

1274

DUSTS

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LEVEL BOOK

No. 380 F

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**THE FREDERICK POST CO.**  
*ENGINEERING and DRAFTING SUPPLIES*  
IRVING PARK STATION  
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This subject begins 7/1/76

x sec	Cypress	Vermont East	2
" "	Jewell	Law Manmoth	9
" "	Manmoth	Congress to Colina	24
" "	Collingwood	" " Manmoth	15
" "	Belle Isle Dr	Culv. Profile	62
" "	San. Clemente	Tennyson to Voltaire	30
" "	Wells	" To Bernice	39
" "	Villa Pr. Chatsworth	To Voltaire	53
" "	Alley Blk 62 Park Villas	Pershing 728 Univ to Wightman	63
" "	Alley Block 1 - J.T. Carverans Sub.	- Eads & Fay - Geny to Ruschle	64
" "	Weaver - 60 <sup>th</sup>	to Republic	67







50' wide  
12' elev  
6.5' 195

Cypress St X Sec Vermont East

8-31-28  
Mills

282.58

2

to W. of Line Vermont

B.M. 3.22 288.18 284.96

N.E. Penn.  
& Vermont.

1/4

1.3 2813

T.P. 1.33. 282.58 6.93 281.25

cb

1.2 2814

11' W. of W. Line Vermont = P.C. curb Return on N  
E. End emb. ch. + walk on S.

S

0.7 281.9

10' S. of N. Line = N. ch. 0.54 282.0

10' E. of W. Line

N. gutter 0.88 281.7

Pavment

S

1.3 281.3

1/4 0.70 281.9

cb

1.0 281.6

c 0.62 281.9

1/4

1.6 281.0

1/4 0.71 281.9

c

1.5 281.1

S. gutter 0.84 281.7

1/4

1.3 281.3

12' N. of S. Line = S. ch. 0.52 292.1

cb

1.2 281.4

S. Line. 0.5 282.1

N. gutter

1.25 281.3

Pavmt.

4' W. of W. Line Vermont = E. End Pavmt

N. emb. ch. Ret

0.49 282.1

S 0.6 282.0

W. ch. line

+12 ch 1.15 281.7

Pavment

N

1.15 281.4

Pavmt

1/4 1.11 281.5

cb

1.1 281.5

c 1.04 281.5

1/4

1.5 281.1

1/4 1.02 281.5

c

1.5 281.1

N. ch 1.07 281.5

1/4

1.0 281.6

+1 = gutter 1.07 281.5

cb

2.3 280.3

+1.8 = emb. ch. Ret 0.53 282.1

S

2.7 279.9

W. Line Vermont

+5

2.7 279.9

9.3 S. of N. = emb. ch. ret. 0.50 282.1

gutter 0.9 281.7

cb 1.0 281.6

1/4 1.0 281.6

c 1.2 281.4



282.58

282.58

From this section E Cypress Ave  $\left\{ \begin{array}{l} 50' \text{ wide} \\ 5.67 \text{ curbs} \\ 9.67 \text{ } \frac{1}{4} \text{S} \end{array} \right.$ 

6' E. of W. curb

- 10		7.0	2754	
S		7.1	2755	
d		5.3	2773	
"4		2.5	280.1	
c		1.2	2914	
"4		1.5	2914	
d		1.1	2815	
N		1.02	281.6	Payment
	W. 1/4			
N		0.97	281.6	Payment
cl		1.2	2814	
"4		1.6	2810	
c		2.0	2806	
"4		4.1	278.5	
cl		6.0	276.6	
S.		7.5	275.1	
+ 15		10.5	272.1	
	E Vermont			
- 15		10.7	2719	
S		7.5	275.1	
cl		6.4	276.2	
"4		3.8	2788	
c		2.5	280.1	
"4		1.8	280.8	

d

N

N

cl

"4

c

"4

cl

S

+ 25

+ 35

- 40

- 14

S.

cl

"4

c

"4

cl

N

N

cl

"4

1.1

1.01

E. 1/4

1.38

1.6

2.0

7.6

13.5

13.2

15.4

20.2

20.5

9' E. of E. 1/4

25.8

25.0

22.0

17.0

12.0

5.5

2.2

1.7

1.82

E. cl

2.00

1.6

1.7

281.5

281.6

281.2

281.0

280.6

275.0

269.1

269.4

267.2

262.4

262.1

2568

2576

260.6

265.6

270.6

277.1

280.4

280.9

280.8

2896

281.0

2809

Payment

Payment

Payment

Payment



282.58  
E. ch. (cont)

¢	4.7	277.9
5.14	12.0	2706
dr.	20.0	2626
S.	22.1	2605
+20	28.0	2546
+45	28.3	2543
10' E. of E. ch.		
-1.60	35.7	246.9
-2.8	31.4	251.2
S	19.5	263.1
dr	16.3	266.3
"4	10.9	271.7
C	5.0	277.6
+5	1.4	281.2
"4	1.3	281.3
dr	1.8	280.8
N	2.08	280.5
00 = E Line Vermont		
N	1.52	281.1
gutter	2.11	280.5
dr	1.9	280.7
"4	1.6	281.0
+4.66	1.4	281.2
C	3.8	278.8
"4	9.2	273.4
dr	14.3	269.3

282.58

15' E.

30' E

Parment

S. End amt.  
ch. Return.

Parment

Cypress Ave

4

S	18.0	264.6
+30	33.0	249.6
+60	37.0	245.6
-50	32.0	250.6
-38	31.5	251.1
-20	24.3	258.3
S	13.8	268.8
dr	10.1	272.5
"4	2.9	279.7
C	1.6	281.0
"4	1.5	281.1
dr	1.3	281.3
N	1.4	281.2
N	1.0	281.6
dr	1.2	281.4
"4	1.3	281.3
C	1.8	280.8
"4	2.3	280.3
dr	5.5	277.1
S.	8.5	274.1
+17	18.0	264.6
+35	23.0	259.6



282.58

45' E

-4	3.4	279.2
S	2.5	280.1
cl	2.3	280.3
1/4	2.6	281.0
C	1.3	281.3
1/4	1.2	281.4
cl	0.6	282.0
N.	0.2	282.4

T.P.	6.20	288.25	0.53	282.05
------	------	--------	------	--------

80' E.

N	4.6	283.7
cl	4.9	283.4
1/4	5.3	283.0
C	5.6	282.7
1/4	5.6	282.7
cl	5.4	282.9
S	5.4	282.9

115' E.

S	4.5	283.8
cl	4.5	283.8
1/4	4.5	283.8
C	4.5	283.8
1/4	4.1	284.2
cl	4.0	284.3
N.	3.4	284.9

288.25

Cypress Ave

5

153' U E = P.C. into Cypress Court	2.6	285.7
	3.1	285.7
	3.3	285.0
	3.6	284.7
	4.0	284.3
	4.3	284.0
	4.3	284.0
	3.7	284.6
1792' E = P.C. into Cypress Court		

S	4.3	284.0
cl	4.3	284.0
1/4	3.5	284.8
C	3.2	285.1
1/4	3.1	285.2
cl	2.6	285.7
N	1.8	286.5

236' E = P.C. into Cypress Court

N. on emb walk to House	1.37	286.9
+2	2.3	286.0
cl	2.4	285.9
1/4	2.4	285.5
C	2.8	285.5
1/4	3.2	285.1
cl	3.4	284.5
+3	3.8	284.5
S	2.8	285.5

827  
45'  
115'  
3/5  
N.



288.25  
260'E.

S	3.0	285.3
cl	2.9	285.4
1/4	3.0	285.3
c	2.7	285.6
1/4	2.8	285.5
cl	2.2	286.1
N	1.5	286.8

290'E

N	1.7	286.6
cl	2.3	286.0
1/4	2.7	285.6
c	2.7	285.6
1/4	2.9	285.4
cl	3.0	285.3
S	3.3	285.0

300'E.

-20	15.3	273.0
S	4.9	283.4
cl	3.1	285.2
1/4	2.9	285.4
c	2.7	285.6
1/4	2.7	285.6
cl	2.3	286.0
N	1.7	286.6

288.25  
320'E

N	1.9	286.4
cl	2.6	285.7
1/4	2.8	285.5
c	3.0	285.3
1/4	3.0	285.3
+5	3.1	285.2
cl	6.0	282.3
S	9.0	279.3

+3	14.4	273.9
+11	19.3	269.0
+30	23.6	264.7

335'E

-25	24.3	264.0
-10	19.3	269.0
-3	14.0	274.3
S	10.0	279.3

+6	3.0	285.3
1/4	2.8	285.5
c	3.1	285.2
1/4	2.9	285.4
cl	2.6	285.7
N	2.1	286.2

350'E

N	1.7	286.6
cl	2.5	285.8
1/4	2.8	285.5

Cypress Ave

6

Tree Line

Line Trees



288.25

350' E. (con)

C 3.2 285.1  
 +5 3.1 285.2  
 S. 1/4 4.0 284.3  
 +5 6.6 281.7  
 cl 11.0 277.3  
 S = Line Trees 13.6 274.7  
 +5 14.5 273.8  
 +25 25.0 263.3

383.2

-20 28.0 260.3  
 -4 20.4 267.9  
 S 20.0 268.3  
 cl 17.2 271.1  
 1/4 12.9 275.4  
 +2 = Tree Line 12.7 275.6  
 +3 12.2 276.1  
 cl 8.0 280.3  
 +7 3.6 284.7  
 1/4 2.9 285.4  
 cl 2.6 285.7

44 2.0 286.3  
 387.8 = W. End of wall on N. 0.8 in ST  
 3.95 E.

N 1.7 286.6  
 +1 2.4 285.9  
 cl 2.6 285.7  
 1/4 3.1 285.2

288.25

Cypress Ave

7

1/4 +1 5.4 282.9  
 cl 13.5 274.9  
 +4 = Line Trees 13.8 274.5  
 1/4 16.2 272.1  
 cl 21.0 267.3  
 S 22.5 265.8  
 +5 23.0 265.3

410' E.

-5 23.0 265.3  
 S 23.0 265.3  
 cl 19.8 268.5  
 1/4 14.8 273.5  
 +7 = Line Trees 11.8 276.5  
 cl 11.6 276.7  
 1/4 5.2 283.1  
 +3 3.2 285.1  
 cl 2.8 285.5  
 +5 2.7 285.6  
 N 1.7 286.6

T.P. 1.75 287.17 283 285.42

421' E

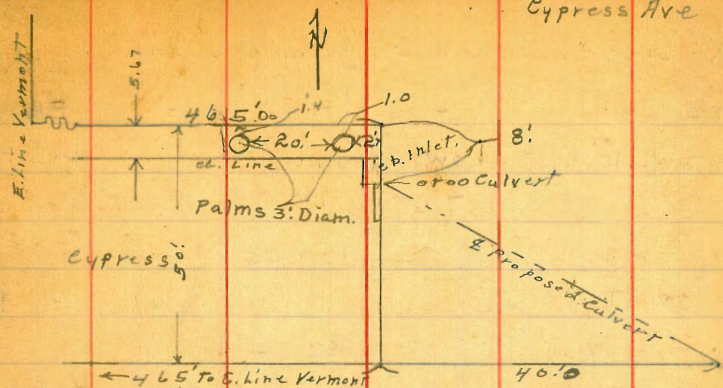
N 0.65 286.6  
 +1 1.7 285.5  
 cl 2.0 285.2  
 +6 2.2 285.0  
 1/4 6.4 282.8



287.17

421'E. Cor

±	10.4	276.8
+2 = Tree Line	10.6	276.6
S. 1/4	15.0	272.2
cb	19.7	267.5
S	23.4	263.8
+5	24.2	263.0
435'E		
-5	26.5	260.7
S	24.5	262.7
cb	20.5	266.7
1/4	13.0	274.2
±	4.8	282.4
+1 = Tree Line	4.4	282.8
1/4	3.7	283.5
cb	2.8	284.4
N.	1.9	295.3
463'E.		
N	3.4	283.8
cb	4.2	283.0
1/4	4.6	282.6
+3 Line Trees.	4.8	282.4



Culvert Levels

H.I. 287.17

0+00	46.5' E. of Vermont	4.4	282.8	fill
0+07	8' S. of N. Line Cypress	4.6	282.6	fill
T.P.	0.70	274.84	13.03	274.14
0+23		4.0	270.8	virgin soil
0+35		6.8	269.0	" "
0+45		11.2	263.6	" "
0+55		14.5	260.3	" "
0+57.8	S. Line Cypress.	18.3	256.5	" "
T.P.	12.85	287.48	0.21	274.63
T.P.	0.66	286.29	1.85	285.63
chk on original E.M.		1.33	284.96	

Cypress Ave

8



X-Section Jewell St. from S.L. Law to

S.L. Monmouth, 80' wide, 20' S.W. 10' Quarter

STA	+ H.I.	-	Elev.
13M. SW. 10' Point	Law & Lomont		142.36
	7.67		
	150.03		
T.P.		13.07	136.96
	5.17	142.13	
T.P.		6.77	135.36
	10.34	145.70 ✓	
T.P.		1.03	144.67 ✓
S.L. Lomont on Jewell			
+10	E.L. Jewel	18.60	
+8		18.90	
E.L.		13.90	131.8
E. Curb		14.60	
E 1/4		15.10	
∅		16.10	129.6
W 1/4		16.70	
W. Curb		17.20	
W.L.		18.60	127.1
+10		19.80	
S. Curb Line Lomont			
+10		20.10	
W.L.		18.70	127.0
W. Curb		17.30	
W. 1/4		16.50	

Plotted 10-3-28-  
C.B.H.

STA	+ H.I.	-	Elev.
∅		10.30	130.4
E 1/4		14.70	
E. Curb		14.20	
E.L.		12.70	133.0
+2		11.80	
+10		11.60	
S 1/4 Lomont			
+10		11.30	
E.L.		11.90	133.8
E. Curb		14.10	
E. 1/4		14.90	
∅		15.60	130.1
W. 1/4		16.30	
W. Curb		17.60	
W.L.		18.90	126.8
+10		19.30	
∅ Lomont			
+10		18.40	
W.L.		18.00	127.7
W. Curb		16.50	
W. 1/4		15.60	
∅		14.80	130.9
E. 1/4		14.30	
E. Curb		13.70	
E. Line		11.70	134.0
+10		10.90	



145.70

Sta	H.I.	elev
N $\frac{1}{4}$ Lomont		
+ 10	10.70	
E.L.	11.60	134.1
+ 2	12.20	
E. Curb	13.30	
E $\frac{1}{4}$	14.90	
☉	14.50	131.2
W $\frac{1}{4}$	15.30	
N Curb	15.70	
W.L.	17.40	128.3
+ 10	17.80	
N. Curb Line Lomont		
+ 10	17.00	
W.L.	16.70	129.0
W. Curb	15.40	
W. $\frac{1}{4}$	15.00	
☉	14.40	131.3
E. $\frac{1}{4}$	13.80	
E. Curb	13.30	
+ 18	11.80	
E.L.	11.00	134.7
+ 10	10.10	
N. Line Lomont		
+ 10	9.40	
E.L.	10.30	135.4

145.70

10

Sta	H.I.	elev
E. Curb	13.00	
E. $\frac{1}{4}$	13.30	132.4
☉	14.00	131.7
W $\frac{1}{4}$	14.40	
W Curb	14.50	
W.L.	14.90	130.8
+ 10	15.20	
0 + 50		
+ 10	10.10	
W.L.	10.70	135.0
W. Curb	11.90	
W. $\frac{1}{4}$	12.10	
+ 5	12.20	
☉	11.40	134.3
E $\frac{1}{4}$	11.00	
E Curb	10.60	
E.L.	9.00	136.7
+ 10	8.10	
1 + 00		
+ 10	5.30	
E.L.	6.20	139.5
E. Curb	7.60	
E. $\frac{1}{4}$	7.80	
☉	8.20	137.5
W $\frac{1}{4}$	8.20	



Sta	+	H.I.	-	elev
		145.70		
			7.60	
			6.40	139.3
			5.50	
1+25 <sup>11</sup>		S. Line Alley		
	+10		3.80	
			4.50	141.2
			5.60	
			6.00	
			5.90	139.8
			5.70	
			5.50	
			4.70	141.0
	+10		3.60	
1+35 <sup>11</sup>		Alley		
	+10		2.80	
			3.70	142.0
			4.70	
			5.00	
			4.80	140.9
			4.70	
			4.60	
			4.00	141.7
	+10		3.20	
1+45 <sup>11</sup>		N. Line Alley		
	+10		2.60	

Sta	+	H.I.	-	elev
		145.70		
			3.20	142.5
			4.00	
			4.30	
			4.30	141.4
			4.20	
			4.20	
			2.60	143.1
			2.00	
			1.00	144.60
2+00				
			12.65	157.32 ✓
			1.07	156.25
	+10		10.0	
	+5'		10.3	
			11.0	146.3
			11.2	
			11.6	
			11.6	145.7
			11.7	
			11.9	
			11.6	145.7
			11.9	
2+50				
	+10		7.2	
			7.3	150.0
			7.5	
			7.4	



157.32

STA	+	H.I.	-	Elev.
☉			7.1	150.2
E 1/4			6.9	
E. Curb			6.6	
E.L.			5.8	151.5
+3'			5.0	
+10'			4.7	
R+69 <sup>2v</sup>		Bottom Concrete Wall		
+10'			1.8	
E.L.			2.2	155.1
E. Curb			3.8	
E 1/4			4.3	
☉			4.8	152.5
W 1/4			5.1	
W. Curb			5.15	
W.L.			5.2	152.1
+10'			5.4	
R+70 <sup>2v</sup>		S.L. Beryl		
+10'		Top	2.0w	
		Bot.	3.3	
W.L.		Top	1.91	155.41
		Bot.	3.1	
W. Curb		Top	1.73	155.59
		Bot.	2.70	
W 1/4		Top	1.53	
		Bot.	2.5	

157.32

12

STA	+	H.I.	-	Elev.
☉			1.35	155.97
			2.2	
E 1/4			1.15	
			2.0	
E. Curb			0.91	156.41
			1.6	
E.L.			0.64	156.68
			1.3	
T.P.	11.42	167.67 ✓	0.78	166.89
R+90 <sup>2v</sup>		S. Curb Beryl		
+10'			9.3	
E.L.			10.6	157.1
E. Curb			11.3	
E 1/4			11.8	
☉			12.2	155.5
W 1/4			12.5	
W. Curb			12.7	
W.L.			12.1	154.6
+10'			12.3	
R+94				
+10'			10.5	
W.L.			10.5	157.2
W. Curb			9.9	
W 1/4			9.6	
☉			9.3	158.4



167.67

167.67

13

STA	+	H.I.	-	Elev.	STA	+	H.I.	-	Elev.
E/4			9.2		3+14				
E.Curb			8.7		+10			5.8	
E.L.			8.4	159.3	E.L.			6.1	161.6
+10'			8.2		E.Curb			7.1	
3+00 <sup>vv</sup>	S/4	Beryl			E/4			7.7	
+10'			6.7		ϕ			8.0	159.7
E.L.			7.2	160.5	W/4			7.9	
E.Curb			7.8		W.Curb			8.1	
E/4			8.2		W.L.			8.8	158.9
ϕ			8.4	159.3	+10'			9.0	
W/4			9.2		3+18				
W.Curb			9.4		+10'			7.8	
W.L.			10.0	157.7	W.L.			7.3	160.4
+10'			10.0		W.Curb			6.7	
3+10 <sup>vv</sup>	ϕ	Beryl			W/4			6.5	
+10'			9.4		ϕ			6.2	161.5
W.L.			9.3	158.4	E/4			5.8	
W.Curb			8.6		E.Curb			5.5	
W/4			8.3		E.L.			5.1	162.7
ϕ			8.2	159.5	+10'			4.6	
E/4			7.8		3+20 <sup>vv</sup>	N/4	Beryl		
E.Curb			7.2		+10'			4.4	
E.L.			6.5	161.2	E.L.			4.8	162.9
+10'			6.1		E.Curb			5.3	
					E/4			5.6	



167.67

14

STA	+	H.I.	-	Elev.	STA	+	H.I.	-	Elev.
☒			5.8	161.9	T.D.	12.39	179.28 ✓	0.90	178.38
W/4			6.1		0 + 50				
W. Curb			6.3		+ 10'			11.0	
W.L.			6.9	169.8	W.L.			11.0	168.3
+ 10'			7.4		W. Curb			10.3	
3 + 30 <sup>vv</sup>	N. Curb	Beryl			W/4			9.9	
+ 10'			4.7		☒			9.2	170.1
W.L.			4.3	163.4	E/4			9.4	
W. Curb			4.3		E. Curb			9.6	
W/4			4.2		E.L.			8.5	170.8
☒			3.6	164.1	+ 10'			8.6	
E/4			3.6		1 + 00				
E. Curb			3.3		+ 10'			4.9	
E.L.			1.7	166.0	E.L.			4.6	174.7
+ 10'			1.7		E. Curb			5.0	
3 + 50 <sup>vv</sup>	N. L.	Beryl =	0 + 00		E/4			5.0	
+ 10'			0.4		☒			5.1	174.2
E.L.			0.5	167.2	W/4			5.0	
E. Curb			0.7		W. Curb			5.9	
E/4			0.4		W.L.			6.2	173.1
☒			0.8	166.9	+ 10'			6.6	
W/4			1.0		1 + 25 <sup>oo</sup>	S. L. Alley			
W. Curb			1.1		+ 10'			2.4	
W.L.			1.3	166.4	E.L.			2.8	176.5
+ 10'			1.4		E. Curb			3.1	



STA	+	H.I.	-	Elev.	STA	+	H.I.	-	Elev.
E 1/4		179.28	3.5			10.72	200.57		
☒			3.2	176.1	BM. End S. Curb Monmouth Drive			13.03	187.54
W 1/4			3.2		T.P.			0.93	199.64
1+35 <sup>00</sup>	☒	Alley				12.75	212.39		
+10'			1.7		T.P.			0.86	211.53
E.L.			1.9	177.4		12.89	224.42		
E. Curb			2.4		T.P.			0.54	223.88
E 1/4			2.5			12.93	236.81		
☒			2.6	176.7	T.P.			0.32	236.49
1+45 <sup>00</sup>		N.L. Alley				10.82	247.31 ✓		
+10'			1.2		X-Section Collingwood Dr. from N.L. Congress Hts. to Monmouth Drive. 50' wide, 10' S.W. 7.5' Quarters,				
E.L.			1.0	178.3	STATIONING on ☒ Collingwood Drive.				
E. Curb			1.0		0+00	N.L. Congress Hts.			
1+24 <sup>15</sup>		S.L. Monmouth Drive			+10'			4.6	
+10'			5.3		E.L.			4.8	242.5
W.W.			4.6	174.7	+2'			6.0	
W. Curb			2.9		E. Curb			6.2	
W 1/4			2.3		E 1/4			6.5	
☒			2.2	177.1	☒			6.9	240.4
E 1/4			1.0		W 1/4			7.4	
E. Curb			0.8		W. Curb			8.0	
1+54 <sup>68</sup>			0.3	179.0	W.W.			8.6	238.7
E.L.			0.0		+10'			9.7	
+10'									
		12.64	191.02						
T.P.			1.17	189.85					

Plotted 10-5-28  
CBH



STA	+	H.I.	-	Elev.
0+50		247.31		
+10'			5.4	
W.L.			5.5	241.8
W. Curb			5.8	
W/4			5.4	
☒			4.7	242.6
E/4			5.0	
E. Curb			5.0	
+7'			5.2	
+8'			3.7	
E.L.			3.9	243.4
+10'			3.5	
1+00				
+10'			2.7	
E.L.			3.1	244.2
+2'			3.3	
+4'			4.2	
E. Curb			4.3	
E/4			4.4	
☒			4.4	242.9
W/4			5.0	
W. Curb			5.0	
W.L.			5.1	242.2
+10'			5.3	

STA	+	H.I.	-	Elev.
1+36 <sup>90</sup>		247.31		
N. W. Malden				
+10'			6.1	
W.L.			6.0	241.3
W. Curb			5.9	
W/4			5.7	
☒			5.8	241.5
E/4			5.6	
E. Curb			5.4	
+5'			5.4	
E.L.			4.6	242.7
+10'			4.0	
1+46 <sup>90</sup>				
N. Curb Malden				
+10'			5.0	
E.L.			5.6	241.7
E. Curb			6.0	
E/4			6.0	
☒			6.3	241.0
W/4			6.3	
W. Curb			6.3	
W.L.			6.5	240.8
+10'			6.5	
1+53 <sup>90</sup>				
N/4 Malden				
+10'			6.8	
W.L.			6.7	240.6
W. Curb			6.7	



247.31

STA	+	H.I.	-	Elev.
W 1/4			6.4	
⊕			6.7	2406
E 1/4			6.6	
E. Curb			6.6	
E. L.			6.2	2411
+10'			5.5	
1+61 <sup>90</sup>	⊕	Malden		
+10'			5.2	
E. L.			6.1	2412
E. Curb			7.2	
E 1/4			7.2	
⊕			7.3	2400
W 1/4			6.9	
W. Curb			7.1	
W. L.			7.1	2402
+10'			7.4	
1+68 <sup>90</sup>	S 1/4	Malden		
+10'			9.0	
W. L.			8.5	2388
W. Curb			8.1	
W 1/4			7.8	
⊕			7.8	239.5
E 1/4			7.9	
E. Curb			7.8	
E. L.			6.6	240.7

247.31

17

STA	+	H.I.	-	Elev.
			6.0	
+10'				
1+76 <sup>90</sup>	S. Curb	Malden		
+10'			6.7	
E. L.			7.4	239.9
+5'			8.3	
E. Curb			8.5	
E 1/4			8.6	
⊕			8.4	238.9
W 1/4			8.6	
W. Curb			9.1	
W. L.			9.3	238.0
+10'			9.7	
1+86 <sup>90</sup>	S. L.	Malden		
+10'			11.5	
W. L.			11.0	236.3
W. Curb			10.4	
W 1/4			10.0	
⊕			9.4	237.9
E 1/4			9.8	
E. Curb			9.6	
+5'			9.6	
+7'			8.5	
E. L.			8.4	238.9
+10'			7.9	



STA	+	H.I.	-	Elev.	STA	+	H.I.	-	Elev.
	T.P.	See pg. 15		236.49 ✓				9.7	
		1.54	238.03 ✓		T.P.			13.24	224.79
2+51 <sup>40</sup>	B.C. Curve to Left. $\Delta = 90^\circ$					5.49	230.28 ✓		
+10'			5.6		3+66 <sup>59</sup>				
E.L.			5.9	2321	+10'			3.6	
+3'			7.6		N.L.			4.8	225.5
E. Curb			7.7		+3'			6.3	
E 1/4			7.6		N. Curb			6.7	
¢			7.8	230.2	N 1/4			6.6	
W 1/4			8.3		¢			7.8	222.5
W. Curb			8.5		S 1/4			8.2	
W.L.			8.8	229.2	S. Curb			9.2	
+10'			9.6		S.L.			10.2	220.1
3+09 <sup>00</sup>					+10'			12.3	
+10'			15.9		4+24 <sup>19</sup>	E.C.			
W.L.			15.6	222.4	+10'			15.8	
W. Curb			14.6		S.L.			13.8	216.4
W 1/4			13.6		S. Curb			12.2	
+5'			13.0		S 1/4			11.0	
¢			12.1	225.9	+2'			10.7	
E 1/4			12.0		¢			9.1	221.2
E. Curb			12.1		N 1/4			9.0	
+4'			12.0		N. Curb			8.7	
+6'			11.0		N.L.			7.7	222.6
E.L.			10.6	227.4	+3'			6.2	



230.28

STA	+	H.I.	-	Elev.
+10			5.1	
4+50				
+10			5.0	
+8'			6.6	
N.L.			8.3	222.0
N.Curb			9.5	
N $\frac{1}{4}$			9.5	
☼			9.6	220.7
S $\frac{1}{4}$			12.1	
S.Curb			13.3	
S.L.			15.0	215.3
+10'			16.5	
T.P.			10.88	219.40
	4.74	224.14 ✓		
5+00				
+10			12.7	
S.L.			10.8	213.3
S.Curb			9.1	
S $\frac{1}{4}$			7.8	
☼			5.3	218.8
N $\frac{1}{4}$			5.3	
N.Curb			5.2	
N.L.			4.2	219.9
+3'			2.1	
+10'			0.7	

224.14

19

STA	+	H.I.	-	Elev.	
5+50					
+10				2.1	
+8'				3.3	
N.L.				5.2	218.9
+2'				6.0	
N.Curb				6.9	
N $\frac{1}{4}$				7.5	
☼				7.9	216.2
+5'				9.9	
S $\frac{1}{4}$				10.5	
S.Curb				12.3	
S.L.				13.9	210.2
+10'				15.7	
6+00					
+10				18.1	
S.L.				15.8	208.3
S.Curb				14.7	
S $\frac{1}{4}$				13.2	
☼				10.1	214.0
N $\frac{1}{4}$				9.7	
N.Curb				9.2	
N.L.				8.1	216.0
+3'				5.9	
+10'				4.4	
T.P.				11.56	212.58



STA	+	H.I.	-	Elev.
	2.93	215.51		
6+50				
N.L. Bottom Ret Well			2.2	213.3
N. Curb			2.5	
N/4			2.6	
☐			2.5	213.0
S/4			6.0	
S. Curb			7.3	
S.L.			8.5	207.0
+10'			10.7	
7+00				
+10'			13.3	
S.L.			11.4	204.1
S. Curb			9.2	
S/4			8.0	
☐			5.1	210.4
N/4			5.1	
N. Curb			4.6	
N.L. Bottom Ret. Wall			3.9	211.6
T.P.			8.76	206.75
	5.21	211.96		
7+46 <sup>09</sup>				
W.L. Colina Jewell			1.40	
+10'				
N.L.			2.2	209.7
N. Curb			3.8	

STA	+	H.I.	-	Elev.
		211.96		
				20
				Elev.
N/4				4.8
☐				6.0
				205.9
S/4				7.2
S. Curb				8.3
S.L.				10.3
				201.6
+14'				13.0
				198.96
HandLevel	0.30	199.26		
N.L. Monmouth Drive,				6.3
				193.0
+20'				9.4
☐	"	"		10.0
				189.3
+17'				11.4
+20'				12.5
S.L.	"	"		14.6
				184.7
+10'				16.0
7+56 <sup>09</sup>				
W. Curb Colina				
+10'				1.6
	Instr.	211.96		
N.L.				2.9
				209.0
+25'				6.6
				206.3
+62' T.P.				13.0
				198.96
HandLevel	0.0	198.96		
+97'				6.0
+130'				9.4
S.L. Monmouth				13.8
				185.1
+10'				15.3



STA	+	H.I.	-	Elev.	STA	+	H.I.	-	Elev.
7+63 <sup>59</sup>	W 1/4 Colina						211.96		
+10'	Instr.	211.96 ✓	1.7		+2'			3.8	
N.L.			3.1	208.8	N.L.			3.8	208.1
+25'			6.7	205.2	+10'			4.7	
+61'	T.P.		13.0	198.96	+25'			7.5	203.5
	Hand Level	0.0	198.96		+58'	T.P.		13.0	198.96
+115'			8.1			Hand Level	0.0	198.96	
S.L. Monmouth			14.0	184.9	+100'			7.0	
+10'			15.4		+127'			10.3	
7+71 <sup>09</sup>	1/4 Colina				S.L. Monmouth			12.8	186.1
+10'	Instr.	211.96 ✓	1.4		+10'			14.0	
+5'			2.4		7+86 <sup>09</sup>	E. Curb Colina			
+3'			3.1		+10'	Instr.	211.96 ✓	2.4	
N.L.			3.3	208.6	+4'			3.1	
+10'			4.0		+2'			4.0	
+25'			7.3	204.6	N.L.			4.2	207.7
+60'	T.P.		13.0	198.96	+15'			5.6	
	Hand Level	0.0	198.96		+54'	T.P.		13.0	198.96
+100'			6.3			Hand Level	0.0	198.96	
+127'			10.0		+93'			5.9	
S.L. Monmouth			13.2	185.7	+100'			7.5	
+10'			14.6		+105'			8.6	
7+78 <sup>59</sup>	E 1/4 Colina				+125'			10.4	
+10'	Instr.	211.96 ✓	2.2		S.L. Monmouth			12.3	186.6
+5'			2.6		+10'			14.0	



STA	+	H.I.	-	Elev.
7+96 <sup>09</sup>	E. L. Colina			
+10'	Instr.	211.96 ✓	3.1	
+3'			4.1	
N.L.			5.3	206.6
+13'			6.2	
+16'			7.5	
+45'	T.P.		13.0	198.96
	HandLevel	0.0	198.96	
+74'			4.0	
+95'			7.3	
+100'			9.0	
+103'			8.7	
+112'			9.3	
+123'			11.0	
S.L. Monmouth			12.7	186.2
+10'			13.1	
8+50	Instr.	211.96 ✓		
	T.P.		10.69	201.27
		3.24	204.51 ✓	
+10'			0.7	
N.L.			2.5	202.0
+1'			3.2	
+4'			2.8	
+15'			3.3	
+20'			5.8	

STA	+	H.I.	-	Elev.
+49'				9.6
+67'	T.P.			13.0
	HandLevel	0.0	191.51	191.51
+72'				0.3
+78'				0.8
+84'				1.2
+87'				2.2
	S.L. Monmouth		5.3	186.2
+10'				6.0
9+00	Instr.	204.51 ✓		
	T.P.		7.02	197.49
		4.25	201.74 ✓	
+10'				1.5
N.L.				2.8
+3'				3.3
+4'				4.4
+8'				4.0
+19'				4.6
+25'				7.0
+46'				10.0
+47'				11.0
+58'				11.5
S.L. Monmouth			15.0	186.7
+10'				16.3



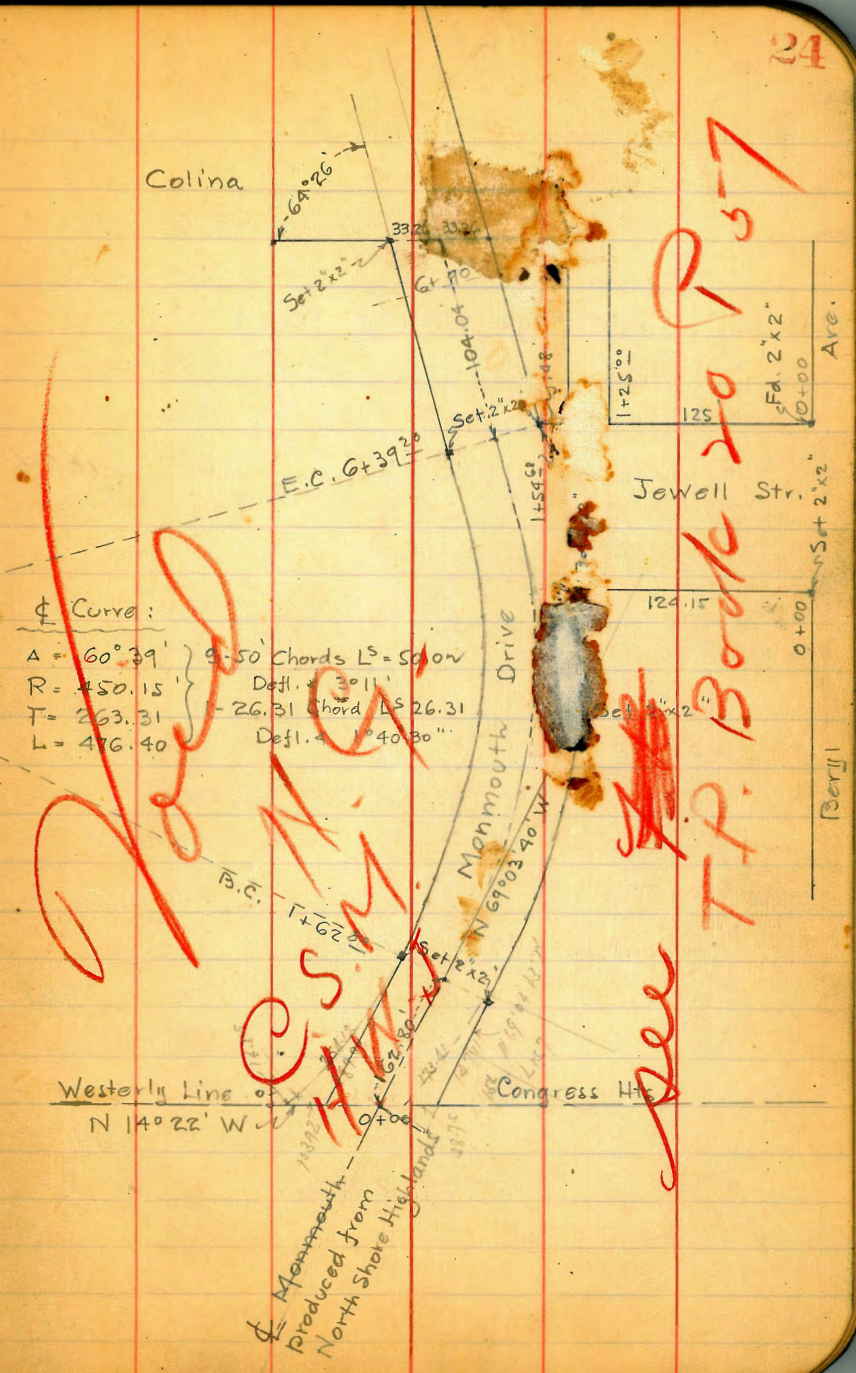




X-Section Monmouth Drive from Westly  
Line Congress Hts to W.L. Colina  
60' wide, 10' S.W. 10' Quarters

STA	+	H.I.	-	Elev	
B.M. End S. Curb		Monmouth Dr.	Sec 9	15	187.59
	8.60	196.14			
0+00		Westly Line Congress Hts.			
+10				13.7	
S.L.				9.0	187.1
S. Curb				8.60	187.54
✓		Both Pavement		9.25	
S/4				9.32	
☐				9.44	187.79
N/4				9.88	
N. Curb				10.37	185.77
✓				9.68	
N.L.				9.90	186.2
+2				9.7	
+3				2.3	
+10				0.5	
0+04		Parallel with Westly Line			
+10				0.8	
N.L.				2.2	193.9
N. Curb				3.4	
+6				3.3	
N/4				9.2	
☐				9.0	187.1
S/4				8.6	

Plotted 10-4-28  
C.B.H.



**CSM**  
Produced from  
North Shore Highlands

**T.P. Bode 20 P 37**  
**Be**



196.14

201.76

STA	+	H.I.	-	Elev.
S. Curb			8.9	87.2
S.L.			9.6	186.5
+10'			13.2	
0+50	Right Angle with $\phi$ Road			
+10'			12.8	
+5'			11.0	
S.L.			10.9	185.2
S. Curb			10.1	
S/4			8.1	
+5'			6.3	
$\phi$			5.9	190.2
N/4			4.6	
+4'			3.8	
+5'			2.5	
N. Curb			1.8	
T.P.			0.0	196.14
Hand Level	10.0	206.14		
N.L.			10.0	196.1
+10'			8.9	
	Instr.	196.14		
T.P.			1.15	194.99
	6.77	201.76		
1+00				
+10'			4.0	
N.L.			6.1	195.7

STA	+	H.I.	-	Elev.
N. Curb			8.3	
+4'			9.0	
+6'			10.3	
N/4			10.5	
+4'			10.7	
+5'			11.9	
$\phi$			12.1	189.7
+6'			12.3	
S/4			14.1	
S. Curb			16.3	
S.L.			18.6	183.2
+10'			20.7	
1+62 <sup>80</sup>	T.P.	B.C.	13.0	181.99
	Hand Level	0.0	181.99	
+10'			8.6	
S.L.			6.6	175.4
S. Curb			4.3	
S/4			2.5	
+3'			0.9	
$\phi$			0.7	181.3
+2'			0.7	
	Inst.	201.76		
+3'			12.1	
N/4			12.0	
+2'			11.8	



STA	+	201.76	-	Elev.	STA	+	201.76	-	Elev.
+3			11.0		+5'			11.9	
N. Curb			9.7		Φ			11.7	1901
N.L.			7.7	194.1	N 1/4			10.2	
+10'			5.7		+2'			9.8	
2+12 <sup>8v</sup>					+5'			8.5	
+10'			4.2		N. Curb			7.6	194.2
N.L.			5.3	196.5	N.L.			6.1	195.7
N. Curb			6.4		+10'			4.1	
+7'			7.7		3+12 <sup>86</sup>				
+8'			9.4		+10'			5.2	
N 1/4			9.6		N.L.			7.1	194.7
Φ			10.7	191.1	N. Curb			9.6	
+2'			12.8		+7'			11.5	
S 1/4 T.P.			13.0	181.99	N 1/4			11.6	
Hand Level	0.0	181.99			Φ			13.2	188.6
+5'			2.0		T.P.			13.0	181.99
S. Curb			3.2		Hand Level	0.0	181.99		
S.L.			5.5	176.5	S 1/4			1.7	
+10'			8.0		S. Curb			3.3	
2+62 <sup>84</sup>					S.L.			5.1	176.9
+10'			5.8		+10'			6.1	
S.L.			4.2	177.8	3+62 <sup>88</sup>				
S. Curb			2.3		+10'			9.8	
S 1/4	Instr.	201.76	13.3		S.L.			8.0	174.0
+2'			13.0		S. Curb			6.0	



STA	+	H.I.	-	Elev.	STA	+	H.I.	-	Elev.
		181.99					190.68		
S 1/4			4.6		4+62 <sup>90</sup>				
¢			3.0	179.0	+10'			18.2	
+3'			2.7		S.L.			16.5	174.2
+6'			1.3		S. Curb			15.2	
N 1/4			1.2		S 1/4			13.4	
N. Curb			0.0		¢			11.8	178.9
	Instr.	201.76 ✓			+6'			10.8	
N.L.			11.6	190.1	+8'			9.7	
+10'			9.8		N 1/4			9.6	
T.P.			12.97	188.79	+9'			9.1	
	1.89	190.68 ✓			N. Curb			8.2	
4+12 <sup>90</sup>					N.L.			6.1	184.6
+10'			1.4		+10'			3.6	
N.L.			2.9	187.8	5+12 <sup>90</sup>				
N. Curb			5.0		+10'			3.1	
+4'			6.0		N.L.			5.5	185.2
+5'			6.9		+9'			7.7	
N 1/4			7.1		N. Curb			8.9	
¢			7.5	183.2	N 1/4			9.5	
S 1/4			9.8		+2'			9.6	
S. Curb			11.2		+6'			11.1	
S.L.			13.0	177.7	¢			11.9	178.8
+10'			14.6		S 1/4			13.8	
					S. Curb			15.6	
					S.L.			16.6	174.1

27  
Elev.



190.68

STA	+	H.I.	-	Elev.
+10			18.5	
S+62 <sup>96</sup>				
+10			16.6	
S.L.			15.9	1748
S.Curb			14.1	
S <sup>1</sup> / <sub>4</sub>			11.9	
ϕ			9.8	1809
+2			9.5	
+6			7.5	
N <sup>1</sup> / <sub>4</sub>			7.3	
+6			7.5	
+7			6.6	
N.Curb			6.0	
N.L.			4.1	186.6
+10			2.1	
T.P.			9.56	181.12
	12.20	193.32 ✓		
G+12 <sup>98</sup>				
+10			3.2	
N.L.			5.3	188.0
N.Curb			7.5	
+1			7.9	
+2			9.2	
N <sup>1</sup> / <sub>4</sub>			9.6	
+2			9.6	

193.32

28

STA	+	H.I.	-	Elev.
+8			12.4	
ϕ			12.7	180.6
S <sup>1</sup> / <sub>4</sub>			13.9	
S.Curb			14.5	
S.L.			15.5	177.8
+10			16.5	
G+39 <sup>20</sup>				E.C
S.L.			14.4	178.9
S.Curb			12.7	
S <sup>1</sup> / <sub>4</sub>			12.0	
ϕ			11.6	181.7
+4			11.0	
+5			9.6	
N <sup>1</sup> / <sub>4</sub>			7.7	
+9			7.4	
N.Curb			5.9	
N.L.			4.1	189.2
+10			2.0	
G+90				
+10			12.2	
S.L.			11.1	182.2
+7			10.1	
S.Curb			9.4	
+2			8.4	
S <sup>1</sup> / <sub>4</sub>			7.9	



193.32

29

STA	+	H.I.	-	Elev.
⊕			7.6	185.7
+5'			7.5	
+6'			6.1	
N <sup>1</sup> / <sub>2</sub>			5.8	
+2'			5.1	
N. Curb			4.8	
+1'			4.7	
+3'			3.8	
N.L.			2.2	191.1
+10'			0.3	
T.P.			11.40	181.92
	1.32	183.24 ✓		
Checked T.P. pg. 14	178.38		4.87	178.37 ✓
T.P.			11.64	171.60
	2.02	173.64		
T.P.			11.44	162.18
	0.09	162.27		
T.P.			13.00	149.27
	2.26	151.53		
B.M. SW. 10' Point Law & Lamont	142.36		9.20	142.33 ✓

STA

+

H.I.

-

Elev.

see Book 1265 p 41 for Colina x sec Notes  
C.B.H.



X Sec. San Clemente St. - Tennyson to  
60' st. - 40' Rdway 10' cbs.

s. ab stake on Tennyson 4+25

B.M. 5.58 133.76

128.13

0+00 = N.L. Tennyson

w.L.	7.1	126.6
cb	7.4	
'4	7.3	
+5	7.4	
⊥	7.8	125.9
'4	7.8	
cb	8.0	
E.L.	8.3	125.4
0+05		
E.L.	6.8	127.0
+5	5.7	
cb	4.7	
'4	4.3	
+2	4.5	
+8	3.7	
⊥	4.0	129.7
+5	4.4	
'4	4.5	
+6	4.1	
cb	4.1	
w.L.	3.7	130.0

C.B.H.

Plotted 11-23-28

Voltaire

Oct 8-28

Leiden

Isbell

Morgan

133.76

0+25

0+

w.L.	3.2	130.5
cb	2.8	
+3	2.7	
+8	2.8	
'4	2.4	
⊥	1.4	132.3
+5	1.3	
'4	1.5	
+6	1.2	
cb	1.4	
+5	2.2	
E.L.	3.3	130.4
0+35		
E.L.	4.2	129.5
+2	3.3	
+5	3.4	
cb	2.7	
'4	2.1	
+8	1.8	
⊥	2.1	131.6
+5	2.3	
'4	2.7	
+7	3.1	
cb	2.9	
+5	2.7	



## San Clemente

0+35	133.76		
wL	2.4	131.3	
0+40			
wL	3.5	131.2	
+3	4.0		
+8	4.0		
cb	4.4		
+3	5.4		
+5	5.0		
1/4	3.8		
+5	4.1		
±	3.7	130.0	
1/4	3.6		
cb	3.8		
+2	7.9		
+6	8.6		
EL	9.2	124.5	
0+49			
EL	12.2	121.5	
cb	10.3		
+2	8.9		
+5	8.8		
+6	10.3		
1/4	9.9		
+1	6.5		
+6	7.0		
+8	7.6		

## San Clemente

31

0+49	133.76		
±	7.0	125.7	
+5	7.8		
1/4	7.5		
+5	8.5		
cb	7.8		
+6	8.3		
+8	10.3		
wL	10.0	123.7	
0+59			
wL	9.9	123.8	
+6	10.2		
cb	10.0		
1/4	9.9		
+5	9.9		
±	10.3	123.4	
1/4	11.0		
+7	11.3		
cb	11.8		
+3	12.4		
EL	12.6	121.1	



0 + 80	133.76		
EL		14.8	1190
+5		14.6	
cb		14.3	
1/4		13.4	
±		13.3	1204
+6		12.9	
1/4		12.9	
cb		12.6	
w.L.		12.3	121.4
T.P.	0.60	122.81	11.55
			122.21
1 + 00			
w.L.		3.0	1198
cb		3.3	
1/4		3.7	
+3		3.9	
+8		3.9	
±		4.1	118.7
+3		4.6	
1/4		4.7	
+3		4.8	
+6		4.5	
cb		4.7	
E.L.		5.2	117.6

San Clemente

32

1 + 20	122.81		
EL		6.8	1160
cb		6.4	
1/4		6.1	
+9		5.7	
±		6.1	116.7
+7		6.2	
1/4		5.8	
+5		5.3	
cb		5.1	
w.L.		4.9	117.9
1 + 40			
w.L.		6.7	116.1
+6		6.8	
cb		7.0	
+6		7.2	
+9		7.7	
1/4		7.5	
±		7.6	115.2
1/4		7.8	
cb		8.2	
EL		8.6	114.2
Floor	at 1 + 47 on East (conc) Garage.	8.63	114.18



1+70	122.81		
E.L	10.4	112.4	
+5	10.7		
cb	10.5		
+4	10.5		
'4	10.1		
±	9.9	112.9	
+3	9.8		
+6	10.0		
+9	9.8		
'4	10.0		
+1	10.2		
+4	9.5		
cb	9.3		
W.L.	8.9	113.9	
2+00			
W.L.	11.2	111.1	
cb	11.8		
+4	11.9		
+9	12.5		
'4	12.2		
+1	12.0		
+4	12.5		
+6	12.1		
±	12.1	110.7	

33

2+00	122.81			
'4			12.7	
+7			12.9	
cb			13.3	
+2			13.0	
E.L			12.9	109.9
T.P. 0.31	110.17	12.95	109.86	
2+25				
E.L			2.5	107.7
+4			2.2	
cb			2.4	
'4			1.8	
±			1.6	108.6
+4			1.5	
+7			2.0	
'4			1.7	
+1			2.0	
+4			1.4	
cb			1.2	
W.L.			0.8	109.3



2 + 50	110.17		
w.L.	3.0	107.2	
+5	3.1		
cb	3.0		
+4	3.1		
+6	3.8		
+9	3.5		
1/4	3.7		
+2	3.0		
+4	3.4		
⊕	3.6	106.6	
1/4	3.9		
cb	4.1		
EL	4.4	105.8	
2 + 70 = S.L. Udal on West			
EL	6.0	104.2	
cb	5.7		
1/4	5.3		
⊕	5.2	105.0	
+5	5.0		
+9	5.2		
1/4	5.4		
+3	5.1		
+7	5.3		
+9	4.9		
cb	4.8		

2 + 70	110.17		
w.L.	4.4	105.8	
3 + 00 = ⊕ Udal			
w.L.	7.1	103.1	
cb	7.2		
+3	7.1		
+6	7.5		
1/4	7.4		
⊕	7.4	102.8	
1/4	7.8		
cb	8.1		
+5	7.9		
EL	8.3	101.9	
3 + 30 = N.L. = Udal on West			
EL	11.3	98.9	
cb	10.9		
1/4	10.3		
⊕	10.1	100.1	
+6	9.7		
1/4	10.0		
cb	10.3		
+4	10.4		
+7	9.7		
w.L.	9.5	100.7	



	110.17		
3+40 = 3L	Vdal 09	East	
w.L.	10.4	99.8	
+3	10.6		
+6	11.2		
cb	11.5		
+4	11.1		
+6	11.7		
+8	10.8		
1/4	10.7		
+5	10.8		
±	11.0	99.2	
1/4	11.5		
cb	12.0		
E.L.	12.6	97.6	
Hub ss. Vdal 2 Sanolamento			
B.M.	12.59	97.58	↑
B.M.	0.07	97.74	97.67
3+50			
E.L.	2.2	95.5	
cb	1.3		
1/4	0.5		
+2	0.0		
1/4	+0.2		
+3	+0.3		
+5	0.6		
+7	0.7		
+8	0.0		

3+50	97.74	
cb	0.4	
+3	0.1	
+5	+0.1	
+9	+0.9	
w.L.	+0.9	98.6
3+65		
w.L.	1.4	96.3
+2	1.5	
cb	2.4	
+2	2.4	
+5	2.7	
1/4	2.3	
+5	2.3	
±	2.6	95.1
1/4	4.0	
+5	4.8	
cb	5.5	
+5	6.3	
E.L.	6.6	91.1



3+90	97.74		
E.L.	9.0	88.7	
+2	8.7		
+7	8.5		
cb	8.6		
1/4	7.9		
⊕	6.9	90.8	
+6	6.9		
1/4	5.8		
+8	5.7		
cb	5.9		
+3	5.6		
+6	5.8		
+9	5.3		
w.L.	5.1	92.6	
4+10 = N.L. Udal on East			
w.L.	7.0	90.7	
+4	7.8		
+7	7.6		
cb	8.0		
+2	7.7		
+8	7.8		
1/4	8.4		
+6	9.3		
⊕	9.4	88.3	
+6	9.6		

4+10	97.74		
1/4	9.1		
+5	9.5		
cb	9.8		
E.L.	10.4	87.3	
4+35			
E.L.	11.6	86.1	
+2	11.8		
+5	12.2		
cb	12.3		
+5	12.2		
+7	11.6		
1/4	11.6		
+5	11.7		
+8	11.9		
⊕	11.8	85.9	
+5	11.6		
1/4	10.8		
+7	10.3		
+8	10.3		
cb	10.1		
+6	10.0		
+8	9.4		
w.L.	9.2	88.5	
garage on w.L. at 4+57	11.8	85.9	



H+62 <sup>5</sup> = s.l. Alley on west.		97.74	
w.l.		12.3	85.4
+6		12.8	
cb		12.8	
1/4		13.1	
+7		13.7	
⊕		13.8	83.9
T.P.	0.33	85.24	12.83
1/4		1.7	84.91
+3		2.0	
+6		2.6	
+9		2.7	
cb		2.5	
+6		2.5	
E.L.		2.2	83.0
H+77 <sup>5</sup>			
E.L.		4.1	81.1
+6		4.3	
cb		4.1	
+6		3.8	
1/4		3.2	
+3		2.9	
⊕		3.0	82.2
+5		2.9	
+8		2.5	
1/4		2.5	

H+77 <sup>5</sup>		85.24	
cb.		2.4	
+6		2.0	
w.l.		1.6	83.6
1/4 # 87	(north floor)	2.1	
double garage 1 <sup>5</sup> W.			
5+00			
w.l.		2.9	82.3
+1		2.9	
+3		3.3	
cb		3.8	
1/4		4.2	
+4		4.5	
+7		5.3	
⊕		5.5	79.7
+2		5.8	
+5		5.7	
1/4		5.7	
+5		5.8	
cb		6.2	
+6		6.2	
+9		5.4	
E.L.		5.4	79.8



5+25		85.24	
EL	7.8	77.4	
cb	7.8		
+2	7.5		
1/4	7.3		
+6	7.1		
⊕	7.1	78.1	
1/4	6.2		
+6	5.8		
cb	5.7		
+6	5.2		
w.L.	4.8	80.4	
5+50			
w.L.	6.1	79.1	
+1	6.6		
+3	6.7		
+6	7.3		
cb	7.4		
1/4	7.7		
+5	8.0		
⊕	8.4	76.8	
+3	8.4		
1/4	8.8		
+4	9.3		
cb	9.3		
EL	9.4	75.8	

5+75		85.24	
EL	11.2	74.0	
cb	11.2		
+2	11.6		
+5	10.6		
+8	10.1		
1/4	10.0		
+5	10.0		
⊕	9.9	75.3	
+4	9.5		
1/4	9.3		
+6	9.1		
cb	9.0		
+5	8.7		
+8	8.0		
w.L.	7.8	77.4	
6+00			
w.L.	9.3	75.9	
+3	10.0		
cb	10.7		
+4	11.1		
+6	11.8		
1/4	12.0		
+8	12.0		
⊕	12.0	73.2	
1/4	12.2		



San Clemente

6+00	25.24	
cb	12.3	
+3	12.5	
+5	12.3	
E.L	12.2	73.0
6+10 = SL	Voltaire	
E.L	12.8	72.4
cb	12.9	
1/4	12.9	
+	12.9	72.3
+8	13.0	
1/4	13.2	
+3	13.3	
cb	12.9	
wL	13.3	71.9

X Sec Wells - Tennyson to Bernice Dr.  
 60' St 40' Rdway 10' cbs

B.M. 12 20	119.31	107.11
0+00 = SL	Tennyson	
E.L		14.6
cb		14.6
1/4		13.5
+		13.2
1/4		12.9
+4		12.7
cb		12.6
+5		12.4
+7		11.9
wL		11.8
0+25		
wL		10.2
+3		10.9
+7		11.0
cb		11.5
+1		11.8
+3		11.6
+5		11.8
1/4		11.7
+		11.8
1/4		12.6
cb		13.2
+1		13.2

Plotted 11-24-28 C.B.H.

39  
 Oct 3-28  
 Loudon  
 Isbell  
 Morgan  
 FH SE.  
 Wells & Tenny.



Wells

0+25	119.31		
+2	13.0		
+5	13.3		
EL	12.9	106.4	
0+50			
EL	11.2	108.1	
+3	11.5		
+5	11.3		
+7	11.3		
+8	11.7		
cb	11.7		
1/4	11.0		
+	10.4	108.9	
1/4	10.3		
+5	10.3		
+6	10.7		
cb	10.3		
+1	9.6		
+3	9.2		
w.L	8.8	110.5	

Wells

0+75	119.31		
w.L	7.2	112.1	
+6	7.6		
+9	8.2		
cb	8.9		
+3	9.2		
+4	8.8		
1/4	8.8		
+	8.9	110.4	
1/4	9.5		
cb	10.0		
+1	10.3		
+2	10.3		
+4	9.5		
EL	9.4	109.9	
1+00			
EL	7.9	111.4	
+6	7.9		
+8	9.0		
+9	9.1		
cb	8.5		
1/4	7.8		
+	7.3	112.0	
+4	7.1		
1/4	2.2		
+8	7.3		



## Wells

1400	11931		
+8 <sup>5</sup>	8.0		
eb	8.0		
+1	7.7		
+3	6.1		
w.L	5.6	113.7	
1+30 = N L Alley			
w.L	3.3	116.0	
+2	3.6		
+6	4.1		
+8	4.7		
+9	5.9		
eb	5.9		
+1	5.9		
+1 <sup>5</sup>	5.3		
1/4	5.1		
1/2	5.1	114.2	
1/4	5.7		
eb	6.4		
+10 <sup>5</sup>	6.5		
+1	7.2		
+2	7.4		
+2 <sup>5</sup>	6.4		
+4	6.1		
+8	6.1		
E.L	5.9	113.4	

## Wells

11

11931			
1+45 = S.L. Alley			
E.L	5.1	114.2	
+2	5.2		
+6 <sup>5</sup>	4.9		
+7	5.2		
+9	5.3		
+9 <sup>5</sup>	6.3		
eb	6.5		
+10 <sup>5</sup>	5.4		
1/4	4.5		
1/2	4.0	115.3	
1/4	4.0		
+9	4.2		
+9 <sup>5</sup>	4.7		
eb	4.6		
+2	3.3		
+5	2.8		
w.L	2.2	117.1	
1+75			
w.L	0.2	119.1	
+1	0.6		
+6	1.1		
+8	2.6		
eb	2.9		
+10 <sup>5</sup>	2.8		
+1	2.2		



Wells

1+75	119.31	
<del>1/4</del>	1.8	
1/4	1.7	
¢	1.9	117.4
+3	2.0	
1/4	2.4	
cb	3.0	
cb	3.8	
+1	3.7	
+1 <sup>5</sup>	3.1	
+3	2.6	
EL	2.8	116.5
2+00		
EL	1.0	118.3
+3	1.2	
+3 <sup>5</sup>	1.5	
+4 <sup>5</sup>	1.2	
+7 <sup>5</sup>	0.9	
+8 <sup>5</sup>	1.2	
+9	2.0	
cb	1.1	
+1	1.4	
+4	1.0	
1/4	0.6	
¢	0.1	119.2
1/4	+0.1	

Wells

42

2+00	119.31	
cb	0.2	
+1	1.1	
+2 <sup>5</sup>	1.2	
T.P. 12.69	131.96	0.04
+3 <sup>5</sup>	11.8	119.27
+7 <sup>5</sup>	11.5	
+8 <sup>5</sup>	11.7	
w.L.	11.3	120.6
2+25		
w.L.	9.7	122.2
+1	9.9	
+4	9.9	
+6	10.4	
+6	12.0	
+8	11.7	
+8 <sup>5</sup>	11.1	
cb	11.1	
1/4	10.9	
¢	11.1	120.9
1/4	11.5	
cb	12.0	
+1	12.8	
+3	11.7	
EL	11.5	120.4



## Wells

	131.96		
E.L	10.0	121.9	
+3	10.2		
+7	9.9		
cb	16.5		
+0 <sup>S</sup>	10.4		
+1	10.9		
+7	10.3		
1/4	9.8		
+7	9.4		
⊕	9.4	122.5	
1/4	9.2		
+6	9.2		
+6 <sup>S</sup>	9.7		
+9	9.8		
cb	9.4		
+2	9.4		
+6	8.7		
+7	9.2		
W.L.	8.1	123.8	

## Wells

43

	131.96		
2 + 75 <sup>2</sup> = NL Alicia Dr			
W.L	6.5	125.4	
+2	7.5		
cb	8.5		
+1	7.8		
+3	7.6		
+4	8.0		
1/4	7.6		
⊕	7.7	124.2	
+4	7.7		
1/4	8.1		
+8	8.6		
cb	8.4		
+3	8.2		
E.L	8.2	123.7	
2 + 85 <sup>2</sup> = Ncb Alicia			
3'E top cb	7.98	123.98	
E.L	8.3	123.6	
cb	7.8		
1/4	7.5		
+7	7.0		
⊕	7.0	124.9	
1/4	6.9		
+3	6.9		
+3 <sup>S</sup>	8.0		
+5	7.9		



## Wells

$2 + 85^2$	131.96		
+5 <sup>5</sup>		7.0	
+8		6.7	
cb		6.5	
+1		6.8	
wL		6.6	125.3
$2 + 95^2 = N \frac{1}{4}$ Alicia			
wL		5.9	126.0
+4		6.3	
cb		5.9	
+1		6.2	
+2		6.4	
+2 <sup>5</sup>		7.0	
+4		6.7	
+6		6.2	
$\frac{1}{4}$		6.2	
$\frac{1}{4}$		6.4	125.5
$\frac{1}{4}$		6.7	
cb		7.2	
E.L.		7.9	124.0
$3 + 05^2 = \frac{1}{4}$ Alicia			
EL		7.3	124.6
cb		6.7	
$\frac{1}{4}$		6.1	
$\frac{1}{4}$		5.7	126.2
+6		5.6	

## Wells

44

$3 + 05^2 =$	131.96		
$\frac{1}{4}$		5.6	
+3		5.8	
cb		5.6	
+3		5.2	
+6		5.3	
+8		5.5	
wL		5.2	126.7
$3 + 15^2 = S \frac{1}{4}$ Alicia			
wL		4.7	127.2
+3		5.0	
+6		4.6	
+8		4.7	
cb		5.4	
+2		5.4	
+3		5.0	
$\frac{1}{4}$		5.1	
$\frac{1}{4}$		5.2	126.7
$\frac{1}{4}$		5.4	
cb		6.0	
EL		6.9	125.0



Wells

131.96

3+25<sup>7</sup> = 5cb Alicia

2.5' E top cb	6.00	125.96
EL	6.4	125.5
+6	6.1	
cb	5.5	
+5	5.0	
1/4	4.8	
+5	4.6	
⊕	4.6	127.3
+7	4.3	
1/4	4.3	
+7	4.3	
+8	4.9	
cb	4.6	
+2	4.4	
+8	4.2	
WL	4.3	127.6
3+35 <sup>2</sup> = 5L Alicia		
WL	2.4	129.5
+3	2.7	
+4	2.5	
+5	2.6	
+7	3.7	
cb	4.2	
+1	4.2	
+3	3.8	

Wells

15

131.96

3+35<sup>2</sup>

1/4	3.7	
⊕	3.9	128.0
+5	4.0	
1/4	4.3	
cb	5.0	
+3	5.6	
+5	5.7	
+6	5.3	
EL	5.4	126.5
3+50		
EL	4.3	127.6
+6	4.3	
+7	5.1	
+8	4.9	
cb	4.1	
1/4	3.4	
+8	3.0	
⊕	3.1	128.8
1/4	2.8	
+5	2.8	
+6	3.2	
cb	3.0	
+2	2.7	
+4	1.8	
+7	1.9	
WL	1.2	130.7



## Wells

3+75	131.96	
T.P. 13.04	143.94	1.06 130.90
w.L		11.3 132.6
+1		11.9
+7		12.2
+9		12.9
cb		13.0
+15		12.8
+25		13.1
+5		13.3
+7		13.0
1/4		13.1
+		13.2 130.7
1/4		13.8
+9		14.4
cb		14.6
+10 <sup>5</sup>		15.0
+15		15.1
+4		14.2
E.L.		14.3 129.6
4+00		
E.L.		12.3 131.6
+7		12.3
+8		13.7
cb		12.6
+2		12.4

## Wells

46

4+00	143.94	
1/4		12.0
+7		11.6
+		11.5 132.4
1/4		11.3
+15		11.5
+25		12.2
+5		12.2
+7		11.3
+8 <sup>5</sup>		10.9
cb		11.0
+1		11.0
+3		10.2
+6		10.3
+7		10.0
w.L		9.4 134.5
4+25		
w.L		7.3 136.6
+1		7.7
+6		8.0
+9		8.9
cb		8.9
+15		9.4
+2		10.5
+3		10.6
+4		9.3



## Wells

4425	143.94	
1/4	9.3	
+	9.4	134.5
+2	9.3	
1/4	9.8	
+6	10.2	
+8	10.1	
cb	10.5	
+1	11.6	
+2	10.6	
+3	10.0	
EL	10.1	133.8
4450		
EL	7.7	136.2
+7	7.6	
+9	8.5	
cb	8.0	
+1	7.8	
1/4	7.5	
+3	7.4	
+8	7.1	
+	7.1	136.8
1/4	7.2	
+6	7.2	
+6	7.7	
cb	7.2	
+1	7.3	

## Wells

17

4450	143.94	
+3	6.4	
+8	5.6	
w.L.	4.8	139.1
4465 = NL Alley		
w.L.	3.8	140.1
cb	5.6	
+4	6.0	
+7	5.7	
1/4	5.8	
+	5.7	138.2
+2	5.7	
1/4	6.2	
+7	6.6	
cb	6.7	
+2	6.7	
+3	6.3	
EL	6.3	137.6
4480 = SL Alley		
EL	4.9	139.0
+7	5.1	
+8	5.3	
cb	5.2	
+4	5.2	
1/4	4.8	
+7	4.4	



## Wells.

H+80	143.94		
⊕		4.3	139.6
1/4		4.3	
+3		4.4	
+6		4.8	
+7		5.3	
+9		5.2	
cb		4.6	
+3		3.5	
+6		3.3	
W.L.		2.6	141.3
5+00			
W.L.		0.1	143.8
+2		1.1	
+7		1.7	
cb		2.5	
+15		2.4	
+2		3.2	
+5		3.2	
+55		2.6	
1/4		2.5	
⊕		2.5	141.4
1/4		3.0	
+6		3.5	
cb		3.5	
+3		3.4	
E.L.		3.3	140.6

## Wells

18

5+25	143.94		
T.P.	12.52	155.85	0.61
E.L.			143.33
+8			13.1
+9			142.7
cb			13.0
+5			13.2
1/4			13.2
⊕			13.1
+9			12.9
1/4			12.3
+3			143.5
+5			12.4
+7			12.8
+9			12.8
cb			12.3
+1			12.0
+8			12.4
W.L.			12.1
5+50			11.1
W.L.			10.4
+3			8.7
+8			147.1
cb			6.7
1/4			149.1
⊕			8.4
			8.6
			9.6
			10.0
			10.2
			145.7



## Wells

5450	155.85		
1/4	10.9		
+6	11.2		
cb	11.2		
+4	11.1		
+7	11.2		
EL	10.8	145.0	
5475			
EL	9.2	146.6	
+8	8.9		
cb	9.0		
1/4	8.5		
±	8.0	147.8	
1/4	7.7		
+2	7.7		
+3	8.0		
+6	7.7		
cb	7.8		
+1	7.6		
+3	6.4		
+8	6.1		
W.L.	4.7	151.1	

## Wells

49

	155.85		
6+10 <sup>3</sup> = NL	Atascadero		
W.L.	3.1	152.7	
+2	3.1		
+6	3.7		
cb	5.3		
+4	5.3		
+5	5.0		
1/4	5.1		
±	5.0	150.8	
1/4	5.5		
+8	5.9		
cb	5.7		
+6	5.7		
EL	5.4	150.4	
6+20 <sup>3</sup> = Ncb	Atascadero		
EL top cb	5.2	150.6	
EL qcd.	5.6		
cb	5.2		
1/4	4.6		
±	4.3	151.5	
+5	4.2		
1/4	4.4		
cb	4.3		
+2	3.6		
W.L.	2.5	153.3	



## Wells

15585

6+30<sup>3</sup> = N<sup>1</sup>/<sub>4</sub> Atascadero

w.L.	2.3	153.5
+7	3.0	
cb	2.0	
1/4	3.3	
±	3.6	152.2
1/4	3.9	
cb	4.1	
EL	4.7	151.1
6+40 <sup>3</sup> = ± Atascadero		
EL	4.4	151.4
cb	3.8	
1/4	3.3	
±	2.9	152.9
1/4	2.7	
cb	2.5	
w.L.	2.1	153.7
6+50 <sup>3</sup> = S <sup>1</sup> / <sub>4</sub> Atascadero		
w.L.	1.5	154.3
cb	1.8	
1/4	2.0	
±	2.2	153.6
1/4	2.6	
cb	3.2	
EL	4.0	151.8

## Wells

15585

6+60<sup>3</sup> = S<sup>1</sup>/<sub>4</sub> Atascadero

EL top	2.76	153.09
EL gut	3.5	
+3	3.0	
cb	2.9	
1/4	2.2	
±	1.7	154.1
1/4	1.6	
+7	1.6	
cb	1.3	
+4	0.7	
+7	1.2	
w.L.	1.0	154.7
(SE. return in)		
cb & walks in 0+00 to 3+75		
6+70 <sup>3</sup> = 0+00 = S.L. Atascadero,		
w.L.	0.1	
cb top cb	0.21	155.64
gut	0.8	155.05
+7	1.0	
1/4	0.9	
±	1.1	154.7
1/4	1.5	
+8	2.3	
gut	2.3	153.58
Ecb	1.78	154.07
T.P. 12-89 16860	0.14	155.71

50



Wells

0+25	168.60	
Ecb	11.90	156.70
gut	12.9	
1/4	12.0	
⊕	11.5	157.1
1/4	11.4	
gut	11.8	
wcb	10.74	157.86
0+50		
wcb	8.54	160.06
gut	9.4	
1/4	9.1	
⊕	9.1	159.5
1/4	9.5	
gut	10.2	
Ecb	9.37	159.23
0+75		
Ecb	6.86	161.74
gut	7.7	
1/4	7.0	
⊕	6.7	161.9
1/4	6.7	
gut	7.2	
wcb	6.31	162.29

Wells

51

1+00	168.60	
wcb	4.12	168.48
gut	4.8	
1/4	4.5	
⊕	4.3	164.3
1/4	4.6	
gut	5.2	
Ecb	4.37	164.21
1+30 = A.L. Alley		
E.L. top cb	1.32	
Ecb	1.69	166.91
gut	2.4	
1/4	2.0	
⊕	1.9	166.7
1/4	2.0	
gut	2.5	
wcb	1.68	166.92
w.L. top cb	1.32	
1+45 = B.C.		
w.L. top cb	0.30	
wcb	0.47	168.13
gut	1.3	
1/4	1.1	
⊕	0.7	167.7
1/4	1.0	
gut	1.2	
Ecb	0.47	168.13



1445	168.60		
EL Feb cb	0.31		
T.P. 6.06	174.35	0.31	168.29
1475			
Ecb	4.86		169.49
gut	5.8		
1/4	5.4		
±	5.2		169.1
1/4	5.5		
gut	5.9		
web	5.06		169.29
2400			
web	4.90		169.65
gut	5.5		
1/4	5.0		
±	4.8		169.5
1/4	4.9		
gut	5.2		
Ecb	4.33		170.02
2425			
Ecb	4.43		169.92
gut	5.3		
1/4	5.0		
±	4.9		169.4
1/4	5.3		
gut	6.0		
web	4.96		169.39

2450	174.35		
web	5.93		168.42
gut	6.9		
1/4	6.3		
±	5.8		168.5
1/4	5.7		
gut	5.9		
Ecb	5.04		169.31
2475			
S = S.L. Bernice.			
Ecb	5.76		168.39
gut pav	6.67		167.64
1/4	6.70		
±	6.96		167.49
1/4	7.52		
gut	8.05		166.30
web	7.36		166.99
Nail Pole N1958		Bernice	
BM 35 de walla 25 S. of	5.57		168.78 (168.78)'







Villa Dr.

101.49

~~101.89~~

0-42 <sup>5</sup>		99.53
10'E tob'cb NE ret.	1.96	<del>99.53</del>
0-34		99.20
3'E tob'cb on NE ret	2.29	<del>99.60</del>
B'eq'ut.	2.4	99.1
E.L.	2.3	99.0
+5	3.0	98.5
cb	2.7	98.8
'A	2.4	99.1
⊕	3.0	<del>98.9</del> 98.5
+10	3.1	98.4
'A	3.3	98.2
+9	3.5	98.0
cb	3.6	97.9
+8	3.4	98.1
w.L.	3.6	97.9
5w'gut	3.7	97.8
5'w' tob'cb NW ret.	2.84	98.65 <del>99.05</del>
0-20		98.11
wL+A tob'cb NW ret.	3.38	98.51
gut	3.7	97.8
+7	3.8	97.7
+8	4.3	97.2
cb	4.1	97.4
+4	4.2	97.3
+7	3.7	97.8

Villa Dr.

101.49

~~101.89~~

0-20			98.0
w'A		3.5	98.2
+3		3.3	<del>98.4</del> 98.4
⊕		3.1	<del>98.9</del>
+8		3.0	98.5
+10		3.4	98.1
'A		3.1	98.4
+8		3.3	98.2
cb		3.1	98.4
+4 (gut.)		3.5	98.0
+4 tob'cb NE ret.	2.74		<del>98.75</del> 99.15
0+00 = EC NE ret			98.32
Ecb		3.17	<del>98.72</del>
gut		4.0	97.5
+3		4.2	97.3
'A		3.6	97.9
+3		3.4	98.1
⊕		3.4	98.1 <del>98.5</del>
+8		3.7	97.8
'A		4.0	97.5
+5		4.2	97.3
+8		4.4	97.1
gut		5.3	96.2
w'cb		4.09	<del>97.40</del> 97.80
tob'cb (on chateworth)			<del>97.80</del>
bc NW ret.		3.18	98.31
(on Villa Dr.)			97.18
tob'cb EC NW ret		4.31	<del>97.58</del>



Villa Dr.

101.49

(101.89)

0+25			96.59
wcb	0+29	4.90	<del>96.99</del>
gut		5.9	95.6
+4		5.3	96.2
1/4		5.0	96.5
+1		4.9	96.6
+5		4.4	97.1
+	0+28	4.1	<del>97.4</del> <del>97.8</del>
+10		4.1	97.4
1/4		4.4	97.1
+8		4.5	97.0
+7		5.0	96.5
gut		5.0	96.5
Ecb		3.93	<del>97.54</del> <del>97.96</del>
0+63	3/4 = SL Alley		96.67
E.L	top cb	4.82	<del>97.07</del>
E.L	pav	4.99	96.50
Ecb		5.03	<del>96.46</del> <del>96.8</del>
gut	pav	5.97	95.52 95.12
+7		5.9	95.6
1/4		5.6	95.9
+	0+68	5.3	<del>96.2</del> <del>96.6</del>
+5		5.5	96.0
1/4		6.0	95.5
gut		7.1	94.4
wcb	0+74	6.47	<del>95.02</del> <del>95.47</del>

Villa

Dr.

101.49

(101.89)

55

D+84	2/5 = NL Alley		94.57
wcb	0+98	6.92	<del>94.97</del>
gut		7.4	94.1
1/4		6.6	94.9
+3		6.3	95.2
+10		5.9	95.6
+	0+91	6.0	<del>95.5</del> <del>95.9</del>
1/4		5.9	95.6
+3		6.2	95.3
+8		6.6	94.9
+9		6.2	95.3
gut	grd.	6.2	95.3
gut	Alley Pav	6.49	95.00 94.6
Ecb		5.73	<del>95.26</del> <del>96.16</del>
E.L	top cb	5.60	<del>95.89</del> <del>96.29</del>
E.L	pav	5.76	95.73
+100			95.46
Ecb		6.03	<del>95.86</del>
gut		6.3	95.2
+5		6.7	94.8
1/4		6.1	95.4
+	1+08	6.3	<del>95.2</del> <del>95.6</del>
+8		6.6	94.9
1/4		7.1	94.4
+3		7.2	94.3
+9		7.6	93.9



Villa Dr.

101.49  
~~101.89~~

1+00			
Web		8.0	93.5
+1 gut.		8.0	93.5
+1 topcb enret into Vdal.	1+166	7.28	94.21 <del>94.61</del>
1+25			
2'W topcb enret		7.81	93.68
2'W gut		8.7	92.8
W.L.	1+29	8.7	92.8 <del>93.2</del>
+2		8.9	92.6
+3		8.4	93.1
1/4		8.2	93.3
+7		7.4	94.1
+10		7.5	94.0
±	1+28	6.8	94.7 <del>95.1</del>
+10		6.5	95.0
1/4		6.7	94.8
+8		7.3	94.3
gut		7.1	94.5
Ecb.		6.55	94.94 <del>95.34</del>

Villa Dr

56

101.49  
~~101.89~~

1+50			
Ecb		6.93	94.56 <del>94.96</del>
gut		7.1	94.4
+4		7.6	93.9
1/4		7.0	94.5
+1		7.0	94.5
±	1+54	7.3	94.2 <del>94.6</del>
1/4		7.7	93.8
+5		7.9	94.0
wcb		8.2	93.3 <del>93.7</del>
W.L.	1+58	8.9	92.6
1+75			
W.L.	1+87	9.1	92.4 <del>92.8</del>
cb		8.7	93.2 <del>93.2</del>
1/4		7.9	93.6
+3		7.7	93.8
±	1+81	7.6	93.9 <del>94.3</del>
+10		7.2	94.3
1/4		7.3	94.2
+6		7.5	94.0
+9		7.9	93.6
gut		7.4	94.1
Ecb		7.14	94.35 <del>94.75</del>



Villa Dr.

101.49  
101.89

2+00			94.33
Ecb		7.16	<del>94.73</del>
gut		7.8	93.7
+7		7.7	93.8
1/4		7.4	94.1
+9		7.3	94.2
+			93.9
+	2+16	7.6	<del>94.3</del>
1/4		8.4	93.6
cb		9.6	<del>91.9</del>
+4		9.6	91.9
+5		10.6	90.9
+7		9.1	92.4
w.L.	2+32	9.2	92.3
(A) See sketch		10.5	91.0 <del>91.1</del>
2+21 = BC NW rat into Udol			
w.L.	2+58	9.2	92.3
+2		8.6	92.9
cb		8.6	<del>92.9</del>
+2		8.5	93.0
+5		8.6	92.9
+6		9.6	91.9
+7		9.0	92.5
+10		8.7	92.8
1/4		8.5	93.0
+			93.9
+	2+31	7.6	<del>94.3</del>
+6		7.5	94.0

Villa Dr.

101.49  
101.89

2+21			
1/4		7.6	93.9
+7		7.9	93.6
+10		8.0	93.5
gut		7.7	93.8
Ecb		7.18	<del>94.31</del>
2+38 <sup>rd</sup> = S.L. Alley			<del>94.71</del>
EL to ecb		6.89	94.60
EL bar.		7.10	95.0
Ecb		7.06	94.39
gut		7.7	94.43
+3		7.9	93.8
1/4		7.7	93.6
+4		7.7	93.8
+8		8.2	93.8
+			93.3
+	2+50	8.2	93.3
+3		8.4	<del>93.7</del>
+5		7.8	93.1
1/4		8.1	93.7
+8		8.6	93.4
+10		8.2	92.9
cb		8.3	93.3
w.L.	2+77	8.9	<del>93.2</del>
total Int. S. Alley line ecb		7.02	93.6
gut pav		7.98	92.6
			<del>94.77</del>
			94.47
			93.56 - 93.11

57



Villa Dr.

101.49

~~101.89~~

2 + 60 <sup>52</sup> = N.L. Alley

w.L	3#02	8.5	93.0
cb		8.2	<del>93.3</del> 93.7
+5		8.5	93.0
1/4		8.2	93.3
+5		7.7	93.8
+	2+81	7.5	<del>94.0</del> 94.4
1/4		7.5	94.0
+10		7.7	93.8
+11		7.5	94.0
cb & gut.		7.5	94.0
E.L. Alley Pav.		6.93	94.56
E.L. to bcb		6.71	<del>94.78</del> 95.18
got Pav.		7.80	93.69 <sup>93.29</sup>
int. N.L. Alley 2 eb line			
+top cb		6.69	94.60
2+75			94.69
Ecb		6.80	<del>95.09</del>
gut		7.5	94.0
+5		7.6	93.9
+9		7.3	94.2
1/4		7.2	94.3
+	2+98	7.6	<del>93.9</del> 94.5
+6		7.8	93.7
1/4		8.2	93.3
+7		8.4	93.1
eb		8.0	<del>93.5</del> 93.9

Villa Dr.

58

101.49

~~101.89~~

2 + 75

cb + 8		8.2	93.3
w.L	3+21	8.7	92.8
3+00			
w.L	3+48	9.1	92.4
+3		8.0	93.5
cb		8.0	<del>93.5</del> 93.9
1/4		8.1	93.4
+	3+25	7.4	<del>94.1</del> 94.5
1/4		7.1	94.4
+2		7.1	94.4
+7		7.2	94.3
+10		6.9	94.6
gut		7.0	94.5
Ecb		6.65	<del>94.84</del> 95.24
3+33 <sup>56</sup> = D.C. SE. ret.			95.22
Ecb		6.77	<del>95.62</del>
gut		6.6	94.9
1/4		6.8	94.7
+	3+61	7.2	<del>94.3</del> 94.7
1/4		7.9	93.6
+10		8.2	93.3
+11		7.7	93.8
cb		7.8	<del>93.7</del> 94.1
+5		8.0	93.5
+7		8.7	92.8
w.L	3+89	10.5	91.0



## Villa Dr.

101.49  
~~101.89~~3+53<sup>56</sup>

W.L.	4+02	9.0	92.5
+5		7.7	93.8
cb		7.7	<del>93.8</del> 94.2
+1		7.7	93.8
+2		8.3	93.2
1/4		7.8	93.7
⊕	3+83	7.0	<del>94.5</del> 94.9
1/4		6.7	94.8
cb		6.4	95.1
+6 (gut)		6.1	95.4
+6 top cb SE ret.		5.63	<del>95.86</del> 96.26
3+66 <sup>2</sup> = SE Valtaire on East.			96.47
11'E top cb on SE ret.		5.02	<del>96.89</del>
11'E gut.		5.8	95.7
E.L. prod.		6.2	<del>95.3</del> 95.7
cb		6.6	94.9
+5		6.7	94.8
1/4		7.0	94.5
⊕	3+97	7.4	<del>94.1</del> 94.5
1/4		8.0	93.5
+8		8.3	93.2
+10		8.2	93.3
cb		7.7	<del>93.8</del> 94.2
+5		7.8	93.7
+7		8.0	93.5
W.L.	4+27+2225 to	8.4	93.1

## Villa Dr.

59

101.49  
~~101.89~~

B.C. SW ret (on Villa Dr.)	8.4	93.1
Sec on S.L. Valtaire		
E.C. SW ret.	9.3	92.2
W.L. prod. 4+49	8.5	93.0
cb	8.2	<del>93.3</del> 93.7
1/4	8.1	93.4
⊕	4+00	<del>93.9</del> 94.3
1/4	7.1	94.4
cb	6.6	94.9
E.L. prod.	6.2	<del>95.3</del> 95.7
7'E gut	5.9	95.6
7'E top cb on SE ret.	5.11	<del>96.38</del> 96.98
Sec on S edg. Pavement on Valtaire		96.65
1/4 <sup>SE</sup> top cb SE ret.	4.84	<del>97.05</del>
gut pav	5.57	95.92
E.L. prod.	6.37	<del>95.12</del> 95.52
cb	6.80	94.69
1/4	7.32	94.17
⊕	4-06	<del>93.62</del> 94.02
1/4	8.52	92.97
cb	9.18	92.31
W.L. prod. 4+55	9.68	<del>91.81</del> 92.21
EC SE ret (on Valtaire)	4.10	<del>97.39</del> 97.8



Elevs on Returns at Zola  
& Evergreen

BM	0.00	138.21	138.21	BP SW Zola cut
T.P	1.41	126.62	13.01	125.20

S.W. Return

A	0.16	126.45
B	1.24	125.37
C	1.96	124.65
D	2.70	123.91
E	3.83	122.78

N.W. Return

A	1.23	125.38
B	2.07	124.54
C	2.86	123.75
D	3.70	122.91
E	4.99	121.62

N.E. Return

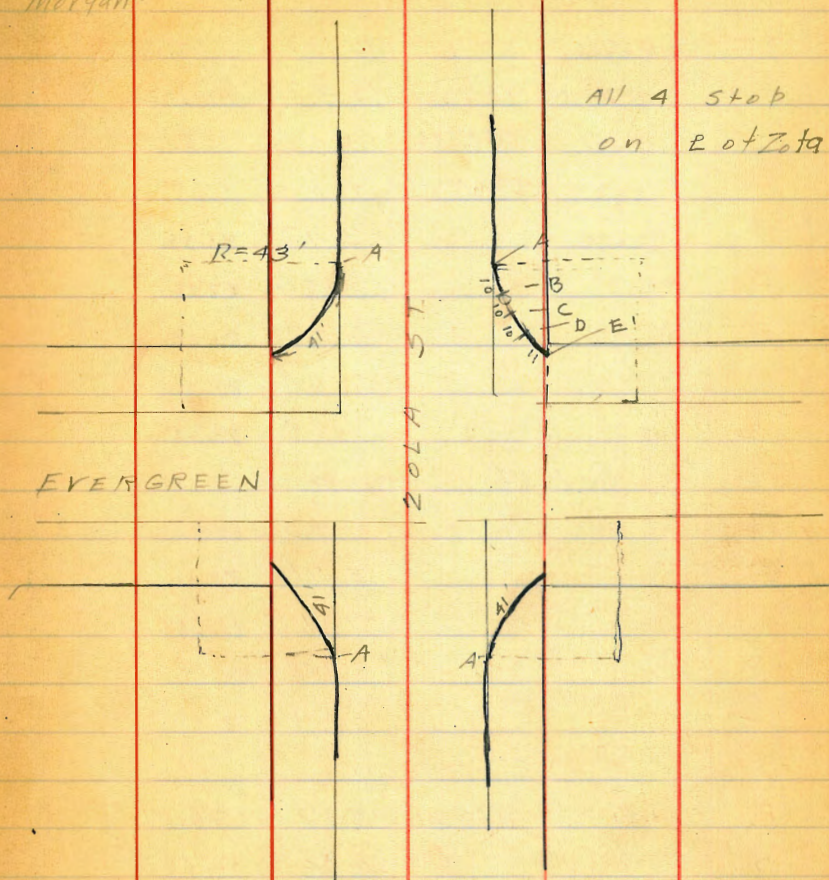
E	5.94	120.67
D	6.31	120.30
C	7.10	119.51
B	8.18	118.43
A	9.16	116.45

S.E. Return

E	4.94	121.67
D	5.34	121.27
C	6.05	120.56
B	7.12	119.49
A	8.23	118.38

Oct 9-28  
Loudon  
Isbell  
Morgan

60



This sketch applies also to  
returns on Zola & Locust



Elevs on returns on  
Zola & Locust.

126.61

T.P.	0.31	114.09	12.83	113.78
T.P.	0.37	101.69	12.77	101.32
T.P.	0.17	88.86	13.00	88.69

SW. Return

A		3.47	85.39
B		5.00	83.85
C		6.28	82.55
D		7.64	81.22
E		9.28	79.55

NW. Return

A		4.43	84.43
B		5.71	83.18
C		7.11	81.78
D		8.67	80.19
E		10.29	78.57

NE. return

E	1.31	77.40	12.77	76.09
D		2.83	74.57	
C		4.25	73.15	
B		5.77	71.63	
A		7.32	70.08	

77.40  
SE. Return

A		6.25	76.15	
B		4.83	72.57	
C		3.39	74.01	
D		1.88	75.82	
E		0.25	77.15	
T.P.	12.64	90.02	0.02	77.38
T.P.	13.10	193.01	0.11	89.91
T.P.	12.84	115.63	0.22	102.79
T.P.	13.01	128.45	0.19	115.44
T.P.	12.27	140.70	0.02	128.43
BM. Beginning		2.46	138.24	



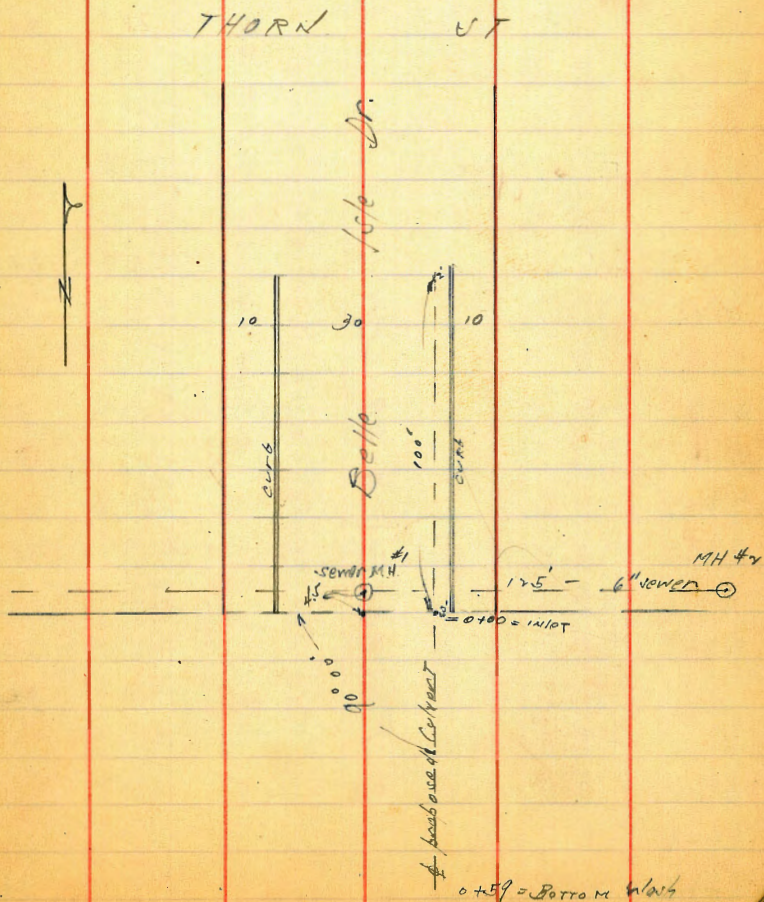
11/1/78  
Moore

Levels for Culvert on Belle Isle Dr.  
South of Thorn St

BM = Top of end of east curb	2.54	302.42	300.0	See BK 1263 Pg 22
Top of West curb	2.40		300	
Flowline of M.H. #1	11.04		291.4	
RIM " "	2.07		300.2	
0+00 = inlet	2.5		299.9	
0+20	2.6		299.8	
0+59 = outlet	21.0		281.4	

F.L. M.H. #2 0.8' lower than M.H. #1 290.6

Culvert levels ok. if desired to shift culvert line to parallel curb line to north.





X-Section Alley Bl. 62, Park Villas  
Alley 15' wide

Not in BM Book

Jaeger  
Bailey  
Clavert  
Brooks  
STA

Febr. 2nd 1929

349.13  
H.L.

63

Elev.

STA	+	H.L.	-	F		+	H.L.	-	Elev.
BM. SW. B.P.	Wightman & Pershing	9.80	347.81	338.013					
	T.P.	4.28	349.13	344.85	+88	φ Garage on E.L.			
	SW. Curb Top		5.88	343.25		E.L.		4.7	344.4
	Botl.		6.28	342.85		φ		4.7	344.4
	SE. Curb Top		5.53	343.60		W.L.		5.2	343.9
	Botl.		5.98	343.15		+3'		5.0	
0+00	E.L. Concrete		5.36	343.77	+96	φ Garage on E.L.			
	φ		5.71	343.42		+3'		5.0	
	W.L.		5.57	343.56		W.L.		5.2	343.9
+25	W.L.		5.0	344.1		φ		5.0	344.1
	φ		5.0	344.1		E.L.		4.8	344.3
	+5'		5.2	343.9		+4' Conc. Apron	0.16 higher	4.66	344.47
	E.L.		4.5	344.6	+21				
+50	E.L.		4.4	344.7		E.L.		5.1	344.0
	+3'		5.1	344.0		φ		4.9	344.2
	φ		4.8	344.3		+4.5		5.0	344.1
	W.L.		4.9	344.2		W.L.		5.7	343.4
	+2.5'		4.8		+50	+0.5	Top of Water Service	5.70	
+78	φ Garage on E.L.					W.L.		5.5	343.6
	+2.5'		5.0			φ		4.8	344.3
	W.L.		5.2	343.9		E.L.		5.1	344.0

Plotted Feb 4-29 CBH.

No evidence of Manhole.

Garage figured Feb 8-29







T 147.13

0+75

E	5.8	141.3
♀	7.1	140.0
W	7.4	139.7

1+00

W	5.9	141.2
♀	6.1	141.0
E	5.9	141.2

1+25

E	4.5	142.6
♀	4.9	142.2
W	5.1	142.0

1+50

W	4.5	142.6
♀	4.2	142.9
+7	4.2	142.9
E	3.6	143.5

1+75

E	3.5	143.6
♀	3.8	143.3
W	4.4	142.7

2+00

W	4.5	142.6
♀	4.2	142.9
E	3.5	143.6

65

T 147.13

2+25

E	3.9	143.2
♀	4.2	142.9
W	4.4	142.7

2+34

♀ 8' Garage 4' Back	E.L. <sup>Dist</sup> 3.6	143.5
---------------------	--------------------------	-------

2+44

♀ 8' Garage 4' Back	E.L. <sup>Dist</sup> 3.6	143.5
---------------------	--------------------------	-------

2+50

W	4.7	142.4
♀	4.8	142.3
E	4.2	142.9

2+67

♀ 8' Garage 6' Back W.L. Concrete Floor	5.33	141.80
---	------	--------

2+75

E	4.5	142.6
♀	4.8	142.3
W	5.2	141.9

3+00

W	5.1	142.0
♀	4.9	142.2
+7	5.1	142.0
E	4.1	143.0

3+25

E	4.6	142.5
+3	5.3	141.8



π 147.13

♀	5.4	141.7
W	5.8	141.3
3+50		
W	6.4	140.7
♀	5.7	141.4
E	5.0	142.1
3+43		
♀ 8' Garage 3' Back Ev. Dirt Floor	4.8	142.3
3+75		
E	5.5	141.6
♀	6.2	140.9
W	6.9	140.2
4+00		
W	6.6	140.5
♀	6.3	140.8
+7	6.2	140.9
E - Base small concrete Wall-Northeast	5.3	141.8
Top Wall	4.18	142.95
3+83		
Southend Top Wall	4.11	143.02
4+25		
E.	6.2	140.9
♀	6.4	140.7
W	6.9	140.2

66

π 147.13

4+50		
W	6.8	140.3
♀	6.5	140.6
E	6.1	141.0
4+75		
E	5.8	141.3
+3	7.0	140.1
♀	7.0	140.1
W	7.2	139.9
4+95		
W	7.7	139.4
♀	8.4	138.7
+7	7.8	139.3
E	6.3	140.8
5+00 = 5 L. Gutter - Paved		
E - Top cb	8.52	138.61
Gutter	9.02	138.11
♀	9.60	137.53
W Top cb + Gutter Flush	9.60	137.53
South Gutter Gutter		
W	10.44	136.69
♀	9.98	137.15
E	9.46	137.67
T.P.	9.71	137.42
+2.15 139.57		
B.M. S.E. Top Hydrant Eads + Rushville	6.11	133.40
Correct		133.42



7-23-29 X-section Weaver St. - 60<sup>th</sup> to  
 J.C. Bliss Republic - 60' wide 10' cbs - 10' 1/2  
 Drebert  
 Paener

B.M. N. E. Nails in Pole 60<sup>th</sup> & Radio Drive 244.56  
 Set by Walker  
 Cont. 12/1-19960 +10.96 255.52  
 -0.32 255.20  
 +12.02 267.22  
 -0.04 267.18  
 +11.02 278.20  
 -0.31 277.89  
 11.61 289.50  
 -0.54 288.96  
 +12.92

Σ 301.88

B.M. S.E. Prob. Hub 60<sup>th</sup> & Weaver -7.02 294.86

Section on EL. 60<sup>th</sup>.

S	7.0	294.9
cb	6.0	295.9
1/4	5.0	296.9
2	3.9	298.0
1/4	3.2	298.7
cb	2.3	299.6
N	1.5	300.4
F.P.	-1.46	300.42

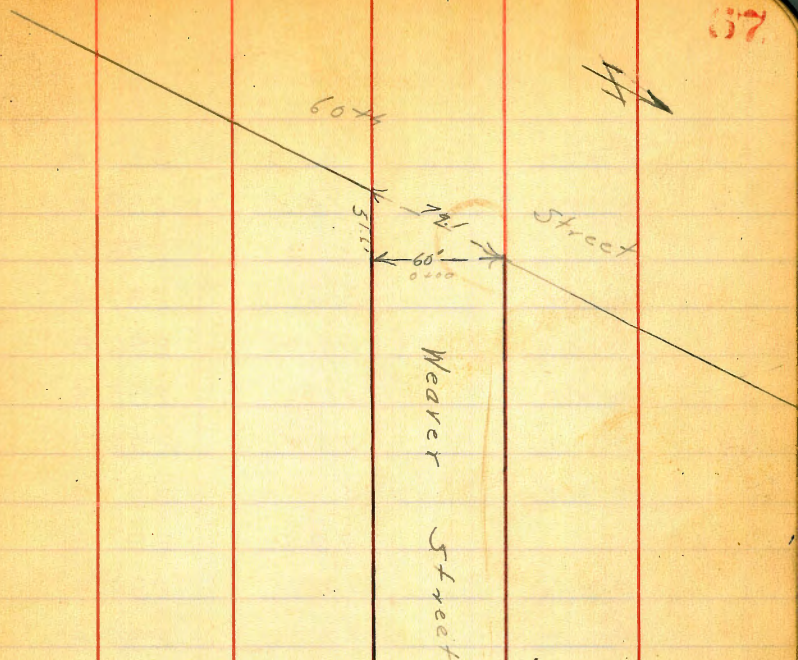
+13.14

Σ 313.54

0+00 = see sketch next page

N

13.3 300.2





T 313.54

cb	13.7	300.8
1/4	14.5	299.0
¢	15.2	298.3
1/4	16.1	297.4
cb	16.7	296.8
S	18.2	295.3
Out 20	21.2	292.3
	0425	
Out 20	22.3	291.2
S	19.2	294.3
cb	17.7	295.8
1/4	16.5	297.0
¢	15.5	298.0
1/4	14.7	298.8
cb	13.6	299.9
N	13.0	300.5
	0450	
N	12.1	301.4
cb	12.9	300.6
1/4	14.0	299.5
¢	15.2	298.3
1/4	16.4	297.1
cb	18.0	295.5
S	20.3	293.2
Out 20	23.8	289.7

T 313.54

68

0475

Out 20	20.2	293.3
S	18.0	295.5
cb	16.5	297.0
1/4	15.0	298.5
¢	13.3	300.2
1/4	12.7	300.8
cb	11.6	301.9
N	10.8	302.7
	1400	
N	9.0	304.5
cb	9.6	303.9
1/4	10.8	302.7
¢	11.8	301.7
1/4	12.7	300.8
cb	13.3	300.2
S	14.1	299.4
Out 20	15.5	298.0
	1425	
Out 10	13.3	300.2
S	12.5	301.0
cb	11.3	302.2
1/4	10.5	303.0
¢	9.9	303.6
1/4	9.0	304.5
cb	7.9	305.6



π 313.54

N	7.0	306.5
	1+50	
N	5.2	308.3
cb	6.1	307.4
1/4	2.0	306.5
£	7.8	305.7
1/4	8.4	305.1
cb	9.2	304.3
S	10.5	303.0
Out 20	13.1	300.4

1+75

Out 20	11.0	302.5
S	9.1	304.4
cb	7.2	306.3
1/4	6.6	306.9
£	6.0	307.5
1/4	5.1	308.4
cb	4.0	309.5
N	3.0	310.5

2+00

N	0.9	312.6
cb	1.8	311.7
1/4	2.9	310.6
£	3.7	309.8
1/4	4.4	309.1

π 313.54

69

cb	5.3	308.2
S	7.2	306.3
Out 20	10.4	303.1
	2+25	
	9.3	304.2
S	5.8	307.7
cb	3.9	309.6
1/4	2.9	310.6
£	2.0	311.5
T.P	-1.06	312.48

+1223

π 324.71

1/4	12.1	312.6
cb	11.0	313.7
N	9.9	314.8
	2+50	
N	8.4	316.3
cb	9.4	315.3
1/4	10.2	314.5
£	11.4	313.3
1/4	12.8	311.9
cb	14.1	310.6
S	12.8	311.9
Out 20	16.2	308.5



T 324.71

2+75

Out 20	18.7	306.0
S	15.1	309.6
cb	13.2	311.5
1/4	11.8	312.9
£	10.5	314.2
1/4	9.3	315.4
cb	8.1	316.6
N	6.9	317.8

3+00

N	5.3	319.4
cb	6.2	318.5
1/4	8.6	316.1
£	9.6	315.1
1/4	11.2	313.5
cb	12.5	312.2
S	14.3	310.4
Out 20	17.5	307.2

3+25

Out 20	16.8	307.9
S	13.4	311.3
cb	11.5	313.2
1/4	10.1	314.6
£	8.6	316.1
1/4	7.5	317.2
cb	5.6	319.1

T 324.71

70

N	2.8	321.9
3150		
N	1.1	323.6
+3	2.6	322.1
cb	4.3	320.4
1/4	6.1	318.6
£	7.4	317.3
1/4	8.9	315.8
cb	10.6	314.1
S	12.3	312.4
Out 20	15.5	309.2

3+75

Out 20	14.1	310.6
S	11.0	313.7
cb	9.3	315.4
1/4	7.7	317.0
£	6.2	318.5
1/4	4.6	320.1
cb	2.4	322.3
+	1.1	323.6
N	0.0	324.7

+ 9.21 329.59

- 4.33 320.38



π 329.59

4+00

N	3.9	325.7
cb	6.3	323.3
1/4	8.3	321.3
£	10.0	319.6
1/4	11.7	317.9
cb	13.3	316.3
S	14.8	314.8
Out 20	17.6	312.0

4+25

Out 20	16.9	312.7
S	14.2	315.4
cb	12.3	317.3
1/4	11.0	318.6
£	9.0	320.6
1/4	7.3	322.3
cb	5.2	324.4
N	3.5	326.1

4+50

N	2.3	327.3
cb	4.5	325.1
1/4	6.6	323.0
£	8.3	321.3
1/4	10.1	319.5
cb	11.8	317.8
S	13.0	316.6

71

π 329.59

Out 20	16.7	312.9
4+75		
Out 20	16.8	312.8
Out 20	13.1	316.5
cb	11.4	318.2
1/4	9.9	319.7
£	7.5	322.1
1/4	5.6	324.0
cb	4.0	325.6
N	1.8	327.8

5+00

N	1.0	328.6
cb	3.1	326.7
1/4	5.4	324.2
£	7.0	322.6
1/4	9.4	320.2
cb	11.1	318.5
S	12.9	316.7

No out account of chicken House

5+25

No out account of chicken House

S	11.9	317.7
cb	10.9	318.7
1/4	9.3	320.3
£	7.2	322.4



T 329.59

1/4	55	324.1
cb	3.4	326.2
N	1.0	328.6
5750		
N	0.8	328.8
cb	3.0	326.6
1/4	5.6	324.0
£	6.8	322.8
1/4	9.0	320.6
cb	10.8	318.8
S	11.6	318.0

No out account chicken house

5781.6 = B.C - 4 Parts Inside Rad. 170'  $\Delta 53^{\circ} 01'$

Out 20	15.7	313.9
S	12.2	317.4
cb	10.6	319.0
1/4	9.1	320.5
£	6.6	323.0
1/4	5.2	324.4
cb	3.1	326.5
N	0.5	329.1

B.M. NE Cor Meter Box - South side Near 5750

+12.11 331.33

-10.97 318.62

T 331.33

72

Part 1

N	2.3	329.0
cb	4.5	326.8
1/4	6.2	325.1
£	7.3	324.0
1/4	9.4	321.9
cb	11.3	320.0
S	12.7	318.6
Out 20	17.2	314.1

Part 2

Out 20	11.4	319.9
S	8.5	322.8
cb	7.1	324.2
1/4	5.8	325.5
£	4.4	326.9
1/4	3.3	328.0
cb	2.0	329.3
N	0.5	330.8
T.P.		-0.50 330.83

+11.36 342.19

Part 3

N	8.2	323.1
cb	10.3	321.0
1/4	12.0	319.3
£	12.7	318.6
1/4	14.1	317.2



π 342.19

cb	15.2	327.0
S	16.5	325.7
Out 20	20.0	322.2
E C 20+00		
Out 20	20.2	322.0
E	16.0	326.2
cb	13.7	328.5
1/4	12.0	330.2
¢	10.5	331.7
1/4	9.1	333.1
cb	6.7	335.5
W	4.8	337.4
0+25		
W	2.7	339.5
cb	5.6	336.6
1/4	7.5	334.7
¢	9.4	332.8
1/4	10.7	331.5
cb	12.2	330.0
E	14.2	328.0
Out 20	18.6	323.6
0+50		
Out 20	17.8	324.4
E	13.5	328.7
cb	11.3	330.9

π 342.19

73

1/4	9.5	332.7
¢	8.1	334.1
1/4	6.3	335.9
cb	3.5	338.6
W	0.9	342.3
0+75		
W	0.4	341.8
cb	3.0	339.2
1/4	5.2	337.0
¢	7.3	339.9
1/4	8.8	333.4
cb	10.6	331.6
E	13.0	329.2
Out 20	16.8	325.4
1+00		
Out 20	16.8	325.4
E	12.5	329.7
cb	10.1	332.1
1/4	7.8	334.4
¢	6.2	336.0
1/4	4.2	338.0
cb	2.3	339.8
W	0.0	342.2
1+25		
W	10.3	342.5



T 342.19

cb	1.7	340.5
1/4	4.1	338.1
£	5.5	336.7
1/4	8.0	334.2
cb	10.5	331.7
E	12.6	329.6
Out 20	17.3	324.9
	14.50	
Out 20	16.7	325.5
E	12.4	329.8
cb	10.4	331.8
1/4	8.0	334.2
£	5.2	337.0
1/4	4.1	338.1
cb	1.4	340.8
W	10.5	342.7
	1486' = B.C. - 2 Parts <sup>at 14° 53'</sup> Outside Rad. 200'	
W.	10.6	342.8
cb	1.1	341.1
1/4	3.8	338.4
£	5.1	337.1
1/4	7.0	337.2
cb	9.3	332.9
E	12.2	330.0
Out 20	15.0	327.2

T 342.19

74

Part 1

Out 20	11.6	330.6
E	9.6	332.6
cb	8.1	334.1
1/4	6.5	335.7
£	4.9	337.3
1/4	3.5	338.7
cb	1.4	340.8
W	10.7	342.9
	E.C. = 0+00	
W	10.5	342.7
cb	1.7	340.5
1/4	2.8	339.4
£	3.2	339.0
1/4	3.9	338.3
cb	3.8	338.4
E	6.3	335.9
Out 20	8.2	334.0
	0+25	
E	3.6	338.6
cb	3.1	339.1
1/4	2.4	339.8
£	1.5	340.7
1/4	1.3	340.9
cb	0.7	341.5
W	0.0	342.2



T 342.19

75

T.P. -0.00 342.19

+1267

T 354.86

0+50

W 11.9 343.0  
 cb 12.3 342.5  
 1/4 12.6 342.2  
 ♀ 12.5 342.3  
 1/4 12.6 342.2  
 cb 12.4 342.4  
 E 12.0 342.8

0+75

E 8.5 346.3  
 cb 9.3 345.5  
 1/4 9.6 345.2  
 ♀ 10.3 344.5  
 1/4 10.7 344.1  
 cb 11.0 343.8  
 W 11.2 343.6

1+27.80 = 5.6 Burian - 60' wide

W 11.0 343.8  
 cb 9.5 345.3  
 1/4 8.7 346.1  
 ♀ 8.6 346.2  
 1/4 7.2 347.6

T 354.86

cb 5.7 349.1  
 E 4.3 350.5

♀ Burian

E 2.5 352.3  
 cb 4.2 350.6  
 1/4 5.6 349.2  
 ♀ 7.0 347.8  
 1/4 8.0 346.8  
 cb 9.5 345.3  
 W 10.7 344.1  
 Out 20 14.0 340.8

Section between N.W. Corner Burian + Weaver

+ S.E. Corner Republic + Weaver

Out 20 13.5 341.3  
 W 9.4 345.4  
 cb 7.6 347.2  
 ♀ 7.1 347.7  
 1/4 5.5 349.3  
 ♀ 4.5 350.3  
 ♀ 4.6 350.2  
 1/4 2.9 351.9  
 cb 0.7 354.1  
 E 11.3 356.1

B.M. N.W. Prop. Hub Burian + Weaver - 9.38 345.48



T.P.		-11.13	343.73
	+5.25		348.98
T.P.		-8.55	340.43
	+4.16		344.59
B.M. Top Boulder Dipper & Weaver	- 8.13		336.46
Set by Jaeger - Book 1302 Pages - Elev -			335.90
Boulder had been moved some			
B.M. N.W. Prop. Hub Weaver & Burien			345.48
	0.89		346.37
T.P.		-13.12	333.25
	+0.01		333.26
T.P.		-13.22	320.04
	+0.21		320.25
T.P.		-12.91	307.34
	+0.28		307.62
		-12.90	294.72
	1.45		296.17
T.P.		-13.19	282.98
	+0.07		283.05
T.P.		-13.18	269.87
	+0.06		269.93
		-12.82	257.11
	0.09		257.20
B.M. Nails in N.E. Post Rods - 60"		-12.72	244.48
		Correct	244.56

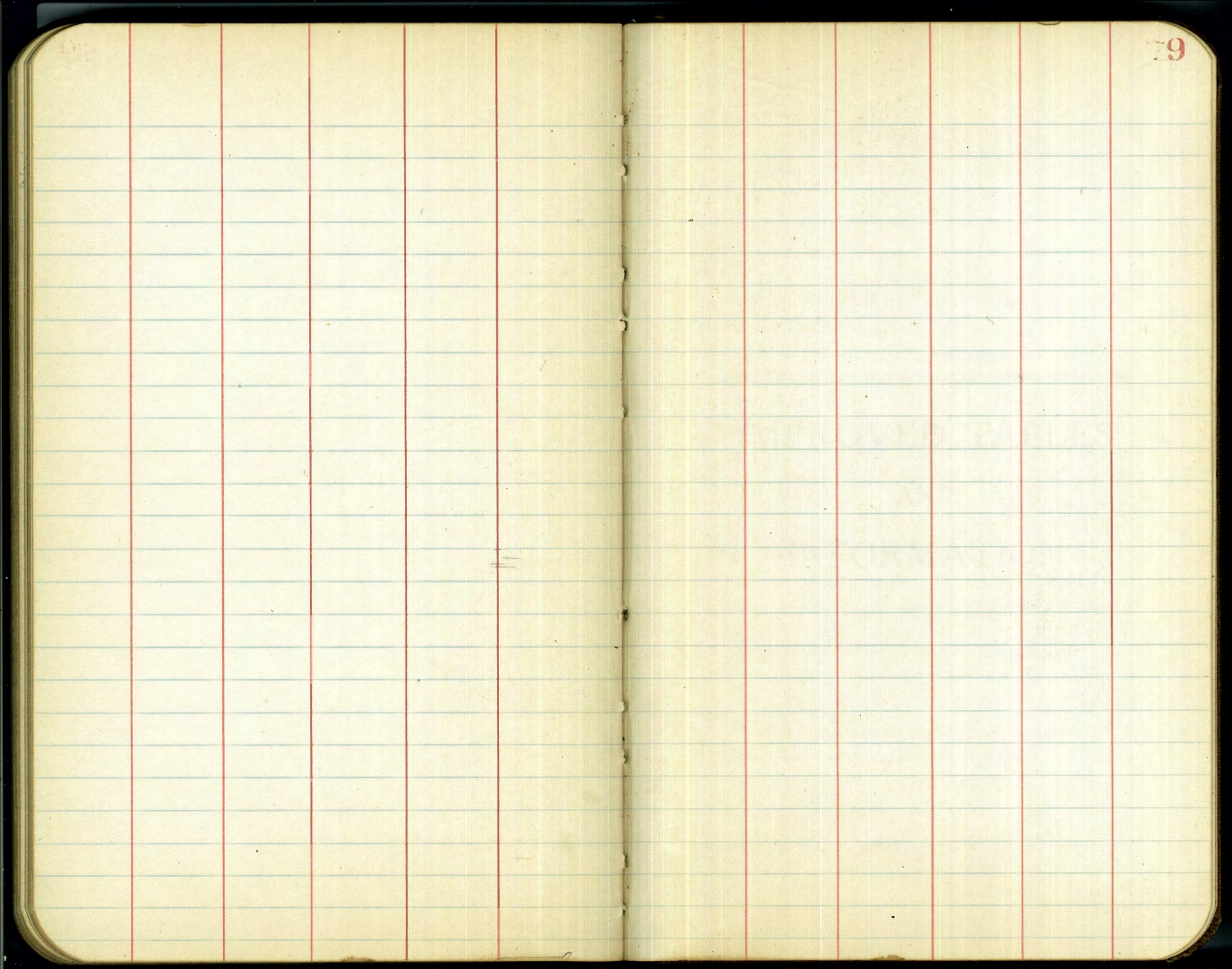














DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 1/2 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body

from side stake to slope stake. If ground is not level, the side stake and slope stake, lower target by the amount it cut - elevate if fill. Add this amount to cut or fill and find in table. Set up rod at this point and line of sight should cut target. If necessary.

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given I may be found by dividing tangent (or external), opposite I by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

**IMPROVED TABLES  
AND  
INFORMATION**



$$\begin{array}{r}
 7 + 56.09 \\
 \quad 7.50 \\
 \hline
 7 + 63.59 \\
 \quad 7.50 \\
 \hline
 7 + 71.09 \\
 \quad 7.50 \\
 \hline
 7 + 78.59 \\
 \quad 7.50 \\
 \hline
 7 + 86.09
 \end{array}$$

$$\begin{array}{r}
 161.53 \\
 144.36 \\
 \hline
 9.17
 \end{array}$$

$$\begin{array}{r}
 338.01 \\
 + 9.80 \\
 \hline
 347.81
 \end{array}$$

$$\begin{array}{r}
 347.81 \\
 - 2.96 \\
 \hline
 344.85
 \end{array}$$

$$\begin{array}{r}
 4.53 \\
 4.37 \\
 \hline
 8.90
 \end{array}$$

$$\begin{array}{r}
 16349.13 \\
 - 6.21 \\
 \hline
 16342.92
 \end{array}$$

$$\begin{array}{r}
 342.92 \\
 + 4.24 \\
 \hline
 347.16
 \end{array}$$

$$\begin{array}{r}
 347.16 \\
 - 9.15 \\
 \hline
 338.01
 \end{array}$$

$$\begin{array}{r}
 338.01
 \end{array}$$

$$\begin{array}{r}
 12 \\
 10 \\
 \hline
 2 \\
 78 \\
 \hline
 80 \\
 208
 \end{array}$$

$$\begin{array}{r}
 197.59 \\
 8.60 \\
 \hline
 206.14
 \end{array}$$

$$\begin{array}{r}
 206.14 \\
 1.15 \\
 \hline
 204.99
 \end{array}$$

$$\begin{array}{r}
 204.99 \\
 + 6.77 \\
 \hline
 211.76
 \end{array}$$

$$\begin{array}{r}
 211.76 \\
 - 14.97 \\
 \hline
 198.79
 \end{array}$$

$$\begin{array}{r}
 198.79 \\
 1.89 \\
 \hline
 200.68
 \end{array}$$

$$\begin{array}{r}
 200.68 \\
 9.56 \\
 \hline
 191.12
 \end{array}$$

$$\begin{array}{r}
 191.12 \\
 + 14.20 \\
 \hline
 203.32
 \end{array}$$

$$\begin{array}{r}
 203.32 \\
 11.40 \\
 \hline
 181.92
 \end{array}$$

$$\begin{array}{r}
 181.92 \\
 + 1.32 \\
 \hline
 193.24
 \end{array}$$

$$\begin{array}{r}
 193.24 \\
 4.87 \\
 \hline
 188.37
 \end{array}$$

$$\begin{array}{r}
 188.37 \\
 193.24 \checkmark \\
 \hline
 11.64 \checkmark
 \end{array}$$

$$\begin{array}{r}
 11.64 \checkmark \\
 181.60 \checkmark \\
 \hline
 2.00 \checkmark
 \end{array}$$

$$\begin{array}{r}
 2.00 \checkmark \\
 183.62 \checkmark \\
 \hline
 11.44 \checkmark
 \end{array}$$

$$\begin{array}{r}
 11.44 \checkmark \\
 172.18 \checkmark \\
 \hline
 0.09 \checkmark
 \end{array}$$

$$\begin{array}{r}
 0.09 \checkmark \\
 172.27 \checkmark \\
 \hline
 13.00 \checkmark
 \end{array}$$

$$\begin{array}{r}
 13.00 \checkmark \\
 159.27 \checkmark \\
 \hline
 2.26 \checkmark
 \end{array}$$

$$\begin{array}{r}
 2.26 \checkmark \\
 151.53 \checkmark \\
 \hline
 9.20
 \end{array}$$

$$\begin{array}{r}
 9.20 \\
 142.33
 \end{array}$$

$$\begin{array}{r}
 142.36 \\
 + 7.67 \\
 \hline
 150.03
 \end{array}$$

$$\begin{array}{r}
 150.03 \\
 - 13.07 \\
 \hline
 136.96
 \end{array}$$

$$\begin{array}{r}
 136.96 \\
 + 5.17 \\
 \hline
 142.13
 \end{array}$$

$$\begin{array}{r}
 142.13 \\
 - 6.77 \\
 \hline
 135.36 \text{ B.M.}
 \end{array}$$

$$\begin{array}{r}
 135.36 \\
 145.70 \\
 \hline
 - 1.03
 \end{array}$$

$$\begin{array}{r}
 - 1.03 \\
 144.67 \\
 \hline
 14.65
 \end{array}$$

$$\begin{array}{r}
 14.65 \\
 157.32 \\
 \hline
 - 1.07
 \end{array}$$

$$\begin{array}{r}
 - 1.07 \\
 156.25 \\
 \hline
 + 11.42
 \end{array}$$

$$\begin{array}{r}
 + 11.42 \\
 177.67 \\
 \hline
 - 0.78
 \end{array}$$

$$\begin{array}{r}
 - 0.78 \\
 176.89 \\
 \hline
 14.39
 \end{array}$$

$$\begin{array}{r}
 14.39 \\
 189.28 \\
 \hline
 - 0.90
 \end{array}$$

$$\begin{array}{r}
 - 0.90 \\
 188.38 \\
 \hline
 + 12.64
 \end{array}$$

$$\begin{array}{r}
 + 12.64 \\
 201.02 \\
 \hline
 - 1.17
 \end{array}$$

$$\begin{array}{r}
 - 1.17 \\
 199.85 \\
 \hline
 10.72
 \end{array}$$

$$\begin{array}{r}
 10.72 \\
 210.57 \\
 \hline
 13.03
 \end{array}$$

$$\begin{array}{r}
 13.03 \\
 197.54
 \end{array}$$

$$\begin{array}{r}
 216.75 \\
 5.21 \\
 \hline
 221.96
 \end{array}$$

$$\begin{array}{r}
 221.96 \\
 - 10.69 \\
 \hline
 211.27
 \end{array}$$

$$\begin{array}{r}
 211.27 \\
 3.24 \\
 \hline
 214.51
 \end{array}$$

$$\begin{array}{r}
 214.51 \\
 7.02 \\
 \hline
 207.49
 \end{array}$$

$$\begin{array}{r}
 207.49 \\
 4.25 \\
 \hline
 211.74
 \end{array}$$