

1277

RAST

LEVEL BOOK

No. 380

V. Section Bk 95 Monrosse & Schiller
Bk 29 Normal H.H.

ENGINEERING DEPARTMENT.
CITY OF SAN DIEGO.
CALIFORNIA.

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This notebook copy 9/27/64

Alley Blk 95 Manasse & Schillers	1-3
" " 29 Normal Hts	4-5
Kalmia st curb levels India to Kettner	6-
X Sec. Chaledony Cass to N.S. Highlands	7-
" " Missouri " " " "	9
" " Linda Vista Rd. at 6th St. extension	13
Taken by Taylor of Cotton Real Estate Company.	
X- Sections of Fern Glen. From Monte Vista	
St. South La Jolla, West to Ocean	14-20
X Section Alley Block D. Belmont from	
E. I. Cajon to Monroe.	
X Sec. California St. Hawthorne	
to Juniper	
X Sec. Ivy St. Kettner to N. line California	37
Alley Blk-3- Palm Hts	51
X sec. 29th St. Bdwy. to F	55
" " E St. 28th to 30th	64

1

of
Coo. Hts.

Base
ation

foors

on line
20 South

of
24 up

Elev.

3008
 008
 3000

73
 68

Miller
Exploring
Station
9-7-28

Cross Section ²⁰ Alley Bk 35

MANHASSA and SCHUBERS Add.

Bet. Main & Newtop
From St. L. Dewey to E. L. Gosby St.

N.F. St			
Main & Dewey	7.67	32.63	24.96
	0+00 = W.L. Dewey St.		
S + 0.45 = top cb.	4.73		27.90
S Gutter in Pav.	4.95		27.68
L on Pav M.H.	5.18		27.45
+ 10.7 on Gutter	4.60		28.03
L + 10.2 " top cb.	4.34		28.29
	0+50		
N	4.7		27.9
L	4.6		28.0
S	4.7		27.9
			27.6
0+80 = East edge Bld on South on line			
+ 9.5 = L Garage on North dirt floor on line 10' wide			
S	5.4		27.2
+ 2	4.8		27.8
+ 3	5.3		27.3
L	5.0		27.6
N at Garage	5.0		27.6
1+50 = East edge "D" Bld on N. = East and West edge Bld's on South			
N-5 = on Floor Bld. on Con. ✓	4.00		28.6
N-5 = at Base of Foundation	5.00		27.6
N	5.0		27.6
L	4.8		27.8
S at Bld's	4.8		27.8
1+75 = West edge "D" Bld on N = L Doorway on S Con Floor			

Plotted
Garage
9-27-28
T&H

32.63

S on Con Floor	✓	4.80	27.83
L		4.7	27.9
N at Base of Foundation		4.7	27.9
+ 0.5 on Con Floor	↓	4.28	28.35
		2+26 = East edge "E" Bld on N 9.5' Back	
N-0.5 at Base Foundation	↓	4.7	27.9
N		4.7	27.9
L		4.8	27.8
S		4.8	27.8
		4.18	28.45
		2+44 = L Doorway "E" Bld on N 7.5' Wide Con Floor	
		2+50 = West edge "B" Bld on South = East edge "F" Bld on South on line	
S on Con Floor "F" Bld.	✓	4.58	28.05
S + 3' on toe Con Apron		4.85	27.78
L		4.6	28.0
N		4.5	28.1
		4.4	28.2
		2+62 = West edge "E" Bld on N on line	
		2+72 = L Dble. Garage on North 0.2' Back dirt Floors	
N-0.2 on Floor		4.6	28.0
L		4.4	28.2
+ 7 on toe Apron "F" Bld.		4.81	27.8
S " Con Floor " " ✓		4.60	28.0
		2+89 = West edge "F" Bld on South on line = East edge "G" Bld on South on line	
S on Con Floor "F" Bld.	✓	4.57	28.06
S + 3' " toe Apron "F" Bld		4.75	27.9
T.P.	5.45	33.51	4.57 28.06
			27.5
3+01 = East edge "H" Bld on N Con Floor			
			4.51
			4.51
			38.13

1

3351

	3+22 = ^{20'} Doorway to "G" Bld. on S. Con. Floor		34th. Con. Apron
S on Con. Floor	↓	552	27.99
+2 " Apron (top)		575	27.76
↓		53	28.2
N at Base Foundation		52	28.3
N on Floor "H" Bld.	↓	448	29.03
	R = 4.8	28.7	Base Foundation
3+51 = West edge "G" Bld. on South			
3+76 = " " "H" " North			
N on Con. Floor "H" Bld.	↓	4.30	29.21
N at Base " "		55	28.0
↓		55	28.0
S		54	28.1
	4+21 = East edge Fringe ^{dirt floor} shed on S. on line		
S		52	28.3
↓		52	28.3
N		51	28.4
	4+49 = West edge Above Shed		
N		48	28.7
+1		51	28.4
↓		52	28.3
+8		56	27.9
S		54	28.3
	4+70 = East edge "I" Bld. on North on Line dirt floor		
S		4.4	29.1
+2		5.0	28.5
↓		5.0	28.5

3351

2

+9		50	28.5
N at Base Wooden Foundation	↓	4.4	29.1
5+00 = West edge "I" Bld. on N		3.3	30.2
N - 92 at Base Bld		4.4	29.1
↓		4.9	28.6
+7		4.7	28.8
S		R = 3.3	30.2
		3.3	30.2
	5+05 = East edge "J" Bld. on North Con. Floor on Line		
	10' wide		
5+20 = Doorway "J" Bld. on Con.		7.65	30.86
	5+35		
N		5.1	28.4
↓		5.0	28.5
+6		5.1	28.4
+7		3.8	29.7
S		3.1	30.4
	5+41 = Doorway 12' wide "J" Bld.	3.84	29.67
	5+69 = West edge "J" Bld. on Line = East edge "K" Bld. on N		
N on Floor		3.80	29.71
" " Ground		4.2	29.3
N+5		5.1	28.0
↓		5.7	27.8
+6		5.6	27.9
+8		3.5	30.0
S		R = 3.5	30.0
		2.9	30.6
	5+87 = West edge "K" Bld.		
	5+98		

N	3.6	29.9
74	6.4	27.1
L	7.0	26.5
+6	6.9	26.6
S	3.6	29.9

6+01 = E.L. Posky

S top cb.	7.46	26.05
S Gut. on Ground	7.5	26.0
L	7.2	26.3
N " " "	7.72	26.3
N top cb.	7.17	26.34
T.P. 10.02 35.88	7.65	25.86
cb. in S.Y. B.P. Newton & Corby	6.94	28.94

28.93 = 8.4
0.01 = Error.

X. Section 15' Alley Blk. 29 Normal Hts.

Est. Adams & Collier
From 33rd to Felton

622 392.93 386.71

S.E. Adams
Mid 33rd St.

E.L. 33rd St. = 0+00

S top Pavng	4.49	388.44
L 00 "	4.58	388.35
N " "	4.39	388.54

0+06

N	3.7	389.2
L	3.9	389.0
S	3.5	389.4

0+47 = West end Hollow Tile Wall on South, 0.4' in Alley

S + 0.4 of Wall on Ground	2.3	390.6
L	2.5	390.4
N	2.5	390.4

0+96 = East end Above Wall 0.3' in Alley

N	2.1	390.8
L	2.0	390.9
+ 7.2 = on Ground at Wall	1.9	391.0
	↓ Rod = 2.08	390.85

1+13 = 1/2 Dble. Garage on North, 11' back Con. Floor Level across

1+28 = West end Con. Porch on South, 1' in Alley

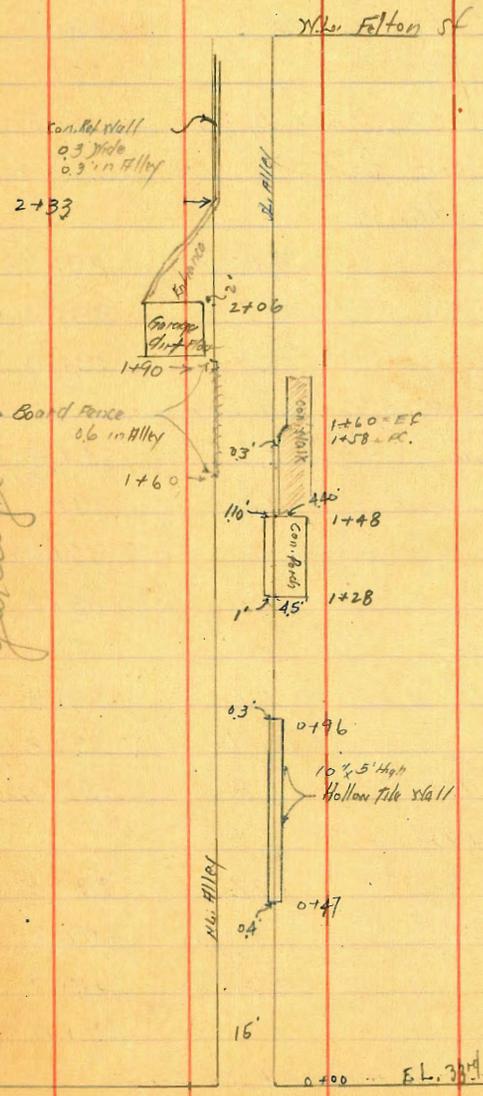
S + 1' on top Con. Porch	0.61	392.32
+ 1 at Bottom "	2.2	390.7
L	2.0	390.9

Rod on top Porch = 0.61
392.31

1+48 = East end Above Porch.

1+58 at P. on Walk. ↓ 1.77 391.16

Plotted 9-13-28 C.B.H.
9-26-28 T.G.H.
Yardage



392.93

1+80

N	2.0	390.9
E	2.0	390.9
S	1.8	391.1

1+95 = 1/2 Board Fence on South 30' long 0.5' in Alley
R = 1.9 391.0 dirt floor

2+06 = East Front Garage on North East entrance see sketch

2+09 = 1/2 Cor. Wall on South on line 3' wide

S on Wall	1.55	391.38
E	1.7	391.2
N	1.9	391.0

2+33 = RC. 3" Cor. Wall. Lady Prop. owner says this foundation of wall about 2' under ground

N+23 on top Wall	1.5	391.4
N+23 " Ground at Wall	1.8	391.1
E	1.8	391.1
S	1.7	391.2

Bottom about 2' lower

2+63

S	1.9	391.0
E	2.1	390.8
+7.4 on top Ground	1.8	391.1
+7.4 on top Wall		Ground Same

2+78

N on top Wall	1.92	391.01
" " Ground at Wall	2.8	390.1
E	3.2	389.7
S	1.9	391.0

27. 1+81.9 = YL Felton Bit 92 Long
1+82.9 = West edge Paving cbs. Stops 1' Short of 2177

392.93

1+82.9

S - 0.2' on top cb	3.64	389.29
S Gutter on Pav.	3.70	389.23
E " "	3.94	388.99
+7.10 on Gut. on Pav.	3.75	389.18
+7.10 on top cb	3.65	389.28

5

Walker
Rep. Inspector
Shaw
9-11-20

CURB LEVELS ON KALMIA ST. 80' wide
14' cbs
13' fs
from W. India to E.L. Kettner Blvd.

36.81

6

0.87 47.74

46.87

54.82
Jumper
2nd In 914 St.

W. India St. = 0+00

S top cb	5.76	41.98
J Gutter on Paving	5.76	41.98
1/4 " "	5.76	41.98
1/2 " "	5.99	41.75
3/4 " "	6.17	41.57
N " "	6.41	41.33
N top cb. (Not on C. Return)	6.01	41.73
	0+25	
N top cb.	7.29	40.45
S " "	7.10	40.64
	0+50	
S " "	8.38	39.86
N " "	8.62	39.12
	0+75	
N " "	9.92	37.82
S " "	9.70	38.04
	1+00 = d MH	
S " "	11.02	36.72
L on Rim MH	11.05	36.69
N top cb.	11.15	36.59
	1+19	
N " "	12.19	35.55
TP	0.25	36.81
	11.18	36.56

Plotted 9-17-28-C.B.H.

Note: South West Road North West Returns at India should be rebuilt

S top cb

4.11

35.70

1+25

S " "

1.45

35.36

N " " in Drive Way

2.06

34.85

1+42

N top cb. in Drive

2.85

33.96

1+44

N top cb.

2.55

34.26

1+50

N top cb.

2.85

33.96

S " "

2.74

34.07

1+75

S top cb.

4.10

32.71

N " "

4.18

32.63

1+99 = End cb. on N

N top cb.

5.40

31.41

1+99.5

S " "

5.29

31.52

2+00 = E.L. Kettner Blvd.

S " "

5.43

31.38

Gutter on Paving

6.01

30.80

1/4 " "

5.46

31.35

1/2 " "

5.34

31.47

3/4 " "

6.24

30.57

N " "

6.55

30.16

N top cb.

5.89

30.92

chk. in SE. B.M. Laurel + Kettner

3.01

33.00
22.97
10.03 = difference

Note: Paving has settled Bet S and N cb.
" Also N.E. Return "

X section of Chalcydony from Cass to
80' st. 20' cbs W.L. N.S.H. Carried over from Book 1204

10' $\frac{1}{4}$				
	70.69			
4+50				
s.L.	3.4	3.4	67.3	
cb	3.5			
$\frac{1}{4}$	2.6			
E	2.4		68.3	
$\frac{1}{4}$	2.1			
cb	1.9			
N.L.	1.3		69.4	
4+98 = W.L. Dawes				
N.L.	0.7		69.0	
cb	1.1			
$\frac{1}{4}$	1.3			
E	1.4		69.9	
$\frac{1}{4}$	1.5			
cb	1.9			
s.L.	2.7		68.0	
			75.53 = B.M.	
2.57	78.10			
0+00 = E.L. Dawes				
s.L.	8.6		69.5	
cb	8.0			
$\frac{1}{4}$	7.9			
E	7.6		70.5	
$\frac{1}{4}$	2.5			
cb	2.1			

Plotted 10-6-28
C.B.H.

78.10

7

N.L.	6.5		71.6	
0+50				
N.L.	5.7		72.4	
cb	6.5			
$\frac{1}{4}$	2.0			
E	7.1		71.0	
$\frac{1}{4}$	7.2			
cb	7.2			
s.L.	7.4		70.7	
1+00				
s.L.	7.1		71.0	
cb	6.4			
$\frac{1}{4}$	6.2			
E	5.9		72.2	
$\frac{1}{4}$	5.5			
cb	5.0			
N.L.	4.3		73.8	
1+50				
N.L.	4.0		74.1	
cb	4.5			
$\frac{1}{4}$	4.8			
E	5.1		73.0	
$\frac{1}{4}$	5.3			
cb	5.5			
s.L.	6.2		71.9	
2+00				

78.10

s.l.	5.3	72.8
cb	4.7	
$\frac{1}{4}$	4.7	
E	4.4	73.7
$\frac{1}{4}$	4.0	
cb	3.8	
N.L.	3.3	74.8

2+50

N.L.	2.5	75.6
cb	3.2	
$\frac{1}{4}$	3.4	
E	3.5	74.6
$\frac{1}{4}$	3.8	
cb	4.3	
s.l.	4.7	73.4

2+60 = 2' Cem. Walk on South H Back ✓

Top Cem	4.28	73.82
---------	------	-------

3+00

s.l.	4.1	74.0
cb	3.6	
$\frac{1}{4}$	3.2	
E	2.9	75.2
$\frac{1}{4}$	2.5	
cb	2.2	
N.L.	1.8	76.3

3+50

78.10

8

N.L.	1.1	77.0
cb	1.8	
$\frac{1}{4}$	2.1	
E	2.2	75.9
$\frac{1}{4}$	2.7	
cb	3.1	
s.l.	3.5	74.6

4+12 = W.L. N.S.H. paving

s.l.	2.4	75.7
Top Cb.	2.52	75.58
gut - on paving	3.15	
$\frac{1}{4}$	2.55	
E	2.16	75.94
$\frac{1}{4}$	2.03	
gut	2.17	75.93
Top Cb.	1.49	76.61
N.L.	1.2	76.9

5-0' East of W.L. N.S.H.

N. Top cb.	0.78	77.32
s. Top Cb.	1.78	76.32

X section of Missouri from Cass to W.L.N.S.H.
 80' st. 20' cbs 10' $\frac{1}{4}$

62.08

9

61.97 = BM. infence

Station	0.11	62.08	
0+00 = E.L. Cass N.L.	8.4	53.7	
cb	9.4		
$\frac{1}{4}$	9.1		
E	8.6	53.5	
$\frac{1}{4}$	8.6		
cb	9.3		
s.L.	10.2	51.9	
0+50			
s.L.	9.6	52.5	
cb	9.2		
$\frac{1}{4}$	9.1		
E	8.9	53.2	
$\frac{1}{4}$	8.6		
cb	8.7		
N.L.	8.3	53.8	
1+00			
N.L.	7.4	54.7	
cb	7.9		
$\frac{1}{4}$	7.8		
E	8.2	53.9	
$\frac{1}{4}$	8.2		
cb	8.5		
s.L.	8.8	53.3	
1+50			

Plotted 10-6-28 C.B.H.

s.L.	7.3	53.8
cb	7.9	
$\frac{1}{4}$	7.6	
E	7.4	54.7
$\frac{1}{4}$	7.0	
cb	7.0	
N.L.	6.4	55.7
2+00		
N.L.	5.8	56.3
cb	6.5	
$\frac{1}{4}$	6.4	
E	6.6	55.5
$\frac{1}{4}$	6.9	
cb	7.2	
s.L.	7.7	54.4
2+50		
s.L.	7.1	55.0
cb	6.7	
$\frac{1}{4}$	6.6	
E	6.3	55.8
$\frac{1}{4}$	6.0	
cb	6.0	
N.L.	5.5	56.6
3+00		
N.L.	5.3	56.8
cb	5.7	

62.08

1/4	5.6	
E	5.8	56.3
1/4	6.0	
cb	6.1	
s.L.	6.5	55.6
	3+50	
s.L.	5.8	56.3
cb	5.6	
1/4	5.4	
E	5.4	56.7
1/4	5.3	
cb	5.2	
N.L.	5.0	57.1
	4+00	
N.L.	3.6	58.5
cb	4.0	
1/4	4.1	
E	4.4	57.7
1/4	4.4	
cb	4.6	
s.L.	4.9	57.2
	4+50	
s.L.	3.4	58.7
cb	3.5	
1/4	3.3	
E	3.1	59.0
1/4	2.8	

62.08

10

cb.	2.7	
N.L.	2.2	59.9
	4+99 = W.L. Dawes	- see Dawes st. x sec. for intec.
N.L.	1.4	60.7
cb	1.8	
1/4	2.0	
E	2.4	59.7
1/4	2.5	
cb	2.7	
s.L.	3.1	59.0
	0+00 = E.L. Dawes	
s.L.	1.9	60.2
cb	1.5	
1/4	1.4	
E	1.3	60.8
1/4	1.0	
cb	1.1	
N.L.	0.5	61.6
	8.11	70.08
	0+50	
N.L.	7.8	62.3
cb	8.8	
1/4	7.4	
E	8.6	61.5
1/4	8.5	
	61.97 = BM.	

7008

cb.	8.6	
s.L.	9.3	60.8
	1+00	
s.L.	8.7	61.4
cb	8.3	
½	8.1	
¾	7.8	62.3
¼	7.4	
cb	7.8	
N.L.	7.3	62.8
	1+50	
N.L.	6.2	63.9
cb	7.2	
½	6.9	
¾	7.0	63.1
¼	7.1	
cb	7.5	
s.L.	8.0	62.1
	1+00	
s.L.	7.1	63.0
cb	6.7	
½	6.4	
¾	6.3	63.8
¼	5.9	
cb	6.0	
N.L.	5.2	64.9

7008

11

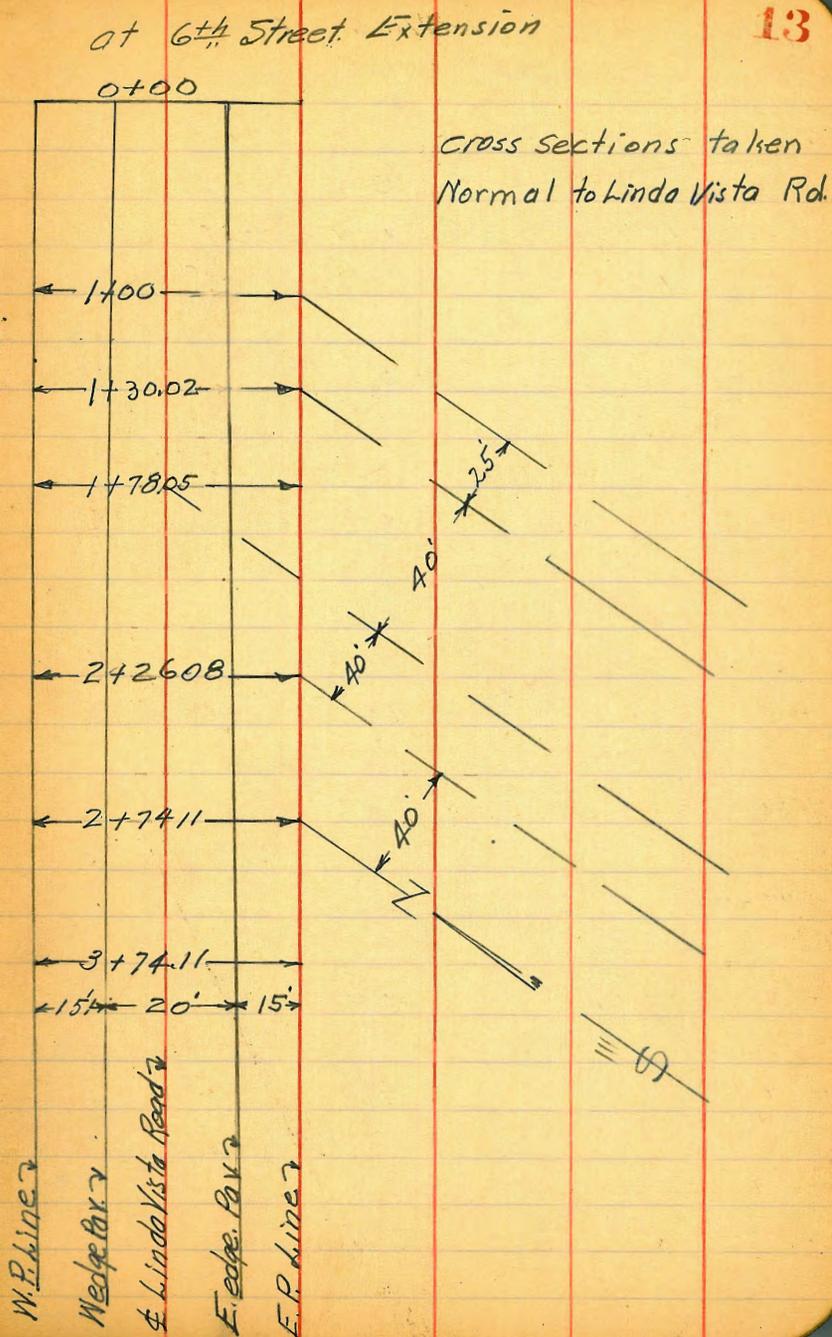
	2+50	
N.L.	4.1	66.0
cb	5.0	
½	4.9	
¾	5.1	65.0
¼	5.6	
cb	6.0	
s.L.	6.6	63.5
	2+75 = 3' com walk on North on line	
Top Com.	3.36	66.72
	3+00.	
s.L.	5.5	64.6
cb	5.5	
½	5.2	
¾	4.4	65.7
¼	4.4	
cb	4.1	
N.L.	3.3	66.8
	3+50	
N.L.	2.0	68.1
cb	3.0	
½	3.3	
¾	3.4	66.7
¼	4.2	
cb	4.6	
s.L.	4.4	65.7
	3+86	

S.L.	3.7	66.4
cb.	4.0	
$\frac{1}{4}$	2.5	
e	2.9	67.2
$\frac{1}{4}$	2.5	
cb	2.3	
N.L. on $\frac{1}{2}$ com. walks.	1.22	68.86
4 + 12.5 = W.L. N. Shore Highlands. = joining		
N.L.	2.6	67.5
Top Cb.	3.17	66.91
gut. on paving	3.90	66.18
$\frac{1}{4}$	3.70	
e	3.80	66.28
$\frac{1}{4}$	4.17	
gut	4.75	65.33
Top Cb.	4.13	65.95
S.L.	4.0	66.1
50 East of W.L. N.S.H.		
S Top Cb.	3.47	66.61
N. Top Cb.	2.5-1	67.57

Oct. 9-1928
Taylor X. Sec - Linda Vista Road
Cotton. R.E.

B.M.	ANA SWly cor. Linda Vista & Medford	353.68
2.016	355.696	
0.948	344.104	12.54 343.156
7.858	347.926	4.036 340.068
9.037	355.187	1.776 346.150
6.050	359.667	1.570 353.617
4.47	358.009	6.128 353.539

Sta	W.P. Line	W. edge Pav.	E. Pav.	E. edge Pav.	E.P. Line
0+00			3.96		
			354.05		
1+00	5.83	4.47	4.30	4.41	4.60
	352.18	353.54	353.71	353.60	353.32
1+30.02	6.15	4.56	4.44	4.53	5.09
	351.86	353.45	353.57	353.48	352.92
1+78.05	6.43	4.72	4.58	4.68	5.08
	351.58	353.29	353.43	353.33	352.93
2+26.08	6.80	4.86	4.79	4.89	5.36
	351.21	353.15	353.22	353.12	352.65
2+74.11	7.20	5.02	4.90	5.03	5.51
	350.81	352.99	353.11	352.98	352.50
3+74.11			5.24		
			352.77		



H.I.
99.65

S Line	3.7
	0+40
SLine	3.9
+20	10.1
run	11.7
+25	8.9
+28	8.0
+32	6.3
+42	4.4
+58	5.2
+62	7.5
+75	10.2
+79	12.1
+82 Bottom	13.5
+83	12.3
+85	11.5
+87	9.5
+120	2.4
	0+50
-100	2.8
-95	3.7
-85	10.1
-83 Bottom	14.0
-78	13.3
-73	10.5
-60	7.6

H.I.
99.65

-52	4.8
-25	4.9
-15	5.6
SLine	3.7
	0+75
SLine	4.4
+17	6.1
+26	10.4
+40	13.2
+53	11.5
+64	12.2
+66 Bottom	15.2
+68	15.2
+72	12.4
+86	8.6
+100	3.7
	0+88
SLine-70	8.2
-65	8.5
-58	11.9
-56 Bottom	16.1
-35	16.8
-27	12.6
-20	10.5
-10	5.6
SLine	4.5

15

42
49.65

1700

S Line		5.6	
+05		6.6	
+17		13.3	
+20		16.8	
+23		17.3	
+25		15.9	
+30		15.0	
+42		10.8	
+50		10.3	
	1+16 ⁴⁰	Right Angles to Back Ton.	
-50		9.~	
-35		11.7	
-23		16.0	
-20	Bottom	18.1	
-17		17.3	
-10		13.9	
S Line Δ		11.0	35.65
T.P.	5.77	44.51	10.85 38.80
	1+16 ⁴⁰	Right Angles To Forward Ton.	
S Line		5.8	
+10		9.~	
+17	Bottom	13.~	
+23		13.9	
+29		10.4	
+33		7.5	
+37		6.~	

H.I.
4457

1750

S-30		8.6	
-25		10.6	
-17		15.4	
-13	Bottom	17.1	
S Line		7.7	
	175		
S Line		6.0	
+05		8.1	
+20	Bottom	12.4	
+27		13.7	
+50		9.0	
	2+00		
-70		10.2	
-60		11.8	
-52		16.6	
-43	Bottom	19.3	
-3~		14.5	
-25		8.9	
S Line		4.~	
	2+35		
S Line		3.5	
+30		8.9	
T.P.	7.04	41.93	9.68 34.89
+60		15.4	
+67	Bottom	18.3	

H.I.
4193

+72		15.2
+85		8.7
		3+00
-60		10.7
-52		11.9
-42		18.6
-40		20.3
-35	Bottom	4.6
-25		16.8
-20		12.5
SLine		3.8
		3+40
SLine		11.1
+13		19.8
+15		22.8
+19	Bottom	22.9
+22		20.7
+30		17.0
+45		18.1
		3+65
-65		13.2
-55		15.5
-42		18.8
-37		23.1
-30	Bottom	23.6
-21		22.0

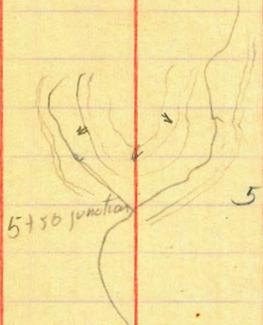
H.I.
4193

17

-14		13.0
SLine		8.7
TP	0:45	36.90
		5.48
		36.45
		9+50
SLine		11.
+20		10.2
+27		14.3
+37		18.7
+40		20.5
+46	Bottom	20.6
+49		17.2
+60		13.3
		9+75
-75		14.5
-46		18.3
-44	Bottom	20.4
-35		20.8
-25		14.7
-08		3.8
SLine		0.7
		5+00
SLine		0.3
+15		2.2
+36		11.4
+42	Bottom	21.1
+48		21.2
+75		20.7

H.I.
3690

+87		20.4
+89	Bottom	20.2
+92		19.9
+100		17.7
		5+25
-100		20.2
-80		22.4
-78	Bottom	24.5
-71		24.4
-70		20.2
-50		16.2
-35		10.5
-23		5.8
S. Line		1.0
		5+50
S. Line		3.3
+30		5.4
+42		9.3
+48		12.9
+50		16.3
+70		19.1
+93		21.5
+96	Bottom	25.3
+98		25.8
+100		24.9
+105		21.7



H.I.
3690

-105		5+68 23.6
-97		23.9
-95	Bottom	27.5
-90		22.8
-70		20.0
-53		16.1
-45		13.0
-40		9.4
-30		7.4
S. Line		6.2
		5+80
S. Line		8.3
+33		9.8
+42		14.3
+48		15.4
+60		21.5
+67		31.0
+82		30.6
+83		28.7
+100		24.9
		6+00
-100		19.1
-96		19.9
-89		31.9
-65		32.8
-50		29.8

18

HI
36.96

-46			22.9	
-33			18.2	
-29			13.0	
S.Line			9.8	
TP	111	25.76	12.25	29.65
			6+45	
S.Line			6.6	
+41			11.4	
+51			15.7	
+57 Bottom			22.9	
+61			22.9	
+65			17.0	
+72			12.8	
+80			10.5	
			6+75	
-90			10.7	
-72			14.2	
-62			20.6	
-59 Bottom			23.5	
-57 Bottom			23.5	
-55			18.9	
-50			18.3	
-47			15.9	
-30			12.1	
S.Line			5.5	
TP	213	16.94	10.95	14.81

HI
16.94
7+00

19

S.Line			0.7	
+35			3.4	
+52			6.2	
+62			11.0	
+65 Bottom			14.5	
+67 "			14.5	
+70			11.5	
+80			7.1	
+90			9.2	
			7+35	
-100			6.8	
-83			10.6	
-80 Bottom			13.3	
-68 "			13.6	
-66			11.3	
-60			8.4	
-40			5.1	
S.Line			1.3	
			7+50 Entrance of Ocean	
S.Line			3.5	
+33			7.4	
+38			10.6	
+66			11.6	
+70 Bottom			14.0	
+85 Bottom			14.0	
+100			12.5	

HJ

2-11

16.94

T.P.	12.79	27.26	2.47	14.47
T.P.	11.78	38.55	0.99 0.45	26.77
T.P.	11.83	50.03	0.35	38.20
T.P.	12.37	62.30	0.10	49.93
T.P.	12.61	74.16	0.75	61.55
			4.38	69.78

check out on
 BM NEBP
 Gen Tel + 10.7616
 8129

SL
 TP

Location Senter Man Hole
Franklin Between 30th & 31st St

33089
Sister

21

3

Franklin

Senter Man Hole
31st St

Flora's Cove 5020

" Flora's 4053

3084

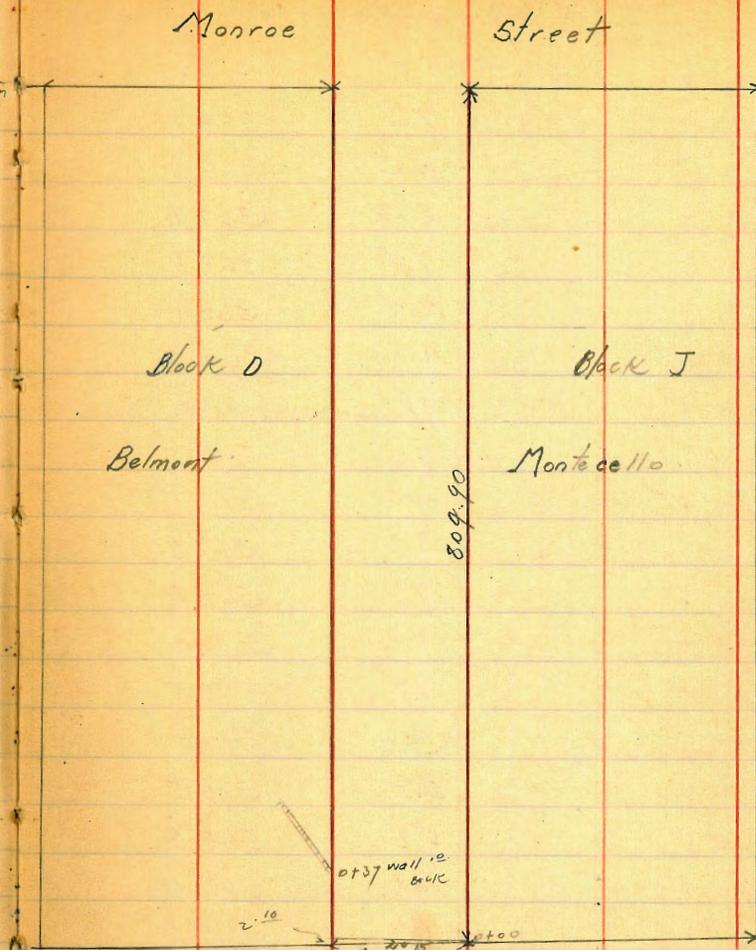
3
31

Bill Bliss
4/1/29

X Section Alley Block "D" Belmont
between 49th + Winona from Monroe
to El Cajon

BM	12.00	367.37	355.37	SW&P E/Open + 49 th
		Sec 4	40.15	
E Topcb		1.90	365.97	
G		2.07	365.30	
d		2.53	364.84	
G		2.41	364.96	
W Topcb		2.33	365.04	
		0+00	Seas sketch	
W		2.2	365.2	
E		2.2	365.2	
G		2.07	365.3	
E Topcb		1.90	365.97	
		0+02		
E		0.1	367.3	
E		1.7	365.7	
17		2.2	365.2	
W		2.0	365.4	
		0+05		
W		1.7	365.7	
+5		1.3	366.1	
E		1.3	366.1	
+4		0.8	366.6	
T.P.	9.50	376.15	0.72	366.65
E			86	367.6
		0+25		

Plotted 4/23/1929 - CBH



HI. - Elev
376.15

0+25

E	7.5	368.7
+5	8.5	367.7
Φ	8.8	367.4
+8	9.1	367.1
VX	10.1	366.1
+10	10.3	365.9

0+37 Concrete Wall on West

1st Back

8.60 367.55 /

0+40

VX	8.3	367.9
Φ	7.9	368.3
+6	7.2	369.0
E	6.7	369.5

0+60

E	5.7	370.5
+4	6.3	369.9
Φ	6.6	369.6
+5	6.6	369.6
VX	7.1	369.1

0+80

W	6.4	369.8
+5	5.8	370.4
Φ	5.8	370.4
+7	5.3	370.9
E	4.1	372.0

HI. - Elev
376.15

0+90 Residence on West

23

E	3.7	372.5
+3	4.5	371.7
Φ	5.0	371.2
+5	5.2	371.0
+7	5.8	370.4
VX	6.5	369.7

Door ^{of Res} 9th Back & Door

5.97 370.68 ✓

1+00

VX	6.0	370.2
+5	5.3	370.9
Φ	4.8	371.4
+7	4.1	372.0
E	3.8	372.9

1+20 Single Garage on West

E	2.9	373.3
+3	3.8	372.4
Φ	4.6	371.6
W	5.0	371.2
Φ	4.97	371.18 ✓

3.5 Back concrete floor

1+42 Single Garage on East

W	4.1	372.1
Φ	3.6	372.6
+7	3.6	372.6
E	3.3	372.9
Φ	3.0	373.2 ✓

2.5 Back Dirt floor

	+	#I 376.15	-	Elev
				1153 Single Garage on West ✓
3-5 Back		concrete floor	±	370 372.45
		1160		
E		2.5		373.7
±5		3.0		373.2
±		2.9		373.3
W		3.4		372.8
		1170		
W		2.9		373.3
±7		2.5		373.7
±		2.3		373.9
±5		1.7		374.5
E		1.0		375.2
		2100		
E		0.9		375.7
±5		1.2		375.0
±		1.4		374.8
W		1.5		374.7
		2125		
W		0.6		375.6
±		0.7		375.5
±6		0.3		375.9
E		0.0		376.2
±P	8.90	384.43	0.62	375.53
		2150		
E		7.9		376.5

	+	#I 384.43	-	Elev
				24
				8.2 376.2
				8.1 376.3
				8.1 376.3
		2175		
				7.5 376.9
				7.3 377.1
				7.27 377.16 ✓
				6.9 377.5
		3100		
				6.4 378.0
				6.4 378.0
				6.4 378.0
				6.6 377.8
				6.7 377.7
		3110		
				6.5 377.9
				6.3 378.1
				6.2 378.2
				6.0 378.4
		3135		
				5.9 378.5
				6.3 378.1
				6.6 377.8
		3150		
				6.4 378.0
				6.0 378.4

H.I.
38443

360. Fence
0.5 m alley

f

H.I.
38443

Elev

25

♂	5.6	378.8
E	5.1	379.3
	3775	
E	4.6	379.8
♂	4.9	379.5
+6	5.2	379.2
+7	5.7	378.7
N	5.7	378.7
	4100	
N	5.3	379.1
+4	5.3	379.1
+5	4.8	379.6
♂	4.5	379.9
+5	4.1	380.3
E	3.8	380.6
	4125	
E	3.9	380.5
♂	4.4	380.0
+5	4.4	380.0
N	4.9	379.5
	4150	
N	4.6	379.8
♂	4.2	380.2
+5	4.0	380.4
E	3.6	380.8
	4175	
E	4.0	380.4

460 End of page

♂	4.4	380.0
+5	4.3	380.1
N	4.4	380.0
T.P.	3.67	384.29
	3.81	380.62
	5100	
N	4.3	380.0
+5	4.1	380.2
♂	4.2	380.1
E	3.9	380.4
	5112	
E	3.9	380.4
♂	4.1	380.2
N	4.1	380.2
	5125	
N	4.1	380.2
+5	3.9	380.5
♂	3.9	380.5
E	3.7	380.6
	5150	
E	3.8	380.5
♂	4.1	380.2
N	4.4	379.9
	6100	
N	5.0	379.3
♂	4.8	379.5
+7	4.8	379.5

+ H.I.
389.29

E	45	379.8
	6+25	
E	50	379.3
+6	5.7	378.6
Φ	5.7	378.6
+6	5.5	378.8
W	5.8	378.5
	6+50	
W	6.3	378.0
+4	6.0	378.3
+6	6.5	377.8
Φ	6.6	377.7
+4	6.5	377.8
E	5.7	378.6
	6+7.5	
E	6.2	378.1
+4	6.9	377.4
Φ	7.1	377.2
W	6.9	377.4
	7+00	
W	7.3	377.0
Φ	7.4	376.9
+6	7.3	377.0
E	7.0	377.3
	7+11	
E	7.2	377.1

+ H.I.
389.29

- E/k

26

Φ	7.3	377.0
+6	7.4	376.7
W	7.7	376.6
	7+00	
W	7.9	376.4
Φ	7.3	377.0
E	6.7	377.6
	7+35	
E	7.3	377.0
Φ	7.7	376.6
W	7.7	376.6
	7+50	
W	7.5	376.8
+5	7.8	376.5
Φ	7.7	376.6
E	7.2	377.1
	7+75	
E	6.9	377.4
Φ	7.0	377.3
W	6.9	377.4
	8+00	
W	7.6	376.7
+4	7.4	376.9
+8	7.6	376.7
Φ	7.1	377.2
E	7.2	377.1

	+	HI 384.29	-	Elev	
E			8+047.1	377.2	
Φ			7.9	376.9	
+3			8.0	376.3	
W			7.9	376.4	
			8+09 ²⁰		S line of Monroe
W			8.9	375.4	
+5			8.4	375.9	
Φ			8.0	376.3	
+7			8.8	375.5	
Φ			8.8	375.5	
E Top ab			8.79	375.50 ↓	
					Elev on street ch. cutter
E-25 Top ab	on paving		8.61	375.68	
E-25 G			9.00	375.29	
E Top of PC - Alley Return			8.75	375.54	
E at PC of Albi Radies			9.10	375.19	
Set BM			4.91	379.38	S.E. Top Fire Hy. Wawona + Monroe
FP	6.70	389.00	1.99	382.30	
check BM			5.86	383.14	S.W. BP. El Cajon + 50 th .
				383.13	
					Δ error

B. H. Bliss
4/10/29

X Sections California St
Hawthorne to Juniper

75 St
12.65
12.75 19^s
SW B.P. India
+ Hawthorne

28

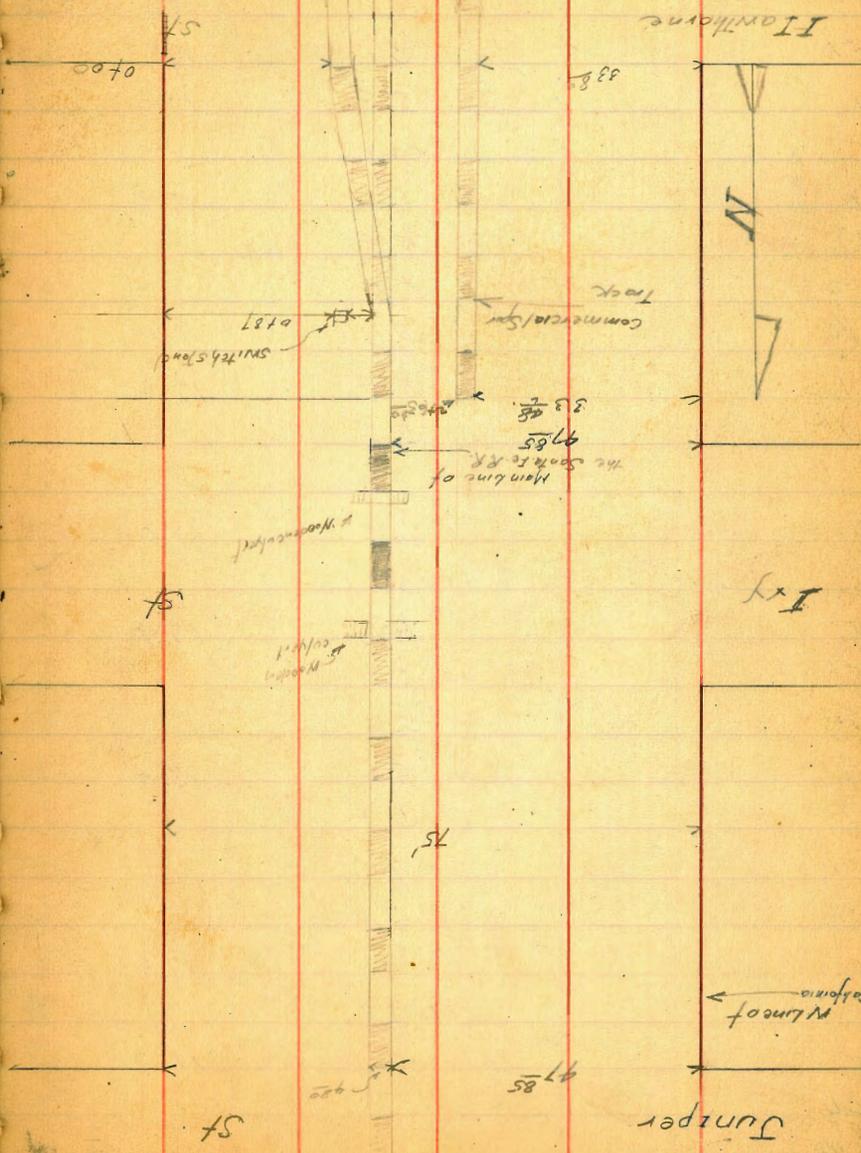
B.M.	2.37	47.37		45.00
T.P.	1.90	37.79	11.78	35.59
check BM			7.47	30.02
T.P.	1.18	26.18	12.49	25.00
Set BM	5.94	22.98	9.14	17.04

NW B.P. India
+ Hawthorne
SW B.P. Hawthorne
+ California

0700

W		5.6		16.4
W Top cb		5.96		17.02
c		6.43		16.55
1/4		5.43		17.55
+ 9 ⁵⁵ W Rail		4.92	18	18.06
1/2		4.75		18.23
+ 1/2 E Rail of West track		4.89		18.09 ✓
+ 10		4.89		18.09
1/4		4.91		18.07
+ 2 ¹⁵ Top Rail		4.87		18.11
+ 3 " "		4.86		18.12
+ 7 ²⁵ " "		4.89		18.12
cb		4.90		18.08
c		3.69		17.29
East end Top cb		4.79		18.19
		0706		
E		5.1		17.9
cb		5.2		17.8
1/4		5.5		17.5

Property lines plotted 4/23-1929 BH



H.I.
2298

ϕ	5.7	17.6
1/4	5.0	18.0
cb	5.2	17.8
N	5.7	17.6
	ot 25	
N	5.8	17.2
7	5.4	
cb	5.3	
1/4	5.3	
ϕ	5.7	17.6
1/4	5.5	
cb	5.6	
E	5.0	18.0
	ot 50	
E	5.2	17.8
cb	5.8	
1/4	5.6	
ϕ	5.5	17.5
1/4	5.2	
cb	5.2	
1/2	5.3	
N	5.7	17.3
	ot 75	
N	5.3	17.7
cb	5.1	
1/4	5.7	

47
+ 2.5
+ 27.2
+ 38.2
+ 42.4
+ 47.4

75
224
516
17.4

29

ϕ	5.6	
1/4	5.6	
cb	6.0	
E	5.3	17.7
	1700	
E	5.7	17.3
78	5.6	
cb	6.4	
73	6.3	
74	5.9	
725	5.26	17.72
1/4	5.7	
Rail	5.23	17.75 ✓
ϕ	5.5	17.5
1/4	5.4	
78	5.0	
cb	5.1	
N	5.2	17.8
	1425	
N	5.3	17.7
cb	5.3	
1/4	5.7	
74	5.7	
ϕ	5.8	17.2
1/4	5.9	
77	5.9	

	H.I.		
	2298		
t9	6.5		
t12	6.5		
c6	6.1		
5	6.0	17.0	
	14.45		
6	6.2	16.8	
t10	6.2		
c6	6.7		
t3	6.6		
t6	5.9		
1/4	5.9		
6	5.8	17.2	
1/4	5.4		
c6	5.6		
N	5.8	17.2	
T.P.	3.81	20.94	5.85
			17.13
			14.75
N	4.1	16.8	
c6	4.0		
t10	3.4		
1/4	3.3		
6	3.9	17.0	
1/4	3.9		
t7	4.0		
t9	4.7		
t11	4.8		

	H.I.		5/6/1
	20.94		
			30
			4.0
			2.9
			3.3
		17.6	
		27.00	
		3.6	17.3
		3.2	
		4.2	
		5.1	
		5.1	
		4.1	
		3.9	
		3.9	17.0
		3.4	
		3.9	
		4.4	
		4.2	
		5.0	15.9
		27.25	
		4.9	16.0
		4.3	
		4.0	
		3.5	
		3.4	
		4.1	16.8
		4.0	
		4.1	
		5.3	

H.I.
20.94

cb	5.3	
t3	4.7	
E	4.9	16.5
	2750	
E	5.4	15.5
cb	5.5	
t7	4.1	
1/4	4.0	
ϕ	4.2	16.7
1/4	4.2	
cb	4.7	
t9	4.6	
N	5.4	15.5

2763³⁰ End of Spur Track
West of Main line ✓

Top Rail

3.82

17.12

Top W Rail

3.84

17.10

see sketch for location ↑

2768

W	5.2	15.7
t6	5.0	
cb	5.0	
t5	5.0	
1/4	4.3	
ϕ	4.0	16.9
1/4	4.1	
t6	4.2	

H.I.
20.94

31

t1	5.6	
cb	5.7	
E	5.2	15.7
	2775	
E	5.1	15.8
t10	5.5	
cb	5.9	
t2	5.7	
t6	4.3	
1/4	4.1	
ϕ	4.0	16.9
1/4	4.7	
t5	5.0	
cb	5.3	
t5	5.1	
N	5.0	15.9
	2785	
W	5.1	15.8
cb	5.1	
1/4	5.5	
ϕ	5.4	15.5
t2	5.3	
t6	4.3	
1/4	4.2	
t6	4.3	
t10	5.0	

	HZ. 20.94	Elev		HZ. 20.94	N. Line of I.V.Y.	47.85 52.00 = 00	32
0 c6		5.7		W	45	16.4	
+2		6.0		c6	47		
B+4		5.2		1/4	47		
E		5.1	15.8	ϕ	46	16.3	
E	3100 ²³	S. Line of I.V.Y.		Top W Rail	3.9	17.02	✓
c6		4.2	16.7	1/4	43		
+5		4.1		Top E Rail	3.90	17.04	
+10		4.9		+6	4.4		
+11		5.9		+10	4.9		
c6		6.1		c6	5.4		
+1		5.9		+3	3.2		
+2		5.0		+8	1.0		
+4		4.8		E	2.1	18.8	
+8		4.2			0.10		
-5260 E Rail		3.70		E	3.3	17.6	
1/4		4.2		+5	3.2		
-9735 W Rail		3.70	17.24 ✓	+9	4.1		
+5		4.5		c6	5.2		
+17		5.3		+6	4.4		
+ϕ		5.5	15.4	1/4	4.5		
c1/4		5.6		+5	4.6		
+4		5.3		ϕ	5.1	15.8	
+6		5.0		+7	5.1		
c6		5.2		1/4	5.1		
W		5.3	15.6	c6	4.7		
				W	4.4	16.5	

	HZ 20.94	-	Elev
		0+25	
W		9.7	16.2
cb		5.2	
1/4		5.5	
¢		5.7	15.2
+3		5.6	
+7		4.6	
¢?		4.5	
+6		4.5	
+10		5.2	
cb		4.6	
+6		2.0	
E		2.3	18.6
		0+50	
E		1.3	19.6
+6		1.9	
cb		5.0	
+2		5.4	
+6		4.6	
1/4		4.6	
+9		4.6	
+6		5.1	
¢		5.2	15.7
1/4		5.5	
cb		5.4	
W		5.2	15.7

	HZ 20.94		
		0+75	
W		5.4	15.5
cb		5.3	
1/4		5.9	
¢		5.4	15.5
+5		5.3	
+8		4.7	
1/4		4.6	
+6		4.6	
+9		5.1	
1/4		4.7	
+7		1.8	
E		1.2	19.7
		1+00	
E		1.5	19.4
+5		1.5	
+10		3.3	
1/4		4.8	
+9		5.3	
+6		4.7	
1/4		4.7	
+4		4.7	
+8		5.4	
¢		5.5	15.4
1/4		5.4	
cb		5.3	

H.I.
20.94

W	5.5	15.4
W-Rail	4.17	16.77
E Rail	9.15	16.79
	11.5	
W	5.4	15.5
cb	5.1	
1/4	5.2	
Φ	5.2	15.7
+4	5.2	
+8	9.7	
1/4	4.7	
+2	9.7	
+9	5.3	
cb	4.3	
1/1	2.3	
E	2.0	18.9
	17.50	
E	2.0	18.9
+7	2.0	
1/4	4.1	
+3	3.2	
+5	5.3	
+7	5.0	
1/4	4.8	
+4	4.8	
+8	5.3	

H.I.
20.94

34

Φ	5.3	15.6
1/4	5.2	
W	5.4	15.5
T.P.	7.34	23.33
	4.95	15.99
	11.75	
W	7.8	15.5
+6	7.5	
cb	7.5	Rail 6.79 v 6.79
1/4	7.5	
Φ	7.7	15.6
+5	7.7	
+8	7.3	
1/4	7.3	
+6	7.2	
+9	7.8	
cb	7.9	
+3	6.6	
+8	6.3	
E	5.5	17.8
	21.00	
E	6.2	17.1
+5	6.2	
cb	7.2	
+3	7.7	
+6	7.3	
1/4	7.3	

HZ.
23.33

t4	7.3		cb
t8	7.6		t3
φ	7.8	15.5	t6
1/4	7.6		1/4
cb	7.5		t4
W	7.7	15.6	t8
Top E Rail for location see sketch	6.79	16.54	φ
Top W " Page 28	6.79	16.54	t8
	2425		1/4
N	8.3	15.0	cb
cb	7.7		W
1/4	7.8		
φ	7.7	15.6	W
t4	7.7		t5
t8	7.4		cb
1/4	7.4		1/4
t6	7.4		φ
t10	7.7		t6
cb	7.5		1/4
t7	7.4		t6
t8	5.7		t10
E	5.5	17.8	1/4
	2450		t3
5	5.0	18.3	t7
t4	5.4		t9
t5	6.9		5

t
HZ.
23.33

35

	7.3		
	7.7		
	7.4		
	7.4		
	7.4		
	7.8		
	7.8	15.5	
	8.0		
	7.8		
	8.0		
	8.2	15.1	
	2475		
	8.3	15.0	
	7.8		
	7.8		
	7.8		
	7.5	15.8	
	7.4		
	7.4		
	7.5		
	7.7		
	7.3		
	6.7		
	6.3		
	4.8		
	4.6	18.7	

23.33

2+88

E	4.8	18.5
t2	5.0	
t5	6.0	
cb	7.4	
t6	7.5	
1/4	7.4	
t6	7.3	
1/4	7.6	15.7
1/4	7.8	
cb	7.9	
N	7.9	15.4
	2+95	
Top cb	8.04	15.29
G	8.64	
t25	8.54	
t5	8.1	
cb	7.9	
1/4	7.8	
1/4	7.6	15.7
1/4	7.5	
cb	7.3	
t7	7.6	
G	7.64	
E. eq Topcb	7.06	16.27
	3+00	S line of Juniper
E Topcb	7.05	16.28

+

H.I.
23.33

36

E Gutter	8.47	14.86
t2 Bottom	8.44	14.89
t2 Top	7.03	16.30
cb	6.98	16.35
E Rail ⁵⁻²⁴	7.00	16.35
1/4	6.98	16.35
N Rail	6.97	16.36 ✓
1/4	7.28	16.05
1/4	7.60	15.73
cb	7.88	15.45
t10 Top	8.05	15.28
t10 Bottom	9.44	13.89
G	9.51	13.82
Top Cb W Prop line	8.10	15.23
Set BM	8.29	15.04
TP	12.25 34.38	120 22.13
Check BM N/W Kutter + Juniper	5.32	29.06
TP	13.23 47.07	0.54 33.84
check out on BM's N/BP	0.18	46.84
		46.87
		0.02 error

SN 727K
Juniper
CaliforniaIndia +
Juniper

Bill Bliss
9/10/29

X Sections Ivy St from the N line of
Kettner to N line of California St

+ H.I. - Elev

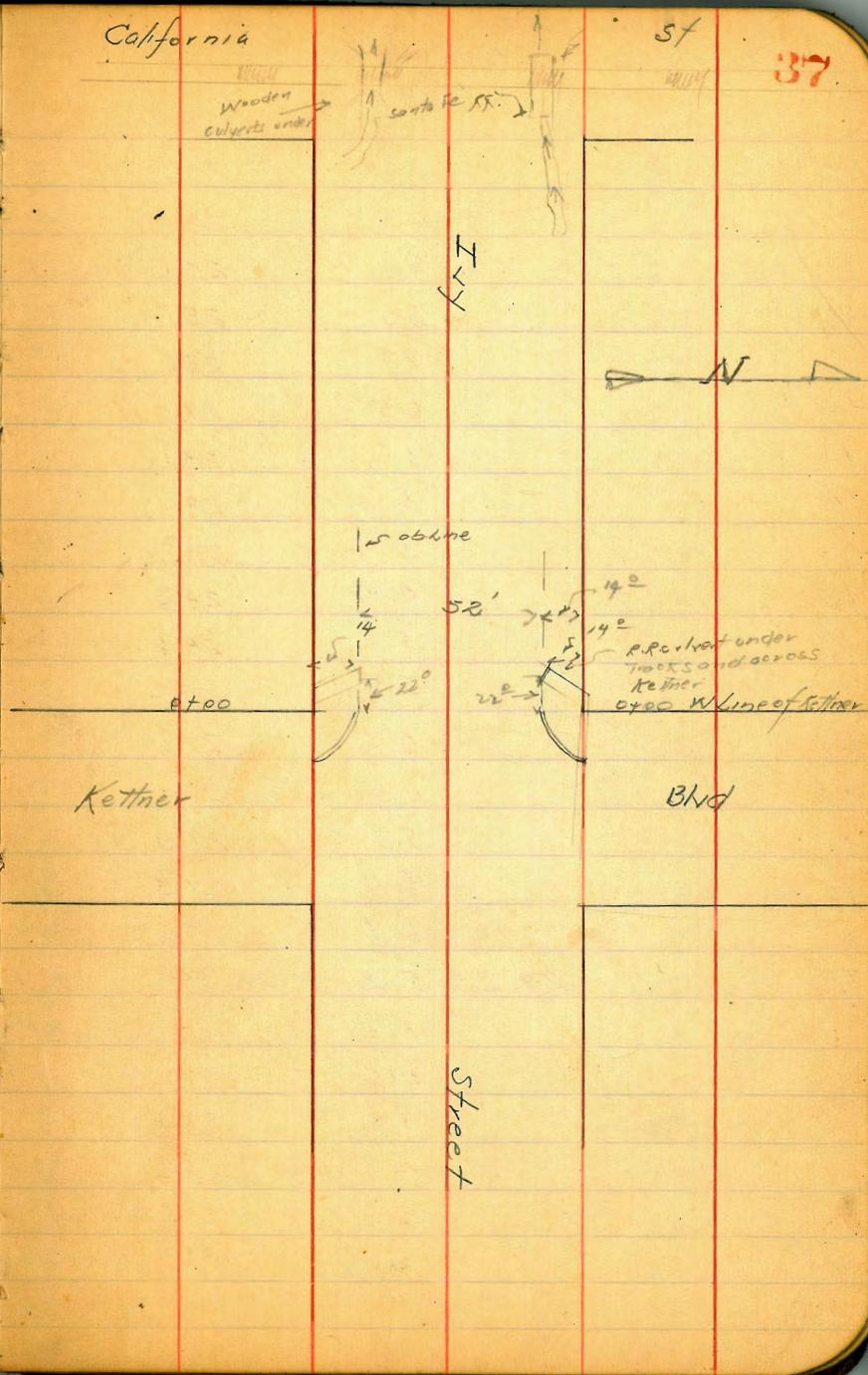
	H.I.	Elev
BM	3.72	30.02
		0+00
S		5.3 28.4
S Top cb		5.70 28.04
E		6.28 27.46
1/4		5.78 27.96
1/4		5.60 28.14
1/4		5.89 27.90
G		6.15 27.59
N Top cb		5.72 28.02
N		5.6 28.1
		0+03
N		5.7 28.0
1/6		6.0 27.7
cb		5.3 28.4
1/6		5.1 28.6
1/4		5.3 28.4
1/4		5.5 28.2
1/4		5.6 28.1
110 Top		6.2 27.5
110 Bottom		7.9 25.8
112 "		7.9 25.8
112 Top		6.1 27.6
cb		5.5 28.2
S		5.3 28.4

Property Lines Plotted 4/29-29-1914

California

St

37



	+	HI	-	Elev
		33.74	0.10	
S			5.0	28.7
+5			5.6	28.1
+1/2 Top			5.3	28.4
+1/2 Bottom			8.6	25.1
cb			8.6	25.1
+3			7.9	25.6
+4			6.5	27.2
+6			5.6	28.1
1/4			5.6	28.1
ϕ			5.0	28.7
+5			4.9	28.3
1/4			5.1	28.6
+5			5.4	28.3
+7			6.6	27.1
cb			6.6	27.1
+1			5.8	27.9
+9			4.4	27.3
N			6.1	27.6
TP	0.71	29.25	5.20	28.54
			0.22	R.P. Culvert on North
on cb line			2.16	27.09
Flow line			3.42	25.83
			0.22	R.P. Culvert on South
Top on cb line			2.36	26.89
Flow line			3.53	25.72

	+	HI	-	Elev
		29.25	0.25	
N			2.2	27.0
cb - Top			2.2	27.0
+1 Bottom			3.7	25.5
+4			3.5	25.7
+6 Top			1.1	28.1
+9			1.1	28.1
1/4			0.6	28.6
+7			0.3	29.0
ϕ			0.8	28.4
+10			1.5	27.7
1/4			1.5	27.7
+5			1.4	27.8
+9			2.9	26.3
+10			4.5	24.7
cb Bottom			4.7	24.5
cb Top			2.2	27.0
+4			1.4	27.8
+9			1.8	27.4
S			1.1	28.1
			0.50	
S			3.3	25.9
+5			3.4	25.8
+10			3.0	26.2
+11 Top			3.1	26.1
+11 Bottom			5.3	24.0

	+	HI 29.25	-	Elev
c6			5.3	24.0
t2			5.1	24.1
t4			4.0	25.2
t9			2.5	26.7
1/4			2.4	26.8
t6			2.6	26.6
φ			2.3	26.9
t5			2.1	27.1
1/4			1.8	27.4
t5			1.4	27.6
t8 Top			2.6	26.6
t8 Bottom			4.7	24.5
c6			5.0	24.2
t0.5			3.5	25.7
t4			3.2	26.0
N			3.1	26.1
		0.63		
N			3.7	25.5
t10			3.6	25.6
t12			5.2	24.0
c6			5.4	23.8
t1 Bottom			5.4	23.8
t1 Top			3.6	25.6
t5			2.5	26.7
1/4			2.8	26.4
φ			3.1	26.1

	+	HI 29.25	-	Elev	39
			3.5	25.7	
			4.3	25.0	
			4.8	24.4	
			5.1	24.1	
			5.6	23.6	
			5.8	23.4	
			5.6	23.6	
			4.4	24.8	
			4.3	24.9	
		0.75			
			5.3	23.9	
			5.3	23.9	
			5.4	23.8	
			6.3	22.9	
			5.9	23.3	
			4.8	24.4	
			4.3	25.0	
			4.3	25.0	
			3.8	25.4	
			3.4	25.8	
			3.5	25.7	
			3.2	26.0	
			4.2	25.0	
			5.9	23.3	
			5.9	23.3	
			6.4	22.8	

#	H.I. 29.25	-	Elev
+6 Top	4.9		24.8
N	4.4		24.8
	0.87		
N	5.2		24.0
+7 Top	5.1		24.1
+7 Bottom	7.8		21.4
+11	8.1		21.1
cb Bottom	9.1		20.1
+11 Top	4.8		24.4
+5	4.1		25.1
1/4	4.2		25.0
ϕ	4.3		24.9
1/4	4.7		24.5
+9	5.7		23.5
+11	6.9		22.3
+12	6.0		23.2
cb	5.8		23.4
S	8.4		22.8
	14.00		
S	7.5		21.7
+6	6.8		22.4
+11	6.6		22.6
cb	7.3		21.9
+3	6.7		22.5
+9	6.0		23.2
1/4	5.8		23.4

#	H.I. 29.25	-	Elev
ϕ	5.1		24.1
1/4	5.1		24.1
+9 Top	5.1		24.1
+9 Bottom	9.5		19.7
cb	10.0		19.2
+5	8.6		20.6
+6	6.6		22.6
+7	5.7		23.5
N	5.6		23.6
	14.25		
N	7.2		22.0
+7 Top	7.3		21.9
+7 Bottom	10.7		18.5
cb Bottom	10.7		18.5
cb Top	6.9		22.3
+6	6.7		22.5
+9	6.1		23.1
1/4	6.5		22.7
+3	6.7		22.5
ϕ	6.5		22.7
+7	7.3		22.0
1/4	7.6		21.6
+4	8.1		21.1
cb	8.2		21.0
+11	9.1		20.1
+12	9.0		20.2

	+	HI 29.25	-	Elev		+	HI 29.25	-	Elev
t3			8.4	20.8	t3 Top			9.3	20.0
t7			8.4	20.8	t3 Bottom			11.1	18.1
S			9.2	20.0	t11			11.7	17.5
			11.40		cb			11.7	17.5
S			10.0	19.2	t2 Bottom			11.7	17.5
t8			9.6	19.6	t3 Top			9.2	20.0
t14			8.8	20.4	t4			8.2	21.0
t12			9.9	19.3	t6			8.2	21.0
cb			10.0	19.2	Φ			8.6	20.6
t1			9.3	20.0	t7			8.8	20.4
t7			9.2	20.0	t4			9.9	19.3
t4			8.7	20.5	t12			10.0	19.2
t7			8.5	20.7	cb			10.6	18.6
t9			7.6	21.6	t1			10.5	18.7
Φ			7.8	21.4	t2			9.7	19.5
t4			7.6	21.6	t7			9.7	19.5
t5			7.1	22.1	S			10.3	18.9
t9			8.2	21.0			17.70		
t10			9.6	19.6	S			12.1	17.1
cb			10.1	19.1	t7			11.7	17.5
t3			11.2	18.0	cb			11.8	17.4
t7 Bottom			11.2	18.0	t3			12.1	17.1
t8 Top			8.2	21.0	t5			12.2	17.0
N			7.9	21.3	t9			11.2	18.0
			11.50		t4			11.1	18.1
N			8.6	20.6	Φ			10.4	18.8

	+	H.I.	-	Elev		+	H.I.	-	Elev
1/4		29.25	10.8	18.4	+10		21.72	5.1	16.6
+9 Top			11.5	17.7	1/4			4.9	16.8
+9 Bottom			12.6	16.6	ϕ			4.6	17.1
cb			12.9	16.3	1/4			4.2	17.5
+3			12.4	16.8	+7 Top			4.0	17.7
+4			11.6	17.6	+7.5 Bottom			6.8	14.9
N			10.5	18.7	cb			6.6	15.1
T9	347	21.72	11.00	18.25	+3			4.3	17.4
			17.75 R.R. Prof Way line		N			4.4	17.3
N			3.0	18.7			2100 E line of California		
+5			3.0	18.7	N			3.0	18.7
+10			4.4	17.3	+11			2.9	18.8
+11			5.2	16.5	cb			6.1	15.6
cb			5.5	16.2	+3 Bottom			6.6	15.1
+5 Bottom			5.1	16.6	+3 Top			4.5	17.2
+5 Top			3.9	17.8	+9			2.6	19.1
1/4			4.0	17.7	1/4			3.3	18.4
ϕ			3.9	17.8	ϕ			4.9	16.8
1/4			4.1	17.6	1/4			5.0	16.7
+4			5.1	16.6	+8			5.7	16.0
cb			4.9	16.8	+9			6.6	15.1
S.			4.7	17.0	+12			6.0	15.7
		17.92			cb			5.3	16.4
S			5.3	16.4	+7			4.6	17.1
cb			5.8	15.9	S			5.0	16.7
+6			5.9	15.8					

75.57
12.65
12.75/45

+	HI 21.72	-	Elev
	E Line	+ 9	
S		5.1	16.6
cb		5.3	16.4
+1		6.7	15.0
+5		7.0	14.7
+6		5.0	16.7
1/4		5.0	16.7
¢		4.3	17.4
1/4		2.4	19.3
+7		2.9	18.8
+10		4.7	17.0
+11		6.6	15.1
cb		6.5	15.2
+4		2.3	19.4
N		1.9	19.8
	E Line + 10		
N		4.9	16.8
+10		5.3	16.4
+13		6.6	15.1
cb flowline of RR culvert		7.9	13.8
+3 " " " "		8.0	13.7
+4		4.7	17.0
1/4		4.3	17.4
¢		5.3	16.4
1/4		5.4	16.3
+5		5.5	16.2

+	HI 21.72	-	Elev
+10	flowline Wooden Culvert	8.0	13.7
cb	" " " "	8.0	13.7
+1		6.7	15.0
+6		5.5	16.2
S		6.0	15.7
	E cb		
S		6.8	14.9
cb		8.0	13.7
+3		8.0	13.7
+3.5		6.7	15.0
+9		5.9	15.8
1/4		5.9	15.8
¢		5.6	16.1
1/4		5.4	16.3
+10 Top		5.5	15.2
+10 Bottom		8.0	13.7
cb "		8.0	13.7
cb Top		5.8	15.9
N		6.0	15.7
TP	5.73	21.55	5.90
		E cb + 4	15.82
N		5.3	16.3
cb		5.2	16.4
1/4		5.3	16.3
¢		5.5	16.1
1/4		5.3	16.3

HL
2155

cb	5.2	16.4
S	5.5	16.1
	Ecb + 7	
+S	4.9	16.7
+cb	5.0	16.6
+1/4	5.1	16.5
Φ	5.0	16.6
1/4	5.0	16.6
cb	5.0	16.6
+N	5.0	16.6
	E 1/4	
N	5.0	16.6
cb	5.0	16.6
1/4	4.9	16.7
Φ	4.9	16.7
1/4	4.9	16.7
cb	4.9	16.7
S	4.8	16.8
	E 1/4 + 12	
S	6.1	15.5
+S	5.1	16.5
+11	5.3	16.3
cb	5.6	16.0
1/4	5.4	16.2
Φ on Ground	5.4	16.2
" on Rim Mn Hole	5.2	16.33

HL
2155

44

17	5.9	16.2	
1/4	5.3	16.3	
cb	5.6	16.0	
+S	4.9	16.7	
N	5.2	16.4	
	Φ		
N	5.2	16.4	
17	4.9	16.7	
cb-Top	6.0	15.6	
+0.5 flowline P. Knot	8.1	13.5	
+3.5 Bottom	8.2	13.4	
+4.0 Top	6.2	15.4	
+7	5.3	16.3	
1/4	5.2	16.4	
Φ	5.4	16.2	
1/4	5.4	16.2	
+7	5.3	16.3	
+9	6.1	15.5	
	+9.5 Bottom	8.1	13.5
cb	8.1	13.5	
+11 Top	5.8	15.8	
+4	5.2	16.4	
+9	5.2	16.4	
S	6.2	15.4	
	W 1/4		
S	6.2	15.4	

HZ
2155

t10	57	15.9
t12	7.6	14.0
cb	8.1	13.5
t3	7.7	13.9
t5	5.4	16.2
1/4	5.2	16.4
ϕ	5.4	16.2
1/4	5.1	16.5
t3	8.2	13.4
t6	7.9	13.7
t9	6.6	14.0
t10	5.0	16.6
cb	4.9	16.7
N	5.4	16.2
	W 1/4 + 3	
N	5.4	16.2
cb	5.0	16.6
t6	5.1	16.5
1/4	4.9	16.7
t3	4.8	16.8
ϕ	5.3	16.3
1/4	5.6	16.0
t5	5.6	16.0
t7	6.8	14.8
t10	8.1	13.5
cb	8.0	13.6

HZ
2155

t3	6.7	14.9
t4	5.7	15.9
s	6.0	15.6
	W 1/4 + 7	
s	5.7	15.9
cb	5.6	16.0
1/4	5.8	15.8
ϕ	5.5	16.1
t9	5.1	16.5
1/4	5.0	16.6
t9	4.9	16.7
cb	5.1	16.5
N	5.4	16.2
	W cb	
N	5.3	16.3
t7	5.0	16.6
cb	9.9	16.7
1/4	5.4	16.2
ϕ	5.4	16.2
1/4	5.7	15.9
cb	5.5	16.1
s	5.6	16.0
	W cb + 4	
s	5.7	15.9
cb	5.6	16.0
1/4	5.7	15.9

#I
21.55

+5	5.7	15.9
♀	5.2	16.4
+9	5.2	16.4
+6	8.1	13.5
+12	8.4	13.2
1/4	6.7	14.9
+6	4.9	16.7
cb	4.7	16.9
N	5.2	16.4
W/cb+7		
N	5.2	16.4
+9	4.7	16.9
cb	4.6	17.0
+8	4.6	17.0
1/4	7.2	14.4
+2	8.6	13.0
+7	8.2	13.4
+9	5.0	16.6
♀	5.0	16.6
+10	5.7	15.9
1/4	5.6	16.0
cb	5.7	15.9
S	5.6	16.0
W line of California		
S	5.0	16.6
+8	5.0	16.6

#I
21.55

S.P. 11.6
S.S. 12.4

16

+10	6.5	15.1
+12	8.6	13.0
cb	9.0	12.6
+3	7.8	13.8
+6	5.7	15.9
1/4	5.3	16.3
♀	5.1	16.5
+2	5.1	16.5
+3	7.4	14.2
+6	8.9	12.7
1/4	7.3	14.3
+2	4.6	17.0
cb	4.8	16.8
N	5.1	16.5
J.P.	5.16	22.22
4.49	17.06	
check BM SW Calif return	5.20	17.02

5-16-29 Miller
 X See Alley Bet BIK B. Watkins & Biddle
 + BIK A Burlingame
 See Page 47. for Plat.

BM.	4.01	293.72	289.71	s.c. 30 th + Kalmia
		00 = E. Line 30 th St	(18.73 wide)	
N. ent. cl on Puchlo line	4.40	289.32		
" pavmt.	4.96	288.76		
4 "	5.25	288.47		
5 "	5.21	288.51		
+ 0.3 "	5.21	288.51		
+ 0.4 = N. edge ent. walk running E+W	4.98	288.74		
	4.6.	(18.74 wide)		
S-0.4 N. edge ent. walk	4.70	289.08		
5	5.0	288.7		
4	5.1	288.6		
+ 3	5.0	288.7		
+ 7	4.2	289.5		
N.	4.2	289.5		
	30'.E.	(18.85 wide)		
N	3.7	290.0		
+ 3	3.8	289.9		
+ 5	4.9	288.8		
4	4.9	288.8		
5	4.7	289.0		
+ 0.3 ent. walk	4.77	288.95		

Plotted 5/20-1929

293.72
 55'.E (18.94 wide)

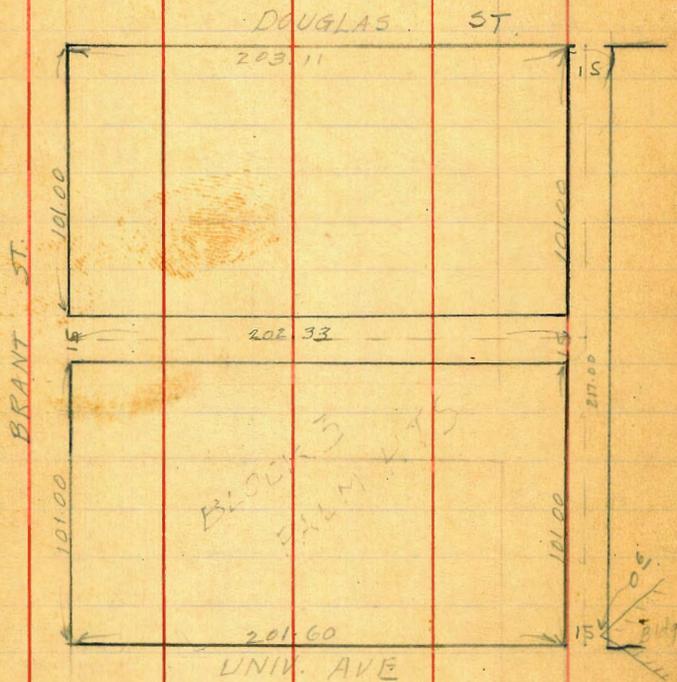
48

S-0.2 - ent. walk	4.77		
5	4.8	288.9	
4	4.8	288.9	
N. = P.L.	4.4	289.3	
83'.E = W. Line garage on S. dirt floor		(Alley 19.06 wide)	
N.	4.7	289.0	
4	4.9	288.8	
0.66 N. of S. line = N. edge garage	4.9	288.8	✓
5.	4.9	288.8	
99'.E = E. End. above garage		(Alley 19.13 wide)	
5.	5.0	288.7	
0.63 N. = N. edge garage	4.9	288.8	✓
4	4.9	288.8	
N.	4.9	288.8	
101'.E = W. End. ent. walk on S. running E+W.		(Alley 19.14 wide)	
0.54 N. of S. line = N. edge walk.	5.1	288.6	✓
137'.E = E. End. above ent. walk		(Alley 19.19 wide)	✓
N	4.9	288.8	
6	5.1	288.6	
0.70 N. of S. line = N. edge walk.	5.1	288.6	
5	5.1	288.6	
170'.E		(Alley 19.40 wide)	
5	4.8	288.9	
4	4.9	288.8	
N	4.9	288.8	

	293.72		
(Alley 19.51) ^{wide} 198'E = Double garage on S. 8.6 Back cmt. floor			
N		5.0	288.7
⊕		5.7	288.3
S		5.4	288.1
+ 6.6 = cmt. Apron		5.4	288.3
+ 8.6 = garage		5.3	288.4
T.P.	5.77	294.13	5.36 288.36
		240'E.	(19.68 wide)
S-S		7.0	287.1
S		6.5	287.6
⊕		6.1	288.0
N.		4.7	289.4
		275'N	(19.81 wide)
N		5.2	288.9
⊕ on N.H.		5.8	288.3
⊕ + 9		6.4	287.7
S.		7.1	287.0
		300'E	19.90 wide
S		6.8	287.3
⊕		6.0	288.1
+ 5		5.0	289.1
N		4.8	289.3
		330'E.	20.02 wide
N		4.5	289.6
C		5.1	289.0
S		5.6	288.5

	294.13		
370'E = garage on N. cmt. floor			
S		5.3	288.8
⊕		4.7	289.4
0.3 S of N. line = cmt. Apron		4.30	289.83
N.		4.26	289.87
N + 3 = garage floor		3.9	290.2
		400'E garage on S. cmt. floor	1.7 Back (Alley 20.30 wide)
N.		4.5	289.6
⊕		4.8	289.3
S		4.9	289.2
S + 1.7 = floor		5.0	289.1
		425'E.	(Alley 20.40 wide)
S		4.6	289.5
⊕		4.7	289.4
+ 4		4.7	289.4
N.		4.3	289.8
		465'E.	(Alley 20.55 wide)
N		3.4	290.7
⊕		4.1	290.0
S		3.8	290.3
		500'E	(20.69 wide)
S		3.8	290.3
⊕		3.6	290.5
N		3.3	290.8

X sec Alleys BK 3 Palm Hts.
7/26/29 London.



NW Douglas
1/2 mile

N-S Alley

BM	805	276.05	268.00
South oblique Douglas			
WL topch		5.55	270.50
WL gutter		6.06	269.99
± gut		5.88	270.17
EL gut		5.67	270.38
EL topch		5.07	270.96
D + 00 = 34 Douglas			
EL topch		4.99	271.06
EL Pav		5.28	270.82
± Pav		5.59	270.46
WL Pav		5.60	270.45
WL topch		5.24	270.81
D + 05			
WL		5.1	270.95
+2		5.0	271.05
±		5.4	270.65
+6		4.8	271.25
EL		4.4	271.65
D + 10			
EL		3.8	272.25
+1		4.5	271.55
+5		5.1	270.95
±		5.0	271.05
WL		5.2	270.85

Plotted 9-29-29
T.G.H.

N⁵ Alley Blk 3 Palm Hts

0+27	276.05		
W.L.	5.6	270.45	
+4	5.1	270.95	
±	5.1	270.95	
+4	4.9	271.15	
EL	4.0	272.05	
0+21 = Garage door 2.3' E. cur. floor			
	3.35	272.70	
0+37			
EL	4.2	271.85	
±	4.8	271.25	
+3	4.6	271.45	
+6	5.5	270.55	
W.L.	5.6	270.45	
0+50			
W.L.	5.8	270.25	
+4.5	5.3	270.75	
±	5.3	270.75	
EL	4.8	271.25	
0+75			
EL	5.5	270.55	
+5	6.0	270.05	
±	6.0	270.05	
+2.5	6.2	269.85	
W.L.	6.2	269.85	

Alley Blk 3 Palm Hts

276.05

52

0+89 = garage 5' 2" E. earth floor			
	5.5	270.55	
1+01 = NLE-W Alley			
W.L.	7.0	269.05	
+3	6.7	269.35	
±	6.5	269.55	
EL	5.8	270.25	
1+08.5 = ± E-W Alley			
EL	6.4	269.65	
±	6.8	269.25	
W.L.	7.2	268.85	
1+16 = SL E-W Alley			
W.L. fence 0.5 m.	7.3	268.75	
+5	7.3	268.75	
±	7.1	268.95	
EL	6.7	269.35	
1+25			
EL	7.1	268.95	
+5	7.4	268.65	
±	7.4	268.65	
+3	7.6	268.45	
W.L. fence 0.5 m.	8.0	268.05	
1+50			
W.L. fence 0.5 m.	8.5	267.55	
+1	8.2	267.85	
+5	8.5	267.55	
±	8.2	267.85	

Alleys BIK 3 Palm Hts

1+50	276.05		
EL	7.8	268.25	
1+57 = N end Double garage	7.5	E Conc. floor	
	8.01	268.04	
1+82 = S end same garage	7.2	E	
	8.02	268.03	
1+75			
EL	8.7	267.35	
±	9.2	266.85	
w.L. fence 0.5 m.	9.0	267.05	
2+00			
w.L.	9.8	266.25	
±	10.0	266.05	
EL - fence 0.5 m.	9.7	266.35	
2+05			
EL fence 0.5 m.	10.0	266.05	
+3	10.3	265.75	
±	10.5	265.55	
w.L.	10.7	265.35	
2+17 = N.L. Univ. Ave.			
w.L.	15.8	260.25	
±	15.3	260.75	
+4	13.4	262.65	
+5	11.7	264.35	
E.L.	11.2	264.85	

Alleys BIK 3 Palm Hts

276.05

EW Alley

53

0+00 = w.L. of N-5 Alley			
S.L. fence 0.5 m.	7.3	268.75	
+2	7.1	268.95	
±	7.2	268.85	
+4	6.9	269.15	
N.L.	7.0	269.05	
0+11			
N.L.	7.6	268.45	
+3	7.8	268.25	
+5	8.0	268.05	
±	7.9	268.15	
+3	8.0	268.05	
S.L. fence 0.5 m.	7.9	268.15	
0+18			
S.L. fence 0.5 m. (cut fence)	8.1	267.95	
+4	8.2	267.85	
±	7.7	268.35	
N.L.	7.8	268.25	
Conc. Walk at 0+21 on S.L. ^{3' wide}	8.14	267.91	
" " " 0+36 on S ^{2' wide}	8.26	267.79	
0+43 = ± garage 5' S curb floor			
	8.8	267.25	
0+50			
N.L.	8.1	267.95	
±	7.9	268.15	
S.L.	8.2	267.85	
Conc. Walk at 0+59 ^{2.5' wide} 1.8' S	8.32	267.73	

0+06 =	End. Double garage	5.2's	earth floor.		
		8.1	267.95		
0+87 =	West side garage	5.3's			
		8.2	267.85		
0+75					
S.L.		8.18	267.87		
+6		7.8	268.25		
±		7.9	268.15		
+5.5		8.1	267.95		
N.L.		7.9	268.15		
Concrete at 96	2.5 wide	1.2's	8.33	267.72	
T.P.	4.12	272.21	7.76	268.09	
1+00					
N.L.		4.0	268.21		
+2		4.3	267.91		
±		4.1	268.11		
+4		4.2	268.01		
S.L.		4.5	267.71		
1+09 =	± garage	7.3' N	Concrete floor		
		3.87	268.34		
1+25					
S.C.		4.7	267.51		
+1		4.3	267.91		
+5		4.4	267.81		
±		4.4	267.81		
N.L.		4.3	267.91		

1+50	272.21.		
N.L.		4.6	267.61
±		4.7	267.51
S.L.		4.3	267.91
Concrete at 146	2.5 wide	1.3' N	4.80
1+75			
S.L.		5.0	267.21
+4		5.2	267.01
±		5.1	267.11
N.L.		4.9	267.31
1+92			
N.L.		5.3	266.91
+5		5.4	266.81
±		5.5	266.71
S.L.		5.2	267.01
2+02 ³³	± EL. Brant		
S.L. top cb		5.59	266.62
S.L. Pav.		5.85	266.36
± Pav		5.78	266.23
N.L. Pav		5.78	266.43
N.L. top cb		5.53	266.68
East cb line Brant			
N.L. top cb		5.65	266.56
N.L. gutter		6.16	266.05
± pit		6.20	266.01
S.L. pit		6.19	266.02
S.L. top cb		5.72	266.49

60' wide
10' chs
10' 1/4s.

29th St X sec Broadway to F St 8-14-29
mills

176.18
3.11
183.07 B.M. B.P. SW. R 9th + Broadway.
186.18

55

B.M. Mon	10.87	186.18	175.31	N. W. 29 th & E. Sts
		00 = S. Line Broadway	184.08	
w.		2.16	183.13	
+ R.S. = W. edge cmt. walk.		3.05	183.10	
+ 7.5 = E. Edge cmt. walk.		3.08	183.02	
cmt. ch		3.16	182.34	
gutter paymt.		3.84	182.49	
1/4 "		3.69	182.45	
1/4 "		3.73	182.10	
1/4 "		4.08	181.61	
gutter "		4.57	182.13	
cmt. ch		4.05	182.13	
+ R.S. = W. edge cmt. walk.		4.05	182.15	
+ 7.5 = E. " " "		4.03	182.18	
E.		4.0		
	2'.3			
E		4.1	182.1	
ch		4.1	182.3	
1/4		3.9	182.6	
C		3.6	182.6	
1/4		3.6	182.6	
+ 3		3.6	184.3	
ch		1.4	184.3	
w.		1.9		
	15'.3			
w		2.6	183.6	
ch		2.1	184.1	
+ 7		1.8	184.4	

Plotted 8-19-29 - CBH

1/4	2.8	183.4
1/4	3.2	183.0
1/4	2.8	183.4
ch	3.2	183.0
C	4.2	182.0
	45'.5	
C	6.7	179.5
ch	6.3	179.9
1/4	4.8	181.4
1/4	4.4	181.8
1/4	4.3	181.9
ch	3.9	182.3
w.	3.5	182.7
	45'.5	
w	6.4	179.8
ch	6.4	179.8
1/4	6.2	180.0
1/4	6.0	180.2
+ 6	6.2	180.0
1/4	8.0	178.2
ch	9.0	177.2
+ 6	9.4	176.8
C	8.5	177.7

186.18
82 S.

-5	9.7	176.5	cl
E	10.5	175.7	W
+4	11.4	174.4	
cl	11.8	174.4	W
"4	10.8	175.4	cl
±	9.0	179.2	"4
"4	7.4	178.8	±
cl	7.6	178.6	"4
W	7.8	178.4	+2

100.5

W	8.2	178.0	E
cl	8.5	177.7	+30
"4	8.3	177.9	
+8	8.1	178.1	-15
±	9.2	177.0	E
"4	15.3	170.9	cl
cl	16.3	169.9	"4
E	17.4	168.8	±
+10	17.3	168.9	"4

115.5

-20	22.4	163.8	cl
E	20.1	166.1	W
cl	18.4	167.8	W
"4	16.1	170.1	cl
±	9.3	176.9	"4
"4	9.2	177.0	±

186.18

29th St.

56

9.1	177.1
8.5	177.7
125.5	
8.2	178.0
9.2	177.0
9.5	176.7
9.9	176.3
11.8	174.4
16.1	170.1

18.0 168.2

20.6 165.6

25.0 161.2

141.5

16.1 170.1

14.5 171.7

12.7 173.5

11.4 174.8

10.3 175.9

9.4 176.8

8.6 177.6

7.2 179.0

165.5

6.3 179.9

9.1 177.1

9.6 176.6

10.0 176.2

186.18
165'.S. (con)

E. 1/4	11.0	175.2
cb.	12.3	173.9
E.	13.0	173.2
+ 5	13.0	173.2

180'.S.

- 5	12.7	173.5
E.	12.4	173.8
cb.	11.3	174.8
1/4	10.6	175.6
1/4	10.2	176.0
1/4	9.3	176.9
cb.	6.9	179.3
W.	6.0	180.2

200'.S.

W.	5.8	180.4
cb.	6.4	179.4
1/4	9.4	176.8
1/4	10.0	176.2
1/4	10.0	176.2
cb.	11.5	174.7
E.	12.0	174.2

220'.S.

E.	11.4	174.8
cb.	10.7	175.5
1/4	9.8	176.4
1/4	7.4	176.8

186.18

1/4	8.2	176.0
cb.	6.8	179.4
W.	6.2	180.0

250'.S.

W.	6.7	179.5
cb.	7.3	178.9
1/4	7.8	178.4
E.	8.3	177.9
1/4	9.1	177.1
cb.	9.9	176.3
E.	10.8	175.4

275'.S.

E.	12.0	174.2
cb.	11.0	175.2
1/4	10.4	175.4
E.	10.1	176.1
1/4	9.3	176.9
cb.	8.9	177.3
W.	8.4	177.8

300'.S. = N. line E. St.

W.	11.5	174.7
cb.	11.8	174.4
1/4	12.5	173.7
E.	13.1	173.1
1/4	13.0	173.2
cb.	13.8	172.4
E.	13.9	172.3

29th St.

57

80' wide
10' depth
10' 1/2

	186.18		
T.P.	0.10	173.20	13.08
		7' S. of N. Line	173.10
E		1.7	171.5
cl		1.1	172.1
"4		0.6	172.6
±		0.7	172.5
"4		0.3	172.9
cl		+0.2	173.4
W.		+0.5	173.7
	+ 10' S. of N. line = Improve line		
W.		2.5	170.7
+5		0.4	172.8
cl		0.2	173.0
"4		0.5	172.7
+3		1.3	171.9
"4		0.9	172.3
±		0.7	172.5
"4		1.2	172.0
cl		1.5	171.7
E.		2.2	171.0
	+ 20' S = N		
E		3.0	170.2
cl		2.5	170.7
"4		2.1	171.1
±		1.5	171.7
"4		1.9	171.3

	173.20	29 th St.
		58
cl	2.2	171.0
W. dirt	2.4	170.8
W. on E. End ext. cl.	3.18'	170.02
	+ 30' = N. '14	
W.	3.0	170.2
cl	2.8	170.4
"4	2.5	170.7
±	2.7	170.5
"4	3.0	170.2
cl	3.5	169.7
E	4.0	169.2
	+ 40' S = ± E. St.	
E.	4.8	168.4
cl	4.4	168.8
"4	3.7	169.5
±	3.2	170.0
"4	3.0	170.2
cl	3.0	170.2
W.	3.0	170.2
	+ 50' S = 5. '14	
W	3.5	169.7
cl	3.7	169.5
"4	3.8	169.4
±	3.7	169.5
"4	4.1	169.1
cl	5.0	168.2
E	5.4	167.8

173.20
+60's = 5 ch. Line E. ST

E	5.8	167.4
ch	5.2	168.0
"4	4.8	168.4
♀	4.3	168.9
"4	6.0	167.2
ch	4.5	168.7
W. em + ch.	4.12	169.08

+70's = 5, Improvement Line

W	3.8	169.4
ch	4.1	169.1
"4	4.5	168.7
♀	8.2	165.0
"4	5.4	167.8
ch.	5.9	167.9
E.	6.2	167.0

+80 = 0400 = 5, line E. ST.

E.	7.2	166.0
ch	6.7	166.5
"4	7.0	166.2
+2	9.7	163.5
♀	9.2	164.0
+7	5.1	168.1
"4	8.9	168.3
ch.	4.5	168.7
W	4.2	169.0

29th ST.

173.20
12' S.

59

W	4.5	168.7
ch	5.0	168.2
"4	5.7	167.5
+5	5.7	167.5
♀	7.0	166.2
+4	8.1	165.1
+5	10.6	162.6
"4	11.9	161.3
ch	11.1	162.1
E	12.1	161.1
+15	14.3	158.9

18' S.

-15	16.0	157.2
E	14.0	159.2
+5	16.0	157.2
ch.	12.0	161.2
"4	8.7	164.5
♀	6.1	167.1
"4	6.3	166.9
ch	5.4	167.8
W.	4.7	168.5

28' S.

W	5.5	167.7
ch	6.0	167.2
ch	7.0	166.2
"4	7.8	164.4
♀	9.4	163.8

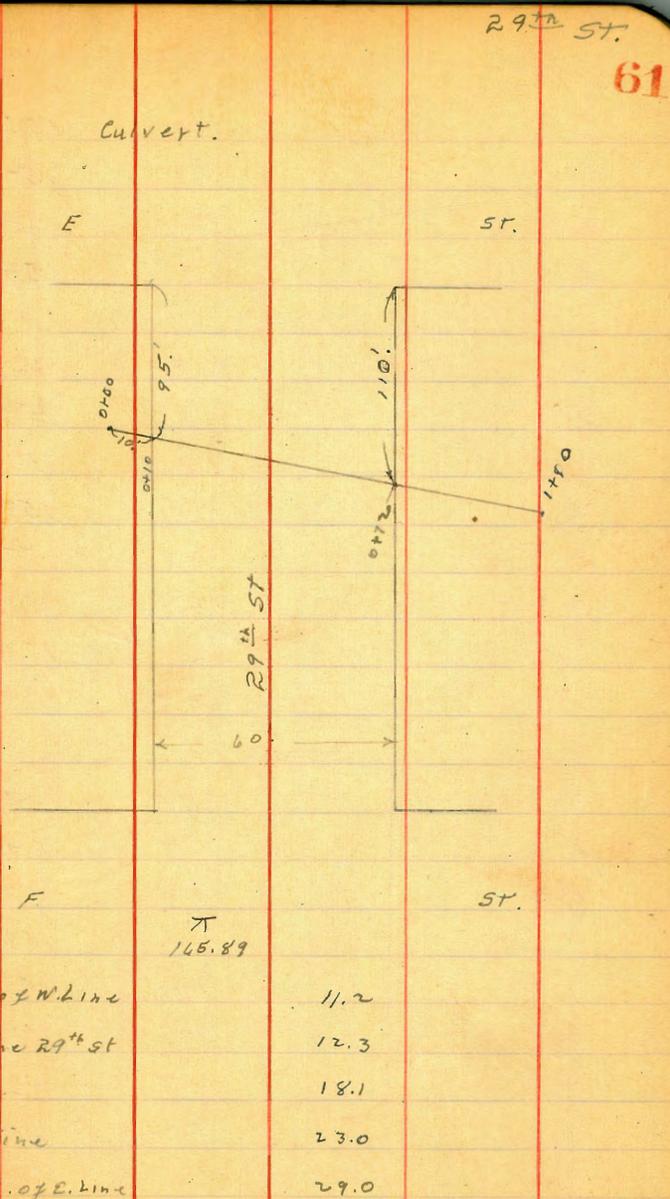
173.20

1/4			13.0	160.2		
T.P.	0.14	165.89	7.45	165.75		
cl			5.8	160.1		
E			10.6	155.3		
+20			11.2	154.7		
		40'S.				
-30			14.0	151.9		
-25			13.8	152.1		
-20			16.0	149.9		
-13			16.0	149.9		
-12			12.0	153.9		
E			11.1	154.8		
cl			7.7	158.2		
1/4			5.0	160.9		
±			2.4	163.5		
1/4			2.0	163.9		
cl			0.4	165.5		
W.			+1.4	167.3		
		55'S.				
-5			2.4	163.5		
W.			3.6	162.3		
cl			5.1	160.8		
1/4			4.6	161.3		
±			6.6	159.3		
1/4			8.7	157.2		
cl			10.7	155.2		

165.89

		29 th ST.				
						60
				E	13.2	152.7
				+8	14.4	151.5
				+9	16.4	149.5
				+16	18.2	147.7
				+20	16.1	149.8
				+30	16.5	149.4
		75'S.				
				-40	21.6	144.3
				-25	22.1	143.8
				-22	19.6	146.3
				E	15.6	150.3
				cl	17.6	151.3
				1/4	14.2	151.7
				±	12.7	153.2
				1/4	11.0	154.9
				cl.	10.0	155.9
				W	8.7	157.2
				+10	7.5	158.4
		100'S.				
				-10	10.3	155.6
				W.	12.3	153.6
				cl	14.6	151.3
				1/4	16.2	149.7
				±	18.0	147.9
				1/4	19.3	146.6
				cl.	19.8	146.1

	165.89		
	100' S. (con)		
E.	20.8	145.1	
+40	26.0	139.9	
	112.5		
-40	29.4	136.5	
E	22.0	142.9	
el	21.0	144.9	
1/4	18.6	147.3	
⊕	16.2	149.7	
1/4	13.6	152.3	
el	11.6	153.3	
W.	10.0	155.9	
+10	8.7	157.2	
	135.5		
W.	6.4	159.5	
el.	7.6	157.3	
1/4	9.5	156.4	
⊕	11.2	154.7	
1/4	13.1	152.8	
el	15.6	150.3	
E	18.1	147.8	
+20	22.7	143.2	
	150.5		
E-20	20.0	145.9	
E	15.6	150.3	
el	13.1	152.8	
1/4	11.3	154.6	



165.89

150' S. (CON)

±	10.0	155.9 on M.H. cover	+5
1/4	7.9	158.0	+7
cl.	7.6	158.3	±
W.	6.2	159.7	1/4

175' S.

W.	4.5	161.4	T.P.
cl.	6.0	159.9	±
1/4	7.3	157.6	+20
±	8.8	157.1	
1/4	10.8	155.1	-20
cl.	12.4	153.5	-15
E.	12.1	150.8	±
+10	17.4	148.5	cl.

200' S.

-15	20.0	145.9	±
E	16.0	149.9	1/4
cl.	13.3	152.6	cl.
1/4	11.4	153.5	W.
±	9.4	156.5	
1/4	8.4	157.5	W.
cl.	6.7	159.2	cl.
W.	5.2	160.7	1/4

225' S.

W	6.2	159.7	±
cl.	8.0	157.9	1/4
1/4	9.1	156.8	cl.

165.89

29th ST.

62

9.9	156.0
11.4	154.5
11.2	154.7
11.7	154.2
14.7	151.2
4.71 158.57	12.03 153.84
±	10.3 148.3
+20	15.0 143.6
250' S.	
	17.2 141.6
	15.8 142.8
±	8.2 150.4
cl.	6.7 151.9
1/4	6.1 152.5
±	4.6 154.0
1/4	2.6 156.0
cl.	1.8 156.8
W.	0.2 158.4
275' S.	
W.	0.4 158.2
cl.	2.1 156.5
1/4	4.7 153.9
±	6.9 151.7
1/4	7.0 151.6
cl.	7.4 151.2
E.	8.2 150.4
+20	19.0 139.6

158.57
297.5

E-15	11.4	147.1
E	9.3	149.2
+3	8.0	150.6
cb	8.0	150.6
+2	8.7	149.8
1/4	7.9	150.7
±	8.5	150.0
+6	8.5	150.0
1/4	5.6	153.0
cb	3.2	155.3
W	1.5	157.0

300'.S. = N. line F. ST

W.	7.1	151.5
cb	7.8	150.8
1/4	8.3	150.3
±	8.1	150.4
1/4	8.4	150.1
cb	8.9	149.7
E.	8.5	150.0

Set BM. N.W. 7' Hub 8.08 150.49 29th + F. ST.

29th ST.

63

80 wide
10' excepted Abs.
10' els.
10' 1/4's

E. ST. X Sec. 28th to 30th

8-14-29

B.M.B.P. 12.78 170.77

157.99 S.S. 28th + E. Sts.

N. cont. el.

170.77
75' E

64

+ 4' = N. edge 5' cont. walk 12.58

158.19

gutter

0.68

170.09

S. cont. el. 12.72

158.05

1/4

1.4

169.4

1/4 12.4

158.4

4.

1.5

169.3

1/4 11.9

158.9

1/4

1.7

169.4

1/4 11.9

158.9

gutter

1.8

169.0

N. cont. el. 12.28

158.49

S. cont. el.

2.0

168.8

+ 4' = S. edge 5' cont. walk. 12.14

158.63

T.P.

12.61

183.28

0.10

170.67

25' E

100' E. Brk.

N. cont. el. 8.46

162.91

S. cont. el.

10.30

172.98

gutter 9.4

161.4

gutter

11.0

172.3

1/4 9.4

161.4

1/4

10.7

172.6

1/4 9.4

161.4

1/4

10.4

172.9

1/4 9.6

161.2

1/4

10.5

172.8

gutter 9.5

161.3

gutter

10.4

172.9

S. cont. el. 9.03

161.74

N. cont. el.

9.26

174.02

50' E

140' E = W. Line Alley

S. cont. el. 5.26

165.51

N. dirt

4.0

179.3 for yardage

gutter 6.0

164.8

N. on N. end Alley Ret.

4.64

178.64 for yardage

1/4 5.7

165.1

N. cont. el.

4.80

178.48

1/4 5.6

165.2

gutter

5.7

177.6

1/4 5.7

165.1

1/4

5.5

177.8

gutter 5.9

164.9

1/4

5.4

177.9

N. cont. el. 4.47

166.10

gutter

6.0

177.3

S. cont. el.

6.2

177.1

S. Line S. End Alley Ret.

5.70

177.58 for yardage

S. dirt

5.50

177.78 for yardage

4.7

178.6 for yardage

Cbs Plotted 8-19-29 C.B.H.

183.28
150' E.

9	4.1	179.2
ch	5.0	178.3
1/4	4.9	178.4
⊕	4.4	178.9
1/4	4.4	178.9
ch	4.7	178.6
+5	3.6	179.7
N.	3.2	180.1

160' E. = E. line Alley

N. dirt	1.9	181.4 for yardage
N. on N. End. ent. Alley Ret	2.38	180.90 No yardage
+5	2.4	180.9 for yardage
N. ent. el	2.54	180.74
gutter	3.4	179.9
1/4	3.4	179.9
⊕	3.5	179.8
1/4	3.9	179.4
gutter	4.2	179.1
s. ent. el	3.42	179.86
S. on S. End. ent. Alley Ret + dirt	3.38	179.90

175' E.

S. ent. el	2.48	180.80
gutter	3.2	180.1
1/4	2.5	180.8
⊕	2.1	181.2
1/4	2.1	181.2

183.28

gutter	2.2	181.1
N. ent. el	1.29	181.99
T.P.	5.32	187.79
		0.81
		182.47
		200' E.
N. ent. el	4.16	183.63
gutter	4.9	182.9
1/4	5.0	182.8
⊕	4.9	182.9
1/4	5.3	182.5

gutter	5.8	182.0
S. ent. el	5.09	182.70

225' E.

S. ent. el	4.05	183.74
gutter	4.8	183.0
1/4	4.4	183.4
⊕	3.8	184.0
1/4	4.1	183.7
gutter	4.1	183.7
N. ent. el	3.22	184.57

250' E

N. ent. el	3.04	184.75
gutter	3.9	183.9
1/4	4.0	183.8
⊕	3.7	184.1
1/4	4.2	183.6
gutter	4.6	183.2
S. ent. el	4.00	183.79

E. ST.

65

	187.79	
	275' E.	
S. cont. el.	4.45	183.34
gutter	5.1	182.7
1/4	4.6	183.2
⊕	4.2	183.6
1/4	4.4	183.4
gutter	4.2	183.6
N. cont. el.	3.52	184.27

	300' E.	
N. cont. el.	4.53	183.26
gutter	5.3	182.5
1/4	5.4	182.4
⊕	5.2	182.6
1/4	5.4	182.0
gutter	6.4	181.4
S. cont. el.	5.51	182.28

	355' E.	
S. cont. el.	9.22	178.57
gutter	10.0	177.8
1/4	9.2	178.6
⊕	8.6	179.2
1/4	8.8	179.0
gutter	9.2	178.6
N. cont. el.	8.19	179.60

	187.79	E. 57.
	410' E.	
N. cont. el.	11.56	176.23
gutter	12.4	175.4
1/4	12.2	175.6
⊕	12.0	175.8
1/4	12.5	175.3
gutter	13.3	174.5
S. cont. el.	12.63	175.16
T.P.	0.37	175.34
	12.82	174.97

	460' E.	
S. cont. el.	2.32	173.02
gutter	3.0	172.3
1/4	2.3	173.0
⊕	1.7	173.6
1/4	1.7	173.6
gutter	1.9	173.4
N. cont. el.	1.24	174.10

	510' E.	
N. cont. el.	3.30	172.04
gutter	3.9	171.4
1/4	3.6	171.7
⊕	3.6	171.7
1/4	4.1	171.2
gutter	4.9	170.4
S. cont. el.	4.28	171.06

175.34

560' E. = N. Line 29th St =
= C. End of mt. walk & curb

S.	6.3	169.0
+10 = line of improvement	5.9	169.4
+11 = sedge mt. walk	6.10	169.24
+16 = N. " " "	6.22	169.12
s. mt. eb.	6.26	169.08
gutter	6.7	168.6
1/4	5.6	169.7
⊕	5.1	170.2
1/4	5.1	170.2
N. mt. eb.	5.32	170.02
+4 = sedge mt. walk	5.29	170.05
+9 = N. " " "	5.19	170.15
+10 = line of improvement	4.6	170.7
+13	1.6	173.7
+20 = N. line	0.6	174.7
T.P. on B.M. Man	0.20	175.51
	0.03	175.31

N.W. 29th St
E. 51'sIntersection Taken 29th St. Page 57. This Book.From 29th to 30th Notes on E. forCo. wid.
10' chs
10' sidewalks00 = E. Line 29th St

N.	4.4	171.1
+10 = eb.	5.2	170.3
1/4	6.2	169.3
⊕	7.1	168.4
1/4	7.8	167.7
eb	8.0	167.5
0 S.	8.5	167.0

175.51

E. St.

67

15.8

S-4
S

d

1/4

⊕

1/4

eb

N

N

eb

1/4

⊕

1/4

eb

S

+5

+15

-20

-10

S

eb

1/4

⊕

+5

1/4

eb

N

10.2

9.4

8.9

8.5

8.0

7.1

6.2

5.0

40' E

6.3

7.5

8.3

9.6

11.0

12.3

14.4

15.4

18.3

20' E

22.0

19.7

17.5

15.6

13.5

11.6

10.6

8.8

8.8

8.2

169.1

166.6

167.0

167.5

168.4

169.3

170.5

169.2

168.0

167.2

165.9

164.5

163.2

161.1

160.1

157.2

153.5

155.8

158.0

159.9

162.0

163.9

164.9

166.7

166.7

167.3

New

New

New

175.51

80'E.

N	10.2	165.3
cl	10.2	165.3
1/4	10.4	165.1
1/2	15.0	160.5
1/4	16.8	158.7
cl	19.0	156.5
S	21.6	153.9
+15	25.0	150.5
+25	21.7	148.8 New
- 24 Front House under Porch	27.7	147.8 New
+15	25.4	150.1
S	23.8	151.7
cl	22.3	153.2
1/4	21.6	153.9
1/2	19.1	156.4
1/4	16.9	158.6
cl	15.0	160.5
N	10.6	164.9
T.P.	0.67	163.93
	12.25	163.26
	100'E.	
N	3.1	160.8
cl	5.1	158.8
1/4	7.0	156.9
1/2	8.4	155.5
1/4	10.1	153.8
cl	11.6	152.3
S	13.0	150.9

163.93

E St.

68

+20	15.8	148.1 ground
+20 = N End Porch	9.8	154.1 Tap Porch
+24 = Front of House	16.8	147.1 New.
115'E.		
S-30	21.0	142.8 New
S-75	19.2	144.7
S	17.0	146.9
cl	14.7	149.2
1/4	13.2	150.7
1/2	11.9	152.0
1/4	10.8	153.1
cl	9.4	154.5
N	8.2	155.7
+10	7.1	156.8
145'E.		
-10	15.7	148.2
N	17.0	146.9
cl	18.2	145.7
1/4	19.3	144.6
1/2	20.8	143.1
1/4	22.3	141.6
cl	23.8	140.1
S	25.4	138.5
+20	28.0	135.9
+40	30.5	133.4 New.
165'E.		
S-30	32.6	131.9 New.
S-30	30.9	133.0
S	28.1	135.8
cl	27.0	136.9

163.93
165'E. (con)

1/4	24.0	137.9
1/2	24.8	139.1
3/4	24.0	139.9
cl	23.0	140.9
N	22.0	141.9
+15	20.6	143.3
+25	19.7	144.2 New
-35	23.2	140.7 New
-20	17.8 N.G.	149.1
-20	24.8	139.1
N	26.7	137.2
cl	27.5	136.4
1/4	28.1	135.8
1/2	28.5	135.4
3/4	29.0	134.9
cl	29.4	134.5
S	30.3	133.6
+15	31.2	132.7
+30	33.2	130.7
+50	32.0	131.3 New
-50	31.8	132.1
-30	32.4	131.5
-20	32.7	131.2
S	32.0	131.9
cl	31.0	132.9
1/4	30.5	133.4
1/2 on Top M.H.	29.3	134.6
1/4	29.3	134.6
cl	28.5	135.4

190'E.
N.G.

205'E.

E. 57.

69

163.93

N.	28.1	135.8
+25	27.2	136.7
+40	26.7	137.2 New
-40	28.8	135.1 New
-25	29.3	134.6
N.	29.8	134.1
cl	30.1	133.8
1/4	30.5	133.4
1/2	30.6	133.3
3/4	31.2	132.7
cl	32.1	131.8
S	32.2	131.7
+10	27.4	136.5
+20	26.5	137.4
+30	25.2	138.7 New
-25	21.4	142.5 New
-15	21.1	142.8
-5	24.6	139.3
cl	27.3	136.6
1/4	30.0	133.9
+7	32.6	131.3
1/2	32.0	131.9
3/4	31.0	131.9
cl	30.4	133.5
N	30.4	133.5
+30	31.4	132.5
+40	28.5	135.4 New

275'E

265'E

	163.93		
	270.6	259	1380
-40		28.0	135.9
-25			
-18		31.5	132.4
N.		32.5	131.4
cl		32.7	131.2
1/4		32.7	131.2
£		32.7	131.2
1/4		26.5	137.4
cl		23.1	140.8
S		22.0	141.9
+15		20.5	143.4
+25		20.0	143.9
	305.8		
-15		8.2	155.7 New
-10		9.5	154.4
S		9.9	154.0
d		10.0	153.9
1/4		10.2	153.7
£		10.5	153.4
1/4		10.7	153.2
cl		11.2	152.7
N		11.5	152.4
+15		12.4	151.5
+25		13.0	150.9 New
T.P.	13.03	0.00	163.93
	345.3		
-15		10.3	166.6
N		11.4	165.3
cl		12.1	164.8
1/4		11.8	165.1

	176.96		E. ST
			70
£		11.7	165.2
1/4		10.7	166.2
cl		10.3	166.6
S		10.2	166.7
+10		10.3	166.6
	360.8		
-10		6.9	170.0
S		7.6	169.3
cl		7.5	169.4
1/4		7.5	169.4
£		7.5	169.4
1/4		7.2	169.7
cl		7.3	169.6
N		4.2	172.7 ^{w. edge dirt} drive
	378.8		
N		3.1	173.8 ^{e. edge dirt} drive
cl		2.7	174.2
1/4		2.2	174.7
£		2.7	174.2
1/4		3.4	173.5
cl		4.2	172.7
S		4.2	172.7
+8		4.0	172.9

	176.96			
	387' E			
- 8		2.0	174.9	
S		1.9	175.0	
el		2.0	174.9	
1/4		1.5	175.4	
1/4		1.5	175.4	
1/4		1.9	175.0	
el		0.5	176.4	
N		0.4	176.5	
T.P.	11.96	188.74	0.18	176.78
		400' E		
N		11.8	176.9	
el		12.0	176.7	
1/4		12.0	176.7	
1/4		12.2	176.5	
1/4		11.3	177.4	
el		11.2	177.5	
S		11.8	176.9	
		414' E		
S		9.2	179.5	
el		9.0	179.7	
1/4		9.4	179.3	
1/4		10.2	178.5	
1/4		9.9	178.8	
+ 9		9.8	178.9	
el		8.2	180.5	
N		8.4	180.3	

188.74

416' E

	188.74			
	416' E			
N		7.8	180.9	
el		7.8	180.9	
1/4		7.9	180.8	
1/4		8.4	180.3	
1/4		9.1	179.6	
el		8.6	180.1	
S		8.8	179.9	
		440' E		
S		6.3	182.4	
el		6.0	182.7	
1/4		5.7	183.0	
1/4		5.5	183.2	
1/4		5.2	183.5	
el		4.9	183.8	
N		4.4	184.3	
		475' E		
N		2.4	186.3	
el		2.6	186.1	
1/4		3.0	185.7	
1/4		3.4	185.3	
1/4		3.7	185.0	
el		3.7	185.0	
S		3.9	184.8	

E. St.

71

188.74
500.8

S	3.1	185.6
cl	3.0	185.7
1/4	2.9	185.8
1/2	2.9	185.8
1/4	2.7	186.0
cl	2.4	186.3
+5	1.9	186.8
+7	1.2	187.5
N	1.2	187.5

550.8

N	0.8	187.9
+4	0.8	187.9
+5	1.7	187.0
cl	2.0	186.7
1/4	2.2	186.5
1/2	2.7	186.0
1/4	2.8	185.9
cl	3.4	185.3
S	3.3	185.4

575.2

S	3.5	185.2
cl	3.5	185.2
1/4	3.0	185.7
1/2	2.6	186.1
1/4	2.3	186.4
cl	2.1	186.6

188.74

150

72

+5	2.0	186.7
+7	1.0	187.7
N	0.8	187.9
60' E. = W. Line 30 th ST.		
N-10 = N. Line 80' ST	0.9	187.0
N-6 = N. end. ent. Walk.	0.98	187.76
N. on ent. walk	1.19	187.55
+4 = N. ent. cl. Return	1.35	187.39
+4.1 gutter parmt.	1.92	186.82

cl on "	2.01	186.73
1/4 " "	2.24	186.50
1/2 " "	2.55	186.19
1/4 " "	3.06	185.68
cl " "	3.74	185.00
+5.9 = present gutter parmt	4.10	184.64
+6 " ent. cl	3.71	185.03
S	3.57	185.17
+10 = S. Line 80' ST.	3.40	185.34
chk. on P.M.B.P. N.W. 30 th & E.	1.10	187.64 = 187.63

Culver T Notes Page 73.

Culvert Xiny E. St Bet R9th + 30th

16393

T.P. 3.5 138.1 29.3 134.6 Top M.H.

Proposed Culvert #1.

45' N. of N. line 60' st	5.4	132.5	in present wash
43' " " " " " "	3.8	134.3	
N. line 60' st	4.2	133.9	
33.26' of N. line = 60' st	4.7	133.4	
66.45' of N. line = S. line 60' st.	6.1	132.0	
35' S. of S. line 60' st.	7.1	131.0	in wash
50' S. " " " " " "	6.8	131.3	

Proposed Culvert #2

138.1

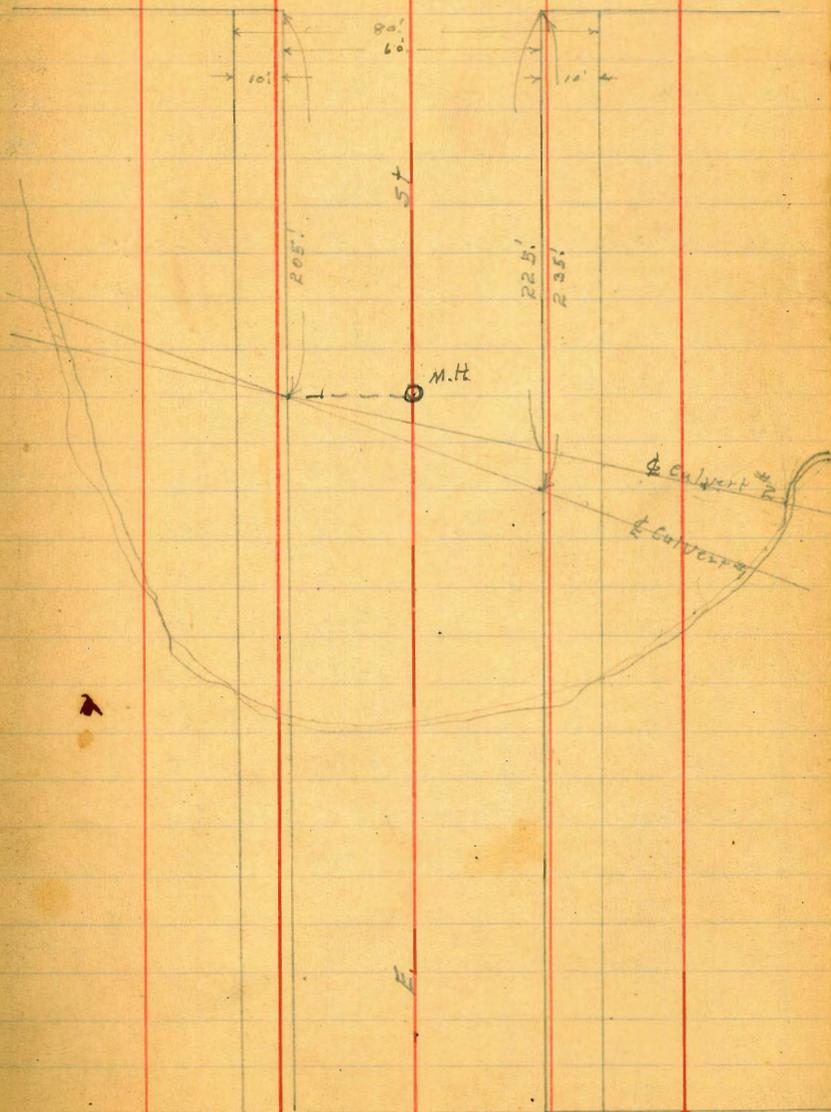
50' N. of N. line 60' st	5.4	132.7	in wash
45	3.2	134.9	
N. line of 60' st	3.9	134.2	
31.55' of N. line = 60'	4.6	133.5	
63' S. of N. line = S. line 60' st.	6.1	132.0	
30' S. of S. line of 60' st	7.3	130.8	in wash
50' S. " " " " " "	7.0	131.1	

E. St.

73

29th

St.



30th

St

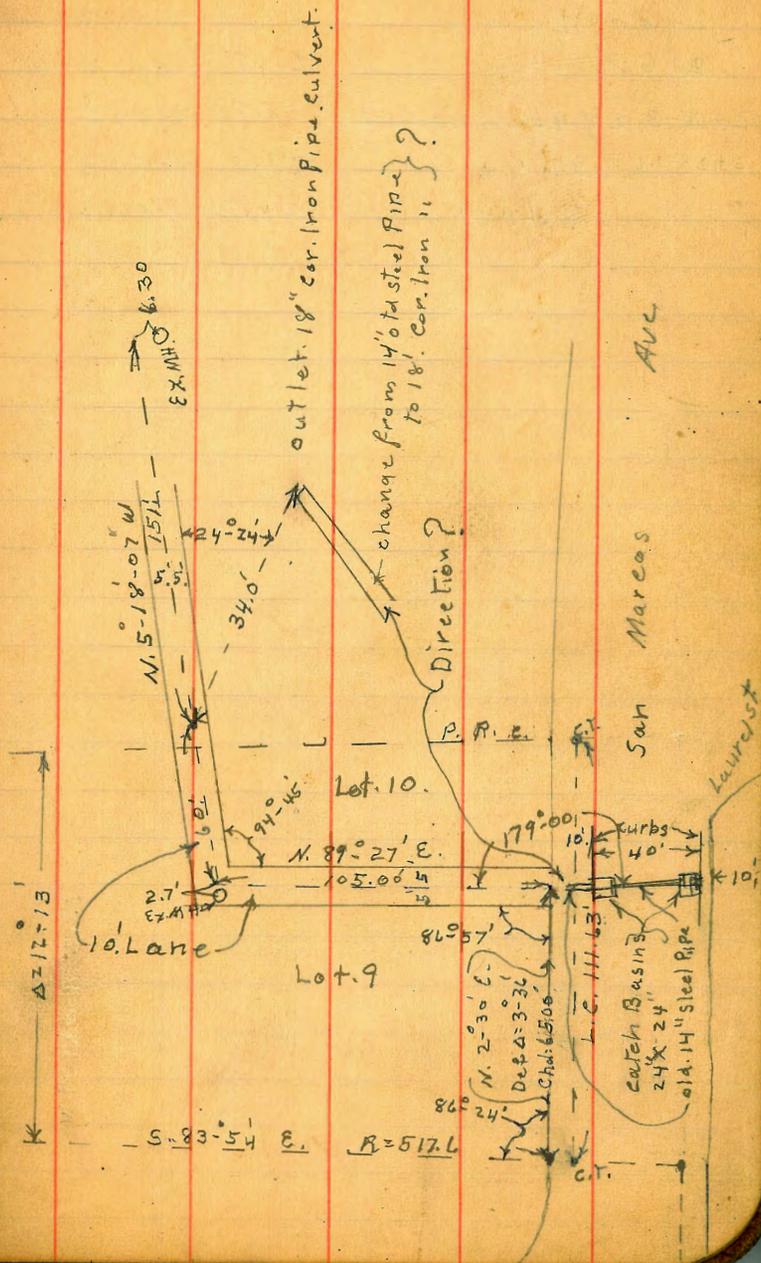
Survey of Existing Culvert
in Path in Blk. H. Burlingame

7-6-36
Miller
Walker
Bliss

indexed
C.S.M.

74

B.M. B.P.	5.38	294.16	288.78	S. E. Laurel + San Marcos
Catch Basin E. cl. line San Marcos	6.86	287.30	287.30	Top. grating
" " " " " "	5.98	288.18	288.18	Top. cl.
" " " " " "	8.74	285.42	285.42	F.L.
14" Coeos Plumosa Palm 2' E. of E. cl & Catch Basin				
Catch Basin W. cl. line curb dipped	7.04	287.10	287.10	Top. grating
in driveway	8.99	285.17	285.17	F.L.
6.3' S. of C.B. Top. of cl.	7.03	287.13	287.13	= S. side Drive
5.0' N " " " " " "	4.91	287.25	287.25	= " " "
12.5' N. of Catch Basin Large Fan Palm 86" Diam 2' W. of W. cl.				
5' E of W. line on curwalk	5.55	288.61	288.61	
0+17	3.55	290.61	290.61	
0+50	3.52	290.64	290.64	
0+75	4.34	289.82	289.82	
0+95	4.48	289.68	289.68	
1+05 A	3.77	290.39	290.39	
F.L. 2x M.H. { 2' N+S. Lane 2.7' S. of E+W Lane	16.19	277.97	277.97	
T.P. 0.70	290.66	4.20	289.96	
E+W. lane ent. pavmt.				
1+10 N. edge ent.	0.5	290.16	290.16	
1+25	2.5	288.16	288.16	
1+57	4.0	286.66	286.66	
T.P. 1.90	280.73	11.83	278.83	
Outlet Ex 18" Cor. Iron Pipe.	14.8	265.93	265.93	F.L.



280.73

2+00	£ Lane	16.7	264.03
2+08	" "	20.5	260.23
2+08-3'	£ of Lane in wash	21.5	259.23
2+25	" " " " " "	22.7	258.03
2+25	£ Lane	20.7	260.03

75

Cross Section #11 of Block 45 Normal H.H.
 3975 St to Mountain View Drive
 Between Adams & Gilmore Place

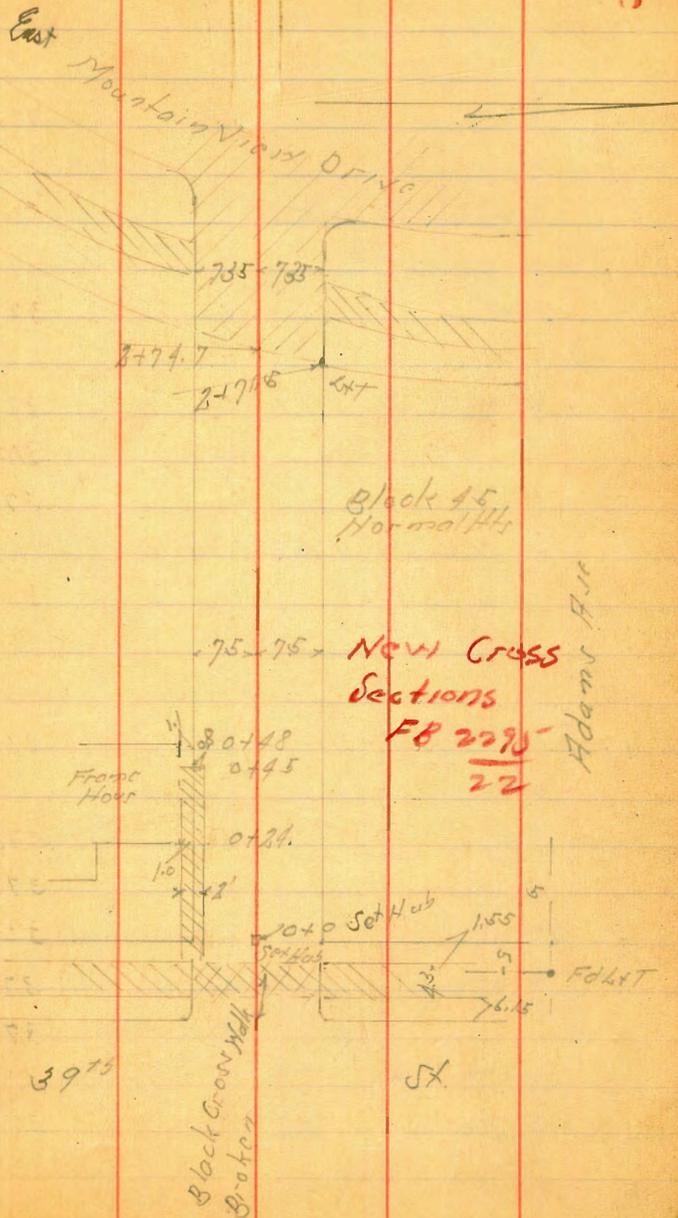
BM	5.08	375.95	370.87	S.F.P.P. F.C.M.S. 3975 St
		0-12 = W.C. Line of 3975 St.		
N Top cb		4.95	371.00	✓
N Ground		5.2	370.8	
S "		5.3	370.7	
S "		5.3	370.7	
S Top cb		5.09	370.91	✓
		0-155 = 1/4 Curb + Conc Walk		
S = 1/4 Cb + Walk		4.85	371.10	✓
N = " " "		4.73	371.22	✓
		0+0 = W.L. 3975 St.		
-8.6 = S.F. Cor. Bldg Conc Floor		3.77	372.18	✓
		Used as S. 5619 160-091		
N		4.7	371.3	
S		5.0	371.0	
+6.6 = 1/4 2' Conc Walk		4.62	371.33	✓
S 07 Walk		4.62	371.33	✓
		0+19		
S 07 Walk		4.25	371.70	✓
+0.9 = 1/4 2' Conc Walk		4.25	371.70	
S		4.3	372.0	
N		3.8	372.2	
+1.0		4.0	372.0	✓
		0+41		
N-8.6 = S.F. Cor. Bldg Conc Floor		2.75	372.20	✓
		Shop 1601 091		

Reduced & Plotted on Profile # 2092
 3-26-42 G.B.H.

Indexed
 C.S.K.

March 25-48
 S. 5619
 North 4th St
 W. 1st St

6



FDNA
 Gilmore Place

Block 45
 Normal H.H.

New Cross
 Sections

FB 2295-

22

Adams Pl.

378.95

0+45 = 1/2 Conc Walk

S+0.8 = 1/2 Conc Walk 3.62 372.33 ✓

0+48

S+11 = Fly Lath House ✓

0+51

-10 3.5 372.5

-0.4 = 1/4 Power Pole ✓

H 3.3 372.7

1/2 3.5 372.5

S 3.4 372.6

TP 5.96 378.58 3.33 372.62

0+64

Fly Garage

S+0.8 = 1/4 Lath House ✓

0+69

S+0.8 = 1/2 Garage Street Conc Floor 5.90 372.68 ✓

1+0

-10 5.5 373.1

S 5.5 373.1

1/2 5.4 373.2

H 5.4 373.2

+10 5.6 373.0

1+06

S-23 = 1/2 Garage Conc Floor 5.42 373.16 ✓

1+16

S = Fly Lath Fence ✓

378.58

1+25

S = 1/2 Conc Walk 5.04 373.54 ✓

1+50

-10 4.5 374.1

-0.4 = 1/4 Power Pole ✓

H 4.6 374.0

1/2 4.7 373.9

S 4.7 373.9

1/2 Fly Lath Fence ✓

+0.4 = Fly Picket Fence ✓

+10 5.2 373.4

TP 2.95 377.38 4.15 374.43

2+0

-10 3.3 374.1

-0.2 = 1/4 Picket Fence ✓

S 3.0 374.4

1/2 3.0 374.4

H 3.0 374.4

2+02

H-3.9 = Fly Conc Apron 2.62 374.76 ✓

H-7.5 = Fly Do Garage Conc Floor 2.43 374.95 ✓

2+18

H-4 = Fly Conc Apron 2.58 374.80 ✓

H-8 = Fly Do Garage 2.38 375.00 ✓

37738

H-4 = Fly Stucco Floor ✓
2+34
Fly Conc Floor 2.60 374.78

2+40
-4 = Fly Stucco House ✓ 2.4 375.0

-0.2 = Fly Power Pole ✓
H 2.8 374.6

2.8 374.6

2.9 374.5

+5 2.7 374.7

2+50

-0.7 = H.I. Car Garage W Entrance ✓
S 3.1 374.3

2.1 374.3

3.1 374.3

+4 = Fly Car Stucco House ✓ 2.4 375.0

2+66

S-0.5 = H.I. Car Garage Conc Floor 2.84 374.54 ✓

2+71.5 = F.L. Mt. View on N.

H Top Cb 4.45 372.93 ✓

H on Pavmg 4.80 372.58 ✓

2 on Conc Slab 4.78 372.60 ✓

S 4.7 372.7

to 6 = Fly Conc Drive 3.34 374.04 ✓

2+747 = F.L. Mt. View on Road

S Top Cb 4.77 372.61 ✓

S on Pavmg 4.94 372.44 ✓

2 " " 5.00 372.38 ✓

H Cb Line Mt. View Dr.

S Top Cb 5.36 372.02 ✓

S on Pavmg 5.77 371.61 ✓

2 " " 5.64 371.74 ✓

H " " 5.50 371.88 ✓

H Top Cb 4.99 372.39

TP 1.83 378.89 0.32 377.06

BM 2.02 376.87

JF BP
Floor 1374
370.87

Faint handwritten notes at the top of the page, possibly including the words "Rock" and "Bridges".

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body

of table in same row and column gives distance from side stake to slope stake. If ground is not

level, the distance from side stake to slope stake is found by the side stake and slope stake, lower table by the amount it cut, elevate it fill. Add this amount to cut or fill and find distance in table. Set up rod at this point and line of sight should cut target.

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add connection found in column of connections.

Degree of curve with a given L may be found by dividing tangent (or external), opposite L by given tangent (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

175
 28.34
 203.34
 23
 203.11

226
 291.6

ENGINEERING DEPARTMENT,
 CITY OF SAN DIEGO,
 CALIFORNIA.

1765 N Wp. 1298 in Driveway

3582
 1791
 12.09

175	- 6.00	368	4774
29	2.90		
51	4519.00		
2/255	2.25	6.60	4.9
	Lucid ME Mon	4.00	
	E/Cajon + 99 SWBP		355.37
	50 SWBP		383.13
	57 st	111.5	386.82
	L. 51 ST	45	3869.0512
		26.5	12.085
			24.75
			12.75
			38.50
			12.75
			50.25
			12.75
			68.00
			137.30
			2/274.65
	293.80	2537.4	
	19	101.48	
	277.80	20.30	
		121.75	
		115.95	
		237.73	
		36.92	
	293.80	274.65	100
	19	274.80	
	274.80		
	5792		
	11595		
	2537.4		
	101.48	293.80	
	36.92	50.	
	138.40	3.80	14850
	10.15		
	148.55	293.80	287.00
		500	
		2/288.80	
		194.40	