

1286

PASTS

LEVEL BOOK

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" "	50 th	" " "	14
" "	ALTADENA AVE.	" "	27
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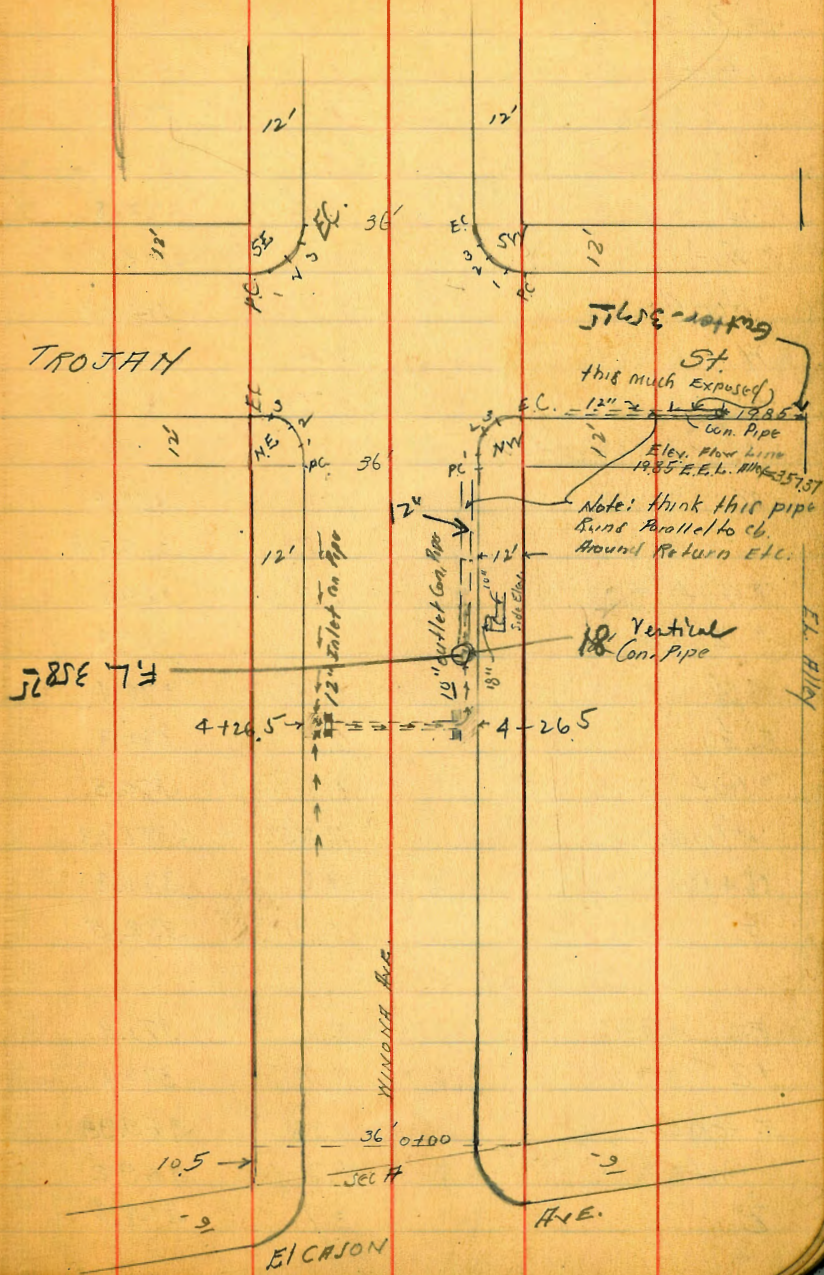
X Section Winona Ave 60' Wide
 from St. El Cason Ave to - 12' CBS
 N.W. Orange Ave. 9' AS

10.43 361.96 351.53
 12.07 373.36 0.67 361.29

Section A

E	+ 1.0	374.4
E top cb	+ 0.52	373.88
" Gutter on Paring	- 0.17	373.19
" 1/4 "	0.49	372.81
" 1/2 "	0.82	372.54
" 1 "	1.43	371.93
" Gut "	2.10	371.26
" top ch.	1.49	371.87
" "	1.7	371.7
0+00		
" "	1.7	371.7
" top cb.	1.57	371.79
" Gut	2.0	371.4
1/4	1.6	371.8
1/2	1.1	372.3
1	0.8	372.6
Gut	0.8	372.6
E top cb.	+ 0.10	373.46
+ 10	+ 0.3	373.7
E	+ 1.0	374.4
0+21		
E	- 0.4	373.0

Plotted 10-15-28-CBH



37336

E top cb.	1.09	372.27
" Gut.	1.6	371.8
" $\frac{1}{4}$	1.8	371.6
$\frac{1}{2}$	2.1	371.2
N $\frac{1}{2}$	2.6	370.8
" Gut.	3.1	370.3
" top cb.	2.67	370.69
N	3.2	370.2
+5	3.5	
	0+41	
N	3.6	369.8
" top cb.	3.58	369.78
" Gut	3.8	369.6
" $\frac{1}{4}$	3.6	369.8
$\frac{1}{2}$	3.0	370.4
E $\frac{1}{4}$	2.7	370.7
" Gut	2.6	370.8
" top cb.	2.83	371.13
cb+10	1.6	371.8
E	0.9	372.5
	0+61	
E	2.1	371.3
+2	2.8	370.6
E top cb.	3.38	369.98
Gut	4.2	369.2
$\frac{1}{2}$	3.9	369.5

37336

$\frac{1}{2}$	41	369.3	2
$\frac{1}{4}$	46	368.8	
Gut	50	368.4	
N top cb.	4.85	368.51	
N	4.7	368.7	
	0+89		
N	6.7	366.7	
" top cb.	6.46	366.90	
" Gut	6.7	366.7	
$\frac{1}{2}$	6.1	367.3	
$\frac{1}{4}$	5.7	367.7	
$\frac{1}{4}$	5.6	367.8	
Gut	5.9	367.5	
E top cb.	5.06	368.30	
E	4.4	369.0	
	1+10		
E	5.3	368.1	
E top cb.	6.25	367.11	
" Gut	6.8	366.6	
$\frac{1}{2}$	6.8	366.6	
$\frac{1}{4}$	7.1	366.9	
$\frac{1}{2}$	7.4	366.0	
Gut	8.1	365.3	
N top cb.	7.70	365.66	
N	8.1	365.3	
+5	8.4		

37336

1+25

-5	9.5	
Y	9.3	364.1
" top cb.	8.55	364.81
Gut	8.8	364.6
$\frac{1}{2}$	8.2	365.7
$\frac{1}{4}$	8.0	365.4
$\frac{1}{2}$	7.8	365.6
Gut	8.2	365.2
E top cb.	7.16	366.20
E	6.7	367.2

1+55

E	8.5	364.9
+12.15 = cb face on top	8.91	364.45
Gut	9.6	363.8
$\frac{1}{2}$	9.3	364.1
$\frac{1}{4}$	9.5	363.9
$\frac{1}{2}$	10.1	363.3
Gut	11.0	362.3
Y top cb. 12.10 inst.	10.25	363.10
	10.7	362.7

1+65

Y	11.4	362.0
+12.10 = top cb.	10.73	362.63
Gut	11.3	362.1
$\frac{1}{2}$	10.5	362.9

37336

$\frac{1}{2}$	9.8	363.6 ³
$\frac{1}{4}$	9.7	363.7
Gut	10.0	363.4
E top cb. 12.15 from Prop.	9.49	363.87
E	8.7	364.7

1+73

E + 12.10 = top cb.	9.85	363.51
Y top cb. 12.06 from Prop	11.19	362.17
	1+82	

Y	11.8	361.6
+3	11.4	362.0
Y top cb.	11.4	362.0

$\frac{1}{4}$	11.0	362.4
$\frac{1}{2}$	10.4	363.0
$\frac{1}{4}$	10.4	363.0
+5	10.5	362.9
Gut	10.1	363.3
top cb.	9.91	363.45
E	9.5	363.9

1+98

E	10.0	363.4
" top cb.	10.12	363.24
" Gut	10.6	362.8
$\frac{1}{4}$	10.8	362.6
$\frac{1}{2}$	10.7	362.7
$\frac{1}{4}$	11.4	362.0

37336

W Gut	11.6	361.8
" top cb.	11.46	361.90
W	11.9	361.5
2+10		
W	12.4	361.0
W top cb.	11.57	361.79
Gut	11.8	361.6
$\frac{1}{2}$	11.4	362.0
$\frac{1}{2}$	10.8	362.6
$\frac{1}{4}$	11.0	362.4
Gut	11.0	362.4
top cb.	10.25	363.11
E	10.1	363.3
2+38		
E	10.5	362.9
" top cb.	10.52	362.84
Gut	11.3	362.1
$\frac{1}{2}$	11.3	362.1
$\frac{1}{2}$	11.2	362.2
$\frac{1}{4}$	11.7	361.7
Gut	12.0	361.4
W top cb.	11.75	361.61
W	12.4	361.0
+5	12.6	
2+66		
-5	12.3	

37336

W	11.9	361.5
W top cb.	11.85	361.51
Gut	12.3	361.1
$\frac{1}{2}$	12.1	361.3
$\frac{1}{2}$	11.5	361.9
$\frac{1}{2}$	11.7	361.7
Gut	11.7	361.7
E top cb. = 12.1° from Pop.	10.81	362.55
E	10.6	362.8
TR	5.34	367.12
	3+00	
E	4.5	362.6
E top cb.	4.85	362.27
Gut	5.7	361.4
$\frac{1}{2}$	5.6	361.5
$\frac{1}{2}$	5.5	361.6
$\frac{1}{2}$	5.8	361.3
Gut	6.2	360.9
W top cb.	5.81	361.31
W	5.6	361.5
3+16		
W top cb.	5.89	361.23
E " "	5.00	362.12
3+25 = $\frac{1}{2}$ Ribbon Drive on E		8" Gutter
3+30		
E top cb.	5.08	362.04

36712

N top cb.	5.97	361.15	Extends to cb line
3+43 = 2' Con Walk on E. 4' wide			
N	6.2	360.9	
" top cb.	6.11	361.01	
" Gutter	6.6	360.5	
$\frac{1}{2}$	6.2	360.9	
$\frac{1}{2}$	5.8	361.3	
$\frac{1}{2}$	6.0	361.1	
Gut	5.9	361.2	
E top cb.	5.18	361.94	
E on top walk	4.56	362.56	
	3+80		
E	5.5	361.6	
" top cb.	5.97	361.65	
Gut	6.4	360.7	
$\frac{1}{2}$	6.2	360.9	
$\frac{1}{2}$	6.1	361.0	
$\frac{1}{2}$	6.6	360.5	
Gut	6.8	360.3	
N top cb.	6.30	360.80	
N	6.6	360.5	
	4+00		
-5	7.4		
N	7.2	359.9	
N top cb.	6.49	360.63	
" Gut	7.0	360.1	

36712

$\frac{1}{4}$	6.6	360.5	
$\frac{1}{4}$	6.4	360.7	
$\frac{1}{4}$	6.3	360.8	
Gut	6.5	360.6	
E top cb.	5.60	361.52	
E	5.7	361.4	
	4+26.5 = 2' Con Gutter see sketch Page 1		
E	6.0	361.1	
" top cb.	5.80	361.32	
Gut.	6.1	361.0	
Flood line 12" Inlet	7.11	360.0 ¹ ₃ thick.	
cb+1.2 = top Hd. Wall Inlet	6.06	361.06 2' wide	
$\frac{1}{4}$	6.1	361.0	
$\frac{1}{2}$ (4+42 N. Grate 359.96)	6.3	360.8	
$\frac{1}{2}$	6.5	360.6	
+7.8 on top Hd. Wall outlet.	6.69	360.43	
Flood line 10" Pipe	7.55	359.57	
Ground Gut.	7.1	360.0	
N top cb.	6.70	360.40	
N	6.7	360.4	
	4+38.3 = 2' Inlet #2		
N top cb.	6.72	360.40	
" Gut. on Con. Pipe	7.38	359.74	
" Flood line Inlet #2	8.50	358.62	
E top cb.	5.77	361.35	
	4+70		

5

367.12

E	5.2	361.9
top cb. (ok for line)	5.24	361.88
Gut.	5.5	361.6
$\frac{1}{2}$	5.7	361.4
$\frac{1}{4}$	5.9	361.2
$\frac{1}{4}$	6.1	361.0
Gut	6.2	360.9
$\frac{1}{4} + 8.88 = \text{top cb.}$	6.04	361.08
X	6.0	361.2
4+85		
X+12.22 = top cb.	5.62	361.50
E top cb. (ok for line)	4.91	362.21
5+06		
E	3.4	363.7
+2	4.1	363.0
E top cb.	4.43	362.69
Gut	4.8	362.3
$\frac{1}{4}$	5.1	362.0
$\frac{1}{4}$	5.0	362.1
$\frac{1}{4}$	5.2	361.9
Gut	6.0	361.1
$\frac{1}{4} + 8.77 = \text{top cb.}$	5.16	361.96
X	5.7	361.4
5+23		
X+12.25 = top cb.	4.55	362.57 ✓
E top cb.	4.03	363.09

367.12

E top cb.	5+33	3.82	363.30 ²² 6
X top cb. 12.30 from Prop.		4.38	362.74
	5+42.95 = N.W. Trojan Ave		
X		4.4	362.7
+12.10 = top cb.		3.97	363.15
Gut		4.8	362.3
$\frac{1}{4}$		4.2	362.9
$\frac{1}{6}$		3.7	363.4
$\frac{1}{4}$		4.0	363.1
Gut		4.1	363.0
E top cb.		3.60	363.52
+8		3.0	364.1
E		2.2	364.9

LEVELS on Returns at Intersection Trojan St.

Note: PC and EC are on prop. lines produced and are divided in 4 parts, as per sketch on Page 1. For X Section of Intersection See Book 1161-67

N.W. Return

PC	3.97	363.15
1	3.92	363.20
2	3.92	363.20
3	4.00	363.12
EC	4.13	362.99

NE Return

PC	3.60	363.52
1	3.31	363.81
2	2.93	364.19

36712

3	2.45	364.67
EC.	1.86	365.26

S.E. Return

P.C.	0.58	366.54
1	0.80	366.32
2	1.04	366.08
3	1.01	366.11
EC.	0.90	366.22

S.W. Return

P.C.	3.00	364.12
1	2.71	364.41
2	2.42	364.70
3	2.15	364.97
EC.	1.97	365.15

S. to Trojan = 0+100

W	2.6	364.5
" top cb.	1.97	365.15
Gut	2.9	364.2
$\frac{1}{4}$	2.2	365.9
$\frac{1}{2}$	1.9	365.2
$\frac{1}{4}$	1.8	365.3
Gut	2.0	365.1
top cb.	0.90	366.22

E	0.3	366.9
TP.	6.26	373.12
	0+30	0.26
		366.86

on Prop. Hub.
S.E. Trojan + 111005

37312

E	4.8	368.3
+3	5.8	367.3
cb.	5.97	367.15
Gut.	6.7	366.4
$\frac{1}{4}$	6.5	366.6
$\frac{1}{2}$	6.5	366.6
$\frac{1}{4}$	7.0	366.1
Gut	7.6	365.5
top cb.	7.00	366.12
W	7.3	365.8

0+60

W	6.1	367.0
" top cb.	6.00	367.12
" Gut.	6.7	366.4
$\frac{1}{4}$	5.9	367.2
$\frac{1}{2}$	5.5	367.6
$\frac{1}{4}$	5.6	367.5
Gut	5.6	367.5
E top cb.	5.05	368.07
E	4.8	368.3

Extends to cb.
0+56 = $\frac{1}{2}$ Cor. Wall
top = 3.42
0+44.5 = Head Cor. Ret. Wall of bottom 5.1
368.369 + Prop.
369.70
368.0
+75 = S. " " " top = 2.58
370.54 top
" " " " " Bottom = 4.4
368.7

0+80

E	3.7	369.4
---	-----	-------

373.12

+2	4.2	368.9
E top cb.	4.45	368.67
Gut	5.1	368.0
$\frac{1}{4}$	5.0	368.1
$\frac{1}{2}$	4.9	368.2
$\frac{1}{4}$	5.4	367.7
cb Gut	6.2	366.9
X top cb.	5.40	367.72
X	5.5	367.6
	1+00	
X	4.7	368.4
cb on top	4.80	368.32
Gut	5.8	367.3
$\frac{1}{4}$	5.0	368.1
$\frac{1}{2}$	4.5	368.6
$\frac{1}{4}$	4.4	368.7
Gut	4.7	368.4
E top cb 12' from Psp.	3.85	369.27
+9	3.9	369.2
E	2.9	370.2
	1+30	
E	2.4	370.7
+3	3.3	369.8
cb ok.	3.41	369.71
Gut	4.2	368.9
$\frac{1}{4}$	4.0	369.1

373.12

8

$\frac{1}{2}$	4.1	369.0
$\frac{1}{4}$	4.7	368.4
Gut	5.2	367.9
X top cb.	4.41	368.71
+10	4.5	368.6
X	3.9	369.2
	1+40	
X top cb.	4.30	368.82
E " "	3.28	369.83
	1+50	
E " "	3.30	369.82
X " "	4.28	368.84
	1+60	
X	3.4	369.7
+2	4.0	369.0
X top cb.	4.30	368.82
" Gut	5.1	368.0
$\frac{1}{4}$	4.4	368.7
$\frac{1}{2}$	3.8	369.3
$\frac{1}{4}$	4.0	369.1
Gut.	4.2	368.9
E top cb.	3.47	369.65
+9	3.0	370.1
E	1.9	371.2
	1+70	
E top cb.	3.71	369.41

373.12

X top cb.	443	368.69
Z+00		
X	39	369.2
+2	49	368.2
X top cb.	482	368.30
" Gut	57	367.4
$\frac{1}{2}$	52	367.9
$\frac{1}{2}$	47	368.4
$\frac{1}{2}$	49	368.2
Gutter	53	367.8
top cb. 12.06 inst.	449	368.63
cb+8	45	368.6
E	31	370.0
Z+39		
E	41	369.0
+3	53	367.8
+12.12 = top cb.	591	367.21
Gut.	66	366.5
$\frac{1}{2}$	61	367.0
$\frac{1}{2}$	58	367.3
$\frac{1}{2}$	63	366.8
Gut.	68	366.3
X top cb. 11.92 inst.	568	367.44
+9	59	367.2
X	44	368.7
Z+50		

373.12

X top cb. 11.92 inst.	615	366.97
E " " 12.15 inst.	629	366.83
Z+60		
E top cb. 12.15 inst.	681	366.31
X " " 12.03 "	670	366.42
Z+70		
X	58	367.3
+5	72	365.9
+12.03 = top cb.	754	365.58
Gut	84	364.7
$\frac{1}{2}$	80	365.1
$\frac{1}{2}$	76	365.5
$\frac{1}{2}$	78	365.3
Gut	79	365.2
E top cb. 12.10 inst.	747	365.65
cb.+9	70	366.1
E	57	367.4
Z+80		
E +12.0 = top cb.	847	364.65
X top cb.	865	364.47
Z+90		
X top cb.	987	363.25
E " " 12.10 inst.	953	363.59
Z+00		
E	94	363.7
+3	10.8	362.3

Note: cb. on West 17 Bd Shape
 det 2+80 and 3+02.6

cb. 12.10 inst	10.81	362.31	
Gut	11.3	361.8	
$\frac{1}{4}$	11.4	361.7	
$\frac{1}{2}$	10.9	362.2	
$\frac{1}{4}$	11.1	361.0	
Gut.	11.3	361.8	
X top cb.	10.63	362.49	
+8	10.5	362.6	
X	9.2	363.9	
(3+02.6) on X top cb.	10.88	362.24	
3+10			
X top cb. off. line	11.94	361.18	
E " " 12.10 inst.	12.13	360.99	
3+20			
T.P. 0.97 361.23	12.86	360.26	on top cb.
E top cb. 12.10 inst.	1.62	359.61	
X " "	1.57	359.66	
3+30			
X	2.3	358.9	
+2	3.0	358.2	
X top cb.	3.12	358.11	
Gut	3.5	357.7	
$\frac{1}{4}$	3.7	357.5	
$\frac{1}{2}$	3.3	357.9	
$\frac{1}{4}$	3.3	357.9	
Gut.	3.5	357.7	

E top cb. 12.15 inst.	2.99	358.24	10
Ecb+6	3.7	357.5	
Ecb+8	4.3	356.9	
E	3.7	357.5	
3+40			
E top cb. 12.18 inst.	4.40	356.83	
X " "	4.70	356.53	
3+50			
-5	6.7	354.5	
X	6.7	354.5	
+8	7.0	354.2	
X top cb.	6.22	355.01	
Gut	6.7	354.5	
$\frac{1}{2}$	6.5	354.7	
$\frac{1}{4}$	6.3	354.9	
$\frac{1}{4}$	6.3	354.9	
Gut.	6.7	354.5	
E top cb. 12.15 inst.	5.86	355.37	
E	6.3	354.9	
+5	6.5	354.7	
3+60			
E top cb. 12.21 inst.	7.38	353.85	
X " " finish gone at this point	7.80	353.43	
3+70			
X top cb. finish ok.	9.28	351.95	
E " " 12.20 inst	8.96	352.27	

36/23

3+80

-5		11.5	349.7
E		11.3	349.9
cb. 12.10' inst.		10.53	350.70
Gut.		10.9	350.3
$\frac{1}{4}$		10.9	350.3
$\frac{1}{2}$		10.6	350.6
$\frac{3}{4}$		10.8	350.4
Gut.		10.9	350.3
W top cb.		10.72	350.51
X		12.0	349.2
+5		12.3	348.9
T.P.	1.06 350.12	12.17	349.06

3+90

W top cb.		0.96	349.16
E " cb. 12.20' inst.		0.96	349.16

4+00

E top cb. 12.20' inst.		2.44	347.68
X " "		2.34	347.78

4+10

-5		5.3	
X		5.1	345.0
+7		4.8	
W top cb.		3.64	346.48
Gut.		4.0	346.1
$\frac{1}{4}$		3.8	

350/2

11

$\frac{1}{2}$		3.9	346.2
$\frac{3}{4}$		3.8	
Gut.		4.2	345.9
E top cb. 12.10' inst.		3.86	346.26
E		4.9	345.2
+5		4.9	

4+20

E top cb. 12.10' inst.		5.13	344.99
W " "		5.02	345.10

4+30

W top cb.		6.11	344.01
E " " 12.10' inst.		6.42	343.70

4+40

-5		8.3	
E		8.4	341.7
E top cb. 12.13' inst.		7.64	342.48

Gut.		8.2	341.9
------	--	-----	-------

$\frac{1}{4}$		8.08	
---------------	--	------	--

$\frac{1}{2}$		7.9	342.2
---------------	--	-----	-------

$\frac{3}{4}$		7.8	
---------------	--	-----	--

Gut.		7.8	342.3
------	--	-----	-------

W top cb.		7.20	342.90
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+3		8.0	
----	--	-----	--

W		8.4	341.7
---	--	-----	-------

+5		8.3	
----	--	-----	--

4+50

350.12

Y top cb.	8.23	341.89
E " " 12.12' inst.	8.88	341.24
4+60		
E top cb 12.10' inst.	9.93	340.19
Y " "	9.23	340.89
4+70		
-5	10.7	
Y	10.9	339.2
" top cb. 11.94' inst.	10.11	340.01
Gut	10.7	339.4
$\frac{1}{2}$	11.0	
$\frac{1}{2}$	10.9	339.2
$\frac{1}{2}$	11.3	
Gut	11.3	338.8
E top cb 12.10' inst.	11.03	339.09
E	11.3	338.8
+5	11.3	
4+80		
E top cb. 12.12' inst.	11.96	338.16
Y " " 11.90' " "	10.90	339.22
4+90		
Y top cb 11.90' inst.	11.68	338.44
E " " 12.10' "	12.89	337.23
T.P. 123 338.37	12.98	337.14
5+00		
-5	2.5	

338.37

12

E	2.3	336.1
" top cb. 12.12' inst.	1.87	336.50
Gut.	2.6	335.8
$\frac{1}{4}$	2.6	
$\frac{1}{4}$	2.2	336.2
$\frac{1}{4}$	1.9	
Gut	1.3	337.1
Y top cb. 11.88' inst.	0.71	337.66
Y	1.0	337.4
+5	1.0	
5+10		
Y top 11.85	1.38	336.99
E " 12.15' inst.	2.57	335.80
5+25		
-5	3.9	
E	3.9	334.5
E top cb. 12.10' inst.	3.44	334.93
Gut	4.4	334.0
$\frac{1}{2}$	4.7	
$\frac{1}{2}$	4.3	334.1
$\frac{1}{4}$	4.3	
Gut.	4.1	334.3
Y top cb. 11.90' inst.	2.39	335.98
cb + 8	2.8	
Y	2.0	336.4
5+50		

338.37

W	3.2	336.2
W top cb. 11.88' inst.	4.02	334.35
Gut	4.9	333.5
$\frac{1}{2}$	5.8	
$\frac{2}{4}$	5.6	332.8
$\frac{1}{4}$	6.0	
Gut	6.1	332.3
E top cb. 12.12' inst.	4.60	333.77
E	5.2	333.2
+5	5.2	
	5+70	
E	5.4	333.0
E top cb. 12.10' inst.	5.47	332.90
Gut	7.6	330.8
+6	8.3	
$\frac{1}{2}$	8.0	
$\frac{2}{4}$	7.5	330.9
$\frac{1}{4}$	8.0	
+3	8.4	
Gut	6.9	331.5
W top cb. 11.90' inst.	5.32	333.05
W	3.5	334.9
	+97 = End	
	5+99 = End	Ext. cb. on E
W	5.5	332.9
" top cb.	6.95	331.42
Gut.	9.0	329.4

338.37

13

+6	9.8	
$\frac{1}{2}$	9.6	
$\frac{1}{4}$	9.4	329.0
$\frac{1}{4}$	9.8	
+4	10.2	
Gut	9.8	328.6
E top cb.	6.75	331.62
E	6.1	332.3
	6+100	
E	9.7	328.7
cb. on ground	9.7	328.7
+2	10.2	
$\frac{1}{2}$	9.8	
$\frac{1}{4}$	9.5	328.9
$\frac{1}{4}$	9.7	
+3	10.0	
cb. on ground	9.3	329.1
W	9.1	329.3
chk. on N.E. Orange + Winona	6.53	331.84
50' N.W. Orange		
T.P. RR. Hub. on E.L. Winona.	5.15	333.22
		chk. ok.

Marker
Rapping
Leaky
Shims 10-6-28

X. Section 50th St 60' wide 12' cbs.
Bet. El Cajon + Orange Ave 9' 45"

386.23

SE. 8 th prop. Hdt. } Trojan + Winona prop. }	12.30	377.16		366.86	
T.P.	7.58	386.57	0.17	378.99	NE. Top Hdt.
T.P.	0.13	386.23	0.47	386.10	El Cajon + 50 th

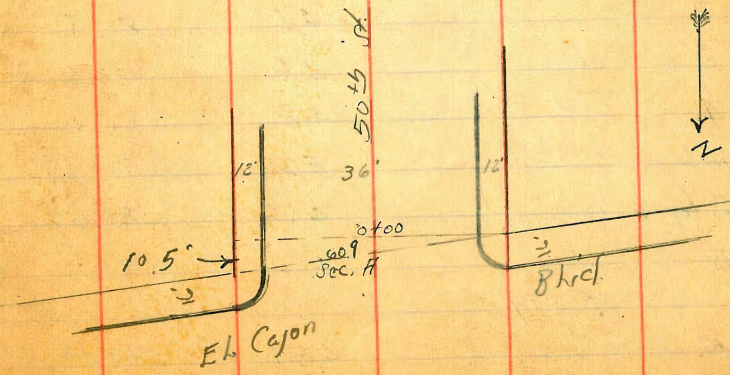
Section A

E _o		2.2		384.0	
" top cb		2.45		383.78	
" Gut on Paving		3.14		383.09	
" 1/4 "		3.00		383.23	
" 1/2 "		3.01		383.22	
" 3/4 "		3.20		383.03	
" Gut "		3.53		382.70	
" top cb.		2.92		383.31	
"		3.3		382.9	
	0+00				
"		3.3		382.9	
" top cb.		2.90		383.33	
Gut		3.5		382.7	
1/4		3.2		383.0	
1/2		2.9		383.3	
3/4		2.8		383.4	
Gut		3.0		383.2	
E _o top cb.		2.54		383.69	
E _o		2.3		383.9	
	0+50				
E _o		2.7		383.5	

Plotted 10-30-28 - C.B.H.

E top cb.	3.10	383.13
Gut.	3.5	382.7
1/4	3.0	383.2
1/2	2.9	383.3
3/4	3.4	382.8
Gut	4.1	382.1
" top cb.	3.37	382.86
"	3.7	382.5
		1+00
"	4.3	381.9
" top cb. 11.75' inst.	3.89	382.34
Gut	4.4	381.8
1/4	3.8	382.4
1/2	3.5	382.7
3/4	3.7	382.5

Note: curb is ok. For line unless noted otherwise



14

Gut	4.0	382.3
E top cb. Finish Gate	3.67	382.56
E	3.3	382.9
1+50		
E	3.7	382.5
E top cb. 12.10 inst.	3.96	382.27
Gut	4.4	381.8
$\frac{1}{2}$	4.0	382.2
$\frac{1}{2}$	4.0	382.2
$\frac{1}{2}$	4.4	381.8
Gut	5.0	381.2
X top cb. 11.50 inst.	4.41	381.82
X	4.3	381.9
Note, sta 1+96 to 1+98 curb should be replaced on E		
R+00		
X	5.0	381.2
" top cb. 11.50 inst.	4.87	381.36
Gut	5.4	380.8
$\frac{1}{2}$	4.7	381.5
$\frac{1}{2}$	4.6	381.6
$\frac{1}{2}$	4.8	381.4
Gut	5.2	381.0
E top cb. 12.20 inst.	4.56	381.67
E	4.6	381.6
R+19		
E top cb. 12.20 inst.	4.80	381.43

X top cb. 11.50 inst.	5.24	380.99
R+50		
X	6.2	380.0
X top 11.60 inst.	5.65	380.58
" Gut.	6.3	379.9
" $\frac{1}{2}$	5.7	380.5
$\frac{1}{2}$	5.3	380.9
E $\frac{1}{2}$	5.4	380.8
" Gut	5.6	380.6
" top cb. 12.10 inst.	5.18	381.05
E	5.1	381.1
R+67		
E	5.2	381.0
" top cb. 12.10 inst.	5.43	380.80
" Gut	6.0	380.2
$\frac{1}{2}$	5.6	380.6
$\frac{1}{2}$	5.5	380.7
$\frac{1}{2}$	6.0	380.2
Gut	6.5	379.7
X top cb. 11.70 inst.	5.97	380.26
X	6.7	379.5
R+87 = E Ribbon Driveway		
R+00		
X	6.9	379.3
" top cb. 11.70 inst.	6.59	379.64
" Gut.	7.0	379.2

Drive extends
to cb line

386.23

N 2	6.3	379.8
E	6.1	380.1
1/4	6.1	380.1
Gut	6.4	379.8
E top cb. 12.15 in st.	5.93	380.30
E	5.7	380.5
	3+30	
E top cb. 12.10 in st.	6.39	379.84
N " " 11.80 " "	7.15	379.08
	3+55	
N	8.2	378.0
" top cb. 11.80 in st.	7.71	378.52
" Gut	8.1	378.1
1/4	7.4	378.8
E	7.0	379.2
1/4	6.9	379.3
Gut	7.3	378.9
E top cb. 12.10 in st.	6.75	379.48
E	6.3	379.9
	3+80	
E	6.7	379.5
" top cb. 12.15 in st.	7.16	379.07
Gut	8.0	378.2
1/4	7.3	378.9
E	7.4	378.8
1/4	7.8	378.4

386.23

N Gut	8.7	377.5	16
" top cb. 11.60 in st.	8.20	378.03	
N	8.7	377.5	
	4+28		
N	9.7	376.5	
" top cb. 11.70 in st.	9.10	377.13	
" Gut	9.7	376.5	
" 1/4	9.1	377.1	
E	8.6	377.6	
E 1/4	8.6	377.6	
" Gut	8.8	377.4	
" top cb. 12.20 in st.	7.96	378.27	
E	7.7	378.5	
T.P.	1.66	380.64	7.25 378.98
	4+53		
E	2.8	377.8	
E top cb. 12.10 in st.	2.84	377.80	
" Gut	3.6	377.0	
1/4	3.4	377.1	
E	3.6	377.0	
1/4	4.3	376.3	
Gut	4.5	376.1	
N top cb. 11.70 in st.	3.90	376.74	
N	4.4	376.7	
	4+85		
N top cb. 11.65 in st.	4.25	376.39	

Note: curb should be replated on East
bet. Sta 4+67 & 4+73

380.64

E Top cb.	3.24	377.40
5+00		
E	4.1	376.5
+11	4.1	376.5
E Top cb.	3.45	377.19
Gut	4.0	376.6
$\frac{1}{4}$	4.3	376.3
$\frac{1}{2}$	4.3	376.3
$\frac{3}{4}$	4.7	375.9
Gut	5.0	375.6
N Top cb. 11.65' inst.	4.31	376.33
+7	4.3	376.3
N	4.9	375.7
+5	5.2	
5+25		
N Top cb. 11.75' inst.	4.45	376.19
E " cb. 11.90' inst.	3.77	376.87
5+50		
-5	5.3	
E	5.2	375.4
+11	5.0	375.6
E Top cb. 11.90' inst.	4.14	376.50
" Gut	5.0	375.6
$\frac{1}{4}$	5.0	375.6
$\frac{1}{2}$	4.7	375.9
$\frac{3}{4}$	5.0	375.6

380.64

Gut	5.2	375.4 ¹⁷
N Top cb. 11.25' inst.	4.58	376.06
N	4.4	376.2
+5	4.1	
5+75		
N	4.0	376.6
+2	4.6	376.0
N Top cb. 11.80' inst.	4.70	375.94
Gut	5.3	375.3
$\frac{1}{4}$	4.8	375.8
$\frac{1}{2}$	4.9	375.7
$\frac{3}{4}$	5.2	375.4
Gut	5.2	375.4
E Top cb. 11.87' inst.	4.48	376.16
+1	4.8	375.8
E	5.4	375.2
+5	5.6	375.0
46		
6+00. = N.L. Trojan Ave		
E	5.8	374.8
+11	5.3	375.3
E Top cb. 11.81' inst.	4.86	375.78 ✓
" Gut	5.7	374.9
+4	6.0	374.6
$\frac{1}{4}$	5.5	375.1
$\frac{1}{2}$	5.0	375.6
$\frac{3}{4}$	5.0	375.6

Note: For Section
of Intersecting
Tropics
See Book 1161-70

380.64

Gut	5.3	375.3
N top cb 1190 in st.	4.69	375.95
+10	4.5	376.1
N	4.1	376.5

N.Y. Return 4 equal Parts

P.C.	4.69	375.95
1	4.50	376.14
2	4.46	376.18
3	4.46	376.18
E.C.	4.43	376.21

S.Y. Return 4 equal Parts

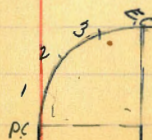
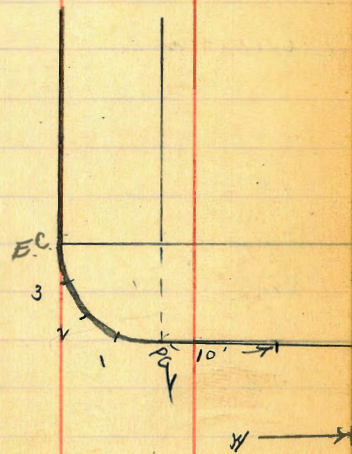
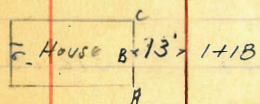
10' west P.C.	4.83	375.81
P.C.	4.61	376.03
1	4.95	375.69
2	5.35	375.29
3	5.67	374.97
E.C.	5.97	374.67

S. L. TIOJAN = 0+00

N	5.8	374.8
+6	6.6	
+9	6.2	
N top cb	5.97	374.67
Gut	6.8	
1/2	6.7	
2/2	6.5	374.1
1/2	6.5	

380.64

cb.	67	18
E	72	373.4
+10	83	
	0+30	
-10	113	



380.64

0+30

E	9.5	371.1
+7	8.6	
cb.	8.4	
$\frac{1}{4}$	8.0	
$\frac{1}{2}$	7.8	372.8
$\frac{3}{4}$	7.6	
+5	8.1	
Gut.	8.7	
1/4 top cb.	7.95	372.69
+7	8.0	
1/4	7.7	372.9
{1/4 top cb. 0+40	8.67	371.975}
1/4	8.6	372.0
+3	9.9	
1/4 top cb.	9.55	371.09
Gut.	10.1	
+2	10.3	
+4	9.4	
$\frac{1}{4}$	9.0	
$\frac{1}{2}$	9.3	371.3
$\frac{3}{4}$	10.0	
cb.	10.7	
E	14.0	366.6
+10	16.3	
1/4 top cb. 0+60	10.43	370.21

380.64

19

T.P.	0.53	369.10	1207	368.57
		0+70		
-15			10.0	
E			7.2	361.9
cb.			4.7	
$\frac{1}{2}$			1.1	
$\frac{1}{4}$			0.6	368.5
$\frac{3}{4}$			0.2	
+6			0.0	
Gut			1.3	
1/4 top cb. 1190 mft.			0.07	369.03
+10			+0.2	
1/4			+1.0	370.1
		11.90 mft.		
1/4 top cb. 0+80			1.36	367.74
" " " 0+90			2.75	366.35
		0+99 = 2nd exist. cb. on vert. 121		
1/4			3.4	365.7
+3			4.5	
+11			4.2	
1/4 top cb. 1190			4.11	364.99
Gut			5.3	
+14			5.3	
+4			7.0	
+5			4.7	
$\frac{1}{4}$			4.6	
$\frac{1}{2}$			4.9	364.2

36910

+5	4.9	
$\frac{1}{2}$	7.2	
cb.	10.8	
E	13.1	356.0
+15	15.8	
1+18 = 2 House on East 13' back see sketch P-18		
F on Ground at house	17.7	351.4
B " Floor	15.6	353.5
C " Ground "	18.4	350.7
1+13		
-13	17.0	
E	14.8	354.3
cb.	13.0	
+5	11.8	
$\frac{1}{2}$	10.0	
+6	6.6	
$\frac{1}{2}$	6.7	362.3
$\frac{1}{2}$	6.6	
+2	6.5	
+6	8.8	
+8	9.0	
cb.	10.4	
+1	6.6	
+4	8.5	
+8	8.1	
Y	5.6	363.5

36910

20

1+39		
Y	10.0	359.1
+4	11.3	
+5	9.7	
+8	10.3	
+9	14.2	
cb.	13.3	
+1	13.3	
+5	10.2	
$\frac{1}{2}$	10.6	
+7	10.5	
$\frac{1}{2}$	10.7	358.4
+5	11.5	
$\frac{1}{2}$	13.9	
cb.	16.3	
E	18.6	350.5
+7	20.0	
+10	21.0	
+15	22.1	
1+53		
-15	24.4	
E	27.0	347.1
cb.	19.3	
+7	18.0	
$\frac{1}{2}$	16.7	
+6	13.2	

369.10

1/2	12.7	356.4
1/2	12.6	
+7	12.7	
cb.	14.8	
+1	17.0	
+3	17.0	
+4	12.3	
+9	12.0	
+10	13.6	
1/4	12.7	356.4
+3 = top Bank.	8.3	
T.P. 0.49	12.79	356.31
1+70		
-3 = top Bank.	+1.0	
1/4	2.1	354.7
+3	4.0	
+4	2.5	
+8	2.7	
+10	5.6	
cb.	5.6	
+2	4.7	
+3	2.4	
1/4	2.7	
1/2	2.8	354.0
+2	2.8	
1/4	6.2	

356.80

+4	8.4	
cb.	9.4	
+7	9.7	
E	10.7	346.1
+15	13.9	
1+97		
-15	15.1	
E	13.4	343.4
cb.	11.0	
1/4	9.3	
+4	7.2	
1/2	6.8	350.0
1/2	6.6	
+4	6.4	
+5	7.2	
cb.	7.0	
+7	6.0	
+9	6.5	
1/4	5.3	351.5
+7 = top Bank.	2.0	
1+08		
-5	4.0	
1/4	7.6	349.2
+3	8.2	
+6	7.6	
cb.	8.1	

21

356.80

+2		10.7	
+3		10.7	
+5		7.9	
$\frac{1}{4}$		8.2	
$\frac{1}{2}$		8.7	348.1
$\frac{1}{4}$		10.5	
cb.		12.2	
E		14.4	342.4
+15		16.7	
T.P.	1.10	12.93	343.87
	2+2/		
-15		6.2	
E		4.0	340.9
cb.		1.9	
+7		0.7	
$\frac{1}{2}$		+1.3	
$\frac{1}{2}$		+2.0	346.9
$\frac{1}{2}$		+2.4	
+2		+2.4	
cb.		0.6	
+8		+3.0	
Y		+4.3	349.3
+3		+7.0	
	2+3/		
-3		+6.0	
Y		+4.0	349.0

344.97

+3		+2.5	
+10		+0.9	
cb.		+1.8	
+3		+0.8	
+4		5.0	
+7		5.0	
$\frac{1}{2}$		+0.9	
$\frac{1}{2}$		+0.8	345.8
+6		+0.3	
$\frac{1}{2}$		0.6	
cb.		2.8	
E		4.9	340.0
+15		7.4	
	2+4/		
-15		8.4	
E		6.8	338.1
cb.		4.8	
$\frac{1}{2}$		1.8	
$\frac{1}{2}$		1.0	344.0
$\frac{1}{2}$		1.0	
+4		1.2	
+5		4.9	
cb.		5.4	
+2		0.7	
+9		0.0	
+12		+1.0	346.0

23

344.97

+3		+4.3	
	R+73		
-3		+0.5	
1/4		2.4	341.5
+2		3.3	
+3		5.3	
+5		3.4	
+11		3.8	
cb.		7.0	
+4		6.4	
+6		4.0	
1/2		4.0	
1/2		4.2	340.7
+8		4.6	
1/2		4.8	
cb.		7.2	
E.		9.2	335.7
+10		10.3	
R+76 = Cypress Tree on E		8.0	
+89 = " " " "		8.8	
3+03 = " " " "		9.8	
+17 = " " " "		10.9	
	R+86		
-10		10.5	
E.		7.5	335.5
+10		8.7	

2" dia
9' in st.
8" dia
9' in st
8" dia
9' in st
8" dia
9' in st

344.97

cb.		7.8		23
+4		6.3		
1/2		6.0		
1/2		5.5	339.5	
1/2		5.4		
+3		5.5		
+4		7.0		
+8		7.9		
cb.		5.2		
+3		5.1		
+5		7.0		
+8		4.8		
1/4		3.8	341.1	
+5		0.9		
	R+98 = 2 Con Steps on E			
-4		2.8		
1/4		5.1	339.8	
+5		8.1		
cb.		7.8		
+5		7.4		
+7		6.5		
1/4		6.5		
1/2		4.5	338.4	
1/2		7.1		
+4 = top 1st Con. Step.		7.24	337.73	
cb. = " Bottom Step.		9.02	335.95	

34497

E	10.2	334.7
+10	11.8	
	3+22	
-10	12.7	
E	11.5	333.4
cb.	10.5	
+5	9.0	
$\frac{1}{2}$	8.7	
$\frac{1}{2}$	8.5	336.4
$\frac{1}{2}$	8.4	
+2	8.4	
+4	7.6	
cb.	9.7	
+5	10.1	
+8	8.8	
W	7.8	337.1
+3 = top Bank.	5.6	
	3+45	
-3	7.0	
W	9.2	335.7
+2	9.7	
+9	9.7	
cb.	12.2	
+4	11.0	
+5	10.0	
$\frac{1}{4}$	10.0	

34497

50th St.

E	10.2	334.7	24
$\frac{1}{2}$	10.2		
cb.	12.5		
E	13.4	331.5	
+10	14.0		
	3+62		
-10	14.5		
E	14.2	330.7	
cb.	13.2		
+2	13.0		
$\frac{1}{2}$	11.3		
$\frac{1}{2}$	11.2	333.7	
$\frac{1}{2}$	11.2		
+3	11.1		
+7	12.7		
cb.	11.2		
+11	10.5		
W	10.0	334.9	
+2	8.5		
T.P.	17.4	334.17	332.43
	3+85		
-1	+0.2		
W	0.7	333.5	
+2	1.6		
cb.	1.8		
+3	2.8		

33417

+7	20	
$\frac{1}{2}$	21	
$\frac{1}{2}$	20	332.2
$\frac{1}{2}$	22	
cb.	33	
E.	41	330.0
+5	44	
A+22 = $\frac{1}{2}$ House on E. 17.5' Back. Cor. Foundation ^{20' wide}		
-17.5 = Floor of House	50	329.2
-17.5 = Ground Elev of house	5.8	
E	52	329.0
cb.	48	
$\frac{1}{2}$	43	
$\frac{1}{2}$	39	330.3
$\frac{1}{2}$	37	
cb.	33	
N	29	331.3
A+50		
N	40	330.2
cb.	45	
$\frac{1}{2}$	46	
$\frac{1}{2}$	47	329.5
$\frac{1}{2}$	49	
cb.	54	
E	58	328.4
+5	59	

33417

50th St.

25

5+00		
-5	7.4	
E	6.9	327.3
cb.	6.3	
$\frac{1}{2}$	6.3	
$\frac{1}{2}$	6.0	328.2
$\frac{1}{2}$	6.5	
+2	6.7	
cb.	6.0	
N. on top R.P. Hub 100' N.W. corner		
5+50	5.33	328.84
N	7.3	326.9
cb.	8.8	
$\frac{1}{2}$	9.1	
$\frac{1}{2}$	9.1	325.1
$\frac{1}{2}$	9.1	
cb.	8.7	
+10	8.4	
E	7.5	326.7
+5	7.8	
5+98		
-5	9.0	
E	9.2	325.0
+9	11.8	
cb.	12.3	
$\frac{1}{2}$	12.2	

33417

50th

5+

26

$\frac{1}{2}$	117	322.5
$\frac{1}{4}$	116	
+5	117	
cb	111	
+10	89	
X	87	325.5

6+00. = N.L. Orange Rice

X	11.0	
" top cb.	11.06	323.11
" Gut	11.7	
$\frac{1}{4}$	117	
$\frac{1}{2}$	11.8	322.4
$\frac{1}{4}$	12.3	
Gut	12.5	
E top cb.	11.98	322.19
E	12.00	
T.P.	0.27	321.81
T.P.	12.63	321.54
T.P.	9.05	312.76

N.E. Polk
Orange & Hodona
rail

Walker
Ketchum
Stover
Leach
10-28-28

Cross Section Alhondra St. 60' wide
12' obs.
7' obs.
From Sh. El Cajon to N.W. Orange Ave.

393.15

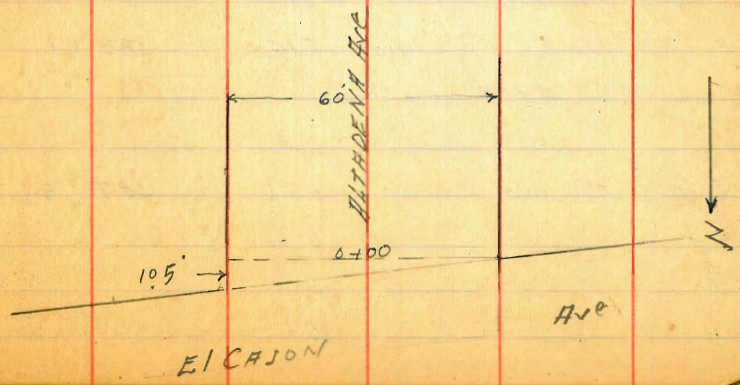
	705	393.15	386.10
		St. El Cajon	
N		5.3	
" top cb.		5.59	387.56
" Gut on Pavimg		6.18	386.97
" 1/4 "		5.88	387.21
1/2 "		5.70	387.45
E 1/4 "		5.77	387.38
" Gut "		5.96	387.19
" top cb.		5.39	387.76
E.		5.3	
	0+00		
E		5.4	
" top cb.		5.35	387.80
" Gut		6.0	
" 1/4 "		5.6	
1/2 "		5.5	387.7
N 1/2 "		5.9	
" Gut		6.1	
" top cb.		5.60	387.55
N		5.4	
	0+25		
N top cb.	1191' inst.	5.62	387.53
E top cb.	1210' inst.	5.29	387.86
	0+50		
E		5.1	

N.E. Top Hydt.
El Cajon, 50th
See Page 14

Plotted 10-30-28 - CBH

Note: All curb is ok for alignment unless noted otherwise

E top cb.	1210' inst.	5.25	387.90
Gut		5.6	
1/2 "		5.4	
1/4 "		5.2	388.0
Gut		5.6	
Gut		6.0	
N top cb.	1190' inst.	5.62	387.53
N		5.6	
	0+75		
N top cb.		5.60	387.55
E " cb	1205' inst.	5.22	387.93
	1+00		
E		5.2	
" top cb.		5.18	387.97
" Gut		5.5	
" 1/4 "		5.3	
1/2 "		5.2	388.0



393.15

$\frac{1}{4}$		5.6	
Gut		6.0	387.2
X top cb.		5.69	387.46
X		5.4	
	1+25		
X top cb.	11.85' inst.	5.56	387.59
E " "		5.18	387.97
	1+50		
E		5.0	
E top cb.	11.92' inst.	5.13	388.02
" Gut.		5.6	387.6
" $\frac{1}{4}$		5.4	
$\frac{1}{2}$		5.0	388.2
W $\frac{1}{2}$		5.0	
" Gut		5.9	387.3
" top cb.	11.90' inst.	4.61	388.54 ?
X		5.2	
	1+75		
X top cb.	11.90' inst.	5.53	387.62
E " "	11.90' "	5.14	388.01
	2+00		
E		5.3	
E top cb.	11.96' inst.	5.21	387.94
Gut		5.7	387.5
$\frac{1}{4}$		5.5	
$\frac{1}{2}$		5.1	388.1

393.15

#1 Adena

$\frac{1}{4}$		5.3	28
Gut		5.7	387.5
X top cb.	11.90' inst.	5.62	387.53
X		5.4	
	2+25		
X top cb.		5.59	387.56
E " "	11.90' inst.	5.36	387.79
	2+50		
E		5.6	
E top cb.	11.95' inst.	5.50	387.65
" Gut.		6.1	387.1
" $\frac{1}{4}$		5.7	
$\frac{1}{2}$		5.4	387.8
W $\frac{1}{2}$		5.6	
" Gut		6.0	387.2
" top cb.		5.67	387.48
X		5.6	
	2+75		
X top cb.		5.72	387.43
E " "		5.55	387.60
	3+00		
E		5.8	
E top cb.	11.95' inst.	5.68	387.47
" Gut		6.2	387.0
" $\frac{1}{4}$		5.9	
$\frac{1}{2}$		5.6	387.6

393.15

$\frac{1}{2}$	5.8	
Gut	6.3	386.9
N top cb.	5.80	387.30
N	6.0	
3+12		
N top cb.	5.80	387.35
E " "	5.84	387.31
3+25		
E " "	6.01	387.14
N " "	6.00	387.15
3+40		
N " "	6.40	386.75
E " "	6.21	386.94
3+50		
E	6.7	
E top cb. 12.10' inst.	6.40	386.75
" Gut	7.0	386.2
" $\frac{1}{2}$	6.7	
$\frac{1}{2}$	6.3	386.9
N $\frac{1}{2}$	6.7	
" Gut	7.0	386.2
" top cb.	6.46	386.69
N	6.7	386.5
3+75		
N top cb.	6.87	386.28
E " " 12.10' inst.	6.86	386.29

393.15

Atadlena

29

4+00		
E	7.5	
E top cb. 12.10' inst.	7.21	385.94
" Gut	7.5	385.7
" $\frac{1}{2}$	7.2	
$\frac{1}{2}$	7.1	386.1
$\frac{1}{2}$	7.3	
Gut.	7.6	385.6
N top cb.	7.27	385.88
N	7.5	
T.P. 0.98	7.54	385.61
4+25		
N top cb.	1.22	385.37
E " " 12.10' inst.	1.02	385.57
4+50		
E	1.3	
E top cb. 11.90' inst.	1.49	385.10
Gut	1.8	
$\frac{1}{2}$	1.5	
$\frac{1}{2}$	1.7	384.9
$\frac{1}{2}$	1.1	
Gut.	1.8	
N top cb.	1.5	385.1
4+75		
N	2.4	
N top cb. 11.93' inst.	2.65	383.94

386.59

Gut	3.1	
$\frac{1}{2}$	2.6	
$\frac{1}{6}$	2.2	384.4
$\frac{1}{4}$	2.6	
Gut	3.1	
E top cb. 11.95' inst.	2.54	384.05
E	2.5	
5+00		
E	4.1	
E top cb. 11.78' inst.	3.95	382.64
Gut	4.7	
$\frac{1}{4}$	4.0	
$\frac{1}{6}$	3.6	383.0
$\frac{1}{4}$	4.0	
Gut	4.7	
X top cb. 12.05' inst.	4.15	382.49
X	3.9	
5+22.6		
X	4.9	
+2	5.7	
X top cb.	5.83	380.76
Gut	6.7	
+1.	7.1	
+3	7.0	
+5	6.0	
$\frac{1}{2}$	5.5	

386.59

$\frac{1}{2}$	5.1	381.5	30
$\frac{1}{4}$	5.7		
Gut	6.0		
E top cb. 12.30' inst.	5.54	381.05	
E	5.5		
5+35			
E top cb. 11.90' inst.	6.55	380.04	
X " "	7.24	379.35	
5+53			
X	7.2		
+2	8.4		
+4	8.0		
cb.	8.14	378.45	
Gut	9.5		
+4	10.7		
+6	10.0		
$\frac{1}{4}$	8.2		
$\frac{1}{6}$	7.8	378.8	
$\frac{1}{4}$	9.0		
Gut	9.4		
E top cb.	8.10	378.49	
E	8.0		
5+61			
E top cb.	9.23	377.36	
X " "	8.71	377.88	
5+74			

Notes

38659

34		7.8	
+1		9.3	
X top cb	11.50' inst.	9.77	376.82
Gut		12.2	374.4
+2		12.3	
+3		10.7	
$\frac{1}{4}$		10.3	
$\frac{1}{2}$		10.2	376.4
$\frac{1}{2}$		11.5	
+6		11.6	
+7		12.3	
Gut		12.4	374.2
E top cb.	12.20' inst.	10.28	376.31
+10		10.2	
E		9.7	
	5+90		
E top cb.	11.70' inst.	11.48	375.11
X " "	12.25' inst.	11.87	374.72
	6+06		
X		11.4	
+3		12.5	
X top cb.	11.50' inst.	12.30	374.29
" Gut.		13.5	373.1
+3		13.7	
$\frac{1}{4}$		13.2	
E		12.9	373.7

38659

31

+6		13.3	
$\frac{1}{4}$		14.4	
+3		14.6	
+6		14.3	
Gut.		13.7	
E top cb.	12.12' inst.	12.86	378.73
+10		12.6	
E		12.0	
T.P.	045	373.96	13.08
	6+25		373.51
E		10	
+3		2.0	
E top cb.	11.70' inst.	1.85	372.11
" Gut.		2.3	
$\frac{1}{4}$		2.3	
$\frac{1}{2}$		1.6	372.3
$\frac{1}{4}$		2.1	
+6		2.6	
Gut		1.9	
X top cb.	11.30' inst.	10.4	372.92
+6		1.2	
+10		1.4	
X		0.5	
	6+50		
X		2.2	
+3		3.3	

373.96

N top cb. 11.20' inst. 285 371.11

Gut 3.3

 $\frac{1}{2}$ 3.4 $\frac{1}{4}$ 3.5 370.4 $\frac{1}{4}$ 3.9

+6 4.3

Gut 4.6

E top cb. 11.70' inst. 3.95 370.01

E 3.8

6+57.96 = N.L. Trojan St.

For X, Sect 1011
In the 1161-74
Book 1161-74

E 6.6

+11 5.1

E top cb. 11.60' inst. 4.66 369.30

Gut 5.4

+4 5.9

 $\frac{1}{2}$ 4.9 $\frac{1}{4}$ 4.3 369.6 $\frac{1}{4}$ 4.0

Gut 3.8

N top cb. 11.10' inst. 3.44 370.52

N 3.2

S.L. TROJAN = 0+00

N 8.5 365.4

+5 10.0

cb. 10.3

 $\frac{1}{4}$ 10.2

373.96

32

L 11.0 362.9

+1 10.6

 $\frac{1}{4}$ 10.8

cb. 10.7

E 15.6 358.3

+20 16.4

T.P. 0 25 361.63 12.58 361.38

0+12

-20 7.1

E 5.3 356.3

cb. 0.4

+2 0.2

 $\frac{1}{4}$ 0.2 $\frac{1}{2}$ 0.5 361.1

+1 0.1

 $\frac{1}{2}$ 0.1

cb. 0.5

+6 0.2

N 1.5 363.1

0+32

N 1.9 359.7

+3 3.2

+10 4.9

cb. 4.3

+3 3.2

 $\frac{1}{4}$ 3.8

36163

+3	2.8	
+8	3.0	
$\frac{1}{2}$	3.8	357.8
$\frac{1}{4}$	3.3	
cb.	3.4	
E	8.4	353.2
+20	10.7	
-20	12.7	
E	11.1	350.5
+6	10.8	
+7	9.0	
cb.	6.6	
+2	6.3	
$\frac{1}{4}$	6.3	
$\frac{1}{2}$	6.6	355.0
+2	6.0	
$\frac{1}{4}$	5.9	
+1	7.5	
+3	7.3	
+5	6.2	
cb.	7.0	
+4	7.7	
+6	6.0	
yr	5.0	356.6

0+68

36163

yr	8.2	353.4	33
+3	8.5		
+8	9.6		
+9	11.3		
+11	11.5		
cb.	9.2		
$\frac{1}{4}$	8.7		
+7	8.6		
+8	9.5		
E	9.3	352.3	
$\frac{1}{2}$	9.2		
cb.	9.2		
+4	11.5		
+5	13.4		
E	13.5	348.1	
+1	14.5		
+15	14.6		
-15	15.0		
-1	14.5		
E	13.8	347.8	
+7	13.7		
+8	11.7		
cb.	9.7		
+2	9.2		
$\frac{1}{4}$	9.5		

0+71

361.63

6			9.7	351.9
+1			9.0	
$\frac{1}{4}$			9.0	
+7			9.7	
+8			11.7	
cb.			11.6	
+5			12.8	
+6			9.5	
X			8.6	353.0
	0+91			
X			12.1	349.5
T.P.	0.32	349.72	12.23	342.40
+5			2.9	
cb.			2.2	
+4			0.7	
$\frac{1}{4}$			0.2	
+7			0.3	
$\frac{1}{4}$			0.8	348.9
$\frac{1}{4}$			0.6	
+6			0.4	
cb.			1.4	
+4			3.2	
E.			3.7	346.0
+15			4.2	
	1+11			
-15			6.3	

349.72

34

E-1			6.7	
E			6.0	343.7
+9			5.8	
cb.			4.4	
+3			3.5	
$\frac{1}{4}$			3.5	
$\frac{1}{4}$			3.8	345.9
$\frac{1}{4}$			3.5	
cb.			4.7	
X			3.1	346.6
		1+54		
X			7.9	341.8
cb.			9.3	
+5			9.7	
$\frac{1}{4}$			9.2	
+7			9.1	
$\frac{1}{4}$			9.5	340.2
$\frac{1}{4}$			8.8	
+7			9.0	
cb.			9.6	
E			10.3	339.4
+10			10.9	
-10			13.27	
-0.5' on Walk			13.25	336.47 ✓
E			13.3	336.4

1+84 = $\frac{1}{2}$ Con. Walk. on East 0.5' Feet S' side

349.72

+9		12.5	
cb		12.5	
+4		11.8	
$\frac{1}{2}$		11.8	
$\frac{1}{2}$		12.3	337.4
$\frac{1}{4}$		12.5	
cb.		12.3	
W		11.0	338.7
T.P.	0.05	12.71	337.01
	R+100		
W		0.7	336.4
cb.		1.2	
$\frac{1}{4}$		1.1	
$\frac{1}{2}$		1.1	336.0
$\frac{1}{4}$		1.1	
cb.		1.1	
E		1.8	335.3
+10		2.0	
	R+25		
-5		3.9	
E		3.8	333.3
+10		2.7	
cb.		2.8	
$\frac{1}{2}$		3.5	
$\frac{1}{2}$		3.5	333.6
$\frac{1}{4}$		3.1	

33706

35

cb.		3.3	
W		3.0	334.1
	2+50		
W		5.3	331.8
cb.		5.7	
$\frac{1}{4}$		5.0	
$\frac{1}{4}$		5.6	331.5
$\frac{1}{4}$		5.5	
cb.		5.1	
+4		4.9	
E		6.4	330.7
+5		7.0	
	2+70		
-5		8.5	
E		8.0	329.1
+9		7.0	
cb.		7.0	
$\frac{1}{4}$		6.9	
$\frac{1}{2}$		7.0	330.1
$\frac{1}{2}$		6.8	
cb.		6.6	
W		6.7	329.4
	3+100		
W		8.2	328.9
cb.		8.4	
$\frac{1}{4}$		8.4	

33706

cb	8.7	328.4
$\frac{1}{4}$	9.1	
cb.	9.0	
E	10.2	326.9
+5	10.9	
	3+25	
-5	12.0	
E	11.3	325.8
+8	10.3	
cb.	10.3	
$\frac{1}{4}$	10.2	
$\frac{1}{2}$	9.8	327.3
$\frac{1}{4}$	9.7	
cb.	9.7	
W	9.6	327.5
	3+73 = North end Glass house on E 2' Back	
W	11.2	325.9
cb.	11.2	
$\frac{1}{2}$	11.6	
$\frac{1}{4}$	11.8	325.3
$\frac{1}{4}$	12.0	
cb.	12.1	
E	14.2	322.9
+2 at House	14.5	322.6
	4+00	
-2' at Glass house	15.5	

33706

E	15.5	321.6	36
cb.	18.3		
$\frac{1}{4}$	13.1		
$\frac{1}{2}$	12.7	324.4	
$\frac{1}{2}$	12.5		
cb.	12.2		
W	12.1	325.0	
T.P.	0.98	325.48	
	4+50		
W	1.2	324.3	
+8	2.3		
cb.	2.1		
$\frac{1}{4}$	2.3		
$\frac{1}{2}$	2.7	322.8	
$\frac{1}{2}$	2.8		
+5	2.7		
cb.	3.4		
+10	4.6		
E	6.0	319.5	
+2 at Glass house	5.7		
	4+67		
-2 at House	6.4		
E	6.2	319.3	
cb.	3.2		
$\frac{1}{2}$	3.2		
$\frac{1}{2}$	3.1	322.4	

32548

$\frac{1}{2}$	2.8	
cb.	2.8	
+5	3.2	
X	2.3	323.2
4+97 = 6 con. walk and steps on West		1.2' Back
top of Bottom step	1.62 ✓	323.86
" " top "	0.21 ✓	325.27 5.2' Back
" Walk	0.40 ✓	325.08 15' Back
5+03 = South end Glass House on E		
X	3.7	321.8
+4	5.2	
cb.	5.8	
$\frac{1}{4}$	5.6	
$\frac{1}{4}$	5.5	320.0
$\frac{1}{4}$	5.5	
+4	4.6	
cb.	6.0	
+4	6.3	
E	8.0	317.5
+2 at Glass base	8.3	317.2 ✓
5+25		
-10	12.1	
E	9.6	315.9
cb.	6.3	
+4	5.1	
+6	5.1	

32548

$\frac{1}{2}$	6.5		37
$\frac{1}{2}$	7.3	318.2	
$\frac{1}{2}$	7.4		
cb.	7.5		
+7	6.8		
X	5.2	320.3	
+5 = top Bank = Lid level	1.2		
5+50			
X	8.7	316.8	
+5	9.8		
cb.	10.0		
$\frac{1}{4}$	9.8		
$\frac{1}{4}$	9.7	315.8	
+4	9.2		
$\frac{1}{4}$	7.6		
cb.	10.0		
E	17.7	307.8	
+15	20.5		
T.P.	363 317.27	11.84	313.64
5+89			
-15	10.7		
-1' on top Xing Wall ✓	4.99	320.49	see plans Orange St. Grading
E	11.5	305.8	
cb.	9.7		
$\frac{1}{2}$	9.0		
$\frac{1}{2}$	4.8	312.5	

$\frac{1}{2}$	4.6	
cb.	5.0	
W	5.5	311.8
+5	5.5	
G + 00 = N.L. Orange		
W-5	4.3	
W	4.4	312.9
W top cb.	4.73	312.54
Gut	5.0	
$\frac{1}{4}$	4.6	
$\frac{1}{2}$	4.8	312.5
$\frac{1}{2}$	5.1	
+ 5.5' on toe Apron	5.65	
Gut + Con. "	5.75	311.52
E top cb.	4.87	312.40
E " Wing Wall ✓	4.96	312.31
chk. on T.P. Page 26	4.53	312.74
		312.76
		.0.02 = Error.

Walker
Rupture
Leaky
Mo. 10-26-28

CURB LEVELS

ISLAND ST.

Bet. 27th + 26th st.

	12.15	138.74		126.59
	12.33	110.36		98.08
T.P.	12.65	122.65	0.36	110.00
T.P.	12.78	134.78	0.65	122.00
T.P.	12.71	146.80	0.67	134.09

W. 27th st. = 0+00 = End Exist. cb. on South

S top cb			3.86	142.94
" Gut on Pav.			4.51	142.29
" 1/4 "			4.70	142.10
" 1/2 "			4.94	141.86
N 1/4 "			5.56	141.24
" Gut "			6.18	140.62
" top cb			5.68	141.12
	0+25			
N top cb			3.56	143.24
S cb. on Ground			2.1	144.7
	0+50			
S " " "			0.2	146.6
N top cb			1.40	145.40
T.P.	12.53	159.00	0.33	146.47
	0+75			
N top cb			11.46	147.54
S cb. on Ground			10.2	148.8
	1+00			
S " " "			8.0	151.0

Plotted 11-16-28-C.B.H.

NE SP

MARKET + 27th
S.W. SP
Island + 28th

Note: No curb or walk on South Bet. Station
0+00 and 1+50

159.00

39

N top cb			9.21	149.79
	1+25			
N " "			7.05	151.95
S cb. on Ground			5.9	153.1
	1+50 = beginning	Exist. cb. and walk on South		
S top cb			3.44	155.56
			4.82	154.18
	1+75			
N top cb			2.66	156.34
S " "			1.39	157.51
T.P.	12.88	171.74	0.14	158.86
	2+00			
S top cb			12.07	159.67
N " "			13.17	158.57
	2+25			
N " "			10.94	160.80
S " "			9.99	161.75
	2+50			
S " "			7.85	163.89
N " "			8.70	163.04
	2+75			
N " "			6.56	165.18
S " "			5.77	165.97
	2+93			
S " "			4.26	167.48
N " "			5.01	166.73

171.74

3+00

N. cb. in Drive Way

5.00

166.74

S top cb

3.67

168.07

3+03

S " "

3.43

168.31

N " "

4.17

167.57

3+10

N " "

3.71

168.03

S " "

2.94

168.80

3+20

S cb. on Drive Way

3.02

168.72

N top cb

3.12

168.62

3+30

N " "

2.75

168.99

S " "

1.88

169.86

3+40

S " "

1.58

170.16

N " "

2.42

169.32

3+50

N " "

2.22

169.52

S " "

1.38

170.36

3+60

S " "

1.28

170.46

N " "

2.08

169.66

3+70

N " "

2.00

169.7

171.74

S top cb

1.21

170.53

3+80

S " "

1.15

170.59

N " "

1.93

169.81

3+90

N " "

2.13

169.61

S " "

1.27

170.47

4+00

S " "

1.47

170.27

N " "

2.31

169.43

4+10

N " "

2.75

168.99

S cb. on Drive Way

2.53

169.21

4+20

S top cb

2.40

169.34

N " "

3.22

168.52

4+26

N top cb

3.70

168.04

S " "

2.67

169.07

4+35

S " "

3.59

168.15

N " "

4.52

167.22

4+45

N " "

5.56

166.18

S " "

4.60

167.14

4+75.7 = End exist. cb. and walk on South

40

S top cb		8.74	163.00
N " "		9.25	162.49
	4+95		
N " "		11.62	160.12
S cb. on Ground		11.5	160.2
T.P.	0.46 159.32	12.88	158.86
	5+20		
S cb. on Ground		2.5	156.8
N top cb.		2.22	157.10
	5+45		
N " "		5.33	153.99
S cb. on Ground		5.8	153.5
	5+70		
S " " "		9.2	150.1
N top cb.		8.43	150.89
	6+00.7 = 5.6. 26 ^{1/11}		
N " "		12.16	147.16
N Gut. on Poring		12.93	146.39
" $\frac{1}{4}$ " "		12.86	146.46
" $\frac{1}{2}$ " "		13.07	146.25
S $\frac{1}{4}$ " "		13.37	145.95
" Gut " "		13.86	145.46
top cb.		13.27	146.05
T.P.	9.76 157.09	11.99	147.33
cbt. on SW. B.P. Market +26 ^{1/4}		3.59	153.50
			153.58 = BM.
			0.08 = Error or diff.

40th ST X Sec
Logan to T. St.

S.W. 40th
National

B.M. Top Hyd 12.00 77.38 65.38

00 = N line of Logan Produced from East.

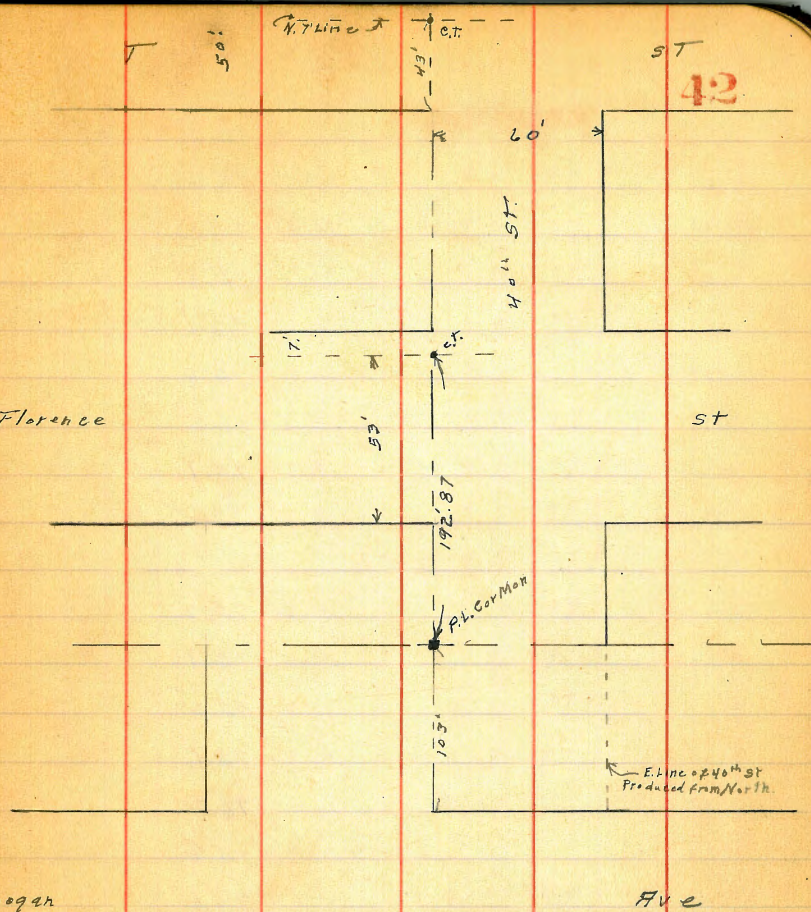
c	5.7	71.7
cb	5.0	72.4
"4	4.5	72.9
c	4.0	73.4
"4	3.6	73.8
cb	3.5	73.9
W	3.2	73.7
W+25	7.7	69.7
N+60	8.1	69.3
10' N		
W-60	7.0	70.4
W-40	6.1	71.3
W-25	7.0	70.4
W-10	5.5	71.9
W	3.2	74.2
cb	2.5	74.9
"4	2.5	74.9
c	3.3	74.1
"4	4.1	73.3
cb	4.8	72.6
E	5.6	71.8
15' N		
E	5.5	71.9
cb	4.8	72.6

Plotted 11/23/28

T.H.

Florence

Logan



77.38

15' N. (con)

e 14	3.9	73.5
e	3.2	74.2
14	2.4	75.0
cl	2.1	75.3
W	2.3	75.1
W+10	3.4	74.0
+14	5.8	71.6
+20	3.7	73.7
+40	3.2	74.2

30' N.

N-60	2.2	75.2
W-25	2.7	74.7
W-5	2.2	75.2
W	0.8	76.6
cl	1.2	76.2
14	2.0	75.4
e	2.4	74.6
14	3.5	73.9
cl	4.2	73.2
e	5.0	72.4
T.P.	7.40	82.25
	2.53	74.85

50' N

e	7.3	75.0
cl	6.2	76.1
14	6.0	76.3
e	6.1	76.2

82.25

40th St

43

14	6.0	76.3
cl	5.5	76.8
W	4.6	77.7
cl	6.0	76.3
N+40	6.4	75.9

75' N

W-30	4.8	77.5
W-3	4.6	77.7
W	3.8	78.5
cl	4.6	77.8
14	5.2	76.1
e	5.4	76.9
14	5.3	77.0
cl	5.3	77.0
e	6.2	76.1

100' N

e	6.4	75.9
cl	6.3	76.0
14	5.3	77.0
e	5.1	77.2
14	4.5	77.8
cl	3.7	78.6
W	2.5	78.8
+10	3.7	78.6

103' N on W = P.L.

82.25

110'N

N	2.9	79.9
cl	3.2	79.1
"	3.8	78.5
e	4.1	78.2
"	4.3	78.0
cl	4.8	77.6
e	5.3	77.0

140'N

e	4.3	78.0
cl	3.4	78.9
"	3.3	79.0
e	3.0	79.3
"	2.9	79.4
cl	2.8	79.5
+8	2.3	80.0
W	1.5	80.8

170'N

W	1.2	81.1
+5	2.3	80.0
cl	2.4	79.9
"	2.9	79.4
e	2.8	78.5
"	3.4	78.9
cl	3.8	78.5
e	4.2	78.1

82.25

200'N

e	4.6	77.7
cl	4.1	78.2
"	4.0	78.3
e	5.2	77.1
"	4.4	77.9
cl	3.7	78.6
W	1.7	80.6

230'N

W	4.3	78.0
+3	5.6	76.7
cl	6.6	75.7
"	7.4	74.9
e	7.8	74.5
"	7.8	74.5
cl	7.9	74.4
e	7.9	74.4

243'N = S. Line Florence

-5	9.8	72.5
e	9.6	72.7
cl	9.3	73.0
"	8.9	73.4
e	8.3	74.0
"	7.9	74.4
cl	7.4	74.9
W	7.1	75.2

40th St

44

	82.25 S. ch		amt. ch
W. No return	7.25	75.00	
ch	7.7	74.6	
"4	8.0	74.3	
E	8.3	74.0	
"4	8.7	73.6	
ch	9.4	72.9	
E	9.9	72.4	
+10	10.2	72.2	
	5.14		
-10	10.7	71.6	
E	9.9	72.4	
ch	9.4	72.9	
"4	8.9	73.4	
E	8.2	74.1	
"4	8.0	74.3	
ch	7.6	74.7	
W	7.2	75.2	
	Φ Florence		
W	6.8	75.5	
ch	7.4	74.9	
"4	7.8	74.5	
E	8.3	74.0	
"4	9.0	73.3	
ch	9.5	72.8	
E	10.5	71.8	
+10	11.0	71.3	

	82.25 R. N. of Φ	
E	10.5	71.8
ch	9.5	72.8
+8	9.3	73.0
"4	11.4	70.9
+3	11.4	70.9
+4	9.0	73.3
E	8.3	74.0
"4	7.9	74.4
ch	7.6	74.7
W	6.8	75.5
	N. 14	
W	6.8	75.5
ch	7.4	74.9
"4	7.9	74.4
E	8.6	73.7
"4	9.3	73.0
+2	9.4	72.9
+6	13.3	69.0
ch	9.9	72.4
E	10.5	71.8
+10	12.0	70.3
	6" N of N. 14	
E	11.0	71.3
+4	10.5	71.8
+6	14.2	68.1
ch	14.0	68.3

82.25

6' N of N. 1/4

E. 1/4	13.8	68.5
e	11.6	70.7
1/4	10.6	71.7
ch	7.5	74.8
w	7.0	75.3
N. ch		
w No Return	4.2	76.03
w	4.8	75.5
ch	7.5	74.8
1/4	8.2	74.1
e	8.8	73.5
+ 9	9.6	72.7
1/4	14.0	68.3
ch	16.5	65.8
e	17.0	65.3
+ 2	11.9	70.4
+ 10	13.5	68.8
5' N of N. ch		
- 10	15.0	67.3
- 5	17.5	64.8
e	12.3	70.0
ch	10.4	71.9
1/4	9.7	72.6
e	9.2	73.1
1/4	8.3	74.0
ch	7.2	75.1
w	6.5	75.8

cont. ch

ground

82.25

00-N Line Florence

40' ST.

46

w	5.9	76.4
ch	6.9	70.4
1/4	8.0	74.3
e	8.9	73.4
1/4	9.8	72.5
ch	10.5	71.8
e	12.3	70.0
+ 9	17.7	64.6
+ 15	17.3	65.0
10' N		
- 15	18.3	64.0
e	14.0	68.3
ch	11.4	70.9
1/4	10.3	72.0
e	8.9	73.4
1/4	7.5	74.8
ch	6.8	75.5
w	5.8	76.5
20' N		
w	5.2	77.1
ch	6.2	76.1
1/4	7.7	74.6
e	9.2	73.1
1/4	11.0	71.3
ch	12.8	69.5
e	15.0	68.3
+ 20	19.0	63.3

	82.25	35'N
E-15	17.3	65.0
E	13.8	68.5
ch	11.5	70.8
"4	9.7	72.6
C	8.0	74.3
"4	6.0	76.3
ch	4.8	77.5
W	4.2	78.1
	50'N	
W	2.8	79.5
ch	4.0	78.3
"4	5.6	76.7
C	7.3	75.0
"4	9.0	73.3
ch	10.8	71.5
E	13.2	69.1
+15	16.4	65.9
	65'N	
-15	16.6	65.7
E	13.0	69.3
ch	11.0	71.3
"4	9.2	73.1
C	7.7	74.6
"4	5.9	76.4
ch	4.0	78.3
W	2.6	79.7

	82.25	80'N	40 th St	
W		4.1	78.2	
ch		5.5	76.8	
"4		7.1	75.2	
C		9.3	73.0	
"4		11.0	71.3	
ch		12.6	69.7	
E		14.1	68.2	
T.P.	1.67	21.35	12.57	69.68
E+15			6.8	64.6
		100'N		
E-15		8.8	62.6	
E		6.3	65.1	
ch		4.9	66.5	
"4		3.4	68.0	
C		2.1	69.3	
"4		0.5	70.9	
ch		+ 0.8	72.1	
W		+ 2.0	73.3	
		125'N		
W		4.4	67.0	
ch		5.0	66.4	
"4		6.1	65.3	
C		7.3	64.1	
"4		8.1	63.3	
ch		9.3	62.1	
E		10.9	60.5	
+10		12.4	59.0	

47

71.35

133' N.

E-10	13.5	57.9	
E	12.1	59.3	
ch	11.0	60.4	
"4	10.0	61.9	
e	9.0	62.4	
"4	8.0	63.4	
ch	7.0	64.4	
+1 = M. H. No. yardage	5.9	65.5	Top
W	6.8	64.6	

140' N

W	2.0	64.4	
ch	7.8	63.6	
"4	8.2	63.2	
e	10.0	61.4	
"4	10.7	60.7	
ch	11.7	59.7	
e	12.5	58.9	
+10	14.6	56.8	
T.P.	0.29	58.64	13.00 58.35

175' N

E-15	9.1	49.5	
E	7.8	50.8	
ch	7.1	51.5	
"4	6.8	51.8	
e	6.2	52.4	
"4	5.2	53.4	

58.64

40² 54

48

ch	4.2	54.4	
W	3.3	55.3	
+10	1.6	57.0	

200' N

-10	5.8	52.8	
W	6.4	52.2	
ch	7.0	51.6	
"4	7.4	51.2	
e	7.6	51.0	
"4	8.4	50.2	
+5	10.2	48.4	
ch	10.4	48.2	
e	11.0	47.6	
+15	11.4	47.2	

215' N

-15	10.6	48.0	
e	9.9	48.7	
ch	10.1	48.5	
"4	10.3	48.3	
e	10.0	48.6	
"4	8.8	49.8	
ch	7.9	50.7	
+5	6.6	52.0	
W	6.9	51.7	
+10	6.4	52.2	

58.64
230' N

-10	5.7	52.9
W	6.4	52.2
ch	7.3	51.3
1/4	7.8	50.8
E	8.7	49.9
1/4	8.9	49.7
ch	10.0	48.6
E	10.9	47.7
+10	11.1	47.5

245' N

-10	9.2	49.4
E	9.7	48.9
+4	10.8	47.8
ch	10.7	47.9
F3	10.7	47.9
1/4	8.7	49.9
E	8.5	50.1
1/4	8.1	50.5
ch	7.2	51.4
W	6.8	51.8

255' N

W	8.8	49.8
ch	8.6	50.0
1/4	9.1	49.5
E	9.3	49.3
+3	10.3	48.3

58.64

1/4	10.5	48.1
+3	10.5	48.1
+6	9.1	49.5
ch	8.9	49.7
E	8.7	49.9

265' N. = S. Line T-5T. ^{50' width}
_{7.5' ch}
_{1/4}

E	8.0	50.6
ch	7.8	50.8
1/4	8.6	50.0
+9	9.3	49.3
E	10.2	48.4
1/4	10.0	48.6
+3	9.0	49.6
ch	8.9	49.7
W	9.0	49.6

5. ch

W	9.10	49.54
N	9.5	49.1
ch	9.7	48.9
1/4	8.2	50.4
E	7.4	51.2
1/4	7.2	51.4
ch	7.1	51.5
E	7.5	51.1

40th St.

49

unt ch
no return
ground

58.64

S. 1/4

e	7.0	51.6
cl	6.7	51.9
1/4	6.0	52.6
r	6.9	51.7
e	7.7	50.9
1/4	8.5	50.1
cl	9.1	49.5
w	9.3	49.3

E. T. St.

w	7.4	51.2
w	8.6	50.0
cl	8.4	50.2
1/4	7.9	50.7
e	7.6	51.0
1/4	7.0	51.6
cl	6.2	52.4
e	6.3	52.3

N. 1/4

e	5.8	52.8
cl	6.2	52.4
1/4	6.5	52.1
e	7.0	51.6
1/4	7.6	51.0
cl	8.6	50.0
w	8.5	50.1

Top M.H.
Noyardage
ground

58.64

N. cl

w cmt Return in	8.09	50.55
w	8.4	50.2
cl	8.3	50.3
1/4	7.6	51.0
e	6.7	51.9
1/4	6.0	52.6
cl	5.6	53.0
e	5.6	53.0

N. Line T. St.

e	5.5	53.1
cl	5.5	53.1
1/4	5.2	53.4
e	6.3	52.3
1/4	7.4	51.2
1/4 gutter	8.0	50.6
w. cmt. curb	7.56	51.08

40th St

50

cmt. cl.
gutter

60' wide
10' chs
40' Rdw.

38th St Curb Levels
Woolman to National

12-15-24
million

S.E. Top Hdyt 37th
+ Woolman Ave

B.M.	8.30	71.72	63.42
T.P.	12.52	83.97	0.27 71.45
		00 = S. line Woolman Ave	
E. ent. ch		2.90	81.07
gutter Pavmt		3.60	80.37
1/4 "		3.32	80.65
c "		3.38	80.59
1/2 "		3.74	80.23
gutter "		4.44	79.53
W. ent. ch		3.95	80.02
		59.85	
W. ent. ch		0.95	83.02
E. " "		0.24	83.73
S.E. B.M. Top Hdyt		0.36	83.59
T.P.	9.10	93.01	0.06 83.91
		119.75 = N. Line Teak on W.	
E. ent. ch		6.60	86.41
W. " "		7.00	86.01
		135.25 = N. Line Alley on E	
E. ent. ch		4.37	86.64
E. Line ent. ch Ret		6.10	86.91
		150.25 = S. Line Alley on E	
E. ent. ch		4.13	86.88
E. Line Alley Ret		6.00	87.01

S.E. 38th
+ Woolman

	129.75 = N. ch. Teak on W.	6.91	86.10
W. line ent. ch. Ret			
	169.75 = S. ch. Teak on W.		
W. line ent. ch. Ret		6.02	86.99
	179.75 = 5 line Teak on W.		
W. ent. ch		5.98	87.03
E. " "		5.99	87.02
	230.5		
E. ent. ch		5.52	87.49
W. " "		5.47	87.54
	286.35 = N. Line Teak on E		
W. ent. ch		4.84	88.17
E. " "		5.00	88.01
	296.35 = N. ch Teak on E		
E. Line ent. ch. Ret		5.00	88.01
	300.75 = N. Line Alley on W		
W. ent. ch		4.42	88.39
W. Line - ent. ch. Ret		4.33	88.68
	318.75 = S. Line Alley		
W. ent. ch		4.40	88.61
W. Line - ent. ch. Ret		4.20	88.81
	337.75 = S. ch Teak on E		
E. Line ent. ch. Ret		4.60	88.41
	344.35 = S. Line Teak on E.		
E. ent. ch		4.80	88.51
W. " "		4.13	88.88

51
This station should
be on opposite page

93.01

443.55 = N. line SST on W.

E. ent. ch 2.31 90.70

W. " " 3.08 89.93

453.55 = N. ch. SST on W.

W. line ent. ch ret. 3.02 89.99

493.55 = S. ch. SST on W.

W. line ent. ch ret. 2.02 90.99

503.55 = S. Line SST on W.

W. ent. ch 2.00 91.01

E. " " 0.92 92.09

545.55 = N. line SST on E.

E. ent. ch 0.00 93.01

W. " " 1.28 91.73

T.P. 4.41 96.76 0.66 92.35

555.55 = N. ch. SST

E. Line ent. ch ret 3.76 93.00

gutter on pavmt E. line 4.18 92.58

562.55 = N. "4

E. Line Pavmt 3.85 92.91

570.55 = ϕ

E. Line pavmt 3.70 93.06

577.55 = S. "4

E. Line Pavmt 3.65 93.11

585.55 = S. ch. SST on E

E. line gutter pavmt 3.80 92.96

E. " ent. ch. 3.31 93.45

96.76

38th ST.595.55 = S. Line SST on E.

E. ent. ch 3.21 93.55

W. " " 4.18 92.58

624.55 = N. Line Alley on W.

W. ent. ch 3.48 93.28

W. Line Alley ret 3.22

646.55 = S. Line Alley on W.

W. ent. ch. 3.10 93.66

W. Line Alley ret 2.91 93.85

655.55 = Brk

W. ent. ch 3.00 93.76

E. " " 2.39 94.37

675.55 = Brk

E. ent. ch 2.15 94.61

W. " " 2.65 94.11

695.55 = Brk

W. ent. ch. 2.56 94.20

E. " " 2.09 94.67

715.55 = Brk

E. ent. ch 2.26 94.50

W. " " 2.78 93.98

735.55 = Brk

W. ent. ch 3.10 93.66

E. " " 2.53 94.23

770.55 = N. Line TST on W.

E. ent. ch 3.23 93.53

W. " " 3.92 92.94

52

96.76

T.P. B.M.	0.46	96.67	0.55	96.21
		780's = N. line "T" St on W.		
W. line emt. el. ret.		3.74		93.02
		795's = N. line "T" St on E.		
E. emt. el.		3.67		93.09
		805's = N. line "T" St on E.		
E. line emt. el. ret.		3.64		93.12
		820's = S. line "T" St on W.		
W. line emt. el. Ret.		4.69		92.07
		830's = S. line "T" St on W.		
W. emt. el.		4.65		92.11
		835's = S. line "T" St on E.		
E. line emt. el. ret.		4.77		91.99
		845's = S. line "T" St on E.		
E. emt. el.		4.70		92.06
W. " "		5.09		91.67
		900' S.		
W. emt. el.		6.53		90.23
E. " "		6.00		90.76
		955's = N. line Alley on W.		
W. emt. el.		7.89		88.87
W. line emt. Alley ret.		7.70		89.06
T.P.	3.19	91.46	8.40	<u>88.27</u>
		970's = N. line Alley on E.		
E. emt. el.		2.34		89.12
E. line emt. Alley Ret.		2.20		89.26

Top Hydt 58. 38th
+ "S" Sts

91.46

		973's = S. line Alley on W.		
		3.17		88.29
		W. line emt Alley Ret.		2.97
		88.49		
		985's = S. line Alley on E.		
		E. emt. el.		2.66
		88.80		
		E. line emt Alley Ret.		2.47
		88.99		
		1050's		
		E. emt. el.		4.11
		87.35		
		W. " "		5.22
		86.24		
		1098' = N. line Florence on W.		
		W. emt. el.		6.50
		84.96		
		1108's = N. line on W.		
		W. line emt. el. ret.		6.53
		84.93		
		1111's = N. line Florence on E.		
		E. emt. el.		5.40
		86.06		
		1121's = N. line on W.		
		E. line emt. el. Ret.		5.45
		86.01		
		1148's = S. line Florence on W.		
		W. line emt. el. ret.		6.57
		84.89		
		1158's = S. line Florence on W.		
		W. emt. el.		6.53
		84.93		
		1161's = S. line Florence on E.		
		E. line emt. el. ret.		5.51
		85.95		
		1171's = S. line Florence on E.		
		E. emt. el.		5.48
		85.98		
		W. " "		6.05
		85.41		
		T.P. on B.M. Top Hydt 5.16		<u>93.40</u>
		3.22		<u>88.24</u>

38th St.

53

0400

0413

58. 38th St.
Florence

	12 12.12		
	93.40		
	1253.35 = Brk P.V.C.		
W. ent. ch	4.87	88.53	0493
E. " "	4.05	89.35	
	1273.35 = Brk		1153
E. ent. ch	3.45	89.95	
W. " "	4.34	89.06	
	1283.5 S = N. Line Alley on W		1253
W. ent. ch	4.15	89.25	✓
W. Line ent. Alley Ret	3.99	89.41	
	1293.35 = Brk		1313
E. ent. ch	3.26	90.14	
	1295.3 S = N. Line Alley on E.		1313
E. ent. ch	3.26	90.14	
E. Line ent. Alley Ret.	5.05	90.35	
	1310.35 = S. Line Alley on E. & W		1423
E. Line ent. Alley Ret	3.10	90.30	
E. ent. ch	3.30	90.10	
W. ent. ch	4.32	89.08	
W. Line ent. Alley Ret	4.04	89.36	
	1313.35 = Brk.		1553
W. ent. ch	4.42	88.98	
E. " "	3.39	90.01	
	1333.35 = Brk E.V.C.		1753
E. ent. ch	4.05	89.95	
W. " "	5.05	88.35	

	93.40		38 th St.
	1383.35		
W. ent. ch	6.97	86.43	25 th 54
E. " "	6.02	87.38	40' wide 14' ch 52' Adv 4853
	1443.35 = N. Line Logan		
E. ent. ch	8.35	85.05	
W. " "	9.37	84.03	? Sta
	N. of Line Logan Ave		
W. line ent. ch ret	9.57	83.83	
E. " " " "	8.39	85.01	
	S. of Logan Ave		
E. Line ent. ch ret	9.40	84.00	
W. " " " "	10.40	83.00	
	00 = S. Line Logan Ave		
W. ent. ch	10.43	82.97	
E. " "	9.50	83.90	
T.P.	0.48	83.51	
	50'. S.	10.37	83.03
E. ent. ch	0.65	82.86	
W. " "	1.67	81.84	
	100'. S.		
W. ent. ch	2.68	80.83	
E. " "	1.69	81.82	✓
	142.5 = N. Line Alley		
E. line ent. Alley Ret	2.35	81.16	
E. ent. ch	2.54	80.97	
W. " "	3.45	80.06	
W. line ent. Alley Ret	3.25	80.16	

83.51

158 S = S. Line Alley

W. Line ent. Alley Rd	3.71	79.80
W. ent. cl.	3.88	79.63
E. " "	2.83	80.68
E. Line ent. Alley Rd	2.61	80.90

200'S

E. ent cl	3.78	79.73
W. " "	4.81	78.70

250'S

W. ent. cl	5.92	77.60
E. " "	4.88	78.67

300 S = N. Line National Ave

E. ent cl.	5.89	76.62
E. gutter on pavmt.	6.61	76.90
E. 'y " "	6.49	77.02
E. " " "	6.54	76.97
W. 'y " "	6.80	76.71
W. gutter " "	7.30	76.21
W. ent. cl.	6.86	76.65
chk on R.M. B.P.	6.94	76.57 = 76.58

S.E. 38th St
+ National Ave

Walker
Robinson
Lucky
Ma Hood
11-29-28

Cross Section 20' Alley in Minthrop Highlands
Bet. Chesnut and Hickory
From N. side Ampudia to S. side Aristo St

254.33

56

4.31 254.33

250.06

N.E. BP
Hickory
and Ampudia

N. side Ampudia = 0+00

N top cb. 6.01 48.32

Gut on pav 6.12 48.21

6.53 47.80

S Gut " 6.32 48.01

S top cb 6.15 48.18

0+05

S 6.0 48.3

6.0 48.3

+6 6.2 48.1

N 5.9 48.4

0+40 = East edge Con Apron to Garage on South

N 5.1 49.2

6 4.8 49.5

+9.85 = toe Con Apron 4.91 49.42

S +4' on Garage Floor 4.74 49.59

0+43 = S Garage on N 4.87 49.46

0+50 = West edge Con Apron to Garage on South

-4' = Garage Floor 4.87 49.46

-0.15' = toe Con Apron 5.04 49.29

6 5.3 49.0

N 5.2 49.1

0+70 = East edge Con Apron to Dble. Garage on South

N 6.3 48.0

4

6.1 48.2

S 5.8 48.5

+4.4 = toe Con Apron 5.62 48.71

+6.6 = Garage Floor 5.62 48.71

0+87 = West edge Con Apron on South

0+87 = East edge Con Apron 6.88 47.45

0+99 = " " " to Garage on North

-5' = Garage Floor 6.58 47.95

-0.8' = toe Con Apron 7.10 47.23

N 7.1 47.2

6 7.0 47.3

S 6.7 47.6

1+50

S 8.5 45.8

6 8.9 45.4

N 9.2 45.1

1+77 = S Dble. Garage on South Con Floor 20' wide

-5' 10.6 43.7

N 10.2 44.1

+4 9.8 44.5

6 9.8 44.5

S 9.0 45.3

+6.7 = Garage Floor 8.05 46.26

2+05 = S Garage on N 4' Back 10' wide

S 9.8 44.5

6 10.5 43.8

Apron = 0.8' Back
to Garage on N

Level across

Con Floor

P/O Head
12-29-28 76.H.

6' Back

Con Floor
4' Back 10' wide

254.33

N	10.5	43.8
+ 4' = Garage Floor	10.29	44.04

2+27

N	11.1	43.2
↳	11.0	43.3
+ 6	10.8	43.5
S	10.3	44.0

2+40

S	10.3	44.0
+ 2	11.3	43.0
↳	11.5	42.8
N	11.5	42.8

T.P.	2.00	244.17	1816	242.17
------	------	--------	------	--------

2+52 = End ridge Cobble Stone Wall on N 0.6' Back.

N - 0.6 on top 4	2.10	42.2
N	2.2	42.0
↳	2.4	41.8
+ 5	2.3	42.9
S	0.8	43.4

2+75

S	2.1	42.1
+ 5	5.0	39.2
↳	5.2	39.0
N	4.8	38.4
+ 0.6 = Base Wall on Ground	4.7	39.5
+ 1.0 = top "	3.0	46.2

244.17

2+87

- 1.0' = top Wall	3.7	40.5
- 0.6' = Bottom Wall on Ground	5.7	38.5
N	5.7	38.5
↳	6.7	37.5
+ 7	6.1	38.1
S	3.5	40.7
+ 2 = top Bank.	2.5	41.7

2+99

S	3.2	41.0
+ 1	7.7	36.5
↳	9.0	35.2
+ 8	8.4	35.8
N	7.5	36.7
+ 1' on top Wall	6.2	38.0

3+00 = S.L.T. line Arista St.

N top cb.	8.84	35.33
" Gut. on Pav.	8.92	35.25
↳ " "	9.15	35.02
S " " "	8.71	35.46
" top cb.	8.54	35.63

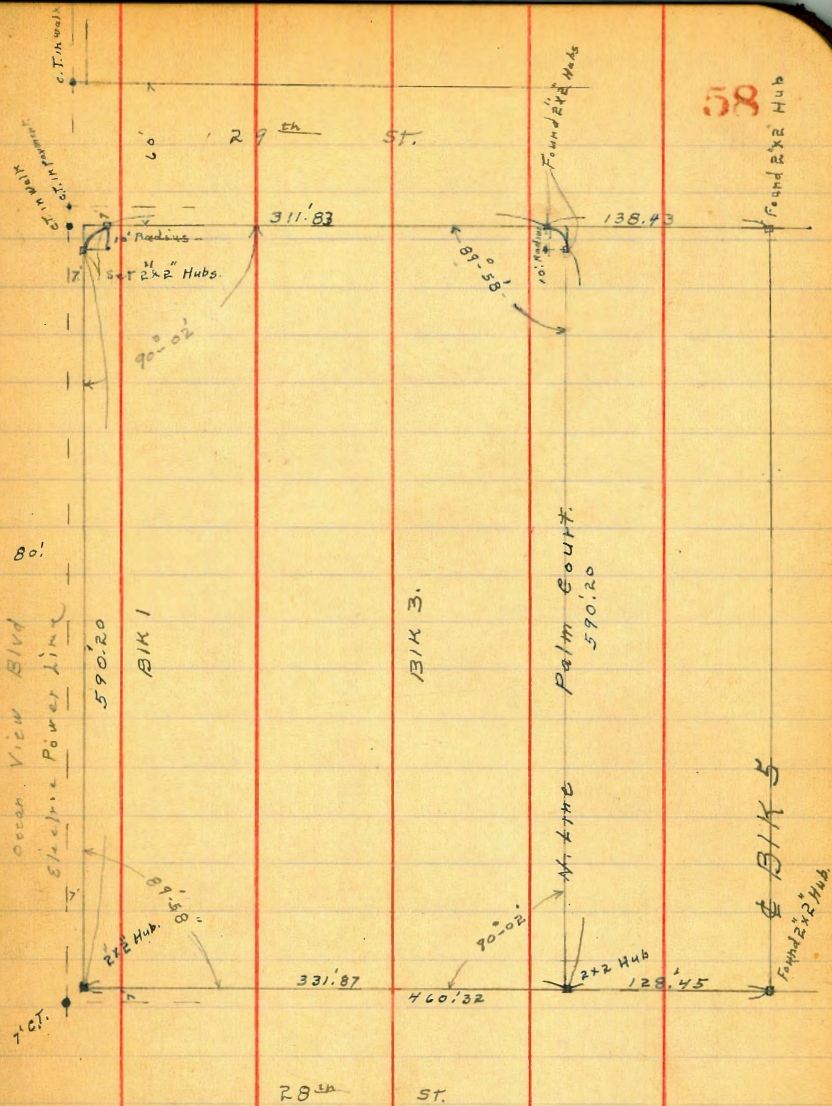
T.P.	11.88	254.05	2.00	242.17
------	-------	--------	------	--------

chk. on B.M. P-56	4.03	250.02
		250.02 = B.M.
		0.00

57

Survey & X See of
 BIKs. 1 & 3 LaBinda Park.
 For S.D. City School Board

1-7-29
 Miller



00.84 W = E. Line 28th St
 00.84 S = S. Line Ocean View Blvd
 X Sec BIKS 1+3
 LaBinda Park
 See Page 58.

1-7-29
 97.45

B.M.	5.97	97.02	91.05
	00.84 W = E. Line 28 th St		
4.5 N. of 00.84 S Edge emt. walk	6.82	90.20	
00.84 S = S. Line Ocean View Blvd	5.8	91.2	
50'S	6.8	90.2	
100'S	7.8	89.2	
150'S	8.8	88.2	
200'S	9.0	88.0	
250'S	9.8	87.2	
300'S	10.6	86.4	
331.87 S = S. Line BIK 3	10.8	86.2	
	50' E. of 28 th		
331.87 S	10.9	86.1	
300'S	11.4	85.6	
250'S	9.8	87.2	
200'S	9.2	87.8	
150'S	8.6	88.4	
100'S	7.4	89.6	
50'S	6.3	90.7	
S. Line Ocean View Blvd	5.1	91.9	
4.5 N. = S. edge emt. walk	5.7	91.3	
	100' E. of 28 th St.		
4.5 N = S edge emt walk	4.6	92.4	
S. Line Ocean View	4.0	93.0	
50'S	6.4	90.6	
100'S	7.1	89.9	

N.E. 28th St
 Ocean View Blvd

150'S	
200'S	
250'S	
300'S	
331.86 S = S. Line BIK 3	
	150' E. of 28 th St
331.86 S	
300'S	
250'S	
200'S	
150'S	
100'S	
50'S	
	00 = S. Line Ocean View
	4.5 N. = S. edge emt. walk
	200' E. of 28 th
	4.5 N. = edge walk
	00 = S. Line Ocean View
50'S	
100'S	
150'S	
200'S	
250'S	
300'S	
331.86 S = S. Line BIK 3	

97.02

8.6	88.4
9.1	87.9
9.6	87.4
10.8	86.2
11.4	85.6
10.6	86.4
9.7	87.3
9.1	87.9
8.7	88.3
8.4	88.6
7.3	89.7
4.9	92.1
3.0	94.0
3.4	93.6
2.3	94.7
1.7	95.3
3.8	93.2
6.3	90.7
7.4	89.6
7.8	89.2
8.8	88.2
9.6	87.4
10.1	86.9

59

97.02

250' E. of 28th St.

331.865 = S. Line BIK 3	10.2	86.8
300'S.	7.5	87.5
250'S	8.5	88.5
200'S	7.3	89.7
150'S	6.06	90.9
100'S	4.6	92.4
60'S	3.9	93.1
50'S	3.0	94.0
00 = S. Line Ocean View Blvd	0.8	96.2
4.5 N. = S. edge emt. walk	1.2	95.8
J.P. 4.14 100.82 0.38		96.64

300' E. of 28th St

4.5 N. = S. edge emt. walk	3.8	97.0
00 = S. Line Ocean View Blvd	3.3	97.5
50'S	5.2	95.6
100'S	8.5	92.3
150'S	9.4	91.4
200'S	10.8	90.0
250'S	12.0	88.8
300'S	13.2	87.6
331.855 = S. Line BIK 3.	13.4	87.4

350' E. of 28th St

331.855 = S. Line BIK 3.	13.4	87.4
300'S	12.6	88.0
250'S	11.7	89.1
200'S	10.4	90.4

100.82

150'S	9.1	91.7
100'S	7.3	93.5
50'S.	3.9	96.9
00 = S. Line Ocean View Blvd	1.6	99.2
4.5 N. = S. edge emt. walk	2.7	98.1
400' E. of 28 th St.		
4.5 N. = S. edge emt. walk	1.7	99.1
00 = S. Line Ocean View.	1.1	99.7
50'S	3.5	97.3
100'S.	4.06	93.7
150'S	7.8	93.0
200'S	9.7	91.1
250'S	11.3	89.5
300'S	12.8	88.0
331.855 = S. Line BIK 3.	13.5	87.3
450' E. of 28 th St		
331.855 = S. Line Lot 3	14.0	86.8
300'S	12.8	88.0
250'S	10.9	89.9
200'S	8.7	92.1
150'S	6.6	94.2
100'S	4.8	96.0
50'S	3.1	97.7
00 = S. Line Ocean View Blvd	1.7	99.1
4.5 N. = S. Edge emt. walk.	2.1	98.7

100.82
500 E. of 28th ST

4.5 N. = s. edge emb. walk	2.6	98.2
00 = S. line Ocean View Blvd	2.6	98.2
50's	4.4	96.4
100's	5.7	95.1
150's	6.9	93.9
200's	8.6	92.2
250's	11.2	89.6
300's	13.1	87.7
331.84 S = S. Line Blk 3.	14.3	86.5

550.8 of 28th ST.

331.84 S = S. Line Blk 3	15.0	85.8
300's	13.5	87.3
250's	11.2	89.6
200's	9.2	91.6
150's	7.5	93.3
100's	5.9	94.9
50's	4.1	96.7
00 = S. Line Ocean View Blvd	3.0	97.8
4.5 N. = edge walk	3.1	97.7

600.20 E. of 28th ST = N. Line 29th ST

4.5 N. = s. edge emb. walk	3.5	97.3
00 = S. Line Ocean View Blvd	3.3	97.5
50's	3.8	97.0
100's	5.8	95.0
150's	7.3	93.5
200's	9.4	91.4

100.82

250's	11.4	89.4
300's	13.1	87.7
331.83 S = S. Line Blk 3.	14.3	86.5
chk on B.M.	2.37	97.45 = 97.45

Electric Power Line S. Side Ocean View Blvd.

BKs. 19-3
La Binda Park

61

N. E. 29th St
Ocean View Blvd
97.45

60' wide
10' chs
10' 1/4's

X See Roadway of 38th St 2-21-29
Ocean View Blvd to National
miller

91.98

135.28 = N. line of Hwy on E.

62

See Page 51. - This Book for Curbs

B.M. Top Hydt 8.39 91.98 83.59

00 = S. line Ocean View Blvd

Page 51.

59.85

W. gutter	9.3	82.7
"	9.8	82.2
"	9.2	82.8
"	8.9	83.1
"	8.8	83.2
E. gutter	9.0	83.0

119.75 = N. line Teak on W.

E. gutter	6.7	85.3
"	6.2	85.8
"	6.2	85.8
"	6.4	85.6
W. gutter	7.0	85.0

129.75 = N. ch. Teak on W.

W. line in gutter	6.4	85.6
"	6.5	85.5
"	6.1	85.9
"	5.8	86.2
"	5.8	86.2
E. gutter	6.3	85.7

S.E. 38th
+ Ocean View

E. line dirt

ch. line gutter

"

"

"

W. ch.

W. line

W. line

ch

"

"

"

E. ch

E. line

ch

"

Top M.H.

"

W. ch.

W. line

ch

"

"

4.9

6.0

5.7

5.6

5.9

6.3

6.4

139.75 = N. "4

6.2

6.2

5.8

5.5

5.6

5.7

142.75 = E. Alley on E.

5.0

5.6

5.6

5.34

5.8

6.0

149.75 = E. Teak to W.

5.9

5.9

5.6

5.3

87.1

86.0

86.3

86.4

86.1

85.7

85.6

85.8

85.8

86.2

86.5

86.4

86.3

87.0

86.4

86.4

86.64

86.2

86.0

86.1

86.1

86.4

86.7

91.98
149.7 S (con)

E. 1/4	5.5	86.5
E. oblique gutter	5.5	86.5
150.2 S = S. Line Alley on E.		
E. line dirt	4.4	87.2
E. ob gutter	5.5	86.5
159.7 S = S. 1/4 Teak on W		
E. gutter	5.5	86.5
"	5.4	86.6
"	5.2	86.8
"	5.5	86.5
W ob	5.9	86.1
N. Line	5.8	86.2
169.7 S = S. ob. Teak on W.		
W Line gutter	5.5	86.5
ob	5.8	86.2
"	4.3	86.7
"	5.1	86.9
"	5.4	86.6
E gutter	5.5	86.5
179.7 S = S. Line Teak on W		
E. gutter	5.5	86.5
"	5.2	86.8
"	5.0	87.0
"	5.3	86.7
W. 1/4 gutter	5.9	86.1

91.98
230.5

W gutter	5.3	86.7
"	4.6	87.4
"	4.5	87.5
"	4.8	87.2
E. gutter	4.2	87.8
286.3 S = N. Line Teak on E		
E. gutter	4.5	87.5
"	4.2	87.8
"	4.0	88.0
"	4.1	87.9
W gutter	4.5	87.5
296.3 S = N. ob. Teak on E.		
N. gutter	4.3	87.7
"	3.9	88.1
"	3.8	88.2
"	4.1	87.9
E. ob	4.1	87.9
E. line gutter	4.3	87.7
306.7 S = N. Line Alley on W.		
W. gutter	4.4	87.6
W. Line Dirt.	3.0	89.0
306.6 S = N. 1/4 Teak on E		
E. line	4.1	87.9
ob	4.0	88.0
"	4.0	88.0
"	3.8	88.2

38th St.

3.93
66.05

63

40' wide
10' ob on N
41.4 Roadway

91.98

306.6 S. 204

W. 1/4	3.9	88.1
W. gutter	4.3	87.7

309.7 S = ϕ Alley on W.

W. line	3.2	88.8
W. gutter	4.1	87.9

317.0 S = ϕ Teak on E.

W. gutter	4.0	88.0
1/4	3.7	88.3
c	3.7	88.3
1/4	4.0	88.0
E. gutter	3.9	88.1
E. line	3.9	88.1

318.7 S = S. line Alley on W.

W. gutter	4.0	88.0
W. line dirt	2.9	89.1

327.3 S = S. 1/4 Teak on E.

E. Line	4.0	88.0
gutter	4.0	88.0
1/4	3.8	88.2
c	3.6	88.4
1/4	3.6	88.4
W. gutter	3.9	88.1

337.7 S = S. ϕ Teak on E.

W. gutter	3.7	88.3
1/4	3.5	88.5
c	3.5	88.5

91.98

38th St.

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1/4	3.7	88.3
gutter	4.0	88.0
E. line gutter	3.9	88.1

346.3 S = S. line Teak on E.

E. gutter	3.8	88.2
1/4	3.6	88.4
c	3.3	88.7
1/4	3.5	88.5
W. gutter	3.5	88.5

400.5

W. gutter	3.2	88.8
1/4	2.6	89.4
c	2.3	89.7
1/4	2.5	89.5
E. gutter	2.9	89.1

T.P. 7.39 97.81 1.56 90.42

443.5 S = N. Line S. St. on W.

40' width
10' edge
10' 11x6

E. gutter	7.7	90.1
1/4	7.4	90.4
c	7.5	90.3
1/4	7.8	90.0
W. gutter	8.4	89.4
emt. ch	7.87	89.74 = 89.73

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97.81
N. cl. Line S. St.

W. line gutter	8.1	89.7
W. cl	8.1	89.7
" ₁₄	7.6	90.2
c	7.2	90.6
" ₁₄	7.2	90.6
E. gutter	7.6	90.2
N. " ₁₄ of S. on W.		
E. gutter	7.4	90.4
" ₁₄	7.0	90.8
c	7.0	90.8
" ₁₄	7.4	90.4
W. cl	7.7	90.1
W. line	7.9	89.9
E S. on W.		
W. line	7.4	90.4
cl	7.5	90.3
" ₁₄	7.2	90.6
c	6.8	91.0
" ₁₄	6.8	91.0
E. gutter	7.1	90.7
S. " ₁₄ S. on W.		
E. gutter	6.9	90.9
" ₁₄	6.6	91.2
c	6.7	91.1
" ₁₄	7.0	90.8
cl	7.4	90.4

97.81

38^{LB} 5+

65

W. line	7.4	90.4
S. cl. S. on W.		
W. line gutter	7.0	90.8
cl	7.2	90.6
" ₁₄	6.7	91.1
c	6.4	91.4
" ₁₄	6.4	91.4
E. gutter	6.7	91.1
503.5 S. = S. line S. on W.		
E. gutter	6.4	91.4
" ₁₄	6.2	91.6
c	6.2	91.6
" ₁₄	6.7	91.1
W. gutter	7.2	90.6
545.5 = N. line "S" st. on E.		
W. gutter	6.5	91.3
" ₁₄	5.9	91.9
c	5.5	92.3
" ₁₄	5.4	92.4
E. gutter	5.2	92.6
555.5 = N. cl. "S" st. on E.		
E. line gutter part.	5.23	92.58
cl	5.1	92.7
" ₁₄	5.2	92.6
c	5.4	92.4
" ₁₄	5.9	91.9
W. gutter	6.4	91.4

97.81

562.5 S = N. 1/4 Sth on E

W. gutter	6.2	91.6
"	5.7	92.1
c	5.3	92.5
"	5.0	92.8
ch	4.9	92.9
		91.91
E. Line parvt.	5.90	92.91
570.5 S = S. on E		
E. Line Parvt	4.75	93.06 ✓
ch	4.8	93.0
"	4.9	92.9
c	5.1	92.7
"	5.6	92.2
W. gutter	6.1	91.7
577.5 S = S. 1/4		
N. gutter	6.1	91.7
"	5.4	92.4
c	4.9	92.9
"	5.0	92.8
ch	4.8	93.0
E. Line parvt.	4.70	93.11 ✓
585.5 S = S. ch.		
E. Line gutter parvt.	4.85	92.96
ch	4.8	93.0
"	4.8	93.0
c	4.9	92.9
"	5.4	92.4
W. gutter	6.0	91.8

97.81

38th ST.595.5 S = S. Line Sth on E.

W. gutter	5.7	92.1
"	5.2	92.6
c	4.7	93.1
"	4.6	93.2
E. gutter	4.6	93.2
628.5 S = N. Line Alley on W.		
E. gutter	4.5	93.3
"	4.3	93.5
c	4.3	93.5
"	4.7	93.1
W. gutter	5.0	92.8
W. Line Dirt	4.1	93.7
637.5 S = S. Alley on W.		
W. Line	4.3	93.5
W. gutter	5.0	92.8
346.5 S = S. Line Alley on W.		
W. Line dirt	4.1	93.7
W. gutter	4.7	93.1
"	4.4	93.4
c	4.0	93.8
"	4.2	93.6
E. gutter	4.2	93.6
655.5 S = Brk.		
E. gutter	4.1	93.7
"	4.0	93.8
c	3.8	94.0
"	4.1	93.7
W. gutter	4.6	93.2

66

97.81

675' S = Brk.

N. gutter	4.4	93.4
"	3.9	93.9
e	3.6	94.2
"	3.7	94.1
E. gutter	3.9	93.9

695' S = Brk

E. gutter	3.8	94.0
"	3.7	94.1
e	3.6	94.2
"	3.9	93.9
N. gutter	4.4	93.4

715' S = Brk

N. gutter	4.5	93.3
"	4.0	93.8
e	3.6	94.2
"	3.8	94.0
E. gutter	3.7	94.1

735' S = Brk

E. gutter	4.4	93.4
"	4.0	93.8
e	3.9	93.9
"	4.3	93.5
N. gutter	4.7	93.1

97.81

38th St.770' S = N. Line T^h St on W.

N. gutter	5.4	92.4
"	4.9	92.9
e	4.6	93.2
"	4.7	93.1
E. gutter	5.1	92.7

780' S = N. cl. T^h on W.

E. gutter	5.1	92.7
"	4.9	92.9
e	4.8	93.0
"	5.1	92.7
cl	5.3	92.5
N. line gutter	5.2	92.6

790' S = N. 44 T^h on W.

N. line	5.5	92.3
cl	5.3	92.5
"	5.3	92.5
e	4.9	92.9
"	5.0	92.8
E. gutter	5.2	92.6

795' S = N. Line T^h St on E.

E. gutter	5.2	92.6
"	5.1	92.7
e	5.0	92.8
"	5.3	92.5
cl	5.4	92.4
N. line	5.6	92.2

67

97.81

800' S = $\frac{1}{2}$ " T on W.

W. Line	5.7	921
cb	5.6	92.2
"y	5.4	92.4
c	5.1	92.7
"y	5.2	92.6
E. gutter	5.3	92.5

805' S = N. $\frac{1}{4}$ " T on E. Paved to E.

E. Line gutter Pavmt.	5.26	92.55
cb	5.3	92.5
"y	5.2	92.6
c	5.2	92.6
"y	5.5	92.3
cb	5.2	92.1
W. Line	5.8	92.0

810' S = S. $\frac{1}{4}$ " T on W.

W. Line	6.0	91.8
cb	5.9	91.9
"y	5.6	92.2
c	5.3	92.5
"y	5.3	92.5
cb	5.3	92.5
E. Line Pavmt.	5.27	92.54

812.5 S = N. $\frac{1}{4}$ " T on E

E. Line Pavmt.	5.29	92.52
cb	5.3	92.5
"y	5.3	92.5

97.81

38th

ST.

68

c	5.4	92.4
"y	5.6	92.2
cb	5.9	91.9
W. Line	6.1	91.7

820' S = $\frac{1}{2}$ " T on E.
5' cb of $\frac{1}{4}$ " T on W.

W. Line gutter	6.1	91.7
cb	5.9	91.9
"y	5.8	92.0
c	5.5	92.3
"y	5.6	92.2
cb	5.7	92.1
E. Line Pavmt.	5.58	92.23

827.5 S = S. $\frac{1}{4}$ " T on E.

E. Line Pavmt.	5.85	91.96
cb	5.8	92.0
"y	5.8	92.0
c	5.7	92.1
"y	6.0	91.8
W. gutter	6.1	91.7

830' S = S. $\frac{1}{4}$ " T on W.

W. emb. cb	5.73	92.08
W. gutter	6.2	91.6
"y	6.0	91.8
c	6.0	91.8
"y	6.0	91.8
cb	6.0	91.8
E. Pavmt.	5.96	91.85

97.81

T.P. BM ^{Top}
Hydt

0.08

96.29

1.20

96.21

se. 'S.' st

7 38th

835' S = S. ch. T on E

E. Line gutter parvit

4.78

91.51

ch

4.6

91.7

"4

4.4

91.9

e

4.5

91.8

"4

4.6

91.7

W. gutter

5.0

91.3

845' S = S. Line T on E.

W. gutter

5.3

91.0

"4

4.8

91.5

e

4.6

91.7

"4

4.7

91.6

E. gutter

4.9

91.4

9.00's

E. gutter

6.3

90.0

"4

6.0

90.3

e

6.1

90.2

"4

6.3

90.0

W. gutter

7.0

89.3

935' S = N. Line Alley on W.

N. Line Dirt

7.6

88.7

W. gutter

8.3

88.0

"4

7.7

88.6

e

7.5

88.8

"4

7.3

89.0

E. gutter

7.4

88.9

96.29.

38th ST.

964' S = Alley on W.

E. gutter

7.5

88.8

"4

7.5

88.8

e

7.7

88.6

"4

8.0

88.3

ch

8.5

87.8

W. Line

8.0

88.3

970' S = N. Line Alley on E.

W. Line

8.0

88.3

ch

8.6

87.7

"4

8.1

88.2

e

7.8

88.5

"4

7.6

88.7

E. gutter

7.5

88.8

E. Line dirt

7.2

89.1

973' S = S. Line Alley on W.

E. Line

7.3

89.0

ch

7.6

88.7

"4

7.7

88.6

e

7.9

88.4

"4

8.2

88.1

W. gutter

8.8

87.5

W. Line dirt

8.0

88.3

977' S = Alley on E.

W. gutter

7.0

87.3

"4

8.2

88.1

e

8.0

88.3

96.29
977.55 (con)

E. 1/4	7.8	88.5
E. gutter	7.6	88.7
E. line	7.3	89.0

985' S = S. line Alley on E.

E. line Dirt	7.4	88.9
E. gutter	8.1	88.2
"y	8.0	88.3
e	8.2	88.1
"y	8.5	87.8
W. gutter	9.3	87.0

1050' S

W. gutter	10.8	85.5
"y	10.2	86.1
e	9.6	86.7
"y	9.4	86.9
E. gutter	9.8	86.5

1098' S = N. line Florence on W.

E. gutter	10.8	85.5
"y	10.6	85.7
e	10.7	85.6
"y	11.2	85.1
W. gutter	11.7	84.6

1108' S = N. ch on W

W. line gutter	12.0	84.3
ch	11.6	84.7
"y	11.2	85.1

96.29

38th St

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e	11.0	85.3
"y	10.9	85.4
E. gutter	10.9	85.4

1111' S = N. line Florence on E

E. gutter	10.9	85.4
"y	11.0	85.3
e	11.1	85.2
"y	11.3	85.0
ch	11.4	84.5
W. line	12.0	84.3

1118' S = N. 1/4 on W.

W. line	11.8	84.5
ch	11.6	84.7
"y	11.4	84.9
e	11.2	85.1
"y	11.1	85.2
E. gutter	10.7	85.6

1121' S = N. ch on E

E. gutter	10.9	85.4
ch	10.8	85.5
"y	11.1	85.2
e	11.2	85.1
"y	11.3	85.0
ch	11.6	84.7
W	11.7	84.6

96.29
1128.5 = 2 on W

W	11.6	84.7
cl	11.5	84.8
14	11.3	85.0
c	11.1	85.2
14	10.9	85.4
cl	10.7	85.6
E	10.6	85.7
1131.5 = N. 14 on E		
E	10.5	85.8
cl	10.7	85.6
14	10.9	85.4
c	11.0	85.3
14	11.2	85.1
cl	11.4	84.9
W	11.6	84.7
1138.5 = S. 14 on W.		
W	11.7	84.6
cl	11.5	84.8
14	11.3	85.0
c	11.0	85.3
14	10.9	85.4
cl	10.6	85.7
E	10.3	86.0
1141.5 = 2 on E		
E	10.3	86.0
cl	10.7	85.6

38" 57

96.29

14	10.9	85.4
C	11.1	85.2
14	11.4	84.9
cl	11.7	84.6
W	11.8	84.5
1148.5 = S. cl on W.		
W. line gutter	12.1	84.2
cl	11.9	84.4
14	11.5	84.8
c	11.2	85.1
14	11.0	85.3
cl	10.8	85.5
E	10.6	85.7
1151.5 = S. 14 on E		
E	10.7	85.6
cl	10.9	85.4
14	11.0	85.3
C	11.2	85.1
14	11.6	84.7
W. gutter	12.0	84.3
1158.5 = S. line Florence on W		
W. gutter	12.0	84.3
14	11.6	84.7
C	11.1	85.2
14	11.1	85.2
cl	11.1	85.2
E	10.8	85.5

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96.29
1161'S = S. line on E

E. line gutter	10.9	85.4
ch	10.9	85.4
"y	11.1	85.2
c	11.1	85.2
"y	11.5	85.8
W. gutter	11.9	84.4

1171'S = S. line Florence on E.

W. gutter	11.7	84.6
"y	11.2	85.1
c	10.7	85.6
"y	10.8	85.5
E. gutter	10.9	85.4
T.P.	2.56	90.80
	8.05	88.24

1212.12 S

E. gutter	3.8	87.0
"y	3.7	87.1
c	3.5	87.3
"y	3.9	86.9
W. gutter	4.5	86.3

1253.3 S = Brk.

W. gutter	2.8	88.0
"y	2.3	88.5
c	2.0	88.8
"y	2.1	88.7
E. gutter	2.2	88.6

90.80
1273.3 S = Brk.

E. gutter	1.7	89.1
"y	1.5	89.3
c	1.4	89.4
"y	1.8	89.0
W. gutter	2.3	88.5

1283.5 S = N. line Alley on N.

W. line Dirt	1.6	89.2
gutter	2.1	88.7
"y	1.7	89.1
c	1.3	89.5
"y	1.3	89.5
E. gutter	1.5	89.3

1293.3 S = Brk.

E. gutter	1.2	89.6
"y	1.2	89.6
c	1.2	89.6
"y	1.7	89.1
W. gutter	2.0	88.8
W. line	1.6	89.2

1295.3 S = N. line Alley on E.

W. line	1.5	89.3
gutter	1.9	88.9
"y	1.7	89.1
c	1.2	89.6
"y	1.2	89.6
E. gutter	1.1	89.7
E. line dirt	0.8	90.3

90.80
1296.9' S = E Alley on W.

E. line	0.4	90.4
gutter	1.2	89.6
"	1.2	89.6
"	1.2	89.6
"	1.8	89.0
gutter	1.8	89.0
W. line	1.5	89.3

1302.8 = E Alley E

W. line Dirt	1.7	89.1
W. gutter	1.8	89.0
"	1.7	89.1
"	1.2	89.6
"	1.3	89.5
E. gutter	1.1	89.7
E. line dirt.	0.1	89.7

1310.3 S = S. line Alley on E & W

E. line dirt	0.3	90.5
gutter	1.2	89.6
"	1.4	89.4
"	1.5	89.3
"	1.9	88.9
gutter	2.2	88.6
W. line dirt	1.7	89.1

1313.3 S = Brk

W. gutter	2.3	88.5
"	2.0	88.8

90.80

38th St.

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"	1.5	89.3
"	1.8	89.3
E. gutter	1.5	89.3
E. gutter	2.3	88.5
"	2.2	88.6
"	2.1	88.7
"	2.8	88.3
W. gutter	2.9	87.9

1333.3 S = Brk

1383.3 S

W. gutter	5.1	85.7
"	4.5	86.3
"	3.9	86.9
"	4.0	86.8
E. gutter	4.0	86.8

14430.85
1433.36 = N. Line Logan Ave

80' 0" dia
14' dia
13' 4.5

E. gutter	6.2	84.6
"	6.1	84.7
"	6.2	84.6
"	6.5	84.3
W. gutter	7.2	83.6

N. cb.

W. line gutter	7.8	83.0
"	7.3	83.5
"	6.9	83.9
"	6.5	84.3

90.80
N. ch Logan (con)

E. 1/4	6.3	84.5
ch	6.1	84.7
E. line gutter	6.3	84.5
N. 1/4		
e	6.1	84.7
ch	6.5	84.3
1/4	6.6	84.2
e	6.8	84.0
1/4	7.1	83.7
ch	7.5	83.3
W	7.6	83.2
E		
W	7.7	83.1
ch	7.5	83.3
1/4	7.3	83.5
e	7.0	83.8
1/4	6.9	83.9
ch	6.6	84.2
E	6.3	84.5
S. 1/4		
E	6.6	84.2
ch	6.9	83.9
1/4	7.1	83.7
e	7.2	83.6
1/4	7.4	83.4
ch	7.7	83.1
W	8.1	82.7

90.80
S. ch

38th St.

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W gutter	8.6	82.2
ch	8.0	82.8
1/4	7.7	83.1
e	7.4	83.4
1/4	7.3	83.5
ch	7.3	83.5
E gutter	7.1	83.7
09 = S. line Logan Ave		
E gutter	7.8	83.0
1/4	7.6	83.2
e	7.6	83.2
1/4	7.8	83.0
W gutter	8.5	82.3
50'.S		
W gutter	9.5	81.3
1/4	8.9	81.9
e	8.5	82.3
1/4	8.4	82.4
E gutter	8.7	82.1
T.B	1.89	84.21
100'.S.		
E gutter	3.1	81.1
1/4	2.8	81.4
e	2.9	81.3
1/4	3.4	80.8
W gutter	4.1	80.1

84.21
142' S = N. Line Alley

w. line dirt	4.4	79.8
gutter	4.4	79.8
"	4.3	79.9
"	3.8	80.5
"	3.7	80.5
gutter	3.7	80.5
E. Line dirt	3.2	81.0
150' S = Alley		
E. Line	3.3	80.9
gutter	3.8	80.4
"	3.8	80.4
"	3.93	80.28
"	4.3	79.9
gutter	4.6	79.6
W. Line	4.8	79.4
158' S = S. Line Alley		
W. Line dirt	4.8	79.4
gutter	5.5	78.7
"	4.6	79.6
"	4.1	80.1
"	4.1	80.1
gutter	4.6	79.6
E. Line dirt	3.5	80.7

Top M.H.

84.21
200' S

E. gutter	5.5	78.7
"	5.1	79.1
"	5.1	79.1
"	5.6	78.6
W. gutter	6.4	77.8
250' S		
W. gutter	7.1	77.1
"	6.6	77.6
"	6.2	78.0
"	6.2	78.0
E. gutter	6.5	77.7
300' S = N. Line National Ave.		
E. gutter part	7.31	76.90
"	7.19	77.02
"	7.24	76.97
"	7.50	76.71
W. gutter	8.00	76.24
chk on BN	7.64	76.57

38th St.

75

58.38th
Nat.

Pearl St. and Herschel Ave.
Cross Section

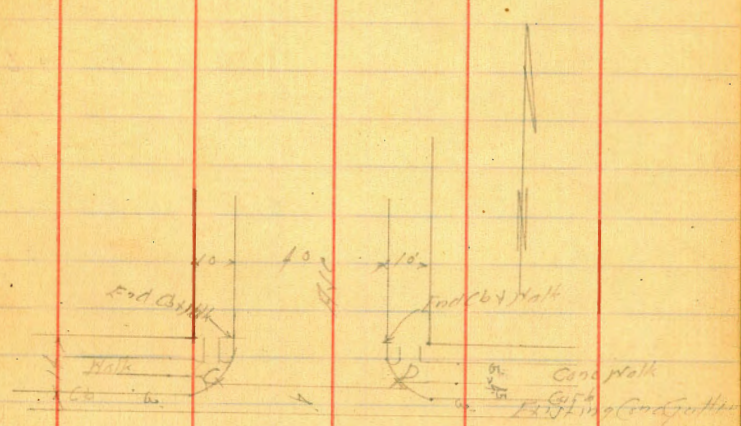
Pearl 8' wide
11' Cb
15' Qtz

Herschel 6' wide
10' Cb
18' Qtz

7-17-89
Sutton
Raphan
North 500
76

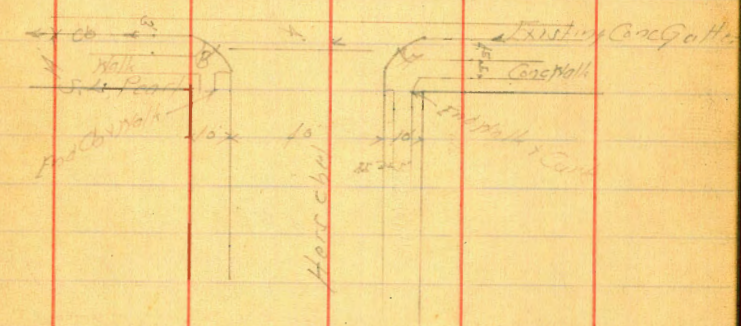
Station	Distance	Station	Distance	Notes
BM	3.58	118.63	115.05	SFBP Pearl + Girard
				S.L. Pearl
N			116.2	
N Cb Top			115.96	
Gutter			115.43	
+1			116.1	
1/2			116.0	
2			116.0	
1/4			116.3	
Gutter			116.3	
E Cb Top			116.99	
F			117.4 ?	
				S.Cb of Pearl
F Top Cb			116.85	
Gutter			115.93	
H Top Cb = 2' Below S.E. Cor			117.00	
Cb on Existing Gutter			115.99	
1/4 "			115.78	
2 "			115.57	
1/4 "			115.35	
Cb "			115.04	
N "			114.86	
Top Cb			115.77	
B Top Cb = 2' S.W. of Corner			115.88	

S.W. of S.Cb - NE Edge Existing Gutter



Pearl

St.



Herschel

11863

N	on Edge Existing Gutter	3.41	115 22
cb	"	3.30	115 33
1/4	"	3.20	115 43
1/2	"	3.00	115 63
1/4	"	2.81	115 82
cb	"	2.63	116 00
E	"	2.50	116 13
	5 1/2 of Pearl		
F	"	2.1	116 5
cb	"	2.4	116 2
1/4	"	2.6	116 0
1/2	"	2.8	115 8
1/4	"	2.9	115 7
cb	"	3.0	115 6
N	"	3.1	115 5
	1/2 Pearl		
N	"	3.1	115 5
cb	"	2.9	115 7
1/4	"	2.9	115 7
1/2	"	2.7	115 9
1/4	"	2.5	116 1
cb	"	2.3	116 3
E	"	2.0	116 6
	1 1/4 of Pearl		
E	"	2.5	116 1

11863

77

cb		2.8	115 8
1/4		3.0	115 6
1/2		3.2	115 4
1/4		3.3	115 3
cb		3.4	115 2
N		3.6	115 0
	10' of N 1/4 = 5 Edge Existing Gutter		
N	on Edge Existing Gutter	4.36	114 27
cb	"	4.20	114 43
1/4	"	4.03	114 60
1/2	"	3.85	114 78
1/4	"	3.68	114 95
cb	"	3.55	115 08
E	"	3.38	115 25
	1/2 Cb of Pearl		
E Gutter		3.63	115 00
E Top Cb		2.66	115 97
D-Top Cb & N E Return		2.60	116 03
cb	on Existing Gutter	3.64	114 99
1/4	"	3.55	114 78
1/2	"	4.06	114 57
1/4	"	4.30	114 33
cb	"	4.50	114 13
N	"	4.67	113 96
N Top Cb		3.73	114 90
C-Top Cb & N E Return		3.74	114 89

11863

Hk of Pool

N	37	114.9
Cb Top	37.6	114.87
Gutter	34.9	115.2 P
1/4	37	114.9
2	38	114.8
1/4	35	115.1
Gutter	31	115.5
Cb Top	26.1	116.02
L	22	116.4

78

117± cb d walk
 W side WINONA No. 21018
 S. of EL Cañon Ave

BMBP	6.80	358.33		351.53
T.P.	9.40	366.01	172	356.61
T.P.	10.27	376.05	023	365.78
T.P.	17.0	373.05	420	371.85 = cb-010
6100	56 EL Cañon			371.87

+10 Break
 371.80
 1.25
 1.69
 F 0.44

+20 Break
 371.30
 1.75
 2.34
 F 0.59

+60
 369.06
 3.99
 4.54
 F 0.53

+100
 366.82
 6.23
 6.87
 F 0.64

+118 end Tab
 365.81
 7.24
 7.89
 F 0.65

Moore
 Begg
 SHEPHERD
 STISSON 363.52
 4.50
 368.02
 4.50
 363.22
 368.22
 4.90
 363.12

PC = 250
 +10 = 5.45
 +20 = 3.52
 363.14
 4.5
 362.96
 7
 362.63

79

DIRECTIONS FOR USE OF TABLES

16.2 ✓
8.0 ✓
24.6 ✓
16.2 ✓
24.6 X

TABLE No. 1

Distance of slope stake from side or shoulder stake for any roadway, slope 1% to 1. If ground is nearly level the cut or fill at side stake is located by the double entry method in left column and top row. The number in body

of table in same row and column gives distance from side stake to slope stake. If ground is not

IMPROVED TABLES AND INFORMATION

TABLE No. 2

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given L may be found by dividing tangent (or external) opposite L by given tangent (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

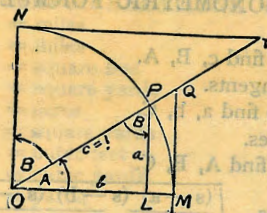


TABLE II
TRIGONOMETRIC FORMULÆ.

$$\angle A = \angle MOP \quad \angle B = \angle PON = \angle OPL$$

$$R = OB = c = 1$$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

$$\sin \frac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \quad \cos \frac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \quad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Sines} \quad \frac{\sin A}{a} = \frac{\sin B}{b} = \frac{\sin C}{c}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$$

31416
12566x
6283.2
753984
31416

TABLE X.
MIDDLE ORDINATES OF RAILS
Length of Rail (feet)

C	R	30	28	26	24	22	20	C	R	30	28	26	24	22	20
o /	Feet	Inch	Inch	Inch	Inch	Inch	Inch	o	Feet	Inch	Inch	Inch	Inch	Inch	Inch
0-20	17189	.08	.07	.06	.05	.04	.03	8	716.8	1.88	1.64	1.42	1.20	1.01	.84
0-40	8594	.16	.14	.12	.10	.08	.07	9	637.3	2.12	1.84	1.60	1.35	1.14	.94
1-0	5730	.24	.20	.18	.15	.13	.10	10	573.7	2.36	2.05	1.78	1.50	1.27	1.04
1-20	4297	.31	.27	.23	.20	.17	.13	11	521.7	2.59	2.26	1.95	1.65	1.39	1.15
1-40	3438	.39	.34	.29	.25	.21	.17	12	478.3	3.83	3.47	3.15	2.81	2.54	2.26
2-0	2865	.47	.41	.35	.30	.25	.20	13	441.7	3.05	2.66	2.30	1.96	1.66	1.36
2-20	2456	.55	.48	.41	.35	.29	.23	14	410.3	3.30	2.87	2.48	2.10	1.78	1.46
2-40	2149	.63	.55	.47	.40	.33	.27	15	383.1	3.54	3.08	2.68	2.26	1.91	1.57
3-0	1910	.71	.62	.53	.45	.38	.31	16	359.3	3.76	3.28	2.83	2.40	2.04	1.67
3-20	1719	.78	.68	.59	.50	.42	.35	17	338.3	4.00	3.48	3.02	2.57	2.16	1.78
3-40	1563	.86	.75	.65	.55	.46	.38	18	319.6	4.21	3.67	3.18	2.70	2.28	1.87
4-0	1433	.94	.82	.71	.60	.50	.42	19	302.9	4.45	3.89	3.36	2.86	2.41	1.98
4-20	1323	1.02	.89	.77	.65	.55	.45	20	287.9	4.70	4.09	3.55	3.00	2.54	2.09
4-40	1228	1.10	.96	.83	.70	.59	.48	22	262.0	5.16	4.44	3.84	3.30	2.80	2.29
5	1146	1.18	1.03	.89	.75	.63	.52	24	240.5	5.64	4.92	4.20	3.59	3.04	2.50
6	955.3	1.41	1.23	1.06	.90	.76	.62	26	222.3	6.07	5.29	4.58	3.88	3.29	2.70
7	819.0	1.65	1.44	1.24	1.05	.89	.73								

TABLE XI.
SHORT RADIUS CURVES

Radius Feet	Chord Feet	Central Angle	Deflection Angle	Deflection for 1 Foot
35	10	16-26	8-13	49.3
45	10	12-46	6-23	38.3
50	15	17-16	8-38	34.5
60	15	14-22	7-11	28.8
75	15	11-30	5-45	23.0
100	20	11-30	5-45	17.3
120	20	9-34	4-47	14.3
150	20	7-39	3-49	11.5
190	25	7-32	3-46	9.15
200	25	7-10	3-35	8.6
225	25	6-25	3-12	7.7
240	25	5-58	2-59	7.2
250	25	5-44	2-52	6.9
275	25	5-12	2-36	6.2
288	50	9-58	4-59	6.0
300	50	9-32	4-46	5.7
350	50	8-12	4-06	4.9
376	50	7-40	3-50	4.6
400	50	7-10	3-35	4.3
410	50	7-00	3-30	4.2

To find length of curve divide angle from P. C. to P. T. by central angle of chord and multiply by length of chord.

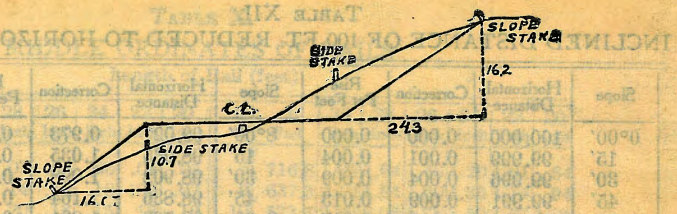
TABLE XII.
INCLINED DISTANCE OF 100 FT. REDUCED TO HORIZONTAL

Slope	Horizontal Distance	Correction	Rise Per Foot	Slope	Horizontal Distance	Correction	Rise Per Foot
0°00'	100.000	0.000	0.000	8°00'	99.027	0.973	0.139
15'	99.999	0.001	0.004	15'	98.965	1.035	0.143
30'	99.996	0.004	0.009	30'	98.902	1.098	0.148
45'	99.991	0.009	0.013	45'	98.836	1.164	0.152
1 00	99.985	0.015	0.017	9 00	98.769	1.231	0.156
15	99.976	0.024	0.022	15	98.700	1.300	0.161
30	99.966	0.034	0.026	30	98.629	1.371	0.165
45	99.953	0.047	0.031	45	98.556	1.444	0.169
2 00	99.939	0.061	0.035	10 00	98.481	1.519	0.174
15	99.923	0.077	0.039	15	98.404	1.596	0.178
30	99.905	0.095	0.044	30	98.325	1.675	0.182
45	99.885	0.115	0.048	45	98.245	1.755	0.187
3 00	99.863	0.137	0.052	11 00	98.163	1.837	0.191
15	99.839	0.161	0.057	15	98.079	1.921	0.195
30	99.813	0.187	0.061	30	97.992	2.008	0.199
45	99.786	0.214	0.065	45	97.905	2.095	0.204
4 00	99.756	0.244	0.070	12 00	97.815	2.185	0.208
15	99.725	0.275	0.074	15	97.723	2.277	0.212
30	99.692	0.308	0.078	30	97.630	2.370	0.216
45	99.657	0.343	0.083	45	97.534	2.466	0.221
5 00	99.619	0.381	0.087	13 00	97.437	2.563	0.225
15	99.580	0.420	0.092	15	97.338	2.663	0.229
30	99.540	0.460	0.096	30	97.237	2.763	0.233
45	99.497	0.503	0.100	45	97.134	2.866	0.238
6 00	99.452	0.548	0.105	14 00	97.030	2.970	0.242
15	99.406	0.594	0.109	15	96.923	3.077	0.246
30	99.357	0.643	0.113	30	96.815	3.185	0.250
45	99.307	0.693	0.118	45	96.705	3.295	0.255
7 00	99.255	0.745	0.122	15 00	96.593	3.407	0.259
15	99.200	0.800	0.126	15	96.479	3.521	0.263
30	99.144	0.856	0.131	30	96.363	3.637	0.267
45	99.087	0.913	0.135	45	96.246	3.754	0.271

TABLE XIII.
MINUTES IN DECIMALS OF A DEGREE.

0 30"	.00833	10 30"	.17500	20 30"	.34167	30 10"	.50833	40 30"	.67500	50 10"	.84167
1 00	.01667	11 00	.18333	21 00	.35000	31 00	.51667	41 00	.68333	51 00	.85000
30	.02500	30	.19167	30	.35833	30	.52500	30	.69167	30	.85833
2 00	.03333	12 00	.20000	22 00	.36667	32 00	.53333	42 00	.70000	52 00	.86667
30	.04167	30	.20833	30	.37500	30	.54167	30	.70833	30	.87500
3 00	.05000	13 00	.21667	23 00	.38333	33 00	.55000	43 00	.71667	53 00	.88333
30	.05833	30	.22500	30	.39167	30	.55833	30	.72500	30	.89167
4 00	.06667	14 00	.23333	24 00	.40000	34 00	.56667	44 00	.73333	54 00	.90000
30	.07500	30	.24167	30	.40833	30	.57500	30	.74167	30	.90833
5 00	.08333	15 00	.25000	25 00	.41667	35 00	.58333	45 00	.75000	55 00	.91667
30	.09167	30	.25833	30	.42500	30	.59167	30	.75833	30	.92500
6 00	.10000	16 00	.26667	26 00	.43333	36 00	.60000	46 00	.76667	56 00	.93333
30	.10833	30	.27500	30	.44167	30	.60833	30	.77500	30	.94167
7 00	.11667	17 00	.28333	27 00	.45000	37 00	.61667	47 00	.78333	57 00	.95000
30	.12500	30	.29167	30	.45833	30	.62500	30	.79167	30	.95833
8 00	.13333	18 00	.30000	28 00	.46667	38 00	.63333	48 00	.80000	58 00	.96667
30	.14167	30	.30833	30	.47500	30	.64167	30	.80833	30	.97500
9 00	.15000	19 00	.31667	29 00	.48333	39 00	.65000	49 00	.81667	59 00	.98333
30	.15833	30	.32500	30	.49167	30	.65833	30	.82500	30	.99167
10 00	.16667	20 00	.33333	30 00	.50000	40 00	.66667	50 00	.83333	60 00	1.00000

C
0-1
0-20
0-40
1-0
1-20
1-40
2-0
2-20
2-40
3-0
3-20
3-40
4-0
4-20
4-40
5
6
7



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

E 0.30 Back
W 0.8 "
21416x
30
9x5x8 0
235

$$60 = \frac{48}{x}$$

$$\frac{105}{48} = x$$

$$2.1875 = x$$

6+57.96
det. on All the same from Elected to
Proposed

485
18
467

ENGINEERING DEPARTMENT,
SAN DIEGO,
CITY OF CALIFORNIA.

410 Me.
24 03 12