

1264

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*This index is for 1964*

MICROFILMED  
DEC 22 1964

*See printed 1964*

Handwritten notes and calculations on the left page, including:  
-  $71.00$   
-  $447$   
-  $1341$   
-  $1788$   
-  $447$   
-  $639.21$  (68)  
-  $558$   
-  $812$   
-  $744$   
-  $680$   
-  $360-10$   
-  $90-04-45$   
-  $93$   
-  $234$   
-  $120$   
-  $359.54$   
-  $87-58-30$   
-  $21.60$   
-  $21.15$   
-  $118$   
-  $179-58-30$   
-  $89-59$   
-  $381.60$   
-  $4577$   
-  $275.33$   
-  $2267.87$   
-  $12273.30$

This index is by page

7/20/44

MICROFILMED

101

X. Sec. Wabaska	Centralonia to Chatsworth	34
" " "	" " Tennyson	35
" " "	Voltaire " "	56
" " Bernice Dr.	Wabaska " La Cresta	41-67-74
" " Atascadero	Tennyson " Wells	44
" " Wawona	Chatsworth " La Cresta	65



BOYD ST.



4

20'40"

302.81'

1'50"

525.00'

JOHNSON

3

200

8

1

South to Line Redwood  
66,330'

4

LINCOLN

3

100'

50'

702  
6222  
87'48" S.P.  
Proposed Sewer

14606  
Hub set

345,270  
96,500  
549.1  
442,224  
89,939  
HAYES AVE  
Cen. Man. Found  
A.V.D.

54404

90255.24  
180'

138.97'

1022.25  
25'30"

23°  
355'  
141.12  
141.12  
1092.5  
938.6  
1092.5  
VERMONT  
LINCOLN AVE  
89,954'

West on South Line of Washington St.

- 0+00 = Int. S.L. Washington St. & E.L. 10<sup>th</sup> St.  
 3+55.28 fd. 3' tie on w 7' Line 9<sup>th</sup>  $\Delta^?$   
 6+57.06 = E of 9<sup>th</sup> St. (from cbs)  
 8+02.06 =  $\Delta$   
 11+15.25 =  $\Delta$   
 12+10.11 =  $\Delta$   
 12+85.02 = Int with E.L. of 6<sup>th</sup> St.

North on East Line of 6<sup>th</sup> St.  
 0+00 = S.E. Cor. 6<sup>th</sup> & Washington.

Sta                      slope    Vert L    Hor. Dist

- 0+00 = S.E. Cor. Washington & 6<sup>th</sup> St.  
 1+05.00 =  $\Delta$  offset 2A' West  
 2+43.32 =  $\Delta$   
 4+32.31 =  $\Delta$  offset back on line.  
 7+56.31 =  $\Delta$   
 8+14.10 =  $\Delta$                       232.00    8°31'    230.43 ✓  
 10+44.53                      138.00    24°20'    121.12 ✓  
 11+65.65 =  $\Delta$   
 14+67.65 =  $\Delta$   
 15+27.65 =  $\Delta$                       245.00    3°28'    244.45    **244.55**  
 17+72.10 =  $\Delta$   
 18+57.10                      56.00    12°44'    54.62 ✓  
 19+11.72                      70.00    29°42'    64.10 ✓  
 19+75.82 =  $\Delta$   
 19+97.56 =  $\Delta$  = Int. with North Line.

402.06

133.06

669.00

4

Falls 1.43' N of S.B. Cor. Wash. & 6<sup>th</sup>

355.24  
 354.85  
 668.57  
 313.72

17+72.20

18+57.20

19+11.82

19+75.92

20+07.56 - 1997.33 on sketch

See Page 7

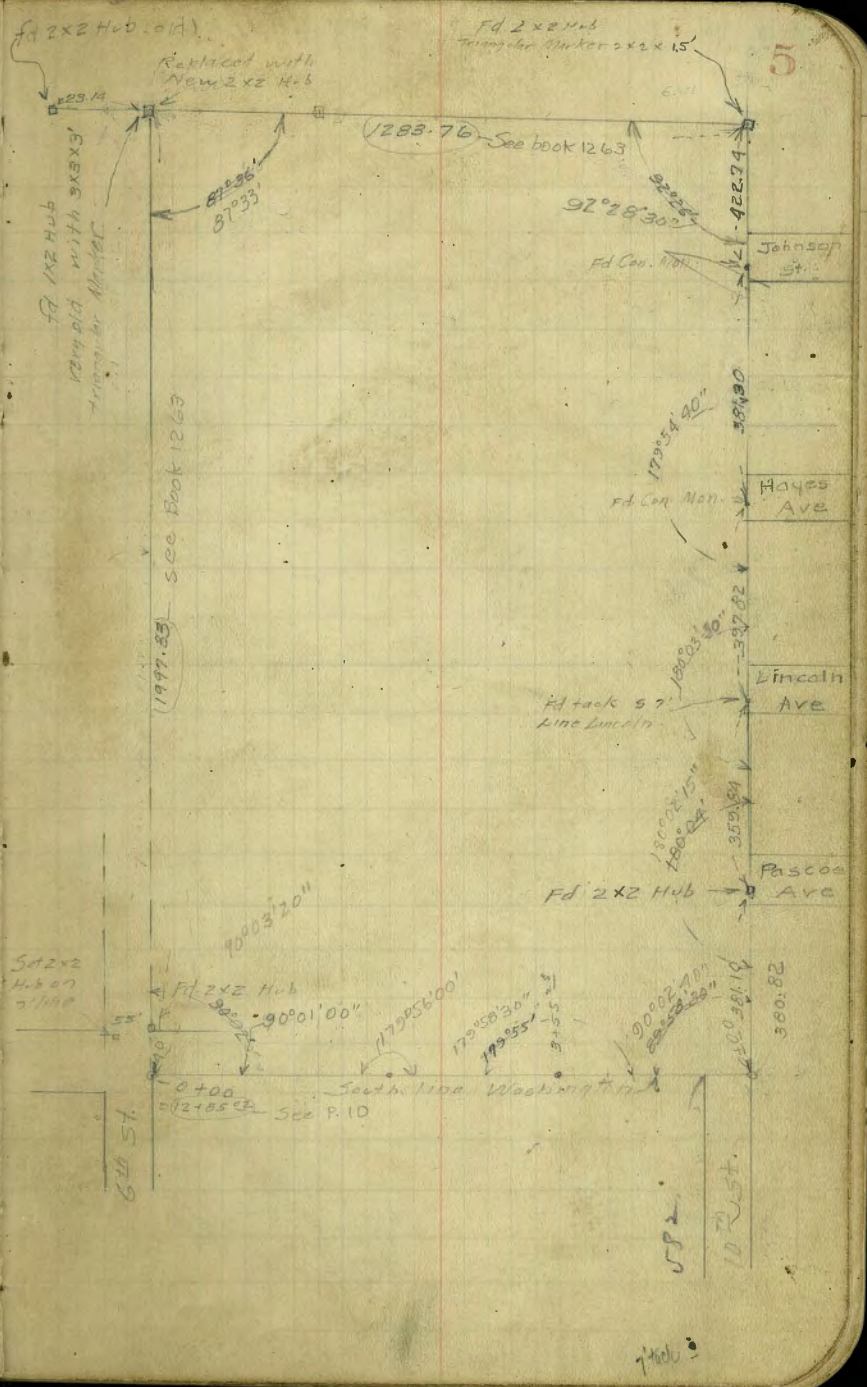
East on Random Map

Sta	slope dist	Vert L	Hor dist	
0+00	Int. BL	6 <sup>M</sup> & N.L.	= a	
0+58 <sup>92</sup>	63.62	22°02'	58.97 ✓	= a
2+56 <sup>12</sup>	227.00	29°43'	197.15 ✓	= a
2+64 <sup>52</sup>	found Hub	Marked V.L.	774	1.6' North.
4+93 <sup>26</sup>	245.00	18°53'	237.84 ✓	= a
5+47 <sup>52</sup>	63.00	31°46'	53.56 ✓	= a
5+88 <sup>56</sup>	450.00	2°21'	445.23 ✓	= a
10+33 <sup>79</sup>			29.00	= a
11+21 <sup>79</sup>	83.00	19°23'	78.27 ✓	= a
12+00 <sup>08</sup>	77.00	34°03'	66.65 ✓	= a
12+66 <sup>73</sup>			9.58	= a
12+76.31				= Int.

381.10  
295.00  
381.10  
86.10

73  
22  
100

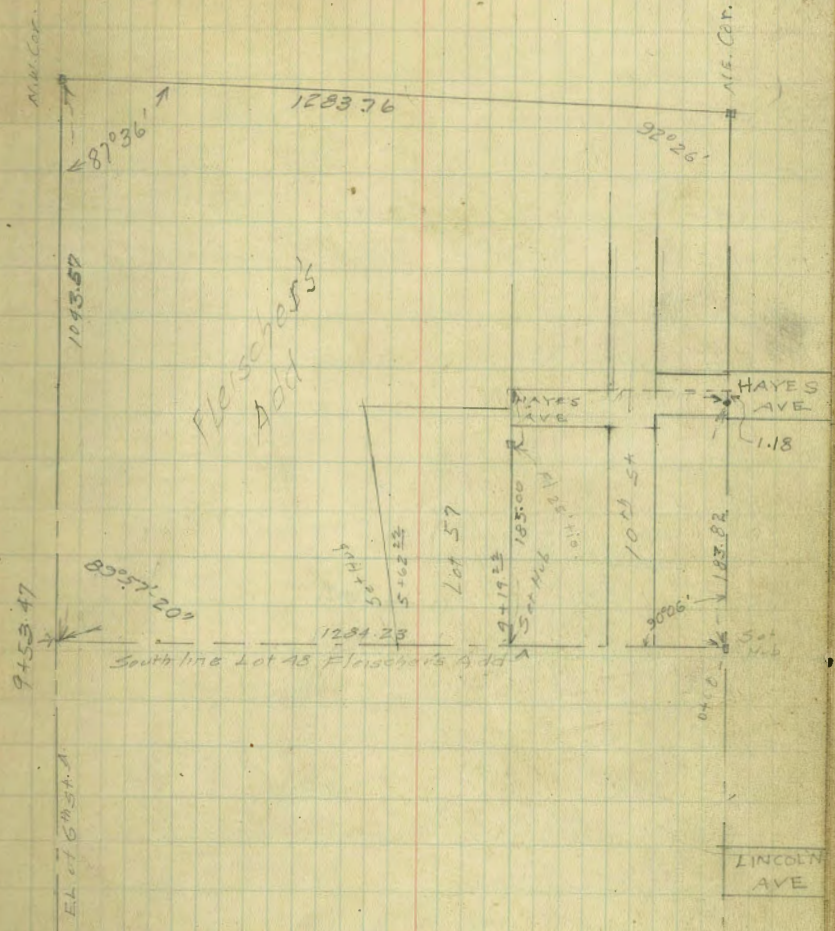
1397.82  
148.91





July 12-28  
 Loudon, Morgan Isbell

1+99 <sup>21</sup>	202.00	15°04'	195.06 ✓	=0	
3+89 <sup>27</sup>	92.00	19°28'	86.54	=0	86.74
4+16 <sup>18</sup>	31.00	30°07'	26.81 ✓		4+76.11
4+16 <sup>23</sup>			6.41	=Int.	5+02.92



North on East line 6th

4+32 <sup>00</sup>				Set 2x2 Hub
7+51 <sup>00</sup>				Set 2x2 Hub
12+14 <sup>00</sup>				Set 2x2 Hub
15+23 <sup>85</sup>	247.80	2°10'	247.42 ✓	Set 2x2 Hub
17+71 <sup>22</sup>				Set 2x2 Hub
19+75 <sup>07</sup>				Set 2x2 Hub
19+10 <sup>22</sup>	71.00	24°22'	64.67 ✓	
19+75 <sup>89</sup>	27.00	31°52'	21.84	22.68
19+97 <sup>23</sup>				
19+97 <sup>33</sup>				
West on North line of Fleischer's Add.				
0+00 = NE Corner				
0+00	81.00	29°46'	70.31 ✓	
0+70 <sup>82</sup>	101.00	20°33'	94.57 ✓	
1+64 <sup>58</sup>			115.00	
2+79 <sup>88</sup>	454.00	8°28'	449.05 ✓	
7+28 <sup>93</sup>	299.00	19°35'	281.70 ✓	
10+10 <sup>63</sup>	fd. Hub on EL Mission Drive vL.364			
	1192.00	2°21'	491.59 ✓	
12+20 <sup>52</sup>	70.00	25°23'	63.24 ✓	
12+83 <sup>76</sup>	= Hub on NW Corner.			

replaced with  
2x2  
fd. 1x2 Hub

319  
432  
751  
463  
1214

24  
13.65  
35.65  
1875.07  
1910.72

500  
33  
463

323  
3  
310  
103.80  
1771.27  
1875.07

8  
5.81  
2.19  
=

91092  
71  
91021  
637644  
6467532  
1910.72  
1975.39

86805  
81  
86805  
694440  
7031205

93637  
93637  
9457237  
7031  
16488  
175  
279.58

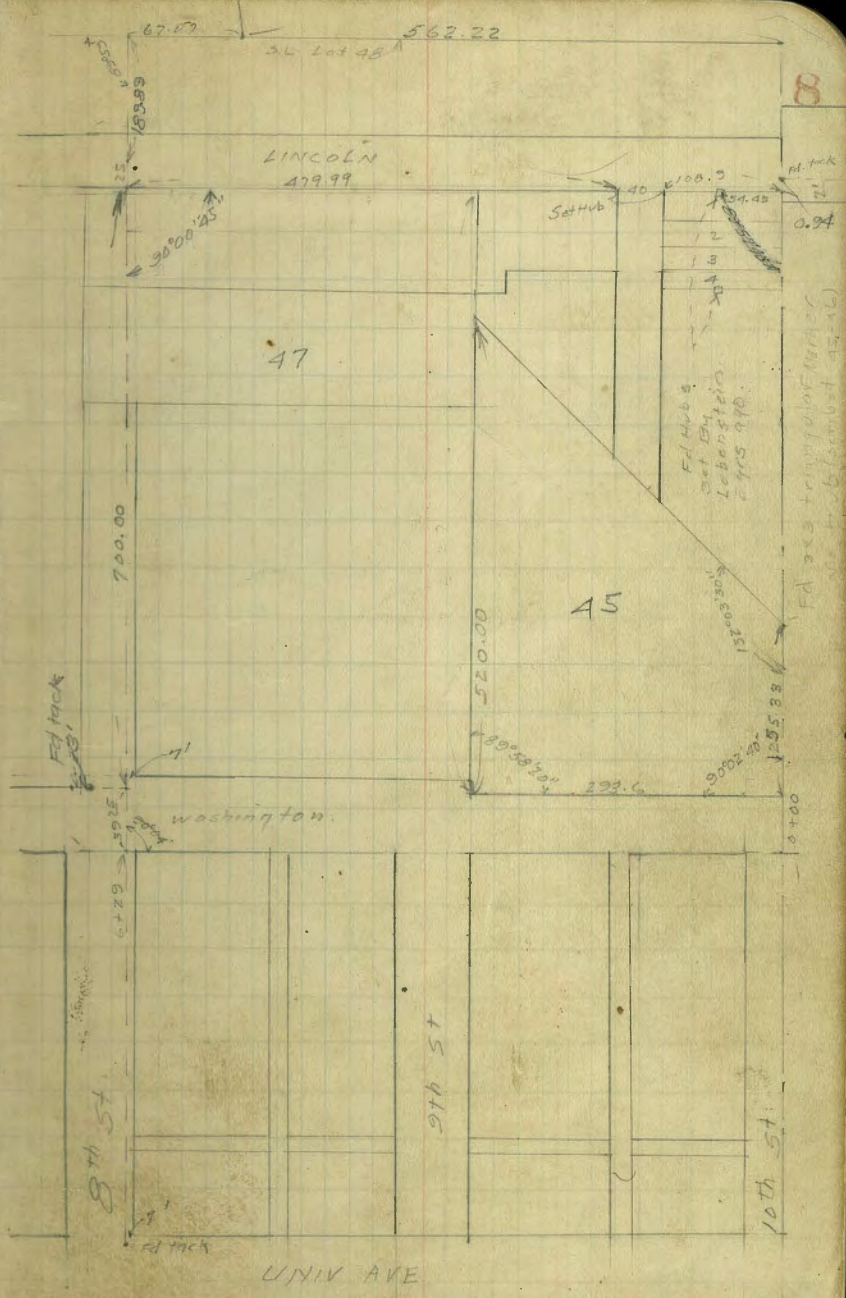
37.05  
432  
509.05

98910  
454  
395640  
494550  
395640  
449.0514  
279.88  
728.93

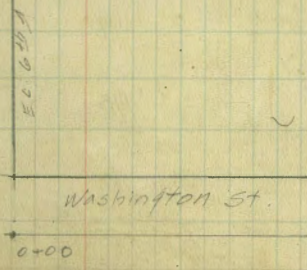
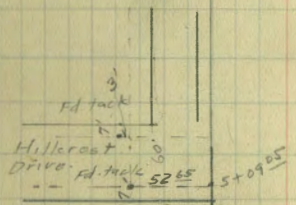
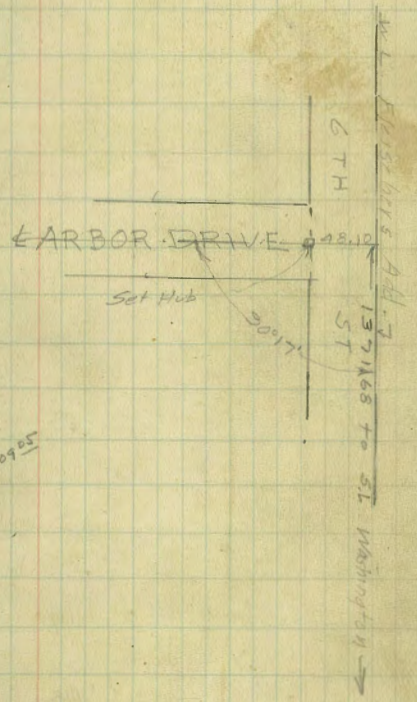
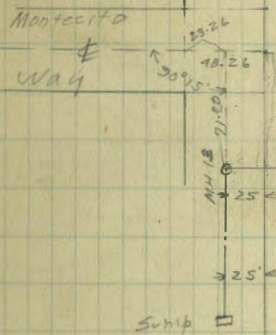
West on South line Lot 48

0+00 = East Line Pflaeschers A.L.

0+02	198	11°50'	193.77	
1+95 <sup>22</sup>	215.00	2°30'	214.79	= 0
4+10 <sup>58</sup>			8.64	= 0
9+19 <sup>22</sup>	131.00	76°0'	128.81	= 0 = SE. Cor Lot 57
5+48 <sup>03</sup>				= 0
5+62 <sup>22</sup>			29.19	= S.W. Cor Lot 57
9+87 <sup>33</sup>	440.00	3°15'	439.30	= 0
10+93 <sup>33</sup>			126.00	= 0
12+78 <sup>33</sup>			185.00	= 0
12+84 <sup>23</sup>			590	= E.L. 6th



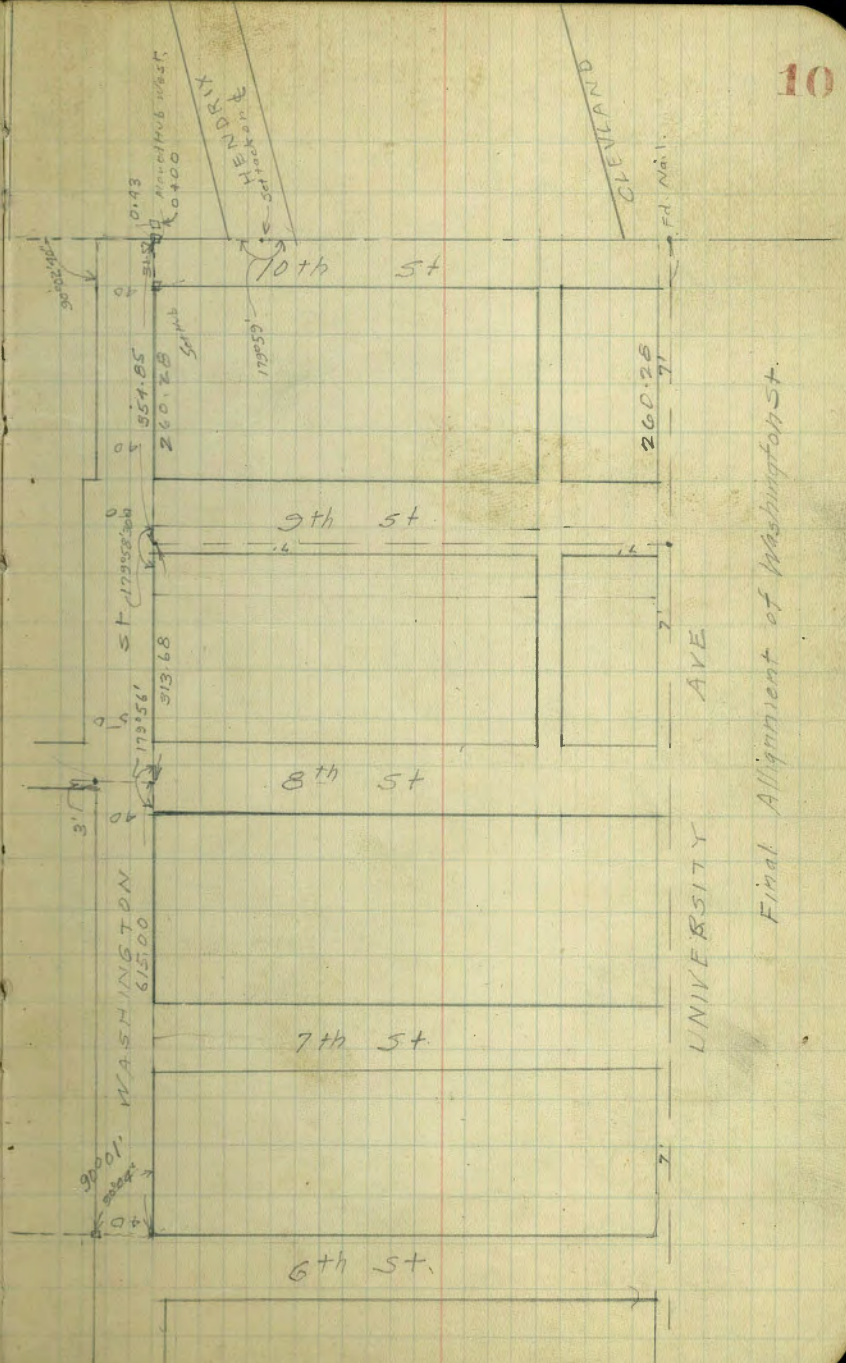
Ties to utility  
Fleischers Add. of  
Montecito Way, Arbor Drive  
and Hillcrest Drive.



27  
 106  
 133  
 482  
 615  
 313 68  
 354 85  
 1283 .53

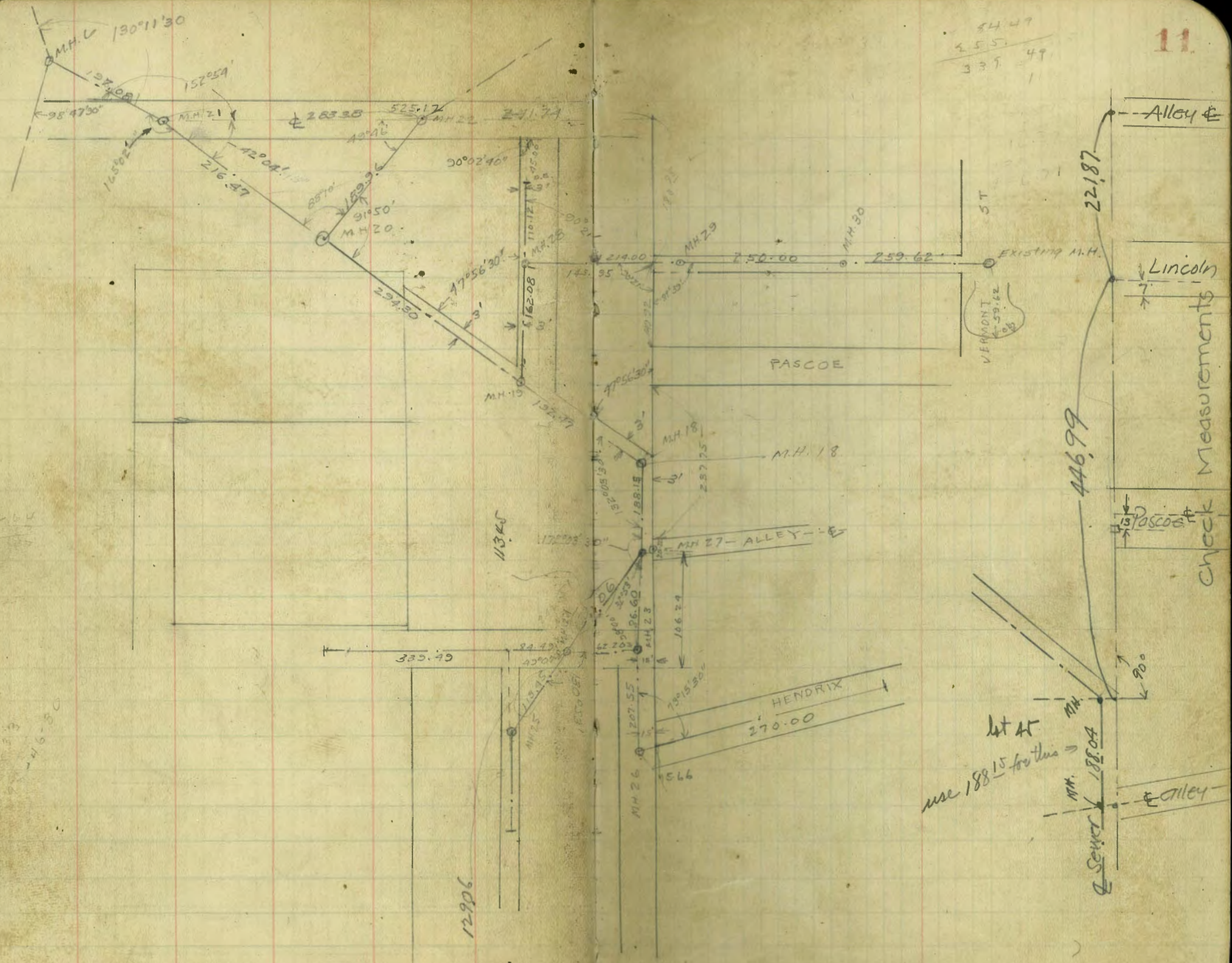
12 85 82  
 93  
 1284 .59

PASCOE ST.



Final Alignment of Washington St.

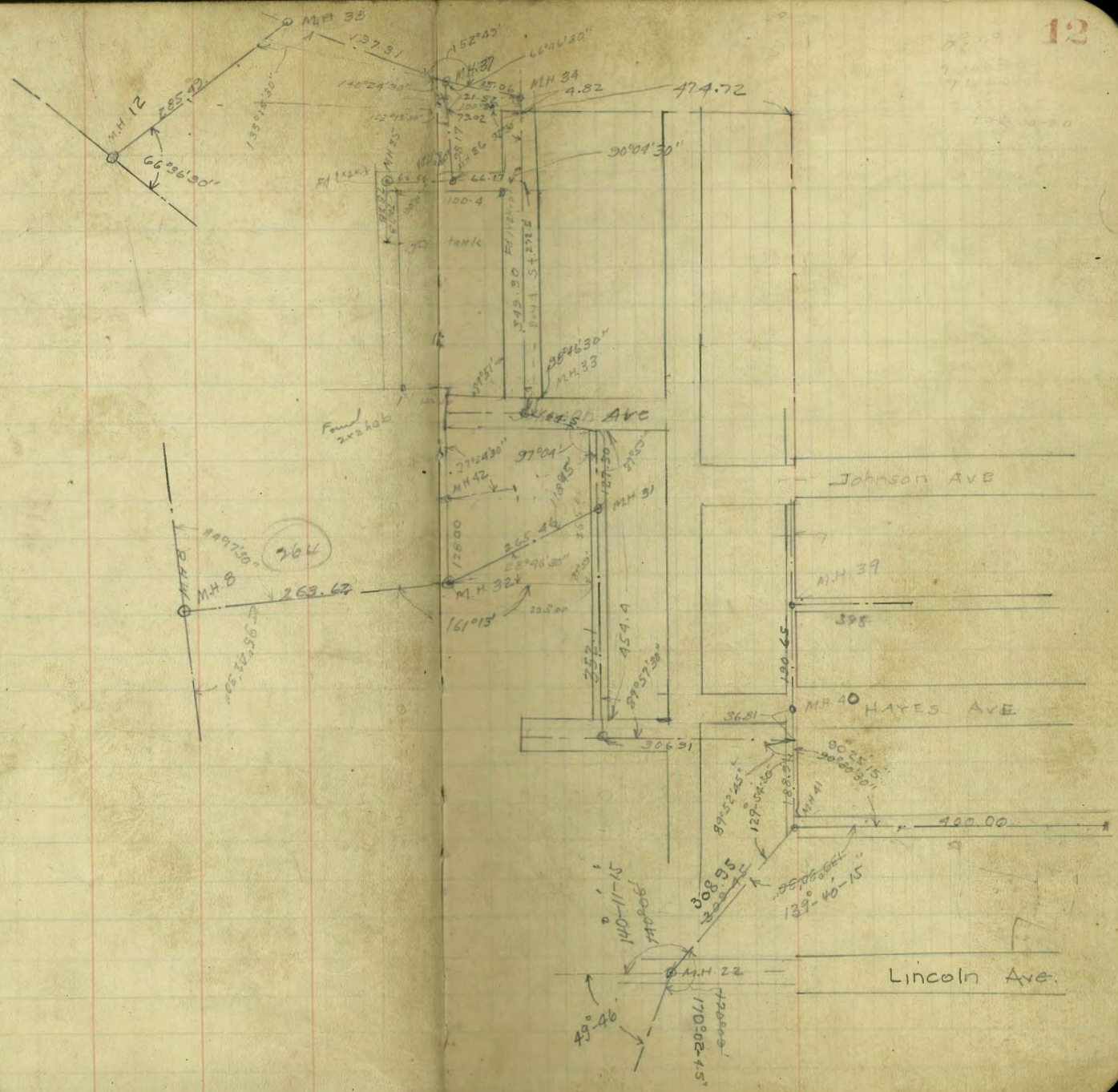
54.47  
5.55  
337.47



Lincoln  
Measurements  
check

12906  
11345  
335.49  
24.49  
119.15  
116.50

lot 45  
use 188.15 for this →  
MH 27  
MH 28  
Alley



272  
272  
100-4  
300-4

Profile 6<sup>th</sup> at Sewers  
(See P. 2) 0+00 = M.H. 1.

3

BM	5.87	289.89	284.02
T.P.	4.49	290.10	4.28 = 285.61
E.L. M.H. 20 <sup>29</sup>	w. of M.H. 1	10.21	279.89
+00 M.H.		6.14	283.96
0+00 = M.H. 1		5.3	284.8
0+24 <sup>1</sup>	= N side drive	5.1	285.0
0+24 <sup>4</sup>	top of	4.91	285.19
0+24 <sup>2</sup>	bar. Drive	5.41	284.69
0+37 <sup>2</sup>	= S side drive	5.57	284.53
0+50		5.1	285.0
0+94		5.3	284.8
1+09		5.0	285.1
1+19		6.2	283.9
1+23		9.5	280.6
1+25		11.0	279.10
1+31		14.5	275.6
T.P.	0.15	277.31	12.94 = 277.16
1+39		6.5	270.81
1+44		10.3	267.0
1+48		12.9	264.4
T.P.	0.47	265.34	12.44 = 264.87
1+55		5.3	260.0
1+58		7.2	258.1
1+62		10.3	255.0
1+70		11.5	253.8
1+76		12.4	252.9
1+77		14.2	251.1

Note:  
Raining was  
1.5' E of line.  
Feetings not more  
than 5' below ground.

Plotted.

July 17-28  
London  
Zebell  
Morgan

13

	265.34	
T.P. 0.43	253.38	12.45 = 252.89
1+82		3.4 = 249.9
1+87		6.3 = 247.0
1+91		7.1 = 246.2
T.P. 0.06	240.43	12.95 = 240.38
1+95		6.9 = 233.5
2+00 = M.H. 1 <sup>2</sup>		9.7 = 230.7
2+02		10.8 = 229.6
2+07		11.7 = 228.7
2+31		11.5 = 228.9
2+60		11.4 = 229.0
2+81 <sup>63</sup>	= M.H. (2) 3	11.34 = 229.09
T.P.		
M.H. (2) <sup>3</sup> to M.H. (3) <sup>5</sup>		(See P. 2)
0+00 = M.H. 2	231.85	229.10
T.P. 276		
0+36		4.0 = 227.8
0+52		3.4 = 228.4
0+76		4.3 = 227.6
0+85		7.1 = 224.8
1+00		8.6 = 223.2
T.P. 0.16	219.40	12.61 = 219.24
1+31 <sup>38</sup>	M.H. 1 <sup>2</sup> H	11.8 = 207.6
1+37		13.2 = 206.2
1+61		14.6 = 204.8
T.P. 0.16	206.95	12.61 = 206.79

Plotted



206.95

1+97		1.3	205.6	
2+ <sup>06</sup> 76		6.0	201.0	
2+ <sup>31</sup> 41		8.3	198.6	
2+ <sup>38</sup> 44		9.5	197.4	
2+ <sup>68</sup> 72		11.6	195.4	
2+ <sup>69</sup> 77		10.7	196.2	
2+ <sup>88</sup> 78		11.8	195.2	
2+95		13.3	193.8	
3+05				
T.P.	2.04	196.48	12.52	194.43
3+14 <sup>50</sup>	= M.H. (3) 5	6.61	189.86	
	M.H. (3) to M.H. (4) 6	0+00 = M.H. (3) 5		
0+17		5.0	191.5	
0+25		4.8	191.7	
0+45		6.0	190.5	
0+55		7.4	189.1	
0+65		8.7	187.8	
0+80		10.6	185.9	
0+95		13.5	183.0	
1+06		13.8	182.7	
1+09		10.9	185.6	
1+21 <sup>25</sup>	= M.H. (4) 6	186.67	9.88	186.58

plotted.

6 7  
M.H. (4) to M.H. (5)  
0+00 = M.H. 4

186.67

0+10		1.8	184.9	
0+17		3.6	183.1	
0+20		5.8	180.9	
0+23		6.2	180.5	
0+48		7.3	179.4	
0+61		5.8	180.9	
0+70		5.5	181.2	
0+91		6.2	180.5	
0+95		6.8	179.9	
1+00		6.9	179.8	
1+10		8.6	178.1	
1+25		9.9	176.8	
1+50		12.5	174.2	
T.P.	0.93	175.74	11.86	174.81
1+77		3.2	172.5	
1+95		5.5	170.2	
2+25		6.5	169.2	
2+60		9.2	167.5	
2+87		9.7	166.0	
3+06		9.9	165.8	
3+15		10.7	165.0	
3+20		10.4	165.3	
3+35		11.3	164.4	
3+38		12.4	163.3	

plotted.

6  
M.H. (4) to M.H. (5)  
175.74

3+47		14.0	161.7
T.P. 8.74	172.63	11.85	163.89
3+54 <sup>40</sup>	= M.H. (5) 7	12.05	160.58
T.P. 12.16	184.33	0.46	172.17
T.P. 11.49	195.29	0.53	183.80
T.P. 13.02	207.79	0.52	194.77
T.P. 12.49	220.11	0.17	207.62
T.P. 12.27	232.55	0.45	219.66
T.P. 12.79	244.80	0.54	232.01
T.P. 12.23	256.93	0.10	244.70
T.P. 12.69	268.68	0.94	255.99
T.P. 12.94	281.51	0.11	268.57
T.P. 10.30	290.21	1.60	279.91
B.M. Beginning	6.21	284.00	

Plotted

~~17.11~~

July 23-28

Landon  
Esbell  
Morgan

Profile 6254 Senors  
M.H. (7) to M.H. (6) (500 P2)  
19 17

15

B.M. 2.63 486.65

sw 542  
Washington  
284.02

T.P. 0.74	285.08	2.31	284.34
0+00 = M.H. (7) 19		3.2	281.9
0+272		3.1	282.0
0+59		2.8	282.3
1+00		2.8	282.3
1+11		3.5	281.6
1+16		4.4	280.7
1+20		5.3	279.8
1+23		7.6	277.5
1+26		8.8	276.3
1+31		11.3	273.8
1+32.5 = M.H. #18		13.5	271.6
1+41		18.9	266.2
1+52		13.05	272.03
T.P. 0.55	272.58	12.49	260.09
T.P. 0.50	260.57	12.40	248.19
T.P. 0.54	248.73	1.2	247.5
1+54		2.0	246.7
1+57		2.4	246.3
1+78		2.8	245.9
2+03		1.0	247.7
2+10 <sup>2</sup>		2.8	245.9
2+18		12.75	235.98
T.P. 2.47	238.45	12.27	226.18
T.P. 0.87	227.05		

Plotted

19  
M.H.(7) to M.H.(6) 17

227.05

2+45 2.0 225.0  
2+47 4.7 222.3  
2+52 6.7 220.3  
2+57 9.2 217.8  
2+62 9.7 217.3  
2+85 13.0 214.0  
T.P. 1.80 216.11 12.74 214.31

plotted

2+94 2.6 213.4  
2+99 = M.H.(4) 17 3.65 212.46

M.H.(4) to M.H.(3) 0+00 = M.H.(6) 17

0+48 6.7 209.4  
0+74 9.5 206.6  
T.P. 1.21 207.33 9.59 206.52

0+84 2.8 204.9  
1+05 4.2 203.5

1+21 5.4 202.3  
1+36 6.6 201.1

1+51 7.4 200.3  
1+60 6.4 201.2

1+68 7.2 200.5  
1+85 9.2 198.5

1+87 10.5 197.2  
2+00 11.7 196.0

2+08 12.5 195.2  
2+18 12.9 194.8

plotted

17 5  
M.H.(4) to M.H.(3)

207.73

T.P. 2.65 198.05 12.33 195.40

2+22 2.5 195.5

2+26 0.6 197.4

2+31 1.1 196.9

2+40 2.4 195.6

2+50 4.3 193.7

2+61 8.2 189.8

2+66 8.9 189.1

2+70 8.2 189.8

2+74# = M.H.(3) 5 9.20 189.85

M.H.(4) to M.H.(5)

0+59 17 16 225.19 212.46

M.H. 16 12.73 12.8 212.4

0+57 8.6 216.6

0+50 6.5 218.7

0+42 4.0 221.2

0+37 4.1 221.1

0+33 T.P. 12.05 236.91 0.33 224.86

0+23 9.2 227.7

0+11 7.9 229.0

0+06 3.2 233.7

0+02 2.0 234.7

0+00 = M.H.(5) 16 3.20 233.71

plotted

16

July 3-28  
London  
Moran  
Isbell.

16  
MH(15) to DE North on 7th St.  
0+00 = MH(15) 16

MH(15) 16	12.77	246.50		233.71
0+08			7.4	239.1
0+13			6.2	240.3
+20 = S Line Washington				
0+23			4.2	242.3
0+24			5.7	240.8
0+27			8.2	238.3
8' w of 0+27 bet of banks			13.4	233.1
0+32			4.7	241.8
0+42			2.0	244.5
0+46			2.4	244.1
0+62			1.8	244.7
12' w of 0+62 bet of bank			13.5	233.0
0+76			1.9	244.6
0+86			2.0	244.5
T.P. 10.51	255.68		1.33	245.17
1+00			11.9	243.8
15' w of 1+00 bet. of banks			21.7	234.00
1+32 (bank was out)			15.4	240.3
1+42			14.8	240.9
1+52			11.5	244.2
1+62	1461 = MH #15		6.9	248.8
1+72			2.4	253.3
T.P. 11.72	267.25		0.15	255.53
1+76			10.0	257.3
1+81			8.5	258.7

plotted

16  
MH(15) to DE North.

17

				267.25
1+88			4.4	262.8
T.P. 11.46	276.55		2.16	265.09
1+96			5.4	271.1
2+03			4.5	272.0
2+55 = DE			0.7	275.8
T.P. 11.93	287.75		0.73	275.82
T.P. 3.95	288.49		3.21	284.54
T.P. 4.64	287.55		5.58	282.91
B.M. on Hendrix 10th			4.40	283.15
MH(26) to DE East on Hendrix				
22				
0+00 = MH(26) 22				
B.M. 4.89	288.04			283.15
0+00 (on Pav)			5.33	282.81
0+16 Edg pav.			4.98	283.06
0+30			5.5	282.5
0+50			5.5	282.5
1+00			5.7	282.3
1+50			5.9	282.1
2+00			6.3	281.8
2+50			6.5	281.5
2+70 = DE			6.4	281.6

plotted

PLOTTED

Hendricks line

22  
MH(26) to MH 23 ✓

288.04

0+00 = MH(26) 22

0+36 = End Pav	5.71	282.33
0+70	10.2	277.8
0+80	11.0	277.0
0+86	12.8	275.2
T.P. 0.09	275.14	12.99 275.05
1+02	2.4	272.8
1+14	3.4	271.8
1+29	13.3	261.8
T.P. 0.04	262.65	12.53 262.81
1+34	4.1	258.5
1+44	8.1	254.5
1+49	8.6	254.0
1+50	10.2	252.4
1+59	13.5	249.1
T.P. 0.15	250.83	11.97 250.68
1+73	7.1	243.7
1+79	9.6	241.2
1+87 <sup>5</sup>	13.9	236.9
T.P. 0.07	238.17	12.73 238.10
1+97 <sup>5</sup>	6.7	231.5
2+07 <sup>55</sup> = MH 23 ✓	11.53	226.62

PLOTTED

10<sup>th</sup> St.

MH 23 to MH 27 ✓

0+00 = MH 23

MH 23 0.29	227.41	226.62
0+12	5.7	221.7
0+14	9.5	217.9
0+22	10.4	217.0
0+35	11.1	216.3
0+46	13.2	214.2
0+49	14.6	212.8
0+63	15.1	212.3
T.P. 0.37	215.56	12.22 215.19
0+76	4.4	211.2
0+86 <sup>60</sup> = MH 27 ✓	4.50	211.06
MH 27 to MH (18) 0+00 = MH 27 ✓	28	
0+25	7.3	208.3
0+50	10.9	204.7
0+65	12.5	203.1
0+75	11.7	203.9
0+85	14.6	201.0
1+00	16.0	199.6
T.P. 0.36	202.95	12.97 202.59
1+25	5.7	197.2
1+55	7.5	195.4
1+75	8.7	194.2
1+86	10.6	192.3
1+88 <sup>15</sup> = MH (18) 28	12.47	190.48

PLOTTED

18.

This line not used.

MH(18) + 0 MH(19) 0+00 = MH(8) 28

MH(18)	0.08	190.56	190.48
0+24		1.6	189.0
0+50		2.8	187.8
0+80 (pipe 4.6' South)		4.7	185.9
1+00 (pipe 4.0' South)		6.2	184.4
1+13		6.5	184.1
+05 pipe 3.9' S of 1+13		7.3	183.3
1+20		6.8	183.8
1+50 (pipe 2.8' South)		7.7	182.9
1+62		8.8	181.8
1+70		10.9	179.7
T.P. (top pipe 1.6' S of M.H. 19)		11.55	178.81

PLOTTED

1+94<sup>2</sup> = MH(19) 33 1.07 177.92

M.H.(19) + 0 MH(20) 0+00 = MH(19) 33 X

0+23		1.5	177.5
0+36		0.4	178.6
0+68		3.7	175.3
0+72		5.2	173.8
0+75		6.9	172.1
0+76		8.5	170.5
0+79		8.3	170.7
0+80		6.5	172.5
0+83 crosses pipe (top pipe)		6.21	172.78
1+08		6.9	172.1
1+20		7.8	171.2
1+40		10.4	168.6

PLOTTED

178.99

1+48 (pipe 1.8 North)	9.9	169.1
top pipe 1+48	9.81	169.18
1+68	7.9	171.2
1+83	8.6	170.4
2+01 (pipe 3' North)	9.5	169.5
2+36	10.1	168.9
2+45	11.0	168.0
2+57	10.9	168.1
2+65	9.9	169.1
2+73	10.8	168.2
2+81	12.5	166.5

PLOTTED

2+94<sup>30</sup> 0.79 167.12 = MH(20) 34 12.66 166.33

M.H.(20) + 0 MH(21) 0+00 = MH(20) 34

0+12	1.9	165.2
0+21	2.7	164.4
0+28	4.1	163.0
0+38	4.8	162.3
0+42	5.2	161.9
0+72	5.9	161.2
0+75	5.9	161.2
0+76	9.3	158.8
0+83	8.1	159.0
0+87	9.1	158.0
0+89	8.7	158.4
0+93	6.7	160.4

PLOTTED

167.12

1+17	7.5	159.6
1+18	9.4	157.7
1+35	11.4	155.7
1+61	11.8	155.3
1+74	12.5	154.6
1+76	10.5	156.6
1+85	10.7	156.4
1+96	11.1	156.0
1+99	12.5	154.6
2+01	11.8	155.3
2+16 <sup>12</sup> = MH (35) <sup>0.77</sup> <sup>155.73</sup>	12.16	154.96
robbipe. pipe 11.3 Net MH 212.09	152.64	
MH (21) + 0 MH (6) 0+00 = MH (21) 35		
0+37	2.9	152.8
0+65	4.1	154.6
0+91	4.8	150.9
1+16	5.6	150.1
1+42	6.8	148.9
1+66	7.0	148.7
1+97 <sup>08</sup> = MH #8	6.95	148.78 (148.85)

PLOTTED

X

MH 27 thru MH 29 to MH 25

20

2+22 <sup>1278</sup> = MH 27	223.84	211.06
2+29	12.8	211.0
2+17	8.8	215.0
2+13	8.4	215.4
2+06	4.4	219.4
T.P. 12.74	236.38	0.20 223.64
1+90	10.9	225.5
1+75	8.3	228.1
1+45	6.3	230.1
1+29 <sup>06</sup> = MH 24	6.98	229.40
1+13	3.9	232.5
1+03	4.0	232.4
0+95	1.2	235.2
0+85	2.8	233.6
0+70	2.7	233.7
T.P. 11.77	247.95	0.20 236.18
0+40	12.4	235.5
0+25	8.0	239.9
0+15	7.2	240.7
0+12	9.8	238.1
0+00 = MH 25	7.74	240.21

PLOTTED

M.H. 25 to D.E. South.

0+00 = M.H. 25 ✓  
247.95

0+23		5.6	242.3
T.P.	7.35	255.11	0.19 247.76
0+49		9.3	245.8
0+64		6.5	248.6
0+80		3.3	251.8
0+89 <sup>29</sup> = DE		2.0	253.1

PLOTTED

alley  
Rt 16

T.P.	0.47	242.65	12.93 242.18
T.P.	0.82	230.88	12.59 230.06
M.H. 24 ✓		1.49	229.39

M.H. 24 to M.H. 23 0+00 = M.H. 24 ✓

0+39		12.3	218.6
0+52		5.9	225.0
0+56		5.5	225.4
0+57		4.0	226.9
0+61		3.6	227.3
0+62 <sup>20</sup> = M.H. 23 ✓		4.29	226.59

PLOTTED

M.H. 24 to D.E. West on Washington

21

0+00 = M.H. 24 ✓

M.H. 24	11.22	240.62		229.90
0+05		7.0		231.6
0+20		3.5		237.1
T.P.	11.82	251.90	0.54	240.08
0+40		9.2		242.7
0+47		5.9		246.0

PLOTTED

+50		5.7		246.2
+52		3.5		248.4
+55		2.0		249.9
T.P.	12.22	263.91	0.21	251.69
0+60		11.4		252.5
0+67		8.8		255.1
0+70		7.1		256.8
0+80		3.6		260.3
0+84 <sup>5</sup>		2.0		261.9

T.P.	11.52	275.25	0.18	263.73
0+96		6.5		268.7
T.P.	10.45	285.40	0.30	274.95
1+18		9.5		275.9
1+28		5.0		280.4
1+30 = M.H. # 26		3.7		281.7
1+36		3.9		281.5
1+43		3.5		281.9
1+56		3.4		282.0
1+84		3.2		282.2
+94				



M.H. 21 to D.E. West

285.40

2+20	3.2	282.2
2+50	2.6	282.8
2+75	2.2	283.2
3+00	2.5	282.9
3+39 <sup>41</sup> = D.E.	2.0	283.4
B.M. 10 <sup>th</sup> Hendrix	2.37	283.08

PLOTTED

Washington St.

1+89 <sup>34</sup> = M.H. (20)	11.40	177.73
1+84	14.5	163.2
1+67	11.7	166.0
1+55	10.8	166.9
1+30	8.3	169.4
1+18	8.1	169.6
1+06	6.6	171.1
1+00	5.8	171.9
0+88	4.4	173.3
0+86	5.7	172.0
0+75	4.5	173.2
0+70	2.1	175.6
T.P. 11.67	189.00	0.40
0+58	11.8	177.2
0+45	10.4	178.6
0+33	9.8	179.2
0+30	11.5	177.5
0+20	8.4	180.6

PLOTTED

189.00

0+02	6.9	182.1
0+00 = M.H. (22)	7.2	181.8
M.H. (22) to M.H. (41) 40		
3+08 <sup>35</sup> = M.H. (22)		181.8
2+78	6.4	182.6
2+76	5.3	183.7
2+70	4.6	184.4
2+69	2.9	186.1
2+55	0.9	188.1
T.P. 11.98	200.77	0.01
2+47	11.9	188.9
2+44	11.8	189.0
2+43	14.4	186.4
2+21	11.8	189.0
2+15	9.4	190.4
1+94	5.6	195.2
1+92	8.2	194.6
1+86	6.9	193.9
1+84	4.4	196.4
1+72	1.7	199.1
1+68	1.3	199.5
1+56	2.0	198.8
T.P. 12.46	212.58	0.65
1+45	9.5	203.1
1+22	11.3	201.3
1+07	9.2	203.4

PLOTTED

41  
MH(22) to MH(41)

212.58

1+00	6.2	206.8	
0+89	4.9	207.7	
0+70	4.9	207.7	
0+60	5.9	206.7	
0+35	4.3	208.3	
0+12	2.4	210.2	
T.P. 11.82	224.21	0.19	212.39
0+00 = MH(41) 40	10.97	213.24	

PLOTTED

MH(41) to D.E. East in Alley.

0+00 = MH(41) 40		213.24	
0+20	7.8	216.4	
bot. Rav. 15's of 0+20	11.9	212.3	
0+40	5.4	218.8	
bot. Rav. 10's of 0+40	10.4	213.8	
0+80	3.1	221.1	
bot. Rav. 8's of 0+80	7.6	216.6	
1+10	0.0	224.2	
bot Rav 9's of 1+10	4.4	219.8	
T.P. 12.83	236.44	0.60	223.61
1+20	12.4	224.0	
bot Rav 7's of 1+20	14.1	222.3	
1+30	12.5	223.9	
4's of 1+30	12.5	223.9	
1+40	10.7	225.7	
11's of 1+40	10.8	225.6	

PLOTTED

Rally #137

11.8  
14.2  
26.1

23

236.44

T.P. 12.37	248.59	0.22	236.22
1+68	11.9	236.7	
17's of 1+68 bot. rav.	21.0	227.6	
1+79	10.2	238.4	
bot. rav. 22's of 1+79	13.9	234.7	
2+02	2.7	245.7	
bot. rav. 22's of 2+02	9.9	238.7	
2+11	3.0	245.6	
T.P. 12.57	260.66	0.50	248.09
2+23	9.3	251.4	
bot. rav. 21's of 2+23	21.1	239.6	
T.P. 12.57	272.61	0.62	260.04
2+34	17.4	255.2	
2+47	15.7	256.9	
2+64	7.6	265.0	
bot. of Rav. 26's of 2+64	26.1	246.5	
2+68	5.3	267.3	
(w. side) yard level. back yard 10's of 2+64	10.4	262.2	
2+75	1.0	271.6	
T.P. 11.58	284.16	0.03	272.58
2+77	9.5	274.7	
2+80	7.3	276.9	
3+08	3.0	281.2	
T.P. 11.61	294.64	1.13	283.03

PLOTTED

294.64

3+16 10.7 282.9  
 3+26 8.8 285.8  
 3+29 9.4 285.2  
 3+35 8.0 286.6  
 3+51 6.8 287.8  
 3+69 5.4 289.4  
 3+76 5.2 289.4  
 4+00 = DE. 3.9 290.7

T.P. 5.54 296.91 3.27 291.37

B.M. Nail top fence post 4.36 292.55

Exist. MH #29 & Vermont Alleg bet Pascoe & Lincoln  
 to MH 30 ✓

B.M. 3.44 295.99 292.55

cb send Barjo 5962's of exist MH 289.92 6.07

2+59<sup>62</sup> = Exist MH (FL.) 7.42 288.572+53<sup>55</sup> = M.H. #29 Top 5.12 290.872+44<sup>62</sup> = wgt vt. 5.67 290.33

2+20 = wL vt. 5.15 290.84

1+50 6.5 289.5

1+00 7.2 288.8

0+50 8.7 287.3

0+00 = M.H. 30 ✓ 9.35 286.64

PLOTTED

PLOTTED

2+60 = MH #31 31

MH 30 to MH (29)

2.06  
2+50 = MH (30) 288.70

1+84 3.5 286.64

1+71 7.7 285.2

1+65 12.0 281.0

1+61 18.0 276.7

1+55 18.7 270.7

1+50 21.6 270.0

1+45 20.8 267.1

1+39 20.4 267.9

1+29 17.1 268.3

1+18 6.0 271.6

0+93 5.2 282.7

0+49 6.1 283.5

0+34 7.6 282.6

0+00 = MH (29) 31 10.03 281.1

MH (29) to MH (28) 31 32

2+14 = MH 29 1.13 279.80 278.67

2+10<sup>21</sup> MH #31 1.7 278.1

2+03 2.9 276.9

1+96 7.9 271.9

T.P. 0.98 267.97 12.81 266.99

1+78 7.6 260.4

1+71 10.8 257.2

1+65 12.4 255.6

T.P. 12.89 255.08

PLOTTED

PLOTTED

12.0  
4  
8.0

24

31  
MH (29) to MH (28)

32

T.P.	0.13	255.21		255.08
1+55			6.6	248.6
1+48			14.2	241.0
T.P. 0.12	242.64	12.69		242.52
1+43			2.0	240.6
1+23			6.5	236.1
1+20			8.1	234.5
1+10			8.4	234.2
1+03			6.8	233.8
0+97			12.0	230.6
0+94			13.5	229.1
T.P. 0.54	231.03	12.15		230.49
0+90			2.1	228.9
0+87			2.4	228.6
0+90			8.7	222.3
0+64			11.4	219.6
T.P. 0.29	218.57	12.75		218.28
0+60			3.6	215.0
0+45			6.6	212.0
0+30			9.6	208.0
0+13			13.4	205.2
T.P. 5.75	211.31	13.01		205.56
0+00 = MH (28)			11.99	199.32

PLOTTED

32

32 33  
MH (28) to MH (19)

211.31

1+62 <sup>08</sup> = MH (28)				199.32
1+49	32	7.9		203.4
1+25		3.8		207.5
1+03		5.5		205.8
T.P. 0.31	199.46	12.16		199.15
0+94		0.0		199.5
0+92		4.8		194.7
0+88		6.6		192.9
T.P. 0.54	189.90	10.10		189.36
0+52		11.6		178.3
0+33		13.7		176.2
0+18		14.1		175.8
0+16		12.9		177.0
0+05		13.0		176.9
0+04		11.8		178.1
0+00 = MH (19)		11.97		177.93

PLOTTED

33

10<sup>th</sup> S of Lincoln

M.H. (28) + 0 DE North

0+00	<sup>13.07</sup> M.H. 28	212.37		199.32
0+03			14.1	198.3
0+09			16.9	195.5
0+14			16.7	195.7
0+19			16.0	196.4
0+34			8.4	204.0
0+44			3.0	209.4
T.P.	12.34	224.39	0.34	212.05
0+54			8.3	216.1
0+64			3.8	220.6
T.P.	12.10	236.44	0.05	224.34
0+74			10.7	225.7
0+87			4.3	231.1
0+90			2.4	234.0
1+00			0.5	235.9
1+10 <sup>12</sup>	= D.E.		+0.4	236.8

PLOTTED

10<sup>th</sup> South of Lincoln

4.67	297.22			
end Vermont				
B.M.	Nail top fence post			292.55
T.P.	4.78	296.27	5.73	291.49
T.P.	2.24	295.06	3.45	292.82
T.P.	2.53	291.57	6.02	289.04
B.M.	Ben Man. Johnson st.	4.72		286.85
T.P.	0.11	280.07	11.61	279.96
(M.H. 33 to end Johnson West)				
M.H. 33		7.79		272.28
0+50		7.7		272.4
0+72 = end		7.0		273.1
DE in Boyd North to M.H. 48				
(M.H. 33 + 0) M.H. (34)				
0+00	<sup>4.56</sup> M.H. 33	276.84		272.28
0+15		5.5		271.3
0+25		4.7		272.1
0+60		4.2		272.6
0+70 = DE		4.1		272.7
1+00		3.4		273.4
1+30		2.9		273.9
1+40		2.9		273.9
1+50		2.8		274.0
2+00		4.9		271.9
W.L. Boyd at 2+00		7.8		269.0
2+30		7.4		269.4
2+50		12.0		264.8
W.L. Boyd at 2+50		21.3		255.5
T.P.	0.49	264.48	12.85	263.99

PLOTTED

PLOTTED

aux.

aux.

	26448			
2+56		2.4	262.1	
2+60		3.4	261.1	
2+65		7.0	257.5	
2+72 <sup>E</sup>		12.8	251.7	
BAI Hub at 2+72	0.19	252.10	12.57	251.91
2+74		2.9	249.2	
2+85		2.7	249.4	
2+95		6.2	245.9	
3+02		8.7	243.4	
3+12		12.6	239.5	
T.P.	0.92	240.70	12.32	239.78
3+18		4.0	236.7	
3+33		12.4	228.3	
T.P.	0.01	228.00	12.71	227.99
3+40		3.3	224.7	
3+49 <sup>30</sup> = MH(34)		9.63	218.37	
MH(34) + 0 MH(37)			218.37	
0+00 = MH(34)			218.37	
0+07		13.2	214.8	
T.P.	0.00	214.91	13.09	214.91
0+25		6.3	208.6	
0+43		14.6	200.3	
T.P.	0.09	202.05	12.95	201.96
0+60		11.2	190.8	
T.P.	0.42	189.40	13.07	188.98

PLOTTED

PLOTTED

	189.40			
0+75		3.7	185.7	
0+81		6.6	182.8	
0+83		9.4	180.0	
0+85 <sup>06</sup> = MH(37)		9.82	179.58	
MH(37) to MH(38)				
0+00 = MH(37)			179.59	
0+10		13.2	176.2	
0+12		11.2	178.2	
0+20		11.2	178.2	
MH 37 1.09	180.67		179.58	
0+37		3.1	177.6	
0+57		7.7	173.0	
0+64		11.5	169.2	
0+74		15.5	165.2	
T.P. 0.22	168.57	12.32	168.35	
0+76		6.9	161.7	
0+78		7.6	161.0	
0+85		7.2	161.4	
0+96		9.1	159.5	
1+06		12.6	156.0	
1+17		12.3	156.3	
1+28		11.1	157.5	
1+44		11.8	156.8	
1+54		13.7	154.9	
T.P. 0.57	156.77	12.39	156.18	

PLOTTED

PLOTTED

156.77

232.49

1+69		3.2	153.6	
1+97 <sup>21</sup>	=MH(38)	5.88	150.89	
	<sup>50</sup>			
	<sup>50</sup>	14		
0+00	=MH(38)+0 MH(12)		150.89	
0+06		7.5	149.3	
0+10		9.8	147.0	
0+16		10.3	146.5	
0+20		12.0	144.8	
T.P.	0.52	144.85	12.44	144.33
0+39		5.3	139.5	
0+46		5.5	139.3	
0+57		8.6	136.2	
0+63		7.5	137.3	
0+64		9.9	134.9	
0+72		9.8	135.0	
0+73		8.9	135.9	
0+80		9.4	135.4	
0+88		10.8	134.0	
T.P.	0.42	132.47	12.78	132.01
1+13		4.0	128.5	
1+20		4.6	127.9	
1+28		6.8	125.7	
1+34		8.9	123.6	
1+41		10.0	122.5	
1+46		11.7	120.8	
1+51		12.6	119.9	

PLOTTED

1+53		13.1	119.4	
1+54		14.8	117.7	
1+59		13.5	119.0	
T.P.	0.87	120.83	12.53	119.96
1+68		3.1	117.7	
1+68		5.6	115.2	
1+73		5.8	115.0	
1+75		4.2	116.6	
1+99		8.6	112.2	
2+19		13.2	107.6	
T.P.	0.20	107.98	13.05	107.78
2+43		5.1	102.9	
2+55		8.0	100.0	
2+73		9.2	98.8	
2+79		10.2	97.8	
2+85 <sup>49</sup>	=MH(12)	9.41	98.57	

PLOTTED

Aug 28

SR Johnson +0 M.H. (38)

B.M. 5.25 292.10 286.85  
 1+50<sup>65</sup> = SR Johnson 4.4 287.7  
 1+30 4.5 287.6  
 1+00 4.4 287.7  
 0+75 3.9 288.2  
 0+50 3.8 288.3  
 0+25 3.8 288.3  
 0+12 4.0 288.1

PLOTTED

0+00 = M.H. (38) 4.87 287.23

M.H. (38) +0 M.H. (39)

1+90<sup>65</sup> = M.H. (39) 287.23

1+77<sup>6</sup> 5.2 286.9

1+40 5.9 286.2

1+10 6.4 285.7

0+97 7.5 284.6

T.R. 0.66 280.97 11.79 280.31

0+55 3.5 277.5

0+25 4.0 277.0

0+21 4.2 276.8

0+20 4.8 276.2

0+00 = M.H. (40) 4.4 276.6

1+88<sup>21</sup> M.H. (40) +0 M.H. (41)  
 (1+89<sup>21</sup>) = M.H. (40) 4.0 276.6

1+73 5.7 275.3

1+70 5.3 275.7

1+59 5.4 275.6

PLOTTED

Leiden  
 Moran  
 Brooks

Par Man  
 Johnson

280.97

T.P. 0.61 269.01 12.57 268.40

1+44 1.0 268.0

T.P. 0.17 256.41 12.77 256.24

1+11 9.0 247.4

1+03 11.5 244.9

0+85 12.9 243.5

T.P. 0.57 243.95 13.05 243.36

0+79 2.1 241.8

0+66 6.6 237.3

0+46 11.8 232.1

T.P. 0.79 231.70 13.04 230.91

0+26 6.8 224.9

T.P. 3.50 222.50 12.70 219.00

0+06 6.4 216.1

0+00 = M.H. (41) 9.24 213.26

40

29



M.H(8)<sup>10</sup> + 0 M.H(32) 44

M.H(8) <sup>10</sup> = 2+6362	11.59	143.12	131.53
2+50 <sup>6</sup>	11.5		131.6
2+47	10.2		132.8
2+37	9.5		133.6
2+16	5.4		137.7
2+00	2.0		141.1
T.P. 12.30	155.11	0.31	142.81
1+94	12.4		142.7
1+81	9.7		145.4
1+68	6.9		148.2
1+55	4.6		150.5
T.P. 11.80	166.84	0.07	155.04
1+39	12.1		154.7
1+26	9.1		157.7
1+22	8.8		158.0
1+04	4.3		162.5
0+96	2.6		164.2
0+90 (T.P.) 12.25	176.99	2.10	164.74
0+82	10.9		166.1
0+72	9.9		167.1
0+62	9.7		167.3
0+50	11.0		166.0
0+47	10.3		166.7
0+41	7.7		169.3
0+32	5.9		171.1
0+24	4.9		172.1

PLOTTED

30

176.99

0+18	3.8		173.2
T.P. 12.68	189.19	0.48	176.51
0+04	11.3		177.9
0+00 = M.H(32) <sup>44</sup>	10.67		178.52
M.H(32) <sup>44</sup> + 0 M.H(31) <sup>43</sup>			
2+6546 = M.H(32) <sup>44</sup>			178.52
2+55	8.0		181.2
2+45	5.3		183.9
T.P. 12.91	201.69	0.41	188.78
2+07	4.0		197.7
T.P. 12.56	213.80	0.45	201.24
1+94	12.0		201.8
1+71	11.1		202.7
1+65	9.2		204.6
1+56	7.6		206.2
1+45	4.5		209.3
1+37	1.9		211.9
1+29	0.1		213.7
T.P. 12.56	226.09	0.27	213.53
1+17	11.0		215.1
0+96	14.0		212.1
0+44	9.2		216.9
0+23	5.6		220.5
0+10	3.0		223.1
0+00 = M.H(31) <sup>43</sup>	2.3		228.4

PLOTTED

+7.6  
+8.0

226.09

T.P.	13.06	238.76	0.39	225.70
T.P.	12.67	250.46	0.97	237.79
T.P.	12.95	261.96	1.45	249.01
T.P.	12.68	274.19	0.45	261.51
T.P.	5.12	277.99	1.32	272.87
MH 33		5.56		272.43

MH(35) to DE South

45

H. Bar 2012 & Boyd.

B.M.	0.00	251.91		251.91
0+78 <sup>28</sup>	= MH(35)	11.34		240.57
0+70 <sup>2</sup>	45	7.3		244.6
0+56		1.7		250.2
0+46		+0.5		254.4
0+44		+2.6		254.5
0+39		+3.1		255.0
0+36		+5.0		256.9
0+15		+8.6		260.5
0+14		+10.1		262.0
0+06		+11.3		263.2
0+05		+12.3		264.2
0+00 = DE		+13.7		265.6
Top septic tank		+14.9		266.8
Pipe entering tank		+14.1		266.0

PLOTTED

MH(35) to MH(36)

45

46

31

251.91

0+00 = MH(35)				240.57
T.P. 0.05	45	240.59	11.37	240.54
0+11			2.1	238.5
0+13			3.5	237.1
0+26			8.2	232.4
0+39			12.6	228.0
0+47			15.2	225.4
0+55			12.6	228.0
0+60			10.9	229.7
0+61			12.0	228.6
0+66 <sup>66</sup>	= MH(36)	11.19		229.40

PLOTTED

MH(36) to MH(37)

0.28

0+00 = MH(36)	46	229.68		229.40
0+05	46		4.0	225.7
0+14			6.9	224.8
0+16			10.0	219.7
0+29			16.8	212.9
T.P. 0.17		216.93	12.92	216.76
0+41			10.0	206.9
0+42			12.9	204.0
T.P. 0.10		204.17	12.86	204.07
0+46			3.1	201.1
0+55			5.9	198.3
0+59			8.4	195.8
0+66			11.1	193.1

PLOTTED

		204.17		
T.P.	0.56	192.37	12.36	191.81
0+76 <sup>5</sup>			3.8	188.6
0+86			6.8	185.6
0+90			8.6	183.8
0+92			11.2	181.2
0+98 <sup>17</sup>	= MH(37)	49	12.75	179.62 (179.58)

PLOTTED

44  
MH(32)+0 MH(42)

51

32

MH 44 (32)				
0700	12.91	191.43		178.52
0+09		8.3		183.1
T.P. 13.06		203.36	1.13	190.30
T.P. 12.76		215.42	0.70	202.66
0+39		10.3		205.1
0+44		9.1		206.3
0+49		5.3		210.1
T.P. 12.44		227.73	0.13	215.29
0+59		9.6		218.1
0+69		3.0		224.7
T.P. 12.81		238.61	2.93	224.80
0+78		8.3		229.3
0+85		4.8		232.8
0+90		1.7		235.9
T.P. 11.28		249.71	0.18	239.43
T.P. 9.70		259.23	0.18	249.53
1+20		9.1		250.1
1+28	(MH 42)	7.4		251.8

MH #51

M.H. 42 to D.E. East

9.2  
3.6  
5.6

33

259.23

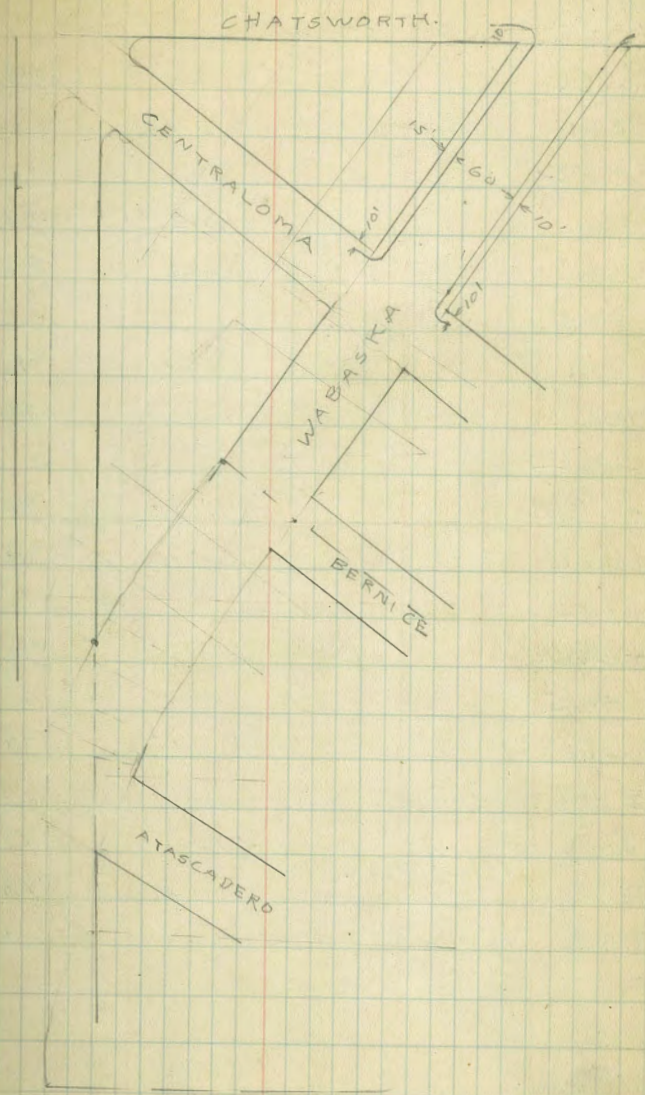
251.8

<del>0+00</del>				
<del>0+20</del>		7.1		21
<del>0+50</del>		8.7		
<del>0+75</del>		9.8		
<del>1+00</del>		11.1		248.1
<del>1+00</del>		15.0		244.2
<del>1+05</del>		15.5		243.7
<del>1+15</del>		16.7		242.5
<del>T.P.</del>	12.77	271.81	0.19	259.04
<del>T.P.</del>	6.94	278.00	0.75	271.06
<del>M.H. 33</del>		5.64		272.36 (272.28)

51  
MH(42) to D.E. East

M.H. 33	4.46	276.74		272.28
	1.21	266.70	11.25	265.49
0+00 = MH(42)			15.1	251.6
T.P.	3.40	257.86	12.24	254.46
0+20			5.5	252.4
0+38			4.9	253.0
0+52			4.0	253.9
0+62			3.8	254.1
1+00			5.8	252.1
1+02			5.1	252.8
1+08			6.6	251.3
1+10			6.1	251.2

Right = East  
Left = West.



X Sec Wabaska St. From S.L.  
Centraloma to N.L. Chatsworth  
cbs 2 walks in - 15' cbs East 10' cbs West  
RPS E  
Tennessee  
Chatsworth.

BM	0.96	97.61	96.65
T.P.	0.50	85.26	12.85
0+00	= S.L. Centraloma Dr.		
Ecb		3.47	81.79
cut		4.25	81.0
1/4		3.72	81.6
1/2		3.46	81.80
3/4		3.50	81.80
cut.		3.89	81.4
wcb		3.17	82.14
0+25			
wcb		3.61	81.65
Ecb		3.77	81.49
0+50			
Ecb		4.08	81.18
wcb		4.05	81.21
0+75			
wcb		4.45	81.81
Ecb		4.54	80.72
1+00			
Ecb		5.03	80.23
wcb		4.91	80.35
1+05 <sup>A</sup>	= N.L. Alley on West		
wcb		5.07	80.19
1+30 <sup>B</sup>	= S.L.		
wcb		5.22	80.04

Plotted 9-14-28 - G.B.H.

Wabeska from N.L. Centraloria to 35

S.L. Tennyson

Right = East  
Left = West.

89.74

85' Street  
60' Footway 15' cb East  
10' cb West.

1+25	85.26		
w cb	5.38	79.88	
Ecb	5.57	79.69	
1+50			
Ecb	6.13	79.13	
wcb	5.85	79.41	
1+75			
wcb	6.30	78.96	
Ecb	6.61	78.65	
1+96.67			
Ecb	7.05	78.21	
wcb	6.72	78.54	
2+00			
wcb	6.77	78.49	
2+25			
wcb	7.19	78.07	
2+73.20 = N.L. Chatsworth on West.			
wcb	7.70	77.56	
Ecb on ret.			
N.L. Chatsworth on East.	7.24	78.02	
T.P.	6.72	89.74	2.24
			83.02

0+00 = N.L. Centraloria.			
E.L.	7.1	82.6	
cb	7.54	82.20	
gut.	8.09	81.65	
1/4	7.78	81.9	
1/2	7.41	82.33	
3/4	7.37	82.9	
gut.	7.72	82.02	
wcb	7.16	82.58	
0+02			
wcb	7.12	82.62	
gut.	7.5	82.2	
1/4	7.5	82.2	
1/2	7.6	82.1	
3/4	7.5	82.2	
1	7.8	81.9	
1/4	7.9	81.8	
1/2	7.7	82.0	
3/4	7.2	82.5	
cb	7.2	82.5	
1/2	7.2	82.5	
1	6.9	82.8	
E.L.	6.8	82.9	

Plotted 9-14-28 C.B.H.

Chs Walks in on West  
No Inquiries on East

Wabaska

0+25	89.74	
E.L.	6.2	83.5
+10	6.2	83.5
cb	6.7	83.0
+5	6.9	82.8
+14	7.2	82.6
1/4	7.6	82.1
+6	8.0	81.7
+6	7.7	82.0
E	7.4	82.3
+10	7.1	82.6
1/4	7.3	82.4
+7	7.5	82.2
gut.	7.3	82.4
web	6.88	82.86
0+50		
web	6.58	83.16
gut.	7.0	82.70
+10	7.0	82.7
1/4	7.0	82.7
+6	6.9	82.8
E	7.0	82.7
+7	7.2	82.5
+12	7.8	81.9
1/4	6.9	82.8
+5	6.9	82.8

36

+12	89.74	6.6	83.1
cb		6.5	83.2
+10		6.4	83.3
E.L.		6.0	83.7
0+75			
E.L.		5.4	84.3
+5		5.7	83.8
+10		6.1	83.6
cb		6.2	83.5
+5		6.5	83.2
+13		6.6	83.1
1/4		6.8	82.9
+3		7.5	82.2
+6		7.1	82.6
E		6.9	82.8
+7		6.6	83.1
1/4		6.7	83.0
+9		6.8	82.9
gut.		6.7	83.0
web		6.27	83.47
1+00			
web		5.96	83.78
gut.		6.6	83.1
+7		6.5	83.2
1/4		6.4	83.3
+5		6.5	83.2
E		6.7	83.0

## Wabaska St.

4+10	8974	6.8	82.9
+12		7.2	82.5
1/4		6.5	83.2
+10		6.2	83.5
cb		6.0	83.7
E.L.		5.6	84.1
1+0.5 = 56. Alley on West.			
E.L.		5.6	84.1
cb		6.0	83.7
1/4		6.5	83.2
+3		7.2	82.5
+9		6.8	82.9
4		6.6	83.1
+7		6.5	83.2
1/4		6.3	83.4
+6		6.4	83.3
+12		6.6	83.1
gut		6.5	83.2
wcb		5.90	83.84
1+20 = NL			
wcb		5.62	84.12
gut		6.4	83.3
+9		6.2	83.5
1/4		6.1	83.6
+7		6.1	83.6
4		6.4	83.3
+5		6.6	83.1

37

1+20	8974		
4+9		6.7	83.0
+13		7.0	82.7
1/4		6.3	83.4
+10		6.2	83.5
+12		6.3	83.4
cb		6.0	83.7
+5		5.8	83.9
E.L.		5.5	84.2
1+50			
E.L.		5.4	84.3
+10		5.8	83.9
cb		5.9	83.8
+3		6.1	83.6
+5		6.0	83.7
+14		6.1	83.6
1/4		6.5	83.2
+2		6.8	82.9
+5		6.5	83.2
+10		6.5	83.2
4		6.0	83.7
+7		5.6	84.1
1/4		5.7	84.0
+5		5.8	83.9
+12		6.0	83.7
gut		5.9	83.8
wcb		5.24	84.50



## Wabaska St

	8974	
1+75		
wcb	4.99	84.75
qvt	5.6	84.1
+5	5.8	83.9
+10	5.5	84.2
1/4	5.4	84.3
+5	5.4	84.3
¢	5.8	83.9
+5	5.9	83.8
+12	6.3	83.4
1/4	6.1	83.6
+4	5.9	83.8
+8	5.8	83.9
+10	5.9	83.8
cb	5.7	84.0
+10	5.4	84.3
E.L.	5.0	84.7
2+00		
E.L.	4.8	84.9
+5	5.1	84.6
+10	5.3	84.4
cb	5.6	84.1
+7	5.6	84.1
+12	5.8	83.9
1/4	5.9	83.8
+2	6.0	83.7
+10	5.8	83.9

	8974	
2+00		
¢	5.6	84.1
+7	5.4	84.2
1/4	5.3	84.4
+5	5.4	84.3
+10	5.4	84.3
qvt	5.4	84.3
wcb	4.83	84.91
2+25		
wcb	4.58	85.16
qvt	5.0	84.7
+5	5.0	84.7
+10	5.1	84.6
1/4	5.1	84.6
+5	5.2	84.5
+10	5.4	84.3
¢	5.6	84.1
+5	5.4	84.3
+10	5.7	84.0
+12	5.5	84.2
1/4	5.6	84.1
+4	5.2	84.5
+10	4.9	84.8
cb	4.8	84.9
+5	4.8	84.9
+6	4.5	85.2
+	4.6	85.1

Wabaska St.

2 + 25 = 0 + 00 = S.L. Bernice  
89.74

0 + 60 89.74

E.L.	4.3	85.4
0 + 30		
E.L.	4.1	85.6
+10	4.4	85.3
cb	4.5	85.2
+5	4.5	85.2
+10	4.5	85.2
1/4	4.8	84.9
+5	5.3	84.3
+10	5.2	84.0
+	5.2	84.5
+8	5.1	84.6
1/4	5.0	84.7
+5	4.8	84.9
cb	4.5	85.2
+5 (10' cbs)	4.4	85.3
W.L.	4.4	85.5
Street Converges dist. from web.		
0 + 60 = N.L. Bernice = B.S. on West		
wcb	4.53	85.21
gut	4.8	84.9
+5	4.7	85.0
+10	4.7	85.0
1/4	4.8	84.9
+5	4.9	84.8
+10	5.0	84.7
+	5.0	84.7

+	5.1	84.6
+10	5.1	84.6
+12	5.1	84.6
1/4	4.9	84.8
+3	4.6	85.1
+10	4.6	85.1
cb	4.6	85.1
+7	4.4	85.3
+12 = E.L.	4.1	85.6
Cv. stationed on West side Sect. radial 10 bars		
wcb		
T.P. 6.10	91.26	4.58
0 + 94.26		85.16
wcb	5.83	85.43
gut	6.2	85.1
+5	6.0	85.3
+10	6.1	85.2
1/4	6.2	85.1
+5	6.2	85.1
+10	6.2	85.1
+	6.3	85.0
+5	6.4	84.9
+8	6.5	84.8
1/4	6.5	84.8
+3	5.9	85.4
+10	5.9	85.4

## Wabaska St.

0+9496	91.26	
Ecb	5.5	85.8
+9 = EL	4.9	80.4
1+2992		
web	5.61	85.65
gut	5.9	85.4
+5	5.9	85.4
+10	6.0	85.3
1/4	6.1	85.2
+5	6.1	85.2
+10	6.1	85.2
E	6.2	85.1
+5	6.2	85.1
+9	6.1	85.2
+13	5.9	85.4
1/4	6.0	85.3
+5	5.7	85.6
+9	5.1	80.2
web	4.6	86.7
+5 = EL	4.5	86.8
1+6488		
web 1160	5.9	85.4
+3	5.9	85.4
+7	5.7	85.7
1/4	5.9	85.4
+5	5.9	85.4
+10	6.0	85.3

146488	91.26	
E	6.0	85.3
+5	5.7	85.6
+11	5.7	85.6
+14	5.2	86.1
1/4	5.2	86.1
+4	4.8	86.5
+9 = Int with Tennyson. SL	4.9	86.5
NL Alleg. at 1+808 web	5.37	85.89
1+9924		
web	5.23	86.03
gut	5.6	85.7
+5	5.7	85.6
+10	5.8	85.5
1/4	5.9	85.6
+5	5.6	85.7
+10	5.8	85.5
E	5.7	85.6
+4 = Int SL Tennyson	5.6	85.7
2+3480		
web	5.06	86.2
gut	5.7	85.6
+5	5.6	85.7
+10	5.5	85.8
1/4	5.5	85.8
+5 = Int SL Tennyson	5.4	85.9

164.88  
15.5  
180.38

40

Wabaska St.

2 + 99<sup>76</sup>

91.26

wcb 5.00 86.3

gut 5.4 85.9

4.5 5.4 85.9

+ 9 = Int with SL Tennyson 5.3 86.0

2 + 90<sup>1</sup> =  $\frac{E.L.}{3}$ : Atascadero.

wcb 4.74 86.52

gut 5.1 86.2

+ 3<sup>E</sup> = Int. S.L. Tennyson 5.3 86.0

Nail Pole SE. Tennyson  
B.M. 2 Wabaska.

7.49 95.59 3.16 88.10

T.P. 5.94 100.73 0.80 94.79

B.M. Beginning 4.09 96.64

Bernice Drive from  
W.L. Wabaska to Lacresta.

41

BM Nail Pole 2.92 91.02 88.10

0 + 00 cbs = walks in  
90' Roadway 10' cbs

Ncb 5.45 85.57

Scb 5.56 85.46

0 + 25

T.P. Scb 10.32 96.34 5.00 86.02

Ncb 10.22 86.1

0 + 50

Ncb 9.55 86.7

Scb 9.63 86.7

0 + 75

Scb 9.00 87.3

Ncb 9.00 87.3

1 + 00

Ncb 8.28 88.0

Scb 8.35 88.0

1 + 25

Scb 7.67 88.6

Ncb 7.66 88.6

1 + 50

Ncb 7.05 89.3

Scb 7.01 89.3

1 + 75

Scb 6.46 89.8

Ncb 6.47 89.8

2+00	96.34		
Ncb	5.83	90.5	
Scb	5.87	90.5	
2+25			
Scb	5.30	91.0	
Ncb	5.14	91.2	
2+50			
Ncb	4.50	91.8	
Scb	4.58	91.8	
2+75			
Scb	3.76	92.5	
Ncb	3.86	92.5	
3+00			
Ncb	3.23	93.1	
Scb	2.94	93.4	
3+25			
Scb	1.92	94.4	
Ncb	2.23	94.1	
3+50			
Ncb	1.15	95.2	
Scb	0.75	95.6	
T.P. 12.09	108.09	0.34	96.00
3+75			
Scb	11.28	96.8	
Ncb	11.68	96.4	

4+00	108.09		
Ncb	10.41	97.7	
Scb	10.00	98.1	
4+25	8.77		
Scb	8.78	99.3	
Ncb	9.18	98.9	
4+50			
Ncb	7.95	100.1	
Scb	7.57	100.5	
4+75			
Scb	6.24	101.9	
Ncb	6.72	101.4	
5+00			
Ncb	5.44	102.7	
Scb	5.04	103.1	
5+25			
Scb	3.83	104.3	
Ncb	4.22	103.9	
5+50			
Ncb	2.96	105.1	
Scb	2.43	105.9	
5+75			
Scb	1.14	107.0	
Ncb	1.66	106.4	
6+00			
Ncb	0.00	108.0	
T.P. 12.92	120.84	0.17	107.92

## Dernice

6400	120.84		
Scb	12.32	108.52	
6+25			
Scb	10.40	110.4	
Ncb	10.93	109.9	
6+50			
Ncb	8.69	112.2	
Scb	8.47	112.4	
6+75			
Scb	6.19	114.7	
Ncb	6.40	114.4	
7+00			
Ncb	4.20	116.6	
Scb	3.98	116.9	
7+25			
Scb	1.77	119.11	
Ncb	1.96	118.9	
T.P.	13.01	133.51	0.3d 120.50
7+50			
Ncb	12.48	121.0	
Scb	12.23	121.3	
7+75			
Scb	10.07	123.4	
Ncb	10.22	123.3	
8+00			
Ncb	7.94	125.6	
Scb	7.83	125.7	

43

8+25	133.51		
Scb	5.38	128.1	
Ncb	5.60	127.9	
6+50			
Ncb	2.84	130.7	
Scb	2.92	130.6	
T.P.	12.38	145.73	0.16 133.35
8+75			
Scb	11.92	133.8	
Ncb	11.98	133.8	
9+00			
Ncb	8.46	137.3	
Scb	8.65	137.1	
9+25			
Scb	5.35	140.4	
Ncb	4.87	140.9	
9+50			
Ncb	1.28	144.5	
9+43 <sup>22</sup>	= BC SW ret.		
Scb	2.96	142.8	
9+59 <sup>2</sup>	(on ret. sw)		
Scb	0.87	144.9	
T.P.	12.47	158.06	0.14 145.59
9+75			
Ncb	10.10	148.0	
9+78 <sup>41</sup>	= BC NW ret	9.67	148.39

Aug 20-28

Landon  
Morgan  
Brookes.

\$58.06

E.L. Lacrestq = 9+85<sup>20</sup> North = 9+75 South.

Ncb	8.99	149.1
R1' - gut	9.50	148.6
1/4	9.65	148.4
1/2	10.04	148.0
3/4	10.54	147.5
Scb	11.14	146.9
+14 = sgut	12.30	145.7

Scb = 9+75 on south

T.P.	12.27	170.27	0.06	158.00
T.P.	3.17	173.37	0.07	170.20
Nail Pole NE. Welles Bernice BM	4.64	168.93		
T.P.	0.55	161.99	11.93	161.44

Ascadero from SL Wall's

W.L. Tennyson.

cb 52 S. Wall's in

44

0+00 = SL Wall's 161.99

40' Railway  
10' Cb 5.

Wcb	8.96	152.03	
Ecb	11.44	150.55	
0+25			
Wcb	10.94	151.05	
Ecb 156	150.49	13.06	148.93
0+50 F			
Ecb	3.23	147.26	
Wcb	1.17	149.32	
0+75			
Wcb	2.76	147.73	
Ecb	4.89	145.60	
1+00			
Ecb	6.48	144.01	
Wcb	4.31	146.18	
1+26 1/2 = B.C.			
Wcb	5.89	144.60	
Ecb	8.04	142.45	
Cont. of Curve			
Ecb	9.13	141.36	
Wcb	8.25	142.24	
EC = 0+00			
Wcb = Scb	11.28	139.21	
Ecb = Ncb	10.56	139.93	
T.P. 0.39	137.94	12.94	137.55

## Atascadero

0+25	137.94		
Ncb	0.42	137.52	
Scb	1.98	135.96	
0+50			
Scb	5.57	132.37	
Ncb	5.00	132.94	
0+75			
Ncb	8.66	129.28	
Scb	9.00	128.94	
1+00			
Scb	12.33	125.61	
Ncb	12.03	125.91	
T.P. 0.05	125.10	12.89	125.05
1+25			
Ncb	2.02	123.08	
Scb	2.53	122.57	
1+50			
Scb	5.03	120.07	
Ncb	4.59	120.41	
1+75			
Ncb	6.93	118.17	
Scb	7.36	117.74	
2+00			
Scb	9.53	115.57	
Ncb	9.23	115.87	

45

2+25	125.10		
Ncb	11.35	113.75	
Scb	11.67	113.43	
T.P. 0.43	112.70	12.83	112.27
2+50			
Scb	1.31	111.39	
Ncb	1.04	111.66	
2+75			
Ncb	2.99	109.71	
Scb	3.08	109.62	
3+00			
Scb	4.84	107.86	
Ncb	4.81	107.89	
3+25			
Ncb	6.51	106.19	
Scb	6.50	106.20	
3+50			
Scb	8.05	104.65	
Ncb	8.05	104.65	
3+75			
Ncb	9.49	103.21	
Scb	9.49	103.21	
4+00			
Scb	10.87	101.83	
Ncb	10.92	101.78	



## Atascadero

A+25	112.70		
Ncb	12.38	100.32	
Scb	12.36	100.34	
T.P. 0.10	99.70	13.10	99.60
A+50			
Scb	0.55	99.15	
Ncb	0.56	99.14	
A+75			
Ncb	1.70	98.00	
Scb	1.81	97.89	
5+00			
Scb	2.92	96.78	
Ncb	2.78	96.92	
5+25			
Ncb	3.90	95.80	
Scb	3.90	95.80	
5+50			
Scb	4.90	94.80	
Ncb	4.99	94.71	
5+75			
Ncb	6.06	93.64	
Scb	5.87	93.83	
6+00			
Scb	6.93	92.77	
Ncb	7.10	92.60	

46

6+25	99.70		
Ncb	8.13	91.57	
Scb	8.04	91.66	
6+50			
Scb	9.00	90.70	
Ncb	9.09	90.61	
6+75			
Ncb	10.15	89.55	
Scb	9.98	89.72	
7+00			
Scb	10.94	88.76	
Ncb	11.10	88.60	
7+25			
Ncb	11.90	87.80	
Scb	11.77	87.93	
7+50			
Scb	12.46	87.24	
Ncb	12.44	87.26	
7+53 <sup>53</sup>	= BC. N.W. return north		
Ncb	12.50	87.20	
7+75			
Scb	12.92	86.78	
T.P. 2.32	91.47	10.55	99.15
7+85 <sup>64</sup>	= W.L. Tennyson on South		
Scb	4.89	86.59	
W.L. Tennyson on North (on rot)			
Ncb	4.39	87.08	

Atascadero

91.77

B.M. Beginning 3.44 88.03 (88.10)  
 B.M. BR NE Tennessee 5.9.1 85.56

London, Esball, Morgan Aug 21-28

Tennyson st from Chatsworth to Wells. 60' street 10' cbs

All cbs & walks in on South side.

Walks & cbs in on North to 6+74<sup>S</sup>

Right = North Left = South.

B.M. 1.02 97.67 96.65

0+00 = End Pav. Chatsworth = E.C. SW. ret.

Scb	3.14	94.5
cut	3.87	93.8
1/4	3.47	94.2
1/2	3.27	94.4
3/4	3.43	94.2
cut	3.83	93.8
Ncb	3.18	94.5
0+25		
Ncb	3.55	94.1
Scb	3.61	94.1
0+50		
Scb	4.08	93.6
Ncb	4.01	93.7
0+75		
Ncb	4.52	93.2
Scb	4.52	93.2

Plotted 9-20-28  
 T.S.H.  
 Yardage 1229-112  
 1 B 12 P 203

1+00

97.67

Scb	4.99	92.7
Ncb	4.93	92.7
1+25		
Ncb	5.39	92.3
Scb	5.41	92.3
1+50		
Scb	5.98	91.7
Ncb	5.89	91.8
1+75		
Ncb	6.43	91.2
Scb	6.40	90.3
2+00		
Scb	6.95	90.7
Ncb	6.84	90.8
2+25		
Ncb	7.32	90.4
Scb	7.47	90.2
2+50		
Scb	7.94	89.7
Ncb	7.82	89.8
2+75		
Ncb	8.33	89.3
Scb	8.33	89.3
3+00		
Scb	8.72	88.9
Ncb	8.80	88.9

## Tennison

3+25		97.67	
T.P.	3.43	92.21	88.79
3+25			
Ncb		3.80	88.7
Scb		3.77	88.4
3+50			
Scb		4.14	88.1
Ncb		4.03	88.2
3+75			
Ncb		4.32	87.9
Scb		4.41	87.8
4+00			
Scb		4.69	87.5
Ncb		4.63	87.6
4+25			
Ncb		4.93	87.3
Scb		4.93	87.3
4+34 <sup>23</sup>	= E.L. Warrington		
Scb		5.3	86.9
Scb		5.07	87.1
Ncb		5.04	87.2
4+50			
Ncb		5.20	87.0
4+75			
Ncb		5.47	86.7
5+00			
Ncb		5.80	86.4

5+25		92.21	
Ncb		6.03	86.2
5+50			
Ncb		6.35	85.8
5+74 <sup>50</sup>	= E.L. Warrington		
Ncb		6.61	85.6
BP NE Warrington & Tennison			
B.M.		6.58	85.6 85.63
10.87		96.50	85.63
6+39 <sup>5</sup>	= W.L. Warrington		
Ncb		10.43	86.1
6+74 <sup>5</sup>	= end of inputs on North.		
N.L.		10.0	86.5
+6		9.9	86.6
Ncb		10.17	86.3
+3		10.5	86.0
1/4		10.2	86.3
1/4		10.1	86.4
1/4		10.0	86.5
+4		9.9	86.6
1/4		10.0	86.5
Scb		9.36	87.14
6+86 <sup>5</sup>			
Scb		9.22	87.3
1/4		10.0	86.5
1/4		9.9	86.6
1/4		10.0	86.5
+8		10.0	86.5

Tennyson  
96.50

6+865		
1/4	10.0	86.5
+5	10.2	86.3
cb	10.2	86.3
N.L.	9.8	86.7
7+00		
N.L.	9.3	87.2
cb	10.0	86.5
+5	10.0	86.5
1/4	9.9	86.6
⊕	9.9	86.6
1/4	9.8	86.7
+5	9.9	86.6
gut	9.9	86.6
5cb	9.11	87.4
7+135	- FC on South	
5cb	8.92	87.6
gut	9.6	86.9
+5	9.7	86.8
1/4	9.7	86.8
⊕	9.6	86.9
1/4	9.7	86.8
+8	9.6	86.9
cb	9.5	87.0
+4	9.1	87.4
N.L.	9.0	87.5

49

7+25

96.50

N.L.	8.8	87.7
+6	9.0	87.5
cb	9.6	86.9
+5	9.8	86.7
1/4	9.7	86.8
⊕	9.5	87.0
1/4	9.6	86.9
gut	9.5	87.0
5cb	8.75	87.8
7+50		
5cb	8.40	88.1
gut	9.2	87.3
1/4	9.1	87.4
⊕	9.1	87.4
+6	9.3	87.2
1/4	9.2	87.3
+5	9.1	87.4
cb	9.0	87.5
N.L.	8.4	88.1
7+75		
N.L.	7.9	88.6
+7	7.9	88.6
cb	8.3	88.2
+8	8.8	87.7
1/4	7.0	87.5
⊕	8.8	87.7

Tennyson  
96.50

7+75  
 4+5 8.7 87.8  
 1/4 8.7 87.8  
 gut 8.8 87.7  
 Seb 8.04 88.5

8+00 = EL. Allegon South

Seb 7.67 88.8  
 gut. 8.4 88.1  
 1/4 8.3 88.2  
 4 8.3 88.2  
 1/4 8.8 87.7  
 +3 8.8 87.7  
 +7 8.0 88.5  
 cb 8.0 88.5  
 +5 7.4 89.1  
 NL 7.0 89.5

8+08<sup>54</sup> = EL. Wabaska on North

NL 7.2 89.3  
 cb 7.8 88.7  
 +2 7.9 88.6  
 +5 8.6 87.9  
 1/4 8.6 87.9  
 4 8.1 88.4  
 +8 8.0 88.5  
 1/4 8.2 88.3  
 +6 8.3 88.4  
 5 cb 8.2 88.3

965

50

8+19 = WL Allegon South

Seb 7.35 89.15  
 gut 7.7 88.6  
 1/4 7.9 88.6  
 +6 7.7 88.8  
 4 7.8 88.7  
 +5 8.0 88.5  
 1/4 8.4 88.1  
 +7 8.5 88.0  
 cb 7.7 88.8  
 +3 8.0 88.5  
 NL 7.4 89.1

8+50

NL 7.2 89.3  
 +2 8.0 88.5  
 cb 7.8 88.7  
 1/4 7.5 89.0  
 4 7.2 89.3  
 1/4 7.2 89.3  
 gut 7.4 89.1  
 Seb 6.66 89.8

8+55

Seb 6.53 90.0  
 gut 7.2 89.3  
 1/4 7.1 89.4  
 +5 7.0 89.5  
 4 7.1 89.4

Tennyson  
96.05

8+55		
1/4	7.4	89.1
cb	7.7	88.8
N.L.	7.8	88.7
8+75		
N.L.	7.5	89.0
cb	7.3	89.2
1/4	6.9	89.6
+4	6.7	89.8
d	6.6	89.9
+7	6.6	89.9
1/4	6.7	89.8
gut	6.7	89.8
Sub	6.03	90.5
9+00		
Sub	5.29	91.2
gut	5.9	90.6
1/4	6.0	90.5
+7	6.0	90.5
d	6.1	90.4
+5	6.2	90.3
1/4	6.4	90.1
+6	6.5	90.0
cb	6.7	89.8
+3	6.6	89.9
+8	7.1	89.4
N.L.	7.3	89.2

51

9+25		
N.L.	5.5	91.0
+2	5.5	91.0
+4	6.0	90.5
cb	6.1	90.7
+5	5.8	90.7
1/4	5.8	90.7
+8	5.7	90.8
d	5.6	90.9
+5	5.6	90.9
+8	5.3	91.2
1/4	5.3	91.2
+5	5.3	91.2
gut	5.3	91.2
Sub	4.54	92.0
9+52	= SL Alicia Dr. on South.	
Sub	3.79	92.7
gut	4.2	92.3
1/4	4.6	91.9
d	4.6	91.9
+8	4.7	91.8
1/4	4.9	91.6
+5	5.0	91.5
cb	5.4	91.1
+4	5.2	91.3
+5	4.8	91.7
N.L.	4.7	91.8

Tennyson

965

9+75

N.L	4.0	92.5
+6	3.8	92.7
+7	4.9	91.6
cb	4.7	91.8
+4	4.3	92.2
1/4	4.0	92.5
⊕	3.7	92.8
1/4	3.6	92.9
+6	3.6	92.9
5. cb	3.6	92.9
10+00		
3 cb	2.6	93.9
1/4	2.8	93.7
⊕	2.9	93.6
+6	2.9	93.6
1/4	3.1	93.4
+5	3.1	93.4
+6	3.8	92.7
+9	4.4	92.1
cb	3.9	92.6
+1	3.3	93.2
N.L	3.1	93.4

965

52

10+26 = N.L Alicia D.C.

N.L	2.8	93.7
+7	2.4	94.1
+8	3.4	93.1
cb	3.4	93.1
+5	2.9	93.6
+6	2.0	94.5
1/4	2.2	94.3
⊕	2.0	94.5
1/4	2.0	94.5
cb+2 = gut	1.7	94.8
5 cb (con ret.)	0.86	95.2
10+35 = F.C. ret.		
5 cb	0.78	95.7
gut	1.6	94.9
1/4	0.7	95.8
⊕	0.7	95.8
1/4	2.0	94.5
+4	1.9	95.6
+6	2.8	93.7
cb	3.2	93.3
+1	2.4	94.1
+6	1.8	94.7
N.L	2.1	94.4

Tennyson

10+50	96.50	95.0
N.L.	1.5	95.0
+6	1.4	95.1
cb	2.5	94.0
+3	2.8	93.7
+8	1.8	94.7
1/4	1.6	94.9
1/2	1.2	95.3
+6	1.1	95.4
1/4	1.3	95.2
+5	1.3	95.2
qut	1.2	95.3
Sub 11.21	107.45	0.26
		96.24
10+75		
Sub	10.30	97.2
qut	11.2	96.3
+4	11.4	96.1
1/4	11.2	96.3
1/2	11.2	96.3
1/4	11.8	95.7
+3	12.0	95.5
+7	12.5	95.0
cb	13.1	94.4
+2	11.7	95.8
+4	11.6	95.9
N.L.	11.6	95.9

11+00

107.45

53

N.L.	10.7	96.8
+8	10.7	96.8
cb	12.2	95.3
+2	12.1	95.4
+7	10.9	96.6
1/4	10.8	96.7
1/2	10.3	97.2
1/4	10.3	97.2
qut	10.3	97.2
cb	9.33	98.1
11+25		
Sub	8.40	99.1
qut	9.1	98.4
1/4	9.3	98.2
1/2	9.5	98.0
+6	9.7	97.9
1/4	9.9	97.6
+6	10.1	97.4
+3	10.4	97.1
+9	11.6	95.9
cb	11.6	95.9
+2	10.3	97.2
+3	9.9	97.6
N.L.	9.8	97.7



Tennyson  
107.45

11450

NL	8.8	98.7
+4	8.9	98.6
+6	9.0	98.5
+9	10.8	96.7
cb	10.7	96.8
+3	9.4	98.1
1/4	9.0	98.5
E	8.5	99.0
1/4	8.3	99.2
gut	8.0	99.5
Sub	7.53	99.9
11+75		
Sub	6.58	100.9
gut	7.3	100.2
1/4	7.6	99.9
E	7.9	99.6
1/4	8.3	99.2
+6	8.7	98.8
cb	9.5	98.0
+1	9.5	98.0
+5	8.1	99.4
NL	7.9	99.6

12+00

NL	7.2	100.3
+5	7.2	100.3
+7	7.9	99.6
+8	9.0	98.5
+9	9.0	98.5
cb	8.4	99.1
+3	7.7	99.6
1/4	7.4	100.1
E	7.0	100.5
+9	6.8	100.7
1/4	6.8	100.7
gut	6.5	101.0
Sub	5.64	101.8
12+10 <sup>A</sup>	= E.L. Alley on South	
Sub	5.35	102.1
12+25 <sup>A</sup>	= NL Alley on South	
Sub	4.70	102.8
gut	5.4	102.1
1/4	6.1	101.4
E	6.1	101.4
1/4	6.5	101.0
+8	6.9	100.6
cb	8.0	99.5
+2	7.9	99.6
+4	6.3	101.2
NL	6.2	101.3

107.45

54

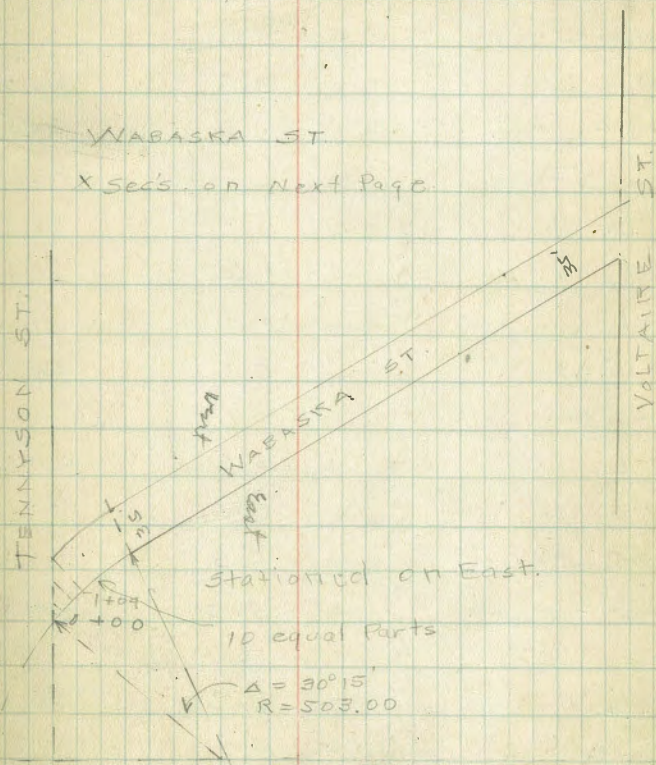
12+50

107.45

N.L.	5.3	102.2
+5	5.4	102.1
+7	5.9	101.6
+8	6.8	100.7
cb	6.7	100.8
+3	5.7	101.8
+7	5.4	102.1
1/4	5.4	102.1
1/2	5.2	102.3
+9	4.8	102.7
1/4	4.8	102.7
+5	4.6	102.9
gut	4.7	102.8
Scb	3.77	103.7
12+75 <sup>3</sup> = E.L. Wells.		
Scb	2.87	104.6
gut	3.6	103.9
1/4	3.8	103.7
1/2	4.1	103.4
1/4	4.6	103.9
+5	5.0	102.5
cb	5.9	101.6
+3	5.8	101.7
+4	4.9	102.6
+5	4.6	102.9
N.L.	4.5	103

107.45  
S.E. Wells & Tennyson.  
B.M. Tab F.H.

0.40

(107.07)  
107.05

X Sec Wabaska St From NL  
 Tennyson to Kottaire. Right = East  
 NE. Warrington & Tennyson. Left = West.  
 BM 8.75 94.38 85.63

0+00		
EL	5.1	89.3
0+26 <sup>50</sup>		
EL	3.9	90.5
+6 <sup>5</sup> = Int.	5.4	89.0
0+53 <sup>10</sup>		
EL	4.1	90.3
+8	4.6	
+11	5.4	
+15 = Int.	5.6	88.8
0+79 <sup>65</sup>		
EL	4.5	89.9
+5	4.5	
+8	5.3	
+24 <sup>4</sup> = Int.	5.2	89.2
1+0A		
EL	5.0	89.4
+4	4.9	
+6	5.8	
EL	5.4	89.0
+26	5.2	
+30	4.6	
W.L. = NL Tennyson on West.	4.1	90.3

PLOTTED 9-14-28 - C.B.H.

Aug 22-28  
 Loudon  
 Isbell  
 Morgan  
 1+06<sup>20</sup>

94.38

56

W.L.	3.9	90.6
+5	4.2	
+9	5.1	
1+32 <sup>50</sup>	5.4	89.0
+25	5.7	
+29	5.9	
+32	4.9	
EL	5.1	89.3
1+32 <sup>25</sup>		
EL	5.7	88.7
+4	6.2	
+17 <sup>5</sup> = EL	5.7	88.7
+24	5.5	
+29	4.4	
+34	4.3	
W.L.	3.6	90.8
1+59 <sup>50</sup>		
W.L.	3.9	90.5
+2	3.9	
+3	5.2	
+5	4.5	
+12	5.7	
+17 <sup>5</sup> = EL	6.0	88.4
+32	6.6	
EL	5.8	88.6

9438

1+85<sup>85</sup>

E.L. 6.0 88.4

+3 6.8

+17<sup>5</sup> = ~~4~~ 6.3 88.1

+24 5.9

+30 4.5

W.L. 3.1 91.3

2+12<sup>10</sup>

W.L. 4.4 90.0

+3 5.5

+7 5.6

+8 6.2

+17<sup>5</sup> = ~~4~~ 6.8 87.6

+29 6.9

+30 6.3

+32 6.3

E.L. 6.9 87.5

2+38<sup>95</sup>

E.L. 7.1 87.3'

+5 7.2

+7 6.5

+9 6.5

+10 7.2

+17<sup>5</sup> = ~~4~~ 7.2 87.2

+29 6.7

+30 6.8

+33 6.3

9438

57

2+38<sup>95</sup>

W.L. 6.3 88.1

2+65<sup>50</sup> = E.C.

W.L. 7.7 86.7

+5 7.5

+17<sup>5</sup> = ~~4~~ 7.9 86.4

+20 7.9

+23 7.0

+25 7.7

+30 7.5

E.L. 7.6 86.8

3+00

E.L. 8.7 85.7

+5 8.5

+10 8.8

+12 8.3

+13 8.6

+17<sup>5</sup> = ~~4~~ 8.7 85.7

+30 8.5

W.L. 8.5 85.9

3+28

W.L. 9.3 85.1

+17<sup>5</sup> = ~~4~~ 9.4 85.0

+23 9.4

+25 9.1

+26 9.5

E.L. 9.2 85.2

9438

3+50		
E.L.	9.9	84.5
+9	9.9	
+11	9.4	
+13	9.7	
+17.5¢	9.9	84.5
+25	9.7	
W.L.	9.8	84.6
4+00		
W.L.	10.8	83.6
+15	10.6	
+17.5¢	10.4	84.0
+20	10.2	
+22	10.4	
+25	10.3	
+30	10.6	
E.L.	11.0	83.3
4+25		
E.L.	11.7	83.7
+10	11.0	
+17.5¢	10.9	83.5
W.L.	11.3	83.1

58

4+50	94.38	
W.L.	11.9	82.5
+6	11.6	
+17.5¢	11.5	82.9
+23	11.7	
+30	11.9	
E.L.	12.1	82.3
T.P. 110	85.38	10.10
84.28		
4+75		
E.L.	4.3	81.1
+6	4.1	
+9	3.2	
+17.5¢	3.0	82.4
+22	3.1	
+30	3.2	
W.L.	3.3	82.1
5+00		
W.L.	3.7	81.7
+10	4.0	
+16	3.7	
+17.5¢	3.7	81.7
+25	4.3	
E.L.	4.5	80.9

8538

5+25		
E.L.	5.5	79.9
+5	5.1	
+12	4.7	
+13	4.4	
+17.5¢	4.2	81.2
+20	4.5	
W.L.	4.2	81.2
5+50		
W.L.	5.1	80.3
+8	5.1	
+15	5.4	
+17.5¢	4.9	80.5
+20	5.5	
+25	6.5	
+32	7.1	
E.L.	8.4	77.0
10'E	11.8	
5+58		
10'E	13.5	
3'E	10.8	
E.L.	8.7	76.7
+5	7.0	
+9	6.7	
+10	9.5	
+15	8.1	
+16	5.6	

8538

59

5+58		
+17.5¢	5.0	80.4
+20	5.5	
W.L.	5.3	80.1
5+60		
W.L.	5.4	80.0
+8	5.4	
+15	5.6	
¢	5.1	80.3
+19	8.8	
+25	10.7	
+30	11.5	
E.L.	12.7	72.7
9'E	13.2	
15'E	14.7	
5+62		
15'E	15.1	
11'E	14.7	
7'E	13.4	
4'E	11.8	
E.L.	12.8	72.6
+4	10.6	
+6	6.8	
+10	6.5	
+17.5¢	5.4	80.0
+20	5.7	
+25	5.5	

85.38

5+62

W.L. 5.5 79.9

5+75

W.L. 5.9 79.5

+8 5.8

+15 5.9

+17.5 ~~4~~ 5.3 80.1

+21 6.4

+30 7.5

+31 9.9

+34 10.6

E.L. 12.8 72.6

6'E 13.8

15'E 16.1

6+00

15'E 17.7

7'E 16.0

E.L. 11.8 73.5

+7 7.7

+11 7.9

+15 6.9

+17.5 ~~4~~ 6.8 78.6

+20 6.6

+30 6.6

W.L. 6.5 78.9

60

85.38

6+25

W.L. 7.3 78.1

+2 7.4

+19 7.1

+17.5 ~~4~~ 7.4 78.0

+20 7.8

+23 7.7

+24 8.3

+27 8.3

E.L. 12.9 72.5

6'E 15.7

15'E 17.0

6+50

15'E 17.4

6'E 16.7

E.L. 14.5 70.9

+8 9.5

+13 8.2

+17.5 ~~4~~ 8.1 77.3

+21 7.7

+32 7.9

W.L. 7.8 77.6

6+75	85.38		
w.l.	8.3	77.1	
+10	8.3		
+17.5 $\phi$	8.5	76.9	
+21	8.6		
+27	10.6		
+34	14.8		
E.L.	15.3	70.1	
4'E	17.7		
15'E	18.9		
T.P. 1.00	77.57	8.81	76.57
7+00			
15'E	12.7		
4'E	10.7		
E.L.	8.9	68.7	
+10	2.7		
+15	1.0		
+17.5 $\phi$	1.2	76.4	
+21	1.1		
w.l.	0.1	77.5	
7+25			
w.l.	1.5	76.1	
+13	1.7		
+17.5 $\phi$	1.8	75.8	
+20	1.2		
+23	2.5		
+26	2.5		

7+25	77.57		
E.L.	7.8	69.8	
15'E	11.6		
7+50			
15E	9.2		
13E	8.4		
5E	6.5		
E.L.	5.6	72.0	
+3	4.2		
+9	2.4		
+12	2.5		
+15	1.7		
+16	2.0		
+17.5 $\phi$	2.1	75.5	
+30	2.0		
w.l.	2.0	75.6	
7+75			
w.l.	2.5	75.1	
+17.5 $\phi$	2.7	74.9	
+21	2.3		
+24	3.1		
+30	3.6		
E.L.	3.8	73.8	
11'E	5.5		
15'E	6.9		



77.57

8+00		
15'E	6.2	
E.L.	4.3	73.3
+10	3.6	
+13	3.0	
+15	3.4	
+17.5¢	3.2	74.4
+28	3.0	
w.L.	3.0	74.6
8+25		
w.L.	3.4	74.2
+17.5¢	3.6	74.0
+22	3.9	
+25	3.9	
+29	4.7	
E.L.	6.7	70.9
7'E	8.2	
15'E	11.4	
8+31		
15'E	12.6	
8'E	10.5	
E.L.	8.6	69.0
+2	7.4	
+9	4.5	
+11	3.9	
+13	4.2	

77.57

62

8+31		
+17.5¢	3.7	73.9
+25	3.5	
w.L.	3.6	74.0
8+50		
w.L.	4.0	73.6
+10	4.0	
+17.5¢	4.2	73.4
+22	4.8	
+24	4.8	
+31	5.5	
E.L.	10.8	66.8
9'E	16.3	
15'E	17.4	
20'E	18.3	
8+75		
20'E	18.0	
9'E	16.1	
E.L.	10.4	67.2
+8	5.9	
+11	4.9	
+17.5¢	4.5	73.1
w.L.	4.3	73.3

77.57

$$\begin{array}{r} 10.4 \\ 2.7 \\ \hline 7.7 \end{array} \quad \begin{array}{r} 13 \\ 6.7 \end{array}$$

9+00

w.L. 4.6 73.0

+7 4.7

+16 4.5

+17.5  $\frac{1}{2}$  4.3 73.3

+20 4.2

+23 4.9

+27 5.8

+30 7.3

E.L. 9.4 68.2

15'E 16.6

20'E 17.7

9+30

20E 20.7

5'E 14.4

E.L. 10.4 67.2

+9 5.5

+12 4.9

+17.5  $\frac{1}{2}$  4.0 73.6

+19 3.9

+20 4.7

+25 5.0

w.L. 5.0 72.6

77.57

7.4

63

9+60

w.L. 5.4 72.2

+13 5.1

+14 4.8

+15 4.3

+17.5  $\frac{1}{2}$  4.3 73.3

+20 4.5

+22 5.0

+25 5.2

E.L. 11.2 66.4

5'E 14.0

8'E 14.5

15'E 17.9

20' 19.2

25'E 17.9

9+33.25 = S.L. Votaire on East.

15'E 12.0

9'E 14.8

E.L. 11.2 66.4

+9 5.6

+15 4.7

+17.5  $\frac{1}{2}$  4.6 73.0

+20 5.1

+22 5.4

+30 5.6

w.L. 5.7 71.9

77.56

Sec on S.L. Voltairo (Pluses measured)

W.L. = 10+23 5.8 71.8

+20 5.6

+22 5.5

+23 4.9

+27  $\Phi$  4.8 72.8

+31 5.0

+39 5.7

+43 5.8

+54 = E.L. 11.2 66.4

10+23 (R+Sec)

W.L. 5.8 71.8

+10 5.7

+13 5.0

+17.5 =  $\Phi$  5.4 72.2

+22 6.1

+25 6.2

+28 5.6

+31 5.6

E.L. = Edg Pav. 6.06 71.50

Sec on S edg Pav. Voltairo

W.L. = 10+69.50 6.00 71.56

 $\Phi$  5.85 71.71

E.L. 6.03 71.53

64

9+97.3

77.57

5'E 7.4

E.L. 9.7 67.9

+2 10.2

+3 9.9

+9 6.6

+11 5.5

+17.5  $\Phi$  4.7 72.9

+22 5.5

+39 5.6

W.L. 5.7 71.9

T.P. 12.97 90.27 0.27 77.30

T.P. 3.48 92.22 1.53 88.74

B.M. Beginning 6.60 85.62

NE 1/4 of Section 10  
Tenn 1860

Curb levels Wawona from  
w.l. Chatsworth to Lacresta.

Right = North Left = South

B.M.	5.40	91.03		85.63
T.P.	0.75	82.33	7.45	81.58
T.P.	10.93	92.75	0.51	81.82
w.l. Chatsworth				
Ncb		8.28		84.47
Scb		6.27		86.48
Cent. Curve				
Scb		5.71		87.04
Ncb		6.14		86.61
0+00 = E.C.				
Ncb		3.92		88.83
Scb		4.90		87.85
0+25				
Scb		3.28		89.47
Ncb		2.18		90.57
0+50				
Ncb		0.61		92.14
Scb		1.70		91.05
0+75				
Scb		0.05		92.70
T.P.	13.00	105.18	0.57	92.18
Ncb		11.49		93.69
1+00				
Ncb		9.92		95.26
Scb		10.88		94.30
1+25				

Plotted 9-13-28 C.B.H.  
Distances Part of with filed Map.

Aug 23-28  
Loudon  
#obell - Morgan

1+25	105.18		
Scb	9.11		96.07
Ncb	8.28		96.90
1+40 = <del>41.09</del>			
Ncb	7.35		97.83
Scb	8.18		97.00
1+74 = <del>41.09</del>			
Scb	5.61		99.57
Ncb	5.19		99.99
2+00			
Ncb	3.59		101.59
Scb	4.16		101.02
2+25			
Scb	2.51		102.67
2+35			
Ncb	1.34		103.84
2+50			
Ncb	0.40		104.78
Scb	0.87		104.31
T.P. 12.81	117.73	0.26	104.92
2+75			
Scb	11.75		105.98
Ncb	7.37		110.36
3+00			
Ncb	9.83		107.90
Scb	10.06		107.67

3+25	117.73		
Scb	8.44	109.29	
Ncb	8.21	109.52	
3+50			
Ncb	6.69	111.04	
Scb	6.77	110.96	
3+75			
Scb	5.07	112.66	
Ncb	5.04	112.69	
4+00			
Ncb	3.05	114.68	
Scb	3.17	114.56	
4+25			
Scb	1.03	116.70	
Ncb	0.79	116.94	
4+35 <sup>2</sup> = <del>EL</del> Alley			
Scb	0.12	117.61	
T.P.	12.99	130.48	0.24
4+50			
Ncb	10.99	119.49	
4+56 <sup>2</sup> = <del>W.L.</del> Alley			
Scb	10.78	119.70	
4+75			
Ncb	8.51	121.97	
Scb	7.11	121.37	

5+00	130.48		
Scb	6.77	123.71	
Ncb	6.05	124.43	
5+35 = B.C. N. ret of cb			
Ncb	12.48	128.00	
Scb	3.38	127.10	
5+46 <sup>2</sup> = B.C. S. ret of cb			
Scb	2.74	127.74	
5+56 <sup>2</sup> (on ret.) of cb			
Scb	1.81	128.67	
5+66 <sup>2</sup> (on ret.) of cb			
Scb	0.79	129.69	
5+79 <sup>2</sup> = E.R. - Scb <small>Lacresta on South.</small>	0.06	130.42	
5+42 (or N. ret.) <small>S.gut.</small>	0.74	129.74	
Ncb	1.64	128.84	
5+52 <sup>2</sup> = E.L. Lacresta on North			
Ncb	0.31	130.17	
gut	1.00	129.48	
T.P.	0.46	118.47	12.47
T.P.	0.30	106.21	12.56
T.P.	0.00	93.16	13.05
T.P.	6.91	87.55	12.52
T.P.	12.91	99.66	0.80
<small>op SE Chateworth &amp; Tennyson</small>			
B.M.	3.00	96.66	76.65

10-11-28 X-section Bernice Drive  
 J.C. Bliss  
 Drebert Wabaska to La Cresta. 40' Roadway  
 Rauner 10' 1/45

B. M. Nail in Pale Tennyson & Wabaska 88.10

+3.07

91.17

West Line Wabaska = 0+00

S Tpcb	5.72	85.5
G	6.2	85.0
1/4	6.1	85.1
£	5.8	85.4
1/4	5.9	85.3
G	6.0	85.2
N Tpcb	5.61	85.5

0+25

N Tpcb	5.06	86.1
G	5.5	85.7
1/4	5.4	85.8
£	5.3	85.9
1/4	5.4	85.8
G	5.7	85.5
S Tpcb	5.17	86.0

0+50

S Tpcb	4.49	86.7
G	5.2	86.0
1/4	4.7	86.5
£	4.6	86.6
1/4	4.8	86.4

91.17

67

G	4.7	86.5
N Tpcb	4.37	86.8

0+75

N Tpcb	3.83	87.4
G	4.4	86.8
1/4	4.0	87.2
£	4.0	87.2
1/4	3.9	87.3
G	4.6	86.6
S Tpcb	3.82	87.4

1+00

S Tpcb	3.16	88.0
G	3.7	87.3
1/4	3.2	88.0
£	3.3	87.9
1/4	3.5	87.7
G	3.8	87.4
N Tpcb	3.09	88.1

1+25

N Tpcb	2.47	88.7
G	3.2	88.0
1/4	2.9	88.5
£	2.6	88.6
1/4	2.7	88.5

$\bar{x}$  91.17

G	3.2	88.0	
STpob. in driveway	304	88.2	
	1450		
STpob	183	89.4	
G	26	88.6	
H	22	89.0	
K	22	89.0	
H	23	88.9	
G	26	88.6	
NTpob	187	89.3	
	1475		
NTpob	130	89.9	
G	20	89.2	
H	16	89.6	
K	14	89.8	
H	14	89.8	
G	20	89.2	
STpob	128	89.9	
T.P.		-0.63	90.54

#1168

 $\bar{x}$  102.22

	2400		
STpob	1173	90.5	
G	125	89.7	
H	119	90.8	

 $\bar{x}$  102.22

68

K	11.8	90.4	
H	121	90.1	
G	124	89.8	
NTpob	1170	90.5	
	2425		
NTpob	1101	91.2	
G	116	90.6	
H	115	90.7	
K	112	91.0	
H	113	90.9	
G	118	90.4	
STpob	1118	91.0	
	2450		
STpob	1047	91.7	
G	111	91.1	
H	106	91.6	
K	106	91.6	
H	108	91.4	
G	109	91.3	
NTpob	1038	91.8	
	2475		
NTpob	974	92.5	
G	102	92.0	
H	100	92.2	
K	98	92.4	

$\pi$  102.22

14	9.8	92.4
G	10.3	91.9
STpcb	9.65	92.5
3400		
STpcb	8.80	93.4
G	9.4	92.8
14	9.0	93.2
£	9.0	93.2
14	9.2	93.0
G	9.5	92.7
N Tpcb	9.09	93.1
3425		
N Tpcb	8.10	94.1
G	8.4	93.8
14	8.2	94.0
£	8.0	94.2
14	8.0	94.2
G	8.4	93.8
STpcb	7.80	94.4
3450		
STpcb	6.63	95.6
G	7.1	95.1
14	7.1	95.1
£	7.1	95.1
14	7.2	95.0

 $\pi$  102.22

69

G	7.5	94.7
N Tpcb	7.04	95.2
3475		
N Tpcb	5.80	96.4
G	6.2	96.0
14	6.1	96.1
£	6.0	96.2
14	6.0	96.2
G	6.0	96.2
STpcb	5.41	96.8
4400		
STpcb	4.15	98.1
G	4.9	97.3
14	4.9	97.3
£	4.8	97.4
14	5.0	97.2
G	5.3	97.9
N Tpcb	4.52	97.7
4425		
N Tpcb	3.30	98.9
G	3.8	98.4
14	3.6	98.6
£	3.6	98.6
14	3.5	98.7
G	3.6	98.6
STpcb	2.91	99.3



1.02.22

4150

STpob	1.70	100.5	
G	2.5	99.7	
1/4	2.3	99.9	
2	2.4	99.8	
1/4	2.5	99.7	
G	2.9	99.3	
N Tpob	2.07	100.1	
4175			
N Tpob	0.84	101.4	
G	1.3	100.9	
1/4	1.3	100.9	
2	1.2	101.6	
1/4	1.2	101.0	
G	1.3	100.9	
STpob	0.42	101.4	
T.P.	-0.34	101.88	

+1325

11.5.13

5700

STpob	12.09	103.0
G	13.0	102.1
1/4	12.7	102.2
2	12.8	102.3
1/4	12.9	102.2
G	13.0	102.1

115.13

70

N Tpob	12.47	102.6
5725		
N Tpob	11.25	103.8
G	11.7	103.4
1/4	11.5	103.6
2	11.4	103.7
1/4	11.5	103.6
G	11.7	103.4
STpob	10.88	104.2

5750

STpob	9.51	105.6
G	10.3	104.8
1/4	10.1	105.0
2	10.0	105.1
1/4	10.0	105.1
G	10.3	104.8
N Tpob	10.00	105.1

5775

N Tpob	8.90	106.2
G	9.0	106.1
1/4	8.7	106.4
2	8.6	106.5
1/4	8.7	106.4
G	9.0	106.1
STpob	8.18	106.9

π 115.13

6+00

S Tpcb	6.63	108.5
G	7.3	107.8
1/4	7.2	107.9
♀	7.0	108.1
1/4	7.3	107.8
G	7.4	107.7
NTpcb	7.03	108.1

6+25

NTpcb	5.23	109.9
G	5.7	108.4
1/4	5.3	109.8
♀	5.5	109.6
1/4	5.5	109.6
G	5.5	109.6
STpcb	4.69	110.4

6+50

STpcb	2.74	112.4
G	3.3	111.8
1/4	3.7	114.4
♀	3.5	111.6
1/4	3.4	111.7
G	3.6	111.5
NTpcb	2.95	112.1

π 115.13

71

6+75

NTpcb	0.67	114.4
G	1.1	113.7
1/4	1.1	114.0
♀	1.2	113.9
1/4	1.4	113.7
G	1.2	113.9
STpcb	0.47	114.6

T.P.

- 0.26 114.87

+ 12.43

π 117.30

7+00

STpcb	10.42	116.9
G	11.3	116.0
1/4	11.3	116.0
♀	11.1	116.2
1/4	11.1	116.2
G	11.5	115.8
NTpcb	10.65	116.6

7+25

NTpcb	8.41	118.9
G	9.2	118.1
1/4	9.0	118.3
♀	8.9	118.4
1/4	8.9	118.4
G	8.9	118.4
STpcb	8.22	119.1

T 127.30

7+50

5 Tpcb	6.00	121.3
G	6.8	120.5
1/4	6.8	120.5
♀	6.7	120.6
1/4	7.0	120.3
G	7.1	120.2
1 Tpcb	6.24	121.1

7+75

1 Tpcb	4.00	123.3
G	4.7	122.6
1/4	4.8	122.5
♀	4.5	122.8
1/4	4.6	122.7
G	4.6	122.7
5 Tpcb	3.84	123.5

8+00

5 Tpcb	1.60	125.7
G	2.4	124.9
1/4	2.3	125.0
♀	2.1	125.2
1/4	2.3	125.0
G	2.6	124.8
1 Tpcb	1.67	125.6
T.P	-0.62	126.68

+1231 138.99

T 138.99

72

8+25

NTpcb	11.05	127.9
G	11.9	127.1
1/4	11.6	129.4
♀	11.7	127.6
1/4	11.5	127.5
G	11.5	127.5
5 Tpcb	10.82	128.2

8+50

5 Tpcb	8.39	130.6
G	9.2	129.8
1/4	9.0	130.0
♀	8.7	130.3
1/4	8.8	130.2
G	9.1	129.9
1 Tpcb	8.29	130.7

8+75

1 Tpcb	5.32	133.8
G	6.0	133.0
1/4	5.7	133.3
♀	5.7	133.3
1/4	5.8	133.2
G	6.0	133.0
5 Tpcb	5.15	133.8

138.99

9+00

S Trcb	1.88	137.1
G	2.7	136.3
1/4	2.7	136.3
2	2.5	136.5
1/4	2.5	136.5
G	2.5	136.5
N Trcb	1.69	137.3
T.P.		-0.35 138.64

+1308

151.72

9+43.77 = E.C. S.E. Return Barroca + La Cresta

N Trcb	8.13	143.6
G	8.9	142.8
1/4	8.6	143.1
2	9.0	142.7
1/4	9.4	142.3
G	9.6	142.1
S Trcb	8.95	142.7

9+59 - on S.E. Return

S Trcb	6.86	144.8
G	7.5	144.2
+3.70 = S.C.B. Line	7.4	144.3
1/4	7.3	144.4
2	6.9	144.8
1/4	6.8	144.9

151.72

73

G	7.0	144.9
N Trcb	6.17	145.5

section along parking on La Cresta

9+85<sup>70</sup> on N.C.B. line + 9+75 on S.C.B. line

N Trcb	2.57	149.15
G	3.18	148.54
+1 = N.C.B. line	3.13	148.59
1/4	3.34	148.38
2	3.73	147.99
1/4	4.24	147.48
S.C.B. line	4.81	146.91

+14.5 gutter 5.95 145.77

S Trcb 5.28 145.44

T.P. - 12.71 139.21

+4.65 143.66

B.M. S.E. B.P. Waxona on La Cresta - 12.53 131.13

131.14

10-15-28 X section Wawona Drive - Chatsworth  
 J. A. Bliss  
 Prebart to La Cresta.  
 Mattoon

40' Radway  
 10' 1/45

74  
 T 96.59

B.M. S.W. B.P. Chatsworth + Wawona 86.44

+10.15 T 96.59

Divided curve at Chatsworth into two parts

26.3 ob radius Southside 66.3 Northside

4.53° 19'

W. L. Chatsworth

S Tpcb	1008	86.51
G	10.7	85.9
1/4	11.2	85.4
¢	11.3	85.3
1/4	11.9	84.7
G	12.4	84.2
N Tpcb	12.09	84.50

Section in center of curve

N Tpcb	9.96	86.63
G	10.7	85.9
1/4	10.7	85.9
¢	10.3	86.3
1/4	10.2	86.4
G	10.2	86.4
S Tpcb	9.53	87.06

Section at end of curve = 0+00

E Tpcb	8.72	87.87
G	9.6	87.0
1/4	9.2	87.4

¢	8.8	87.8
1/4	8.6	88.0
G	8.5	88.1
W Tpcb	7.73	88.86

0+25

W Tpcb	6.01	90.58
G	6.9	89.7
1/4	7.0	89.6
¢	7.1	89.5
1/4	7.7	88.9
G	7.6	89.0
E Tpcb	7.11	89.48

0+50

E Tpcb	5.54	91.05
G	6.4	90.2
1/4	5.9	90.7
¢	5.5	91.1
1/4	5.4	91.2
G	5.2	91.4
W Tpcb	4.42	92.17

0+75

W Tpcb	2.90	93.69
G	3.9	92.7
1/4	3.8	92.8
¢	3.8	92.8

$\pi$  96.59

1/4	42	92.4
G	47	91.9
E Tpcb	390	92.69
	1400	
E Tpcb	229	94.30
G	3.2	93.4
1/4	27	93.9
♀	22	94.4
1/4	22	94.4
G	22	94.4
W Tpcb	132	95.27
T.P.		- .01 96.58

+12.84

 $\pi$  109.42

1440 = N.L. Alley

W Tpcb	1158	97.84
G	126	96.8
1/4	124	97.0
♀	123	97.1
1/4	128	96.6
G	132	96.2
E Tpcb	1242	97.00

1474 = S.L. Alley

E Tpcb	9.85	99.57
G	10.6	98.8

 $\pi$  109.42

75

1/4	10.1	99.3
♀	9.9	99.5
1/4	10.1	99.3
G	10.2	99.2
W Tpcb	9.43	99.99
	2400	
W Tpcb	7.83	101.59
G	8.5	100.9
1/4	8.4	101.0
♀	8.2	101.2
1/4	8.5	100.9
G	9.0	100.4
E Tpcb	8.40	101.02

2435

E Tpcb	6.10	103.32
G	6.8	102.6
1/4	6.3	103.1
♀	6.0	103.4
1/4	6.0	103.4
G	6.3	103.1
W Tpcb	5.58	103.84
W Tpcb	3.04	106.38
G	3.7	105.7
1/4	3.5	105.9

π 109.42

♀	33	106.1
1/4	36	105.8
♂	42	105.2
ETpob	345	105.97
	3400	
ETpob	174	107.68
♂	25	106.9
1/4	21	107.3
♀	18	107.6
1/4	20	107.4
♂	22	107.2
WTpob	152	107.90
T.P		- 0.56 108.86

+12.80

π 121.66

	3425	
WTpob	12.15	109.51
♂	12.9	108.7
1/4	12.7	109.0
♀	12.4	108.3
1/4	12.8	108.9
♂	13.3	108.4
ETpob	12.38	109.28

π 121.66

6

	3450	
ETpob	1072	11094
♂	11.6	1100
1/4	11.2	110.4
♀	10.8	110.8
1/4	11.0	110.6
♂	11.3	110.3
WTpob	10.64	111.02
	3475	
WTpob	8.98	112.68
♂	9.5	112.2
1/4	9.2	112.4
♀	9.1	112.5
1/4	9.5	112.2
♂	9.7	111.9
ETpob	9.02	112.64
	4100	
ETpob	7.12	114.54
♂	8.0	113.6
1/4	7.7	113.9
♀	7.2	114.4
1/4	7.3	114.3
♂	8.0	113.6
WTpob	7.00	114.66

π 121.66

4135.5 Center N Alley Return

W T p c b	370	117.96
G	46	117.0
//	42	117.4
♀	40	117.6
//	46	117.0
G	51	116.5
E T p c b	407	117.59

4156.5 = center South Alley Return

E T p c b	199	119.67
G	26	119.0
//	24	119.2
♀	18	119.8
//	20	119.6
G	23	119.3
W T p c b	145	120.21

5100

-0.13 121.53

410.93

π 132.46

5100

W T p c b	80.5	124.41
G	9.0	123.4
//	8.7	123.7
♀	8.6	123.8
//	9.2	123.2

π 132.46

77

G	95	123.0
E T p c b	877	123.69

5+35 = B.C. N.W. Return

E T p c b	541	127.05
G	62	126.2
//	56	126.8
♀	51	127.3
//	48	127.6
G	51	127.3

W T p c b	751	127.95
-----------	-----	--------

5+52.7 = Paving on West side

W T p c b	232	130.14
G	292	129.54
48.5 = W c b	28	129.6
//	3.0	129.4
♀	3.3	129.1
//	3.8	128.6
G	41	128.3
E T p c b	369	128.77

Section along paving from 5+52.7 on West to 5+67.7 on East.

E T p c b	298	130.38
G	271	129.75
43 = E c b line	260	129.86
//	227	130.19



132.46

78

¢	226	130.20
1/4	237	130.09
W ob Line	260	129.86
f. 7 - gutter	292	129.54
W Troob	232	130.14
B. M. N. W. B. P. Wawone & La Cresta	-138	131.08
		131.14



DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 1/2 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body

of table in same row and column gives distance

from side stake to slope stake. If ground is not

the side stake and slope stake, lower stake by this amount if cut, elevation of top stake. Add this amount

to cut or fill and find distance in table. Set up rod at this point and the slope stake should cut

target.

necessary.

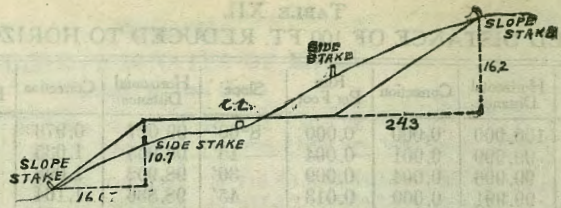
TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given L may be found by dividing tangent (or external) opposite L by given tangent (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

**IMPROVED TABLES  
AND  
INFORMATION**



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING;

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

9248

10222  
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ENGINEERING DEPARTMENT,  
CITY OF SAN DIEGO,  
CALIFORNIA.

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