

1263

PASTS

FIELD BOOK

No. 385F

MICROFILMED

DEC 22 1964

$$\begin{array}{r}
 99055 \\
 285 \\
 \hline
 495275 \\
 772440 \\
 \hline
 693385 \\
 77758195
 \end{array}$$

$$\begin{array}{r}
 39324 \\
 46.62
 \end{array}$$

$$\begin{array}{r}
 33 \\
 28.2 \\
 46.62 \\
 \hline
 74.82
 \end{array}$$

$$\begin{array}{r}
 751.00 \\
 95.19 \\
 12 \\
 \hline
 858.19 \\
 9.12 \\
 \hline
 854.07
 \end{array}$$

$$\begin{array}{r}
 87673 \\
 72 \\
 \hline
 175346 \\
 613711 \\
 \hline
 6312456 \\
 7038 \\
 726
 \end{array}$$

500
246
54

ENGINEERING DEPARTMENT, CITY OF SAN DIEGO, CALIFORNIA.

Our Leather Bound Engineers Note Books are carried in the following rulings:

- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
- No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.
- No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.
- No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

We also carry the Note Books listed above, bound in extra strong Fabri-Hide (otherwise the same quality of book), which can be furnished at a somewhat lower price.

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THE FREDERICK POST CO.
ENGINEERING and DRAFTING SUPPLIES
IRVING PARK STATION
CHICAGO, ILL.

6 th St Sewers	4-14
X Sec Alleys B1Ks B1 & B4	
Sub of Lots 48-49-50 Fleischer's Add	15-19
X sec Lewis St Hawkto Bald Finch	20-21
X sec Tslinair	22-31
" " SANTA CRUZ. Santa Barbar. Ebers	32-62
" " CORONADO " " Guizot	63-69
" " " Ebers " "	70-

cont in Book 1279.

Hayler
H. McCarty
Kelly

6-12-28

1

Brass Plug in Curb
B.M. West Cor Rosecrans and Carleton.

	0.29	14.84	14.55	
	0.89	5.62	10.11	4.73
			6.36	-0.74
				-4.74
0+00			8.6	-3.0
+20			9.2	-3.6
+22			8.0	-2.4
+60			6.9	-1.3
+87			9.8	-4.2
1+00			9.74	-4.12
			10.8	-5.2
+25			9.86	-4.24
				-6.2
+50			9.93	-4.31
				-6.7
+75			10.08	-4.46
				-7.1
2+00			10.14	-4.52
				-7.4
+25			10.26	-4.64
				-7.8
+50			10.30	-4.68
				-8.5
+75			10.32	-4.76
				-9.4

Top of Manhole Shaffer + Carleton

Invert "

Ground at Manhole

Ground

"

"

Ground + Top of 10" G.I. Pipe (Beginning of G.I. Pipe)

Top of Pipe

Ground

Top of Pipe

Ground

Top of Pipe

Ground

Top of Pipe

Ground

Top of Pipe

Ground

Top of Pipe

Ground

Top of Pipe

Ground

Top of Pipe

Ground

ENGINEERING DEPARTMENT,
CITY OF SAN DIEGO,
CALIFORNIA.

5.62

3+00	10.52	-4.70		Top of Pipe
		-10.6	-5.7	Ground
+25	10.67	-5.05		Top of Pipe
		-11.5	-6.5	Ground
+50	10.69	-5.07		Top of Pipe
		-12.1	-7.0	Ground
+75	10.83	-5.21		Top of Pipe
		-12.2	-7.0	Ground
4+00	10.73	-5.11		Top of Pipe
		-12.5	-7.4	Ground
+05	10.70	-5.08		Top of Pipe at end of existing outfall.
		-12.6	-7.5	Ground
Soundings	-5.08 1.50 <u>-6.58</u>	-6.58		Elev of Gunwale of skiff

Set up at Sta 1+00 of Outfall.
F.S. on end of Outfall. Turned 70°00' R
Sta. 4+00 BS on 1+00 of Outfall.

0+00 = & Scott and & Shafter

		-6.58	-1.55	-5.08
4+05	44°03'			-12.6
4+33	47°32'		4.2	-10.8
4+60	49°40'		4.5	-11.1
4+73	52°08'		4.5	-11.1
5+15	56°31'		4.3	-10.5
5+85	62°50'		3.3	-9.9
6+64	68°39'		3.6	-10.2
6+92	70°28'		5.1	-11.7
7+63	74°28'		4.6	-11.2
8+55	78°43'		6.0	-12.6
9+53	82°19'		8.6	-15.2
10+24	84°29'		11.0	-17.6
11+19	86°55'		13.0	-17.6
12+18	89°02'		15.0	-21.6

Gunwale of Skiff.
End of Outfall.

July 19-20

Luten
Fell
Morgan

Island and Hoitt S.W. Plug in Mon.

~~106.06~~

2.21	130.21		128.00
6.43	126.64	10.00	120.21
		10.78	115.86

sw. Dodson
and island

4.73 132.73 128.00

& Dodson
& Island

4.1 128.6

N.L. Island = 0+00

3.4 129.3

+ 50 2.6 130.1

1+00 1.4 131.3

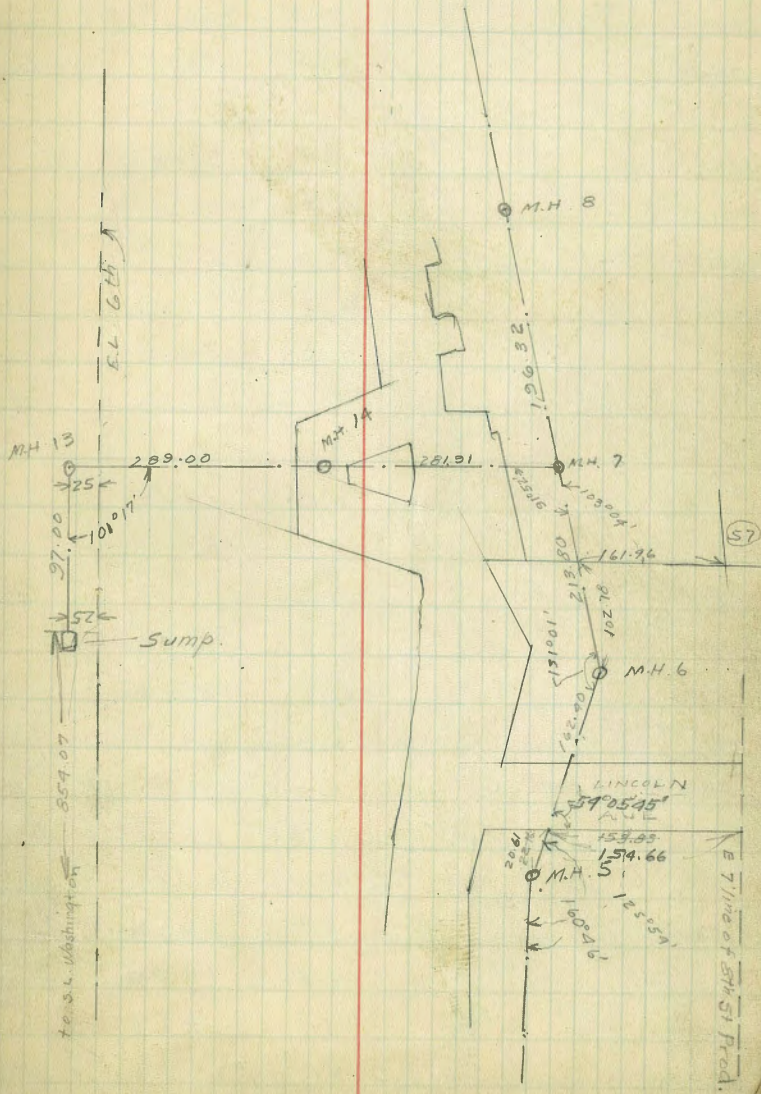
1+50 0.3 132.4

2+00 0.4 132.3

2+50 0.3 132.4

3+00 s.L. Market 134.00

M.H. 5 160.58



M.H. 6 to M.H. 7

150.73

0+50	5.6	
0+52	7.3	143.4
0+55	6.1	144.6
0+68	6.1	144.6
0+81	6.8	143.9
0+83	10.1	140.6
0+95	10.1	140.6
0+96	7.5	143.2
1+00	7.0	143.7
1+15	7.9	142.8
1+34	8.9	141.8
1+65	10.3	140.4
1+68	10.6	140.1
1+72	12.3	138.4
1+80	13.3	137.4
1+82	11.1	139.6
2+00	12.2	138.5
T.P. 2.55	140.65	12.63 138.10
2+13 ⁸⁰ = M.H. 7	3.52	137.13
M.H. 7 to M.H. 8 0+00 = M.H. 7		
0+05	4.5	136.1
0+17	5.0	135.6
0+40	5.7	134.9
0+41	4.9	135.7
0+47	4.9	135.7
0+60	4.2	136.4

Plotted

140.32

6

140.65

0+76	4.7	135.9
1+00	5.9	134.7
1+28	7.3	133.3
1+50	7.7	132.9
1+65	8.3	132.3
1+96 ³² = M.H. 8	9.12	131.53

M.H. 8 to M.H. 9 0+00 = M.H. 8

0+25	9.8	130.8
0+42	9.8	130.8
0+55	10.5	130.1
0+70	11.5	129.1
0+72	11.9	128.7
0+74	13.8	126.8
0+79	11.7	128.9
0+85	12.1	127.5
0+90	14.8	125.8
0+92	12.1	128.5
T.P. 1.04	129.66	12.03 128.62
0+95	1.4	128.3
1+00	3.8	125.9
1+03	4.5	125.2
1+30	5.3	124.4
1+45	5.9	123.6
1+52	4.8	124.9
1+60	4.0	125.7

Plotted

M.H. 8 to M.H. 9

129.66

1+70	5.0	124.7
2+00	4.3	125.4
2+27	6.4	123.3
2+40 = M.H. 9	7.5	122.2
M.H. 9 to M.H. 10	0+00 = M.H. 9	
0+02	8.7	121.0
0+05	9.3	120.4
0+25	9.9	119.8
0+30	9.6	120.1
0+45	9.6	120.1
0+47	11.8	117.9
0+55	13.3	116.4
0+60	12.8	116.9
0+61	10.5	119.2
0+70	10.9	118.8
0+80	10.1	119.6
1+20	11.5	118.2
1+35	11.6	118.1
1+65	12.8	116.9
T.P. 2.30	119.25	12.71 116.95
1+90	3.3	115.9
2+05	4.6	114.6
2+40 ⁰² = M.H. 10	6.0	113.2

Plotted

7

179.25

M.H. 10	to	M.H. 11	0+00 = M.H. 10
0+10		6.7	112.5
0+11		8.1	111.1
0+15		9.0	110.2
0+16		9.9	109.3
0+20		10.0	109.2
0+21		7.7	111.5
0+23		7.6	111.6
0+33		8.1	111.1
0+40		9.5	109.7
0+50		10.9	108.3
0+51		13.6	106.6
0+58		12.8	106.4
0+60		10.8	108.4
0+70		10.4	108.8
0+90		11.3	107.9
1+05		12.3	106.9
1+10		14.4	104.8
1+12		14.6	104.6
1+20		12.6	106.6
T.P. 2.49	109.40	12.34	106.91
1+55		4.7	104.7
1+70		6.1	103.3
1+82		5.1	104.3
2+00		4.5	104.9
2+32		5.5	103.9

Plotted

M.H. 10 to M.H. 11

109.40

2+64 ⁰⁴ = M.H. 11		7.13	102.27
T.P. 12.91	119.82	2.49	106.91
T.P. 12.27	131.79	0.30	119.52
T.P. 12.33	142.97	1.15	130.64
T.P. 11.03	153.04	0.96	142.01
T.P. 11.32	162.32	2.04	151.00
M.H. 5		1.76	160.56 (160.58)

M.H. 11 to M.H. 12 0+00 = M.H. 11

M.H. 11	1.65	103.83	102.28
0+24		3.2	100.7
0+31		2.7	101.2
0+48		2.7	101.2
0+58		3.0	100.9
0+71		3.9	100.0
0+77		3.6	100.3
1+00		4.7	99.2
1+17 ²⁰ = M.H. 12		5.32	98.61

M.H. 12 to M.H. #90 Oldtown Sewer
0+00 = M.H. 12

0+28		6.1	97.8
0+29		7.5	96.4
0+31		7.6	96.3
0+32		6.3	97.6
0+40		5.7	98.2
0+57		6.4	97.5
0+87		7.4	96.5

Plotted

103.93

1+00		7.7	96.2
1+27		9.0	94.9
1+56		9.8	94.1
1+76 = M.H. #90 ^{Oldtown} Sewer		10.61	93.32

Profile 6th St Sewers
Jump to M.H. 13 (500 PA)

B.M.	2.03	287.05		284.02
T.P.	4.90	290.09	1.86	285.19
T.P.	0.11	277.44	12.76	277.33
T.P.	0.11	264.79	12.76	264.68
B.M.	S.W. cor. Sump.		7.02	257.77
T.P.	0.21	252.54	12.46	252.33
0+00	= N side of Sump		5.2	247.3
0+03			5.5	247.0
0+03.5			7.0	245.5
0+08			7.8	244.7
0+09			9.1	243.4
0+13			9.3	243.0
0+14			11.1	241.4
0+16			11.2	241.3
0+17			12.5	239.0
0+20			13.0	239.5
T.P.	1.11	241.28	12.37	240.17
0+22			5.0	236.3
0+30			4.7	236.6
0+31			6.6	234.7
0+31			6.6	234.7
0+34			8.6	232.7
0+42			9.2	232.1
0+47			13.8	227.5
T.P.	0.54	229.74	12.08	229.20

SW
500
Washington

El Bottom of
Sump. 245.20

Jump to M.H. 13

				229.74
0+49			3.0	226.7
0+55			8.7	221.0
0+56			9.9	219.8
0+58			13.4	216.3
T.P.	0.73	218.73	11.79	217.95
0+67			4.4	214.3
0+72			6.5	212.2
0+79			8.9	209.8
0+81			11.0	207.7
T.P.	0.09	206.01	12.81	205.92
0+97	= M.H. 13		6.0	200.0
	M.H. 13 to M.H. 14		0+00	= M.H. 13
0+08			8.0	198.0
0+13			11.9	194.1
T.P.	0.42	193.94	12.49	193.52
0+19			3.9	190.0
0+23			4.8	189.1
0+25			7.6	186.3
0+30			7.4	186.5
0+31			6.2	187.7
0+50			5.8	188.1
0+55			7.5	186.4
0+71			9.4	184.5
0+76			10.3	183.6
0+94			10.7	183.2

Plotted

19394				
1+00		10.0	183.9	
1+08		8.9	185.0	
1+16		9.3	184.6	
1+24		11.0	182.9	
1+30		13.5	180.4	
T.P.	2.17	184.50	12.61	182.33
1+36		4.7	179.8	
1+50		5.1	179.4	
1+54		6.5	178.0	
1+59		6.4	178.1	
1+70		7.6	176.9	
1+77		7.3	177.2	
1+90		8.2	176.3	
2+06		9.0	175.5	
2+07		7.9	176.6	
2+14		8.3	176.2	
2+15		9.2	175.8	
2+25		9.3	175.2	
2+62		10.1	174.4	
2+77		10.2	174.3	
2+89 = M.H. 14		10.1	174.4	

Plotted

M.H. 19 to M.H. 7
 0+00 = M.H. 14
 184.50

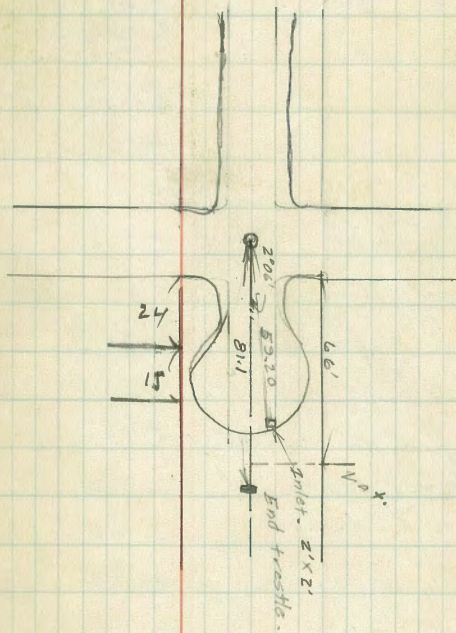
0+21		10.3	174.2	
0+24		9.4	175.1	
0+30		8.7	175.8	
0+33		9.8	174.7	
T.P.	4.67	176.90	12.27	172.23
0+64		17.0	159.9	
0+75		18.0	158.9	
T.P.	1.35	165.18	13.07	163.83
0+97		8.5	156.7	
1+06		9.4	155.8	
1+23		10.6	154.6	
1+28		11.6	153.6	
1+29		13.7	151.5	
T.P.	0.72	153.36	12.54	152.64
1+35		3.2	150.2	
1+39		1.8	151.6	
1+41		1.3	152.1	
1+43		3.6	149.8	
1+57		3.9	149.5	
1+61		4.6	148.8	
1+67		4.9	148.5	
1+90		5.5	147.9	
2+00		6.5	146.9	
2+04		7.6	145.8	
2+23		9.3	144.1	

Plotted

153.36

2+50		12.4	141.0
2+57		14.4	139.0
T.P	1.39	142.43	12.31 141.05
2+69		3.9	138.5
2+72		4.9	137.5
2+76		3.8	138.6
2+81 ^{9L}	= M.H. 7	5.26	137.17 (137.13)

Plot steel



Profile from MH & Vermont &
 Alley North to trash B.
 0+00 = M.H.

B.M.	2.05	294.60	292.55
0+00		3.74	
+20		4.14	
+40		4.46	
+55		5.10	
+59 ⁶²	cut banjo	5.31	
+59 ⁶²	cb banjo.	4.89	
+70	ground.	4.5	
+75		5.7	
+84		10.0	
1+00		18.1	
0+85	8" C.I. top pipe	5.9	
Lat 66' set Alley on E		5.69	
0+75	comes in here.	4.5	
E 66's of Alley East.		4.47	
cb 39's of Alley West.		4.25	
cb 24's of Alley West		3.92	
SW Alley return.		3.63	
NW " "		3.48	
N.E. " "		3.96	
S.E. " "		6.68	
FL. Curb Inlet.			

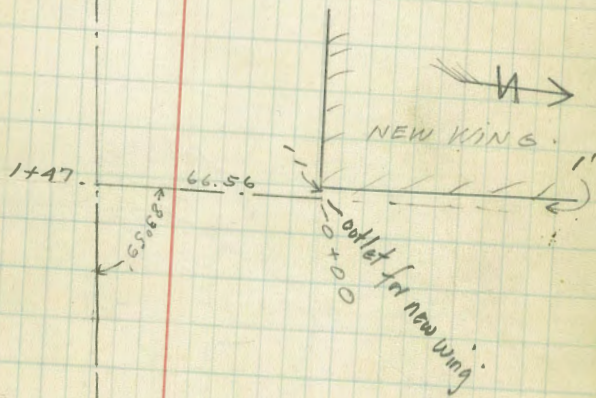
12.57

12

Hospital Sump.

El. of top of Sump	257.77
Sounding	12.57
El. of bottom	245.20

0+00 M.H. 2

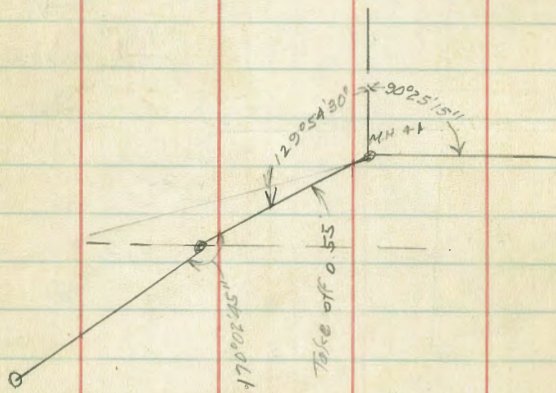


Lateral from New Wing Hosp.

Aug 8-28
Location

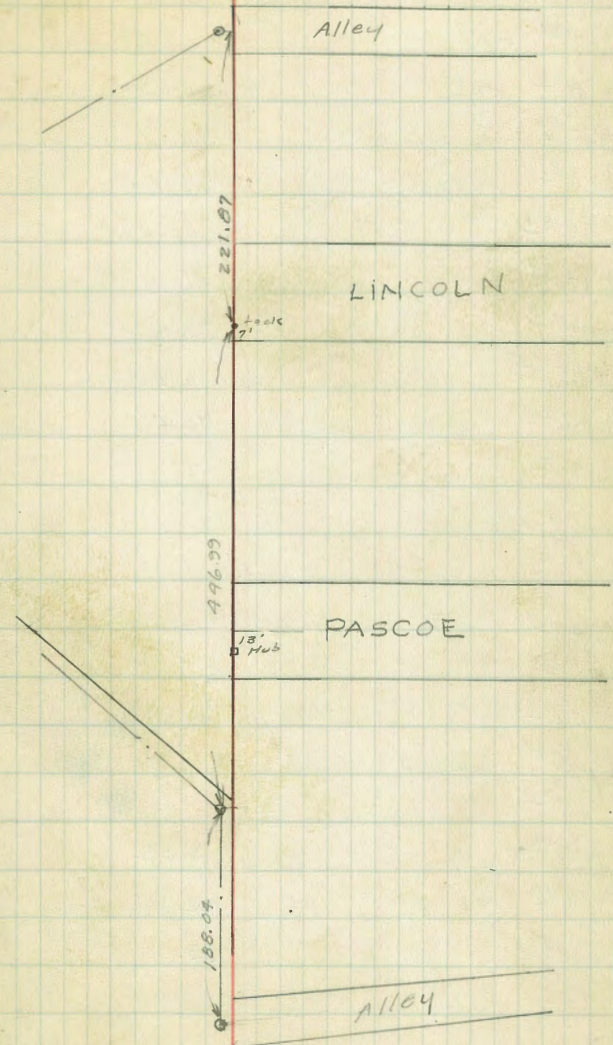
Profile for Hospital Sewer Lateral Sixth-St Sewers

M.H. 3	12.54	20240		18986
T.P.	12.67	21381	1.26	20114
0+66 ⁵⁶			8.1	2057
0+60			6.8	2070
T.P.	10.79	22427	0.33	21348
0+54			5.5	2188
0+39			2.2	222.1
0+20			2.7	221.6
0+07			+1.0	225.3
0+00			+6.5	230.8



23410-05-30
170.02-45

222.57
221.87



Measurement West Line
Fleisher's Add.

Sta.	slope Dist.	Vert. L	Hor. Dist.
0+00	= S.L. Washington 751.05		
7+51 ⁰⁵	Hub		462.88
12+13 ⁹³	Hub		254.00
14+67 ⁹³			55.94
15+23 ⁸⁷	Hub		61.00
16+84 ⁸⁷			186.56
17+71 ⁹³	Hub		70.00
18+44 ⁴³			33.82
18+75 ²⁵			46.00
19+21 ²⁵	85.00	26°00'	76.40
19+97 ⁸⁵	= N.W. Cor.		

Sta.

West on North Line

0+00	= N.E. Corner		
0+70 ³⁸	81.00	29°40'	70.38
1+65 ⁶⁴	101.00	19°25'	95.26
2+80 ²⁰			115.06
2+83 ⁷²			3.02
6+96 ¹⁷	427.00	8°05'	422.75
7+21 ⁸²	487.14		23.10
12+17 ²¹	487.67	2°40'	487.14
12+84 ⁵⁷	73.00	22°16'	67.56 = N.W. Cor.

Previous Sta.

7+51⁰⁰
12+14⁰⁰
17+71²⁷
18+75⁰⁷

17+23⁹³
1523.87
4
1584.87
1591.43
13.41
23
18-5
421

500
810
137.56

14

N.E. Cor. to Mon. on Johnson.

37.00	31°00'	33.42
0+33 ⁰²	100.00	14°43'
		96.72
		14.00
		21.00
		23.00
		27.00
		29.00
		100.00
		78.63
		422.77

2+79⁸⁸
7+28⁷³

Aug 2-29
London

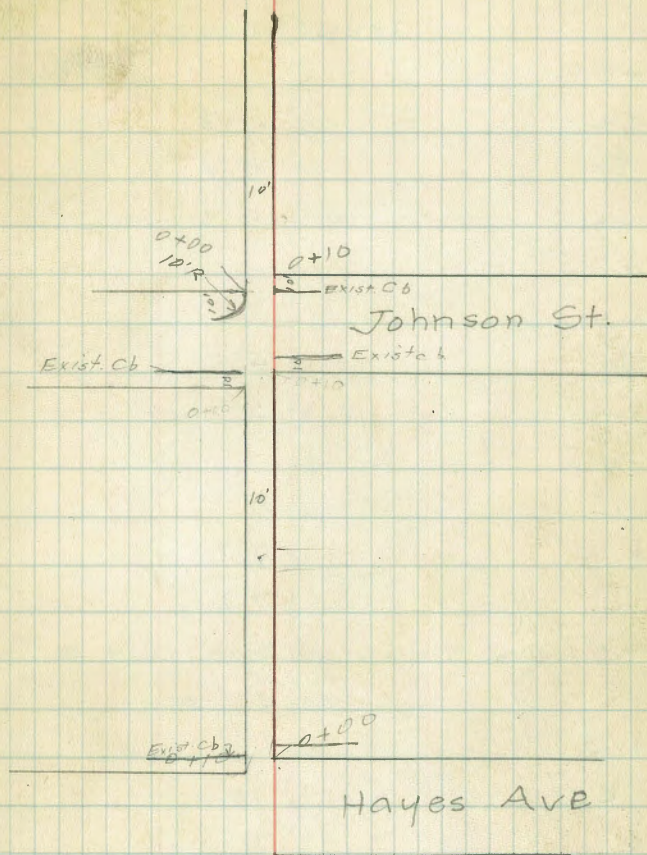
15

X Section Alley 5 Blks B1 & B4
Sub of Lot 48-992 Por of Lot 50 Fleischers Add

0+00 = N.L. Johnson on West
0+10 = " " on East
Can Mon. Johnson

From Johnson St North

B.M.	5.46	292.31	286.85
0+00	wcb	5.90	
±		5.8	
E.L.		5.7	
Ecb		5.37	
0+10			
E.L.		4.6	
±		4.5	
w.L.		4.5	
0+30			
w.L.		3.8	
±		3.6	
E.L.		3.5	
0+64	Sand 2 car garage 68'E Conc. floor		
		2.81	
0+85	Sand Same garage 72'E		
		2.81	
0+67			
E.L.		3.0	
±		3.3	
w.L.		3.6	
0+85			
w.L.		3.6	
±		3.6	
E.L.		3.3	



Can Mon Johnson
MH 39

286.85
287.23

	292.31		
1+00			
E.L.	4.3		
±	4.1		
W.L.	4.2		
1+25			
W.L.	5.2		
±	5.4		
E.L.	5.6		
1+45			
E.L.	7.9		
±	7.6		
W.L.	7.1		
1+46 = 2 Single garage 18.4' W Panc. floor			
	5.20		
1+68			
W.L.	10.0		
±	11.1		
E.L.	12.0		
T.P.	0.33	280.53	12.11
			280.20
1+83			
10'E	5.2		
E.L.	3.2		
±	2.6		
+2	1.8		
W.L.	1.4		

1+95	280.53		
W.L.	3.4		
+3	3.7		
±	4.7		
E.L.	5.6		
15'E	10.0		
2+15			
15'E	15.6		
3'E	12.3		
E.L.	12.0		
±	10.7		
+3	8.8		
W.L.	6.2		
3'W	5.8		
2+30			
W.L.	12.4		
+2	12.8		
±	14.1		
E.L.	14.6		
3'E	15.0		
10'E	16.8		
15'E	18.0		
T.P.	0.81	268.63	12.71
			267.82

2+45	268.63		
15'E		12.2	
4'E		8.6	
EL.		7.5	
±		5.8	
+1		5.6	
w.L.		3.7	
2+60			
w.L.		8.8	
±		10.9	
EL.		13.2	
3'E		14.7	
9'E		16.6	
15'E.		19.4	
T.P.	0.26	256.44	12.95
			255.68
2+66			
15'E		11.8	
9'E		8.7	
4'E		7.0	
EL.		4.3	
±		1.2	
+5		0.7	
w.L.		+1.5	

2+73	256.44		
w.L.		2.0	
+3		3.8	
±		4.6	
EL.		6.7	
8'E		11.2	
10'E		11.6	
15'E		13.0	
T.P. 12.19.	267.86	0.74	255.68
T.P. 12.63	280.33	0.16	267.70
T.P. 12.25	292.46	0.12	280.21
B.M. Beginning		5.61	286.85

Alley Johnson to Hayes
 Aug 10-28

B.M. 7.25 294.10 286.85

0+00 = S.L. Johnson ONE

wcb 6.60

wL 7.0

⊕ 6.5

E.L. 6.4

Ecb 0-10 6.20

0+06

E.L. 6.5

⊕ 6.1

wL 6.4

0+12

wL 6.4

⊕ 6.4

E.L. 6.3

0+25

E.L. 6.3

⊕ 6.4

wL 6.3

0+40

wL 6.0

⊕ 6.2

E.L. 6.2

0+70

E.L. 6.0

⊕ 6.2

wL 6.3

con Man
 Johnsonst.

0+80 294.10

wL 6.2

⊕ 5.9

E.L. 6.0

1+00

E.L. 5.5

⊕ 5.9

wL 6.2

1+25

wL 6.2

⊕ 6.0

E.L. 5.7

1+45

3'E 5.9

2'E 5.7

E.L. 5.6

1/2 5.5

⊕ 6.0

1/4 6.5

wL 6.7

1+56

wL 6.7

⊕ 6.5

E.L. 6.4

2+00	294.10		
E.L.		7.5	
⊕		7.5	
W.L.		7.6	
2+25			
W.L.		8.3	
⊕		8.0	
E.L.		8.1	
2+35			
E.L.		8.2	
⊕		8.2	
W.L.		8.2	
2+55			
W.L.		9.3	
⊕		9.5	
E.L.		9.5	
2+70			
E.L.		11.4	
⊕		11.6	
W.L.		11.3	
T.P.	8.06	289.76	12.40 281.70
2+98			
W.L.		12.2	
⊕		12.2	
E.L.		12.4	
2+98 =	End grade 2'E	Facing Hayes Cone Floor.	
		12.70	

3+215 =	289.76	ML Hayes on West.
W.L.	12.7	12.7
⊕		12.5
E.L.		12.5
B.M. M.H. 39	12.54	287.29
B.M. Beginning	2.89	286.89

Ans 16
London
Meylan
Brookings

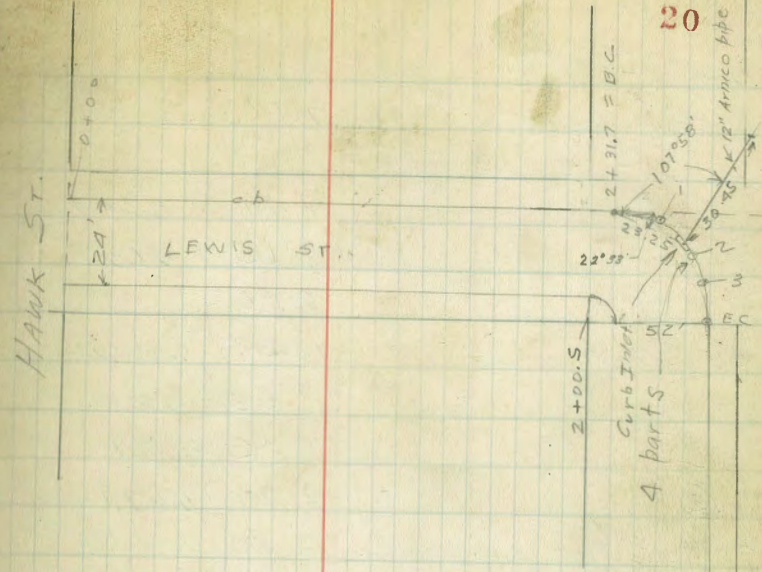
ob Elevs on Lewis St
Hawk to Gold finch

BPSW
Goldfinch
SFC (London)

BM	2.30	270.92	268.62
TP	6.42	272.61	4.73
0+00			
Sob		4.57	268.0
9ut		5.14	267.3
3'4		5.18	267.4
±		5.32	267.3
N'4		5.61	267.0
N'9ut		5.95	266.6
N'cb		5.50	267.1
0+25			
Sob		4.44	268.2
N'cb		5.36	267.3
0+50			
N'cb		5.24	267.4
S'cb		4.31	268.3
0+75			
S'cb		4.26	268.3
N'cb		5.13	267.5
0+90			
N'cb		5.07	267.5
S'cb		4.24	268.4
1+00			
S'cb		4.22	268.4
N'cb		5.07	267.5
1+01		4.73	
N'cb		5.09	267.5

Lewis St.

20



		272.61
1+12		
Sob	4.49	268.1
N'cb	5.31	267.3
1+25		
N'cb	5.54	267.1
S'cb	4.85	267.8
1+50		
S'cb	5.40	267.4
N'cb	6.22	266.4
1+75		
N'cb	6.95	265.6
S'cb	5.94	266.7
2+00 ±	= w.L. Goldfinch	
S'cb	6.42	266.2

Lewis St.

2+00 ⁵	272.61		
Ncb	7.66	264.9	
2+31 ² = BC NE Ret			
Ncb	8.30	264.3	
①	8.65	263.9	
cb & Inlet	8.80	263.81	
FL Catch basin	11.39	261.22	
cut at Inlet	9.60	263.0	
②	8.83	263.78	
③	8.77	263.84	
E.C. NE Ret sl. Lewis	8.56	264.05	
Egut. Bold finch	9.10	263.51	
E'g	8.15	264.46	
£	7.56	265.05	
W'g	7.20	265.41	
w'gt	7.34	265.27	
w'cb - bc sw. ret	6.61	266.00	
Cent. Sw. ret	6.53	266.08	
T.P.	8.64	272.91	8.34 264.27 ✓
			4.28 268.63 ✓
pipe from Inlet & profile beyond			
	1.29	265.10	263.81
End pipe from cb Inlet	8.89	265.72	
ground at end	11.4	253.7	
+10'	17.1	248.0	
+23'	24.0	241.1	
+27'	22.4	244.7	

Lewis St.

21

265.10

29.7 235.4

Corrected
+40.46

0+29	297.52		
Sub	4.58	292.94	33.40
0+49 = 0+00 = EC SE ret.			
Sub	4.60	292.92	33.38
0+25			
Sub	4.52	293.00	33.46
Ncb	4.62	292.90	33.36
0+50			
Ncb	4.64	292.88	33.34
Sub	4.41	293.11	33.57
0+75			
Sub	4.36	293.16	33.62
Ncb	4.55	292.97	33.43
1+00			
Ncb	4.58	292.94	33.40
Sub	4.16	293.36	33.62
1+06 ⁸⁹ = Bc. Cr on North - Bc. S.W. ret. to Belle Isle			
Sub	4.09	293.43	33.59
Ncb	4.63	292.89	33.35
①			
Ncb	4.80	292.72	33.15
②			
Ncb	5.01	292.51	32.97
0+00 = EC Cr on North			
Ncb	5.14	292.38	32.84

297.52
S.W. ret into - Belle Isle

①				
Sub	4.16	293.36	33.742	
②				
Sub	4.07	293.45	33.91	
③				
Sub	4.08	293.44	33.88	
④				
Sub	4.10	293.42	33.88	
EC = 0+00 Belle Isle				
Sub=Ncb	4.12	293.40	33.86	
Isle Vista				
0+00 = EC Cr on North				
0+25				
Ncb	5.35	292.17	32.63	
0+50				
Ncb	5.40	292.12	32.52	
0+75				
Ncb	5.51	292.01	32.47	
1+00				
Ncb 3.88	295.81	5.59	291.93	32.29
1+08 ⁹⁰ = Bc. SE. ret				
Ncb	3.88	291.93	32.29	
Sub	3.31	292.50	32.46	

295.81

SE rot. into Belle Isle.

①				
cb	3.16	292.65	33.11	
②				
cb	3.00	292.81	33.27	
③				
cb	2.90	292.91	33.37	
B.C. = 0 + 41 ⁰	Belle Isle			
	2.80	293.01	33.47	
	Isla Vista			
1 + 25				
Ncb	4.06	291.75	32.21	
Scb	3.43	292.38	32.84	
1 + 50				
Scb	3.59	292.22	32.68	
Ncb	4.19	291.62	32.08	
1 + 75				
Ncb	4.45	291.36	31.82	
Scb	3.83	291.98	32.44	
2 + 00				
Scb	4.01	291.80	32.27	
Ncb	4.74	291.07	31.53	
2 + 25				
Ncb	5.09	290.72	31.18	
Scb	4.22	291.59	32.05	

295.81

24

2 + 43 ⁷³ = B.C.

Scb	4.37	291.44	31.90
Ncb	5.33	290.48	30.94
①			
Ncb	5.50	290.31	30.77
Scb	4.45	291.36	31.82
②			
Scb	4.54	291.27	31.73
Ncb	5.56	290.25	30.71
③			
Ncb	5.69	290.12	30.58
Scb	4.61	291.20	31.66
④			
Scb	4.74	291.07	31.53
Ncb	5.80	290.01	30.47
EC = 0 + 00			
Ncb = Ecb	5.86	289.95	30.41
Scb = Wcb	4.87	290.94	31.40
T.P. 149	293.77	3.53	292.28
0 + 25			
Ecb	4.03	289.74	30.20
Wcb	3.03	290.74	31.20
0 + 50			
wcb	3.20	290.57	31.03
Ecb	4.18	289.59	30.05

293.77

0+75			
Ecb	4.45	289.32	329.78
web	3.42	290.35	30.81
1+00			
web	3.57	290.20	30.66
Ecb	4.58	289.19	29.65
1+25			
Ecb	4.80	288.97	29.43
web	3.81	289.96	30.42
1+50			
web	3.99	289.78	30.24
Ecb	4.98	288.79	29.25
1+75			
Ecb	5.12	288.65	29.11
web	4.14	289.63	30.09
2+00			
web	4.42	289.35	29.81
Ecb	5.30	288.47	28.93
2+25			
Ecb	5.51	288.26	28.72
web	4.58	289.19	29.65
2+50			
web	4.74	289.03	29.45
Ecb	5.75	288.02	28.48
2+75			
Ecb	6.07	287.70	28.16
web	5.05	288.72	29.18

293.77

3+00			
web	5.47	288.30	328.76
Ecb	6.43	287.34	327.80
3+25			
Ecb	6.73	287.04	327.50
web	5.91	287.86	328.32
3+50			
web	6.56	287.21	327.67
Ecb	7.07	286.70	327.18
3+75			
Ecb	7.63	286.14	326.66
web 0.70	287.30	7.17	286.60 327.06
4+00			
web	1.37	285.91	326.37
Ecb	1.71	285.59	326.05
4+25			
Ecb	2.41	284.89	325.35
web	2.16	285.14	325.60
4+50			
web	2.94	284.36	324.82
Ecb	3.03	284.27	324.73
4+75			
Ecb	3.68	283.62	324.08
web	3.70	283.60	324.06
5+00			
web	4.58	282.72	323.18
Ecb	4.29	283.01	323.47

25

	287.30			
5+10 ^{6L}	B.C. ret's N Thorn			
Web	4.78	282.52	322.98	
Ecb	4.59	282.71	323.17	
5+25				
Ecb	4.94	282.36	322.82	
5+50				
Ecb	5.54	281.76	322.22	
5+80 ^{6L}	= B.C. ret's S Thorn			
Ecb	6.31	280.99	321.45	
Web	6.29	281.01	321.47	
6+00				
Ecb	7.44	279.86	320.32	
Web	7.50	279.80	320.26	
6+25				
Web	9.00	278.30	318.76	
Ecb	8.99	278.31	318.77	
6+50				
Ecb	10.57	276.73	317.19	
Web	10.59	276.71	317.17	
6+75				
Web	12.17	275.13	315.59	
Ecb	13.0	276.50	315.66	
7+00				
Feb	2.86	273.64	314.10	
Web	2.98	273.52	313.98	

	276.50		
7+25			
Web	4.54	271.96	312.42
Ecb	4.37	272.13	312.77
7+50			
Ecb	5.90	270.60	311.06
Web	6.07	270.43	310.89
7+75			
Web	7.58	268.92	309.38
Ecb	7.48	269.02	309.48
7+91 ²	= B.C. banjo		
Ecb	8.48	268.02	308.48
Web	8.58	267.92	308.38
PRC Banjo			
Web	9.49	267.01	307.47
Ecb	9.51	266.99	307.45
A & B arc pts midway between RRC and Slot			
B	9.87	266.63	307.09
A	9.89	266.61	307.07
Wend slot	10.03	266.47	306.93
gut Wend slot	11.31	265.19	305.65
Cent slot	10.05	266.45	306.91
gut at Cent	11.38	265.12	305.58
End slot	10.02	266.48	306.94
gut at End	11.31	265.19	305.65
B.M. from P.O. Lot 9 end of banjo Isla Vista			
	9.71	266.77	307.25
M.H. in Banjo	9.75		307.21

Belleisle Drive

300.02

27

B.M.	6.50	300.02	293.22	2+00		
0+00 = E.C. SW ret from Isle Vista				Ecb	7.95	292.07 332.53
wcb	6.61	293.41	333.87	wcb	7.73	292.29 332.25
0+25	6.70	293.32	333.78	2+25		
0+41 = E.C. SE ret from Isle Vista				wcb	8.08	291.94 332.40
wcb	6.79	293.23	333.69	Ecb	8.16	291.86 332.32
Ecb	7.00	293.02	333.48	2+50		
0+50				Ecb	8.18	291.84 332.50
Ecb	7.06	292.96	333.42	wcb 125	292.86 8.41	291.61 332.07
wcb	6.82	293.20	333.66	2+75		
0+75				wcb	1.80	291.06 331.52
wcb	6.98	293.04	333.50	Ecb	1.52	291.34 331.00
Ecb	7.21	292.81	333.27	3+00		
1+00				Ecb	2.03	290.83 331.29
Ecb	7.34	292.68	333.14	wcb	2.50	290.36 330.82
wcb	7.15	292.87	333.33	3+25		
1+25				wcb	3.36	289.50 329.96
wcb	7.26	292.76	333.22	Ecb	2.64	290.22 330.68
Ecb	7.43	292.59	333.05	3+50		
1+50				Ecb	3.42	289.44 329.90
Ecb	7.66	292.36	332.82	wcb	4.34	288.52 328.98
wcb	7.42	292.60	333.06	3+75		
1+75				wcb	5.24	287.62 327.08
wcb	7.55	292.47	332.93	Ecb	4.48	288.38 328.84
Ecb	7.80	292.22	332.68	4+00		
				Ecb	5.45	287.41 327.87
				wcb	6.22	286.64 327.10

4+25	292.86			
wcb		7.11	285.75	326.21
Ecb		6.39	286.47	26.93
4+50				
Ecb		7.31	285.55	26.01
wcb		8.12	284.74	25.20
4+75				
wcb		9.10	283.76	24.22
Ecb		8.21	284.65	25.11
5+00				
Ecb		9.23	283.63	24.09
wcb		10.10	282.76	23.22
5+25				
wcb		11.12	281.74	22.20
Ecb		10.20	282.66	23.12
5+50				
Ecb		11.13	281.73	22.19
wcb		12.03	280.83	21.29
5+75				
wcb		13.05	279.91	20.27
Ecb		12.03	280.83	21.29
150	281.31		279.81	20.27
6+00				
wcb		2.40	278.91	19.37
Ecb		1.45	279.86	20.32

6+25				
Ecb		2.44	278.87	319.33
wcb		3.29	278.02	318.48
6+50				
wcb		4.25	277.06	317.52
Ecb		3.38	277.93	318.39
6+75				
Ecb		4.16	277.15	317.61
wcb		5.16	276.15	316.61
6+89 ²⁰	= Ec rets N Thorn			
wcb		5.60	275.71	316.17
Ecb		4.50	276.81	317.27
	NE return			
①		4.54	276.77	317.23
②		4.57	276.74	317.20
③		4.58	276.73	317.19
E.C. Thorn		4.55	276.76	317.22
	NW return			
①		5.74	275.57	316.03
②		5.96	275.35	315.81
③		6.19	275.12	315.59
E.C. Thorn		6.38	274.93	315.39

281.31

S.W. return

B.C. Thorn	6.88	274.43	314.89
①	6.83	274.48	314.94
②	6.85	274.46	314.92
③	6.87	274.44	314.90
Ec. Belle Isle = 0+00	6.90	274.41	314.87

S.E. return

B.C. Thorn	5.31	276.00	316.46
①	5.44	275.87	316.33
②	5.62	275.69	316.15
③	5.72	275.59	316.05
Ec. Belle Isle = 0+00 E	5.87	275.44	315.90
0+25			
Ecb.	6.88	274.43	314.89
Web	7.87	273.44	313.90
0+50			
Web	8.80	272.51	312.97
Ecb	8.10	273.21	313.67
0+75			
Ecb	9.10	272.21	312.67
Web	9.73	271.58	312.04
1+00			
Web	10.63	270.68	311.14
Ecb	9.89	271.42	311.88

281.31

29

1+25			
Ecb	10.95	270.36	310.82
Web	11.64	269.67	310.13
1+50			
Web	12.58	268.73	309.19
Iron Pip. Ec. S.W. ret. Thorn & Belleisle			
B.M.	6.63	274.48	315.14
3.20		271.93	268.73
1+50			
Ecb	2.58	269.35	309.81
1+75			
Ecb	3.66	268.27	308.78
Web	4.12	267.81	308.27
2+00			
Web	5.12	266.81	307.27
Ecb	4.62	267.31	308.77
2+25			
Ecb	5.64	266.29	306.75
Web	6.08	265.85	306.31
2+50			
Web	7.07	264.86	305.32
Ecb	6.65	265.28	305.74
2+75			
Ecb	7.64	264.29	304.75
Web	8.00	263.93	304.39
3+00			
Web	8.96	262.97	303.43
Ecb	8.65	263.28	303.74

3+25

271.93

Feb

9.70

262.23

302.69

Web

9.88

262.05

302.51

3+50

Web

10.86

261.07

301.53

Feb

10.73

261.20

301.66

3+75

Feb

11.74

260.19

300.65

Web

11.80

260.13

300.59

3+92 = End. on west

Web

12.47

259.46

299.92

3+93 = End on East

Feb

12.49

259.44

299.90

B.M. End of Isla Vista.

5.13

266.80

266.79

Thorn St.

30

B.M. 2.49

275.17

274.68

TP 5.06

267.37

12.76

262.21

E.L. Euclid on south

cb

9.20

258.27

cut.

9.28

257.99

E.L. Euclid on North

cb

7.85

259.42

cut.

8.17

259.10

0+00 = EC rats from Euclid.

Scb

8.43

258.84

Ncb

7.43

259.84

0+25

Ncb

5.47

261.80

Scb

6.31

260.96

0+50

Scb

4.13

263.14

Ncb

3.34

263.93

0+75

Ncb

1.21

266.06

Scb

1.98

265.29

MH. at 0+99Z

277.55

on E

0.11

267.16

1+00

Scb

10.10

267.44

Ncb

10.38

267.17

1+25

Ncb

7.27

270.28

Scb

7.92

269.63

298.73

299.45

299.88

299.56

299.30

300.30

302.26

301.92

303.60

304.39

306.52

305.75

307.62

307.90

307.63

310.71

310.09

1+50	277.55			
Scb	5.74	271.81	312.27	
Ncb	5.19	272.36	312.82	
1+75				
Ncb	3.04	274.51	314.97	
Scb	3.54	274.01	314.47	
1+80 = Ec. rets w Belle Isle				
Scb	3.11	274.44	314.90	
Ncb	2.63	274.92	315.38	
Gas. Co Box	2.09	275.46	315.92	
0+00 = Ec. rets E Belle Isle				
Scb	1.55	276.00	316.46	
Ncb	0.99	276.76	317.22	
0+25				
Ncb 6.10	283.57	277.49	317.95	
Scb	6.92	276.67	317.13	
0+50				
Scb	6.16	277.43	317.89	
Ncb	5.40	278.19	318.65	
0+75				
Ncb	4.66	278.93	319.39	
0+78E				
Scb	5.39	278.20	318.66	
1+00				
Scb	4.78	278.81	319.27	
Ncb	3.94	278.65	319.11	

1+25	283.57			
Ncb	3.19	280.40	320.86	
Scb	4.10	279.49	319.95	
1+50				
Scb	3.40	280.19	320.65	
Ncb	2.48	281.11	321.57	
1+80 = Ec. rets w Isla Vista				
Ncb	1.58	282.01	322.47	
Scb	2.55	281.04	321.50	
S.W. return 4 parts				
①	2.56	281.03	321.49	
②	2.58	281.01	321.47	
③	2.55	281.04	321.50	
Ec. Isla Vista	2.56	281.03	321.49	
N.W. return 4 parts				
①	1.12	282.17	322.63	
②	1.32	282.27	322.73	
③	1.18	282.41	322.87	
Ec. Isla Vista				
B.M.	8.91	274.68	315.14	

X Sec. Santa Cruz Santa Barbara to
 Ebers. Cbses. walks in to 6+00
 52' Roadway 14' cbs 80' street.

B.M	268	258.18	255.50	sw Santa Barb. & Santa Cruz
0+00	= W.L	Santa Barbara		
scb		2.69	255.49	
gut		3.4	1 (255.2) 254.8	
1/4		2.9	255.3	
1/4		2.6	255.6	
1/4		2.6	255.6	
gut		2.8	255.4	
Ncb		2.02	256.16	
0+25				
Ncb		2.03	256.15	
gut		2.9	255.3	
1/4		2.6	255.6	
1/4		2.5	255.7	
1/4		2.7	255.5	
gut		3.5	254.7	
scb		2.70	255.48	
0+50				
scb		2.80	255.38	
gut		3.7	254.5	
1/4		2.8	255.4	
1/4		2.6	255.6	
1/4		2.7	255.5	
gut		3.2	255.0	
Ncb		2.10	256.08	

Plotted 10-18-28 - C.B.H.

Yardage figured Yardage Book # 13
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 F.C.L.
 5-3-29

Sept 13-28

London
 Isbell
 Morgan.

32

0+75	258.18	
Ncb	2.50	255.68
gut	3.5	254.7
1/4	3.1	255.1
1/4	2.8	255.4
1/4	3.2	255.0
gut	4.2	254.0
scb	3.16	255.02
0+100		
scb	3.59	254.59
gut	4.8	253.4
1/4	3.9	254.3
1/4	3.5	254.7
1/4	3.7	254.5
gut	4.3	253.9
Ncb	3.13	255.05
0+25		
Ncb	4.16	254.08
gut	5.0	253.2
1/4	4.7	253.5
1/4	4.5	253.7
1/4	4.9	253.3
gut	5.6	252.6
scb	4.36	253.82

258.18

1+50		
Scb	5.32	252.86
gut	6.4	251.8
1/4	5.9	252.3
¢	5.6	252.6
1/4	5.8	252.4
gut	6.2	252.0
Ncb	5.17	253.01
1+75		
Ncb	6.70	251.48
gut	7.6	250.6
1/4	7.2	251.0
¢	7.0	251.2
1/4	7.1	251.1
+10	7.8	250.4
gut	7.3	250.9
Scb	6.48	251.70
2+00		
Scb	8.00	250.18
gut	8.7	249.5
+3	9.4	248.8
+5	8.7	249.5
1/4	8.7	249.5
¢	8.7	249.5
1/4	9.1	249.1
+12	9.3	248.9
gut	9.8	248.4

258.18

33

2+00		
Ncb	8.71	249.47
2+25		
Ncb	10.79	247.39
gut	11.4	246.8
+2	11.2	247.0
1/4	11.0	247.2
¢	10.6	247.6
1/4	10.7	247.5
+8	10.7	247.5
+9	11.7	246.5
+12	11.0	247.2
gut	10.5	247.7
Scb	9.75	248.43
2+50		
Scb	11.76	246.42
gut	12.2	246.0
+4	12.6	245.6
+5	14.1	244.1
+8	12.6	245.6
1/4	12.6	245.6
¢	12.6	245.6
1/4	12.9	245.3
+11	13.4	244.8
gut	13.7	244.5
Ncb	12.78	245.40

	25818		
FP.	0.18	245.79	12.57
			245.61
2+95			
Ncb		2.33	243.46
gut		3.1	242.7
+3		3.1	242.7
1/4		2.5	243.3
1/4		2.1	243.7
1/4		2.2	243.6
+7		2.1	243.7
+9		3.5	242.3
+11		2.8	243.0
gut		2.2	243.6
Scb		1.35	244.44
3+00			
Scb		3.55	242.24
gut		4.1	241.7
+4		4.4	241.4
+6		5.5	240.3
+7		5.2	240.6
+9		4.2	241.6
1/4		4.2	241.6
+2		4.4	241.4
+3		4.9	240.9
+5		4.3	241.5
1/4		4.2	241.6
1/4		4.5	241.3

	245.79	34
3+00		
N 1/4 +11	5.0	240.8
gut	5.3	240.5
Ncb	4.36	241.43
3+25		
Ncb	6.31	239.48
gut	7.3	238.5
1/4	6.7	239.1
1/4	6.3	239.5
+9	6.4	239.4
+10	6.7	239.1
+11	6.4	239.4
1/4	6.4	239.4
+4	6.3	239.5
+5	7.1	238.7
+8	7.4	238.4
+9	6.5	239.3
+12	6.7	239.1
gut	6.4	239.4
Scb	5.78	240.01
3+50		
Scb	7.67	238.12
gut	8.4	237.4
+6	8.3	237.5
+7	8.8	237.0
+9	8.2	237.6
1/4	8.3	237.5

3 + 50	245.79	
+3	8.8	237.0
+6	8.5	237.3
¢	8.4	237.4
¼	8.8	237.0
+9	9.0	236.8
+12	9.3	236.5
9¢	9.2	236.6
Ncb	8.33	237.46
3 + 75		
Ncb	10.28	235.51
9¢	11.3	234.5
+2	10.8	235.0
¼	10.6	235.2
¢	10.3	235.5
+12	10.1	235.7
¼	10.2	235.6
+7	10.5	235.3
+7.5	11.0	234.8
+8	10.4	235.4
9¢	10.3	235.5
Scb	9.62	236.17

4400	245.79		35
Scb	11.76	234.03	
9¢	12.5	233.3	
+4	12.4	233.4	
+5	13.2	232.6	
+5.5	12.5	233.3	
¼	12.2	233.6	
¢	12.3	233.5	
¼	12.5	233.3	
+9	12.7	233.1	
9¢	13.3	232.5	
Ncb	12.49	233.30	
TP 0.15	232.87	13.07	232.72 ✓
4 + 25			
Ncb	1.56	231.31	
9¢	2.5	230.4	
+4	2.1	230.8	
¼	1.7	231.2	
¢	1.4	231.5	
¼	1.3	231.6	
+4	1.5	231.4	
+5	2.3	230.6	
+6	1.4	231.5	
+11	1.6	231.3	
+11.5	2.0	230.9	
9¢	1.9	231.0	
cb	0.98	231.89	

	23287	
4+50		
Scb	2.98	229.89
gut	4.0	228.9
+2	3.7	229.2
+8	3.3	229.6
+9	4.1	228.8
+10	3.2	229.7
1/4	3.2	229.7
+3	3.4	229.5
+4	3.2	229.7
ϕ	3.3	229.6
1/4	3.6	229.3
+10	4.2	228.7
+12	4.7	228.2
gut	4.2	228.7
Ncb	3.52	229.35
4+75		
Ncb	5.44	227.43
gut	6.3	226.6
+3	6.4	226.5
+6	5.9	227.0
1/4	5.4	227.5
ϕ	5.1	227.8
1/4	5.2	227.7
+6	5.1	227.8
+7	5.8	227.1
+7.5	5.2	227.7

	23287	36
4+75		
+12	5.6	227.3
gut	6.0	226.9
Scb:	4.96	227.91
5+00 = EL Guizot on North		
Scb	7.15	225.72
gut	7.9	225.0
+2	8.3	224.6
+3	7.6	225.3
1/4	7.0	225.9
ϕ	7.1	225.8
1/4	7.5	225.4
+7	8.0	224.9
+10	8.5	224.4
gut	8.2	224.7
cb	7.51	225.36
5+10		
NL endret	7.91	224.96
gut	8.7	224.2
cb	9.0	223.9
+2	8.6	224.3
+6	8.6	224.3
1/4	8.2	224.7
ϕ	7.8	225.1
+7	7.9	225.0
1/4	7.8	225.1

	232.87	
5+10		
5/4+10	8.5	224.4
+10 ⁵	9.0	223.9
gut	8.7	224.2
Scb	7.98	224.89
5+25		
Scb	9.15	223.72
gut	10.0	222.9
+2	9.6	223.3
1/4	9.0	223.9
¢	8.7	224.2
1/4	9.2	223.7
+7	9.7	223.2
cb	9.6	223.3
N.L.	9.3	223.6
5+50		
N.L. and ret.	11.03	221.84
gut at B	11.1	221.8
+12	11.5	221.4
cb	11.2	221.7
+2	9.5	221.4
+6	11.5	221.4
+7	11.1	221.8
1/4	10.9	222.0
¢	10.5	222.4
1/4	10.4	222.5
+8	10.8	222.1

	232.87	
5+50		
+8 ⁵	11.4	221.5
gut	11.5	221.4
cb	10.63	222.24
5+60		
Scb	11.16	221.71
gut	12.0	220.9
+5	12.0	220.9
+6	11.4	221.5
1/4	11.2	221.7
¢	11.2	221.7
1/4	11.5	221.4
+5	11.8	221.1
+8	13.4	219.5
gut	12.5	220.4
Ncb	11.33	221.54
TP. 0.86	220.65	13.08
5+75		
Ncb	0.12	220.53
gut	1.4	219.3
+3	2.5	218.2
+5	2.5	218.2
+6	0.3	220.4
1/4	0.2	220.5
¢	0.0	220.7
1/4	0.0	220.7
+6	0.1	220.6

5775

220.65

+7	0.7	220 0
gut	0.5	220 2
Seb	+0.2	220.8 ?
6+00 = EL Guizat	07 South	
Seb	1.16	119.49
gut	2.3	218 4
+4	2.4	218 3
+8	1.4	219.3
1/4	1.5	219 2
+2	1.7	219 0
+3	2.2	218 5
+4	1.6	219 1
±	1.6	(119.1) 219.1
+1	1.7	219 0
+2	2.0	218.7
+3	1.7	219.0
1/4	2.0	218.7
+3	1.9	218 8
+8	2.1	218 6
+9	2.8	217.9
+10	3.1	217 6
+11	3.5	217 2
+12	3.5	217 2
+12 ^S	2.8	217 9
gut	2.7	218 0
Nob	1.81	218.84

6+10

220.65

38

N.L.	1.5	219.2
+3	1.9	218.8
+11	2.1	218.6
+13	2.6	218.1
cb	3.7	217.0
+1	3.5	217.2
+7	3.2	217.5
+8	2.6	218.1
1/4	2.7	218.0
+1	3.0	217.7
+2	2.6	218.1
+7	2.8	217.9
+8	2.4	218.3
+9	2.4	218.3
±	2.2	218.4
+8	2.5	218.2
+10	2.8	217.9
+12	2.5	218.2
1/4	2.5	218.2
+9	2.4	218.3
+11	3.0	217.7
+12	2.4	218.3
cb	2.5	218.2
+6	1.4	219.3
S.L.	1.2	219.4
S.L. (opendret.)	1.26	219.39

	220.65	
6+30		
S.L.	2.5	218.1
+3	2.6	218.1
+12	3.7	217.0
cb	3.6	217.1
+5	3.9	216.8
+6	4.6	216.1
+9	3.9	216.8
1/4	3.9	216.8
+8	3.6	217.1
±	3.8	216.9
+10	4.2	216.5
1/4	4.9	215.8
+3	4.1	216.6
+7	5.4	215.3
+10	3.7	217.0
+12	4.2	216.5
cb	3.2	217.5
+9	3.3	217.4
+11	4.0	216.7
N.L.	4.2	216.4

	220.65	
6+50		
N.L.	4.2	216.4
+5	5.2	215.5
+6	10.0	210.7
+9	11.2	209.5
+10	5.2	215.5
cb	5.0	215.7
+1	5.7	215.0
+5	6.4	214.3
+7	5.9	214.8
1/4	5.9	214.8
+1	6.0	214.7
+2	6.8	213.9
+8	5.4	215.3
±	5.2	215.4
+9	5.0	215.7
+9	10.4	210.3
+11	10.4	210.3
+12	5.3	215.4
1/4	5.2	215.5
cb	4.9	215.8
S.L.	3.8	(217.0) ⁷
		216.8

6+57	220.65		
S.L.		14.0	2066
+7		4.7	216.0
cb		5.0	215.7
+6		5.8	214.9
1/4		5.6	215.1
+1		5.6	215.1
+1		11.6	209.1
+3		11.6	209.1
+3		5.5	215.2
2		6.1	214.6
+5		5.9	214.8
+10		7.3	213.4
1/4		6.5	214.2
+4		6.4	214.3
+6		6.9	213.8
+10		6.2	214.5
cb		6.2	214.5
+10		5.9	214.8
N.L		12.2	208.4
6'N		12.0	208.7
7'N		5.2	215.5
12'N		4.7	216.0

6+68	220.65		
20'N			
17'N		6.5	214.2
14'		6.3	214.4
10'N		13.4	207.3
5'N		13.3	207.4
3'N		10.2	210.5
N.L		6.1	214.6
+1		5.8	214.9
cb		7.1	213.6
+7		7.0	213.7
+9		7.2	213.5
1/4		7.9	212.8
+5		7.4	213.3
+10		7.6	213.1
2		6.8	213.9
+4		6.8	213.9
+5		6.5	214.2
+9		7.0	213.7
+9		6.8	213.9
+11		13.6	207.1
+11		13.6	207.1
1/4		6.7	214.0
+1		6.6	214.1
+2		6.6	214.1
+7		5.1	215.6
		5.5	215.2

6+68	220.65		
cb	15.7	205.0	
+8	15.4	205.3	
+13	13.3	207.4	
S.L.	13.1	207.6	
6+78			
S.L.	12.6	208.1	
+4	12.9	207.8	
+5	14.4	206.3	
+6	14.1	206.6	
+11	13.5	207.2	
cb	16.0	204.7	
+7	16.2	204.5	
+10	9.7	211.0	
1/4	10.9	209.8	
+2	15.7	205.0	
+3	15.7	205.0	
+5	8.6	212.1	
2	8.2	212.4	
1/4	8.3	212.4	
+2	9.0	211.7	
+5	8.4	212.3	
cb	8.1	212.6	
+12	8.3	212.4	
+13	7.1	213.6	
N.L.	7.0	213.7	
9/11	7.4	213.3	

6+86	220.65		
S'N	7.9	212.8	
N.L.	8.3	212.3	
N.L.	7.3	211.3	
cb	9.2	211.5	
1/4	9.4	211.3	
+8	9.2	211.5	
4	9.5	211.2	
+2	10.2	210.5	
+5	13.2	207.5	
+10	16.7	204.0	
cb ^{1/4?}	15.8	204.9	
+3	17.8	202.9	
+7	16.5	204.2	
+10	15.0	205.7	
cb	15.0	205.7	
+4	16.0	204.7	
+3	15.1	205.6	
+8	15.2	205.5	
+11	14.1	206.6	
S.L.	14.0	206.7	

6+92	220.65		
S.L.	8.9	211.7	
+5	14.9	205.8	
cb	15.6	205.1	
+2	16.6	204.1	
+4	15.7	205.0	
+8	16.3	204.4	
+11	17.5	203.2	
1/4	17.5	203.2	
+3	17.5	203.2	
ϕ	10.2	210.4	
1/4	10.4	210.3	
cb	10.6	210.1	
+5	10.9	209.8	
N.L.	9.9	210.7	
5'N	9.3	211.4	
7+15			
5'N	13.4	207.3	
T.P.	0.09	207.82	12.92
N.L.			207.73
cb	0.5	207.3	
1/4	0.7	207.1	
+5	0.7	207.1	
+12	1.0	206.8	
ϕ	9.8	198.0	
+2	9.8	198.0	
	9.0	198.8	

7+15	207.82		
4+6	5.1	202.7	
4	5.0	202.8	
+4	4.4	203.4	
+6	5.2	202.6	
+12	0.8	207.0	
cb	0.6	207.2	
+4	0.5	207.3	
+6	+0.2	208.0	
3L	0.7	207.1	
7+55			
3L	2.0	205.8	
cb	2.6	205.2	
+6	3.6	204.2	
+12	4.4	203.4	
1/4	8.8	199.0	
+3	10.2	197.6	
+7	8.5	199.3	
ϕ	8.7	199.1	
+4	8.4	199.4	
+8	11.7	196.1	
+10	11.8	196.0	
1/4	8.4	199.4	
+8	4.7	203.1	
cb	4.5	203.3	
+8	4.3	203.5	
N.L.	3.3	204.5	

7+75	207.82	5.3	202.5
^{5'N} N.L.		6.3	201.5
+4		8.9	198.9
cb		9.0	198.8
1/4		9.5	198.3
+1		13.4	194.4
+3		13.7	194.1
+7		17.0	196.8
ϕ		11.1	196.7
+5		10.9	196.9
+8		13.1	194.7
+10		13.1	194.7
1/4		8.3	199.5
+3		7.9	199.9
+5		5.3	202.5
cb		4.5	203.3
S.L.		3.4	204.4
8+00			
S.L.		5.2	202.6
cb		6.2	201.6
+10		7.0	200.8
1/4		10.1	197.7
+3		11.6	196.2
+3		15.7	192.1
+5		15.6	192.2
+8		13.5	194.3

8+00	207.82		
ϕ		13.5	194.3
+7		13.7	194.1
+11		15.9	191.9
1/4		15.7	192.1
+2		15.6	192.2
+3		12.2	195.6
+7		11.5	196.3
cb		11.7	196.1
+10		11.3	196.5
N.L.		8.3	199.5
5'N		7.3	200.5
8+25			
5'N		9.8	198.0
2'N		10.1	197.7
N.L.		11.2	196.6
+3		13.5	194.3
cb		14.8	193.0
+7		14.5	193.3
+10		15.6	192.2
+11		17.5	190.3
1/4		17.5	190.3
+3		17.4	190.4
+5		16.3	191.5
ϕ		15.8	192.0
+3		16.0	191.8

8+25	207.82		
2+7		18.0	1898
+9		18.0	1898
+11		14.0	1938
1/4		11.8	1960
+3		9.2	1986
cb		8.3	1995
S.L.		7.1	2007
T.P. 3.21	201.04	9.99	19783
8+50			
S.L.		2.2	1988
cb		3.5	1975
+6		4.2	1968
+8		6.4	1946
1/4		8.0	1930
+3		11.7	1893
+7		12.3	1887
+10		11.5	1895
2		11.3	1897
+7		11.4	1896
+10		12.8	1882
1/4		11.8	1892
+3		11.2	1898
+7		9.6	1914
cb		9.3	1917
+9		8.3	1927

8+50	201.04		
cb+11		6.4	194.6
N.L.		6.1	194.9
S'N		5.3	195.7
8+75			
S'N		7.0	194.0
N.L.		9.3	191.7
+4		9.9	191.1
+4		11.7	189.3
cb		12.0	189.0
+8		12.7	188.3
1/4		15.9	185.1
+1		15.8	185.2
+2		14.1	186.9
E		13.6	187.4
+7		14.2	186.8
1/4		11.2	189.8
+10		4.5	196.5
cb		3.9	197.1
S.L.		2.3	198.7

Street offset 1.50 North
at W Bound. Pt Loma Hts

201.04

8+86¹⁴ = Section on Boundary = 8+83 on North

S.L.	2.1	198.9
cb	4.0	197.0
+4	4.5	196.5
+5	7.0	194.0
+9	8.4	192.6
'A	12.7	188.3
+7	14.7	186.3
⊖	14.4	186.6
+10	15.2	185.8
⊖	17.0	184.0
+2	17.0	184.0
+5	12.7	188.3
cb	12.5	188.5
+10	12.3	188.7
+10	10.2	190.8
N.L. (Pt Loma Hts.)	9.6	191.4
N.L. (Ocean Beach)	8.8	192.2
5' N	8.0	193.0
9+00		
5' N	9.5	191.5
N.L.	10.2	190.8
+2	11.4	189.6
+2	12.7	188.3
cb	13.5	187.5
+4	12.3	188.7

9+00

201.04

'A	17.6	183.4
+2	18.8	182.2
+5	16.5	184.5
⊖	16.6	184.4
+6	16.6	184.4
+9	18.0	183.0
'A	15.7	185.3
+12	4.2	196.8
cb	4.2	196.8
S.L.	2.0	199.0
9+25		
by N.L.	2.2	198.8
cb	4.5	196.5
+2	4.9	196.1
+9	16.2	184.8
'A	19.2	181.8
+5	19.1	181.9
+7	18.4	182.6
⊖	18.5	182.5
+4	18.6	182.4
+6	20.1	180.9
+10	18.4	182.6
'A	18.1	182.9
+8	13.5	187.5
cb	13.8	187.2
+11	13.3	187.7

9+25	201.04		
+12		11.8	1892
N.L.		11.7	1893
1'N		11.1	1899
+5		11.2	1898
T.P.	0.88	189.00	1292 188.12
9+50			
N.L.		1.2	1878
+3		2.2	1868
+5		2.8	1862
+8		3.0	1860
+8		4.6	1844
cb		4.6	1844
+3		4.5	1845
+4		3.2	1858
+7		1.7	1873
+10		2.4	1866
+11		6.1	1829
1/4		6.6	1824
+6		9.5	1795
+7		11.1	1779
+9		8.5	1805
±		8.9	1801
+6		8.7	1803
+10		11.0	178.0
1/2		6.3	1827
+3		4.0	1850

9+50	189.00		
cb		+6.6	1956
S.L.		+8.7	1977
9+75			
S.L.		+6.7	195.7
cb		+4.7	1937
+7		5.9	1831
1/4		7.4	1816
+3		14.4	1746
+7		14.2	1748
+8		11.0	1780
±		11.2	1778
+7		11.5	1775
+9		11.6	1774
+10		11.6	1774
1/4		8.4	180.6
+5		3.6	185.4
+7		3.0	186.0
+11		4.9	184.1
cb		5.1	183.9
+5		4.9	184.1
+5		3.4	185.6
N.L.		3.9	185.1
S'N		4.1	184.9

10+00	189.00		
S.N	9.1	179 9	
N.L.	8.2	180 8	
+12	5.8	183 2	
+12	6.8	182 2	
cb	6.8	182 2	
+10	6.0	183 0	
1/4	16.9	172 1	
+3	16.9	172 1	
+8	13.7	175 3	
±	13.5	175 5	
+5	13.5	175 5	
+8	16.1	172 9	
1/4	16.1	172 9	
cb	+2.2	191 2	
S.L.	+3.7	192 7	
10+25			
S.L.	+1.6	190 6	
cb	0.3	188 7	
1/4	14.3	174 7	
1/4	17.8	171 2	
+7	18.3	170 7	
+7	16.3	172 7	
±	16.0	173 0	
+5	16.3	172 7	
+6	18.8	170 2	

10+25	189.00		
+8	18.8	170.2	
1/4	12.5	176.5	
+4	8.6	180.4	
cb	9.5	179.5	
+2	9.7	179.3	
+2	8.6	180.4	
N.L.	9.6	179.4	
T.P. 0.23	178.08	11.15	177.85 ✓
10+50			
N.L.	2.1	176.0	
+5	1.4	176.7	
cb	0.6	177.5	
+7	+0.2	178.3	
1/4	9.0	169.1	
+5	9.0	169.1	
+8	7.6	170.5	
±	7.4	170.7	
+6	7.3	170.8	
+7	9.0	169.1	
1/4	8.8	169.3	
+11	+5.0	183.1	
cb	+6.0	184.1	
+15	+6.4	184.5	
+2	+8.2	186.3	
S.L.	+9.5	187.6	

11.5
5.6

10.7

48

10+75

178.08

11+00

171.67

SL.		+7.5	185.6
+10		+5.9	184.0
cb		+4.0	182.1
+2		+3.5	181.6
+10		10.6	167.5
1/4		10.6	167.5
+3		10.6	167.5
+4		9.8	168.3
±		9.6	168.5
+5		9.4	168.7
+7		10.3	167.8
+10		10.3	167.8
1/4		6.4	171.7
+4		2.2	175.9
cb		3.2	174.9
+2		2.6	175.5
+5		3.1	175.0
N.L.		4.6	173.5
T.P.	5.37	171.67	11.78
11+00			166.30
N.L.		1.1	170.6
+12		+0.5	172.2
+12		1.4	170.3
cb		1.6	170.1
1/4		1.6	170.1
+6		5.6	166.1

+10		5.3	166.4
±		5.8	165.9
+7		5.7	166.0
+10		6.7	165.0
1/4		6.2	165.5
+10		+4.1	175.8
cb		+4.5	176.2
+2		+5.9	177.6
+7		+7.2	178.9
+7		+9.0	180.7
SL.		+10.2	181.9
11+25			
SL.		+6.3	178.0
+9		+4.2	175.9
+9		+3.1	174.8
cb		+2.2	173.9
+4		+0.5	172.2
+9		2.3	169.4
1/4		9.0	162.7
+5		9.1	162.6
+6		8.4	163.3
±		8.0	163.7
1/4		8.4	163.3
+3		4.0	167.7
cb		4.1	167.6
+3		4.0	167.7

11+25	17167		
+3	2.5	1692	
N.L.	3.6	1681	
11+50			
N.L.	7.6	164.1	
+12	6.4	165.3	
cb	6.6	165.1	
1/4	6.6	165.1	
+4	11.0	160.7	
+8	10.0	161.7	
⊕	10.3	161.5 ^{161.4}	
+6	10.2	161.5	
+10	11.4	160.3	
+10	12.6	159.1	
+12	12.6	159.1	
1/4	10.7	161.0	
+5	6.8	164.9	
+11	5.0	166.7	
+12	2.8	168.9	
cb	2.7	169.0	
+2	2.6	169.1	
+2	+0.1	171.8	
S.L.	+1.3	173.0	

11+75	171.67		
S.L.	3.3	168.4	
cb	4.7	167.0	
+0.5	6.6	165.1	
+8	7.3	164.4	
1/4	12.4	159.3	
+1	15.0	156.7	
+5	15.4	156.3	
+6	13.4	158.3	
⊕	12.6	159.1	
1/4	12.7	159.0	
+2	10.5	161.2	
+9	10.9	160.8	
cb	10.7	161.0	
+5	11.2	160.5	
N.L.	12.6	159.1	
11+86			
N.L.	14.4	157.3	(156.3) ?
cb	13.9	157.8	
1/4	13.6	158.1	
+3	14.5	157.2	
+6	14.8	156.9	
⊕	13.9	157.8	
+6	14.4	157.3	
+9	16.2	155.5	
+12	16.2	155.5	

11+86	171.67		
1/4		13.8	157.9
+5		9.2	162.5
+7		8.5	163.2
+8		7.6	164.1
cb		7.2	164.5
S.L.		5.2	166.5
12+00			
S.L.		7.3	164.4
cb		9.7	162.0
+6		10.1	161.6
+8		11.9	159.8
+10		12.5	159.2
1/4		14.8	156.9
1/4		16.9	154.8
+4		16.9	154.8
+5		15.7	156.0
±		15.1	156.6
+9		15.4	156.3
+11		17.9	153.8
1/4		17.9	153.8
+3		15.1	156.6
cb		15.0	156.7
N.L.		16.0	155.7
T.P.	0.41	159.17 159.15	12.91 158.76 ✓

12+16	159.17 159.15		
10'N		5.8	153.4
N.L.		5.5	153.7 ✓
+2		8.6	150.6
+11		8.0	151.2
+13		4.7	154.5
cb		4.5	154.7
1/4		4.3	154.9
±		4.0	155.2 ✓
+7		4.3	154.9
+9		5.4	153.8
1/4		5.2	154.0
+2		2.6	156.6
+5		1.4	157.8
+10		0.0	159.2
cb		10.7	159.9
+12		3.0	162.2
S.L.		4.0	155.2 ✓
12+20			
S.L.		+3.2	(162.4) 162.3
+1		+2.8	162.0
cb		+0.3	159.5
+5		0.5	158.7
+8		1.8	157.4
+11		2.9	156.3
1/4		5.5	153.7

12+20	159.15		
1/4 +6	5.6	153	6
+7	4.6	154	6
⊕	4.3	154	8
1/4	4.6	154	6
cb	5.0	154	2
+7	5.3	153	9
+7	8.9	150	3
N.L.	9.6	(149)	6
3'N	9.5	149	7
8'N	5.9	153	3
15'N	6.4	152	8
12+25			
15'N	6.8	152	4
10'N	6.6	152	6
6'N	10.4	148	8
N.L.	10.0	149	2
+3	5.5	153	7
cb	5.4	153	8
1/4	5.0	154	2
⊕	4.6	154	6
+6	5.9	153	3
+10	5.7	153	5
1/4	4.6	154	6
+2	3.4	155	8
+7	1.5	157	7
cb	0.4	158	8

12+25	159.15		
S.L.	+2.6	161.8	✓
12+36		160.3	
S.L.	+1.1	160.2	
cb	1.5	157.7	
+10	3.0	156.2	
1/4	5.2	154.0	
+1	7.9	151.3	
+4	7.6	151.6	
+6	5.9	153.3	
⊕	5.5	153.7	✓
+5	6.0	153.2	
1/4	5.9	153.3	
+3	5.9	153.3	
cb	7.1	152.1	
N.L.	11.7	147.5	✓
9'N	12.1	147.1	
14'N	11.1	148.1	
20'N	9.2	150.0	
12+40			
20'N	13.0	146.2	
7'N	12.2	147.0	
3'N	12.2	147.0	
N.L.	7.7	151.5	✓
+5	7.0	152.2	
cb	7.8	151.4	

	159.15	
12+40		
+10	6.3	152.9
1/4	6.2	153.0
+8	6.2	153.0
ϕ	5.8	153.4 [✓]
+7	6.3	152.9
+10	8.0	151.2
+11	8.0	151.2
1/4	6.4	152.8
+2	4.5	154.7
+5	3.0	156.2
cb	1.8	157.4
S.L.	+0.7	159.9 [✓]
12+50		
S.L.	0.6	158.6 [✓]
cb	2.9	156.3
+8	3.9	155.3
1/4	7.0	152.2
+3	9.4	149.8
+4	9.4	149.8
+5	7.5	151.7
ϕ	6.5	152.6 ¹⁵²
+4	6.9	152.3
1/4	6.7	152.5
cb	8.0	151.2
+5	9.2	150.0
N.L.	8.5	150.7

	159.15	
12+50		
9'N	8.7	150.5
10'N	13.1	146.1
15N	13.6	145.6
12+60 = E.L. Fraude		
15'N	10.7	148.5
2'N	9.4	149.8
N.L.	9.6	149.6 [✓]
+6	10.4	148.8
+11	9.4	149.8
cb	9.7	149.5
1/4	7.5	151.7
ϕ	7.1	152.0 ^{152.1}
+5	7.4	151.8
+6	9.7	149.5
+10	9.9	149.3
1/4	7.5	151.7
+5	4.6	154.6
cb	3.7	155.5
S.L.	2.3	156.8

Santa Cruz From Froude to Ebers

53

0 + 00 = W.L. Froude 159.15

S.L.	10.4	¹⁴⁸⁸ 1487
cb	13.7	1455
+5	17.4	1418
+6	14.8	1444
1/4	13.1	1461
+4	10.9	1483
£	10.4	¹⁴⁸⁸ 1487
+12	11.0	1482
1/4	11.7	1475
+7	14.0	1452
+10	15.1	1441
cb	14.2	1450
+3	13.3	1459
+10	16.8	1424
N.L.	17.1	1420
15'N	18.5	1407
T.P.	0.04	^{146.60} 146.60
0 + 25	12.59	146.56 ^{146.58}
15N	8.2	1384
N.L.	7.0	1396
cb	5.9	1407
+9	5.2	1414
1/4	3.3	1433
+5	0.8	1458
£	0.0	146.6

0 + 25 146.60

£ + 9	0.2	146.4
1/4	5.0	141.6
+2	6.8	139.8
+5	6.7	139.9
+10	0.5	146.1
cb	0.5	146.1
S.L.	+0.1	146.7 ✓
0 + 50		
S.L.	3.9	142.7 ✓
+9	5.7	140.9
cb	5.7	140.9
+2	5.6	141.0
+3	7.6	139.0
+5	7.6	139.0
+6	5.6	141.0
+11	5.2	141.4
1/4	4.2	142.4
+4	2.5	144.1
£	2.3	144.3 ✓
1/4	2.8	143.8
+8	7.5	139.1
cb	8.7	137.9
N.L.	9.2	137.4 ✓
15'N	10.2	136.4

0475	146.60	
15'N	11.3	135.3
NL	10.3	136.3
cb	9.1	137.5
+9	8.5	138.1
1/4	5.9	140.7
+3	4.7	141.9
1/2	4.6	142.0
+9	5.6	141.0
1/4	7.0	139.6
+7	7.6	139.0
+11	10.4	136.2
+10	8.9	137.7
cb	8.9	137.7
+2	8.1	138.5
S.L.	7.5	139.1
1+00		
SL	9.9	136.7
+11	9.5	137.1
cb	12.2	134.4
+2	12.0	134.6
+4	9.3	137.3
+11	9.3	137.3
1/4	8.7	137.9
+10	7.0	139.6
1/2	6.9	139.7
+3	7.1	139.5

1+00	146.60	
1+10	6.1	140.5
1/4	6.9	139.7
+8	10.0	136.6
cb	11.0	135.6
N.L.	11.8	134.8
15N	13.0	133.6
1+25		
15N	14.2	132.4
N.L.	13.8	132.8
cb	13.3	133.3
+7	13.1	133.5
1/4	10.7	135.9
+4	9.1	137.5
+8	9.5	137.1
1/2	9.2	137.4
+9	9.9	136.7
1/4	11.4	135.2
cb	11.6	135.0
+8	11.7	134.9
+12	15.0	131.6
SL	13.5	133.1
2.5	11.9	134.7
10.5	11.2	135.4

1443	14660		
10N	13.1	1335	
4N	13.5	1331	
2N	14.6	1320	
5 ⁹ NL	16.1	1305	
+5	13.1	1335	
cb	13.2	1334	
+11	13.1	1335	
1/4	12.9	1337	
+5	11.3	1353	
⊕	10.5	1361	
+9	10.8	1358	
1/4	12.5	1341	
+5	14.3	1323	
cb	14.2	1324	
NL	15.4	1312	
15N	16.4	1302	
1450			
15N	16.0	1299	
NL	16.0	1306	
cb	14.9	1317	
+7	15.4	1312	
1/4	13.4	1332	
+4	11.6	1348	
⊕	7.6	1390	?
+7	12.5	1341	

1450	14660		
6 1/4	13.9	132.7	
cb	13.7	132.9	
+11	13.8	132.8	
5.6	13.8	132.8	
3'S	15.7	129.9	
8'S	13.9	132.7	
13'S	13.0	133.6	
T.P. 070	134.53	12.77	133.83
1475			
13'S	2.7	131.8	
8'S	5.2	129.3	
5'S	2.9	131.6	
5L	3.2	131.3	
cb	4.0	130.5	
+9	4.1	130.4	
1/4	3.6	130.9	
+9	1.7	132.8	
⊕	1.5	133.0	
+9	2.2	132.3	
1/4	3.3	131.2	
+4	5.4	129.1	
cb	6.1	128.4	
NL	6.2	128.3	
15N	6.6	127.9	

1+80	134.53		
15N	7.11	(127 4)	
N.L.	6.7	127.8	
cb	6.9	127.6	
+7	6.3	128.2	
1/4	4.8	129.7	
+6	2.3	132.2	
¢	2.0	132.5	
+5	2.2	132.3	
1/4	3.8	130.7	
+5	4.6	129.9	
cb	4.5	130.0	
S.L.	3.3	131.2	
2S	6.0	128.5	
7S	6.0	128.5	
10S	2.7	131.8	
1+84			
10S	3.1	131.4	
5S	3.6	130.9	
3S	6.3	128.2	
S.L.	6.3	128.2	
+2	3.6	130.9	
cb	4.5	130.0	
+11	4.8	129.7	
1/4	3.9	130.6	
+8	2.4	132.1	
¢	2.1	132.4	

1+84	134.53		
¢+8	2.6	131.9	
1/4	4.5	130.0	
+7	6.6	127.9	
cb	7.1	127.4	
N.L.	7.1	127.4	
15N	7.3	127.2	
1+96			
15N	8.1	126.4	
N.L.	8.0	126.5	
cb	8.3	126.2	
+5	8.0	126.5	
+11	6.9	127.6	
1/4	6.0	128.5	
+7	3.7	130.8	
¢	3.5	131.0	
+5	3.9	130.6	
1/4	5.2	129.3	
+2	5.8	128.7	
cb	5.0	129.5	
76	4.7	129.8	
+7	7.0	127.5	
S.L.	6.8	127.7	
1S	4.7	130.3	
15'S	4.1	130.4	

2+000	134.53	
155	4.4	1301
S.L.	4.6	1299
+7	4.9	1296
+3	7.1	1274
+7	7.1	1274
+9	5.0	1295
cb	5.4	1293
+12	5.9	1286
1/4	5.4	1291
+8	4.0	1305
⊕	3.7	1308
+6	4.0	1305
1/4	5.9	1286
cb	8.4	1261
N.L.	8.6	1259
15N	8.6	1259
2+25		
15N	10.4	1241
N.L.	10.9	1236
cb	10.8	1237
+7	10.0	1245
1/4	7.9	1266
+4	6.2	1283
⊕	6.2	1283
+9	6.4	1281

2+25	134.53	
5A	7.4	127.1
+6	7.4	127.1
+8	8.2	126.3
+11	9.1	125.4
+12	6.8	127.7
cb	6.8	127.7
+11	7.0	127.5
S.L.	7.5	127.0
+25	6.6	127.9
155	6.0	128.5
2+50		
105	8.6	125.9
S.L.	9.2	125.3
+9	9.0	125.5
+11	10.4	124.1
cb	9.9	124.6
+1	9.5	125.0
1/4	9.4	125.1
+8	8.2	126.3
⊕	8.2	126.3
+8	8.8	125.7
1/4	10.8	123.7
+3	11.5	123.0
cb	12.9	121.6
N.L.	12.9	121.6
15N	13.1	121.4

2+75	134.53			3+00	123.00		
15N		15.3	1192	1/4		1.7	121.1
N.L.		15.6	1189	±		1.2	121.8
cb		15.4	1191	+9		1.7	121.3
+9		15.6	1189	1/4		3.1	119.9
1/4		13.3	1212	+7		6.8	116.2
+5		10.9	1236	cb		6.9	116.1
±		10.5	1240	N.L.		6.2	116.8
+7		11.0	1235	15N		6.3	116.7
+9		11.7	1228	3+25			
1/4		11.5	1230	15N		9.0	114.0
+2		11.4	1231	N.L.		8.9	114.1
+6		13.5	1210	cb		9.4	113.6
+10		11.7	1228	+3		9.0	114.0
cb		11.4	1231	1/4		5.3	117.7
S.L.		10.7	1238	+4		4.0	119.0
10S		10.5	1240	±		3.6	119.4
J.P.	0.55	123.00	12.08	+5		3.6	119.4
3+00			122.45	+10		4.7	118.3
10N		1.6	1214	1/4		5.0	118.0
9 N.L.		1.8	1212	+4		5.2	117.8
+10		2.6	1204	+5		6.4	116.6
cb		2.3	1207	+6		5.2	117.8
+3		2.6	1204	cb		4.9	118.1
+6		4.1	1189	S.L.		3.1	117.9
+8		2.7	1203	10S		4.6	118.4

	12300	
3+50		
105	7.4	1156
S.L.	8.1	1149
cb	7.7	1153
+10	7.9	1151
1/4	7.2	1158
+6	6.0	1170
E	5.8	1172
+10	6.6	1164
1/4	8.0	1150
+8	10.5	1125
cb	11.5	1115
N.L.	11.2	1118
15N	10.7	1123
3+75		
15N	13.1	1099
N.L.	13.5	1095
cb	13.2	1098
+8	13.0	1100
1/4	10.3	1127
+5	8.2	1148
E	7.9	1151
+10	8.2	1148
1/4	9.6	1134
+10	9.2	1138
cb	9.5	1135

	12300	
3+75		
S.L.	10.5	1125
105	10.2	112.8
4+00		
105	12.0	111.0
S.L.	12.8	1102
+4	13.0	110.0
+8	12.6	110.4
cb	12.5	110.5
1/4	12.3	110.7
+1	12.3	110.7
+7	10.5	112.5
E	10.3	112.7
+5	10.5	112.5
1/4	12.9	110.1
+8	14.5	108.5
cb	15.6	107.4
N.L.	16.4	106.6
15N	16.0	107.0
TP. 062	111.32	12.30
		110.70

	111.32	
4+25		
15N	6.0	1053
N.L.	6.0	1053
cb	6.0	1053
+8	4.9	1064
1/4	2.4	1089
+3	1.1	1102
⊕	0.6	1107
+10	1.4	1099
1/4	2.6	1087
cb	2.9	1084
S.L.	3.1	1082
10.5	2.9	1084
4+50		
10.5	4.5	1068
S.L.	4.5	1068
+8	4.9	1064
cb	4.4	1069
1/4	4.3	1070
+5	3.1	1082
⊕	3.0	1083
+10	3.1	1082
1/4	3.8	1075
+6	6.8	1045
cb	7.5	1038
N.L.	7.9	1034
15N	7.9	1034

	111.32	
4+75		
15N	9.4	1019
N.L.	9.6	1017
cb	9.6	1017
+3	9.6	1017
1/4	7.2	104.1
+4	5.4	105.9
⊕	5.4	105.9
+5	5.5	105.8
1/4	5.7	105.6
cb	6.0	105.3
S.L.	6.2	105.1
15	5.4	105.9
10.5	4.8	106.5
5+00		
10.5	6.1	105.2
S.L.	7.1	104.2
+3	7.0	104.3
cb	7.6	103.7
+7	8.0	103.3
1/4	7.9	103.4
+4	8.1	103.2
⊕	7.5	103.8
+8	7.8	103.5
1/4	10.1	101.2
cb	10.7	100.6

5+00	111.32		
N.L.	11.7	99.6	
15N	11.7	99.6	
5+25			
15N	12.6	98.7	
N.L.	12.1	99.2	
+10	12.7	100.6	
cb	11.0	100.3	
1/4	11.3	100.0	
+8	9.6	101.7	
1/2	9.8	101.5	
+5	10.0	101.3	
1/4	9.4	101.9	
+6	9.0	102.3	
+8	9.3	102.0	
cb	9.0	102.3	
S.L.	8.1	103.2	
105	7.0	104.3	
5+50			
105	9.3	102.0	
SL	10.0	101.3	
+5	10.5	100.8	
cb	10.6	100.7	
1/4	11.1	100.2	
+2	11.6	99.7	
+4	11.3	100.0	

5+50	111.32		
1/2	11.1	100.2	
+8	11.1	100.2	
1/4	12.3	99.0	
cb	12.7	98.6	
+8	13.3	98.0	
N.L.	13.3	98.0	
15N	13.6	97.7	
5+75			
15N	14.6	96.7	
N.L.	12.4	98.9	
cb	13.8	97.5	
+8	13.5	97.8	
1/4	12.8	98.5	
+9	12.5	98.8	
+10	13.5	97.8	
1/2	13.7	97.6	
+1	12.7	98.6	
+10	12.7	98.6	
1/4	12.3	99.0	
+3	11.7	99.6	
cb	12.1	99.2	
S.L.	11.4	99.9	
105	10.5	100.8	
T.P. 1.11	100.15	12.28	99.04

5+88	100.15		
10 S		0.0	100 1
S.L.		0.6	99.5
+8		1.4	98.7
cb		0.9	99.2
1/4		1.3	98.8
1/4		3.5	96.6
+4		2.4	97.7
±		2.8	97.3
+3		3.1	97.0
+8		2.1	98.0
1/4		2.3	97.8
cb		3.0	97.1
+10		2.7	97.4
N.L.		3.9	96.2
15 N		4.6	95.5
5+90			
15 N		4.6	95.5
N.L.		4.1	96.0
+4		3.4	96.7
cb		3.0	97.1
1/4		2.4	97.7
+5		2.4	97.7
+9		3.5	96.6
±		3.1	97.0
+9		2.8	97.3

5+90	100.15		
S 1/4		4.3	95.8
+10		4.1	96.0
+11		1.2	98.9
cb		1.1	99.0
+5		1.5	98.6
S.L.		0.8	99.3
10 S		0.2	99.9
5+99			
10.5		0.2	99.9
S.L.		1.5	98.6
+11		1.6	98.5
cb		4.3	95.8
1/4		4.6	95.5
+8		3.8	96.3
±		4.1	96.0
+6		4.6	95.5
+9		5.8	94.3
+10		4.3	95.8
1/4		2.9	97.2
cb		3.2	96.9
+13		2.9	97.2
N.L.		3.6	96.5
5 N		5.5	94.6
15 N		6.3	93.8

6+00=E.L. Ebers
100.15

15 N	6.8	93.3	
N.L	6.1	94.0	
cb	5.6	94.5	
+2	5.5	94.6	
+3	6.3	93.8	
1/4	5.3	94.8	
+3	6.0	94.1	
+6	4.9	95.2	
±	4.5	95.6	
+7	4.3	95.8	
1/4	4.9	95.2	
cb	4.6	95.5	
S.L.	4.4	95.7	
105	3.9	96.2	
Monsieur			
B.M. Ebers & Santa Cruz	4.60	95.55	95.42
T.R. 10.97 110.44	0.68	99.47	
B.M. Mon N.W. Ebers & Coronado	4.89	105.55	

Sept 19-28
X Sec Coronado From W.L. Loudon.
Santa Barbara to EL Guizot. 63
80'5+ 40' Roadway 70' cbs

B.M. 11.20	251.43	240.17	
0+00=W.L. Santa Barbara			
scb	11.20	240.23	
gut	11.6	239.8	
1/4	11.6	239.8	
±	11.4	240.0	
1/4	11.5	239.9	
+6	11.7	239.7	
gut	11.4	240.0	
Ncb	11.33	240.10	
0+25			
Ncb	10.21	241.22	
gut	10.6	240.8	
+3	10.7	240.7	
1/4	10.4	241.0	
±	10.2	241.2	
1/4	10.3	241.1	
gut	10.6	240.8	
scb	9.96	241.47	
0+50			
scb	8.80	242.63	
gut	9.7	241.7	
1/4	9.1	242.3	
±	8.9	242.5	
1/4	9.2	242.2	
+7	9.7	241.7	

Cbs 5 walks in
0+00 to 5+80

In 5+80 to 6+00 on North
but washed out & broken.
5 walks fair to 6+00

0+50	251.93		
Ngt	9.6	241.8	
Ncb	9.05	242.38	
0+75			
Ncb	7.92	243.51	
gut	8.7	242.7	
+2	8.7	242.7	
1/4	8.1	243.3	
¢	7.7	243.7	
1/4	8.0	243.4	
gut	8.7	242.7	
Scb	7.54	243.89	
1+00			
Scb	6.33	245.10	
gut	7.5	243.9	
1/4	6.8	244.6	
¢	6.5	244.9	
1/4	7.0	244.4	
gut	7.7	243.7	
Ncb	6.77	244.66	
1+25			
Ncb	5.60	245.83	
gut	6.7	244.7	
+7	6.0	245.4	
1/4	5.7	245.7	
¢	5.5	245.9	

1+25	251.93		
1/4	5.6	245.8	
gut	6.3	245.1	
Scb	5.06	246.37	
1+50			
Scb	3.90	247.53	
gut	5.1	246.3	
1/4	4.4	247.0	
¢	4.4	247.0	
1/4	4.7	246.7	
gut	5.5	245.9	
Ncb	4.51	246.92	
1+75			
Ncb	3.66	247.77	
gut	4.7	246.7	
1/4	3.9	247.5	
¢	3.4	248.0	
1/4	3.5	247.9	
+7	3.7	247.7	
gut	4.1	247.3	
Scb	2.97	248.46	
2+00			
Scb	2.33	249.10	
gut	3.3	248.1	
1/4	2.9	248.5	
¢	2.8	248.6	

2+00	251.43		
N $\frac{1}{4}$	3.3	248.1	
gut	3.9	247.5	
Ncb	3.13	248.30	
2+25			
Ncb	2.91	248.52	
gut	3.6	247.8	
$\frac{1}{4}$	2.9	248.5	
$\frac{1}{2}$	2.5	248.9	
$\frac{1}{4}$	2.5	248.9	
+5	2.6	248.8	
gut	2.8	248.6	
Scb	2.00	149.4	
2+50			
Scb	2.13	149.30	
gut	3.0	248.4	
$\frac{1}{4}$	2.6	248.8	
$\frac{1}{2}$	2.5	148.9	
$\frac{1}{4}$	2.9	248.5	
gut	3.7	247.7	
Ncb	3.03	148.40	
2+75			
Ncb	3.45	147.98	
gut	4.4	247.0	
$\frac{1}{4}$	3.6	247.8	
$\frac{1}{2}$	3.1	148.3	

65

2+95	251.43		
$\frac{1}{4}$	3.0	248.4	
gut	3.1	248.3	
Scb	2.47	248.96	
3+00			
Scb	3.18	248.25	
gut	4.0	247.4	
$\frac{1}{4}$	3.8	247.6	
$\frac{1}{2}$	3.9	247.5	
$\frac{1}{4}$	4.4	247.0	
gut	5.1	246.3	
Ncb	4.25	247.18	
3+25			
Ncb	5.32	246.11	
gut	6.1	245.3	
$\frac{1}{4}$	5.4	246.0	
$\frac{1}{2}$	4.9	246.5	
$\frac{1}{4}$	4.8	246.6	
gut	4.9	246.5	
Scb	4.22	247.21	
3+50			
Scb	5.54	245.89	
gut	6.3	245.1	
$\frac{1}{4}$	6.1	245.3	
$\frac{1}{2}$	6.2	245.2	
$\frac{1}{4}$	6.6	244.8	

3+50

251.43

Ngut	7.6	243.8
Ncb	6.64	244.79
3+75		
Ncb	8.09	243.34
gut	8.9	242.5
1/4	8.0	243.4
¢	7.5	243.9
1/4	7.5	243.9
gut	7.6	243.8
Scb	6.96	244.47

4+00

Scb	8.37	243.06
gut	9.2	242.2
1/4	8.9	242.5
¢	8.9	242.5
1/4	9.0	241.8
gut	10.3	241.1
Ncb	9.58	241.85

4+25

Ncb	11.00	240.43
gut	11.9	239.5
1/4	10.9	240.5
¢	10.4	241.0
1/4	10.3	241.1
gut	10.5	240.9
Scb	9.76	241.67

4+50

251.43

Scb	11.19	240.24
gut	11.8	239.6
1/4	11.6	239.8
¢	11.7	239.7
1/4	12.4	239.0
gut	13.4	238.0
Ncb	12.43	239.00
TP.054	238.92	13.05
4+75		238.38

4+75

Ncb	1.34	237.58
gut	2.0	236.9
+1	2.1	236.8
+2	1.8	237.1
1/4	1.2	237.7
¢	0.6	238.3
1/4	0.5	238.4
gut	0.6	238.3
Scb	0.03	238.89

5+00

Scb	1.48	237.44
gut	2.4	236.5
1/4	2.0	236.9
¢	2.0	236.9
1/4	2.6	236.3
+6	3.2	235.7
gut	3.4	235.5

	23892		
5+00			
Ncb	2.81	136.11	
5+25			
Ncb	4.29	134.53	
gut	5.2	233.7	
+3	4.8	234.1	
1/4	4.1	234.8	
¢	3.5	135.4	
1/4	3.4	235.5	
+5	3.3	235.6	
gut	3.5	235.4	
Scb	2.92	136.00	
5+50			
Scb	4.37	134.55	
gut	5.0	233.9	
+5	4.6	234.3	
1/4	4.8	234.1	
¢	5.0	133.9	
1/4	5.3	233.6	
+5	5.7	233.2	
gut	6.3	232.6	
Ncb	5.66	133.26	

67

	23892		
5+75			
Ncb.	7.10	231.82	
gut	7.6	231.3	
+5	7.1	231.8	
1/4	6.7	232.2	
¢	6.5	232.4	
1/4	6.2	232.7	
gut	6.0	232.9	
Scb	5.66	233.26	
6+00			
SL.	7.0	231.9	
+7	6.8	232.1	
cb	7.1	231.8	
+2	7.8	231.1	
1/4	8.2	230.7	
¢	8.3	230.6	
+6	8.5	230.4	
1/4	8.5	230.4	
+6	8.7	230.2	
+8	9.1	229.8	
cb	8.7	230.2	
NL.	8.1	230.7	

6+10

23892

NL end ret	8.27	230.65
put a NL	8.8	230.1
+16	9.1	229.8
cb	10.4	228.5
+6	8.8	230.1
1/4	8.6	230.3
+7	8.4	230.5
⊕	8.4	230.5
1/4	8.2	230.7
cb	7.9	231.0
+5	7.7	231.0
+8	7.3	231.6
S.L.	7.3	231.6
6+16		
S.L.	8.4	230.5
cb	8.1	230.8
1/4	8.1	230.8
+8	8.3	230.6
⊕	8.2	230.7
1/4	8.5	230.4
cb	9.1	229.8
+2	10.7	228.2
+11	10.8	228.1
+11	9.0	229.9
N.L.	8.7	230.2

68

6+17

23892

NL	11.6	227.3
+17	10.7	228.2
+18	9.0	229.9
cb	8.9	230.0
1/4	8.5	230.4
⊕	8.2	230.7
1/4	8.1	230.8
cb	8.1	230.8
S.L.	8.4	230.5
6+20		
S.L.	8.3	230.6
cb	8.0	230.9
1/4	8.0	230.9
⊕	8.1	230.8
1/4	8.5	230.4
cb	8.7	230.2
+4	8.9	230.0
+10	9.8	229.1
+16	10.2	228.7
N.L.	11.5	227.4

23892

6+30 = 6 Guizot

N.L.	11.5	227.4
+11	9.2	229.7
+17	8.6	230.3
cb	8.5	230.4
1/4	8.4	230.5
2	8.2	230.7
1/4	8.0	230.9
cb	7.9	231.0
+12	8.0	230.9
S.L.	8.4	230.5
6+40		
S.L.	8.9	230.0
+10	8.5	230.4
cb	8.2	230.7
1/4	8.2	230.7
2	8.2	230.7
1/4	8.5	230.4
+5	8.7	230.2
cb	8.6	230.3
+8	8.7	230.2
+15	10.1	228.8
N.L.	10.7	228.2

6+46

23892

69

N.L.	8.6	230.3
+1	8.5	230.4
+5	9.2	229.7
+10	9.1	229.8
+17	8.7	230.2
cb	8.8	230.1
+8	8.9	230.0
1/4	8.7	230.2
2	8.5	230.4
+2	8.4	230.5
+5	8.5	230.4
1/4	8.4	230.5
+5	8.4	230.5
cb	8.5	230.4
S.L.	9.3	229.6
6+50		
S.L.	8.8	230.1
+10	8.4	230.5
+11	8.9	230.0
cb	8.9	230.0
1/4	8.6	230.3
2	8.6	230.3
+5	8.8	230.1
1/4	9.0	229.9
cb	9.0	229.9
+6	9.4	229.5

238.92

6+50 = w.cb line Guizot
 +9 8.8 2301
 +15 9.2 2297
 +18 8.7 2302
 N.L. 8.9 2300

Coronado - Guizot to Ebers

60' St Ad Rdway, 10' cbs

0+00 = w.L Guizot
 N.L. 9.3 2296
 +9. 9.4 2295
 cb 10.0 228.9
 1/4 9.6 2293
 1/2 9.3 2296
 +4 9.2 2297
 1/4 9.4 2295
 1/2 9.6 2293
 +2 8.9 2300
 S.L. 8.8 2301
 0+35
 S.L. 11.1 2278
 cb 10.9 2280
 +1 11.9 2270
 +5 11.6 2273
 1/4 11.3 2276
 1/2 11.3 2276
 1/4 11.5 2274
 +8 11.9 2270

0+25 238.92

N.cb 12.2 2267
 +2 11.3 2276
 N.L. 11.4 227.5
 0+50
 N.L. 13.9 2250
 +9 13.6 225.3
 cb 14.4 2245
 1/4 13.9 225.0
 1/2 13.4 225.5
 1/4 13.5 225.4
 +7 13.6 225.3
 +7 13.7 225.2
 cb 13.1 225.8
 S.L. 13.0 225.9
 T.P. 0.07 226.67 12.32 226.60
 0+75
 S.L. 3.8 2229
 +3 3.2 223.5
 cb 2.7 224.0
 +1 3.8 222.9
 +2 3.6 223.1
 1/4 3.4 223.3
 1/2 3.4 223.3
 +3 3.5 223.2
 1/4 4.0 222.7

70

	22667	
0+75		
Ncb	4.7	RRRP
+1	4.0	222.7
NL	3.7	223.0
1+00		
NL	5.7	221.0
+9	6.3	220.4
cb	7.1	219.6
+3	6.9	219.8
1/4	6.3	220.4
1/4	5.9	220.8
1/4	5.7	220.8
+9	6.2	220.5
cb	5.3	221.4
+9	5.4	221.3
S.L.	5.7	221.0
1+25		
S.L.	8.3	218.4
+2	7.9	218.8
cb	7.7	219.0
+1	8.6	218.1
1/4	8.3	218.4
1/4	8.1	218.6
+7	8.3	218.4
1/4	8.7	218.0
48	9.3	217.4

-1

	226.67	
1+25		
Ncb	9.5	217.2
+1	8.6	218.1
NL	8.2	218.5
1+50		
NL	10.1	216.6
+3	10.6	216.1
+9	10.8	215.9
cb	11.8	214.9
+5	11.2	215.5
1/4	11.0	215.7
1/4	10.6	216.1
1/4	10.5	216.2
+9	10.7	216.0
cb	10.0	216.7
S.L.	10.1	216.6
1+75		
S.L.	11.5	215.2
+1	12.2	214.5
cb	12.1	214.6
+1	13.0	213.7
1/4	12.9	213.8
1/4	12.9	213.8
1/4	13.1	213.6
+4	13.2	213.5
+7	13.6	213.1

1475	226.67		
+9		14.0	212.7
cb		13.0	213.7
+8		12.8	213.9
N.L.		12.3	214.4
T.P. 1.01	217.08	10.60	216.07
2+00			
N.L.		5.2	211.9
+4		5.7	211.4
+9		5.9	211.2
cb		6.7	210.4
+2		6.7	210.4
+5		6.1	211.0
1/4		5.9	211.2
1/2		5.5	211.6
1/4		5.5	211.6
+7		5.5	211.6
+9		5.8	211.3
cb		4.7	212.4
SL		4.7	212.4

2+25	217.08		
SL		6.9	210.2
+1		7.1	210.0
cb		7.1	210.0
+1		8.0	209.1
+3		8.1	209.0
+5		7.7	209.4
1/4		7.8	209.3
1/2		8.0	209.1
1/4		8.4	208.7
+7		8.8	208.3
+8		9.1	208.0
+9		9.1	208.0
cb		8.3	208.8
+7		8.5	208.6
N.L.		6.1	209.0 (208.0)
Boundary Pt Loma Hts (Street offsets) 2+34 ² on North = 2+35 ² on South } 1.85 North			
Sec on Boundary:			
N.L. Ocean Beach		7.9	209.2
N.L. Pt Loma Hts		9.4	207.7
+9		9.2	207.9
cb		9.9	207.2
+3		9.9	207.2
+5		9.4	207.7
1/4		9.4	207.7
1/2		9.1	208.0

217.08

Sac on Board

1/4	8.8	208.3
+7	9.1	208.0
+9	9.1	208.0
cb	8.3	208.8
+6	8.3	208.8
SL + Lonia H+s.	8.0	209.1
2+50		
SL	9.4	207.7
+8	9.6	207.5
+9	10.3	206.8
cb	10.3	206.8
+3	12.0	207.1
1/4	10.2	206.9
2	10.4	206.7
1/4	10.7	206.4
+4	11.0	206.1
+5	11.3	205.8
+7	11.3	205.8
+8	10.6	206.5
cb	10.5	206.6
+7	10.9	206.2
+9	10.4	206.7
N.L.	9.2	207.9

73

2+95

217.08

N.L.	12.8	204.3
+3	13.1	204.0
cb	12.9	204.2
+1	12.8	204.3
+2	13.5	203.6
+4	13.5	203.6
+5	13.3	203.8
1/4	13.0	204.1
2	12.5	204.6
1/4	12.4	204.7
+7	12.3	204.8
+8	12.5	204.6
cb	12.4	204.7
+1	12.3	204.8
+2	11.8	205.3
SL	11.8	205.3
T.P. 0.42	204.81	12.69
204.39		
3+00		
SL	1.8	203.0
+8	1.6	203.2
+9	2.3	202.5
cb	2.3	202.5
1/4	2.2	202.6
2	2.4	202.4
1/4	2.9	201.9
+3	3.1	201.7

	204.81		
3+00			
1/4+6	3.6	201 2	
+9	3.6	201 2	
cb	2.9	201 9	
+5	2.8	202 0	
+8	2.8	202 0	
N.L.	2.0	202 8	
3+25			
N.L.	4.6	200 2	
+2	5.2	199 6	
cb	5.1	199 7	
+1	5.7	199 1	
+4	5.6	199 2	
1/4	5.0	199 8	
1/4	4.5	200 3	
1/4	4.3	200 5	
cb	4.5	200 3	
+1	3.6	201 2	
S.L.	3.9	200 9	
3+50			
S.L.	5.9	198 9	
+9	5.9	198 9	
cb	6.5	198 3	
1/4	6.6	198 2	
1/4	6.8	198 0	
1/4	7.3	197 5	
+4	7.8	197 0	

	204.81		
3+50			
+9	7.7	197.1	
cb	7.2	197.6	
+7	7.4	197.4	
N.L.	6.8	198.0	
3+75			
N.L.	9.0	195.8	
+1	9.3	195.5	
+9	9.5	195.3	
cb	9.7	195.1	
+7	9.8	195.0	
+8	9.5	195.3	
1/4	9.4	195.4	
1/4	8.9	195.9	
1/4	8.8	196.0	
+9	8.9	195.9	
cb	8.7	196.1	
+1	8.3	196.5	
S.L.	8.6	196.2	
H+00			
S.L.	10.7	194.1	
+9	10.7	194.1	
cb	11.0	193.8	
1/4	11.0	193.8	
1/4	11.2	193.6	
1/4	11.6	193.2	
+3	11.9	193.0	

4+00

204.81

cb	11.8	193 0
+1	11.8	193 0
+8	11.5	193 3
N.L.	10.8	194 0
4+25		
N.L.	13.5	191.3
cb	13.8	191.2
+8	13.7	191 1
1/4	13.5	191 3
1/4	13.0	191.8
1/4	12.9	191 9
cb	13.0	191.8
+4	12.6	192 2
S.L.	12.5	192.3
T.P. 1042	191.93	13.00
		191.81
4+50		
S.L.	1.2	190.7
+9	1.3	190 6
cb	1.8	190.1
1/4	1.9	190 0
1/4	1.8	190.1
1/4	2.4	189 5
+6	2.7	189 2
cb	2.7	189.2
+1	2.4	189 5

4+50

191.93

N.L.	2.3	189.6
4+75		
N.L.	3.8	188.1
+9	3.7	188.2
cb	4.3	187.6
+7	4.4	187.5
1/4	4.0	187.9
1/4	3.4	188.5
+2	3.2	188.7
1/4	3.2	188.7
+8	3.5	188.4
cb	3.2	188.7
+1	2.7	189.2
S.L.	2.5	189.4
5+00		
S.L.	4.1	187.8
+1	3.8	188.1
+9	4.3	187.6
cb	4.7	187.2
+3	4.9	187.0
1/4	4.6	187.3
1/4	4.6	187.3
1/4	5.4	186.5
+4	5.6	186.3
+5	5.9	186.0
cb	5.7	186.0

75

5+00

191.93

Ncb+1	5.4	1865
N.L.	5.2	1867
5+25		
N.L.	6.6	1853
+9	6.6	1853
cb	7.3	1846
+4	7.4	1845
1/4	6.6	1853
¢	6.0	1859
1/4	6.0	1859
cb	6.1	1858
+1	5.5	1864
+9	5.6	1863
S.L.	6.0	1859
5+50		
S.L.	6.3	1856
cb	6.9	1850
+1	7.5	1844
1/4	7.4	1845
¢	7.5	1844
1/4	8.1	1838
+7	8.9	1830
+9	8.9	1830
cb	8.0	1839
N.L.	8.3	1836

5+75

191.93

76

N.L.	10.1	181.8
+2	9.6	182.3
+7	9.5	182.4
cb	9.7	182.2
+1	10.3	181.6
+2	10.4	181.5
+3	10.0	181.9
1/4	9.4	182.5
¢	8.9	183.0
1/4	8.8	183.1
+9	8.7	183.2
cb	8.3	183.6
S.L.	7.7	184.0
5+78		
S.L.	7.8	184.1
+1	8.2	183.7
cb	8.2	183.5
+1	8.9	183.0
1/4	8.9	183.0
¢	9.0	182.9
1/4	9.5	182.4
+8	10.2	181.7
+9	10.7	181.2
cb	10.7	181.2
+2	10.4	181.5

5+78	191.93	
+4	11.6	180.3
N.L.	12.9	179.0
5+80		
N.L.	10.0	181.9
cb	9.8	182.1
+1	10.2	181.7
1/4	9.7	182.2
£	9.2	182.7
1/4	9.0	182.9
+9	9.1	182.8
cb	8.6	183.3
+9	8.4	183.5
S.L.	7.9	184.1
6+00 = E.L. F. Coude.		
S.L.	9.5	182.4
+9	9.7	182.2
cb	10.0	181.9
+2	10.2	181.7
+5	9.9	182.0
1/4	9.8	182.1
£	10.0	181.9
1/4	10.7	181.2
+5	10.9	181.0
cb	11.0	180.9
+4	10.7	181.2

6+00	191.93	
N.L.	10.9	181.0
6+10		
N.L.	11.4	180.5
cb	11.3	180.6
1/4	10.9	181.0
£	10.4	181.5
1/4	10.2	181.7
cb	10.3	181.6
+5	10.6	181.3
+8	10.0	181.9
S.L.	10.0	181.9
6+30		
S.L.	10.4	181.5
cb	10.6	181.3
1/4	10.4	181.5
£	10.6	181.3
1/4	11.1	180.8
cb	11.6	180.3
+5	11.4	180.5
N.L.	11.4	180.5

>

6+30		191.93	
N.L.	11.7	1802	
+5	11.7	1802	
+6	12.3	1796 [✓]	
+7	11.8	1801	
cb	11.7	1802	
1/4	11.4	1805	
1/4	11.0	1809	
1/4	10.7	1812	
+8	11.1	1808	
cb	11.0	1809	
S.L.	10.4	181.5	
6+34			
S.L.	10.5	181.4	
cb	11.0	1809	
+2	11.2	1807	
1/4	10.8	1811	
1/4	11.1	1808	
1/4	11.5	1804	
cb	12.0	1799 [✓]	
+5	11.9	1800	
+7	12.8	1791 [✓]	
N.L.	11.9	1800 [→]	

6+37		191.93	
N.L.	13.4	178.5	
+4	12.1	179.8	
cb	12.1	179.8	
1/4	11.7	180.2	
1/4	11.2	180.7	
1/4	10.9	181.0	
+8	11.3	180.6	
cb	11.1	180.8	
S.L.	10.7	181.2	
6+40			
S.L.	10.8	181.1	
cb	11.2	180.7	
+3	11.4	180.5	
+9	10.9	181.0	
1/4	11.0	180.9	
1/4	11.3	180.6	
1/4	11.7	180.2	
+9	12.3	179.6	
cb	12.2	179.7	
N.L.	12.0	179.9	

19193

6+50 = m cb line Froud G.

N.L	12.3	179.6
+5	12.4	179.5
+8	12.8	179.1
cb	12.7	179.2
+1	13.0	178.9
+2	12.7	179.2
1/4	12.1	179.8
E	11.6	180.3
1/4	11.3	180.6
+1	11.2	180.7
+7	11.7	180.2
cb	11.5	180.4
+5	11.6	180.3
+9	10.7	181.2
S.L.	10.7	181.2

0+00 = Next seg. Cont in Book 1279

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ENGINEERING DEPARTMENT
CITY OF SAN DIEGO, CALIFORNIA

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 1/2 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance

**IMPROVED TABLES
AND
INFORMATION**

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given I may be found by dividing tangent (or external), opposite I by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

4.90
22-30

ENGINEERING DEPARTMENT
CITY OF CALIFORNIA
SAN DIEGO
189

23.25
22.0
77.27
5780.61
79.96
65

7.18
4.70
2.48
4.29
1.81

1997.65
17471.43
226.22

268.62
2.30
270.92
4.72
266.19
6.42
272.61
4.57
268.04