

1287

1947

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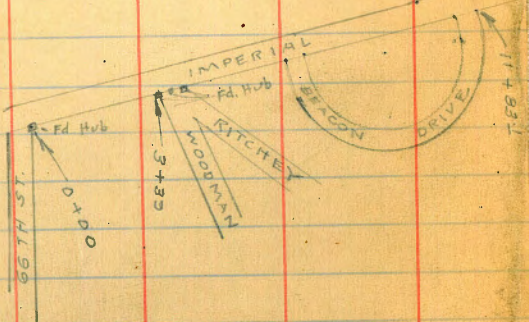
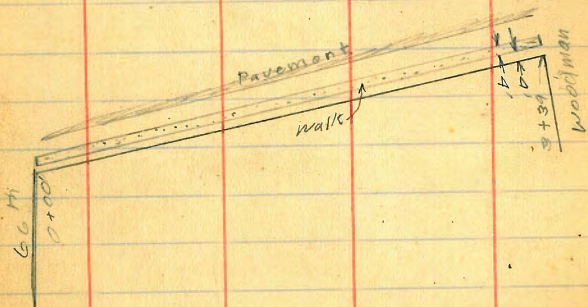
DEC 42 1964

No. 385 1/11/20

No. 1000 1/11/10

X See Imperial 66th to Cityline

1-62



Shir. Palo
Not track
w. 66th

X sec. Imperial from EL
66th on south to City line
60' 5" 10' obs 40' runway.

Oct 14-28
London

BM 12.05 232.61 220.56

0+25 232.61

0+00 = EL 66th on South

SL	7.0	225.6
+4 walk.	7.97	224.64
+8 walk	8.04	224.57
cb	7.3	225.30
+3	7.4	225.20
+4	8.6	224.0
+7	10.0	222.6
1/4	9.9	222.7
+2 s Pav	9.64	222.97
± +1 ± Pav	9.50	223.11
1/4 N. Pav.	9.63	222.98
+4	9.8	222.80
+6	9.0	223.6
cb	9.4	223.2
+5	10.1	223.5
NL	11.6	221.0
5' N	11.8	220.8
10' N	13.2	219.4

10' N	10.3	222.3
5' N	10.7	221.9
NL	10.5	222.1
+6	10.1	222.5
cb	8.7	223.9
+4	8.9	223.7
+5	9.4	223.2
1/4 N. Pav	9.14	223.47
+9 ± Pav	9.02	223.59
+8 s Pav	9.13	223.48
1/4	9.3	223.3
+4	9.5	223.1
+6	8.8	223.8
+7	7.5	225.1
cb	7.5	225.1
+2 walk	7.57	225.04
+6 ✓	7.45	225.16
+9	7.1	225.5
SL	6.7	225.9
0+50		
S.L.	6.0	226.6
+1	6.7	225.9
+4	6.95	225.66
+8	7.04	225.57
cb	6.8	225.8

0+50		232.61	
+3		6.8	225.8
+5		8.5	224.1
+7		9.1	223.5
1/4		9.0	223.6
+2	S. Pav	8.60	224.01
±+1	± Pav	8.52	224.09
1/4	N. Pav	8.58	224.03
+4		8.9	223.7
+7		8.4	224.2
+9		8.5	224.1
cb		8.9	223.7
+3		9.7	222.9
N.L.		10.5	222.1
10'N		10.9	221.7
0+75			
10N		10.6	222.0
N.L.		9.6	223.0
+4		9.0	223.6
+8		8.7	223.9
cb		8.2	224.4
1/4	N. Pav	8.03	224.58
+9	± Pav	7.98	224.63
±+8		8.08	224.54
1/4		8.2	224.4
+4		8.6	224.0

0+75		232.61	
+6		7.0	225.6
+8		6.4	226.2
cb		6.7	225.9
+2	walk	6.55	226.06
+6	✓	6.44	226.17
+9		6.4	226.2
S.L.		5.5	227.1
1+00			
S.L.		5.6	227.0
+2		6.2	227.4
+4	walk	5.99	226.82
+8	✓	6.10	226.50
cb		6.3	226.30
+3		6.1	226.50
+5		6.6	226.00
+8		8.4	224.20
1/4		7.9	224.7
+2	S. Pav	7.53	225.08
±+1	± Pav	7.46	225.15
1/4	N. Pav	7.57	225.04
cb		7.9	224.7
N.L.		8.7	223.9
10N		9.3	223.3

1425 232.61

10X	8.5	224.1
N.L.	7.9	224.7
cb	7.2	225.4
1/4 N Pav	7.00	225.61
+9 & Pav	6.92	225.69
& +8 S Pav	7.03	225.58
1/4	7.6	225.0
+2	7.9	224.7
+8	5.1	227.5
cb	5.3	227.3
+2 walk	5.52	227.09
+6 ✓	5.40	227.21
S.L.	5.2	227.4
1450		
S.L.	4.0	228.6
+2	4.9	227.7
+4 walk	4.93	227.68
+8 ✓	4.98	227.63
cb	4.8	227.8
+2	4.6	228.0
+4	5.2	227.4
+8	7.5	225.1
1/4	6.9	225.1
+2 S Pav	6.45	226.16
& +1 & Pav	6.35	226.26

1450 232.61

1/4 N Pav	6.45	226.16
+7	7.0	225.6
cb	7.1	225.5
N.L.	7.5	225.1
10N	8.1	224.5
1475		
10N	7.7	224.9
N.L.	7.2	225.4
+3	7.1	225.5
+9	6.3	226.3
cb	6.3	226.3
+3	6.0	226.6
+5	6.8	225.8
1/4 N Pav	5.93	226.68
+9 & Pav	5.50	226.81
& +8 S Pav	5.92	226.69
1/4	6.4	226.2
+2	7.0	225.6
+6	4.5	228.1
cb	4.4	228.2
+2 walk	4.45	228.16
+6 ✓	4.36	228.15
+7	4.0	228.6
S.L.	3.4	229.2

Imperial.

2+00		232.61	
SL		1.5	231
+2		3.4	229.2
+4	walk	3.80	228.91
+8	✓	3.87	228.74
cb		3.9	228.7
+3		3.9	228.7
+7		6.2	226.4
'A		5.9	226.7
+2	s Pav.	5.38	227.23
¢+1	¢ Pav	5.21	227.40
'A	N Pav	5.37	227.24
+5		5.9	226.7
+7		5.3	227.3
cb		5.3	227.3
+7		5.9	226.7
NL		6.6	226.0
10N		7.0	225.6
2+25			
10N		6.0	226.6
NL		4.9	227.7
+2		4.8	227.8
+6		5.4	227.2
cb		5.0	227.6
+3		4.9	227.7
+5		5.5	227.1

Imperial

2+25		232.61	
'A	N Pav	4.92	227.69
+9	¢ Pav	4.75	227.86
¢+8	s Pav	4.90	227.71
'A		5.5	227.1
+2		6.0	226.6
+5		4.9	227.7
+7		3.4	229.2
cb		3.2	229.4
+2	walk	3.46	229.15
+6	✓	3.30	229.31
SL		0.7	231.9
2+50			
SL		0.4	232.2
+3		2.9	229.7
+4	walk	3.10	229.51
+8	✓	3.21	229.40
cb		3.0	229.6
+4		3.0	229.6
+7		5.3	227.3
+8		5.5	227.1
'A		5.1	227.5
+2	s Pav	4.52	228.09
¢+1	¢ Pav	4.38	228.23
'A	N Pav	4.53	228.08
+4		5.2	227.4

5

Imbergal

2450	232.61		
+7		4.3	228.3
cb		3.8	228.8
N.L.		4.9	227.7
10N		5.1	227.5
2475			
10N		4.2	228.4
N.L.		4.3	228.3
+5		4.0	228.6
cb		4.1	228.5
+2		4.0	228.6
+5		4.7	227.9
1/4 N Pav		4.26	228.55
+9 ϕ Pav		4.14	228.47
ϕ +8 S Pav		4.28	228.33
1/4		4.6	228.0
+2		5.0	227.6
+6		2.9	229.7
cb		3.0	229.6
+2 walk		2.95	229.66
+6 \checkmark		2.89	229.72
S.L.		2.6	230.0

Imbergal

6

3400	232.61		
S.L.		2.3	230.3
+4 walk		2.61	230.00
+8 \checkmark		2.67	229.92
cb		3.1	229.5
+7		4.5	228.1
1/4		4.3	228.3
+2 S Pav		4.11	228.50
ϕ +1 ϕ Pav		3.78	228.63
1/4 \checkmark		4.06	228.55
+4		4.4	228.2
+6		3.9	228.7
cb		4.0	228.6
+3		3.9	228.7
+5		2.1	229.5
N.L.		3.2	228.4
10N		3.7	228.9
3+39 = W.L. Woodman			
10N		3.2	229.4
N.L.		2.8	228.8
+6		2.6	230.0
cb		2.7	229.9
+3		3.6	229.0
1/4 N Pav.		3.92	228.69
+9 ϕ Pav		3.84	228.74
ϕ +8 S Pav		3.92	228.69
1/4		3.8	228.8

Impairal

3+39 232.61
 +3 3.8 228.8
 +7 2.2 230.4
 cb 2.1 230.5
 +4 walk 2.17 230.44
 +6 2.27 230.44
 SL 1.6 231.0

3+50

S.L. 1.5 231.1
 cb 2.0 230.6
 +3 3.4 229.2
 +6 3.7 228.9
 1/4 3.7 228.9
 +2 S.Pav 3.88 228.73
 1/4 +1 1/4 Pav 3.88 228.73
 1/4 3.86 228.75
 +7 3.5 229.1
 cb 3.5 229.1
 +4 2.4 230.2
 N.L. 2.7 229.9
 10N 2.8 229.6

T.P. 3.08 234.16 1.53 231.02
 P.O. 20167 B.M. 3.09 231.02 231.03

Impairal

7

3+55 234.16
 10N 4.2 230.0
 N.L. 4.3 229.9
 +6 4.0 230.2
 cb 5.0 229.2
 +3 5.0 229.2
 1/4 N Pav 5.42 228.74
 +9 1/4 Pav 5.36 228.80
 1/4 +8 S Pav 5.42 228.74

1/4 5.2 229.0
 +4 5.0 229.2
 +6 5.1 229.1
 cb 4.9 229.3
 +5 3.9 230.3
 SL 3.3 230.9

3+60

S.L. 4.1 230.1
 +5 4.6 229.6
 cb 4.7 229.5
 +4 5.0 229.2
 +8 5.0 229.2
 1/4 5.1 229.1
 +2 S.Pav 5.39 228.77
 1/4 +1 1/4 Pav 5.34 228.82
 1/4 N Pav 5.39 228.77
 +4 5.4 228.8
 +6 5.2 229.0

3+60

234.16

cb	4.9	229.3
+5	3.6	230.6
N.L.	3.9	230.3
5N	3.7	230.5
10N	4.2	230.0
3+75		
10N	3.7	230.5
7N	3.4	230.8
N.L.	4.5	229.7
+3	3.7	230.5
+6	3.3	230.9
cb	4.4	229.8
+2	5.1	229.1
+5	5.5	228.7
1A N Pav	5.33	228.83
+9 E Pav	5.26	228.90
E+8 S Pav	5.34	228.82
1A	5.2	229.0
cb	4.4	229.8
S.L.	3.6	230.6

3+80

234.16

SL	4.1	230.1
+5	4.4	229.8
+8	4.4	229.8
cb	4.6	229.6
1A	5.0	229.2
+2 S Pav	5.27	228.89
E+1 E Pav	5.21	228.95
1A	5.31	228.85
+5	5.7	228.5
+6	5.3	228.9
cb	4.7	229.5
N.L.	4.5	229.7
4N	4.7	229.5
7N	3.8	230.4
10N	4.0	230.2
3+90		
10N	4.4	229.8
5N	4.7	229.5
N.L.	4.7	229.5
+7	4.5	229.7
cb	4.9	229.3
+4	5.4	228.8
+5	5.8	228.4
1A N Pav	5.28	228.88
+9 E Pav	5.20	228.96

8

3+90	234.16		
±+8 S Pav	5.26	228.90	
'A	5.0	229.2	
+4	5.0	229.2	
cb	4.7	229.5	
+6	4.0	230.2	
S.L.	1.2	233.0	
4+00			
S.L.	0.7	233.5	
+9	1.1	233.1	
cb	1.7	232.5	
+3	4.7	229.5	
'A	5.0	229.2	
+2 S Pav	5.19	228.97	
±+1 ± Pav	5.13	229.03	
'A N.Pav	5.21	228.95	
+4	5.6	229.6	
+5	5.3	228.9	
+8	4.5	229.7	
cb	4.4	229.8	
N.L.	4.7	229.5	
10N	5.2	229.0	

234.16

OK.
4+12 ²⁵ = E.L. Woodman.

10N	6.8	227.4
N.L.	5.5	228.7
+8	4.2	230.0
cb	4.7	229.5
+2	5.7	228.5
+4	4.8	229.4
cb+98 N Pav	5.18	228.98
'A+88 ± Pav	5.09	229.07
±+78 S Pav	5.14	229.02
'A	5.0	229.2
+3	4.8	229.4
+4	3.1	231.1
+6	1.7	232.5
cb	1.2	233.0
+6	0.9	233.3
S.L.	1.2	233.0
4+23		
S.L.	1.3	232.9
cb	1.6	232.6
+6	4.2	230.0
+7	5.2	229.0
+8	5.3	228.9
'A	4.9	229.3
+22 S Pav	5.15	229.01
±+13 ± Pav	5.12	229.04

		234.16	
7+23			
N 1/4+0 ²	N Pav	5.16	229.00
+2		4.7	229.5
cb		5.6	228.6
+5		5.8	228.4
NL		9.9	224.3
AN		12.6	221.6
15N		13.2	221.0
4+26			
15N		13.2	221.0
NL		12.6	221.6
+4		11.7	222.5
+8		6.0	229.2
cb		6.0	228.2
+7		5.5	228.7
+8		4.8	229.4
+9 ^B	N Pav	5.16	229.00
1/4+8 ^B	E Pav	5.13	229.03
E+7 ^E	S Pav	5.12	229.04
1/4		4.9	229.3
+2		5.7	228.5
+8		2.5	231.7
cb		2.5	231.7
SL		3.0	231.2

		234.16	
4+32			
SL		11.7	222.5
cb		11.5	222.7
+2		12.6	221.6
+4		11.4	222.8
1/4		4.8	229.4
+2 ²	S Pav	5.14	229.02
E+1 ²	E Pav	5.14	229.02
1/4+0 ²	N Pav	5.17	228.99
1/4+1		4.9	229.3
cb		11.7	222.5
+1		13.0	221.2
NL		13.1	221.1
15N		13.5	220.7
4+37	= W wall Colrect		
15N		14.5	219.7
NL		14.0	220.2
cb		14.1	220.1
+9	N. end w wall	14.6	219.6
+9	bottom of N beam	6.95	227.21
+9	top of N Cab	4.87	229.29
+9 ^B	N Pav	5.11	229.05
1/4+8 ^B	E Pav	5.10	229.06
E+7 ^B		5.08	229.08
+9	top s. Cab	4.95	229.21
+9	bottom of s. beam	7.02	227.14

234.16			
+9	grd. bot. w. wall	15.6	218.6
1/4		15.6	218.6
cb		15.1	219.1
S.L		15.0	219.2
15'S		15.6	218.6
A+57 = E Wall Culvert			
15'S		13.0	221.2
S.L		13.3	220.9
cb		14.0	220.2
1/4		15.2	219.0
+1	grd.	15.2	219.0
+1	bottom S beam	6.99	227.17
+1	top S cap	4.94	229.22
+2 ^z	S Pav	5.06	229.10
±+1 ^z	E Pav	5.01	229.15
1/4+0 ^z	N Pav	5.08	229.08
+1	top N cap.	4.86	229.30
+1	bottom of N beam	6.94	227.22
+1	grd. bot. E wall	14.9	219.3
cb		14.7	219.5
N.L		14.7	219.5
5'N		10.6	223.6
15'N		8.7	225.3

4+63		234.16	
15'N		9.5	224.7
6'N		7.7	226.3
A'N		9.0	226.2
N.L		9.0	225.2
cb		9.7	224.5
+9		8.4	223.8
+9		5.0	229.2
+9 ^z	N. Pav	5.08	229.08
1/4 ^z	E. Pav	4.98	229.28
±7 ^z	S. Pav	5.05	229.11
+9		4.81	229.4
1/4		5.3	228.9
+4		8.8	225.4
+5		11.4	222.8
cb		12.1	222.1
+8		10.7	223.5
+9		8.6	225.6
S.L		9.0	225.2
11'S		9.1	225.1
2'S		10.7	223.5
4'S		11.5	222.7
15'S		12.3	221.9

4+80	234.24		
10 N	7.6	226.4	
N.L	7.2	227.0	
+9	7.0	227.2	
cb	6.6	227.6	
+6	4.7	229.5	
+9 ⁸ N.Pav	5.01	229.23	
1/4+8 ⁸ E.Pav	4.98	229.26	
1/4+7 ⁸ S.Pav	5.03	229.21	
1/4	5.1	229.1	
+1	5.2	229.0	
+5	7.0	227.2	
cb	7.2	227.0	
S.L	7.3	226.9	
1's	7.4	226.8	
5's	10.2	224.0	
15's	12.3	221.9	
5+00			
20's	14.4	219.8	
15's	14.6	219.6	
14's	12.2	222.0	
11's	11.1	223.1	
10's	7.5	226.7	
S.L	7.1	227.1	
cb	6.4	227.8	
+4	6.2	228.0	

5+00	234.24		
S'4	5.5	228.7	
+2 ³ S.Pav	4.95	229.29	
1/4+1 ³ E.Pav	4.83	229.41	
1/4+0 ³ N.Pav	4.98	229.26	
+4	5.5	229.7	
+6	5.4	229.8	
+8	6.9	227.3	
cb	7.1	227.1	
N.L	6.8	227.4	
10 N	7.3	226.9	
5+25			
10 N	7.1	227.1	
1 N	6.6	227.6	
N.L	6.9	227.3	
cb	6.7	227.5	
+2	6.4	227.8	
+5	5.4	228.8	
+6	5.6	228.6	
+9 ² N.Pav	4.86	229.38	
1/4+8 ² E.Pav	4.77	229.47	
1/4+7 ² S.Pav	4.88	229.36	
1/4	5.3	228.9	
+1 ⁵	5.5	228.7	
+3	5.1	229.1	
+7	6.2	228.0	
cb	6.5	227.7	

Imperial

5+25	234.24		
S.L.	6.8	227.4	
1'S	6.9	227.3	
5'S	12.4	221.8	
15'S	13.8	220.4	
5+56			
15'S	13.3	220.9	
7'S	13.8	220.4	
4'S	13.5	220.7	
3'S	12.3	228.9	
1'S	11.1	223.1	
S.L.	6.1	228.1	
cb	5.9	228.3	
+5	5.5	228.7	
+7	5.0	229.2	
+8	5.3	228.9	
1/A	5.1	229.1	
+2 ³ S Pav	4.72	229.42	
1/2+1 ³ E Pav	4.65	229.59	
1/A+0 ³ N Pav	4.72	229.52	
+4	5.3	228.9	
+7	5.2	229.0	
+9	6.2	228.0	
cb	6.3	221.9	
N.L.	6.5	227.7	
8'N	6.3	227.9	
10N	6.7	227.5	

Imperial.

14

5+62	234.24		
10N	6.3	227.9	
N.L.	6.3	227.9	
+9	5.7	228.3	
cb	5.8	228.4	
+3	5.1	229.1	
+5	5.3	228.9	
+9 ² N Pav	4.72	229.42	
1/A+8 ² E Pav	4.65	229.59	
1/2+7 ² S Pav	4.69	229.55	
1/A	5.1	229.1	
+2	5.3	228.9	
+3	4.8	229.4	
+5	5.5	228.7	
cb	5.7	228.5	
+8	6.1	228.1	
+9	12.1	222.1	
S.L.	12.6	221.6	
15'S	13.3	220.9	
5+80			
15'S	13.1	221.1	
3'S	13.0	221.2	
S.L.	12.3	221.9	
+4	11.1	223.1	
+5	5.6	228.6	
cb	5.4	228.8	

	234.24		
5+80			
cbf?		4.7	229.5
+85		5.1	229.1
1/4		4.9	229.3
+2 ³ s Pav		4.68	229.56
♀+1 ³ ♀ Pav		4.55	229.69
1/4+0 ³ N Pav		4.68	229.56
+5		5.4	228.8
+6		5.2	229.0
cb		5.6	228.6
NL		5.6	228.6
10N		6.1	228.1
6+05			
10N		5.6	228.6
N.L.		5.5	228.7
+5		5.4	228.8
cb		5.0	229.2
+4		4.7	229.5
+5		5.1	229.1
+9 ² N Pav		4.46	229.78
1/4+8 ² ♀ Pav		4.43	229.81
♀+7 ² s Pav		4.58	229.66
1/4		4.8	229.4
+1 ⁵		4.9	229.3
+3		4.5	229.7
+7		5.0	229.2

	234.24		
6+05			
5 cb		5.2	229.0
+8		5.6	228.6
5.L.		12.2	222.0
7'S		13.8	220.4
15'S		13.0	221.2
6+08			
15'S		13.0	221.2
7'S		14.0	220.2
2'S		13.2	221.0
5.L.		5.7	228.5
cb		5.2	229.0
+8		4.4	229.8
+9		4.8	229.4
1/4		4.8	229.4
+2 ³ s Pav		4.56	229.68
♀+1 ³ ♀ Pav		4.44	229.80
1/4+0 ³ N Pav		4.45	229.79
+5		5.1	229.1
+7		4.7	229.5
cb		5.0	229.2
N.L.		5.4	228.8
10N		5.6	228.6

	234.24		
6+25			
10N		5.6	228.6
4N		5.2	229.0
N.L.		5.4	228.8
cb		4.8	229.4
+3		4.4	229.8
+5		4.9	229.3
+92	1N Pav	4.43	229.81
1/4+8 ²	± Pav	4.37	229.87
±+7 ²	S Pav	4.51	229.73
1/4		4.6	229.6
+1 ⁵		4.7	229.5
+3		4.3	229.9
+6		4.8	229.4
cb		5.0	229.2
S.L.		5.5	228.7
4'S		6.1	228.1
7'S		8.7	225.5
9'S		13.9	220.3
13'S		13.3	220.9

	234.24		
6+50			
8'S top ditch		5.8	228.4
S.L.		5.2	229.0
cb		4.6	229.6
+5		4.2	230.0
+8 ⁵		4.6	229.6
1/4		4.5	229.7
+2 ³	S Pav	4.21	230.03
±+1 ³	± Pav	4.23	230.01
1/4+0 ³	N Pav	4.29	230.05
+4		4.7	229.5
+6		4.2	230.0
cb		5.1	229.1
+5		4.9	229.3
N.L.		6.5	227.7
10N		6.8	227.4
6+83 ^L	w.L. Beacon Dr.		
10N		6.4	227.8
2N		6.3	227.9
N.L.		5.8	228.4
+3		5.1	229.1
cb		4.6	229.6
+4		4.1	230.1
+6		4.4	229.8
+92	N Pav	4.06	230.18
1/4+8 ²	± Pav	3.98	230.26
±+7 ²	S Pav	4.10	230.14

o.k. 6+83 ¹ = W. line	239.24	
1/4	4.3	229.9
+1 ⁵	4.4	229.8
+5	4.0	229.2
cb	4.6	229.6
S.L.	4.9	229.3
19's top ditch	5.8	229.4
7+0 ^{ok} 8 ² = E Beacon Dr		
15's	4.8	229.4
S.L.	3.8	230.4
+4	3.8	230.4
+7	4.3	229.9
cb	3.8	230.4
+6	3.8	230.4
+8 ⁵	4.3	229.9
1/4	4.1	230.1
+2 ³ S.Pav	3.94	230.30
♀+1 ³ ♀ Pav	3.80	230.4
1/4+0 ³ N.Pav	3.91	230.33
+4	4.3	229.94
+5	3.9	230.3
+7	4.3	229.9
cb	4.5	229.7
N.L.	5.0	229.2
20'N	5.4	228.8

o.k. 7+33 ¹ = E.L. Beacon Dr	234.24	
10N	5.0	229.2
N.L.	4.9	229.3
cb	4.6	229.6
+4	3.7	230.5
+6	4.1	230.1
+9 ³ N.Pav	3.70	230.74
1/4+8 ² ♀ Pav	3.56	230.68
♀+7 ² S.Pav	3.66	230.58
1/4	3.9	230.3
+2	4.0	230.2
+7	3.6	230.6
cb	3.6	230.6
S.L.	3.9	230.3
Line of trees - 7+42 ⁶ 8' N of S.L.		
T.D. 6.79	237.56	3.47 230.77
7+75		
S.L.	6.9	230.7
cb	6.5	231.1
+8 ⁵	7.2	230.4
1/4	7.0	230.6
+2 ³ S.Pav	6.70	230.87
♀+1 ³ ♀ Pav	6.56	231.00
1/4+0 ³ N.Pav	6.67	230.89
+4	7.1	230.5

7475	237.56		
+7		6.6	231.0
ob		6.8	230.8
NL		7.4	230.2
5N		7.4	230.2
√ 8+25			
5N		6.1	231.5
NL		6.5	231.1
+3		6.8	230.8
+9		6.1	231.5
ob		6.3	231.3
+3		6.2	231.4
+6		6.6	231.0
+9 ² N Pav		6.31	231.25
1/4+8 ² E Pav		6.19	231.38
1/2+7 ² S Pav		6.28	231.28
1/4		6.5	231.1
+2		6.7	230.9
+5		6.3	231.3
ob		6.4	231.2
S.L.		6.8	231.3

8475	237.56		
S.L.		5.8	231.8
ob		5.6	232.0
+5		6.0	231.6
+8		6.0	231.6
1/4		5.9	231.7
+2 ³ S Pav		5.70	231.87
1/2+1 ³ E Pav		5.53	232.03
1/4+0 ³ N Pav		5.57	231.97
+4		5.9	231.7
+7		5.6	232.0
ob		5.6	232.0
+2		5.7	231.9
+4		5.4	232.2
NL		5.7	231.9
5N		5.4	232.2
9+25			
5N		4.8	232.8
NL		4.9	232.7
+5		4.8	232.8
+7		5.0	232.6
ob		5.0	232.6
+4		5.0	232.6
+6		5.1	232.5
+9 ² N Pav		4.90	232.76
1/4+8 ² E Pav		4.68	232.88
1/2+7 ² S Pav		4.88	232.68

9+25	237.56		
1A		5.1	232.5
+2		5.3	232.3
cb		4.4	233.2
SL		4.3	233.3
9+75			
SL		3.3	234.3
cb		3.5	234.1
+6		4.0	233.6
+8		4.7	232.9
A		4.4	232.9
+2 ³ S Pav		4.04	233.52
±1 ³ ± Pav		3.92	233.84
4+0 ³ N Pav		3.96	233.60
+4		4.4	233.2
+6		4.3	233.3
+8		4.3	233.3
cb		4.6	233.0
+3		4.3	233.3
+8		4.2	233.4
N.L.		4.4	233.2
2N		4.4	233.2
5N		3.8	233.8

10+25	237.56		
5N		2.6	235.0
2N		3.1	234.5
N.L.		3.0	234.6
+4		2.9	234.7
+5		3.2	234.4
cb		3.2	234.4
+2		3.3	234.3
+5		3.9	233.7
+9 ⁸ N Pav		3.17	234.39
1/4+8 ² ± Pav		3.12	234.44
±+7 ² S Pav		3.27	234.29
1A		3.5	234.1
+1 ⁵		3.6	234.0
+4		3.1	234.5
cb		2.6	235.0
+6		2.4	235.2
S.L.		2.5	235.1
10+50			
10'S		2.7	234.9
S.L.		2.5	235.1
cb		2.1	235.5
+6		2.5	235.1
+8 ⁵		3.2	234.4
1A		3.1	234.1
+2 [±] S Pav		2.84	234.72

10+50		237.56	
ϕ+1 ^z	ϕ Pav	2.74	234.82
1/4+0 ^z	N Pav	2.80	234.76
+5		3.5	234.1
eb		3.3	234.3
+3		3.1	234.5
+6		3.2	234.4
+7		2.9	234.7
N.L.		2.7	234.9
5N		2.4	235.2
10+75			
5N		2.4	235.4
N.L.		2.5	235.1
+3		2.5	235.1
+5		3.0	234.6
eb		2.9	234.7
+4		2.8	234.8
+5		3.0	234.5
+9 ^e	N Pav	2.41	235.15
1/8 ^e	ϕ Pav	2.32	235.24
ϕ+7 ^e	S Pav	2.49	235.01
1/4		2.8	234.8
+1		2.9	234.7
+4		2.5	235.1
+8		2.4	235.2
eb		2.7	234.9

10+75		237.56	
5L		4.7	232.9
10S	top ditch	5.1	232.5
1/1+00			
15's		7.6	230.0
12's		7.0	230.6
9's		4.8	232.8
5L		4.5	233.1
+4		4.5	233.1
eb		3.7	233.9
+6		2.1	235.5
+9		2.6	235.0
1/4		2.4	235.2
+2 ^z	S Pav	2.09	235.47
ϕ+1 ^z	ϕ Pav	1.89	235.67
1/4+0 ^z	N Pav	1.96	235.60
+5		2.5	235.1
eb		2.6	235.0
+6		2.7	234.9
+7		2.3	235.3
N.L.		2.2	235.4
5N		2.3	235.3

11+25	237.56		
5N	2.1	235.5	
N.L.	1.8	235.8	
+2	1.6	236.0	
+4	2.4	235.2	
cb	2.4	235.2	
+5	2.1	235.5	
+9 ^e N. Pav	1.61	235.95	
1/4+8 ^e E Pav	1.53	236.03	
E+7 ^e S Pav	1.62	235.94	
1/4	2.1	235.5	
+2	2.2	235.5	
cb	3.4	234.2	
+6	4.3	233.3	
S.L.	4.3	233.3	
10's	4.8	232.8	
11+33 ^{ok} = W.L. Beacon Dr.			
15's	9.1	228.5	
12's	8.5	229.1	
10's	6.7	230.9	
S.L.	5.1	232.5	
cb	3.8	233.8	
+7	2.0	235.6	
+6 ^s	2.1	235.5	
1/4	1.9	235.7	

11+33	237.56		
1/4+2 ¹ S Pav	1.51	236.05	
E+12 E Pav	1.41	236.15	
1/4+0 ^e N Pav	1.56	236.00	
+4	2.1	236.05	
cb	2.2	235.4	
+6	2.3	235.3	
+7	1.8	235.8	
N.L.	1.6	236.0	
5N	1.9	235.7	
11+58 ¹ = E Beacon Dr			
5N	1.2	236.4	
N.L.	0.9	236.7	
+2	1.0	236.6	
+3	2.1	235.5	
cb	1.9	235.7	
+5	1.7	235.9	
+9 ^e N Pav	1.09	236.47	
1/4+8 ^e E Pav	1.03	236.53	
E+7 ^e S Pav	1.11	236.45	
1/4	1.6	236.0	
cb	3.0	234.6	
S.L.	4.3	233.3	
10's	6.0	231.6	

137.56

11+83^{ok} = E.L. Beacon Dr.

10 S	9.6	228.0
2 S	9.5	228.1
S.L.	4.2	233.4
cb	2.7	234.9
+4	2.6	235.0
+8	1.1	236.5
+8 ⁵	1.4	236.2
1/4	1.2	236.4
+2 ⁴ S Pav	0.74	236.82
±+1 ⁴ ± Pav	0.60	236.96
1/4+0 ⁴ N Pav	0.75	236.81
+4	1.3	236.3
cb	1.4	236.2
+9	0.9	236.7
N.L.	0.7	236.9
5 N	0.4	237.2
12+00		
5 N	0.5	237.1
N.L.	0.8	236.8
+1	1.4	236.2
+4	1.5	236.1
cb	1.2	236.4
+6	1.0	236.6
+9 ⁴ N Pav	0.47	237.09
1/4+8 ⁶ ± Pav	0.37	237.19

12+00

±+7 ⁶ S Pav	0.47	237.09
1/4	0.8	236.8
+1 ⁵	1.0	236.6
+3	0.6	237.0
+5	0.7	236.9
cb	2.2	235.4
+4	3.0	234.6
+8	5.4	232.2
S.L.	8.4	229.2
5 S	10.2	227.4
10 S	9.5	228.1
12+15 ⁵ = wind ret wall, on south.		
10 S	9.6	228.0
5 S	9.8	227.8
S.L.	10.8	226.8
+4	10.0	227.6
cb	5.7	231.9
+2 ⁵	4.3	233.3
+3 top ret. wall.	2.2	235.4
+7	0.9	236.7
1/4	0.9	236.7
+2 ⁴ S Pav	0.15	237.41
±+1 ⁴ ± Pav	0.08	237.46
1/4+0 ⁴ N Pav	0.17	237.39
+5	0.7	236.9

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12+15	237.56		
cb	1.0	236.6	
+5	1.1	236.5	
+6	1.3	236.3	
+9	1.3	236.3	
N.L.	0.3	237.3	
5N	0.2	237.4	
T.P. #3 7.31	244.69	0.18	237.38
12+32			
5N	7.0	237.7	
2N	6.8	237.9	
N.L.	7.5	237.2	
+1	8.3	236.4	
+6	7.8	236.9	
cb	7.6	237.1	
+5	7.5	237.2	
+9 ⁶ N Pav	7.06	237.63	
1/4+8 ⁶ S Pav	7.00	237.69	
1/4+7 ⁶ S Pav	7.24	237.25	
1/4	7.4	237.3	
+1 ⁵	7.4	237.3	
+2	7.2	237.5	
+4	7.6	237.1	
+7 top rot. wall	9.00	235.69	
+8 ⁵ at bottom wall	16.5	228.2	

12+32	244.69		
cb	18.0	226.7	
+5	12.9	231.8	
SL	16.6	228.1	
7's	15.6	229.1	
15's	13.0	231.7	
12+45			
15's	17.1	227.6	
SL	17.4	227.3	
cb	18.2	226.5	
+1 ⁵	18.2	226.5	
+3 top rot. wall	8.7	236.0	
+6	7.2	237.5	
+9	7.3	237.4	
1/4	7.2	237.5	
+2 ⁶ S Pav	7.05	237.64	
1/4+1 ⁶ S Pav	6.80	237.89	
1/4+0 ⁶ N Pav	6.86	237.83	
+5	7.4	237.3	
cb	7.5	237.2	
+3	7.5	237.2	
+4	8.0	236.7	
+8	7.6	237.1	
N.L.	6.8	237.9	
5N	6.8	237.9	

Station	Distance	Elevation
12+60	244.69	
5N	6.5	238.2
N.L.	6.4	238.3
+1	6.6	238.1
+2	7.7	237.0
+4	7.6	237.1
+5	7.3	237.4
cb	7.1	237.6
+9 ^E N Pav	6.59	238.10
1/4+8 ^E & Pav	6.54	238.15
1/4+7 ^E S Pav	6.78	237.91
1/4	7.0	237.7
+1 ^E	7.2	237.5
+3	7.1	237.6
+7 top wall	8.4	236.3
8 ^E at bottom of wall	16.7	228.0
cb	16.5	228.2
+2	15.7	229.0
S.L.	15.8	228.9
10 S	15.1	229.6
15 S	14.5	230.2

Station	Distance	Elevation
12+82	244.69	
15 S	14.8	229.9
S.L.	14.7	230.0
+4	14.8	229.9
cb	12.9	231.8
+1 ^E at bot. of wall	12.9	231.8
+3 top wall	8.0	236.7
+8	6.9	237.8
1/4	6.6	238.1
+2 ^A S Pav	6.15	239.54
1/4+1 ^A & Pav	6.01	239.68
1/4+0 ^A	6.04	238.65
+5	6.4	238.3
cb	6.5	238.2
+1	6.6	238.1
+2	7.3	237.4
+4	7.3	237.4
+8 ^E	6.9	237.8
+9	6.3	238.4
N.L.	6.1	238.6
5N	6.2	238.5

244.69

12+93 = w end ret. wall.

5N	5.7	239.0
N.L.	5.7	239.0
+2	6.8	237.9
cb	6.4	239.3
+9 ^e N. Pav	5.70	238.99
1/4+8 ^e ♀ Pav	5.61	239.08
♀+7 ^e S Pav	5.78	238.91
1/4	6.2	238.5
+2	6.2	238.5
+7	7.8	236.9
+8	10.5	234.2
cb	11.4	233.3
+3	11.7	233.0
+5	14.5	230.2
S.L.	14.9	229.8
15's	15.2	229.5
13+00		
15's	14.8	229.9
G's	11.2	233.5
S.L.	10.5	234.2
+5	9.5	235.2
cb	7.4	237.3
+5	5.6	239.1
+7	5.5	239.2
+8	6.0	238.7

13+00

244.69

1/4	5.9	238.8
+2 ^e S Pav	5.63	239.06
♀+1 ^e ♀ Pav	5.48	239.21
1/4+0 ^e N Pav	5.57	239.12
cb	6.3	238.4
+8	6.7	238.0
N.L.	5.5	239.2
5N	5.7	239.0
13+20		
5N	5.6	239.1
N.L.	5.2	239.5
+1	6.5	238.2
+3	6.5	238.2
cb	5.8	238.9
+9 ^e N Pav	5.08	239.61
1/4+8 ^e ♀ Pav	5.02	239.67
♀+7 ^e S Pav	5.12	239.57
1/4	5.1	239.6
+2	5.4	239.3
+4	5.1	239.6
cb	5.5	239.2
+7	5.7	238.8
S.L.	6.4	238.3
G's	7.0	237.7
10's	6.5	238.2

25

244.69

13+50

10 S	5.7	239.0
3 L	5.1	239.6
+3	5.0	239.7
+6	5.2	239.5
cb	5.1	239.6
+6	4.6	240.1
+9	4.9	239.8
19	4.7	240.0
+2 [±] S Pav	4.36	240.33
±+1 [±] ± Pav	4.22	240.47
19+0 [±] N Pav	4.32	240.37
+5	4.7	240.0
cb	5.1	239.6
+5	5.4	239.3
+8	6.3	238.4
+9	4.2	240.5
NL	4.4	240.3
5N	4.8	239.9

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13+75

244.69

5N	4.0	240.7
NL	3.7	241.0
+1	3.7	241.0
+2	4.9	239.8
+5	5.6	239.1
+7	4.8	239.9
cb	4.6	240.1
+5	4.0	240.7
+9 [±] N Pav	3.70	240.97
19+8 [±] ± Pav	3.55	241.14
±+7 [±] S Pav	3.71	240.98
19	4.1	240.6
+2	4.3	240.3
+4	3.7	241.0
+5	3.8	240.9
+7	4.2	240.5
cb	4.4	240.3
5L	5.1	239.6
5S	5.1	239.6

Imperial

(14+54.91 = B.C. Curve 18' Strip Pav.)
 $\Delta = 46^\circ 17' 20''$ LT.
 $R = 1500'$

244.69

244.69

14+00		
55	4.2	240.5
S.L.	4.2	240.5
+5	3.7	241.0
e.b	3.8	240.9
+6	3.0	241.7
+8	3.5	241.2
14	3.4	241.3
+2 [±] S Pav	3.02	241.67
±+1 [±] ± Pav	2.91	241.78
14+0 [±] N Pav	3.01	241.68
+6	3.5	241.2
e.b	4.0	240.7
+3	4.4	240.3
+4	4.7	240.0
+8	4.2	240.0
+9	2.9	241.8
N.L	3.0	241.7
14+50		
N.L	2.3	242.4
+15	3.4	241.3
+4	3.3	241.4
e.b	2.7	242.0
+4	2.2	242.5
+9 [±] N Pav	1.80	242.89
14+8 [±] ± Pav	1.55	242.14

±+7 [±] S Pav	1.53	243.16
14	1.8	242.9
+4	2.0	242.7
+5	1.7	243.0
c.b	2.2	242.5
S.L	2.3	242.4
14+62 [±] = B.C. Curve Stationed on South Side		
55	2.4	242.3
S.L.	2.4	242.3
+4	2.1	242.6
c.b	1.7	243.0
+5	1.3	243.4
+8	1.7	243.0
14	1.5	243.2
+2 [±] S Pav	1.21	243.48
±+1 [±] ± Pav	1.24	243.40
14+0 [±] N Pav	1.47	243.22
+6	1.7	243.0
e.b	2.1	242.6
+4	2.5	242.2
+7	3.0	241.7
+9	3.1	241.6
N.L.	2.3	242.4

July 1938

14+61.130 L Δ = 46° 12' R = 1542.69 L = 1243.22 (outside)

sections radial

244.69

1A+75		
N.L.	16	243.1
+2	2.7	242.0
+4	2.2	242.0
+5	2.4	242.3
1A	1.9	242.8
+3	1.5	243.2
+9 ⁵ N Pav	1.15	243.54
1A+8 ⁵ & Pav	0.90	243.79
&+7 ⁵ S Pav	0.90	243.79
1A	1.1	243.6
+6	1.0	243.7
cb	1.1	243.6
S.L.	1.8	242.9
5'S	2.1	242.6
15+00		
5'S	0.8	243.9
S.L.	0.6	244.1
cb	0.1	244.6
+5	0.0	244.7
1A	0.3	244.4
+3 S Pav.	0.30	244.39
&	0.32	244.37
+2 & Pav	0.35	244.34
1A	0.55	244.14
+1 N Pav	0.61	244.08

28

15+00

244.69

cb		1.0	243.7	
+9		1.9	242.8	
N.L.		0.9	243.8	
15+25				
N.L.		0.0		
T.P.#4	9.15	253.78	0.06	244.63
15+25				
N.L.		7.2	244.6	
+3		10.1	243.7	
+6		9.9	243.9	
cb		9.4	244.4	
+5		9.1	244.7	
+9 ⁵ N Pav		9.02	244.76	
1A		8.98	244.80	
+8 ⁵ & Pav.		8.76	245.02	
&		8.72	245.06	
+7 ⁵ S Pav		8.74	245.04	
1A		8.8	245.0	
+7		8.4	245.4	
cb		8.4	245.4	
S.L.		8.6	245.2	
5'S		8.7	245.1	

15+50

253.78

S.L.	7.8	256.0
cb.	7.9	255.9
+2	7.8	256.0
1/4	8.2	255.6
+3 ^L S Pav	8.13	245.65
£	8.12	245.66
+2 ^L £ Pav	8.15	245.63
1/4	8.36	245.42
+1 ^L N Pav	8.38	245.40
cb	8.6	245.2
N.L.	8.0	245.8
15+80 [≡] = w.L. Oniel st.		
N.L.	8.0	245.8
+3	8.2	245.6
cb.	8.0	245.8
+5	7.8	246.0
+9 ^L N Pav	7.70	246.08
1/4	7.66	246.12
+8 ^L £ Pav	7.44	246.34
£	7.41	246.37
+7 ^L S Pav	7.45	246.33
1/4	7.3	246.5
+7	6.9	246.9
cb	7.0	246.8
+5	7.2	246.6
S.L.	7.3	246.5

253.78

29

16+11[≡] = £ Oniel st.

N.L.	7.2	246.6
+4	7.1	246.7
+5	8.0	245.8
+6	8.0	245.8
cb	7.5	246.5
+9. N Pav	6.96	246.82
1/4	6.91	246.97
+8 £ Pav	6.72	247.06
£	6.68	247.10
+7 S Pav	6.72	247.06
1/4	6.8	247.0
cb	6.6	247.2
S.L.	6.9	246.9
16+42 [≡] = E.L. Oniel st.		
S.L.	6.1	247.7
+6	6.1	247.7
cb	5.9	247.9
+4	5.9	247.9
1/4	6.1	247.7
+3 S. Pav.	6.06	247.72
£	6.07	247.71
+2 £ Pav	6.10	247.68
1/4	6.32	247.46
+1 N Pav	6.35	247.43
cb	6.9	246.9

253.79

16+42³

+7	7.4	246.4
8	7.6	246.2
+9	7.5	246.3
N.L.	6.8	247.0

16+75

N.L.	7.4	246.4
+1	7.3	246.5
+3	6.7	247.1
cb	6.4	247.4
+8 ^S N Pav	6.02	247.76
1/4	5.93	247.85
+9 ^S L Pav	5.74	248.04
±	5.72	248.06
+6 ^S S Pav	5.65	248.13
1/4	5.8	248.0
+3	5.5	248.3
+5	5.0	248.8
cb	5.3	248.4
S.L.	5.6	248.2
5S	5.7	248.1

30

253.79

17+00

5S	5.0	248.8
S.L.	5.0	248.8
+4	4.8	249.0
cb	4.7	249.1
+5	4.7	249.1
1/4	5.5	248.3
+3 ² S Pav	5.39	248.39
±	5.45	248.33
+2 ² L Pav	5.49	248.29
1/4	5.64	248.14
+1 ² N Pav	5.66	248.12
cb	6.2	247.6
+8	6.6	247.2
+9	7.1	246.7
N.L.	7.1	246.1
1'N	7.1	246.1
2N	6.2	247.6
5N	5.7	248.1
17+25		
5N	5.5	248.3
2N	6.1	247.7
N.L.	6.1	247.7
+1	7.0	246.8
+5	6.3	247.5
cb	6.0	247.8

253.78

17+25

+8 ⁵ N Pav	5.51	248.27
1/4	5.46	248.32
+7 ⁵ E Pav	5.30	248.48
±	5.28	248.50
+6 ⁵ S Pav	5.20	248.58
1/4	5.2	248.6
cb	5.1	248.7
SL	5.1	248.7
SS	5.2	248.6
17+50		
SS	5.0	248.8
SL	5.1	248.7
cb	5.0	248.8
1/4	5.0	248.8
+3 ⁸ S Pav	4.93	248.86
±	5.03	248.75
+2 ⁸ E Pav	5.03	248.75
1/4	5.17	248.61
+1 ⁸ N Pav	5.28	248.50
cb	5.7	248.1
+5	6.1	247.7
+7	6.5	247.3
+8	5.9	247.9
N.L.	5.4	248.4
2N	4.0	249.8
5N	4.0	249.8

253.78

17+75

5'N	3.7	250.1
2'N	3.7	250.1
N.L.	4.7	249.1
+2	5.5	248.3
+3	5.9	247.9
+4	6.0	247.8
cb	5.4	248.4
+6 N Pav	4.97	248.81
1/4	4.94	248.84
+7 E Pav	4.86	248.92
±	4.74	248.04
+6 S Pav	4.70	249.08
1/4	4.8	249.0
cb	4.8	249.0
SL	4.8	249.0
SS	4.8	249.0
Floor garage 82' S	4.55	249.33
18+00		
SS	4.7	249.1
SL	4.7	249.1
cb	4.6	249.2
1/4	4.5	249.3
+4 ^L S Pav	4.43	249.35
±	4.47	249.31
+3 ^L E Pav	4.53	249.25

31

18+00

253.78

1/4		4.65	249.13	
+2 ¹	N Pav.	4.71	249.07	
cb		5.0	248.8	
+6		5.0	248.2	
+7		5.5	248.3	
+8		5.0	248.8	
+9		5.0	248.8	
NL		4.4	249.4	
2N		3.6	250.2	
5N		3.5	250.3	
T.P.	2.67	258.15	4.30	249.48

18+25

5s		9.5	248.7
1s		9.5	248.7
SL		9.0	249.2
cb		8.7	249.5
1/4		8.6	249.6
+4 ³	s Pav	8.58	249.57
⊕		8.58	249.57
+3 ³	⊕ Pav	8.63	249.52
1/4		8.73	249.42
+2 ³	N Pav	8.72	249.38
cb		9.1	249.1
+7		9.5	248.7
+9		9.4	248.8

18+25

258.15

cb		9.1	249.1
+4		8.0	250.2
NL		7.9	250.3
18+50			
NL		9.1	249.1
+4		9.2	249.0
+8		8.8	249.4
cb		8.7	249.5
+8 ²	N Pav	8.60	249.55
1/4		8.56	249.59
+7 ²	⊕ Pav	8.45	249.70
⊕		8.40	249.75
+5 ²	s Pav	8.35	249.86
1/4		8.4	249.8
cb		8.6	249.6
SL		9.2	249.0
5s		9.4	248.8
18+75			
5s		9.1	249.1
SL		8.9	249.3
cb		8.6	249.6
1/4		8.1	250.1
+4 ⁵	s Pav	8.05	250.10
⊕		8.11	250.04
+3 ⁵	⊕ Pav	8.19	249.96

32

		258.15	
18+75			
1/4		8.32	249.83
+2 ²	N Pav	8.40	249.75
cb		8.5	249.7
+8		9.0	249.2
+9		8.7	249.5
NL		8.8	249.4
19+00			
NL		8.4	249.8
+2		8.3	249.9
+3		8.9	249.3
+4		8.9	249.3
+5		8.6	249.6
cb		8.4	249.8
+2		8.3	249.9
+3		8.4	249.8
+7 ⁵	N Pav	8.15	250.00
1/4		8.05	250.10
+6 ⁵	E Pav	7.96	250.19
E		7.91	250.24
+5 ¹		7.86	250.29
1/4		8.0	250.2
+3		8.1	250.1
cb		8.4	249.8
+5		9.0	249.2
SL		9.3	248.9
55		9.5	248.7

		258.15	
19+25			
55		9.9	248.5
SL		9.5	248.7
cb		6.4	249.8
+4		8.0	250.2
1/4		7.6	250.6
+4 ²	S Pav	7.58	250.47
E		7.63	250.52
+3 ²	E Pav	7.70	250.45
1/4		7.80	250.35
+2 ²	N Pav	7.92	250.23
+7		8.2	250.0
+8		7.9	250.3
cb		8.1	250.1
+5		8.4	249.8
+7		8.6	249.6
+8		8.2	250.0
NL		8.1	250.1
19+50			
NL		7.9	250.3
+2		7.9	250.3
+3		8.6	249.6
+5		7.9	250.3
+7		7.7	250.5
cb		7.6	250.6
+3		7.7	250.3

258.15

19+50			
cb+2 ^L	N Pav	7.68	250.47
1/4		7.60	250.55
+6 ^L	E Pav	7.44	250.71
E		7.40	250.75
+5 ^L	S Pav	7.34	250.81
1/4		7.4	250.8
+2		7.5	250.7
cb		8.4	249.8
+3		9.2	249.0
+6		9.9	248.3
S.L.		10.1	248.1
10's		10.6	247.6
19+75			
10's		11.2	247.0
S.L.		10.6	247.6
cb		10.4	247.8
+1		9.2	249.0
+6		8.8	249.4
+9		7.3	250.9
1/4		7.1	251.1
+5 ^L	S Pav	7.10	251.05
E		7.15	251.00
+4 ^L	E Pav	7.24	250.91
1/4		7.36	250.79
+3 ^L	N Pav	7.43	250.72
+6		7.5	250.7

258.15

34

19+75			
+7		7.2	251.0
cb		7.3	250.9
+4		7.3	250.9
+9		7.9	250.3
N.L.		7.7	250.7
20+00			
N.L.		7.1	251.1
+1		7.1	251.1
+2		7.7	250.5
+5		7.2	251.0
cb		6.9	251.3
+3		7.0	251.2
+4		7.3	250.9
6 ⁸	N Pav	7.20	250.95
1/4		7.11	251.04
5 ⁸	E Pav	7.01	251.14
E		6.95	251.20
+4 ⁸	S Pav	6.86	251.29
+9		7.1	251.1
1/4		6.8	251.4
+3		7.0	251.2
+5		9.7	248.5
cb		10.2	248.0
+7		10.4	247.8
S.L.		11.9	246.3
10's		11.1	247.1

20+25

258.15

10'S		11.3	246.9
SL		11.2	247.0
cb		10.5	247.7
+3		10.0	248.2
+9		6.9	251.3
1/4		6.7	251.5
+5 ^B	S Pav	6.55	251.60
±		6.61	251.54
+4 ^B	± Pav	6.66	251.49
1/4		6.81	251.34
+3 ^B	N Pav	6.91	251.24
+7		7.1	251.1
+8		6.8	251.4
cb		6.7	251.5
+1		6.5	251.7
+5		6.6	251.6
+8		7.3	250.9
NL		6.9	251.3
5'N		7.1	251.1

20+50

258.15

5N		7.1	251.1
NL		6.7	251.5
+2		6.5	251.7
+3		6.8	251.4
+8		6.2	252.0
cb		6.4	251.8
+2		6.4	251.8
+3		6.8	251.4
+6 ^B	N Pav	6.53	251.62
1/4		6.51	251.64
+5 ^B	± Pav	6.37	251.78
±		6.31	251.84
+4 ^B	S Pav	6.22	251.93
1/4		6.4	251.8
+3		6.3	251.9
+8		9.6	248.6
cb		10.0	248.2
+5		10.7	247.5
SL		10.9	247.3
105		10.8	247.4

35

258.15

20+75

10.5	10.6	247.6
S.L.	10.5	247.7
+8	10.4	247.8
cb	9.7	248.5
+6	6.0	252.2
1/4	6.0	252.2
+5 ²	5.95	252.20
±	6.01	252.14
+4 ²	6.06	252.09
1/4	6.17	251.98
+3 ²	6.26	251.89
+7	6.5	251.7
+8	6.3	251.9
cb	6.2	252.0
+2	5.9	252.3
+6	5.7	252.5
+8	6.1	252.1
N.L.	6.9	251.3
3N	8.0	250.2
5N	8.1	250.1
10N	7.7	250.5

258.15

21+23² = w.L. Front + St.

10N	8.9	249.3
5N	9.0	249.2
N.L.	8.0	250.2
+4	6.4	251.8
+6	5.5	252.7
+9	5.5	252.7
cb	5.8	252.4
+2	6.1	252.1
+5 ²	5.63	252.52
1/4	5.57	252.58
+4 ²	5.48	252.64
±	5.36	252.79
+3 ²	5.30	252.85
+8	5.6	252.6
1/4	5.1	253.1
+1	4.8	253.4
+7	7.0	251.2
cb	8.5	249.7
+2	9.0	249.2
S.L.	9.4	248.8
14S	9.5	248.7
15S	11.5	246.7

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258.15

21+32			
10 S		11.6	246.6
6 S		11.5	246.7
5 S		9.6	248.6
S.L.		9.2	249.0
+5		8.7	249.5
cb		8.0	250.2
+2		7.4	250.8
+8		5.2	253.0
+9		4.6	253.6
1/4		4.9	253.3
+2		5.4	252.8
+6 ²	S Pav	5.22	252.93
±		5.28	252.81
+5 ²	S Pav	5.39	252.76
1/4		5.48	252.67
+4 ²	N Pav	5.57	252.58
+8		6.0	252.2
1/4		5.7	252.5
+4		5.3	252.9
+7		7.2	251.0
NL		7.7	250.5
2'N		12.6	245.6
5'N		13.1	245.1
7'N		12.3	245.9
12'N		12.6	245.6
14'N		9.2	249.0

258.15

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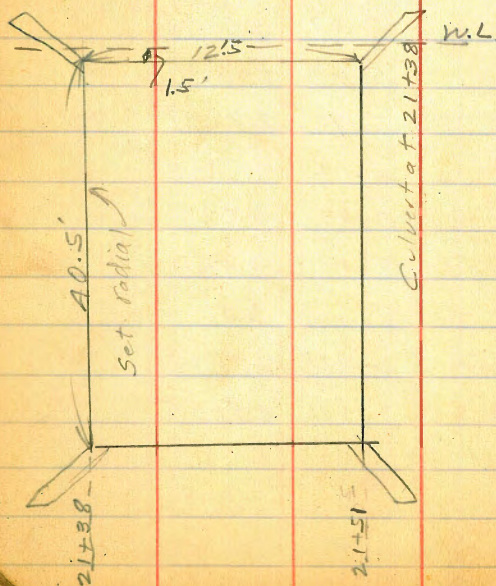
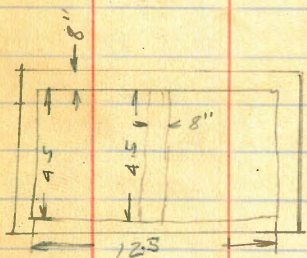
21+38 = w.wall culvert.

18'N		9.9	247.3
17'N		12.1	246.1
10'N		12.3	245.9
6'N		12.5	245.7
4'N		10.7	247.5
NL		11.3	246.9
+1	bottom wall send.	11.3	246.9
+1 ⁵	bottom slab ✓	6.89	251.26
+1 ⁵	top slab ✓	6.11	252.04
+3		5.4	252.8
+5		5.0	253.2
+9		5.2	253.0
cb		5.9	252.3
+5 ²	N Pav	5.47	252.68
1/4		5.37	252.78
+4 ²	± Pav	5.29	252.86
±		5.17	252.98
+3 ²	S Pav	5.14	253.01
+8		5.4	252.8
+8		5.1	253.1
1/4		5.6	252.6
+1 ⁵	top slab send	6.44	251.71
+1 ⁵	bottom slab ✓	7.10	251.05
+1 ⁵	bottom wall send	11.4	246.8
+5		11.8	246.4
cb		11.9	246.3

258.15

21+38

5.2	11.7	246.5
5.5	11.9	246.3
8.5	12.8	245.4
13.5	12.2	246.0
17.5	10.7	247.5



258.15

21+51 = E. end Culvert

15' 5	7.0	249.2
12' 5	8.6	249.6
5.2	9.6	248.6
+3	10.0	248.2
+4	10.7	247.5
+7	11.1	247.1
cb	10.3	247.9
+7	10.7	247.5
+8 at bottom of wall send	10.7	247.5
+8 bottom of slab send	6.95	251.20
+8 top slab	6.27	251.88
+9	5.5	252.7
1/4	5.1	253.1
+2	5.2	253.0
+6 S Pav	4.92	253.23
±	5.01	253.14
+5 ± Pav	5.10	253.05
1/4	5.20	252.95
+4 N Pav	5.29	252.86
+8	5.8	252.4
cb	5.4	252.8
+1	5.1	253.1
+5	5.1	253.1
+7 ± top slab send	6.18	251.97
+7 ± bottom slab	6.86	251.29
+7 ± at bottom wall send	10.8	247.4

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258.15

21+51			
N.L.	109	247.3	
6N	103	247.9	
19N	105	247.7	
25N	85	249.7	
21+56			
25N	87	249.5	
20N	106	247.6	
7N	106	247.6	
5N	96	249.6	
N.L.	96	248.6	
+1	97	248.5	
+1 ⁵	67	251.5	
+5	51	253.1	
+8	52	253.0	
cb	55	252.7	
+2	58	252.4	
+5 ⁵	N Pav	5.20	252.95
1/4		5.12	253.03
+4 ⁵	E Pav	5.05	253.10
4		4.95	253.20
+3 ⁵	S Pav	4.85	253.30
+8		5.3	252.9
1/4		5.0	253.2
+2		5.6	252.6
cb		8.0	250.2

258.15

39

21+56			
+4	85	249.7	
B.L.	83	249.9	
55	81	250.1	
65	86	249.6	
155	89	249.3	
21+75			
155	86	249.6	
75	81	250.1	
S.L.	76	250.6	
cb	64	251.8	
1/4	52	253.0	
+6 ²	S Pav	4.67	253.48
4		4.73	253.42
+5 ²		4.83	253.32
1/4		4.89	253.26
+4 ⁴	N Pav	4.96	253.19
+9		5.6	252.6
cb		5.3	252.9
+2		4.9	253.3
+6		5.0	253.2
N.L.		7.6	250.6
3N		8.3	249.9
73N		8.2	250.0

258.15

22+00

10 N	7.8	250.4
5 N	7.8	250.4
N.L.	6.6	251.6
+3	5.0	253.2
+9	4.8	253.4
cb	5.0	253.2
+1	5.3	252.9
+5 ³ N Pav.	4.65	253.50
1/4	4.54	253.61
+4 ³ E Pav	4.44	253.71
E	4.32	253.83
+3 ³ S Pav	4.25	253.90
+7	4.6	253.6
1/4	4.6	253.6
+4	4.5	253.7
+8	6.9	251.3
cb	7.4	250.8
+3	7.9	250.3
+7	7.7	250.5
SL	7.7	250.5

258.15

40

22+25

10 S	7.2	251.0
SL	6.8	251.4
+5	6.9	251.3
cb	4.7	253.5
+1	4.4	253.8
1/4	4.1	254.1
+6 ² S Pav	4.08	254.07
E	4.13	254.02
+5 ⁴ E Pav	4.23	253.92
1/4	4.29	253.86
+4 ² N Pav	4.38	253.77
+9	5.0	253.2
cb	4.6	253.6
+5	4.7	253.5
N.L.	6.2	252.0
10 N	7.4	250.8
22+50		
10 N	7.7	250.5
5 N	7.9	250.3
N.L.	6.4	251.8
+6	4.3	253.9
cb	4.2	254.0
+1	4.8	253.4
+5 ⁶ N Pav	4.11	254.04
1/4	4.03	254.12

258.15

22+50

1/4 4 ^e ± Pav	3.96	254.19
±	3.86	254.29
+3 ^e S Pav	3.80	254.35
1/4	3.7	254.5
+5	4.0	254.2
cb	4.7	253.5
S.L.	5.2	253.0
10 S	5.8	252.4
13 S	5.2	253.0
22+75		
10 S	5.4	252.8
7 S	5.1	253.1
S.L.	4.9	253.3
+8	4.9	253.3
cb	5.3	252.9
+4	5.6	252.6
+8	5.4	252.8
1/4	4.6	253.6
+2	3.7	254.0
+7 S Pav	3.51	254.64
±	3.54	254.61
+6 ± Pav	3.65	254.50
1/4	3.71	254.44
+5 N Pav	3.86	254.29
+9	4.4	253.8
cb	3.9	254.3

258.15

22+75

+5	4.3	253.9
+7	5.0	253.2
+8	6.6	251.4
NL	6.8	251.4
8 N	7.1	251.1
10 N	7.8	250.4
22+96		
10 N	8.1	250.1
7 N	7.2	251.0
NL	6.6	251.6
+4	6.0	252.2
cb	3.7	254.5
+1	4.3	253.9
+5 N Pav	3.63	254.52
1/4	3.50	254.65
+4 ± Pav	3.47	254.68
±	3.36	254.79
+3 S Pav	3.33	254.82
+7	3.6	254.6
+9	3.6	254.6
1/4	4.7	253.5
+5	6.8	251.4
cb	6.8	251.4
S.L.	5.9	252.3
10 S	4.9	253.3

41

258.15

23+00

10 S	4.6	253.6
7 S	4.2	254.0
S.L.	4.3	253.9
+3	4.5	253.7
+6	7.0	251.2
cb	7.0	251.2
+5	6.8	251.4
1/4	4.6	253.6
+2	3.5	254.7
+3	3.6	254.6
+7 ² S Pav	3.28	254.87
4	3.31	254.83
+6 ² 4 Pav	3.41	254.73
1/4	3.47	254.68
+5 ² N Pav	3.60	254.55
+9	4.2	254.0
cb	3.6	254.6
+2	4.4	253.8
+8	6.4	252.8
N.L.	6.8	251.4
1DN	8.2	250.0

23+25

10 N	8.5	249.7
7 N	7.0	251.2
2 N	6.0	252.2
N.L.	6.0	252.2
+4	6.0	252.2
cb	3.4	254.8
+1	4.0	254.2
+4 ² N Pav	3.38	254.79
1/4	3.22	254.93
+3 ² 4 Pav	3.11	255.04
4	3.02	255.13
+2 ² S Pav	2.99	255.16
+7	3.2	255.0
+8	3.2	255.0
1/4	4.7	253.5
+3	5.6	252.6
+8	6.4	251.8
cb	6.4	251.8
+2	6.1	252.1
+4	4.5	253.7
+6	4.2	254.0
S.L.	4.5	253.7
+5	4.1	254.1
+10	4.2	254.0

258.15

42

258.15

23+50

10 S	2.6	255.6
5 L	3.4	254.8
+6	4.1	254.1
+9	5.4	252.8
cb	6.0	252.2
+5	6.0	252.2
+8	5.5	252.7
1/4	4.9	253.3
+3	3.2	255.0
+7 ⁵ S Pav	2.81	255.34
¢	2.83	255.32
+6 ⁵ ¢ Pav	2.88	255.27
1/4	2.95	255.20
+5 ⁵ N Pav	3.07	255.08
+9	3.8	254.4
cb	3.2	255.0
+2	3.2	255.0
+6	5.7	252.5
N.L	6.3	251.9
+4	6.5	251.7
+8	8.1	250.1
+10	8.1	250.1

259.15

23+75

10 N	8.1	250.1
8 N	7.8	250.4
4 N	6.4	251.8
N.L.	5.8	252.4
+4	5.5	252.7
+6	3.4	254.8
+9	2.8	255.4
cb	3.5	254.7
+4 ² N Pav	2.81	255.34
1/4	2.70	255.45
+3 ⁵ ¢ Pav	2.61	255.54
¢	2.51	255.64
+2 ² S Pav	2.49	255.66
+7	2.7	255.5
1/4	4.1	254.1
+4	5.6	252.6
cb	5.3	253.9
+1	5.3	252.9
+2	4.0	254.2
+5	3.1	255.1
5 L	2.8	255.4
5's	2.5	255.7

43

258.15

24400

5'B	2.7	255.5
S.L.	2.8	255.4
+5	2.9	255.3
cb	4.5	253.7
+7	5.3	252.9
+9	5.1	253.1
1A	4.2	254.0
+5	2.3	255.9
+7 ² S Pav	2.24	255.91
±	2.25	255.90
+6 ² ± Pav	2.37	255.78
1A	2.46	255.69
+5 ² N Pav	2.59	255.56
cb	3.2	255.0
+1	2.7	255.5
+5	3.2	255.0
A.L.	5.7	252.5
3N	5.9	252.3
7N	7.7	250.5
10N	7.7	250.5

24+25

258.15

10N	7.8	250.4
7N	7.5	250.7
2N	5.4	252.8
NL	4.0	254.2
+5	2.7	255.5
+8	2.4	255.8
cb	2.9	255.3
+A N Pav	2.34	255.81
1A	2.15	256.00
+3 L Pav	2.10	256.05
±	2.01	256.14
+2 S Pav	1.98	256.17
+5	2.2	256.0
1A	4.6	253.6
cb	4.4	253.8
+3	2.6	255.6
+5	2.1	256.1
S.L.	2.3	255.9
T.P.#5	10.39	266.66
	1.88	256.27

14

266.66

24+75			
SL	9.2	257.5	
+7	9.4	257.3	
+9	10.5	256.2	
cb	10.8	255.9	
+1	11.0	255.7	
+5	11.1	255.6	
1/4	10.3	256.4	
+4	10.1	256.6	
+5	10.4	256.3	
+8 ⁵ SPav	9.95	256.71	
±	9.97	256.69	
+7 ⁵ ± Pav	10.12	256.54	
1/4	10.16	256.50	
+6 ⁵ N Pav	10.31	256.35	
cb	10.9	255.8	
+2	10.4	256.3	
+5	10.8	255.9	
NL	12.5	254.2	
4N	13.0	253.7	
8N	14.5	252.2	
10N	15.2	251.5	

254.00

10N	14.9	257.8	
8N	14.9	257.8	
5N	13.1	253.6	
NL	12.4	254.3	
+4	10.4	256.3	
+7	10.2	256.5	
+9	10.7	256.0	
cb	10.6	256.1	
+3 ² N Pav	10.07	256.59	
1/4	9.95	256.71	
+2 ² ± Pav	9.90	256.76	
±	9.73	256.93	
+1 ² SPav	9.71	256.95	
+5	12.2	256.5	
+6	10.0	256.7	
1/4	10.9	255.8	
+7	11.0	255.7	
cb	10.7	256.0	
+5	8.1	258.6	
SL	7.9	258.8	

266.66

45

25+25

266.66

S.L.	7.3	259.4
+8	7.4	259.3
cb	9.4	257.3
+2	10.1	256.6
1/4	10.0	256.7
+4	9.8	256.9
+5	10.1	256.6
+9 ⁺	3 Pav	9.43 257.23
E	9.42	257.24
+8 ⁺	E Pav	9.64 257.02
1/4	9.65	257.01
+1 ⁺	N Pav	9.80 256.86
cb	10.3	256.4
+2	10.6	256.1
+3	9.8	256.9
+7	10.2	256.4
N.L.	10.9	255.8
5N	13.2	253.5
8N	15.3	251.4
10N	13.3	253.4

25+75

266.66

12N	14.4	252.3
10N	12.6	254.1
3N	10.0	256.7
N.L.	10.0	256.7
+7	9.2	257.5
+9	10.0	256.7
cb	9.7	257.0
+2 ⁺	N Pav	9.30 257.36
1/4	9.17	257.49
+1 ⁺	E Pav	9.14 257.52
E	8.98	257.68
+10 ⁺	S Pav	8.98 257.68
+4	9.3	257.4
+6	8.3	258.4
+8	8.7	258.0
1/4	8.6	258.1
+5	7.9	258.8
cb	7.2	259.5
S.L.	6.0	260.7

46

26+25 266.66

S.L	3.2	263.5
+7	3.4	263.3
cb	4.5	262.2
+2	5.3	261.4
+5	5.9	260.8
1/4	6.7	260.0
+4	7.5	259.2
+6	8.5	258.2
⊕ 5 Pav	8.51	258.15
+9 ⊕ Pav	8.67	257.99
1/4 ?	6.69	257.97
+8 N. Pav	8.87	257.79
cb	8.9	257.8
+3	9.1	257.6
+4	8.6	258.1
+5	9.0	257.7
NL	9.3	257.4
+3	9.3	257.4
10N	11.8	254.9
13N	13.5	253.2

26+25 266.66

13N	12.5	254.2
8N	11.5	255.2
4N	9.4	257.3
NL	8.8	257.9
+6	8.3	258.4
+8	8.7	258.0
cb	8.5	258.2
+12 N Pav	8.45	258.21
1/4	8.23	258.43
+12 ⊕ Pav	8.22	258.44
+9 ⁵ S Pav	8.10	258.56
⊕	8.2	258.5
+4	8.5	258.2
+6	7.1	259.6
1/4	7.8	258.9
+6	7.0	259.7
+8	6.1	260.6
cb	5.8	260.9
S.L	4.8	261.9

266.66

27+06²⁹ = EC

S.L.	4.3	262.4
+5	4.5	262.2
cb	5.6	261.1
+2	5.8	260.9
+6	7.0	259.7
1A	7.1	259.6
+6	7.8	258.9
+7	8.2	258.5
±	7.9	258.8
+0 ² S Pav	7.77	258.89
+9 ² ± Pav	7.86	258.80
1A	7.86	258.80
+8 ² N Pav	8.03	258.63
cb	8.2	258.5
+3	8.5	258.2
+5	8.0	258.7
+9	8.2	258.5
N.L.	8.5	258.2
4N	9.1	257.6
6N	12.6	254.1
10N	13.5	253.2

27+50

266.66

10N	12.9	253.8
6N	13.0	253.7
4N	11.6	255.1
N.L.	10.5	256.7
+2	8.3	258.3
+6	7.5	259.2
+7	8.0	259.7
cb	7.5	259.2
+1 ² N Pav	7.41	259.25
1A	7.30	259.36
+0 ² ± Pav	7.30	259.36
+9 S Pav	7.26	259.40
±	7.5	259.2
+3	7.8	258.9
+6	7.2	259.5
1A	6.9	259.8
+5	6.2	260.5
+8	4.8	261.9
cb	4.3	262.4
+5	2.9	263.8
S.L.	2.6	264.1

18

27+75

266.66

SL	1.4	265.3
+5	1.9	264.8
cb	2.9	263.9
+4	3.8	262.9
+6	5.0	261.7
+9	5.1	261.6
1/4	5.5	261.2
+4	7.2	259.5
+6	7.1	259.6
+7	7.5	259.2
±	7.2	259.5
+1 S Pav	7.02	259.64
1/4 ± Pav	7.05	259.61
+9 N Pav	7.19	259.47
cb	7.5	259.2
+3	7.9	258.8
+4	7.4	259.3
+8	7.8	258.9
N.L.	10.5	256.2
2N	11.4	255.3
+3N	12.7	254.0
10N	12.5	254.2

28+00

266.66

10N	11.7	255.0
8N	12.9	253.8
5N	13.1	253.6
N.L.	10.0	256.7
+5	6.7	260.0
+8	6.7	260.0
+8	7.1	259.6
cb	7.0	259.7
+1 ² N Pav	6.96	259.70
1/4	6.86	259.80
+0 ² ± Pav	6.86	259.80
+8 ² S Pav	6.84	259.82
±	7.0	259.7
+2	7.3	259.4
+4	6.9	259.8
1/4	6.5	260.2
+5	5.1	261.6
+7	3.7	263.0
cb	3.0	263.7
SL	1.3	265.4

49

28+25

266.66

SL		1.2	265.5
cb		3.3	263.4
+3		3.5	263.2
+5		5.5	261.2
1/4		6.0	260.7
+4		6.8	259.9
+7		7.2	259.5
±		6.8	259.9
+0 ⁸	s Pav	6.66	260.00
+9 ⁸	± Pav	6.64	260.02
1/4		6.64	260.02
+8 ⁸	N Pav	6.79	259.87
cb		6.8	259.9
+1		6.9	259.8
+2		6.4	260.3
+5		6.3	260.4
NL		9.5	257.2
+4		11.8	254.9
+10		12.7	254.0

28+50

266.66

10N		11.2	255.5
4N		11.0	255.7
NL		8.1	258.6
+2		6.9	259.8
+5		6.5	260.2
+7		7.0	259.7
cb		6.7	260.0
+1 ²	N Pav	6.50	260.16
+9 ⁸	± Pav	6.41	260.25
1/4		6.41	260.25
+8 ⁸	s Pav	6.45	260.21
±		6.7	260.0
+3		6.9	259.8
+4		6.5	260.2
+9		6.9	259.8
1/4		6.6	260.1
+6		3.8	262.9
cb		2.8	263.9
SL		0.9	265.8

50

28+75

266.66

S.L	4.4	262.3
+3	4.2	262.5
+5	4.9	261.8
cb	5.7	261.0
+8	6.2	260.5
1/4	7.0	259.7
+3	6.5	260.2
+5	6.3	260.4
+7	6.8	259.9
±	6.5	260.2
+0 ⁸ S Pav	6.44	260.22
+9 ⁸ ± Pav	6.28	260.38
1/4	6.28	260.38
+8 ⁸ N Pav	6.34	260.32
cb	6.6	260.1
+3	6.9	259.8
+4	6.3	260.4
+7	6.4	260.3
N.L.	7.9	258.8
3N	9.3	257.4
7N	11.2	255.5
10N	11.2	255.5

29+00

266.66

10N	10.6	256.1
7N	10.4	256.3
5N	9.0	257.7
N.L.	8.4	258.3
+7	6.4	260.3
+8	6.7	260.0
cb	6.4	260.3
+1 ³ N Pav	6.18	260.48
±	6.09	260.57
+0 ² ± Pav	6.09	260.57
+8 ² S Pav	6.16	260.50
±	6.3	260.4
+3	6.6	260.1
+4	6.2	260.5
1/4	6.7	260.0
cb	5.8	260.9
+5	5.5	261.2
S.L.	5.4	261.3

29+25

266.66

S.L.	6.4	260.3
+5	6.7	260.0
cb	6.7	260.0
+5	6.7	260.0
'4	6.4	260.3
+5	5.9	260.8
+7	6.3	260.4
±	6.1	260.6
+0 ⁸ S Pav	6.06	260.60
+9 ⁸ ± Pav	5.96	260.70
'4	5.96	260.70
+8 ⁶ N Pav	6.04	260.62
cb	6.2	260.5
+3	6.4	260.3
+4	5.9	260.8
+9	6.0	260.7
N.L.	6.5	260.2
+7N	9.2	257.5
10N	10.0	256.7

29+75

266.66

11N	10.4	256.3
10N	8.5	258.2
5N	7.0	259.7
N.L.	6.0	260.7
+6	5.5	261.2
+7	6.0	260.7
cb	5.8	260.9
+1 ³ N Pav	5.63	261.03
'4	5.59	261.07
+0 ³ ± Pav	5.59	261.07
+9 ³ S Pav	5.67	260.99
±	5.8	260.9
+3	6.0	260.7
+4	5.6	261.1
+7	6.0	260.7
'4	5.7	261.0
cb	5.7	261.0
+5	5.8	260.9
S.L.	5.4	261.3

52

266.66

30+00			
S.L	4.6	262.1	
+3	4.7	262.0	
cb	5.7	261.0	
1/A	6.1	260.6	
+6	5.6	261.1	
+7	5.8	260.9	
£	5.6	261.1	
+1 ²	5.42	261.24	S Pav
1/4	5.39	261.27	E Pav
+9	5.46	261.20	N Pav
cb	5.6	261.1	
+2	5.8	260.9	
+3	5.2	261.5	
N.L	5.7	261.0	
BN	6.2	260.5	
8N	8.8	257.9	
10N	9.6	257.1	

266.66

53

30+50			
10N	9.0	257.7	
8N	8.3	258.4	
4N	6.9	259.8	
2N	5.2	261.5	
N.L.	5.1	261.6	
+7	4.5	262.2	
+9	5.1	261.6	
cb	5.1	261.6	
+1	5.07	261.59	N. Pav
1/4	4.99	261.67	E Pav
+9	5.07	261.6	S Pav
£	5.3	261.14	
+3	5.6	261.1	
+4	5.0	261.7	
1/4	5.2	261.5	
cb	5.2	261.5	
+8	4.9	261.6	
S.L	4.9	261.6	

26666

31+00

S.L.		4.9	261.8
cb		5.1	261.6
+6		4.5	262.2
1/4		4.6	262.1
+3		4.4	262.3
+6		4.6	262.1
+7		5.0	261.7
±		4.9	261.8
+1	S Pav	4.69	261.97
1/4	± Pav	4.63	262.03
+9	N Pav	4.59	262.07
cb		4.6	262.1
+2		4.6	262.1
+4		3.9	262.6
+8		4.2	262.5
N.L.		7.1	259.6
10N		8.3	258.4

266.66

31+50

10N		7.3	259.4
N.L.		8.0	258.7
+1		8.0	258.7
+2		3.7	263.0
+7		3.5	263.2
+8		4.2	262.5
cb		4.1	262.6
+1	N Pav	4.03	262.63
1/4	± Pav	4.07	262.59
+9	S Pav	4.13	262.53
±		4.3	262.4
+3		4.7	262.0
+4		4.1	262.6
1/4		4.3	262.4
+5		3.4	263.3
cb		3.1	263.6
+5		2.3	264.4
S.L.		2.2	264.5

54

32+00		266.60		
S.L.		1.0	265.7	
cb		1.7	265.0	
+7		1.5	265.2	
1/4		2.3	264.4	
+3		3.3	263.4	
+6		3.1	263.6	
+7		3.9	262.8	
±		3.6	263.1	
+1	S Pav	3.46	263.20	
1/4	± Pav	3.36	263.30	
+9	N Pav	3.46	263.20	
cb		3.5	263.2	
+3		3.7	263.0	
+5		2.6	264.1	
+7		3.0	263.7	
+8		6.3	260.4	
NL		6.7	260.0	
10N		7.1	259.6	
T.P. #6	8.77	273.84	1.59	265.07

32+50		273.84		
10N		12.6	261.2	
3N		13.9	259.9	
NL		12.5	261.3	
+2		9.1	264.7	
+6		9.1	264.7	
+8		9.9	263.9	
cb		10.0	263.8	
+1	N Pav	9.95	263.89	
1/4	± Pav	9.95	263.89	
+9	S Pav	10.04	263.80	
±		10.2	263.6	
+2		10.2	263.6	
+4		9.4	264.4	
1/4		8.1	265.7	
+4		7.5	266.3	
cb		7.8	266.0	
+6		8.0	265.8	
S.L.		7.9	265.9	

273.84

33+00

SL	6.9	266.9
+5	6.8	267.0
cb	6.9	266.9
+5	6.8	267.0
+7	7.2	266.6
'A	7.9	265.9
+4	8.7	265.1
+6	9.0	264.8
+8	9.9	263.9
±	9.6	264.2
+1 S Pav	9.41	264.43
'A ± Pav	9.39	264.45
+9 N Pav	9.39	264.45
cb	9.5	264.3
+3	9.5	264.3
+5	8.6	265.2
N.L.	9.0	264.8
HN	12.0	261.8
10N	12.5	261.3

273.84

33+25

10N	11.0	262.8
.4N	10.1	263.7
N.L.	8.8	265.0
+5	8.3	265.5
+7	9.4	264.4
cb	9.2	264.6
+1 N Pav	9.08	264.76
'A ± Pav	9.06	264.78
+9 S Pav	9.08	264.76
±	9.3	264.5
+3	9.7	264.1
+4	8.8	265.0
+7	8.6	265.2
+9	7.7	266.1
'A	7.6	266.2
+5	6.9	266.9
cb	6.9	266.9
+5	6.7	267.1
SL	6.0	267.8

56

273.84

33+75

SL		4.2	269.6
+5		5.0	268.8
cb		5.1	268.7
1/4		5.9	267.9
+5		8.2	265.6
+6		8.3	265.5
+7		9.3	264.5
E		8.7	265.1
+1	S Pav	8.45	265.39
1/4	E Pav	8.38	265.46
+9	N Pav	8.45	265.39
cb		8.7	265.1
+4		9.1	264.7
+6		7.6	266.2
+9		7.3	266.5
NL		7.7	266.1
+7N		9.5	264.3
10N		9.1	264.7

Imperial

273.84

57

34+00

10N		8.6	265.2
NL		7.3	266.5
+4		7.2	266.6
+5		7.5	266.3
+6		8.9	264.9
cb		8.3	265.5
+0 ⁶	N Pav	8.14	265.70
+9 ⁶	E Pav	8.08	265.76
1/4		9.09	265.75
+8 ⁶	S Pav	8.11	265.73
E		8.4	265.4
+3		9.0	264.8
+4		7.9	265.9
+6		7.5	266.3
1/4		5.0	268.8
+6		4.5	269.3
cb		4.5	269.3
SL		3.5	270.3

273.84

34+25

S.L.		3.2	270.6
Cb		4.1	269.7
+5		4.1	269.7
1/4		4.8	269.0
+1		4.8	269.0
+6		7.6	266.2
+7		8.8	265.0
±		8.1	265.6
+1	S Pav	7.76	266.08
1/4	± Pav	7.77	266.07
+9	N Pav	7.88	265.96
+4		8.7	265.1
+5		7.4	266.4
+8		7.0	266.8
NL		7.5	266.3
2N		7.9	265.9
10N		9.0	264.8

273.84

34+50

10N		8.5	265.3
6N		8.6	265.2
NL		7.5	266.3
+5		7.0	266.8
+6		7.3	266.5
+7		8.3	265.5
Cb		7.8	266.0
+1	N Pav	7.60	266.24
1/4	± Pav	7.51	266.33
+9	S Pav	7.52	266.32
±		7.8	266.0
+3		8.4	265.4
+4		7.5	266.3
+5		7.2	266.6
+9		5.3	268.5
1/4		5.2	268.6
Cb		4.6	269.2
+5		4.4	269.4
S.L.		3.9	269.9

58

273.84

35+00

SL	3.6	270.2
cb	4.2	269.6
+5	4.4	269.4
1/4	5.0	268.8
+4	6.8	267.0
+6	7.0	266.8
+7	7.8	266.0
±	7.3	266.5
+1 S Pav	6.95	266.89
1/4 ± Pav	6.92	266.92
+9 N Pav	6.93	266.91
cb	7.2	266.6
+4	7.8	266.0
+5	6.4	267.4
+8	6.2	267.6
NL	6.7	267.1
+8N	8.0	265.8
+9N	11.1	262.7
10N	10.8	263.0

273.84

35+50

10N	10.1	263.7
6N	9.8	264.0
2N	8.3	265.5
NL	6.5	267.3
+5	6.1	267.7
+6	6.8	267.0
cb	6.4	267.4
+1 N Pav	6.31	267.53
1/4 ± Pav	6.29	267.55
+9 S Pav	6.30	267.54
±	6.4	267.4
+3	7.0	266.8
+5	5.9	267.9
+8	3.1	270.7
1/4	3.0	270.8
+5	2.4	271.4
cb	2.3	271.5
SL	1.6	272.2

59

573.84

35+82

SL		0.4	273.4
+8		1.0	272.8
cb		1.6	272.2
1/4		1.9	271.9
+3		2.6	271.2
+5		5.2	268.6
+7		6.4	267.4
4		6.0	267.8
+1	S Pav	5.87	267.97
1/4	E Pav	5.87	267.97
+9	N Pav	5.86	267.98
cb		6.0	267.8
+3		6.4	267.4
+5		5.3	268.5
NL		6.0	267.3
+4N		6.7	267.1
6N		10.3	263.5
10N		9.8	264.0

273.84

60

35+91

10N		9.9	263.9
6N		10.0	263.8
3N		8.7	265.1
2N		6.1	267.7
NL		6.1	267.7
+5		5.6	268.2
+6		6.4	267.4
cb		5.9	267.9
+1	N Pav	5.79	268.05
1/4	E Pav	5.82	268.02
+9	S Pav	5.83	268.01
4		6.1	267.7
+3		6.3	267.5
+4		5.5	268.3
+5		5.1	268.7
1/4		5.3	268.5
+7		4.8	269.0
cb		4.1	269.7
SL		1.6	272.2

27384

36+00			
S.L.	3.7	269.1	
cb	4.6	269.2	
1/4	4.9	268.9	
+6	5.1	268.7	
+7	6.1	267.7	
±	5.8	268.0	
+15 ⁵ S Pav	5.73	268.11	
1/4 ± Pav	5.72	268.12	
+8 ⁵ N Pav	5.66	268.18	
cb	5.8	268.0	
+4	6.2	267.6	
+5	5.3	268.5	
N.L.	6.1	267.7	
2N	6.5	267.3	
3N	8.8	265.0	
10N	9.5	264.3	

London
Isbell
Merrill

Oct 17-28

27384

61

36+16⁸⁸ = Cty Lincoln North

10N	9.5	264.3	
1N	8.9	264.9	
N.L.	6.0	267.8	
+5	5.3	268.5	
+6	6.1	267.7	
cb	5.5	268.3	
+0 ³ N Pav	5.40	268.44	
+9 ³ ± Pav	5.45	268.39	
1/4	5.48	268.36	
+8 ² S Pav	5.51	268.33	
±	5.7	268.1	
+2	5.9	267.9	
+5	4.9	268.9	
1/4	4.6	269.2	
cb	4.1	269.7	
44	4.0	269.8	
+8	3.4	270.4	
S.L.	3.3	270.5	

Imperial

27384

62

Secon City line 36+60⁵⁰ on South

SL 1.5 272.3

cb 2.6 271.2

+8 3.6 270.2

1/4 4.2 269.6

+7 4.7 269.1

+8 5.4 268.4

1/2 5.3 268.5

+2 S Pav 5.1 268.7

1/4 E Pav 5.11 268.73

+9 N Pav 5.28 268.56

cb 5.4 268.4

+4 6.0 267.8

+6 5.2 268.6

N.L. 6.0 267.8

B.M. 5.36 268.48

T.P. 2.37 266.01 10.20 263.64

T.P. 2.30 261.70 6.61 259.40

Culvert at 29+25 (12" Ormco.)

FL Sand 2.65 259.05

FL Nend 4.40 257.30

T.P. 1.82 254.81 8.71 252.99

T.P. 0.88 244.39 11.40 243.41

T.P. 1.72 234.42 11.69 232.70

B.M. Pole #70169 3.28 231.14 (231.07)

2407

7+57	Eucalyptus tree on line	11.6	13.47	✓	1 1/4" diam
8		10.6	14.47	✓	
+20		8.6	16.47	✓	
+50		1.6	25.47	✓	X
T.P.	12.21	36.87	0.41	✓	24.66
+80		7.0	29.87	✓	
9+00		4.1	32.77	✓	
"	30' North	1.4	35.67	✓	
"	50' South	15.0	21.87	✓	
+20		1.6	35.27	✓	
T.P.	2.89	39.60	0.16	✓	36.71
9+50		2.9	36.70	✓	
9+69		2.4	37.40	✓	
"	20' North	1.0	38.60	✓	
"	50' South	11.0	28.60	✓	
9+72		2.2	37.40	✓	
"	20' North	1.0	38.60	✓	
"	30' South	2.0	17.60	✓	Cor. of Excavation
"	50' South	22.6	17.00	✓	
9+90		8.0	31.60	✓	
"	1' North	1.3	38.30	✓	
"	20' "	1.3	38.30	✓	
"	3' South	22.3	17.30	✓	
"	50' "	23.5	16.10	✓	
10+00		11.1	28.50	✓	
"	2' North	8.8	30.80	✓	
"	20' "	6.4	33.40	✓	
"	3' South	22.4	17.20	✓	
"	50' "	23.8	15.80	✓	

3960

64

10+19		14.9	24.70	✓	
"	1" North	13.9	25.7	✓	13.9
"	15' "	13.0	26.6	✓	
"	3' South	23.0	16.6	✓	
"	50' "	23.8	15.8	✓	
T.P.	0.60	27.54	12.66	✓	26.94
10+23	Floor of Excavation	13.0	14.54	✓	
T.P.	0.07	14.87	12.74	✓	14.80
10+50		1.2	13.67	✓	
11		3.3	11.57	✓	
11+18.90	on to B-line of E. Sewer	5.8	9.07	✓	(-3.24)
Ex. M.H. #1	Flowline	17.90	-3.03	✓	
					Here check FL grade
	"B" Line Sewer				= center line
7+20.7 = 0+00	P. 92	22.15	13.23	✓	on line
"	0+60	10.2	11.95	✓	
"	1	8.9	13.25	✓	
"	1+12	11.1	11.05	✓	
"	1+50	11.8	10.35	✓	
"	2	12.2	9.95	✓	
"	+22	11.4	10.75	✓	
"	2+65	5.1	17.05	✓	
"	3	4.8	17.35	✓	
3+23.64 = Δ	LT	4.9	17.25	✓	
"	" 5' South - Nudge paving	5.20	16.95	✓	
4+00		8.2	13.95	✓	

4+75			11.6	10.55 ✓	
T.P.	242	13.48	11.09	11.06	
4+86.75 = Elev of Ex. Sewer			5.29	8.19 ✓	(-3.45) ON HUB
Ex. Sewer M.H. #22 Flowline			17.03	-3.55 ✓	

Please check FL grade

12/14/28 12:00 noon Main Sewer flowing full capacity.

Water 2.5' above flowline in M.H.

80' wide
17' els
13' 1/2

F. St. X Sec. R6th to R7th.

3-7-29
Miller
170.19 NW. 27+E

190.49

66

BM.	12.37	190.49	178.12	NW. 26 th + F. St	1/4	4.6	
		00 = E. Line R6 th St.			+2	4.6	
N.		9.3	181.2		+3	9.2	
N. emb. cl.		11.43	179.06		c	9.5	181.0
gutter paint		12.21	178.28		+6	9.3	
1/4 "		12.06	178.43		+8	5.7	
c "		12.10	178.39		1/4	5.4	
1/4 "		12.33	178.16		cl	5.4	
gutter "		12.89	177.60		s	6.2	184.3
S. emb. cl.		12.35	178.14				
S		12.03	178.46		s	4.9	185.6
		3'E			cl	4.3	
S		8.4	182.1		1/4	4.4	
+5		9.0			+8	4.6	
+7		6.0			+9	5.4	
cl		5.6			c	5.6	184.9
1/4		5.8			+5	5.1	
+6		10.0			+8	3.7	
c		10.6	179.9		1/4	3.6	
+9		10.4			cl	3.7	
1/4		5.4			N	3.4	187.1
cl		4.9					
N		4.8	185.7		N	2.9	187.6
		8'E			cl	3.0	
N.		4.8	185.7		1/4	2.9	
cl		4.6			c	4.0	186.5

Plotted 8/14-29 CBH

30'E

45'E

190.49			
45' E. (cont)			
14	4.0		
cl	4.3		
S	4.4	186.1	
70' E			
S	4.2	186.3	
cl	3.7		
14	3.6		
e	3.7	186.8	
14	3.6		
cl	3.5		
N	3.1	187.4	
90' E			
N	4.0	185.5	
cl	3.9		
14	4.1		
e	4.3	186.2	
14	4.1		
cl	4.2		
S	4.3	186.2	
105' E.			
S	5.1	185.4	
cl	5.0		
14	5.2		
e	6.0	184.5	
14	5.7		
cl	6.0		
N	6.5	184.0	

190.49		F. St.	
130' E		67	
N	11.1	179.4	
cl	10.6		
14	10.3		
C	10.2	180.3	
14	10.5		
cl	9.7		
S	8.8	181.7	
142' C.			
S	11.7	178.8	
cl	11.8		
14	11.8		
T.P.	0.97	179.59	178.62
e	1.3	178.3	
14	2.3		
+6	2.9		
cl	1.8		
N	2.1	177.5	
146' E			
N	4.8	174.8	
cl	4.2		
14	3.3		
C	2.4	177.2	
14	1.1		
cl	1.2		
S	1.4	178.2	

179.59
154'E.

S	1.5	178.1
cb	2.0	
14	3.2	
C	4.1	175.5
14	4.9	
cb	5.1	
N	5.6	174.0
	167'E.	
N-5	8.1	
N	8.1	171.5
cb	8.1	
14	8.1	
C	7.6	172.0
14	7.4	
cb	7.0	
S	6.7	172.9
+5	6.7	
	190'E.	
-5	11.6	
S	11.7	167.9
cb	12.2	
14	12.6	
C	12.8	166.8
14	12.6	
cb	12.2	
N	13.1	166.5
+5	13.0	

179.59
210'E.

F. ST.

68

-5	16.0	
N	16.0	163.6
T.P.	0.27	167.09
cb	12.77	166.82
14	4.2	
14	3.8	
C	3.3	163.8
14	2.7	
cb	2.7	
S	3.0	164.1
15	2.6	
	220'E.	
-5	5.1	
S	4.9	162.2
+8	3.8	
cb	5.3	
14	5.9	
C	5.8	161.3
14	6.2	
cb	6.2	
N	6.4	160.7
+5	6.4	
	235'E.	
-5	7.7	
N	7.6	159.5
cb	8.1	
14	8.0	

167.09

235. E. Con

e	8.0	159.1
1/4	7.9	
eb	7.6	
S	7.6	159.5
+5	7.6	

250' E

S.	9.4	157.7
eb	9.4	
1/4	9.1	
e	9.3	157.8
1/4	10.2	
eb	11.1	
N	10.7	156.4

262' E.

N.	14.5	152.6
eb	14.3	
1/4	13.2	
e	12.1	155.0
1/4	11.1	
eb	11.3	
S	11.5	155.6
T.P.	0.30 154.85	12.54 154.55

283' E.

S	4.5	150.3
eb	3.6	151.3
1/4	5.2	149.5

154.85

F. ST.

69

e	6.2	148.7
1/4	6.9	
eb.	8.1	
N.	7.5	147.4

305' E

-5	13.1	
N	13.0	141.9
eb	13.5	
1/4	12.8	
e	12.6	142.3
1/4	12.2	
eb	11.6	
S	11.7	143.2
+5	11.5	

T.P. 0.95 142.75 13.05 141.80

326' E.

-10	3.0	
S	3.0	139.7
eb	3.7	
1/4	3.9	
e	3.7	139.1
1/4	4.9	
eb	4.8	
N	4.5	138.3
+10	4.3	

142.75
345.8

-15	9.4	
N	9.8	133.0
eb	10.1	
"4	10.1	
C	9.9	132.9
"4	9.6	
eb	9.1	
S	8.5	134.3
+15	8.9	
		365.8
-20	13.5	
S	13.1	129.7
eb	13.8	
"4	13.7	
C	13.3	129.5
"4	12.5	
eb	12.1	
N	12.1	130.7
+20	11.9	
		389.8
-30	12.9	
N	13.4	129.3
eb	13.7	
"4	14.1	
C	14.4	128.4
"4	14.7	

142.75

F. 57-70

eb	15.3	
S	15.8	127.0
+30	17.3	
		391.8 2 Bottom Ditch Location for Culvert
-30	17.3	
S	16.0	126.8
eb	16.3	
"4	15.9	
C	15.7	127.1
"4	15.3	
eb	15.3	
N	15.3	127.5
+30	15.3	
		193.8
-30	13.3	
N	13.7	129.1
eb	14.0	
"4	14.4	
C	14.5	128.3
"4	14.4	
eb	15.1	
S	16.0	126.8
+30	17.3	

142.75

408'.E

-30	17.6	
S	16.0	126.8
ch	16.0	
'14	15.7	
C	15.2	127.6
'14	14.5	
ch	14.0	
N	13.2	129.6
+20	12.4	

427'.E

N-0.5 front porch	6.2	✓1366 floor porch
N-0.5 " " "	10.6	1322 ground
N	10.6	1322
ch	12.0	
'14	12.9	
C	12.5	130.3
'14	12.0	
ch	12.4	
S	13.2	129.6
+20	14.4	

440'.E

-20	11.9	
S	11.4	131.4
ch	10.7	
'14	10.1	
C	9.8	133.0

142.75

F. St. 71

'14	9.5	
ch	8.4	
N	7.6	135.2
+0.5 dirt	7.6	
+0.5 porch floor	6.1	136.7
	452'.E	
-10	5.9	
N	6.5	136.3
ch	6.5	
'14	6.9	
C	7.7	135.1
'14	8.2	
ch	8.6	
S	9.4	133.4
+15	10.0	
	465'.E	
S-6 = Front of House	7.7	135.1 ✓
S	7.7	135.1
ch	6.6	
'14	4.7	
C	4.1	138.7
'14	3.9	
ch	2.9	
+8	2.6	
+10	1.4	
N	1.3	141.5
+15	0.6	

142.75

155.50

F. St.

72

490'.E

T.P.	12.75	155.50	0.00	142.75	Ngil Pole	-10	
		470'.E				N	
-15			12.7			ch	
N			13.3	142.2		"4	
ch			14.6			C	
"4			14.9			"4	
C			15.3	140.2		+5	
+7			15.0			+7	
"4			15.8			ch	
ch			17.0			+7	
S			17.0	138.5		S	
+6 = Front of House & ground			17.2			+10	
" " " " " floor			13.8	141.7 ✓			
		480'.E				-10	
-10 E. side House			14.0			S	
S			14.0	141.5		+12	
ch			13.6			ch	
+7			12.1			"4	
"4			12.7			C	
+8			13.2			"4	
C			11.7	143.8		ch	
"4			11.3			N	
ch			10.6			+10	
N			10.6	144.9			
+10			10.4				

7.8

7.8

7.8

7.8

8.8

9.2

9.5

10.5

10.3

9.9

11.6

12.6

9.7

8.5

8.1

6.2

6.2

6.2

5.5

4.9

5.3

5.5

147.7

146.7

143.9

500'.E

147.0

149.3

150.2

153.50				166.87				F. St.
518'.E.								73
-10	Bottom cobble wall		1.4				9.4	157.5
N	"		1.0	154.5			11.0	
eb	"		0.5				12.1	
"	"		0.5				13.7	153.2
C	"		1.7	153.8			14.4	
"	"		2.2					
eb	"		3.8					
S	"		4.6	150.9			10.8	156.1
+10	"		5.5				10.5	
520'.E.								
-10	"		5.0				9.4	
S	"		4.1	151.4			8.3	158.6
eb	"		3.4				7.3	
"	"		2.0				7.3	
C	"		1.2	154.3			8.0	158.9
T.P.	11.54	166.87	0.17	155.33				
"			11.0				7.2	159.7
eb			11.2				7.0	159.9
+9.5			11.1					
+10	Top cobble wall		8.8	158.0			6.2	160.7
N	"		8.8	158.0			6.0	160.9
+10	"		8.8				6.5	
530'.E.								
N	"		8.2	158.7			6.6	
eb	"		8.3				7.5	159.4
"	"		7.7				7.7	
							8.7	
							9.4	157.3
							11.3	

N. on & cont. walk to House
 = S. edge cont. walk
 10.5' of N. line (from Here to 29. St.)

545'.E.

+10' s. edge 2.5 cont. walk

166.87
560.9 = garage on S. dirt floor 2' Buck

S-2			7.2	159.7	floor
S			7.2	159.7	
cl			6.4		
"4			5.7		
C			4.7	162.2	
"4			3.9		
cl			3.4		
+3.7 S. edge			3.25	163.62	emt. walk
N			3.0	163.9	
T.P.	7.86	173.48	1.25	165.62	
		585'E			
N			5.2	168.3	
+1.66 S. edge			5.7	167.8	2.5 emt. walk
cl			5.8		
"4			6.3		
C			6.8	166.7	
"4			6.3		
cl			6.8		
S			7.3	166.2	
		597'E			
S			5.6	167.9	
cl			5.2		
"4			4.9		
C			4.6	167.9	
"4			4.2		
cl			4.0		

173.48

F. ST.

74

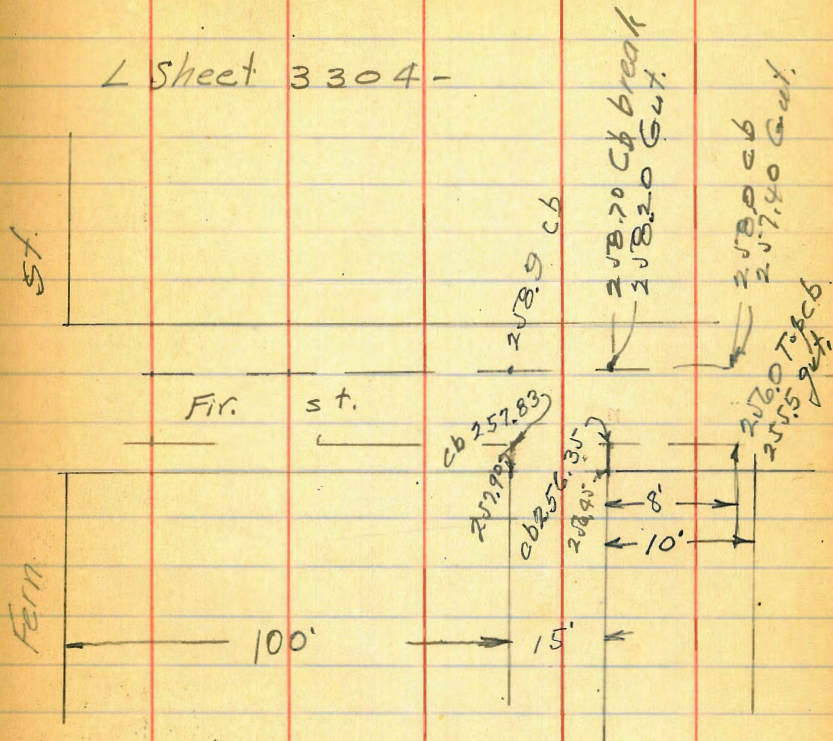
+3.2 S. edge			3.8	169.7	2.5 emt. walk
N			3.9	169.6	
					600'E = W. line 27 th St.
N			3.4		
+3.5 = N. cor.			3.16	170.32	emt. Return
emt. cl			3.34	170.14	✓
gutter, parmt.			4.02	169.46	
"4			4.14	169.34	
C			4.50	168.98	✓
"4			5.05	178.43	
gutter			5.81	167.67	
emt. cl			5.31	168.17	✓
S. on emt. walls			5.09	168.39	N.W. 27 th St
T.P. on B.M.			3.20	170.24 = 170.19	

3/12-1929-

75

In Grade Book

L Sheet 3304-



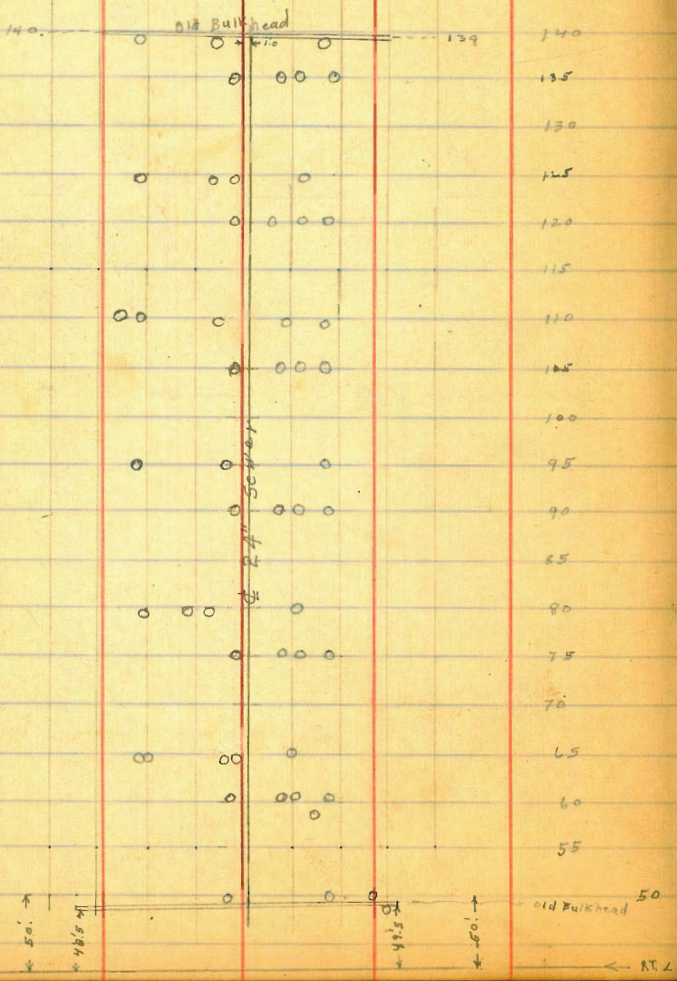
7-12-27
Miller

Location of Old Piling 32nd St Bridge

o = Pile

← 32nd St →

← 5' * 5' * 5' * 5' * 5' * 5' * 5' * 5' →



← 50' →
← 46 1/2' →

120'

← 50' →

← 50' →

← 46 1/2' →

← 48 1/2' →

← 50' →

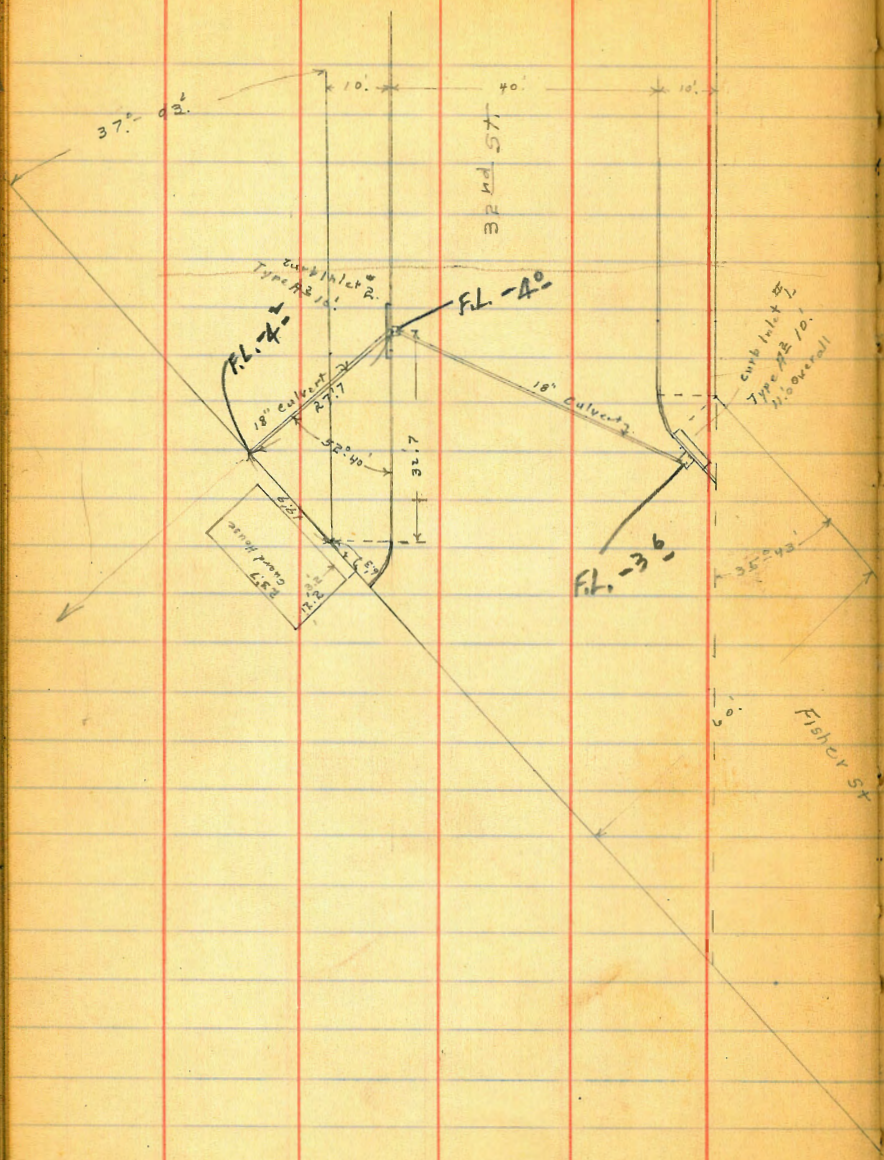
Old Bulkhead 50

← RT 2 Line at Angle Point

Location Curb Inlets & Culvert
at Fisher & 32nd St.

7-29-29
mills

77



5.47

79

0 + 95	in	drive	5.05	0.42	
1 + 08	"	"	5.04	0.43	
1 + 19	"	"	5.04	0.43	
1 + 24	gut		5.03	0.44	
"	CB	end drive	4.41	1.06	
1 + 50	in	gut	4.99	0.48	approx
1 + 75	"	"	4.99	0.48	0.56 curb face along here
2	"	"	4.97	0.50	
+ 25	"	"	4.95	0.52	
+ 50	"	"	4.95	0.52	
+ 75	"	"	4.90	0.57	
3	"	"	4.90	0.57	
+ 25	"	"	4.89	0.58	
+ 50	"	"	4.88	0.59	
+ 75	"	"	4.85	0.62	
4	"	"	4.80	0.67	

TABLE X.
MIDDLE ORDINATES OF RAILS
Length of Rail (feet)

C	R	30	28	26	24	22	20	C	R	30	28	26	24	22	20
o /	Feet	Inch	Inch	Inch	Inch	Inch	Inch	o	Feet	Inch	Inch	Inch	Inch	Inch	Inch
0-20	17189	.08	.07	.06	.05	.04	.03	8	716.8	1.88	1.64	1.42	1.20	1.01	.84
0-40	8594	.16	.14	.12	.10	.08	.07	9	637.3	2.12	1.84	1.60	1.35	1.14	.94
1-0	5730	.24	.20	.18	.15	.13	.10	10	573.7	2.36	2.05	1.78	1.50	1.27	1.04
1-20	4297	.31	.27	.23	.20	.17	.13	11	521.7	2.59	2.26	1.95	1.65	1.39	1.15
1-40	3438	.39	.34	.29	.25	.21	.17	12	478.3	3.83	2.47	2.15	1.81	1.54	1.26
2-0	2865	.47	.41	.35	.30	.25	.20	13	441.7	3.05	2.66	2.30	1.96	1.66	1.36
2-20	2456	.55	.48	.41	.35	.29	.23	14	410.3	3.30	2.87	2.48	2.10	1.78	1.46
2-40	2149	.63	.55	.47	.40	.33	.27	15	383.1	3.54	3.08	2.68	2.26	1.91	1.57
3-0	1910	.71	.62	.53	.45	.38	.31	16	359.3	3.76	3.28	2.83	2.40	2.04	1.67
3-20	1719	.78	.68	.59	.50	.42	.35	17	338.3	4.00	3.48	3.02	2.57	2.16	1.78
3-40	1563	.86	.75	.65	.55	.46	.38	18	319.6	4.21	3.67	3.18	2.70	2.28	1.87
4-0	1433	.94	.82	.71	.60	.50	.42	19	302.9	4.45	3.89	3.36	2.86	2.41	1.98
4-20	1323	1.02	.89	.77	.65	.55	.45	20	287.9	4.70	4.09	3.55	3.00	2.54	2.09
4-40	1228	1.10	.96	.83	.70	.59	.48	22	262.0	5.16	4.44	3.84	3.30	2.80	2.29
5	1146	1.18	1.03	.89	.75	.63	.52	24	240.5	5.64	4.92	4.20	3.59	3.04	2.50
6	955.3	1.41	1.23	1.06	.90	.76	.62	26	222.3	6.07	5.29	4.58	3.88	3.29	2.70
7	819.0	1.65	1.44	1.24	1.05	.89	.73								

TABLE XI.
SHORT RADIUS CURVES

Radius Feet	Chord Feet	Central Angle	Deflection Angle	Deflection for 1 Foot
35	10	16-26	8-13	49.3
45	10	12-46	6-23	38.3
50	15	17-16	8-38	34.5
60	15	14-22	7-11	28.8
75	15	11-30	5-45	23.0
100	20	11-30	5-45	17.3
120	20	9-34	4-47	14.3
150	20	7-39	3-49	11.5
190	25	7-32	3-46	9.15
200	25	7-10	3-35	8.6
225	25	6-25	3-12	7.7
240	25	5-58	2-59	7.2
250	25	5-44	2-52	6.9
275	25	5-12	2-36	6.2
288	50	9-58	4-59	6.0
300	50	9-32	4-46	5.7
350	50	8-12	4-06	4.9
376	50	7-40	3-50	4.6
400	50	7-10	3-35	4.3
410	50	7-00	3-30	4.2

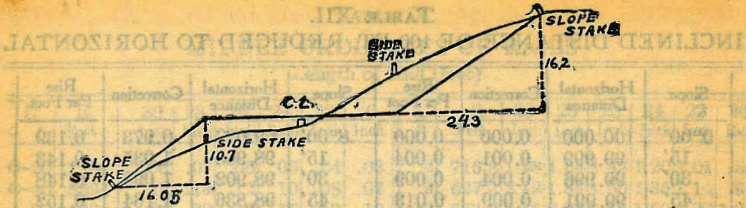
To find length of curve divide angle from P. C. to P. T. by central angle of chord, and multiply by length of chord.

TABLE XII.
INCLINED DISTANCE OF 100 FT. REDUCED TO HORIZONTAL

Slope	Horizontal Distance	Correction	Rise Per Foot	Slope	Horizontal Distance	Correction	Rise Per Foot
0°00'	100.000	0.000	0.000	8°00'	99.027	0.973	0.139
15'	99.999	0.001	0.004	15'	98.965	1.035	0.143
30'	99.996	0.004	0.009	30'	98.902	1.098	0.148
45'	99.991	0.009	0.013	45'	98.836	1.164	0.152
1 00	99.985	0.015	0.017	9 00	98.769	1.231	0.156
15	99.976	0.024	0.022	15	98.700	1.300	0.161
30	99.966	0.034	0.026	30	98.629	1.371	0.165
45	99.953	0.047	0.031	45	98.556	1.444	0.169
2 00	99.939	0.061	0.035	10 00	98.481	1.519	0.174
15	99.923	0.077	0.039	15	98.404	1.596	0.178
30	99.905	0.095	0.044	30	98.325	1.675	0.182
45	99.885	0.115	0.048	45	98.245	1.755	0.187
3 00	99.863	0.137	0.052	11 00	98.163	1.837	0.191
15	99.839	0.161	0.057	15	98.079	1.921	0.195
30	99.813	0.187	0.061	30	97.992	2.008	0.199
45	99.786	0.214	0.065	45	97.905	2.095	0.204
4 00	99.756	0.244	0.070	12 00	97.815	2.185	0.208
15	99.725	0.275	0.074	15	97.723	2.277	0.212
30	99.692	0.308	0.078	30	97.630	2.370	0.216
45	99.657	0.343	0.083	45	97.534	2.466	0.221
5 00	99.619	0.381	0.087	13 00	97.437	2.563	0.225
15	99.580	0.420	0.092	15	97.338	2.662	0.229
30	99.540	0.460	0.096	30	97.237	2.763	0.233
45	99.497	0.503	0.100	45	97.134	2.866	0.238
6 00	99.452	0.548	0.105	14 00	97.030	2.970	0.242
15	99.406	0.594	0.109	15	96.923	3.077	0.246
30	99.357	0.643	0.113	30	96.815	3.185	0.250
45	99.307	0.693	0.118	45	96.705	3.295	0.255
7 00	99.255	0.745	0.122	15 00	96.593	3.407	0.259
15	99.200	0.800	0.126	15	96.479	3.521	0.263
30	99.144	0.856	0.131	30	96.363	3.637	0.267
45	99.087	0.913	0.135	45	96.246	3.754	0.271

TABLE XIII.
MINUTES IN DECIMALS OF A DEGREE.

0 30"	.00833	10' 30"	.17500	20' 30"	.34167	30' 10"	.50833	40' 30"	.67500	50' 10"	.84167
1 00	.01667	11 00	.18333	21 00	.35000	31 00	.51667	41 00	.68333	51 00	.85000
30	.02500	30	.19167	30	.35833	30	.52500	30	.69167	30	.85833
2 00	.03333	12 00	.20000	22 00	.36667	32 00	.53333	42 00	.70000	52 00	.86667
30	.04167	30	.20833	30	.37500	30	.54167	30	.70833	30	.87500
3 00	.05000	13 00	.21667	23 00	.38333	33 00	.55000	43 00	.71667	53 00	.88333
30	.05833	30	.22500	30	.39167	30	.55833	30	.72500	30	.89167
4 00	.06667	14 00	.23333	24 00	.40000	34 00	.56667	44 00	.73333	54 00	.90000
30	.07500	30	.24167	30	.40833	30	.57500	30	.74167	30	.90833
5 00	.08333	15 00	.25000	25 00	.41667	35 00	.58333	45 00	.75000	55 00	.91667
30	.09167	30	.25833	30	.42500	30	.59167	30	.75833	30	.92500
6 00	.10000	16 00	.26667	26 00	.43333	36 00	.60000	46 00	.76667	56 00	.93333
30	.10833	30	.27500	30	.44167	30	.60833	30	.77500	30	.94167
7 00	.11667	17 00	.28333	27 00	.45000	37 00	.61667	47 00	.78333	57 00	.95000
30	.12500	30	.29167	30	.45833	30	.62500	30	.79167	30	.95833
8 00	.13333	18 00	.30000	28 00	.46667	38 00	.63333	48 00	.80000	58 00	.96667
30	.14167	30	.30833	30	.47500	30	.64167	30	.80833	30	.97500
9 00	.15000	19 00	.31667	29 00	.48333	39 00	.65000	49 00	.81667	59 00	.98333
30	.15833	30	.32500	30	.49167	30	.65833	30	.82500	30	.99167
10 00	.16667	20 00	.33333	30 00	.50000	40 00	.66667	50 00	.83333	60 00	1.00000



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

30°06
 16540
 3°24' L
 188-29
 10.7
 5.33
 16.03
 70
 14
 56

674.5
12.4

37.6
31.3
5.57

37.2
12.4
49.6

10
13
22
33

234.1
246.8
480.9
1642.3
2123.2

3.00
103.64
41.25
100.00

ENGINEERING DEPARTMENT,
CITY OF SAN DIEGO,
CALIFORNIA.

10.41
6.62
17.03
27.16
52.40