5	
F	11.0	36.4
+10	13.2	
+20	14.7	
	275.5	
-20	11.8	
F	8.8	39.2
Cb	6.7	
1/4	6.4	
1/2	5.5	41.9
1/4	4.0	
Cb	3.2	
X	3.1	44.3
	500.5	
X	3.9	43.5
Cb	2.3	

47.36

71

1/4	1.7	
1/2	2.0	45.4
1/4	3.1	
1/4	3.1	
Cb	3.2	
F	3.8	43.6
+10	5.1	
1/2	10.94	57.76
	325.5	46.82
F	10.9	46.9
Cb	10.6	
1/4	10.3	
+7	10.5	
1/2	10.0	47.8
1/4	10.4	
Cb	11.5	
X	13.2	44.6
+10	15.1	
	350.5	
-10	15.5	
X	18.0	45.8
Cb	10.7	
1/4	9.6	
1/2	8.6	48.2
1/4	8.4	
Cb	8.3	

5776

F	8.5	49.3
	8.75V	
F	7.4	50.4
Cb	7.3	
1/4	7.5	
1/4	8.0	49.8
1/4	8.1	
Cb	9.6	
H	11.0	46.8
+10	12.3	
	400S	
-10	11.7	
H	10.3	47.6
Cb	9.1	
1/4	7.8	
1/4	6.6	51.2
1/4	5.6	
Cb	5.3	
F	5.5	52.3
	425S	
F	4.5	53.3
Cb	4.7	
1/4	5.0	
1/4	6.3	51.5
1/4	7.5	
Cb	8.9	

5776

H	9.8	48.0
+10	10.4	
	450S	
H	8.0	49.8
Cb	8.0	
+5	6.7	
1/4	6.0	
1/4	5.2	52.5
1/4	5.2	
Cb	4.8	
F	4.2	53.6
	420S	
F	4.1	53.7
Cb	4.5	
1/4	4.9	
1/4	5.6	53.2
1/4	5.4	
Cb	5.7	
H	6.6	51.2
	+11 - Conc. Cb on Tap Circle Dr. via 70' Halpint Hand H's on 540'S	52.3 ✓
	-15 - Conc. Cb on Tap Circle Dr	53.06 ✓
H	6.2°	51.6
+5	5.2	
Cb	5.3	
1/4	5.4	

2	50	52.5
1/4	45	
cb	42	
F	31	54.0
575'S		
F	27	55.1
cb	30	
1/4	32	
2	41	53.7
1/4	47	
cb	52	
H	52	52.0
550'S		
H	55	52.3
cb	44	
1/4	42	
2	39	54.5
1/4	27	
cb	19	
F	15	56.3
600'S		
F	14	55.4
cb	25	
1/4	30	
2	35	54.3
1/4	37	

cb	36	
H	41	53.7
650'S		
H	30	54.8
cb	29	
1/4	29	
2	23	55.5
1/4	22	
cb	22	
F	19	55.9
700'S		
F	18	56.6
cb	15	
1/4	16	
2	17	56.1
1/4	16	
cb	16	
H	22	55.5
F	23	58.1
750'S		
-12	18.5	56.50
= Co. c. 607 Top Circle Dr. 20 ft. 100 ft. Hand Horse		
H	34	56.96
cb	32	55.4
1/4	33	
2	34	55.4
1/4	31	

5881

Cb	2.0		
F	2.9	55.9	793'S of 31' 30" Existing MH
			333.0087
			5948
F	3.3	55.5	
Cb	3.1		842'S of E.L. = Core Walk
1/1	3.1		3.78 55.02
2	3.8	55.0	
1/1	4.3		
Cb	4.4		
1/1	4.2	54.6	
			850'S
1/1	5.2	53.0	
1/1	7.1		
1.5	6.0		
Cb	6.1		
1/1	6.0		
2	4.9	53.9	
1/1	4.5		
Cb	4.2		
F	4.5	54.3	
			900'S
F	6.5	52.3	
Cb	6.4		
1/1	7.0		
2	7.6	51.2	
1/1	8.4		

5881

74

Cb	8.5		
1.5	8.6		
1/1	9.4		
1/1	8.0	50.8	
			943.30 = N.L. Log 02
1/1	9.4	49.4	Log 02
2	9.4		80' wide 11' Cb 18' 9" H
1/1	9.7		
2	8.6	50.2	
1/1	8.2		
Cb	8.4		
F	8.6	50.2	
			N Cb of Log 02
F as Cb	8.75	50.6	
Ground	9.3	49.5	
Cb	9.3		
1/1	8.9		
2	9.0	49.8	
1/1	9.6		
Cb	10.3		
1/1	10.3	48.5	
			2 of Log 02
1/1	11.1	47.7	
Cb	11.4		
1/1	11.4		
2	11.2	47.6	

5881

1/4		99	
cb		101	
F		97	49.1
	S. of Logan		
F on Endless Ground		981	4900
cb		102	
1/4		117	
2		128	46.0
1/4		128	
cb		127	
N		117	47.1
TP	145	4971	1055
			4826
	S. of Logan		
N		36	46.1
cb		39	
1/4		38	
2		37	46.0
1/4		24	
45		15	
cb		14	
F		09	45.8
	S. of S. Logan		
F		24	47.3
cb		24	
1/4		17	
43		22	

4971

2		39	45.8
1/4		39	
cb		39	
N		30	46.7
	50'S		
N		29	46.8
cb		45	
75		52	
17		31	
1/4		32	
2		32	46.5
1/4		37	
cb		39	
F		40	45.7
	75'S		
F		55	44.2
cb		54	
1/4		49	
2		40	45.7
1/4		19	
43		53	
75		68	
cb		63	
N		51	44.6
	100'S		
N		59	43.8

4971

cb	68	
1/4	69	
1/6	66	
2	53	44.4
1/4	62	
cb	68	
F	68	42.9

125°S

F	75	42.2
cb	77	
1/4	74	✓
2	80	41.7
1/4	74	
cb	67	
H	56	41.1

150°S

H	68	42.9
cb	76	
1/4	87	
2 - Existing MH on Riv	81	41.10
2 Ground	94	40.3
1/4	87	
cb	91	
F	95	40.2

175°S

F	103	39.4
---	-----	------

4971

76

cb	106	
1/4	95	
1/7	96	
2	106	39.1
1/2	94	
1/4	88	
cb	77	
H	67	43.0

200°S

H	55	44.2
15	69	
cb	75	
1/4	89	
2	109	38.8
1/4	102	
cb	110	
F	108	38.9

225°S

F	107	39.0
cb	113	
1/4	110	
2	106	39.1
1/2	101	
cb	90	
H	73	42.4

250°S

36th St.

4971

N	72	42.5	
Cb	84		
1/4	95		
1/2	107	39.0	
1/4	110		
Cb	120		
1/2	116		
F	109	38.8	
	500 S 002 399 S 021 = 1/4 National		
F	117	38.0	
Cb Top End Palan	1185	37.86	
Gutter on Pavlog	1235		
1/4 " "	1156		
1/2 " "	1095	38.76	
1/4 " "	1070		
Gutter " "	1068		
Cb Top End Palan	981	39.90	
N	85		
BM	1271	36.97	SFBP National 36 3698

Howard Ave Pavim Elevations
Park Blvd To Oregon
Continued from Page 63

77

T 367.86 from ch elev's Page 56

10' E. of E. line Hamilton = E. line Paving

N. ch. Top	4.41	363.45	ment
N. gutter	5.12	362.74	Pavment
E. Hamilton	5.38	362.48	"
S. gutter	6.47	361.39	"
S. ch. Top	5.76	362.10	

W. line Oregon

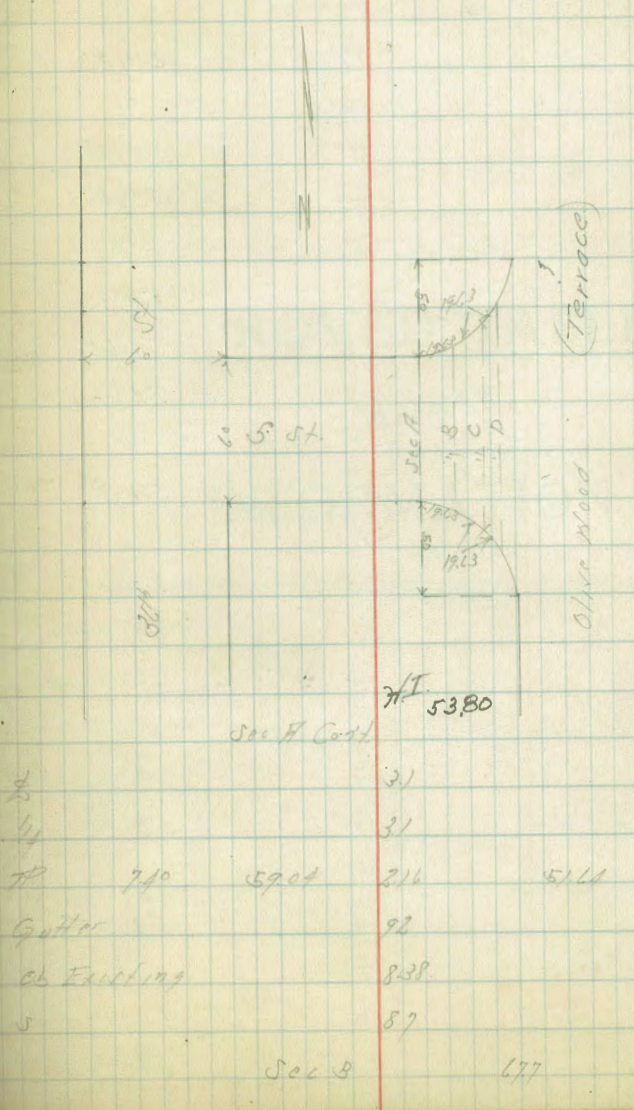
T 378.00 from ch elev's Page 57

S. ch	3.98	374.02	eAK
E. Howard	4.11	372.86	pavment
N. ch	4.01	373.99	eAK

S. St. Cross Sections
36th St to Olive Wood

60 wide.
10065
1021r

BM	12.78	53.80	41.02	101 NE Corner Post S 52 + 36th St.
	FL 36th St.			
H	12.8		41.0	
Cb. of End	10.91		42.89	
Gutter	11.3		42.5	
"	10.9			
S	10.2		43.6	
"	10.1			
Gutter	10.7		43.1	
Cb. of End	10.02		43.78	
S	9.9		43.9	
	15' F. of FL 36th St.			
S	6.2		47.6	
Cb. Existing	6.29		47.41	
Gutter	7.8		46.6	
"	6.6			
S	6.3		47.5	
"	6.6			
Cb. Existing & Ground	6.68		47.12	
H	7.2		46.6	
	50' F. - RC Sec 4			
H	2.3		51.5	
Cb. Existing	2.7		51.13	
Gutter	2.8		51.0	
"	3.1			



		53.80		
	Sec 4 Cont.			
S		31		50.7
"		31		
H	7.10	59.04	216	51.11
Gutter		92		49.8
Cb. Existing		8.38		51.06
S		8.7		50.3
				Cb 11.3
	Sec 8		677	47.11.3

14.94
60

13.52

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1% to 1%. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body

of table in same row and column gives distance from side stake to slope stake. If ground is not

IMPROVED TABLES
AND
INFORMATION

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given I may be found by dividing tangent (or external), opposite I by given tangent (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

59.04

S		65	52.5
Cb Existing		613	52.91
Gutter		69	52.1
"		65	
"		63	52.7
"		65	
Cb Existing Ground		593	53.11
"		54	53.6
"		54	53.148
	Sec C	893	51.149
"		42	54.8
Cb Existing		439	54.65
Gutter		50	54.0
"		49	
"		47	54.3
"		54	
"		60	53.0
Gutter		528	53.75
Cb Existing		54	53.6
"		54	53.703
	Sec D	1220	94.203
"		50	54.0
"		510	53.94
Cb Existing & Gutter		48	
"		43	54.7
"		42	
"		45	54.5
Gutter		418	54.86
Cb Existing		39	55.1

ENGINEERING DEPARTMENT,
CITY OF SAN DIEGO,
CALIFORNIA.