1282

DESK

Our Leather Bound Engineers Note Books are carried in the following rulings:

No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.

No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.

No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.

No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

We also carry the Note Books listed above, bound in extra strong Fabri-Hide (otherwise the same quality of book), which can be furnished at a somewhat lower price.

In ordering Fabri-Hide covered books, add the letter *"F"* to catalog number.

Zeros indexed to pp. 80 7/5/20 AH.

X sec. Froude St. From Pascadero to Coronado. Graded. No Improvements. 60' st. 12' cbs. 36' Roadway

BM	13.10	107.91 ✓		94.81	Pascadero & Froude
0+00 = NL Pascadero					
E.L.			9.2	98.7	
+35	walks		10.62	97.3	
+85	✓		10.69	97.2	
cb			10.83	97.1	
gut	Pav		11.50	96.4	
¼	✓		11.51	96.4	
℄	✓		11.61	96.3	
¼	✓		11.97	95.9	
gut	✓		12.38	95.5	
cb			11.77	96.1	
+35	walk		11.75	96.2	
+85	✓		11.65	96.3	
N.L.			11.7	96.2	
0+05					
N.L.			11.6	96.3	
+3			11.3	96.6	
+4			11.0	96.9	
+11			11.1	96.8	
cb			11.5	96.4	
+2			11.6	96.3	
¼			11.4	96.5	
℄			11.1	96.8	
+4			10.8	97.1	

12/6/28 T.W.

Plotted ✓

Sept 24-28

Loudon.

0+05	107.91		
¼		10.9	97.0
+6		11.0	96.9
cb		10.6	97.3
+2		10.2	97.7
+7		9.9	98.0
+9		9.6	98.3
E.L.		8.5	99.4
0+25			
E.L.		8.3	99.6
+2		8.5	99.4
+11		8.6	99.3
cb		8.7	99.2
¼		8.6	99.3
℄		8.8	99.1
¼		9.2	98.7
+6		9.3	98.6
cb		9.3	98.6
+		9.8	98.1
+10		9.9	98.0
N.L.		9.3	98.6

0+50	107.91		
w.c.	7.0	100.9	
+3	7.6	100.3	
+11	7.6	100.3	
cb	7.3	100.6	
+4	7.2	100.7	
1/4	7.3	100.6	
℄	7.0	100.9	
1/4	6.7	101.2	
cb	6.8	101.1	
+5	6.6	101.3	
+11	6.4	101.5	
E.L.	6.2	101.7	
0+75			
E.L.	4.1	103.8	
+2	4.4	103.5	
+10	4.5	103.4	
cb	5.1	102.8	
+5	5.1	102.8	
1/4	4.9	103.0	
+5	4.8	103.1	
℄	4.9	103.0	
1/4	5.6	102.3	
+7	5.9	102.0	
cb	5.9	102.0	
+1	5.8	102.1	
+2	5.5	102.4	

0+75		
+10	5.7	102.2
w.c.	5.0	102.9
1+00		
w.c.	3.2	104.7
+2	3.6	104.3
+11	3.6	104.3
cb	3.9	104.0
1/4	3.6	104.3
℄	2.9	105.0
1/4	2.7	105.2
cb	2.7	105.2
+2	2.8	105.1
+3	2.5	105.4
+5	2.5	105.4
+6	2.7	105.2
+7	2.5	105.4
+11	2.4	105.5
E.L.	2.1	105.8
1+25		
E.L.	0.0	107.9
+5	0.3	107.6
+10	0.2	107.7
+10	0.5	107.4
cb	0.5	107.4
+5	0.6	107.3
1/4	0.5	107.4

1+25	107.91		
℄		0.8	107.1
¼		1.4	106.5
cb		1.9	106.0
+7		1.6	106.3
+10		1.7	106.2
N.L.		1.5	106.5
T.P. 12.98	120.88	0.01	107.90
1+40 = S.L. Alley			
N.L.		13.0	107.9
+1		13.0	107.9
+2		13.5	107.4
+10		13.3	107.6
cb		13.4	107.5
¼		13.0	107.9
℄		12.4	108.5
¼		12.1	108.8
+4		11.9	109.1
cb		12.0	108.9
+2		12.0	108.9
+2		11.7	109.2
+7		11.6	109.3
E.L.		11.6	109.3
1+60 = N.L. Alley			
E.L.		9.0	111.9
+2		9.2	111.7
+10		9.7	111.2

1+60	120.88		
+11		10.1	110.8
cb		10.1	110.8
+3		10.0	110.9
¼		10.2	110.7
℄		10.5	110.4
¼		11.2	109.7
+6		11.6	109.3
cb		11.8	109.1
+8		11.8	109.1
N.L.		11.4	109.5
1+75			
N.L.		11.3	109.6
+05		10.2	110.7
+3		9.9	111.0
+7		9.9	111.0
+11		9.5	111.4
cb		9.8	111.1
+4		10.1	110.8
¼		9.7	111.2
℄		9.1	111.8
¼		8.6	112.3
+7		8.6	112.3
cb		8.6	112.3
+2		8.6	112.3
+3		8.2	112.7
E.L.		7.7	113.2

2+00	120.88			
E.L.		5.0	115.9	
+3		5.6	115.3	
+11		5.3	115.6	
cb		5.8	115.1	
+5		6.1	114.8	
℄		6.0	114.9	
℄		6.0	114.9	
℄		6.5	114.4	
+2		7.0	113.9	
cb		6.9	114.0	
+1		6.4	114.5	
+8		6.6	114.3	
W.L.		6.7	114.2	
2+25				
W.L.		3.4	117.5	
cb		3.3	117.6	
+1		4.0	116.9	
+3		4.1	116.8	
℄		3.4	117.5	
℄		3.1	117.8	
℄		2.9	118.0	
+3		2.8	118.1	
+4		3.2	117.7	
cb		3.1	117.8	
+2		3.0	117.9	
+3		2.3	118.6	

2+25	120.88		
E.L.		2.2	118.7
T.P. 13 04	133.38	05 4	120 34
2+50			
E.L.		11.5	121.9
+1		11.5	121.9
+2		11.3	122.1
+9		11.1	122.3
+9		12.9	120.5
cb		13.1	120.3
+3		13.1	120.3
+3		12.0	121.1
℄		11.9	121.5
℄		12.0	121.4
℄		12.6	120.8
+6		13.1	120.3
+6		13 8	119.6
cb		13.8	119.6
cb		12.5	120.9
W.L.		12.5	120.9

2+75	133.38		
N.L		9.2	124.2
cb		8.8	124.6
+1		10.8	122.6
+2.5		10.9	122.5
+3		9.6	123.8
1/4		9.0	124.4
℄		8.7	124.7
1/4		8.6	124.8
+1		8.6	124.8
+1		10.3	123.1
+8		10.5	122.9
+9		8.8	124.6
cb		8.8	124.6
+2		7.9	125.5
+9		7.7	125.7
E.L		7.4	126.0
3+00 = S.L Orchard.			
E.L		4.3	129.1
+7		4.9	128.5
+9		7.4	126.0
+1		7.4	126.0
cb		8.3	125.1
+2		8.3	125.1
+2		7.9	125.5
+4		7.7	125.7
+4		6.2	127.2

3+00		
cb +7	6.3	127.1
+8	6.1	127.3
1/4	6.0	127.4
℄	6.5	126.9
+5	6.6	126.8
1/4	6.8	126.6
+2	6.8	126.6
cb	7.2	126.2
+1	6.1	127.3
+9	6.0	127.4
N.L.	6.2	127.2
0+00 = N.L. Orchard.		
N.L.	3.8	129.6
cb	3.4	130.0
+3	4.1	129.3
+7	3.1	130.3
1/4	3.1	130.3
+5	2.9	130.5
+7	2.8	130.6
℄	3.6	129.8
+2	4.0	129.4
+6	3.9	129.5
1/4	2.6	130.8
+5	2.6	130.8
cb	2.4	131.0
+2	2.2	131.2

0+00	133.38			
E.L.		1.5	131.9	
T.P.	12.97	145.87	0.58	132.80
0+25				
E.L.		11.4	134.4	
+4		11.7	134.1	
cb		11.8	134.0	
+1		13.6	132.2	
+4		13.6	132.2	
+5		12.6	133.2	
1/4		12.5	133.3	
+7		12.5	133.3	
℄		12.5	133.3	
+5		12.7	133.1	
1/4		12.9	132.9	
cb		13.1	132.7	
+10		13.1	132.7	
W.L		12.8	133.0	
0+50				
W.L		9.9	135.9	
+2		9.9	1359	
+7		9.5	136.3	
+11		9.2	136.6	
cb		10.4	135.4	
+2		10.1	135.7	
+3		9.6	136.2	
+4		9.5	136.3	

145.77

0+50		
+5	10.0	135.8
+8	9.3	136.5
1/4	9.5	136.3
+1	9.3	136.5
+7	8.8	137.0
℄	8.8	137.0
+3	8.8	137.0
+8	9.0	136.8
1/4	9.0	136.8
+6	9.2	136.6
+7	12.0	133.8
+7.5	12.0	133.8
cb	8.2	137.6
E.L.	7.7	138.1
0+75		
E.L.	3.5	142.3
+3	3.9	141.9
+11	4.4	141.4
cb	6.2	139.6
+1	8.1	137.7
+2	5.3	140.6
+8	5.0	140.8
1/4	5.1	140.7
℄	5.0	140.8
+6	4.7	141.1
1/4	5.6	140.2

0+25	145.77			
+1			6.0	139.8
+2			5.7	140.1
+3			5.7	140.1
+6			5.8	140.0
+8			6.8	139.0
cb			6.4	139.4
+1			5.5	140.3
9			5.5	140.3
+11			6.1	139.7
n.c.			5.6	140.2
1400				
n.c.			2.0	143.8
+4			2.3	143.5
+5			1.7	144.1
+8			1.5	144.3
cb			1.6	144.2
+1			3.6	142.2
+2			2.3	143.5
+5			1.8	144.0
+6			1.9	143.9
+7			2.4	143.4
1/4			1.8	144.0
+3			1.5	144.3
&			1.2	144.6
+8			1.1	144.7
+1/4			1.6	144.2

	145.77		
+1		1.1	144.7
+2		1.2	144.6
+8		2.6	143.2
+9		2.6	143.2
cb		1.5	144.3
+2		0.6	145.2
+11		+0.3	146.1
E.L.		+0.7	146.5
T.P 1305	158.61	0.21	145.56
1+25			
E.L.		9.3	149.3
+2		9.9	148.7
+11		10.0	148.6
cb		11.5	147.1
+3		11.5	147.1
+3		10.8	147.8
1/4		10.8	147.8
+2		10.6	148.0
&		10.7	147.9
+5		10.9	144.7
1/4		1/4	
+1		12.0	146.6
+2		11.6	147.0
+4		11.5	147.1
+7		11.9	146.7
+8		12.6	146.0

1+25	158.61		
mcb		11.1	147.5
+8		11.3	147.3
+11		11.2	147.4
n.L.		11.4	147.2
1+40 = S.L. Alley			
~~E.L.~~		9.7	148.9
cb		9.5	149.1
+1		10.7	147.9
+2		10.2	148.4
+5		9.8	148.8
1/4		9.6	149.0
℄		9.1	149.5
+2		9.0	149.6
+8		9.2	149.4
1/4		9.4	149.2
+1		9.2	149.4
+5		9.0	149.6
+6		9.2	149.4
+7		10.2	148.4
cb		8.9	149.7
+1		8.4	150.2
+3		8.2	150.4
E.L.		8.2	150.4

158.61

8

1+60 = N.L. Alley		
E.L.	6.5	152.1
+11	6.6	152.0
cb	7.7	150.9
+1	8.4	150.2
+2	7.5	151.1
1/4	7.3	151.3
℄	7.1	151.5
1/4	7.7	150.9
+7	8.2	150.4
+8	8.7	149.9
cb	9.6	150.0
cb	7.6	151.0
+10	8.0	150.6
n.L.	7.4	151.2
1+75		
n.L.	6.7	151.9
+4	6.9	151.7
cb	6.5	152.1
+1	7.5	151.1
+2	6.9	151.7
1/4	6.5	152.1
℄	6.0	152.6
1/4	6.1	152.5
+5	6.1	152.5
+6	6.8	151.8

158.61

1+75			
cb	6.8	151.8	
+1	5.4	153.2	
E.L.	5.1	153.5	
2+00			
E.L.	3.3	155.3	
+11	3.9	154.7	
cb	4.2	154.4	
+1	5.2	153.4	
+3	4.6	154.0	
¼	4.4	154.2	
℄	4.4	154.2	
¼	4.7	153.9	
+7	5.2	153.4	
+8	5.7	152.9	
cb	4.7	153.9	
n.L.	5.0	153.6	
2+25			
n.L.	4.0	154.6	
cb	3.5	155.1	
+1	4.1	154.5	
+3	3.9	154.7	
¼	3.5	155.1	
℄	3.1	155.5	
¼	3.1	155.5	
+6	3.1	155.5	
+6	3.5	155.1	

2+25		
e b	3.5	155.1
+1	2.5	156.1
+2	2.4	156.2
+9	2.1	156.5
E.L.	1.6	157.0
2+50		
E.L.	0.4	158.2
+5	0.9	157.7
+10	1.2	157.4
cb	1.8	156.8
+1	2.2	156.4
+6	1.7	156.9
¼	1.6	157.0
+5	1.5	157.1
℄	1.7	156.9
¼	2.2	156.4
cb	2.7	155.9
+1	2.2	156.4
n.L.	2.4	156.2
2+75		
n.L.	0.9	157.7
+5	0.6	158.0
cb	0.5	158.1
+1	1.2	157.4
¼	0.6	158.0
+2	0.4	158.2

2+75		158.61		
℄			0.3	158.3
+6			0.1	158.5
14			0.2	158.4
+7			0.2	158.4
+7			0.7	157.9
cb			0.7	157.9
T.P.	12.85	171.27 ✓	0.19	158.42
+2			12.2	159.1
+4			12.0	159.3
+9			11.9	159.4
E.L			11.8	159.5
3+00 = S.L. Del Mar Ave.				
E.L			10.0	161.3
cb			10.6	160.7
+1			11.1	160.2
+2			11.3	160.0
+3			11.9	159.4
+4			11.6	159.7
14			11.3	160.0
℄			11.4	159.9
+5			11.6	159.7
14			11.9	159.4
+8			12.4	158.9
cb			12.1	159.2
+1			11.7	159.6
W.L.			12.0	159.3

0+00 = N.L. Del Mar		
N.L	7.9	163.4
+2	8.5	162.8
+7	8.7	162.6
+8	8.9	162.4
+10	8.7	162.6
cb	8.7	162.6
+1	9.5	161.8
14	8.8	162.5
+2	8.6	162.7
+4	8.4	162.9
℄	8.2	163.1
+3	8.0	163.3
14	8.0	163.3
+6	7.9	163.4
cb	7.6	163.7
+10	6.8	164.5
E.	+2.2	173.5
0+25		/
E.L.	+5.3	176.6
+2	3.5	167.8
cb	4.0	167.3
+1	5.0	166.3
+3	4.7	166.6
14	4.6	166.7
℄	4.7	166.6

0+25	171.27			
℄+3		5.0	166.3	
+4		4.9	166.4	
¼		5.3	166.0	
+4		5.6	165.7	
+6		5.7	165.6	
cb		5.0	166.3	
+3		5.2	166.1	
+8		5.2	166.1	
+9		5.2	166.1	
w.L.		4.6	166.7	
0+50				
w.L.		1.3	170.0	
+2		2.1	169.2	
+7		1.8	169.5	
cb		1.7	169.6	
+2		2.8	168.5	
+3		2.3	169.0	
¼		2.0	169.3	
+1		1.9	169.4	
+4		1.6	169.7	
℄		1.5	169.8	
¼		1.3	170.3	
+4		1.3	170.3	
+6		2.0	169.3	
+8		1.4	169.9	

0+50	171.27		
cb		0.4	170.9
+10		0.2	171.1
E.L.		+8.6	179.9
T.P. 12.72	18388 V	0.11	171.16
0+75			
E.L.		5.0	178.9
+1		9.5	174.4
+2		9.8	174.1
+11		9.9	174.0
cb		10.6	173.3
+1		11.0	172.9
+2		10.7	173.2
¼		10.5	173.4
℄		10.7	173.2
+3		10.9	173.0
+5		10.8	173.1
+8		11.4	172.5
¼		11.1	172.8
+3		11.2	172.7
+6		11.8	172.1
+8		11.7	172.2
cb		10.8	173.1
+11		11.1	172.8
w.L.		10.3	173.6

1+20	18388		
w.l.	5.5	178.4	
+1	7.4	176.5	
+3	7.7	176.2	
+11	7.5	176.4	
cb	7.8	176.6	
+1	9.5	175.4	
+3	8.2	175.7	
1/4	7.6	176.3	
+2	7.7	176.2	
+5	7.3	176.6	
℄	7.3	176.6	
+2	7.1	176.8	
1/4	7.0	176.9	
+6	7.2	176.7	
+7	7.7	176.2	
+8	7.3	176.6	
cb	7.1	176.8	
+1	6.6	177.3	
+11	6.1	177.8	
E.L.	1.4	182.5	

1+25		
E.L.	2.9	181.0
+11	3.2	180.7
cb	3.7	180.0
+1	4.2	179.5
+2	4.1	179.8
1/4	3.7	180.2
℄	3.8	180.1
+6	4.1	179.8
1/4	4.3	179.6
+6	4.6	179.3
+7	5.1	178.8
cb	4.0	179.9
+9	4.0	179.9
+11	3.9	180.0
w.l.	2.7	181.2
1+38 = S.L. Alley		
w.l.	1.7	182.2
+1	2.5	181.4
cb	2.5	181.4
+1	3.2	180.7
1/4	2.8	181.1
+5	2.4	1815
℄	2.2	181.7
+5	2.2	181.7
1/4	2.3	181.6
+5	2.4	1815

1+38		183.88		
+8			2.9	181.0
cb			2.0	181.9
+1			1.7	182.2
+11			1.3	182.6
E.L.			0.3	183.6
T.P.	4.81	188.04	0.65	183.23
1+58 = N.L. Alloy.				
E.L.			4.2	183.8
cb			4.3	183.7
+1			5.3	182.7
+3			5.0	183.0
¼			4.8	183.2
℄			4.8	183.2
¼			5.3	182.7
+6			5.5	182.5
cb			5.1	182.9
+1			5.0	183.0
+11			5.1	182.9
N.L.			4.8	183.2

1+75		
N.L.	3.1	184.9
+2	4.4	183.6
cb	4.4	183.6
+1	5.1	182.9
¼	4.7	183.3
℄	4.3	183.7
¼	4.3	183.7
+3	4.3	183.7
+8	4.7	183.3
cb	3.7	184.3
+10	3.6	184.4
E.L.	3.3	184.7
2+00		
E.L.	3.3	184.7
+11	3.6	184.4
cb	4.2	183.8
+1	4.5	183.5
+4	4.1	183.9
¼	4.1	183.9
℄	4.0	184.0
+5	4.2	183.8
¼	4.5	183.5
+8	5.2	182.8
cb	4.3	183.7
+10	4.5	183.5
N.L.	0.9	187.1

2+25		
w.l	4.4	183.6
+2	4.7	83.3
+11	4.8	83.2
cb	5.4	82.6
1/4	4.9	83.1
℄	4.4	83.6
1/4	4.4	83.6
+3	4.4	83.6
+8	4.8	83.2
cb	3.9	84.1
+7	3.7	84.3
E.L.	3.6	84.4
2+50		
E.L.	4.2	83.8
cb	4.6	83.4
+1	5.3	82.7
+4	5.0	83.0
1/4	5.0	83.0
℄	5.0	83.0
1/4	5.5	82.5
+8	6.0	82.0
cb	5.2	82.8
+1	5.0	83.0
w.l	5.0	83.0

2+75	188.04	
w.l	5.0	183.0
+1	5.5	82.5
cb	5.6	82.4
+1	6.6	81.4
1/4	5.9	82.1
℄	5.6	82.4
1/4	5.7	82.3
+3	5.7	82.3
+8	6.0	82.0
cb	5.4	82.6
+7	5.1	82.9
+10	5.0	83.0
E.L.	4.3	83.7
3+07.41 = S.L. Coronado		
E.L.	5.7	81.3
+11	6.1	81.9
cb	6.6	81.4
+1	6.8	81.2
1/4	6.5	81.5
℄	6.5	81.5
1/4	6.8	81.2
+16	7.3	80.7
cb	7.5	80.5
+1	6.8	81.2
w.l.	6.6	81.4
T.P. (El. 178.97)	9.08	178.86

X Sec. Guizot St. - Del Monte to Santa Cruz.
60' street 40' Roadway 10' Cbs.

					↳ S.W. Santa Cruz.
BM.	0.86	256.36		255.50	↳ Santa Cruz.
T.P.	0.05	243.53	12.88	243.48	
T.P.	0.20	230.75	12.98	230.55	
BM.			5.30	225.45	N.E. Guizot ↳ Santa Cruz.

Cbs and walks in on West 0+00 to 2+00
Cbs and walks in on East 0+00 to 1+40
(5.5' Combination walks & cbs)

0+00 = S.L. Del Monte

Ecb		11.19	219.56
gut		12.2	↗18.6
+8		12.0	↗18.8
¼		12.0	↗18.8
℄	Tst.	11.9	↗18.9
+3		12.0	↗18.8
¼	Plotted 12/6/28	12.5	↗18.3
gut		13.0	↗17.8
wcb		12.42	↗18.33
0+45			
wcb		11.38	↗19.37
gut		12.0	↗18.8
+2		11.6	↗19.2
¼		11.0	↗19.8
℄		10.5	↗20.3
¼		10.6	↗20.2
+4		10.8	↗20.0

Sept 26-28
Loudon
Isbell
Morgan

0+25	230.75		
+9.		11.0	219.8
gut		11.1	219.7
Ecb		9.86	↗20.89
0+50			
Ecb		8.83	↗21.92
gut		10.1	↗20.7
+4		9.9	↗20.9
+8		9.9	↗20.9
¼		9.6	↗21.2
+3		9.4	↗21.4
℄		9.5	↗21.3
¼		10.1	↗20.7
+8		10.1	↗20.1
gut		10.9	↗19.9
wcb		10.48	↗20.27
0+75			
wcb		9.47	↗21.28
gut		9.9	↗20.9
¼		9.3	↗21.5
℄		8.7	↗22.1
¼		8.8	↗22.0
+4		9.0	↗21.8
+9		8.7	↗22.1
gut		8.7	↗22.1
Ecb		8.06	↗22.69

Guizot

230.75

1+00			
Ecb		7.65	223.10
gut		84	224
1/4		82	226
+8		81	22.7
℄		8.2	22.6
1/4		89	21.9
+8		9.3	21.5
gut		9.2	21.6
Wcb		9.03	21.72
1+25			
wcb		8.76	21.99
gut		89	21.9
1/4		84	22.4
℄		7.8	23.0
1/4		7.8	23.0
Gut		7.8	23.0
Ecb		7.18	23.57
1+40 = N.L. Alley = End wall Ecb on East.			
E.L.		6.1	24.7
+4 walk		6.74	24.01
cb		6.94	23.83
gut		7.2	23.6
1/4		7.5	23.3

Guizot

1+40		
℄	2.7	223.1
1/4	84	22.4
gut	88	22.0
wcb	8 59	22.16
1+60 = S.L. Alley		
wcb	8.36	22.39
gut	85	22.3
1/4	81	22.7
℄	7.4	23.4
1/4	7.2	23.6
cb	6.6	24.2
E.L.	5.8	25.0
1+75		
E.L.	5.7	25.1
+1	5.9	24.9
+8	6.0	24.8
cb	6.5	24.3
+2	7.0	23.8
1/4	7.2	23.6
℄	7.2	23.6
1/4	7.9	22.9
gut	8.5	22.3
wcb	8.24	22.51

Guizot

230.75

2+00 = End cos walk on West		
w.l.	8.1	222.7
+4	7.9	22.9
+4 walk	7.75	23.0
cb	7.99	22.76
9 ft	8.3	22.5
1/4	7.9	22.9
℄	7.4	23.6
1/4	6.9	23.9
+8	7.1	23.7
cb	6.6	24.2
+1	6.4	24.6
+9	5.8	25.0
E.L.	5.4	254
2+25		
E.L.	4.6	26.2
+3	5.6	25.2
cb	6.1	24.7
+4	6.9	23.9
1/4	6.8	24.0
℄	7.0	23.8
1/4	7.7	23.1
+5	8.1	22.7
cb	8.2	22.6
+3	8.1	22.7
w.l.	8.1	22.7

Guizot

2+50		
w.l.	8.1	222.7
+8	8.0	22.8
cb	8.2	22.6
1/4	7.6	23.2
℄	6.8	24.0
1/4	6.6	24.2
+8	6.7	24.1
cb	6.2	24.6
+2	5.7	25.1
E.L.	5.2	25.6
2+75		
E.L.	4.4	26.4
+4	5.3	25.5
cb	5.6	25.2
+2	6.3	24.5
1/4	6.4	24.4
℄	7.1	23.7
1/4	7.9	22.9
cb	8.6	22.2
+2	8.2	22.6
+8	8.5	22.3
w.l.	7.9	22.9

3+00 = N.L. Santa Cruz		230.75		
W.L.			8.9	221.9
+8			8.8	22.0
cb	top cb		8.90	21.85
+2			8.8	22.0
1/4			8.4	22.4
+5			7.9	22.9
℄			7.5	23.3
1/4			6.9	23.9
+8			6.6	24.2
cb	top cb		5.73	25.02
cb	grd.		6.3	24.5
+4			5.6	25.2
E.L.			4.9	25.9
T.P.	0.54	222.45	8.84	221.91

Guizot From Santa Cruz to Coronado
60' st 40' Rdway 10' cbs. (Not Graded)

222.45		
0+00 = S.L. Santa Cruz		
E.L.	2.6	219.9
cb top cb	2.97	19.48
1/4	3.7	18.8
℄	4.3	18.2
1/4	4.8	17.7
cb	5.6	16.9
+1	5.6	16.9
+7	16.0	06.5
W.L.	16.0	06.5
0+02		[illegible]
W.L.	16.1	06.4
+4	16.2	06.3
cb	5.6	16.9
1/4	4.8	17.7
+6	4.3	18.2
℄	4.3	18.2
1/4	3.7	18.8
cb	2.8	19.7
+9	2.5	20.0
E.L.	0.2	22.3

Plotted 12/6/28 T.J.

Guizot

222.45

0+25		
EL.	+0.5	223.0
+1	1.6	20.9
cb	2.1	20.4
¼	2 6	19.9
½	3 4	19.1
+3	3 7	18.8
+5	13 7	08.8
¼	14.1	08.4
+5	14 2	08.3
cb	11 9	10.6
+1	12.1	10.4
+3	12 6	09.9
+4	12 2	10.3
+8	13 2	09.3
mc.	12 7	9.8
1'w	12 5	10.0
4 w	12 0	10.5
9'w	5 1	17.4
14 w	4 4	18.1

Guizot

19

0+30		
1'w	4 2	218.3
5'w	5 0	17.5
m.c.	12 2	10.3
+4	12 7	9.8
+6	12 6	10.5
+8	11 7	10.8
cb	12 1	10.4
+2	11 4	11.1
+5	11 3	11.2
+8	13 2	9.3
¼	13 9	8.6
+9	13 4	9.1
½	12 5	10.0
+5	10 5	12.0
+5	2 9	19.6
¼	2 6	19.9
cb	2 0	20.5
+9 5	1 5	21.0
EL.	+0 6	23.1

0+37	222.45		
E.L		+0.6	223.1
+1		+0.6	223.1
+1		1.5	21.0
ob		1.8	20.7
1/4		2.5	20.0
+5		2.7	19.8
+6		10 5	12.0
℄		12.9	9.6
+3		12.8	9.7
+5		9.0	13.5
+8		10 2	12.3
1/4		10 3	12.2
+4		10 8	11.7
+5		11.5	11.0
+6		11.5	11.0
+7		11.0	11.5
+9		11.1	11.4
cb		11.8	10.7
+2		11.8	10.7
+5		11.5	11.0
+8		10.8	11.7
w.L		4.6	17.9
5w		3.7	18.8

0+50		
w.L.	3.1	219.4
+5	3.7	18.8
+9	10 6	11.9
cb	11.0	11.5
+3	9.9	12.6
+8	10.0	12.5
1/4	9 9	12.6
+1	10 3	12.2
+2	9.6	12.9
+4	9.5	13.0
+8	11.0	11.5
℄	12.0	10.5
+4	11.3	11.2
+9	2.0	20.5
1/4	2.0	20.5
+5	1.6	20.9
cb	1.4	21.1
+9.5	1.0	21.5
E.L.	+0.8	23.3

0+75	222.45		
E.L.		+2.0	224.5
+0^5		0.0	22.5
cb		0.1	22.4
+7		0.3	22.2
1/4		10.1	12.4
+6		10.4	12.1
+7		7.6	14.9
℄		7.6	14.9
+2		7.8	14.7
+3		8.4	14.1
4		8.0	14.5
+6		8.4	14.1
1/4		8.3	14.2
+2		8.4	14.1
+4		7.7	14.8
+6		2.3	20.2
cb		2.2	20.3
+2		1.7	20.8
+5		1.8	20.7
wL		2.2	20.3

Gc 1204

1+00		
wL	1.3	221.2
cb	0.8	21.7
+7	1.0	21.5
1/4	7.1	15.4
+2	6.6	15.9
+5	6.9	15.6
+7	6.3	16.2
+9	6.1	16.4
℄	6.8	15.7
+1	6.2	16.3
+4	6.0	16.5
+7	8.7	13.8
1/4	9.0	13.5
+3	0.0	22.5
cb	+0.7	23.2
+9^5	+0.7	23.2
E.L.	+2.3	24.8
1+25		
E.L.	+3.2	25.7
+1	+3.2	25.7
+1	+1.3	23.8
cb	+1.1	23.6
+5	+0.8	23.3
+7	7.3	15.2
1/4	7.6	14.9
+1	7.6	14.9

1+25		222.45		
1/4 + 2			4.6	17.9
+5			4.3	18.2
+8			4.6	17.9
+9			5.2	17.3
℄			4.6	17.9
+4			5.0	17.5
+6			4.4	18.1
+8			5.1	17.4
+9			4.9	17.6
1/4			3.8	18.7
+1			0.2	22.3
+6			0.2	22.3
+8			0.1	22.4
cb			-0.1	22.4
W.L.			-0.3	22.2
T.P.	6.69	228.85	0.29	222.16
1+40 = N.L. Alley.				
W.L. =			6.1	222.8
+7			5.7	23.2
cb			5.7	23.2
+6			5.8	23.1
+8			6.3	22.6
1/4			10.5	18.4
+3			10.4	18.5
+6			10.0	18.9
+7			10.4	18.5

1/4 + 8	9.9	219.0
℄	9.9	19.0
℄	10.7	18.2
+1	10.7	18.2
+2	10.0	18.9
+5	9.9	19.0
+8	12.7	16.2
1/4	12.7	16.2
+3	13.1	15.8
+5	5.4	23.5
cb	5.3	23.6
+9	4.7	24.2
+9	2.9	26.0
E.L.	2.9	26.0
1+60 = S.L. Alley.		
E.L.	2.0	26.9
+1	2.0	26.9
+1	4.2	24.7
cb	4.6	24.3
+7	5.1	23.8
+9	10.8	18.1
1/4	10.8	18.1
+4	10.9	18.0
+6	8.5	20.4
+8	8.7	20.2
+9	9.4	19.5

Guizot

228.85

1+60			
℄	8.7	220.2	
+3	8.7	20.2	
+4	9.2	19.7	
+5	8.7	20.2	
+8	9.2	19.7	
¼	8.9	20.0	
+2	8.2	20.7	
+3	5.4	23.5	
+7	4.8	24.1	
cb	4.9	24.0	
+8	5.1	23.8	
wL	5.3	23.6	
1+66			
wL	5.2	23.7	
cb	4.7	24.2	
+3	4.6	24.3	
+8	5.0	23.9	
¼	8.6	20.3	
+4	8.5	20.4	
+7	8.8	20.1	
+9	8.5	20.4	
℄	9.4	20.5	
+1	8.4	20.5	
+1	9.2	19.7	
+2	8.5	20.4	
+4	8.2	20.7	

Guizot.

23

1+66		
℄+6	8.2	220.7
+7	8.8	20.1
+9	8.6	20.3
¼	10.6	18.3
+2	7.0	21.9
+4	4.9	24.0
cb	4.6	24.3
cb	2.6	26.3
EL	1.7	27.2
1+75		
EL	1.5	27.4
cb	2.2	26.7
+05	4.2	24.7
+7	4.6	24.3
¼	8.9	20.0
+3	9.5	19.4
+7	7.8	21.1
+8	8.6	20.3
℄	7.7	21.0
+2	8.0	20.9
+4	8.4	20.5
+6	8.0	20.9
+8	8.0	20.9
¼	7.9	21.0
+1	7.4	21.5
+3	4.7	24.2

1+75		228.85		
+7			4.2	224.7
cb			4.3	24.6
w.l.			4.7	24.2
2+00				
w.l.			3.8	25.1
cb			3.2	25.7
+1			3.2	25.7
+5			3.7	25.2
+8			4.0	24.9
1/4			7.1	21.8
+4			6.4	22.5
+6			6.7	22.2
+9			6.4	22.5
4			6.5	22.4
+1			6.6	22.3
+2			6.8	22.1
+3			6.5	22.4
1/4			6.3	22.6
+3			6.2	22.7
+5			3.3	25.6
+9			3.2	25.7
+7			1.0	27.9
cb			0.9	28.0
E.L.			0.4	28.5
T.P.	5.68	232.39	2.14	226.71

2+25	232.39		
E.L.		2.9	229.5
C.b		3.6	28.8
cb		5.6	26.8
+7		5.9	26.5
+8		8.6	23.8
1/4		8.7	23.7
+6		8.7	23.7
+7		8.5	23.9
+8		8.7	23.7
6		8.4	24.0
+2		8.5	23.9
+4		8.9	23.5
+5		8.6	23.8
+7		9.2	23.2
1/4		9.5	22.9
+2		5.9	26.5
+8		5.6	26.8
cb		5.6	26.8
w.l.		5.9	26.5
NE. 3/4 face Coronado & Guizot B.M.		1.83	230.56
B.M. 182	232.16		230.34

2+50	232.16		
w.L.		4.9	227.3
cb		4.5	27.7
+2		4.4	27.8
+8		4.7	27.5
+9		6.8	25.4
¼		7.1	25.1
+4		7.4	24.8
+6		7.9	24.3
+8		7.3	24.9
+9		7.2	25.0
℄		7.2	25.0
+4		7.3	24.9
+5		7.6	24.6
¼		7.7	24.5
+3		7.7	24.5
+4		4.7	27.5
cb		4.2	28.0
cb		2.4	29.8
E.L.		1.6	30.6

2+52	232.16		
E.L.		1.5+	230.7
cb		2.3	29.9
+7		3.1	29.1
+7		7.6	24.6
¼		7.6	24.6
+5		7.5+	24.7
+7		7.2	25.0
℄		7.2	25.0
+2		7.2	25.0
+4		7.8	24.4
+6		7.3	24.9
¼		7.1	25.1
+1		6.7	25.5
+3		4.6	27.6
+8		4.4	27.8
cb		4.5	27.7
w.L.		4.9	27.3
2+75			
w.L.		3.8	28.4
cb		3.9	28.9
+3		3.3	28.9
+7		4.1	28.1
¼		5.5	26.7
+1		6.1	26.1
+4		6.2	26.0
+6		6.6	25.6

232.16

2+25		
+8	6.2	226.0
℄	6.0	26.2
1/4	6.2	26.0
+1	6.2	26.0
+1	2.4	29.8
+5	1.5	30.7
eb	1.2	31.0
+3	0.9	31.3
E.L.	0.6	31.6
2+91		
E.L.	0.1	32.1
eb	0.7	31.5
+5	1.0	31.2
+9	2.3	29.9
1/4	5.5	26.7
+8	5.6	26.6
℄	5.5	26.7
+4	5.8	26.4
+9	5.6	26.6
1/4	4.7	27.5
+6	2.5	29.7
eb	2.6	29.6
W.L.	3.2	29.0

Guizot

Sept. 27-28
Loudon
Isbell
Morgan

26

3+00 = N.L. Coronado.

W.L.	2.8	229.4
eb	2.3	29.9
+4	2.0	30.2
+8	3.1	29.1
1/4	4.0	28.2
+3	4.9	27.3
+6	5.0	27.2
℄	4.8	27.4
1/4	4.8	27.4
+1	5.1	27.1
+3	5.0	27.2
+3	2.1	30.1
qvt	2.2	30.0
eb to b end ret.	1.69	30.47
E.L.	1.5	30.7

Guizot - S.L. Coronado to Alma Ave
60' St 36' Roadway 12' cbs.
0+00 = S.L. Coronado.

E.L.	0.4	31.8
+10	0.7	31.5
eb	0.9	31.3
+2	1.8	30.4
1/4	1.7	30.5
℄	1.8	30.4
1/4	2.3	29.9
+6	2.6	29.6

Plotted 1/16/18 T.V.

0+00	232.16		
¼+8		3.0	229.2
℄		2.6	29.6
+1		2.2	30.0
+10		2.2	30.0
w.l.		1.4	30.8
0+25			
w.l.		3.7	28.5
+3		3.3	28.9
+11		3.2	29.0
cb		3.7	28.5
+1		3.9	28.3
+4		3.5	28.7
¼		3.2	29.0
℄		2.9	29.3
¼		2.8	29.4
+6		2.7	29.5
+8		2.8	29.4
cb		2.4	29.8
+1		2.0	30.2
+4		2.0	30.2
+5		2.7	29.5
+6		2.4	29.8
+7		1.9	30.3
+10		1.8	30.4
E.L.		1.0	31.2

Guizot

27

0+50	232.16		
E.L.		2.7	229.5
+2		3.1	29.1
+7		3.1	29.1
cb		3.4	28.8
cb		4.2	28.0
+2		4.2	28.0
+3		4.0	28.2
¼		3.9	28.3
℄		3.9	28.3
¼		4.4	27.8
+7		4.9	27.3
+8		5.1	27.1
cb		5.0	27.2
+1		4.2	28.0
+3		4.2	28.0
+9		4.5	27.7
w.l.		4.8	27.4
0+75			
w.l.		6.3	25.9
+3		5.9	26.3
+11		5.7	26.5
cb		6.4	25.8
+1		6.4	25.8
¼		5.7	26.5
℄		5.3	26.9

Guizot

0+75	232.16		
℄		5.3	226.9
+6		5.3	26.9
+8		5.6	26.6
cb		4.6	27.6
+7		4.3	27.9
+10		3.9	28.3
E.L.		3.5	28.7
1+00			
E.L.		4.9	27.3
+7		5.9	26.3
cb		6.1	26.1
+1		7.2	25.0
+3		7.3	24.9
+4		6.7	25.5
℄		6.6	25.6
℄		6.7	25.5
℄		7.1	25.1
+7		7.7	24.5
+8		8.0	24.2
cb		7.0	25.2
+5		7.1	25.1
W.L.		8.1	24.1

1+25		
W.L.	9.2	223.0
+4	8.9	23.3
cb	8.8	23.4
+1	9.7	22.5
+2	9.7	22.5
+2	9.4	22.8
℄	8.9	23.3
℄	8.5	23.7
+5	8.2	24.0
℄	8.3	23.9
+3	8.2	24.0
+6	8.5	23.7
+7	9.0	23.2
+8	8.9	23.3
cb	7.7	24.5
+8	7.6	24.6
+10	7.3	24.9
E.L.	6.1	26.1
1+40 = W.L. Alley		
E.L.	7.9	24.3
+2	8.9	23.3
+11	8.9	23.3
cb	10.1	22.1
+3	10.0	22.0
+4	9.5	22.7

1+40		232.16		
¼			9.5	222.7
+4			9.5	22.7
℄			9.5	22.7
+4			9.9	22.3
¼			10.0	22.2
+6			10.4	21.8
+7			10.7	21.5
cb			10.7	21.5
+1			9.8	22.4
+7			9.8	22.4
w.l.			10.0	22.2
TP.	1.15	221.35	11.96	220.20
1+60	=			
w.l.			0.4	21.0
+11			0.2	21.2
+11			1.1	20.3
cb			1.2	20.2
+1			0.9	20.5
+5			0.5	20.9
¼			0.5	20.9
℄			0.2	21.2
¼			0.2	21.2
+4			0.3	21.1
+4			0.7	20.5
+8			1.0	20.4
cb			0.5	20.9

Guizot

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1+60	221.35		
cb		0.0	221.4
+7		+0.3	21.7
+10		+1.2	22.6
E.L		+3.0	24.0
1+75			
E.L		+0.7	22.1
+2		1.1	20.3
+9		1.4	20.0
+10		1.9	19.5
cb		2.0	19.4
+5		2.5	18.9
+7		2.0	19.4
¼		1.9	19.5
+4		1.6	19.6
℄		1.8	19.6
+4		1.9	19.5
¼		2.0	19.4
+7		2.2	19.2
+7		2.6	18.8
cb		2.5	18.9
+1		1.7	19.7
w.l.		1.7	19.7

Gulzat

2+00	221.35		
w.L		+1.0	220.4
+2		4.3	217.1
+4		4.7	16.7
+11		4.6	16.8
cb		5.3	16.1
+3		5.2	16.2
1/4		4.8	16.6
+6		4.5	16.9
℄		4.5	16.9
+1		4.4	17.0
1/4		4.5	16.9
+3		4.8	16.6
cb		4.9	16.5
cb		4.0	17.4
+8		3.9	17.5
+9		3.5	17.9
E.L.		+1.4	22.8
2+25			
E.L		+3.2	24.6
+4		6.1	15.3
+5		6.5	14.9
+11		6.8	14.6
cb		7.7	13.7
+9		7.9	13.5
1/4		7.6	13.8
+9		7.4	14.0

2+25		
℄	7.5	213.9
+3	7.6	13.8
1/4	7.9	13.5
+4	8.1	13.3
+6	8.4	13.0
cb	8.4	13.0
+1	8.0	13.4
+7	8.2	13.2
+9	7.6	13.8
w.L	1.7	19.7
2+50		
w.L	5.7	15.7
+3	11.2	10.2
+5	11.7	09.7
+10	11.6	9.8
+11	11.9	9.5
cb	11.9	9.5
+4	11.9	9.5
1/4	11.4	10.0
+6	11.0	10.4
℄	10.9	10.5
1/4	10.7	10.7
+7	10.8	10.6
cb	10.3	11.1
+2	10.1	11.3

2+50		221.35		
cb+6			9.8	211.6
+7			9.5	11.9
E.L.			12.4	23.8
2+75				
E.L.			1.3	20.1
+5			13.0	8.1
+7			13.4	8.0
T.P.	0.02	208.49	12.88	208.47
cb			0.7	07.8
1/4			0.9	07.6
¢			1.2	07.3
+5			1.5	07.0
1/4			1.8	06.7
+4			2.3	06.2
+8			2.2	06.3
cb			1.7	06.8
+8			1.3	07.2
w.L.			+6.0	14.5
3+85 = N.L. Del Mar				
w.L.			2.7	05.8
+2			4.5	04.0
+4			4.7	03.8
cb			4.3	04.2
+1			4.7	03.8
1/4			4.3	04.2

3+00		
1/4+7	3.9	204.6
¢	3.9	04.6
1/4	3.7	04.8
+5	3.4	05.1
cb	3.5	05.0
+5	3.4	05.1
+9	2.1	06.4
E.L.	0.1	08.4
0+00 = S.L. Del Mar		
E.L.	6.1	02.4
cb	6.9	01.6
+1	8.2	00.3
+4	8.2	00.3
+5	7.9	00.6
1/4	8.0	0.5
+7	7.7	0.8
¢	7.7	0.8
1/4	8.0	0.5
+3	8.3	0.2
+6	8.7	199.8
cb	8.7	199.8
+1	8.0	200.5
+7	8.1	200.4
w.L.	8.5	200.0

0+25		208.49		
w.L			10.4	198.1
cb			10.0	98.5
+1			10.6	97.9
1/4			10.2	98.3
℄			9.6	98.9
+3			9.8	98.7
1/4			10.1	98.4
+7			10.0	98.5
cb			9.0	99.5
+9			8.8	99.7
E.L.			8.9	99.6
0+50				
E.L.			11.1	97.4
cb			11.3	97.2
+1			12.2	96.3
1/4			12.3	96.2
℄			12.1	96.4
+7			12.2	96.3
1/4			12.4	96.1
cb			12.8	95.7
cb			12.3	96.2
+5			12.4	96.1
w.L.			12.6	95.9
T.P.	0.00	195.40	13.09	195.40

Guizot

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0+75	195.40		
w.L		1.8	193.6
cb		1.5	93.9
cb		2.0	93.4
+3		2.0	93.4
+4		1.8	93.6
1/4		1.7	93.7
+4		1.4	94.0
℄		1.2	94.2
+7		1.4	94.0
1/4		1.4	94.0
cb		1.5	93.9
cb		0.7	94.7
+5		0.6	94.8
E.L.		0.6	94.8
1+00			
E.L		2.6	92.8
cb		2.7	92.7
cb		3.6	91.8
1/4		3.6	91.8
+7		3.5	91.9
℄		3.4	92.0
1/4		3.9	91.5
cb		4.4	91.0
+1		3.7	91.7
w.L.		4.1	91.3

	195.40			
1+25				
w.l.		6.5	188.9	
+5		6.1	89.3	
cb		6.1	89.3	
cb		6.6	88.8	
1/4		6.2	89.2	
℄		5.9	89.5	
+5		5.8	89.6	
1/4		6.0	89.4	
+2		5.9	89.5	
cb		5.9	89.5	
cb		4.9	90.5	
+9		4.7	90.7	
E.L.		4.8	90.6	
1+40 = N.L. Alley				
E.L.		6.1	89.3	
+11		6.5	88.9	
cb		7.2	87.2	
+8		7.3	88.1	
1/4		6.9	88.5	
℄		7.2	88.2	
1/4		7.6	87.8	
cb		7.9	87.5	
cb		7.5	87.9	
+7		7.4	88.0	
w.l.		7.8	87.6	

1+60 = S.L. Alley		
w.l.	9.9	185.5
+8	9.2	86.2
cb	9.3	86.1
cb	9.8	85.6
1/4	9.4	86.0
℄	8.8	86.6
+7	8.7	86.7
1/4	8.8	86.6
cb	9.0	86.4
cb	8.3	87.1
+3	8.1	87.3
+10	7.9	87.5
E.L.	7.3	88.1
1+75		
E.L.	8.8	86.6
+1	8.9	86.5
+11	9.5	85.9
cb	10.2	85.2
+4	10.2	85.2
1/4	9.9	85.5
℄	10.0	85.4
+6	10.3	85.1
1/4	10.6	84.8
+8	11.1	84.3
cb	10.5	84.9

1+75		195.40		
℄ 6-14			10.4	185.0
W.L.			11.2	84.2
2+00				
W.L.			12.9	82.5
+1			12.7	82.7
cb			12.5	82.9
cb			13.1	82.3
1/4			12.7	82.7
+4			12.4	83.0
℄			12.2	83.2
+7			12.0	83.4
1/4			12.1	83.3
cb			12.4	83.0
cb			11.6	83.8
+11			11.2	84.2
E.L.			11.0	84.4
T.P.	0.07	182.48	12.99	182.41
2+25				
E.L			0.5	182.0
+6			0.9	81.6
+10			0.9	81.6
+10.5			1.5	81.0
cb			1.6	80.9
1/4			1.5	81.0
+7			1.5	81.0

2+25		
℄	1.6	180.9
+5	1.8	80.7
1/4	2.1	80.4
+8	2.5	80.0
cb	1.8	80.7
W.L.	2.0	80.5
2+50		
W.L.	4.4	78.1
+11.5	4.0	78.5
cb	4.4	78.1
+1	4.6	77.9
1/4	4.2	78.3
+4	4.0	78.5
℄	3.9	78.6
1/4	3.7	78.8
+5	3.8	78.7
cb	3.6	78.9
+1	3.1	79.4
+7	3.1	79.4
E.L	2.7	79.8

182.48

2+75

E.L	4.9	177.6
+7	5.4	77.1
cb	5.8	76.7
+3	5.8	76.7
1/4	5.8	76.7
℄	6.2	76.3
1/4	6.5	76.0
+8.5	6.8	75.7
cb	6.2	76.3
+10	6.4	76.1
W.L.	6.7	75.8

2+99.22 = N.L. Orchard.

W.L	8.7	73.8
+3	8.6	73.9
cb	8.3	74.2
+1	8.8	73.7
1/4	8.5	74.0
℄	8.0	74.5
1/4	7.6	74.9
cb	7.4	75.1
+2	7.2	75.3
E.L.	6.6	75.9

Guizot

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0+00 = S.L. Orchard

E.L.	8.6	173.9
+7	9.3	73.2
cb	10.3	72.2
1/4	10.1	72.4
℄	10.1	72.4
1/4	10.7	71.8
+4	10.8	71.7
+8	11.1	71.4
cb	10.4	72.1
W.L.	10.7	71.8

0+25

W.L	11.4	71.1
cb	11.3	71.2
+1	12.0	70.5
+5	11.6	70.9
1/4	11.4	71.1
℄	11.2	71.3
+6	11.2	71.3
1/4	11.3	71.2
+8	11.5	71.0
cb	11.2	71.3
+1	10.5	72.0
+10	10.2	72.3
E.L	9.6	72.9

0+50			
E.L		9.2	173.3
+15		11.1	71.4
+5		11.4	71.1
cb		11.6	70.9
+1		12.5	70.0
1/4		12.1	70.4
℄		12.1	70.4
1/4		12.3	70.2
+5		12.4	70.1
+8		12.9	69.6
cb		12.1	70.4
+11		12.3	70.2
w.l.		12.1	70.4
0+75			
w.l.		12.7	69.8
+2		13.0	69.5
cb		12.9	69.6
+1		13.0	68.9
+5		13.3	69.2
1/4		13.2	69.3
℄		13.1	69.4
+5		12.9	69.6
1/4		12.9	69.6
+8		13.3	69.2
cb		12.6	69.9
+1		12.5	70.0

Guizot

0+75	182.48		
cb+9		12.4	170.1
E.L.		8.1	174.4
TP.057	170.00	13.05	169.43
1+00			
E.L.		+4.2	174.2
+3		0.5	69.5
+11		0 8	69.2
cb		1.6	68.4
+3		1.4	68.6
1/4		1.3	68.7
℄		1.5	68.5
1/4		1.6	68.4
+5		1.9	68.1
+8		2.1	67.9
cb		1.3	68.7
+10		1.3	68.7
w.l.		0 5	69.5
1+25			
w.l.		+3.5	73.5
+1		2.4	67.6
cb		2.3	67.7
+05		3.0	67.0
+11		2.7	67.3
1/4		2.4	67.6
℄		2.1	67.9
+7		2 3	67.7

Guizot.

	170.00		
1+25			
1/4		2.2	167.8
+5		2.1	67.9
+8		2.4	67.6
cb		1.5	68.5
+8		1.4	68.6
+95		1.0	69.0
E.L.		+5.3	75.3
1+40 = N.L. Alley			
E.L.		+5.2	75.2
+2		1.1	68.9
+4		1.8	68.2
cb		2.1	67.9
+05		2.8	67.2
+4		2.6	67.4
1/4		2.6	67.4
℄		2.6	67.4
1/4		2.9	67.1
+6		3.1	66.9
+8		3.7	66.3
cb		2.8	67.2
+9		3.1	66.9
+10		2.7	67.3
W.L.		+0.6	70.6
MH. on ℄ at 1+50		2.75	168.25

Guizot.

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1+60 = S.L. Alley		
W.L.	0.6	169.4
+2	4.1	5.9
+3	4.4	5.6
cb	3.8	6.2
+1	5.0	5.0
+3	4.6	5.4
1/4	4.0	6.0
℄	3.7	6.3
1/4	3.5	6.5
+5	3.4	6.6
cb	3.6	6.4
+05	2.9	7.1
+7	2.7	7.3
+10	2.0	8.0
+11	0.0	170.0
E.L.	+1.1	171.1
1+75		
E.L.	+1.6	71.6
+2	3.3	66.7
+3	3.6	6.4
cb	3.8	6.2
+05	4.8	5.2
+5	4.3	5.7
1/4	4.4	5.6
℄	4.8	5.2

Guizot

1+75	170.00		
1/4		5.0	165.0
+6		5.6	4.4
+8		6.2	3.8
cb		5.0	5.0
+10		5.5	4.5
ML		3.4	6.6
2+00			
ML		4.2	5.8
+2		7.1	2.9
Cb		6.9	3.1
+05		7.7	2.3
+5		7.2	2.8
1/4		6.9	3.1
E		6.6	3.4
1/4		6.2	3.8
+4		6.3	3.7
+6		6.5	3.5
+8		6.8	3.2
cb		5.7	4.3
+8		5.4	4.6
+10		4.4	5.6
EL		4.0	6.0

Guizot

2+25		
EL	6.1	163.9
+2	7.2	2.8
cb	7.6	2.4
+1	8.6	1.4
+3	8.4	1.6
1/4	8.2	1.8
E	8.5	1.5
+6	8.6	1.4
1/4	8.7	1.3
+7	9.3	0.7
+85	9.6	0.4
cb	8.7	1.3
+10	9.0	1.0
ML	6.2	3.8
2+50		
ML	8.5	1.5
+1	10.8	159.2
+4	10.8	9.2
+115	10.4	9.6
cb	11.5	8.5
+1	11.2	8.8
1/4	10.6	9.4
E	10.3	9.7
+7	10.3	9.7
1/4	10.2	9.8
+3	10.2	9.8

2+50		
1/4+5	10.3	159.7
+8	10.0	160.0
cb	9.6	60.4
+11	9.8	61.2
E.L.	7.2	62.8
2+75		
E.L.	9.2	60.8
+1	10.9	59.1
+7	11.3	58.7
cb	11.4	58.6
+1	12.0	58.0
1/4	12.0	58.0
℄	12.0	58.0
+7	12.3	57.7
1/4	12.5	57.5
+4	12.9	57.1
cb	12.9	57.1
+1	12.8	57.2
+1.5	12.4	57.6
+8	12.6	57.4
+11	12.7	57.3
W.L.	10.8	59.2

Guizot

170.00

3+00 69 = N.L. Pascadero		
W.L.	14.1	155.9
+11	13.8	56.2
cb	14.4	55.6
+2	14.4	55.6
+3	14.1	55.9
1/4	13.8	56.2
℄	13.5	56.5
+6	13.3	56.7
1/4	13.4	56.6
+6	13.2	56.8
cb	13.1	56.9
+2	12.9	57.1
E.L.	12.1	57.9
T.P. 0.66 157.59	13.07	156.93
0+00 = S.L. Pascadero		
E.L.	1.9	1557
+4	2.3	55.3
+7	2.3	55.3
cb	2.5	55.1
+1	3.0	54.6
1/4	3.1	54.5
℄	3.2	54.4
+6	3.5	54.1
1/4	3.8	53.8
+2	3.8	53.8
+3	4.2	53.4

0+00		157.59		
1/4+4			3.9	153.7
+7			4.0	53.6
cb			4.3	53.3
cb			3.5	54.1
m.c.			4.0	53.6
0+25				
m.c			5.3	52.3
+2			5.8	51.8
+11			5.3	52.3
c.b			5.9	51.7
+1			6.6	51.0
+3			6.6	51.0
+5			5.5	52.1
1/4			5.1	52.5
+5			4.8	52.8
℄			4.8	52.8
1/4			4.6	53.0
+3			4.6	53.0
+8			4.8	52.8
cb			4.0	53.6
+3			3.7	53.9
+7			3.6	54.0
+10			3.2	54.4
E.L			2.7	54.9

Guizot.

40

0+50		
E.L	4.8	152.8
+7	5.6	52.0
cb	5.7	51.9
+2	6.7	50.9
1/4	6.3	51.3
+6	6.2	51.4
℄	6.2	51.4
+6	6.5	51.1
1/4	6.8	50.8
+6	7.4	50.2
+6 5	8.2	49.4
+8	8.0	49.6
cb	6.8	50.8
+10	7.3	50.3
m.L	6.8	50.8
0+75		
m.L.	8.2	49.4
+2	8.7	48.9
cb	8.4	49.2
+1	9.3	48.3
1/4	8.4	49.2
+1	7.9	49.7
℄	8.0	49.6
1/4	8.0	49.6
+2	8.4	49.2
+8	8.2	49.4

157.59.

0+75			
cb	7.4	150.2	
+1	7.5	50.1	
+2	7.9	49.7	
+3	7.3	50.3	
EL	6.5	51.1	
1+00			
EL	8.8	48.8	
+6	8.7	48.9	
cb	8.9	48.7	
+1	10.1	47.5	
+7	9.8	47.8	
1/4	9.7	47.9	
℄	9.7	47.9	
1/4	10.1	47.5	
+6	10.6	47.0	
+7	11.0	46.6	
+8	10.9	46.7	
cb	9.9	47.7	
w.L	10.3	47.3	

Guizot

41

1+25		
w.L.	11.8	145.8
cb	11.5	146.1
+05	12.6	45.0
+2	12.5	45.1
+3	12.0	45.6
+5	11.7	45.9
1/4	11.5	46.1
℄	11.2	46.4
1/4	11.1	46.5
+5	11.4	46.2
+6	11.8	45.8
+85	11.7	45.9
cb	10.5	47.1
+3	10.3	47.3
+11	10.2	47.4
E.L.	9.7	47.9
1+40 = N.L. Alley		
EL	10.6	47.0
+5	11.4	46.2
+7	11.2	46.4
cb	11.3	46.3
+2	12.5	45.1
+4	12.7	44.9
+4	12.2	45.4
1/4	12.0	45.6

Guizot

1+40		157.59		
℄			12.1	145.5
¼			12.5	45.1
+7			13.1	44.5
+8			13.4	44.2
cb			13.3	44.3
+1			12.5	45.1
+3			12.4	45.2
w.L			12.7	44.9
TP	0.02	144.57	13.04	144.55
1+60 = S.L		Alley		
w.L			0.8	43.7
cb			0.6	43.9
+05			1.5	43.1
+7			1.6	43.0
+2			1.2	43.4
¼			0 6	44.0
℄			0 3	44.3
¼			0 3	44.3
+4			0 7	43.9
+8			0 7	43.9
cb			+0.4	145.0
+5			+0.2	44.8
E.L.			+0 4	45.0

Guizot.

42

1+75	144.57		
E.L.		0 6	144.0
+7		0.6	44.0
cb		0 7	43.9
+05		1.5	43.1
¼		1.4	43.2
℄		1.2	43.4
¼		1.5	43.1
+65		2 1	42.5
+7		2.6	42.0
+8		2 5	42.1
cb		1.4	43.2
w.L		1.7	42.9
2+00			
w.L		3.3	41.3
+11		3.1	41.5
cb		4.2	40.4
+2		4.2	40.4
+3		3.9	40.7
+4		3.6	41.0
¼		3.2	41.4
℄		2 9	41.7
¼		2.9	41.7
+3		3 1	41.5
cb		3.1	41.5
+05		2 3	42.3

2+00	1445.7		
cb +5		2.2	142.4
+11		2.2	42.4
E.L.		1.9	42.7
2+25			
E.L.		3.3	41.3
+5		3.6	41.0
cb		3.7	40.9
+05		4.6	40.0
+5		4.7	39.9
+6		4.4	40.2
1/4		4.4	40.2
℄		4.3	403
+6		4.6	40.0
1/4		4.8	39.8
+4		5.3	393
cb		5.5	39.1
cb		4.6	40.0
w.L.		5.0	39.6

Guide +

2+50		
w.L.	6.5	138.1
cb	6.4	38.2
+1	7.2	37.4
+6	7.1	37.5
+7	6.7	37.9
1/4	6.5	38.1
℄	6.1	38.5
+6	6.0	38.6
1/4	6.0	38.6
+1	6.2	38.4
+8	6.0	38.6
cb	5.2	39.4
EL	4.7	39.9
2+75		
E.L.	6.3	38.3
+4	6.5	38.1
+7	6.4	38.2
cb	6.7	37.9
+1	7.4	37.2
+5	7.5	37.1
1/4	7.5	37.1
℄	7.6	37.0
1/4	8.1	36.5
+3	8.3	36.3
+6	8.8	35.8
+8	8.8	35.8

Guizot

2+75	144.57		
cb		7 9	136.7
+6		8 0	96.6
m.L.		7.9	36.7
2+95			
m.L.		6.6	38.0
+1		8.9	35.7
+7		9.1	35.5
+9		9.3	35.3
+10		9.7	34.9
cb		9.7	34.9
+2		9.7	34.9
+4		9.5	35.1
1/4		9.2	35.4
+4		9.2	35.4
¢		8 9	35.7
+5		8.8	35.8
1/4		8.7	35.9
+8		8 6	36.0
cb		8.2	36.4
+3		7.8	36.8
+9		7.6	37.0
EL		6.5	38.1

Guizot

144.57

41

3+00 = M.L. Bermuda		
E.L	7.6	137.0
+35 walk	8.53	136.04
+11 +abcb.endret	8.69	135.88
gut pav	9.37	135.20
1/4 v	9.33	35.24
¢ v	9.41	35.16
1/4 v	9.75	34.82
cb+1 gut v	10.25	34.32
cb+1 +abcb endret	9.69	34.88
+95 walk	9.61	34.96
m.L	9.0	35.57
0+00 = S.L. Bermuda		
m.L.	10.9	33.7
+3 walk	10.72	33.85
+11 +abcb endret	10.75	33.82
gut	11.35	33.22
1/4	10.78	33.79
¢	10.45	34.12
1/4	10.32	34.25
gut	10.32	34.25
cb+1 +abcb endret	9.70	34.87
+8 walk	9.46	35.11
E.L.	8.9	35.7

Guizot

0+25	144.57		
E.L.		3.6	141.0
+3		10.8	33.8
+11		11.0	33.6
cb		11.4	33.2
+1		11.9	32.7
1/4		11.6	33.0
℄		11.6	33.0
1/4		11.9	32.7
+3		12.2	32.4
+7		12.3	32.3
cb		11.8	32.8
+2		11.8	32.8
+8		12.2	32.4
WL.		12.0	32.6
0+50			
WL.		12.7	31.9
+5		12.6	32.0
+10		12.8	31.8
cb		13.2	31.4
+2		13.8	30.8
+4		13.8	30.8
1/4		13.1	31.5
℄		12.7	31.9
1/4		12.8	31.8
+2		12.9	31.7
+4		13.1	31.5

Guizot

45

0+50	144.57		
1/4 +8		13.1	131.5
cb		12.3	32.3
+7		12.3	32.3
+8		11.8	32.8
E.L.		5.0	39.6
T.P. 0.00	131.68	12.89	131.68
0+75			
E.L.		+7.0	138.7
+2		0.3	31.4
cb		0.7	31.0
+1		1.3	30.4
1/4		1.2	30.5
℄		1.2	30.5
+6		1.3	30.4
1/4		1.6	30.1
+4		2.2	29.5
+7		2.3	29.4
cb		1.7	30.0
+5		1.6	30.1
WL.		1.6	30.1

Guizot.

1+00	131.68		
W.L.		3.1	128.6
+11		2.6	29.1
cb		3.0	28.7
+12		3.5	28.2
+5		3.1	28.6
⅛		2.7	29.0
+4		2.4	29.3
℄		2.2	29.5
⅛		2.2	29.5
+8 S		2.4	29.3
cb		1.9	29.8
+1		1.5	30.2
+5		1.4	30.3
+10		1.1	30.6
E.L.		+4.2	35.9
1+32 6 = N.L. Alley			
E.L.		+1.2	32.9
+2		2.5	29.2
+4		2.9	28.8
cb		3.1	28.6
+1		3.2	28.5
+1		3.8	27.9
+7		3.8	27.9
⅛		3.6	28.1
℄		3.6	28.1

Guizot.

1+32 6		
⅛	4.0	127.7
+3	4.3	27.4
+7	4.9	26.8
cb	4.9	26.8
+2	4.3	27.4
W.L.	4.6	27.1
1+52 6 = S.L. Alley		
W.L.	5.5	26.2
+11	5.1	26.6
@ 6	6.0	25.0
+4	5.5	26.2
⅛	5.2	26.5
+4	4.7	27.0
℄	4.6	27.1
⅛	4.4	27.3
+8	4.8	26.9
cb	4.1	27.6
+11	3.8	27.9
E.L.	0.2	31.5

Guizot

131.68

1+75		
E.L.	0.8	130.9
+1	4.9	26.8
+3	5.1	26.6
cb	5.2	26.5
+1	5.9	25.8
+7	5.9	25.8
1/4	5.8	25.9
℄	5.8	25.9
1/4	6.3	25.4
+6	6.8	24.9
cb	7.0	24.7
+1	6.3	25.4
w.L	6.7	25.0
2+00		
w.L	8.0	23.7
+11	7.6	24.1
cb	8.3	23.4
+2	8.3	23.4
+3	8.1	23.6
1/4	7.5	24.2
℄	7.2	24.5
1/4	7.1	24.6
+8	7.2	24.5
cb	6.6	25.1
+6	6.5	25.2

Guizot

2+00		
cb+11	6.6	125.1
E.L.	1.6	130.1
2+25		
E.L.	4.6	27.1
+1	8.2	23.5
+3	8.4	23.3
+5	8.1	23.6
cb	8.0	23.7
+05	8.5	23.2
1/4	8.4	23.3
℄	8.4	23.3
1/4	8.8	22.9
+7	9.6	22.1
cb	9.3	22.4
+2	8.9	22.8
w.L.	9.3	22.4
2+50		
w.L.	10.6	21.1
+6	10.3	21.4
cb	10.5	21.2
+4	10.6	21.1
1/4	10.2	21.5
℄	9.9	21.8
1/4	9.8	21.9
+8	9.6	22.1
cb	9.2	22.5

Guizot

131.68

2+50			
ob+10		9.2	122.5
E.L.		2.3	29.4
2+75			
E.L.		4.5	27.2
+10 1		9.7	22.0
+7 10		10.1	21.6
cb		10.4	21.3
+1		10.6	21.1
1/4		10.8	20.9
+4		10.8	20.9
℄		11.1	20.6
+5		11.1	20.6
1/4		11.4	20.3
+6		11.6	20.1
cb		11.3	20.4
W.L.		11.4	20.3
M.H. at 1+42 6 end		3.84	27.84

Guizot

131.68

2+85 2 = N.L. Pt. Loma Ave.

W.L.		11.9	119.8
+4		11.7	20.0
+9		11.5	20.2
cb		11.6	20.1
1/4		11.6	20.1
℄		11.4	20.3
1/4		11.1	20.6
+8		10.9	20.8
cb		10.5	21.2
+7		10.1	21.2
E.L.		9.0	22.7
T.P. 0.40	119.28	12.80	118.88
T.P. 0.46	107.09	12.65	106.63
s.w. 9' tack Pascadero & Frovdo BM		12.36	94.73 (94.81)
T.P. 12.99	119.89	0.19	106.90
T.P. 13.01	132.81	0.09	119.80
T.P. 12.94	145.72	0.03	132.78
T.P. 13.06	158.59	0.19	145.53
T.P.x		1.60	156.99 (156.99)

B.P. S.W. Naragansett & Santa Barbara

X sec Naragansette From W.L. Santa Barbara to W.L. Catalina Blvd. 52' Rdway 14' cbs 80' street. to E cb line Venice.

BM.	7.25	225.93		218.68
0-60 = W.L Santa Barbara				
S cb			7.25	218.68
gut	Pav		8.00	17.93
1/4	✓		7.71	18.22
℄	✓		7.80	18.13
1/4	✓		8.18	17.75
gut	✓		8.91	17.02
N cb			8.32	17.61
0-50 = W cb Santa barbara				
N.L. top cb			8.55	17.38
N.L. gut			9.54	16.39
cb			8.9	17.0
1/4			8.3	17.6
℄			7.8	18.1
1/4			7.4	18.5
cb			7.7	18.2
+4			7.8	18.1
S.L. top cb			6.89	19.01
S.L. gut			6.9	19.0
0-40 = W 1/4 Santa Bar.				
S.L.			6.3	19.6
cb			6.7	19.2
1/4			7.1	18.8
℄			7.6	18.3
1/4			8.1	17.8

Curbs & Sidewalks all in

Sept 28
Loudon
Isbell
Morgan

0-40		
N cb	8.6	217.3
N.L	9.3	216.6
0-30 = ℄		
N.L	9.1	16.8
cb	8.4	17.5
1/4	7.8	18.1
℄	7.2	18.7
1/4	6.7	19.2
cb	6.3	19.6
S.L	5.8	20.1
0-20 = E 1/4 Santa Bar		
S.L	5.8	20.1
cb	6.2	19.7
1/4	6.6	19.3
℄	7.0	18.9
1/4	7.7	18.2
cb	8.3	17.6
N.L	9.1	16.8
0-10 = E cb Santa Bar.		
N.L top cb	8.17	17.76
N.L gut	8.6	17.3
cb	8.3	17.6
+7	8.0	17.9
1/4	7.9	18.0
℄	7.1	18.8
+2	7.0	18.9

0–10	225.93		
+8		7.2	218.7
1/4		6.9	19.0
cb		6.5	19.4
S.L. gut		5.8	20.1
S.L. top cb		6.14	19.79
0+00 = E.L. Santa Barb.			
Scb		6.02	19.91
gut		6.4	19.5
+8		6.7	19.2
1/4		6.6	19.3
℄		6.8	19.1
1/4		7.7	18.2
+9		8.3	17.6
+10		8.5	17.3
gut		8.6	17.3
Ncb		8.00	17.9
0+25			
Ncb		7.74	18.19
gut		8.2	17.7
+3		8.2	17.7
1/4		7.3	18.6
℄		6.4	19.5
+4		6.2	19.7
1/4		6.2	19.7
+9		6.4	19.5
gut		6.2	19.7

225.93

0+25		
Scb	5.74	220.19
0+50		
Scb	5.36	220.57
gut	5.9	20.0
+3	6.0	19.9
1/4	5.6	20.3
+11	5.9	20.0
℄	6.0	19.9
1/4	6.7	19.0
+9	7.7	18.2
gut	7.9	18.0
Ncb	7.33	18.60
0+75		
Ncb	6.98	18.95
gut	7.3	18.6
+3	7.5	18.4
1/4	6.5	19.4
℄	5.6	20.3
1/4	5.4	20.5
+6	5.4	20.5
+10	5.7	20.2
gut	5.5	20.4
Scb	5.00	20.9

Naragansett

225.93

1+00		
Scb	4.63	221.30
gut	5.2	20.7
+3	5.3	20.6
+7	5.2	20.7
1/4	5.1	20.8
℄	5.3	20.6
1/4	6.2	19.7
+10	7.1	18.8
gut	7.0	18.9
Ncb	6.61	19.32
1+25		
Ncb	6.27	19.66
gut	6.4	19.5
+4	6.5	19.4
1/4	5.9	20.0
℄	5.0	20.9
1/4	4.9	21.0
+9	5.1	20.8
gut	4.8	21.1
Scb	4.29	21.64

Naragansett

51

1+50		
Scb	3.95	21.98
gut	4.6	21.3
+4	4.7	21.2
1/4	4.6	21.3
℄	4.7	21.2
1/4	5.4	20.5
+10	6.1	19.8
gut	6.0	19.9
Ncb	5.92	20.01
1+75		
Ncb	5.62	20.31
gut	5.8	20.1
+4	5.7	202
1/4	5.0	20.9
℄	4.3	21.6
1/4	4.2	21.7
+5	4.1	21.8
+10	4.3	21.6
+12	4.0	21.9
gut	4.2	21.7
Scb	3.61	22.32

Narragansett

225.93

2+00		
Scb	3.29	22.64
gut	3.8	22.1
+1	3.6	22.3
+2	3.9	22.0
+4	4.0	21.9
¼	3.8	22.1
℄	3.9	22.0
¼	4.8	21.1
+9	5.4	20.5
gut	5.3	20.6
Ncb	5.26	20.67
2+25		
Ncb	4.87	21.06
gut	4.9	21.0
+6	5.0	20.9
¼	4.4	21.5
℄	3.5	22.4
¼	3.4	22.5
+9	3.6	22.3
gut	3.4	22.5
Scb	2.90	23.0

Narragansett

52

2+50		
Scb	2.52	22.37
gut	3.1	2.8
+4	3.2	2.7
¼	3.1	2.8
℄	3.2	2.7
¼	4.2	1.7
+6	4.7	1.2
gut	4.8	1.1
Ncb	4.55	1.38
2+75		
Ncb	4.26	1.67
gut	4.4	1.5
+5	4.6	1.3
¼	3.9	2.0
℄	3.1	2.8
¼	2.9	3.0
+9	3.0	2.9
gut	2.6	3.1
Scb	2.26	3.67

3+00	225.93		
Scb		2.20	223.70
gut		2.8	23.1
+4		3.0	22.9
1/4		3.1	22.8
+9		3.2	22.7
+12		3.1	22.8
℄		3.2	22.7
1/4		4.0	21.9
+7		4.5	21.4
gut		4.5	21.4
Ncb		4.12	21.81
3+25			
Ncb		4.32	21.61
gut		4.6	21.3
+5		4.7	21.2
+8		4.5	21.4
1/4		4.2	21.7
℄		3.4	22.5
+3		3.3	22.6
1/4		3.4	22.5
+9		3.3	22.6
gut		3.1	22.8
Scb		1.44	23.49

3+50		
Scb	2.95	222.98
gut	3.7	22.2
+5	3.8	22.1
1/4	3.7	22.2
+11	3.8	22.1
℄	3.8	22.1
1/4	4.6	21.3
+7	5.1	20.8
+8	5.4	20.5
+11	5.3	20.6
gut	4.9	21.0
Ncb	4.82	21.11
3+75		
Ncb	5.52	20.41
gut	5.5	20.4
+1	5.7	20.2
+4	6.2	19.7
+5	6.2	19.7
+7	5.5	20.4
1/4	5.4	20.5
℄	4.4	21.5
+4	4.3	21.6
1/4	4.2	21.7
+8	4.4	21.5
+12	4.3	21.6
gut	4.5	21.4

Narragansett

3+75		225.93		
Scb			3.75	222.18
TP	0.39	221.97	4.35	221.58
H+00				
Scb			0.76	221.21
gut			1.1	20.9
+1			1.1	20.9
+3			1.7	20.3
+5			1.4	20.6
1/4			1.1	20.9
+11			1.1	20.9
℄			1.2	20.8
1/4			2.2	19.8
+7			2.9	19.1
+8			3.2	18.8
+10			3.3	18.7
+11			2.7	19.3
gut			2.9	19.1
Ncb			2.45	19.52
H+2.5				
Ncb			3.40	18.57
gut			3.7	18.3
+2			3.9	18.1
+3			4.3	17.7
+6			4.3	17.7
+7			3.7	18.3
1/4			3.1	18.9

Narragansett

H+25		
℄	2.2	219.8
+3	2.0	20.0
1/4	2.1	19.9
+7	2.6	19.4
+9	3.1	18.9
+10	3.0	19.0
+11	2.7	19.3
gut	2.0	20.0
Scb	1.91	20.06
4+50		
Scb	3.12	18.85
gut	3.2	18.8
+3	3.7	18.3
+4	4.4	17.6
+6	3.7	18.3
1/4	3.4	18.6
+10	3.4	18.6
℄	3.5	18.5
1/4	4.2	17.8
+6	4.8	17.2
+6.5	5.6	16.4
+7.5	5.6	16.4
+8	5.2	16.8
gut	4.6	17.4
Ncb	4.37	17.60

Narragansett

221.97

4+75			
Ncb		5·39	16 58
gut		5·8	16.2
+4		6·7	15.3
+4⅝		7.5	14.5
+5		6·9	15.1
+6		6·8	15.2
+6⅝		6·3	15.7
1/4		5·7	16.3
±		5·0	16.0
¼		4·9	17.1
+7		5·2	16.8
+9		6·1	15·9
+11		5·3	16.7
gut		4·7	17.3
Scb		4·50	17.47
5+00			
Scb.		6·36	15.61
gut		6·4	15.6
+3⅝		7.5	14.5
+4⅝		7·7	14.1
+5		7·2	14.8
¼		6·6	15.4
±		6·7	15.3
¼		7·2	15·8

Narragansett

55

5+00		
¼+6	7·7	214.3
+7	8·4	13,6
+8	8·d	13.6
+9	9·2	12.8
+10	8·2	13.8
gut	7·7	14.3
Ncb	7·13	14.84
5+25		
Ncb	9·31	12.66
gut	10·1	11.9
+3	10·3	11.7
+4	11·5	10.5
+5	11·4	10.6
+6	10·7	11.3
+8	9·9	12.1
¼	9·5	12.5
±	9·0	13.0
¼	8·8	13.2
+7	9·1	12.9
+8	9·7	12.3
+9	9·8	12.2
+10	9·3	12.7
gut	8·9	13.1
Scb	8·79	13.18

Narragansett

5+50		221.97		
Scb			11.34	210.63
gut			11.6	10.4
+4			12.0	10.0
+5			12.3	09.7
+6			11.8	10.2
1/4			11.5	10.5
℄			11.5	10.5
1/4			12.1	9.9
+6			12.6	9.4
+7			13.7	8.3
+8			13.7	8.3
+8.5			13.1	8.9
gut			12.8	9.2
Ncb			11.79	10.18
TP	0.12	209.15	12.94	209.03
5+75				
Ncb			1.45	207.70
gut			1.9	7.3
+2			1.9	7.3
+4			2.7	6.5
+6			2.7	6.5
+7			2.1	7.1
1/4			1.7	7.5
℄			1.1	8.1
+4			1.1	8.1

Narragansett

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5+75	209.15	
1/4	1.5	207.7
+5	1.7	7.5
+6	1.8	7.4
+11	2.1	7.1
gut	1.8	7.4
Scb	1.20	8.0
6+00 = w.c. Venice.		
Scb	3.95	205.20
gut	3.9	5.3
+6	3.8	5.4
1/4	3.6	5.6
+12	3.1	6.1
℄	3.1	6.1
1/4	3.7	5.5
+7	4.1	5.1
gut	4.2	5.0
Ncb	3.91	5.24
6+10 = wcb Venice		
N.L top cb	4.00	5.15
N.L gut	4.8	4.4
cb	5.0	4.2
1/4	4.4	4.8
℄	4.1	5.1
+3	4.0	5.2
1/4	4.2	5.0

6+10	209.15		
cb		4.6	204.6
S.L. gut		4.6	4.6
S.L. top cb		3.94	5.21
6+20 = W ¼ Venice			
S.L.		4.8	4.4
cb		5.2	4.0
¼		4.8	4.4
℄		4.6	4.6
¼		4.9	4.3
cb		5.3	3.9
N.L.		5.1	4.1
6+30 = ℄ Venice.			
N.L.		5.6	3.6
cb		5.8	3.4
+1		5.9	3.3
+3		5.6	3.6
¼		5.4	3.8
℄		5.1	4.1
¼		5.3	3.9
cb		5.7	3.5
S.L.		5.1	4.1

6+40 = ~~E~~ ¼ Venice		
S.L.	5.7	203.5
cb	6.2	3.0
¼	5.8	3.4
+10	5.5	3.7
℄	5.5	3.7
¼	5.8	3.4
cb	6.4	2.8
N.L.	6.0	3.2

40' Rdway 20' cbs From 6+50 to Catalina.

6+50 = E cb Venice		
N.L. top cb	6.00	203.20
N.L. gut	6.1	3.1
+15	6.4	2.8
cb	7.1	2.1
¼	6.3	2.9
℄	6.0	3.2
+8	6.1	3.1
¼	6.2	3.0
cb	6.9	2.3
+2	7.1	2.1
+9	6.3	2.9
S.L. gut	6.1	3.1
S.L. top cb	5.95	3.20

Naragansett

209.15

6+60 = 0+00 = E.L. Venice			
Scb		6.36	202.79
gut		6.5	2.7
+4		7.4	1.8
1/4		6.8	2.4
+6		6.5	2.7
℄		6.5	2.7
+7		6.7	2.5
1/4		6.9	2.3
+5		7.3	1.9
+8		7.1	2.1
gut		6.6	2.6
Ncb		6.36	2.79
0+25			
Ncb		7.33	1.82
gut		7.3	1.9
+1		7.4	1.8
+6		8.4	0.8
1/4		7.8	1.4
+7		7.4	1.8
℄		7.4	1.8
+6		7.6	1.6
1/4		8.0	1.2
+4		8.6	0.6
+9		7.3	1.9
gut		7.3	1.9
Scb		7.29	1.86

Naragansett

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0+50	209.15		
Scb		8.45	200.70
gut		9.1	200.1
+6		9.6	199.6
1/4		9.3	199.9
+3		8.7	200.5
+8		8.5	00.7
℄		8.5	00.7
1/4		8.9	00.3
+4		9.5	199.7
gut		8.8	200.4
Ncb		8.45	200.70
0+75			
Ncb		10.47	198.68
gut		10.6	198.6
+1		11.0	98.2
+7		11.4	97.8
1/4		11.0	98.2
℄		10.7	98.5
+3		10.8	98.4
1/4		11.0	98.2
+4		11.5	97.7
+9		11.2	98.0
gut		10.7	98.5
Scb		10.37	98.78
T.P. 0.48	196.56	13.07	196.08

1+00	196.56		
Scb		0.52	196.04
qut		0.6	96.0
+1		1.1	5.5
+6		2.0	4.6
1/4		1.3	5.3
℄		1.0	5.6
1/4		1.3	5.3
+4		1.8	4.8
+5		1.4	5.2
+6		1.2	5.4
qut		0.7	5.9
Ncb		0.57	5.99
1+25			
Ncb		3.79	192.77
qut		4.0	2.6
+2		4.5	2.1
+6		4.8	1.8
+9		4.9	1.7
1/4		4.5	2.1
+5		4.2	2.4
℄		4.3	2.3
+8		4.5	2.1
1/4		4.9	1.7
+4		5.0	1.6
+9		4.1	2.5
qut		3.8	2.8

1+25		
Scb	3.70	192.86
1+50		
Scb	7.18	189.38
qut	7.4	9.2
+1	7.7	8.9
+7	8.7	7.9
1/4	8.5	8.1
+1	8.1	8.5
℄	7.6	9.0
1/4	8.0	8.6
+1	8.2	8.4
+4	8.2	8.4
qut	7.4	9.2
Ncb	7.15	9.41
1+75		
Ncb	10.55	186.01
qut	10.8	185.8
+6	11.5	5.1
+9	11.6	5.0
1/4	11.3	5.3
+1	11.1	5.5
℄	10.8	5.8
+5	10.9	5.7
+9	11.2	5.4
1/4	11.5	5.1

Naragansett

		1956		
+4			11.7	184.9
+8			11.2	5.4
qut			11.1	5.5
Scb			10.51	6.05
T.P.	0.22	183.75	13.03	183.53
2+00				
Scb			0.80	182.95
qut			09	2.9
+1			1.1	2.7
+7			1.7	2.1
¼			1.4	2.4
+1			1.1	2.7
℄			0.9	2.9
+9			1.2	2.6
¼			1.3	2.5
+5			1.6	2.2
qut			1.0	2.8
Ncb			0.94	182.81
2+25				
Ncb			3.64	180.11
qut			3.8	0.10
+6			4.3	179.5
¼			4.0	179.8
+1			3.8	180.0
℄			3.5	180.3

Naragansett

60

2+25		
℄ +6	3.4	180.4
¼	3.7	80.1
+4	4.2	79.6
qut	3.7	80.1
Scb	3.64	80.11
2+50		
Scb	5.66	178.09
qut	5.5	8.3
+6	6.1	7.7
+8	5.7	8.1
¼	5.6	8.2
℄	5.6	8.2
+9	5.9	7.9
¼	6.2	7.6
+4	6.5	7.3
+5	6.2	7.6
qut	5.8	8.0
Ncb	5.72	178.03
2+75		
Ncb	7.13	176.62
qut	7.3	6.5
+8	7.8	6.0
¼	7.4	6.4
℄	6.9	6.9
¼	7.0	6.8
+1	7.0	6.8

Naragansett

2+75	183.75		
1/4+5		7.6	176.2
+8		7.0	176.8
gut		6.7	7.1
Scb		6.80	6.85
3+00			
Scb		7.84	175.91
gut		7.9	5.9
+5		8.4	5.4
1/4		8.0	5.8
+9		7.9	5.9
℄		7.9	5.9
+9		8.4	5.4
1/4		8.5	5.3
+4		9.1	4.7
+6		8.9	4.9
+8		9.5	5.3
gut		8.3	5.5
Ncb		8.33	5.42
3+25			
Ncb		9.40	174.35
gut		9.5	4.3
+4		9.9	3.9
+5		10.2	3.6
+8		9.91	3.9
1/4		9.5	4.3

Naragansett

61

3+25		
℄	8.9	174.9
+2	8.9	4.9
1/4	9.0	4.8
+1	9.1	4.7
+5	9.6	4.2
gut	9.1	4.7
Scb	8.80	4.95
3+50		
Scb	10.02	173.73
gut	10.3	3.5
+6	11.0	2.8
1/4	10.2	3.6
℄	10.2	3.6
+9	10.6	3.2
1/4	10.9	2.9
+2	11.3	2.5
+5	11.5	2.3
gut	10.9	2.9
Ncb	10.62	3.13
3+75		
Ncb	12.24	1.71
gut	12.4	1.4
+2	12.9	0.9
+7	13.2	0.6
1/4	12.9	09
+5	12.3	15

Naragansett

3+75		183 75		
℄			12.0	171.8
¼			12.1	1.7
+5			12.7	1.1
gut			12.0	1.8
Scb Nail Pole			11.64	2.11
T.P.	0 38	171.06	13.07	170.68
4+00				
scb			0.85	170.21
gut			1.1	70.0
+1			1.5	69.6
+5			2.1	69.0
¼			1.5	69.6
℄			1.4	69.7
+5			1.6	69.5
¼			2.4	68.7
+3			2.9	68.2
+8			2.1	69.0
gut			1.8	69.3
Ncb			1.55	69 51
4+35 = w.L. Alley on North.				
N.L.	top cb	alley cb	4.26	166 80
N.L	gut		4.1	67.0
Ncb			4.46	66.60
gut			5.0	66.1
+2			5.6	65.5
+6			5 7	65 4

Naragansett

62

4+35	
¼	
+5	
+7	
℄	
¼	
+5	
+8	
gut	
Scb	
4+50 = E.L Alley on North	
5cb	
gut	
+3	
+7	
¼	
℄	
+9	
¼	
+3	
+8	
gut	
Ncb	
N.L top Alley cb	
N.L gut (alley)	

5.0	166.1
4.6	66.5
4.4	6.7
4.4	6.7
4.6	6.5
5.1	6.0
4.9	6.2
4.2	6.9
3.97	67.09
5.52	65.54
5.6	65. 5
6.4	64.7
6.5	64.6
6.0	5.1
5.8	5.3
6.2	4.9
6.3	4.8
6.7	4.4
6.7	4.4
6.1	5.0
5.94	5.12
5.50	5.56
5.0	6.1

4+75	171.06		
Ncb		8.12	162.94
gut		8.4	2.7
+5		8.8	2.3
1/4		8.6	2.5
+6		8.2	2.9
℄		8.2	2.9
1/4		8.2	2.9
+4		8.8	2.3
+8		8.6	2.5
gut		8.1	3.0
Scb		8.02	3.04
4+98½ = B.C. ret on South			
Scb		10.25	160.81
gut		10.9	0.2
+4		10.6	0.5
1/4		10.6	0.5
+3		10.3	0.8
℄		10.5	0.6
+5		10.6	0.5
1/4		10.9	0.2
+5		11.2	159.9
gut		10.9	160.2
Ncb		10.26	160.80

171.06

5+148½ = B.C. ret on North		
Ncb	11.64	159.42
gut	11.9	9.2
+6	12.5	8.6
1/4	12.2	8.9
℄	12.0	9.1
1/4	12.1	9.0
+7	12.2	8.9
cb	12.0	9.1
+3 gut	11.70	159.36
+3 top cb on S. ret.	11.68	159.38
5+26.		
5.L.+10 top cb on S. ret	12.80	58.26
TP 7.31 165.84	12.53	158.53
gut at S.L.+10	8.2	7.6
Scb	7.8	8.0
+8	7.4	8.4
1/4	7.3	8.5
℄	7.6	8.2
1/4	7.9	7.9
+7	8.3	7.5
cb	8.1	7.7
+1½ gut	7.9	7.9
+1¼ top cb on N ret	7.26	158.58

Naragansett

1658 4

5+26[1] on South = 5+37[2] on North

end section on E.L. Catalina

N.L. +14[25]	top cb on N	ret+8.06		157.78
gut	Pav		8.71	57.13
cb	"		8.61	57.23
1/4	"		8.43	7.41
℄	"		8.36	7.48
1/4	"		8.30	7.54
cb	"		8.40	7.44
+11[8]	gut		8.46	7.38
+18[8]	top cb on S.	ret+7.78		8.06
T.P.	12.32	177.89	0.27	165.57
T.P.	12.95	190.55	0.29	177.60
T.P.	12.74	203.10	0.19	190.36
Nail Pole B.M.	SE Venice & Naragansett		0.01	203.09
	12.52	215.61		203.09
T.P.	11.94	227.45	0.00	215.61
B.M.	Beginning		8.77	218.68

X Sec. Venice – Naragansett to DelMonte

64

All cbs = sidewalks in on East.

Unlike cbs in on West 0+00 to 1+40

60' st. 10' cbs 40 Raiway.

B.M. 998 213.07 203.09

0+00 = S.L. Naragansett

Ecb	9.86	203.21
gut	10.0	3.1
+4	10.4	2.7
1/4	9.7	3.4
℄	9.0	4.1
+6	8.7	4.4
1/4	8.7	4.4
gut	8.5	4.6
wcb	7.85	5.22
0+25		
wcb	6.80	6.27
gut	7.7	5.4
1/4	7.7	5.4
+5	7.7	5.4
℄	8.0	5.1
1/4	8.8	4.3
+6	9.4	3.7
gut	9.3	3.8
Ecb	9.00	4.1

0+50	213.07		
Ecb		8.02	205.05
gut		8.3	4.8
+4		8.6	4.5
¼		7.8	5.3
℄		7.1	6.0
¼		6.6	6.5
gut		6.7	6.4
wcb		5.79	7.28
0+75			
wcb		4.75	8.32
gut		5.9	7.2
¼		5.6	7.5
℄		6.0	7.1
¼		6.7	6.4
+6		7.5	5.6
gut		7.3	5.8
Ecb		6.88	6.19
1+00			
Ecb		5.73	7.34
gut		6.5	6.6
+4		6.4	6.7
¼		5.7	7.4
℄		4.9	8.2
¼		4.6	8.5
+8		4.8	8.3
gut		4.7	8.4

1+00		
Wcb	3.68	209.39
1+40 = N.L. Alley	= end ebo 2 walk = on West.	
W.L. top Alley cb	1.98	211.09
W.L. gut.	1.8	11.3
Wcb	2.14	10.93
gut	2.9	10.2
+5	3.3	09.8
¼	3.3	9.8
℄	3.4	9.7
¼	3.9	9.2
+6	4.5	8.6
gut	4.4	8.7
Ecb	4.09	8.98
E.L. Alley gut.	4.4	8.7
E.L. top Alley cb	3.84	9.23
1+60 = S.L. Alley		
E.L. top Alley cb	3.24	9.83
E.L. gut	3.9	9.2
Ecb	3.41	9.66
gut	4.2	8.9
¼	3.4	9.7
47	2.9	10.2
℄	2.9	10.2
¼	2.8	10.3
+8	2.8	10.3

Venice

1+60	231.07		
ebb		2.9	210.2
+2		2.8	10.3
+4		1.9	11.2
w.l.		1.9	11.2
2+00			
w.l.		1.2	11.9
+6		1.3	11.8
+8		2.0	11.1
eb		2.1	11.0
1/4		2.0	11.1
±		1.9	11.2
1/4		2.6	10.5
gut		3.5	9.6
Feb		3.15	9.92
2+25			
Feb		3.06	210.01
gut		3.1	10.0
+1		3.3	9.8
+5		3.0	10.1
1/4		2.5	10.6
±		1.8	11.3
1/4		1.8	11.3
eb		1.9	11.2
+2		1.9	11.2
+4		1.0	12.1
W.L.		1.0	12.1

Venice

66

2+50		
w.l.	1.0	212.1
+7	1.2	11.9
+8	1.7	11.4
+9	1.9	11.2
eb	1.9	11.2
1/4	1.8	11.3
±	1.9	11.2
+2	1.9	11.2
1/4	2.4	10.7
+6	3.0	10.1
gut	3.2	09.9
Feb	2.99	210.08
2+75		
Feb	2.91	210.16
gut	3.0	10.1
+3	2.9	10.2
1/4	2.3	10.8
±	1.9	11.2
1/4	1.7	11.4
eb	1.7	11.4
+1	1.8	11.3
+2	1.6	11.5
+3	1.0	12.1
+6	0.7	12.4
w.l.	0.8	12.3

Venice

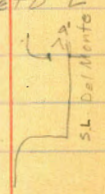
213.07

3+00 = ℄ N.L. Del Monte

w.l.	0 3	212.8
+6	0.5	12.6
+9	1.4	11.7
cb	1.6	11.5
+5	1.8	11.3
1/4	1.8	11.3
℄	2.0	11.1
+5	2.1	11.0
1/4	2.4	10.7
+6	2.8	10.3
gut	3.1	210.0
Ecb	2.83	

3+04 = end w ret. cb does not come to P.

+ob wcb 0.61



Xsec Venice – Naragansett to Niagra

60'st 40'cbs 40' Rdway. All cbs > walls 3 in.

213.07

0+00 = ℄ N.L. Naragansett.

Ecb	9.87	203.20
gut	10.0	03.1
+2	10.3	2.8
1/4	10.0	3.1
℄	9.5	3.6
1/4	9.0	4.1
+6	8.9	4.2
gut	8.7	4.4
wcb	7.91	205.16
0+25		
wcb	7.38	205.69
gut	8.3	01.8
+1	8.1	5.0
+2	8.4	4.7
1/4	8.7	4.4
℄	8.6	4.5
+5	8.8	4.3
1/4	9.1	4.0
+4	9.5	3.6
gut	9.3	3.8
Ecb	9.13	3.94

Venice

213.07

0+50			
Ecb		6.51	204.56
gut		8.8	4.3
+6		8.8	4.3
1/4		8.5	4.6
+7		8.1	5.0
℄		8.0	5.1
1/4		8.1	5.0
+3		7.9	5.2
gut		7.8	5.3
wcb		6.89	6.18
0+75			
wcb		6.29	6.78
gut		7.0	6.1
+1		7.2	5.9
+6		7.2	5.9
1/4		7.4	5.7
+5		7.5	5.6
℄		7.3	5.8
+5		7.5	5.6
1/4		7.8	5.3
+3		8.1	5.0
+7		7.9	5.2
gut		8.1	5.0
Ecb		7.75	5.32

Venice

1+00		
Ecb	7.12	205.95
gut	7.3	5.8
+6	7.4	5.7
1/4	7.1	6.0
+5	6.8	6.3
℄	6.7	6.4
+6	6.8	6.3
1/4	6.7	6.4
+4	6.4	6.7
+9	6.4	6.7
gut	6.1	7.0
wcb	5.75	7.32
1+40 = S.L. Alley		
W.L. top Alley cb	4.63	208.44
W.L. gut	5.0	8.1
wcb	4.84	8.23
gut	5.3	7.8
+5	5.2	7.9
1/4	5.4	7.7
℄	5.5	7.6
+7	5.7	7.4
1/4	5.6	7.3
+4	6.1	7.0
+8	6.0	7.1
gut	6.3	6.8
Ecb	6.06	7.01

1+40		213.07		
E.L.	top Alley cb		5.82	207.25
E.L.	gut		6.0	7.1
T.P.	11.07	219.12	5.02	208.05
1+60				
E.L.	top Alley cb		11.12	208.00
E.L.	gut		11.6	7.5
Ecb			11.32	7.80
gut			11.4	7.7
+6			11.2	7.9
1/4			11.1	8.0
+7			11.0	8.1
℄			10.8	8.3
1/4			10.8	8.3
gut			10.4	8.7
Wcb			10.25	8.87
W.L.	top Alley cb		10.15	8.97
W.L.	gut		10.2	8.9
2+00				
Wcb			8.24	10.88
gut			8.4	10.7
+2			8.7	10.4
+5			8.8	10.3
+7			8.5	10.6
1/4			8.6	10.5
℄			8.8	10.3
+3			8.8	10.3

2+00		
1/4	9.1	210.0
+3	9.0	10.1
gut	9.2	09.9
Ecb	9.07	10.05
2+25		
Ecb	7.37	11.75
gut	7.4	11.7
+5	7.2	11.9
+6	7.5	11.6
1/4	7.5	11.6
℄	7.1	12.0
+6	7.0	12.1
1/4	7.1	12.0
+3	7.2	11.9
+35	7.7	11.4
+4	7.5	11.6
+6	7.3	11.8
gut	7.2	11.9
Wcb	6.72	12.40

Venice

2+50	219.12		
Wcb		5.13	214.99
gut		5.3	13.8
+3		5.5	3.6
+4		5.4	3.7
+6		5.6	3.5
+6 5		6.1	3.0
+7		5.7	3.4
+9		5.5	3.6
1/4		5.5	3.6
&		5.4	3.7
1/4		5.6	3.5
+1		5.7	3.4
+4		6.0	3.1
+5		5.5	3.6
gut		5 7	3.4
Ecb		5.56	3.56
2+75			
Ecb		3.87	215.25
gut		4.1	5.0
+5		4.1	5.0
+8		4.3	4.8
1/4		4.1	5.0
&		4.0	5.1
+5		3.9	5.2
1/4		4.0	5.1

Venice

2+75	219.12		
1/4+3		4.1	215.0
+5		4.3	4.8
+6		4.0	5.1
gut		4.0	5.1
Wcb		3.59	5.53
3+00			
Wcb		2.02	217.10
gut		2.7	6.4
+4		2.7	6.4
+5		3.0	6.1
+7		2.8	6.3
+9		3.0	6.1
1/4		2.9	6.2
+5		2.8	6.3
&		2.8	6.3
+5		2.8	6.3
1/4		3.0	6.1
+4		3.1	6.0
+6		2.9	6.2
gut		2.8	6.3
Ecb		2.26	6.86
T.P 2.12.	210.19	11.05	208.07
BM Beginning		7.07	203.12

Cross levels on Poe St From Chatsworth Blvd. to La Cresta Drive

North = Right S = Left

B.M. X.E. Tennyson & Harrington

BM	3.19	88.87		85.68
T.P.	1.45	89.38	0.94	87.93
0+00 = w.l. Chatsworth				
Ncb			11.37	78.01
Scb			10.40	78.98
F.L. culvert N ret.			13.70	75.68
F.L. " S ret			14.29	5.09
0+25				
Scb			8.95	80.43
Ncb			9.95	79.43
0+50				
Ncb			8.47	80.91
Scb			7.52	81.86
0+75				
Scb			5.99	83.39
Ncb			7.02	82.36
0+90 = B.C.				
Ncb			6.16	83.22
Scb			5.01	84.37
Curve in 3 parts				
1				
Scb			3.95	85.43
Ncb			4.74	84.64
2				
Ncb			3.25	86.13
Scb			2.76	86.62

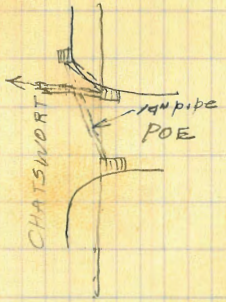
Sept. 29-28

Loudon
Isbell
Morgan.

60' St 40 Rdway
10' cbs

3.95
10.34
14.29

71



89.38

F.C. = 0+00			
Scb		1.85	87.53
Ncb		1.91	87.47
0+25			
Ncb		1.05	88.33
Scb		0.91	88.47
0+50			
Scb		0.02	89.36
Ncb		0.19	89.19
T.P. 12.05	101.28	0.15	89.23
0+75			
Ncb		10.88	90.40
Scb		10.93	90.35
1+00			
Scb		9.86	91.42
Ncb		9.87	91.41

Poe

10128

1+25			
Ncb	8.87	92.41	
Scb	8.88	92.40	
1+50			
Scb	7.91	93.37	
Ncb	7.89	93.39	
1+75			
Ncb	6.93	94.35	
Scb	6.97	94.31	
2+00			
Scb	5.91	95.37	
Ncb	5.97	95.31	
2+25			
Ncb	4.97	96.31	
Scb	4.85	96.43	
2+50			
Scb	3.79	97.49	
Ncb	3.89	97.39	
2+75			
Ncb	2.91	98.37	
Scb	2.74	98.54	
3+00			
Scb	1.76	99.52	
Ncb	1.95	99.33	

Poe.

73

10128

3+25			
Ncb		0.88	100.40
Scb		0.86	100.42
3+50			
T.P. 12 97	114.08	0.17	101.11
Scb		12.61	101.47
Ncb		12.66	1.42
3+75			
Ncb		11.58	2.50
Scb		11.52	2.56
4+00			
Scb		10.40	103.68
Ncb		10.42	103.66
4+25			
Ncb		8.95	5.13
Scb		8.82	5.26
4+50			
Scb		6.96	107.12
Ncb		6.94	107.14
4+75			
Ncb		4.45	109.63
Scb		4.34	109.74
5+00			
Scb		1.49	112.59
Ncb		1.63	112.45

Poe

114.08

T.P.	12.84	126.63	0.29	113.79
5+25				
Ncb			11.44	115.19
Scb			11.30	115.33
5+50				
Scb			8.49	118.14
Ncb			8.66	117.97
5+75				
Ncb			6.01	120.62
Scb			5.65	120.98
6+00				
Scb			2.82	123.81
Ncb			3.23	123.40
6+17.9 = B.C. return on North.				
Ncb			1.19	125.44
Scb			0.95	125.68
T.P	3.74	130.22	0.15	126.48
6+37 = BC ret on South				
Scb			2.45	127.77

return on South in 3 parts

1				
Scb			1.57	128.65
2				
Scb			0.86	129.36
E.C. on Lacresta				
Scb			0.53	129.69

Returns plotted 10-9-1928

Poc.

643
617.4
25.6

73

130.22

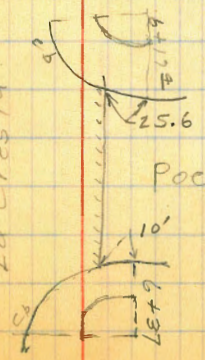
return on North in 3 parts

1		
Ncb	3.07	127.15
2		
Ncb	2.00	128.22
E.C. on Lacresta		
Ncb	1.54	128.68

(end Pavement Lacresta)

Scc on E.L. Lacresta brod. thru Intersection

2.5 sot scb line top cb gut	1.66	128.56
gut	2.29	127.93
scb line	2.23	127.99
1/4	2.12	
E	2.19	
1/4	2.28	
Ncb line	2.55	127.67
9.25 N of Ncb line. gut.	2.99	127.23
top cb	2.36	127.86



		Poe.		
		130.22		
T.P.	0.24	117.41	13.05	117.17
T.P	0.39	104.77	13.03	104.38
T.P.	2.77	94.79	12.75	92.02
B.M. Beginning.			9.09	85.70

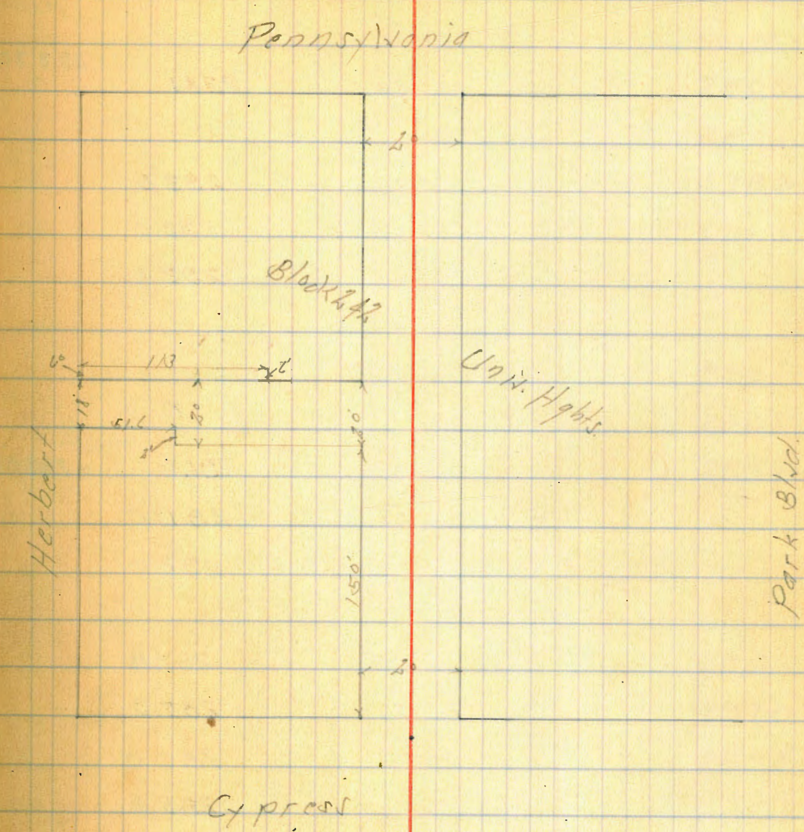
Cross Section East & West Alley Blk 242 Univ. Hghts
Cypress - Pennsylvania Herbert & Park Blvd

10-31-28
Sisson
McHugh
Kanagy
Flood

7

Plotted 11-7-28- CBHough

BM	6.89	297.38		290.49	S.E.B.P Cypress & Herbert
		E.L. Herbert			
S			3.7	293.7	
℄			4.4	293.0	
N			4.6	292.8	
+L Gutter			4.8		
+L Top Curb			4.26	293.12	
		25' E of E.L. Herbert			
-L Top Curb			4.04	293.34	
Gutter			4.5	292.9	
N			4.3	293.1	
℄			4.1	293.3	
+L			3.9		
S			3.3	294.0	
		51.6' E			
S	Garage 1.0 in Alley on Conc Floor		2.93 ↓	294.45	51.6' E ℄ Garage 1' N of S.L.
℄			3.7	293.7	Conc Floor 3.01 = 294.37
N			4.0	293.4	
+L on			4.2		64' E = ℄ Garage 1' N of S.L.
on Top Curb			3.98	293.40	Conc Floor 3.30 = 294.08
		75' E			
-L Top Curb			3.83	293.55	
Gutter			4.2		
N			4.2	293.2	
℄			4.1	293.3	



		297.38			
+6 = N Edge Conc Walk			3.59	293.79	104'E = East End of Existing Cb. on N
+8.5 = Stucco Fence					4.18 = 293.20
S			3.3	294.1	
		113'E			
S			3.9	293.5	
℄			4.4	293.0	
N			4.8	292.6	
+6			4.7		
TP	1.50	294.28	4.60	292.78	
		133'E			119'F = Garage 45 of S.L. Conc Floor
N			2.8	291.5	0.20 = 294.08
℄			3.3	291.0	
S			2.3	292.0	
		145'E			
-10			6.5	287.8	
S			7.0	287.3	
℄			7.3	287.0	
N			9.1	285.2	
+10			12.3		
		160'E			
-15			17.8		
-2			16.5		
N			13.7	280.6	
℄			11.5	282.8	
S			10.8	283.5	

	294.28		
+10		9.4	
	173'E		
-10		12.4	281.9
S		13.4	280.9
℄		14.2	280.1
N		16.0	278.3
+20		18.1	276.2
	200'E		
-20		16.1	
N		14.2	280.1
℄		12.2	282.1
S		10.9	283.4
+10		10.6	
	220'E		
-10		9.1	
S		8.6	285.7
℄		7.3	287.0
N		5.8	288.5
+10		5.2	
	235'E		
-5		2.3	
N		2.3	292.0
+2		2.3	
+7		4.2	
℄		4.1	290.2
S		3.5	290.8

		294.38		
45			3.5	
		353' E		
-20 = 2 Garage			0.6	
5			1.1	293.2
2			1.4	292.9
N			0.7	293.6
		357.5 = 15' of N & S Alley		
N			0.4	293.9
2			0.9	293.4
5			1.2	293.1
TP	6.05	299.98	0.35	293.93

Cross Section North & South Alley Blk 342 Univ. Hgts
Cypress to Pennsylvania

77

29.998

N & Cypress

N Top Co	550	294.48
Gutter on Paving	586	294.12
2	610	293.88
Gutter on Paving	590	294.18
E Top Co	528	294.76
10' N of N & Cypress		
E	55	294.5
2	58	294.2
N	55	294.5
31' N		
N	63	293.7
2	64	293.6
E	64	293.6
68' N		
E	66	293.4
2	70	293.0
N	74	292.6
100' N		
N Fence on S in Alley	9'	292.9
2	65	293.5
E	57	294.3
150' N = 52 E of Alley		
E	53	294.7
2	61	293.9

Plotted 11-2-28 CBH

		299.98		
W		6.9	293.1	168' N: Garage 7' E of EL Dirt Floor 4.1 ↓
	170' N = NL E & W Alley			
W		6.2	293.8	295.9
℄		5.3	294.7	
E		4.7	295.3	
	200' N			
E		4.6	295.4	
℄		4.8	295.2	
W		5.7	294.3	
	225' N			
W		5.8	294.2	
℄		4.8	295.2	
E		4.1	295.9	
	250' N			
E		4.7	295.3	
℄		5.0	295.0	
W		5.5	294.5	
	265' N			
W		5.7	294.3	
+5		4.7		
℄		4.5	295.5	
E		3.8	296.2	
	300' N			
E		3.9	296.1	
℄		4.4	295.6	
+6		4.6	295.4	

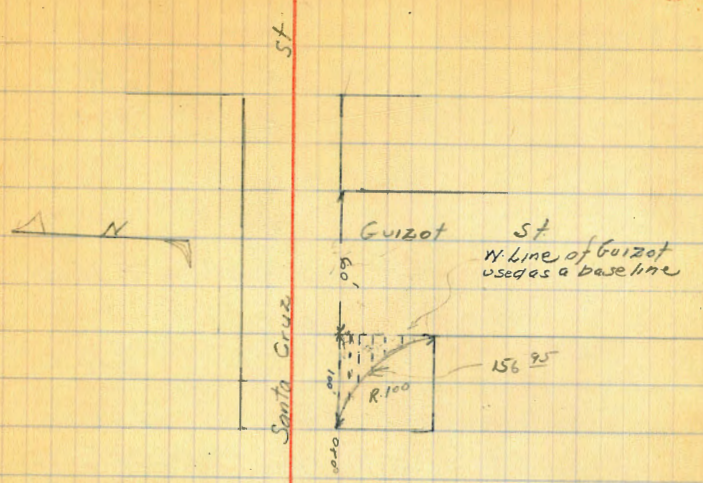
	299.98		
W		5.2	294.8
	315' N		
W		4.9	295.1
℄		4.2	295.8
E		3.5	296.5
	322' N		
E		3.7	296.3
℄		4.7	295.3
W		4.9	295.1
	324.5 = SL Pennsylvania		
W Top Cb + Ground		5.06	294.82
℄		5.0	295.0
E Top Cb + Ground		4.49	295.49

Bill Bliss
Joe Ducrmit
J Jacobszoon
Hrdg

X Sections Guizot Street from the South Line of Santa Cruz to P.C. of Curve 100' South

	+	H.I.	−	Elev	
BM	0.94	225.83		224.89	NEBP Guizot & Santa Cruz
T.P.	0.97	214.36	12.44	213.39	
			0+00		
-100 P.C. of Curve		214.4	9.1	205.3	
-85			7.6	206.8	
-70			6.9	207.5	
-55			5.9	208.5	
-40			3.5	210.9	
-33'			2.5	211.9	
-29			7.8	206.6	
-20			8.0	206.4	
-8			6.7	207.7	
-4			8.1	206.3	
W			8.2	206.2	
			0+09		
W			5.5	208.9	
+18			6.8	207.6	
+27			2.1	212.3	
+40			1.9	212.5	
+55			4.9	209.5	
+58 Intersects curve			5.1	209.3	
T.P.	10.69	221.80	3.20	211.16	
			0+19		
-91.20 Intersects curve			6.2	215.6	
-30			5.9	216.4	

+	HI 221.80	Elev	
-13	221.8	5.3	216.5
-10		13.0	208.8
W		12.5	209.3
		0+25	
W		12.0	209.8
+5		11.4	210.4
+8		6.7	215.1
+10		5.1	216.7
+15		3.9	217.9
+25		4.6	217.2
+33 Intersects curve		5.1	216.7
		0+34	
W		11.1	220.7
+3		4.4	217.4
+9		3.4	218.4
+24 Intersects curve		4.5	217.3



	+	H.I. 221.80	−	Elev
			0+38	
-2½. Intersects curve			4.1	217.7
-05			3.1	218.7
W			4.2	217.6
			0+50	
W			2.4	219.4
+13 P.I.			3.3	218.5
			0+25	
-3 P.I.			1.8	220.0
VX			1.7	220.1
			1+00 P.C. of curve	
VY			0.8	221.0
T.P.	5.10	226.00	0.90	220.90
check on Starting BM			0.60	225.90 —

IMPROVED TABLES AND INFORMATION

ENGINEERING DEPARTMENT
CITY OF SAN DIEGO.
CALIFORNIA.

25.0
240.17
9.83
165.41
155.58

8/31
1993

156.93
0.65
157.58
12.99
144.61

144.64
12.96
131.70

144.64
8.74
135.90

A B C D E F G H I J K L

15693
13.06
169.99
0.06
169.93
13.02
182.95
0.22
182.73
13.04
195.77
0.16
195.61
13.00
208.61
0.05
208.56
12.97
221.43
0.16
221.27
10.99
232.26
5.97
226.29

etc.
17160
1082
160.78

15693