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Handwritten notes and calculations on the left page of the notebook, including numbers like 81-25, 73-53, 1564, 31-29, 95874, and various mathematical operations.

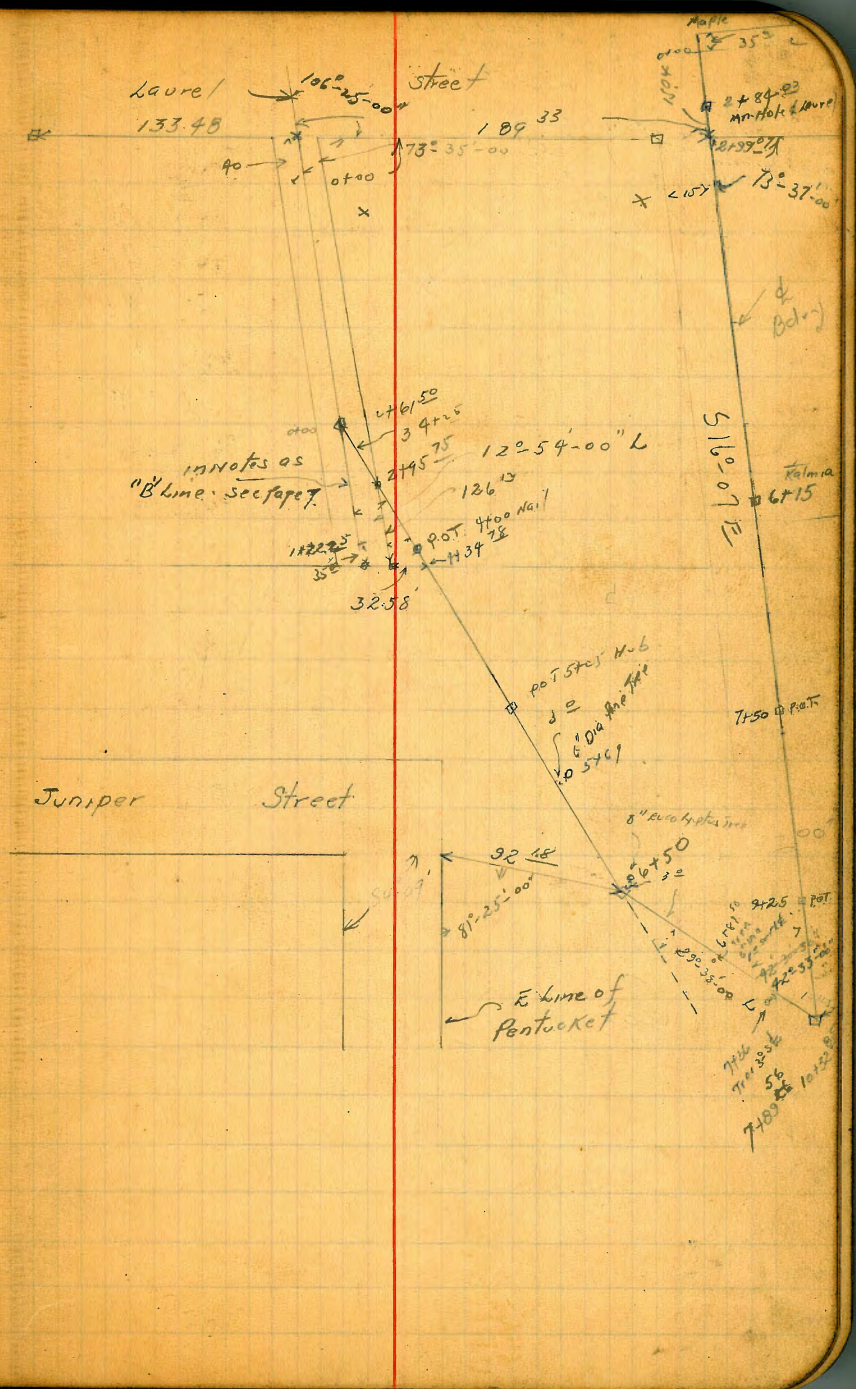
Index.

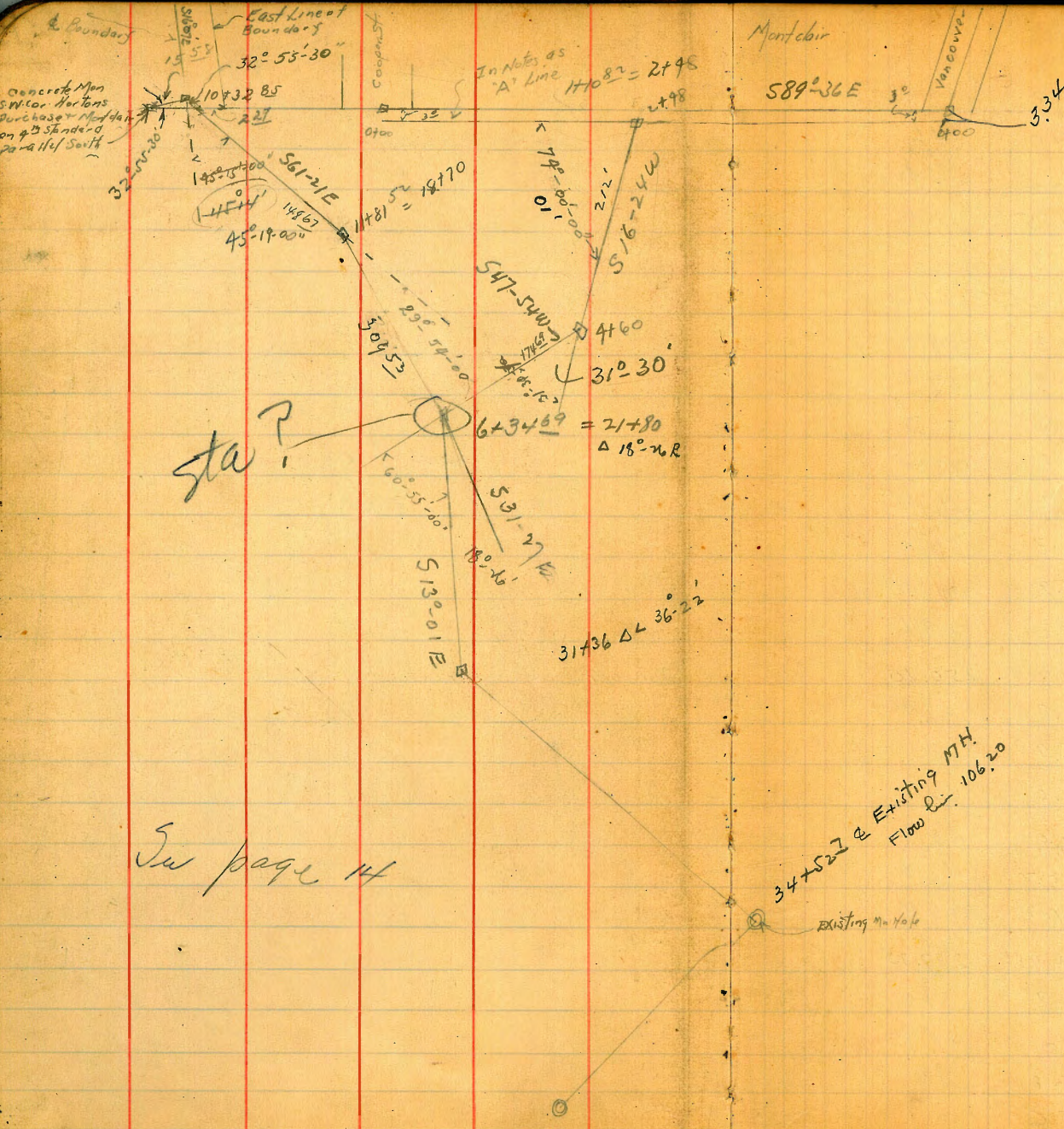
Pages 1-16. Sewer Survey Montclair Subdivision
" 18-32 X Section Lindwood St. Pringle to Andrews
" 33-49 X " " Guy St. Pringle to Andrews
" 50-63 X " " Puterbaugh " " "
" 64-75 X " " Torrence " " "
" 80 - Levels on Ret. SE. cor Bancroft & Ivy
" 81 - location Sewer Keating & Puterbaugh

W. E. Bliss
 Dec 17
 Jacobson
 Kienan
 1948
 Sewer Levels & Boundary from 35' South
 of the S. Line of Maple to S. N. Line

BM. Mon. & Maple E. Line of Boundary	157	297.46		295.89
0+00			2.9	946
0+50			3.5	940
1+00			4.2	933
1+50			5.0	925
2+00			5.7	918
2+50			6.5	910
2+89 1/2 Laurel Mn 46.6			7.4	90.1
3+00			7.9	89.6
3+50			9.9	87.6
4+00			11.5	86.0
7P	0.54	286.21	11.79	285.67
4+50			1.7	84.5
5+00			3.0	83.2
5+50			4.4	81.8
5+75			5.3	80.9
6+00			6.8	79.4
6+15 Mn Top & Kalmia on stab			7.2	278.92
6+25			7.9	78.3
6+40			8.8	77.4
6+50			9.3	76.9
6+75			10.9	75.3
6+85			11.8	74.4
7P	0.06	273.60	12.67	273.54
7+00			0.7	72.9
7+25			3.1	70.5

Plotted





See page 14

273.60

238.68

4

7+50			6.0	67.6
7+75			9.0	64.6
+87			11.2	62.4
+98			12.5	61.1
8+00			13.3	60.3
T.P.	0.86	262.10	12.36	61.24
8+10			3.3	58.8
+14			4.4	57.7
+25			5.8	56.3
+32			6.9	55.2
+39			8.7	53.4
+50			10.3	51.8
+56			11.9	50.2
+61			13.0	49.1
T.P.	0.60	250.70	12.00	250.10
+66			2.8	47.9
+75			5.9	45.3
+86			8.0	42.7
+95			10.0	40.7
9+00			10.7	40.0
+05			11.3	39.4
T.P.	0.93	238.68	12.95	237.75
+18			1.7	37.0
+21			3.0	35.7
+25	top of 1566 ft.		3.28	35.4
+30			5.6	33.1

+40			9.1	29.6
+50			12.8	25.9
T.P.	0.64	226.64	12.68	226.00
+56			2.9	23.7
+65			7.0	19.6
+70			9.8	16.8
+75			12.4	14.2
T.P.	0.85	215.00	12.49	214.15
+82			3.6	11.4
+87			6.1	08.9
+90			6.7	08.3
10+00			9.4	05.6
T.P.	3.37	205.98	12.39	202.61
+11			2.6	03.4
+25			6.8	19.9
+30			8.2	19.8
10+32	25	Δ E 95°-15'-00"	7.30	198.68
+45			8.7	97.3
+50			9.5	96.5
+63			8.6	97.4
+75			10.3	95.7
+79			11.8	94.2
+89			12.7	93.3
+91			11.4	94.6
11+00			10.9	95.1
+25			10.7	95.3

Dated

20598

5

+ 40			11.8	94.2
+ 50			12.6	93.4
79	3.55	196.54	12.99	192.99
+ 67			5.6	90.9
+ 75			6.3	90.2
1181.5 = 18 + 70.01411063			6.99	189.66
				189.55
				0.110110

Plotted

10/8/1918
W.E. Bliss

Server Levels. Alley East of
Common North South of Laurel

267.05

6

B.M.	127	297.16	295.89	+87	7.9	56.2
0400			12.00 85.2	+99	9.3	54.8
T.P.	2.02	287.26	11.96 285.20	+100	10.9	53.2
+25			3.4 83.9	+103	10.6	53.5
+34			4.5 84.8	+105	9.8	54.3
+36			5.1 84.2	+115	9.5	54.6
+50			6.0 81.3	+25	10.8	53.3
+57			6.6 80.7	+35	11.0	53.1
+62			8.2 79.1	+40	10.4	53.7
+75			9.9 77.4	+50	11.6	52.5
+87			12.3 75.0	T.P. 1.00	252.51	12.54 51.51
T.P.	114	275.48	12.92 274.34	+56	2.2	50.3
+100			4.2 71.3	+61.50	$\Delta 12^{\circ} 54' 00'' L$	2.69 279.8
+105			4.8 70.7	+76	3.1	49.4
+11			6.0 69.5	+83	2.5	50.0
+19			6.9 68.6	+96	3.2	49.3
+25			7.5 68.0	+100	3.4	49.1
+31			8.0 67.5	+115	5.7	46.8
+4			10.0 65.5	+25	7.1	45.4
+50			10.9 64.6	+34	8.0	44.5
+56			12.8 62.7	+50	12.0	40.5
T.P.	131	267.05	12.74 262.74	T.P. 0.47	291.39	11.59 40.92
+69			4.5 59.6	+61	1.7	39.7
+72			4.8 59.3	+67	2.2	39.2
+75			6.9 57.2	+75	4.2	37.2
+82			8.1 55.7	+86	7.8	33.6

24139

22009

7

4100	P.O.T. Nail	8.2	33.2 ✓
+16		6.8	34.6 ✓
T.P.	2.86	237.38	234.52
+25		4.0	33.4
+30		5.1	32.3
+35		3.6	33.8
+40		4.9	32.5
+50		8.0	29.4
+61		10.8	26.6
+75		11.7	25.7
+88		12.3	25.1
5100		11.9	25.5
T.P.	418	229.68 ✓	225.50
+09		5.0	24.7
+18		7.5	22.2
+25	P.O.T. Hobbit's Pine	8.90	21.3
+50		11.5	18.2
+58		11.8	17.9
+65		16.3	19.4
+75		10.4	19.3
+83		11.0	18.7
6100		14.5	18.2
T.P.	321	220.09 ✓	216.88
+11		6.1	14.0
+27		7.3	12.8
+50	Δ 29°-30'-00" L	7.95	12.14 ✓

+64		11.0	209.10
+75		13.0	207.1
T.P.	090	208.40 ✓	208.00
+700		3.2	205.2
+25		4.8	203.6
+34		5.0	203.4
+46		4.0	204.4
+50		4.4	204.0
+66		6.9	201.5
+75		9.6	198.8
+85		10.3	198.1
+789 ²⁶ - 10+32 ⁸⁵		9.74	198.66 ✓
see sketch page 2 "B" line Sewer levels from 21615° to 122.25 South #1 45608 ✓			
+0100	67.0	6.26	249.5
+16		5.0	251.1
+25		2.9	53.2
+37		2.2	53.9
+50		3.0	53.1
+65		3.6	52.5
+75		4.0	52.1
+100		4.4	51.7
+122 ²⁵ D.E. 350 N of lot line		5.6	50.5 ✓

Sewer levels from a point 3' south
of 4th Standard parallel South of Vancouver
West to a point 2.98 and then S. West to coincide
with original location

SM Mon of Vancouver	3.34	266.17	-	262.83	
0+00			3.2	63.0	14+41 ²⁹ =200
0+25			2.7	63.5	14+66 ²⁹
0+50			3.5	64.7	14+91 ²⁹
0+63			4.5	61.7	15+04 ²⁹
0+75			6.4	59.8	15+16 ²⁹
1+00			11.4	54.8	15+41 ²⁹
T.P.	130	254.59	12.88	253.29	
1+18			4.1	50.5	15+59 ²⁹
1+25			7.1	47.5	15+66 ²⁹
T.P.	0.89	292.60	12.88	241.71	
1+50			3.1	39.5	15+91 ²⁹
+65			8.5	34.1	16+06 ²⁹
+75			13.5	29.1	16+16 ²⁹
T.P.	331.10	231.03	12.67	229.93	
T.P.	0.10	217.90	13.23	217.8.0	
2+00			2.6	15.3	16+41 ²⁹
2+20			10.7	107. ✓	16+61 ²⁹
2+25			13.3	707.6	16+66 ²⁹
T.P.	0.64	205.42	13.12	204.78	
2+37			7.1	98.3	16+78 ²⁹
2+43			10.3	95.1	16+84 ²⁹
2+45			10.4	95.0	16+86 ²⁹
2+48 A	792.00-00 L		9.12	96.30	16+89 ²⁹
T.P.	0.38	196.68	9.12	196.30	
+57			0.1	76.6	16+98 ²⁹

19668

8

+67	17+08 ²⁹	2.5	94.2	
+68	17+09 ²⁹	3.3	93.4	
+75	17+16 ²⁹	3.7	93.0	
3100	17+41 ²⁹	4.8	91.9	
+15	17+56 ²⁹	5.1	91.6	
+25	17+66 ²⁹	4.1	92.6	
+41	17+82 ²⁹	4.8	91.9	
+50	17+91 ²⁹	5.5	91.2	
+60	18+01 ²⁹	7.8	88.9	
+75	18+16 ²⁹	9.5	87.2	
+87	18+22 ²⁹	10.7	86.0	
+82	18+23 ²⁹	11.9	84.8	
4+00	18+41 ²⁹	12.5	84.2	
4+10	18+51 ²⁹	12.7	84.0	
+11	18+52 ²⁹	11.6	85.1	
+17	18+58 ²⁹	11.1	85.6	
+25	18+66 ²⁹	11.5	85.2	
+40	18+81 ²⁹	12.4	84.3	
+50	18+91 ²⁹	13.8	82.9	
T.P.	0.05	184.13	12.60	184.08
160 A	31°-30'-30" R.	0.84	19+01 ²⁹	183.29
+75	19+16 ²⁹	2.7	81.4	
+83	19+24 ²⁹	3.0	81.1	
+92	19+38 ²⁹	4.1	80.0	
+93	19+36 ²⁹	5.5	78.6	
5200	19+42 ²⁹	5.9	78.2	

HZ
18413

5+07	19+48 ²⁹	6.3	77.8
+10	19+51 ²⁹	5.5	78.6
+25	19+66 ²⁹	5.7	78.4
+50	19+91 ²⁹	5.9	78.2
+75	20+16 ²⁹	7.5	76.6
+88	20+29 ²⁹	8.9	75.2
6+00	20+41 ²⁹	9.9	74.2
+11	20+53 ²⁹	10.9	73.2
+21	20+62 ²⁹	12.0	72.1
+25	20+66 ²⁹	11.9	72.2
6+34	20+76 ²⁹	12.52	71.61

171.68 old notes
171.61
0.07 error

A line from Mon. & Cooper, South E.

along 4th standard parallel to Δ

1+10⁸² = 498

DM Mon & Cooper
4th standard parallel to Δ
0.97

237.20

Eto
236.23

0+00		1.6	✓ 35.6	11+84 ⁶³
0+15		4.7	32.5	11+99 ⁶³
0+25		7.4	29.8	12+09 ⁶³
0+45		13.3	23.9	12+29 ⁶³
T.P.	1.17	225.57	12.83	224.37
0+60		3.6	21.9	12+34 ⁶³
0+58		7.0	18.5	12+42 ⁶³
0+75		13.0	12.5	12+58 ⁶³
T.P.	0.52	213.21	12.85	212.69
0+85		3.8	20.4	12+64 ⁶³
0+99		7.0	20.6	12+78 ⁶³

21321

9

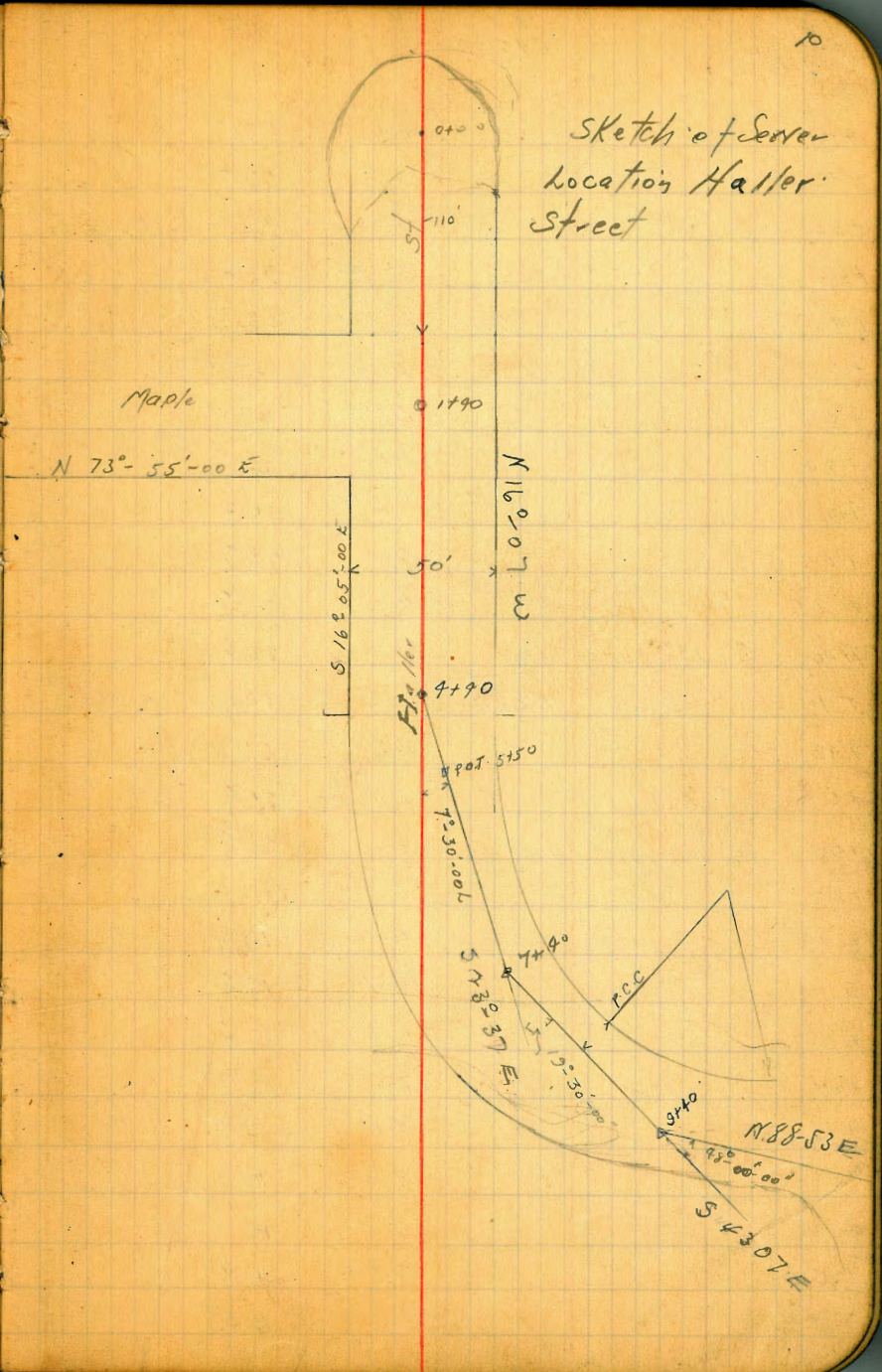
1+00	9.7	12+84 ⁶³	203.5 ✓
1+05	12.7	12+89 ⁶³	200.5 ✓
T.P. 1.93	202.58	12.56	200.65 ✓
1+10	7.0	12+94 ⁶³	198.6 ✓
1+10 ⁸² Δ = 498	6.23	12+95 ⁶³	196.35 ✓
			196.30
			0.05

See page 23 Book 1191 page 23

Bliss
Duermit
Jacobson
Kjerner
10/10/18
B.M. Sierra Club
at Haller & Maple

	HI	+	HI	+	ELV
	3.15		278.82	✓	275.67
0+00			2.0		76.8
+50			2.2		76.6
1+00			2.6		76.2
1+90 E. Maple			3.22		75.60
1+50			3.5		75.3
2+00			4.5		74.3
+50			5.7		73.1
3+00			7.2		71.6
+50			9.2		69.6
4+00			11.2		67.6
4+90 Δ 7° 30' 00" left			12.80		66.0
T.P.	2.19	268.19	12.80		266.02
+50			2.7		65.5
5+00			4.7		63.5
+13			5.7		62.5
+35			6.7		61.5
+50 P.O.T. 1" Hub			8.3		59.9
6+7			10.9		57.3
7+5			13.0		55.2
T.P.	1.95	256.68	12.96		255.23
+90			4.7		52.0
6+00			6.6		50.1
+03			7.8		48.9
+18			11.5	✓	45.2
T.P.	0.94	245.01	12.61	✓	244.07

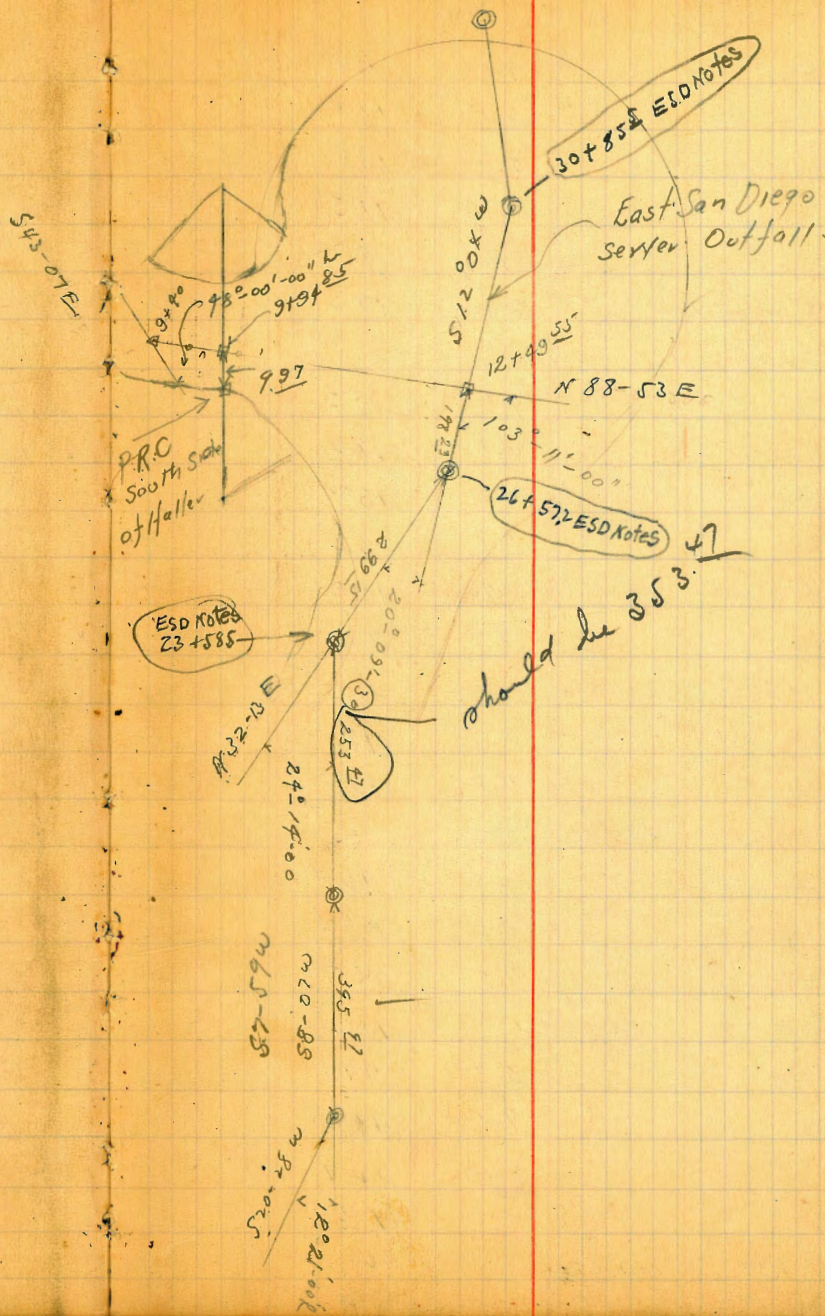
Sewer levels of Haller Street
Montclair Addition from 110 North of the N
Line of Maple South to Intersection with East San



295.01

11

+25			2.6	42.4
+90			7.3	37.7
+50			9.9	35.1
160			13.4	31.6
TP	0.32	83 232.73	12.50	232.51
+75			2.9	29.9
+85			5.9	27.4
+94			7.0	25.8
7100			8.6	24.2
+09			9.1	23.7
+25			11.0	21.8
7140	Δ	19° 30' 00" left	12.23	20.60
TP	3.28	88 223.78	12.23	220.50 ⁶⁰
+48			2.7	21.2
+63			2.3	21.6
+75			3.0	20.9
+88			3.6	20.3
+94			4.7	19.2
8100			6.1	17.8
+06			6.3	17.6
+09			7.2	16.7
+25			9.0	14.9
+34			9.0	14.9
+90			9.8	14.1
+50			9.1	14.8
+65			7.6	16.3



	+	HI	-	Elev
		223.78		
		88		
+67			7.0	16.9
+75			6.5	17.4
+100			5.0	18.9
+10			5.6	18.3
+25			5.7	18.2
+90	Δ 98°-00'-00" left		6.60	17.3
T.P.	1.08	218.28	6.60	217.28
+97			0.1	18.3
+53			0.1	18.3
+61			2.2	16.2
+69			5.1	13.3
+77	95° P.O.T 144.6		8.40	10.0
+80		96	9.4	9.0
T.P.	1.68	206.86	13.08	205.18
+100			8.9	198.1
+05			11.9	195.1
T.P.	0.95	195.10	12.21	194.65
+12			2.8	92.4
+23			8.0	87.2
+25			9.5	85.7
T.P.	0.09	182.28	12.91	182.19
+37			3.3	79.1
+47			9.4	73.0
+50			10.3	72.1
+57			12.8	69.6
T.P.	0.33	163.62	12.99	169.29

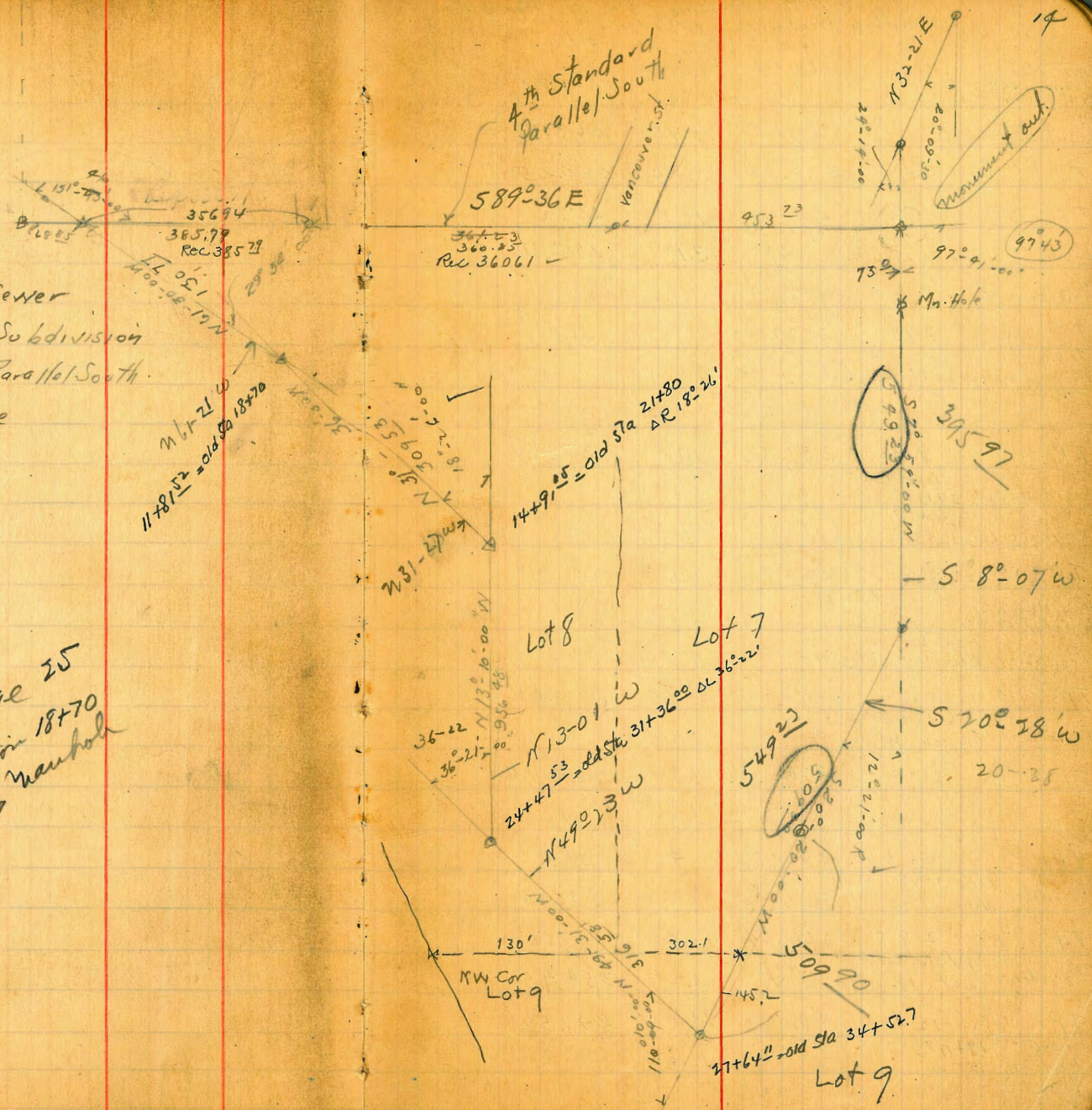
	+	HI	-	Elev
		(169.62)		
		169.72		
				12
+65			4.3	165.4
+67			5.6	64.1
+70			6.9	62.8
+75			9.9	59.8
T.P.	0.10	157.50	12.22	157.40
+88			3.9	53.7
+95			6.7	50.9
+100			7.6	50.0
+25			10.7	46.9
+50			11.9	45.7
+15			12.3	45.3
T.P.	4.68	150.05	(193.95) 12.23	145.27
+98			5.5	44.6
+100			8.3	41.8
+06			8.1	42.0
+09			7.0	43.1
+17			6.6	43.5
+26			7.0	43.1
+30			4.6	45.5
+47			5.0	45.1
+49	5.5		4.44	45.61
Set B.M. Mon			2.56	147.49
T.P.	8.15	157.00	1.10	(147.39)
Set B.M. Mon			5.82	149.85
T.P.	8.63	159.88	5.75	151.18
T.P.	9.62	167.11	2.39	151.59

HI
21
(16711)

TP	10.32	175.35	2.08	13
check on	56.1			165.03
rim of Monte	in Sisson's Notes	2.57		172.88
				(172.78)

Traverse to tie up sewer
 outfall for Montclair Subdivision
 South of 9th Standard Parallel South
 Across Hortons Purchase
 See Page 16

See Book 1191 page 25
 for levels from station 18+70
 to Existing manhole

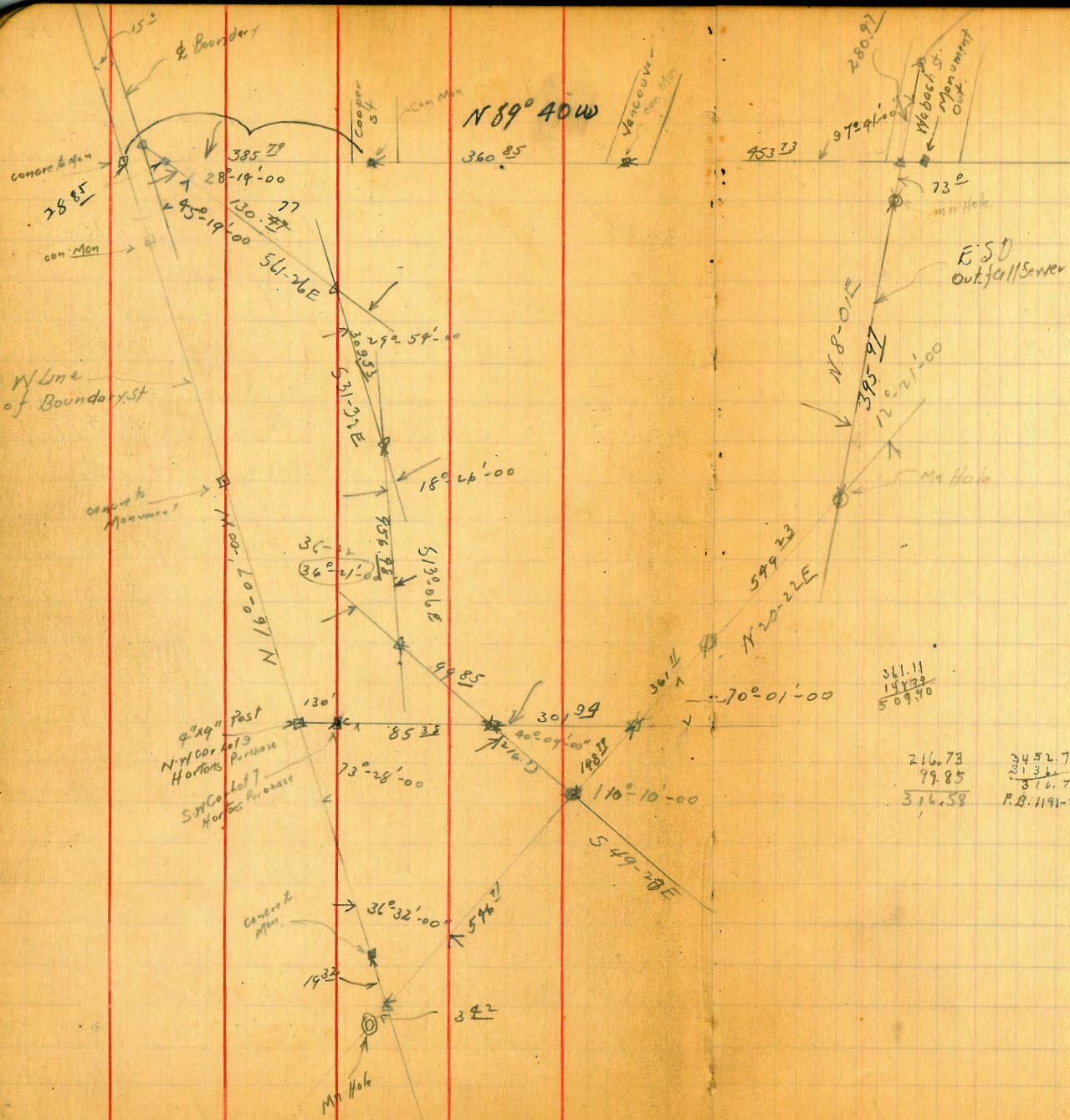


Levels to Determine Elevation of Plumbing
in existing Residences of Montclair

	#2	Elev
B.M. Mon Vancouver Standard Pacific S.	5.66	268.49
Residence Lot West Side bar	4.6	263.38
T.P.	8.35	271.60
T.P.	10.97	270.18
Residence S. Side Vancouver	13.13	257.05
Residence N. Side	1.96	682.2
T.P.	7.75	277.70
TWO Green Residence W. Side of Madison	3.05	74.65
T.P.	7.33	283.32
Residence Lots 34 & 35	6.36	76.96
Residence Lots 36 & 37	5.13	78.19
T.P.	3.12	283.90
Residence West Side Cooper House	3.55	80.35
Residence Block N. Lot 5 N. Half	4.55	72.35
T.P.	0.82	271.63
Residence Block W	2.20	69.43
T.P.	6.79	270.93
Res	0.95	69.98
T.P.	2.68	261.15
Residence Block W. Side Cooper	7.32	253.83
T.P.	2.98	260.69
Residence W. Side Cooper Lot 19 - Block "N"	6.21	254.43
T.P.	12.4	298.83
check on Mon	12.62	136.21

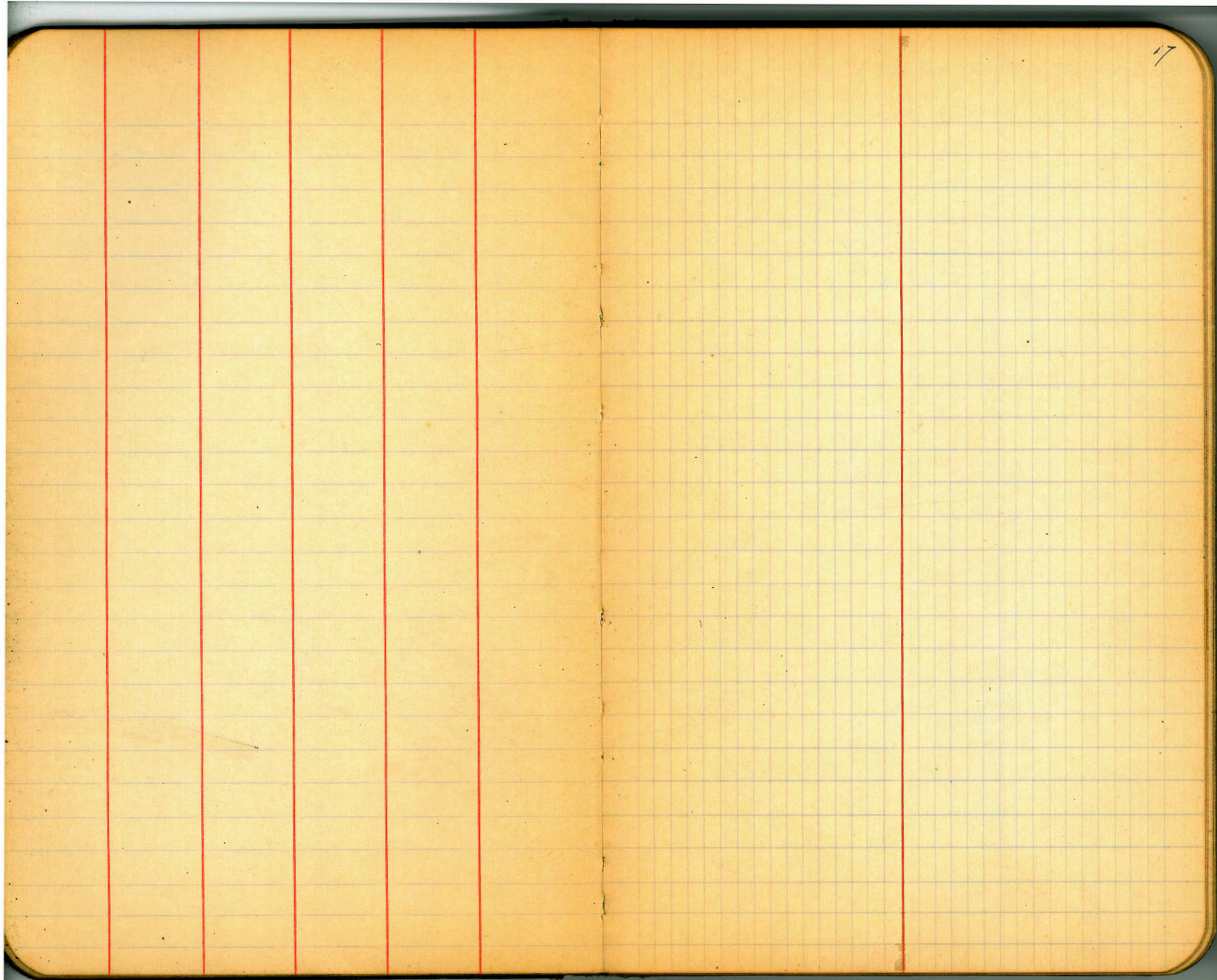
B.M. & Haller's Map

4.44	280.11	275.67
Residence Lot 6 Block R.	7.10	273.01
B.M. & Boundary Kalmia	0.35	279.27
Residence Block 9	5.50	273.77



Corrected Traverse
 South of Montclair + 9th
 Standard Parallel South
 To Tie up Sewer outfall

361.11	
147.23	
509.90	
216.73	3452.7
99.85	213.2
316.58	316.7
	P.B. 1191-20



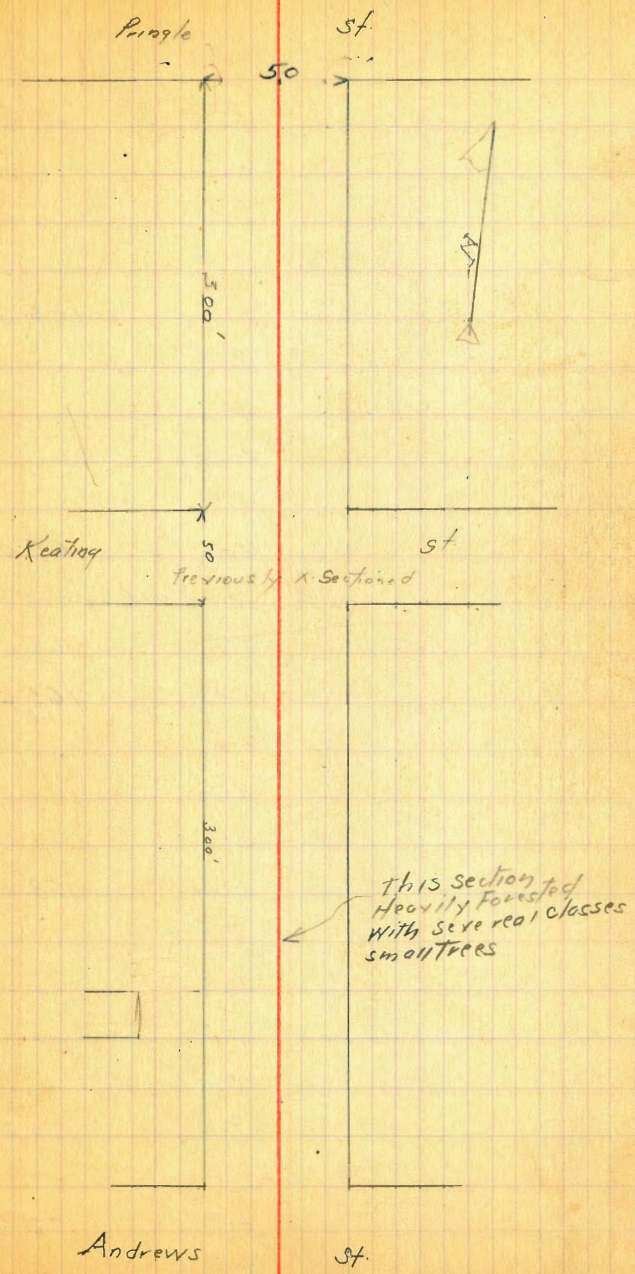
W.E. Bliss
Ducmit
Jacobson
Kier 1929
12/4/28

X Sections of Linwood Street from
the S. Line of Pingle to the North
Line of Andrews

50 St
10 cbs
25 ft

	+	H.I	-	Elev
8W SW Top of Pingle + Guy	0.23	198.10		197.87
T.P.	0.95	186.12	12.93	185.67
T.P.	3.12	176.27	12.97	173.15
		0400		
E		on paving		82
Top 6		887		167.40
Gutter		7.63		
1/4		10.10		
1/2		10.86		165.41
3/4		11.90		
Gutter		13.10		
W top 6		12.65		169.62
W		12.6		
		0402		
W		11.7		164.6
7~		12.4		
6b		11.8		
1/4		11.6		
1/2		10.6		165.7
3/4		9.7		
76.5		9.0		
6b		8.5		
E		5.6		170.7

Plotted Jan. 9-29 C.B.H.



HI
17627

0110

E	5.2	171.1
cb	6.1	
t2	8.0	
1/4	8.4	
£	9.4	166.9
1/4	9.7	
cb	10.1	
t3	11.2	
t8	11.7	
W	11.3	165.0

0123. Waikona West

£. 11.19 165.08

0125 11.1 165.2

t7	10.8	
cb	9.3	
1/4	8.8	
£	8.2	168.1
1/4	7.6	
cb	6.6	
t09	5.9	
t05	5.3	
£	4.6	171.7

0150

E	3.9	172.4
t03	4.9	

HI
17627

19

t08

5.6		
cb	6.2	
1/4	7.0	
£	7.8	168.5
1/4	8.4	
cb	8.6	
t09	10.8	
W	10.8	165.5

0175

W	10.6	165.7
---	------	-------

t05

t08

10.5		
8.8		
cb	8.5	
1/4	8.1	
£	7.5	168.8
1/4	6.6	
cb	5.7	
t06	5.1	
E	4.2	172.1

T.P. 470

173.38 7.59

168.68

1100

E	2.0	171.4
---	-----	-------

cb	3.0
----	-----

t09	3.5
-----	-----

t06	3.9
-----	-----

1/4	4.0
-----	-----

HZ
17338

2	4.8	168.6
1/4	5.2	
+6	5.4	
cb	5.6	
+2	5.8	
+4	7.1	
W	7.3	166.1
	1410	
W	7.4	166.0
+6	7.0	
17	6.4	
cb	5.7	
1/4	5.6	
2	5.0	168.4
1/4	4.4	
cb	3.7	
E	2.9	171.0
	1425	
E	4.2	169.2
cb	5.0	
1/4	5.3	
2	5.7	167.7
1/4	5.4	
cb	6.6	
+3	6.8	
+2	7.3	

HZ
17338

20

W	7.5	165.9
	1412 Walk on West	
	1 st BACK	7.57 ✓ 165.81
	1453	
W	8.6	164.8
cb.	8.4	
1/4	7.8	
2	7.4	166.0
1/4	7.2	
cb.	6.9	
E	6.3	167.1
E-1	^{TOP} 5.9	168.24
	1462	
E on edge concrete	9.07	164.31
cb	8.9	
+6	8.5	
1/4	7.9	
2	7.7	165.7
1/4	8.2	
cb	8.7	
W	9.2	164.2
	1481	
W	10.2	163.2
cb	9.8	
1/4	9.7	
2	9.7	163.7

H.I.
17338

1/4		9.9	
06		10.0	
E. Sedge Truss - Garage Concrete Apron		9.17	↓ 164.21
	1490		
E. Top Rubble Wall		9.9	164.0
E on Ground		10.7	162.7
+5		10.8	
+8		11.5	
06		11.3	
1/4		11.5	
ϕ		11.9	162.0
1/4		11.~	
+5		11.8	
06		11.3	
+3.		11.0	
N		11.5	161.9
	2100		
Top Rubble Wall on East		9.9	163.5
TP	1.29	12.61	160.77 161.17
N		1.6	160.5
06		1.6	
1/4		1.3	
+4		2.2	
ϕ		2.2	159.9
1/4		2.4	
06		2.9	

H.I.
16206

+22 4.3

24

+3		3.2	
+9		3.7	
E on Ground		3.6	158.5
E Top Rubble Wall		2.~	159.9
	218		
E Top Wall		4.1	158.0
E on Ground		7.2	154.9
06		7.0	
+2		7.0	
+6		6.2	
1/4		6.3	
ϕ		6.4	155.7
+5		6.4	
1/4		5.9	
06		5.0	
N		4.3	157.8
	2125		
N		5.5	156.6
06		6.7	
1/4		7.2	
ϕ		7.3	154.8
1/4		7.6	
06		7.7	
+7		8.7	
E		8.6	153.5

H.I
16206

2431

E	9.0	1531
+3	9.0	
cb	8.5	
1/4	8.1	
ϕ	7.9	1542
1/4	7.9	
ob	7.0	
W	6.2	1559

2445

W	8.6	1535
cb	9.1	
1/4	9.1	
ϕ	9.2	152.9
+6	9.3	
1/4	10.3	
+3	11.6	
ob	11.4	
7~	11.5	
+4	12.4	
E on Ground	12.7	149.4
E Top Rubble Wall	9.6	152.5

2450

Top Rubble Wall	9.8	152.3
Bottom Wall	13.3	148.8
E on Ground	13.9	148.2

H.I
16208

22

+6	13.4	
cb	12.0	
1/4	11.6	
+3	9.6	
ϕ	9.6	152.5
1/4	9.6	
cb	9.8	
W	10.1	152.0

2457

W	11.8	150.3
+7	16.7	
cb	10.7	
1/4	10.7	
ϕ	10.7	151.4
+2	11.5	
+3	13.2	
1/4	13.2	
+4	13.2	
cb	13.3	
+2	14.6	
+3	15.8	
E	15.5	146.6
E Top Wall	14.9	147.2

2462

E Top Wall	16.2	145.9
E	16.8	145.3

H.I
162.06

+7		17.2	
+8		16.5	
cb		15.6	
1/4		14.3	
ϕ		17.5	147.6
+2		14.4	
+4		12.2	
1/4		12.6	
cb		12.9	
+6		11.8	
W		11.8	150.3
TP.	082	149.80	13.08
		2467	148.98
W		2.7	147.1
cb		2.6	
+5		3.0	
1/4		3.8	
ϕ		3.1	146.7
+1		2.8	
+5		4.0	
1/4		4.4	
+6		5.1	
cb		5.6	
+3		6.5	
E		6.5	143.3

H.I
199.80

23

		2775	
E. Top Wall		7.2	142.6
E		8.0	141.8 ✓
+8		8.1	
+9		7.4	
cb		7.2	
1/4		6.8	
ϕ		5.9	143.9
1/4		5.0	
cb		5.2	
+2		4.6	
W		7.0	145.8
		2786	
W		7.1	142.7
cb		8.1	
1/4		8.3	
ϕ		8.6	141.2
1/4		9.2	
cb		10.0	
E on Ground		10.1	139.7
E on Top Wall		8.8	141.0
		2795 End Wall on East	
		9.7	139.9 ✓
		3400	
E		12.1	137.7
cb		12.4	

HI
14980

HI
12412

29

1/4			120	
ϕ			11.9	137.9
1/4			11.5	
cb			11.6	
+8			11.0	
W			11.2	1386
TP	0.31	137.06	13.05	136.75
		0+00 S-Line Keating		
E-10			11.8	
E			11.5	125.6
cb			11.7	125.4 ✓
+5			11.2	
1/4			11.0	
ϕ			10.9	126.2
1/4			11.1	
cb			10.6	
W			10.0	127.1
TP	0.14	129.12	13.08	123.98
		0+15		
W			0.3	123.8
cb			0.9	
1/4			1.2	
ϕ			1.1	123.0
1/4			1.4	
cb			2.3	121.8 ✓
+5			2.1	

E			2.9	121.7
E+10			3.2	
		0+25		
E-10			6.0	
E			4.4	119.7
+5			4.9	
cb			4.7	119.4 ✓
1/4			4.1	
ϕ			4.0	120.1
+2			3.6	
1/4			3.4	
cb			3.5	
W			3.2	120.9
		0+30 Beginning concrete wall on West		
		on line	4.26	119.86
		0+32		
W			4.7	119.4
cb			4.8	
1/4			5.1	
ϕ			5.8	118.3
1/4			6.5	
cb			7.3	116.8 ✓
E			7.4	116.7
E+10			8.3	
		0+44 End wall on West		
		TOP	4.29	119.86
		BOTTOM	7.8	116.3

HI
129.12

HI
111.18

25

5⁰ End
Porch
11⁰ East

		0145		E	5.4	105.8
E-10		1.8		cb	5.5	105.7 ✓
E		11.5	112.6	1/4	5.6	
cb		11.1	113.0 ✓	1/4	5.6	105.6
+3		11.2		1/4	5.1	
1/4		10.1		cb	5.1	
1/4		9.6	114.5	1/4	5.3	105.9
1/4		8.9				
cb		8.6		Top	3.80	107.38
1/4		8.3	115.8	Bottom	5.79	105.39
TP	0.06	111.18	111.12		0187	
		0165		1/4	7.8	103.4
1/4		1.7	109.5	cb	7.5	
cb		1.8		1/4	7.7	
1/4		2.5		1/4	8.0	103.2
+5		3.2		cb	7.9	
1/4		3.1	108.1	1/4	7.6	103.6
+3		2.8		1/4	7.6	
1/4		3.2		+7	8.2	
cb		3.4	107.8	E	8.4	102.8
E		3.3	107.9	E+10	8.4	
E+10		3.2				
		0167	Burning Wall	3 rd Back Floor	4.95	106.23
	Top	3.75	107.43		1100	
		0175		E-10	11.1	
E-10		5.3		E	11.0	100.2

H.I.
11/18

109.77

26

cb		11.3	99.9 ✓
+2		11.8	
+6		9.9	
1/4		10.0	
⊕		10.4	100.8
+2		10.5	
1/4		9.3	
+2		9.7	
cb		9.9	
W		10.6	100.6
Top End of Wall on West		5.88	105.30 ✓
TP	415	109.77	105.6 100.62
North End of Residence for Residence on East ^{Two} story			
Porch 5' Back	Ground at Bottom steps	4.33	100.44 ✓
Main Residence	11' Back Top	0.90	103.87 ✓
		11.15	
W-10		8.0	
W		7.9	96.9
+3		8.1	
+6		8.3	
cb		7.9	
1/4		7.5	
+2		9.7	
+4		9.0	
⊕		8.7	96.1
+4		7.8	

1/4		7.9	
cb		8.0	96.8 ✓
East		8.1	96.7
Entrance to Residence	Bottom 11' 2' story Back.	8.0	96.8
11-3 South End of Residence			
Floor Elev. Top floor		0.90	103.87
Bottom Floor		8.0	96.8 ✓
		11.20	
⊕		9.9	95.4
cb		10.2	93.6 ✓
+4		10.2	
1/4		10.5	
⊕		10.8	94.0
+1		10.6	
+4		9.8	
1/4		10.3	
+3		11.2	
+5		9.6	
cb		9.7	
+2		9.9	
+5		9.8	
W		8.7	96.1
W+15		9.1	
TP	1.94	94.24	12.47 92.50
		11.35	
W-35		8.6	

H.I.
9424

H.I.
9429

27

W-15	6.9	
W	6.1	88.1
+2	5.1	
+9	4.6	
cb.	5.5	
1/4	5.5	
E	5.3	88.9
1/4	5.0	
cb	4.7	87.8 ✓
+4	4.0	
+6	4.5	
+9	8.8	
E	9.0	85.2
Bottom channel		
+15	8.5	
+25	7.0	
1+98		
E-25	5.5	
E-15	5.2	
E	6.6	87.6
+1 Top	6.6	
+1 Bottom	8.4	
+5	9.0	
cb	10.1	84.7 ✓
+3	10.0	
+9	5.5	
1/4	5.9	

2	5.5	88.7
1/4	5.9	
cb	6.3	
+6	7.5	
W	7.0	87.2
W+15	8.7	
W+25	9.9	
1+53		
T.P. 4.2	91.24	7.2 87.04
W-25	8.3	
-15	6.7	
W	5.6	85.6
+6	4.9	
+7	5.5	
cb	5.5	
1/4	5.7	
Q	4.6	86.6
+1	4.1	
1/4	3.5	
+2	3.3	
+5	4.2	
+6	7.1	
cb	7.3	83.9
+2	7.2	
E	4.3	86.9
+1	3.8	

7P 7.2 9929 4.2 87.04
 E+15 6.5
 E+25 6.2
 1+68
 E-25 6.5
 E-15 7.9
 E-1 7.1
 E 11.1 83.1
 +8 10.0
 cb 7.5 87.7 ✓
 1/4 7.5
 +2 8.1
 φ 8.7 85.5
 1/4 8.8
 cb 9.0
 W 9.2 85.0
 +15 10.3
 +25 11.2
 1+70
 W-25 10.9
 W-15 10.3
 W 10.1 84.1
 cb 9.2
 1/4 9.0
 φ 8.6 85.6
 1/4 7.8

+4 7.6
 cb 8.5 86.7
 +2 10.2
 +7 11.7
 +9 7.3
 E 6.7 87.5
 1+73
 E 6.7 87.5
 +1 7.3
 +4 11.5
 cb 10.7 84.5
 1/4 10.9
 +.55 11.2
 φ Top Mt Hope 9.1 85.1
 +2 12.2
 1/4 12.7
 cb 12.6
 W 13.0 81.2
 +15 13.9
 +25 13.7
 1+80
 W-25 12.1
 W-15 11.4
 W 11.9 82.3
 cb 11.7
 1/4 11.5

HI
93.94

HI
93.94

29

ϕ	11.6	82.6
1/4	11.6	
ϕ6	11.1	
+4	10.5	
E	8.2	86.0
+3	7.3	
+15	6.9	
+25	6.5	
1184		
E-25	6.5	
E-15	7.0	
E-3	7.3	
E	8.1	86.1
+5	9.8	
ϕ6	9.7	
1/4	9.7	
ϕ	9.3	84.9
1/4	9.5	
ϕ6	10.6	
W	11.0	83.2
W+10	10.6	
+15	10.0	
+25	9.8	
T.P.	8.85	93.94
North End	2703	Residence on West.
W-25	9.9	

W-5 Top Wall House	7.9	86.0
W-23.5 Top Wall		
23.5 Top Wall	6.3	87.6
W-15	6.3	
W-85 Top Wall	6.7	
V-5	8.0	
W-95 Top Wall	6.4	
W.	6.7	87.2
+3	6.7	76 15 91
+4	7.7	
ϕ6	7.9	
+9 Top of crest 18" Amco	7.2	
Floor Line	9.1	
1/4	8.4	
+5	10.0	
ϕ	10.6	83.3
1/4	10.3	
ϕ6	8.9	
+5	7.8	
+7	6.6	
E	6.5	87.4
E+15	5.3	
+25	4.2	
2+		
T-25	1.3	?
E-15	2.3	

HZ
93.94

103

267.100

1723

HZ
103.68

30

93.94
267
91.27

E	4.1	89.8
+7	3.4	
+8	6.8	
cb	7.2	
+5	8.4	
+6	5.3	
1/4	5.8	
Φ	5.4	88.5
1/4	5.7	
+5	5.7	
cb	5.2	
N	5.5	88.4
W+15	5.5	
W+15 floor Residence	2.9	
	2.20	
W-15	2.8	
N	2.3	91.6
+5	2.2	
+6	0.8	
cb	1.4	
1/4	1.2	
Φ	1.0	92.9
+5	0.6	
1/4	1.2	
+1	0.9	
T.P.	10.30	103.68
	0.56	93.38

+4	9.2
+7	9.3
cb	10.5
+7	10.2
E	8.3
E+15	7.7
+25	5.8
	2+23 Walk on West
online	12.37
	2+30
E-25	2.3
E-15	2.4
E	3.7
cb	5.2
1/4	6.2
Φ	6.9
1/4	7.8
cb	9.0
+6	10.2
N	11.7
W+15 Porch	12.0
W+25 House	12.1
	2+35
W-25	5.6
W-3	5.2
N	8.2

95.4
91.31
100.0
96.8
92.0
91.7
91.6
95.5

HI
10368

cb		7.9	
+5		7.2	
1/4		6.7	
E		5.9	97.8
1/4		4.8	
cb		3.4	
+5		2.7	
+6		1.9	
E		1.7	102.0
E+15		0.2	
TP	9.86	113.26	0.28 103.90
		2145	
E-15		5.3	
E-4		8.1	
E		8.7	104.6
cb		9.9	
1/4		11.2	
E		13.0	100.3
+4		12.9	
1/4		14.2	
cb		14.3	
+6		15.4	
W		14.9	98.4
+1		14.9	
+2		12.9	
+15		13.0	

+

HI
113.26

Klev 31

TP	7.68	116.96	4.48	108.78
		2160		
N-15			13.0	
N			14.7	101.8
1/4			12.1	
cb			10.6	
1/4			9.7	
E			8.7	107.8
+4			7.0	
1/4			6.3	
+3			6.2	
+6			6.9	
cb			6.8	
+5			5.3	
E			4.3	112.2
+10			0.8	
TP	7.27	122.01	1.72	114.74
		2170		
E-10			1.5	
E			3.3	118.7
+5			4.5	
cb			5.8	
+5			8.0	
1/4			8.3	
+6			8.0	
E			8.5	113.5
1/4			4.0	

HZ
122.01

cb			11.8	
+3			12.8	
+6			14.4	
N			14.9	107.1
+15			14.8	
			2480	
N-15			12.2	
-7			12.9	
N			11.8	110.2
+5			9.1	
cb			6.7	
+4			5.3	
1/4			4.9	
+4			4.0	
ϕ			2.0	120.0
1/4			1.3	
T.P.	6.70	127.76	0.95	121.06
cb			5.8	
E			5.2	122.6
+10			4.8	
			+90	
B-10			5.0	
E			4.7	123.1
cb			4.1	
+5			3.8	
1/4			4.0	

HZ
127.76

32

ϕ			4.7	123.1
1/4			5.2	
+3			5.4	
cb			6.8	
+5			9.2	
N			11.4	116.4
+3			13.1	
+10			16.2	
+15			17.1	
+25			17.1	
			3400	North line of Andrews
N-15			10.5	
-2			8.0	
N			8.1	119.7
+3			7.7	
+4			5.7	
+6			4.9	
cb			4.8	
1/4			3.7	
ϕ			3.3	124.4
1/4			3.1	
cb			2.8	
+5			2.9	
E			3.5	124.3
T.P.	13.05	139.37	1.44	126.32
T.P.	12.69	151.75	0.31	139.06
T.P.	11.72	163.20	0.27	151.48
			3.88	157.32

Set 3/11 12 Pole NW Cor. Andrews St. Guy

W.B.H.S.
Dermid
Jacobson
Kiernan
1948
B.M.S.W. Top 4y
Guy's Pringle

X Sections of Guy Street from the
S. line of Pringle to N. line of Andrews
446 202.33 19787 50' St
10' obs
7.5/9

See sketch
page 90

Plotted Jan 9-29- CBH

Station	0100	19787	0100	Station	1984
E	3.50	198.83	+	3.9	1984
W Top cb	3.76	198.57	cb	9.8	
G	4.59		W	4.9	
1/4	4.80		+10	5.6	
W 1/4	5.31	197.02		7.1	195.2
1/4	6.05		W-15	8.7	
G	7.12		W	0140	
W Top cb	6.67	195.66	cb	9.5	
W	6.58		1/4	7.8	194.5
W	6.6	195.7	1/4	6.5	
cb	6.1		E	5.6	
1/4	5.7		E	4.7	197.6
1/4	4.9	197.4	cb	3.8	
1/4	4.1		E	2.9	
cb	3.6		E	1.6	200.7
cb	2.6		0160	3.9	198.9
cb	2.1		cb	4.4	
E	0.9	201.4	cb	5.2	
E	0.7		1/4	6.1	196.2
EE	0.5	201.8	1/4	6.8	
cb	1.1		cb	7.6	
cb	1.9		cb	8.7	193.6
1/4	3.0		W	10.2	
			+15	0175	
			W-15	11.8	

+

HZ
20233

-

E/ev

39

W	10.0	192.3
cb	8.6	
1/4	7.5	
⊕	6.6	195.7
1/4	5.8	
cb	5.3	
E.	4.6	197.7
	of 90	
E	6.0	196.3
cb	7.0	
1/4	7.5	
⊕	8.3	194.0
1/4	9.1	
cb	10.0	
W	11.1	191.2
+15	13.0	
	14.0	
W-15	14.2	
W	12.6	189.7
cb	11.5	
1/4	10.8	
⊕	10.1	192.2
1/4	9.2	
cb	8.5	
E	7.6	194.7

+

HZ
20233

-

E/ev

1110

E-10	10.3		
E	10.4	191.9	
+4	10.2		
cb	11.4		
+4	11.8		
1/4	11.7		
⊕	12.2	190.1	
+3	12.5		
+5	13.2		
1/4	14.0		
T.P. 2.84	192.09	13.13	189.20
cb	3.7		
+2	3.2		
W	3.9	188.1	
W+15	5.1		
	14.20		
W-15	6.7		
W	5.9	186.1	
cb	5.6		
1/4	5.4		
⊕	4.8	187.2	
1/4	4.4		
cb	4.2		
+4	4.3		
E	3.2	188.8	

HI
19200

HI
19200

35

E+10	2.7		
	1x+28		
E-10	4.7		
E	5.1	186.9	
+6	6.8		
cb	8.0		
1/4	7.6		
ϕ	8.4	183.6	
+9	8.0		
1/4	8.3		
cb	9.0		
W	9.1	182.9	
W+15	9.6		
	1x+32 - North End Residence on East		
W-15	10.8		
W	10.3	181.7	
cb	9.7		
1/4	9.3		
ϕ	9.1	182.9	
1/4	8.8		
cb	8.2		
E	7.8	184.2	
+10	7.9		
+19	6.4	185.6 ✓	
+23	9.0	188.0 ✓	

Bottom Hood in Steps
Entrance
House Floor on North Side

	12+38		
E-10	7.7		
E	8.0		184.0
+6	8.3		
+7	9.6		
cb	10.9		
+5	10.8		
1/4	10.5		
+5	10.3		
ϕ	10.0		182.0
1/4	11.4		
cb	11.7		
W	12.2		179.8
+15	12.9		
	12+45		
W-15	15.2		
W	14.2		177.8
cb	13.7		
1/4	13.2		
E	13.3		178.7
1/4	13.2		
+4	13.4		
cb	12.1		
+6	11.7		
+8	8.8		
E	8.5		183.5

HI
192.04

HI
180.30

36

+10	77		
	1754	Tree	
E-10	88		
E	10.1	181.9	
+1	13.9		
cb	15.3		
+2	16.2		
1/4 + 1 Tree	16.3		
+3	16.4		
⊕	16.4	1756	
1/4	16.9		
cb	17.5		
W	18.7	173.3	
W+15	19.0		
	1757		
W-15	19.0		
W	19.2	172.8	
cb	18.7		
1/4	18.4		
⊕	18.1	173.9	
1/4	17.7		
cb	16.9		
+8	15.1		
E	12.7	179.3	
E+10	1.4		
T.P.	118	180.30	12.92
			179.12

	1764		
E-10	45		
E	47	1756	
+1	53		
cb	65		
1/4	7.3		
⊕	7.4	1729	
+5	7.5		
1/4	8.4		
+4	8.6		
cb	8.2		
W	8.1	1722	
+15	8.1		
	1775		
W-15	12.9		
W	11.8	1685	
cb	11.4		
1/4	11.6		
⊕	11.2	169.1	
1/4	10.5		
cb	10.2		
+9	9.7		
E	8.3	1720	
+10	8.2		
	1789		
E-10	11.0		

H.I.
180.30

E		11.4	168.9
+1		12.2	
cb		13.2	
T.P.	1.24	168.74	12.80
1/4		2.0	167.50
E		2.7	166.0
1/4		2.7	
cb		3.0	
W		3.6	165.1
+15		4.4	
		2100	
W-15		4.3	
W		5.8	162.9
cb		6.1	
1/4		5.9	
E		6.1	162.6
1/4		5.3	
cb		4.7	
E		4.1	164.6
+10		4.0	
		2108	
-10		5.7	
E		6.2	162.5
cb		6.7	
1/4		7.2	
E		7.8	160.9

H.I.
168.74

37

1/4		8.7	
cb		8.9	
W		9.9	158.8
+15		11.0	
		2119	
W-15		12.1	
W		11.6	157.1
cb		11.0	
1/4		10.7	
E		9.9	158.8
1/4		9.4	
cb		9.3	
E		8.8	159.9
+10		8.3	
		2123	
-10		9.4	
E		9.5	159.2
cb		10.0	
1/4		10.5	
+1		11.3	
E		12.2	156.5
+7		12.8	
1/4		11.7	
cb		12.1	
W		13.3	155.4
+15		19.6	

H.I.
16874H.I.
15711

38

T.P. 066 157.11 12.29 156.45

2450

W-15

2434

W-15

7.1

3.3

W

6.5

150.6

W

2.7

154.4

Cb

5.7

Cb

3.4

1/4

5.0

1/4

2.9

+3

4.5

E

2.2

154.9

E

4.6

152.5

1/4

1.8

1/4

4.3

+6

0.2

Cb

3.9

Cb

0.2

E

3.4

153.7

E

0.1

157.0

+10

2.8

+10

0.0

2467

2437

-10

6.0

-10

0.5

E

6.8

150.3

E

1.1

156.0

Cb

7.5

Cb

1.4

1/4

7.8

+1

1.5

E

8.2

148.9

1/4

2.6

1/4

8.4

E

3.1

154.0

Cb

8.9

+5

3.8

W.

9.7

147.4

1/4

3.8

+15

10.3

+4

3.6

2475

Cb

3.5

-15

11.8

W

4.7

152.4

W

12.3

144.8

+15

5.3

+9

12.5

Cb

11.1

H.I.
15711

1/4		10.6	
2		10.0	147.1
1/4		9.6	
06		9.2	
E		8.7	148.4
+10		8.4	
		2785	
-10		11.1	
E		11.6	145.5
06		12.0	
1/4		12.5	
+1		13.2	
+9	2.23	146.97	12.37
2		3.5	143.5
1/4		3.1	
06		3.0	
+5		3.0	
N		3.9	143.6
+15		2.7	
		2792	
-15		4.9	
-4		5.0	
N		5.9	141.1
06		5.0	
1/4		3.9	
+5		2.9	

H.I.
14697

39

2		3.0	144.0
+1		3.6	
1/4		3.9	
06		4.4	
+2		4.6	
+7		4.1	
+9		3.1	
E		3.1	143.9
+10		2.3	
		3100 N Line Keating	
-10		6.0	
E		5.6	141.4
+7		4.7	
1/4		4.9	
+3		5.7	
1/4		6.4	
2		6.5	140.5
1/4		7.1	
06		7.7	
W		8.7	138.3
+15		8.2	
		Keating X sectioned	
		13619	1234
			139.63
		Sline Keating = 00	
		9.0	
		8.9	127.8

TP. 156
N-15
N

H.I.
13619

40

06		8.0	
1/4		7.9	
ϕ		7.9	1283
1/4		8.0	
06		8.3	
E		8.5	127.7
+15		8.8	
	0+09		
-15		11.2	
E		11.5	124.7
06		11.3	
1/4		11.1	
ϕ		11.1	125.1
1/4		11.0	
06		11.0	
W		11.1	125.1
+15		11.3	
TP	0.60	124.21	125.2
		0+25	123.61
-15		2.9	
W		3.2	121.0
06		3.8	
1/4		3.7	
ϕ		4.0	120.2
1/4		4.0	
06		3.8	

Pringle

Street

300'

G.V. St.

Keating

g Street

300'

0+53

75'

0+74

0+182

0+288

0+295

75'

4 Trees 75' off center

Andrews

St

H.I.
129.2

E	3.8	120.4
+15	3.8	
	0+40	
E-15	8.5	
E	9.1	115.1
cb	9.0	
1/4	8.6	
ϕ	8.3	115.9
1/4	7.9	
cb	7.3	
N	6.8	117.4
+15	6.7	
	0+46	
-15	8.7	
N	8.8	115.4
+3	8.9	
+5	9.8	
cb	10.0	
1/4	10.6	
+3	10.2	
+5	10.2	
ϕ	11.1	113.1
1/4	12.0	
cb	12.9	
E	12.9	111.0
+7	11.9	

H.I.
129.2

41

+15	10.7	
	Residence 19 ^o Base	
	0+53 Concrete Wall *North End Res ✓	
	12.7	
	-8	14.4
E	15.2	109.0
+5	14.8	
cb	14.7	
1/4	14.2	
ϕ	14.0	110.2
1/4	13.3	
cb	12.8	
N on Top Wall	10.56	113.65
W on Ground	11.5	112.7
+19 Edge House	10.9	113.3
	0+55 Walk on West	
	ϕ 2 ^o 14 street ^{Walk 8^o wide}	11.99
	0+61 Rubble wall on West	1127.2 ✓
W-15	11.6	
N Top Rubble Wall	11.8	112.4
+7	12.2	
cb	13.7	
1/4	14.3	
ϕ	15.0	109.2
+2	16.1	
1/4	16.7	
cb	17.6	

H.I.
12421

111.62

42

E		17.7	106.5
E+7		17.0	
+15		16.6	
E25		15.9	
T.P.	0.58	111.62	111.04

0763

E-LS		3.5	
E		5.9	105.7
+5		5.6	
cb		5.5	
+5		6.0	
1/4		6.5	
1/4		6.5	105.1
1/4		5.8	
cb		6.0	
W		6.2	105.4
+13	Edge concrete steps	6.0	105.6

0772 S. End of Residence

19° Back Foundation

		4.7	106.9
		0780	
W-20		9.2	
W		9.2	102.0
+7 Top		9.7	
+7 Bottom		10.6	
cb		10.5	
1/9		10.9	

1/4		10.9	100.7
1/4		11.1	
cb		11.5	
E		11.0	100.6
E+2		9.5	
E+25		8.4	

0784

E-25		8.7	
-7		9.8	
-6		10.9	
E		11.6	100.0
cb		12.2	
1/4		12.0	
+4		11.7	
E		11.2	100.4
1/4		11.2	
+1		12.4	
cb		13.3	
+1 Bottom Rubble wall		13.3	
+1 Top " "		10.0	101.6
W		9.7	101.9
+25		10.2	
		0785	
W-25		15.1	
W		13.5	98.1
cb		13.3	

H.I.
111.62

1/4			12.9	
1/2			13.2	98.4
1/4			13.1	
cb			12.9	
E			11.9	99.7
+25			9.3	
TP	3.38	104.38	10.62	101.00
			+9.5	
E-25			3.1	
E-1			4.9	
E			5.9	98.5
cb			6.3	
1/4			6.5	
1/2			6.6	97.8
1/4			7.4	
cb			7.5	
W			7.6	96.8
W+25			9.2	
			+9.8	
W-25			9.7	
W.			8.0	96.4
cb Top			8.0	
cb Bottom			10.9	
1/4			10.9	
1/2			10.0	94.4
1/4			9.1	

H.I.
109.38

43

cb			7.2	
1/2			6.5	97.9
+2			5.2	
+22			3.6	
			17.00	
E-22			3.7	
-3			5.3	
E			6.6	97.8
cb			7.9	
1/4			10.6	
1/2			10.9	93.5
1/4			11.5	
cb			11.5	
W			11.3	93.1
+10			11.6	
+11			9.4	
+25			9.8	
			17.09	
-25			10.2	
-23			12.0	
W			12.1	92.3
cb			11.8	
1/4			11.3	
1/2			10.3	94.1
1/4			10.1	
cb			9.6	

HI.
10438

+5	81	
E	7.0	97.4
+5	5.6	
+22	9.8	
+25	7.8	
+32	7.8	
	1+06	
E	7.0	97.4
cb	9.5	
1/4	10.0	
E. Ma. Hole	8.8	95.6
	Rim	
1/4	9.1	
cb	8.9	
W	8.9	95.5
+7 Top Well	9.4	
+8 Bottom	12.0	
+24	12.1	
+25	10.5	
	1+18	
W-25	9.9	
X	7.9	97.0
cb	7.2	
1/4	7.1	
+3	7.1	
+9	6.5	
4	6.3	98.1

HI.
10438

94

1/4	6.8	
+1	8.6	
cb	9.1	
+7	8.8	
+8	7.8	
E	7.5	96.9
+7	7.1	
+8	8.6	
+14	8.6	Bottom channel
+25	7.1	
+30	6.3	
	1+23	Bottom
E-30	5.8	
-18	7.6	
-17	8.2	
-13	8.3	
E	8.9	95.5
+9	9.4	
+5	7.9	
cb	8.9	
+6	8.5	
1/4	6.6	
E	5.3	99.1
+2	5.9	
1/4	6.3	
cb	6.6	

H.I.
104.38

N	6.8	97.6
+25	9.3	
	1+27	
-25	8.8	
N	6.3	98.1
cb	6.2	
1/4	5.9	
+1	4.4	
+3	3.5	
E	3.8	100.6
+5	5.4	
1/4	8.1	
+3	8.5	
cb	8.0	
E	7.3	97.1
+25	5.8	
	1+45	
-25	3.7	
-13	4.9	
-3	5.3	
-2	7.1	
E	7.1	97.3
cb	7.8	
+5	7.8	
1/4	4.9	
+2	3.7	

H.I.
104.38

46

E	3.9	101.0
1/4	2.8	
cb	3.1	
+3	3.1	
+5	3.8	
N	3.9	100.5
+25	5.1	
	1+50	
-25	4.8	
N	3.2	101.2
+2	2.3	
+5	2.2	
cb	1.4	
1/4	1.2	
E	0.5	103.9
+3	1.0	
1/4	3.3	
cb	4.6	
E	4.5	99.9
+14	4.2	
+25	1.8	
TR 11/12	119.07	102.95
	1+58	
-25	9.3	
-20	10.7	
E	11.6	102.5

H.I.
114.07

cb	10.2	
1/4	8.9	
1/4	9.2	104.9
1/4	9.6	
cb	10.0	
W	10.4	103.7
+25	11.8	
	1462	
-25	11.9	
W	10.2	103.9
cb	9.6	
1/4	9.4	
1/4	8.6	105.5
1/4	8.8	
cb	9.6	
E	10.6	103.5
+10	10.3	
+25	7.9	
	1468	
-25	4.8	
E	7.1	107.0
+7	6.4	
cb	6.4	
1/4	6.6	
1/4	7.4	106.7
1/4	8.2	

H.I.
114.07

47

cb	8.5	
W	9.2	104.9
+25	10.5	
	1483	
W-10	7.0	
W	6.0	108.1
cb	5.0	
1/4	4.0	
1/4	3.3	110.8
1/4	2.9	
cb	2.4	
E	1.7	112.4
+10	0.5	
J.P.	11.84	125.57
	0.34	113.73
	2400	
-10	6.8	
E	7.9	117.7
cb	8.3	
1/4	8.9	
1/4	9.2	116.4
+5	9.4	
1/4	9.8	
cb	11.0	
W	12.8	112.8
+10	14.0	

	+	HZ	-	E/ef
		125.57		
		2720		
-10			7.3	
W			6.9	119.2
cb			5.2	
1/4			4.0	
⊕			2.6	123.0
1/4			2.1	
cb			1.3	
E			1.0	124.6
+10			0.1	
TP	11.28	136.17	0.68	124.89
			2735	
-10			6.3	
E			7.0	129.2
cb			7.3	
+1			8.1	
1/4			8.2	
⊕			9.0	127.2
1/4			9.8	
cb			10.1	
W			11.1	125.1
+15			12.9	
			2749	
-75			7.8	
-5			6.9	
W			6.8	129.4
cb			6.6	

	+	HZ	-	Elev	48
		136.17			
+5			6.5		
1/4			5.5		
⊕			5.1	131.1	
1/4			4.3		
cb			3.7		
E			2.4	133.8	
+10			1.3		
TP	12.79	198.63	0.33	135.84	
			2753		
-10			9.9		
E			10.1	138.5	
cb			10.9		
1/4			11.5		
⊕			12.3	136.3	
1/4			13.7		
cb			14.0		
+5			14.1		
N			14.8	133.8	
+15			16.3		
			2768		
-15			11.1		
-10			10.3		
W			8.2	140.4	
cb			6.9		
1/4			6.8		
⊕			5.5	143.1	

	+	H.I. 14863	-	Elev
1/4			3.9	
cb			2.3	
E			2.0	146.6
T.P.	12.37	159.79	121	147.42
			2+77	
E			9.9	150.4
cb			10.2	
1/4			11.1	
E			12.9	147.4
1/4			13.1	
cb			13.5	
W			14.2	145.6
+3			14.5	
+15			17.6	
			2+81	
-15			15.1	
-6			14.0	
W			11.8	148.0
cb			10.0	
1/4			10.2	
+5			9.8	
E			9.0	150.8
1/4			8.5	
cb			7.4	
+7			6.9	
E			7.5	152.3

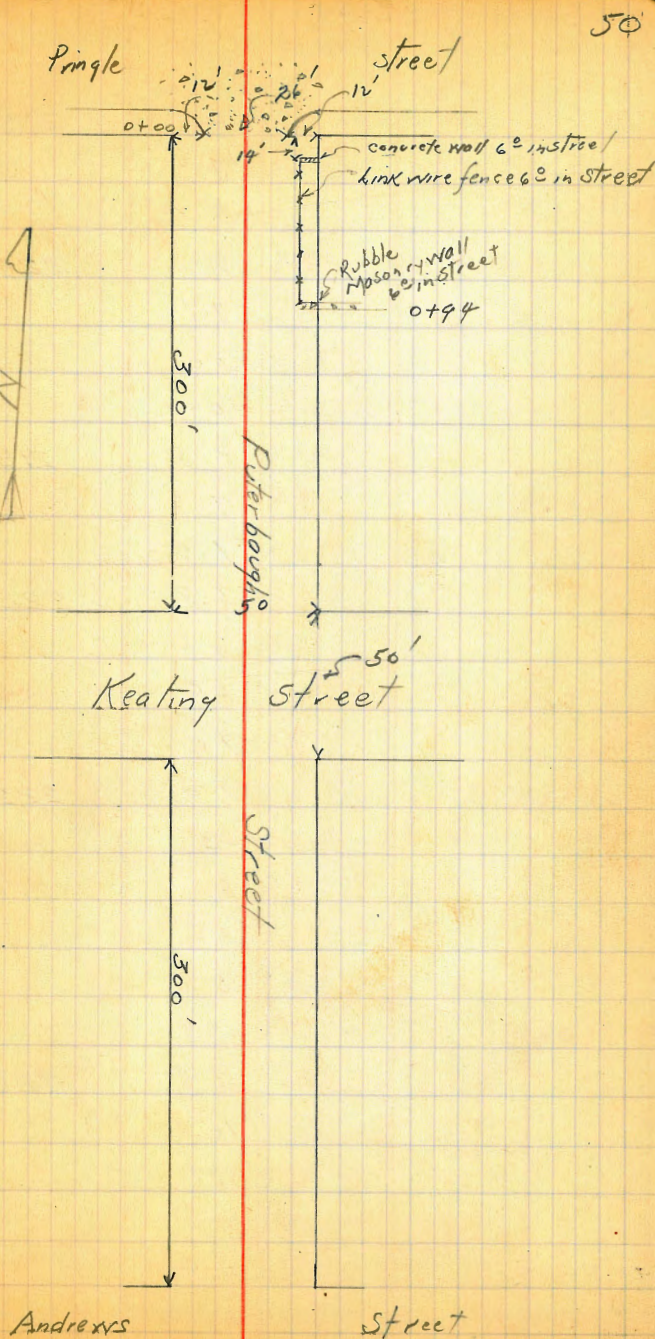
		H.I. 159.79			49
			2+91		
E			1.1		158.7
cb			1.8		
1/4			3.0		
E			3.6		156.2
1/4			4.6		
cb			5.2		
W			7.4		152.4
+15			10.0		
			3+00		
W-15			6.5		
W			4.0		155.8
cb			1.6		
1/4			0.3		
T.P.	9.55	168.85	0.99		159.30
E			8.7		160.1
1/4			8.2		
cb			7.2		
E			7.1		161.7
check out on BM ^{set} on section Wood			9.55		159.30
					158.30
					0.02

Bliss
Duermit
Jacobson
12/16/15

BMSW Top Hs
Terrance & Pringle

X-Section Peterbaugh from the Sline of Pringle to the Nline of Andrews				
	+	HZ	-	Elev
	0.50	237.77		237.27
				50.51
				12' cbs
				6.5.14 ²
TP	1.50	229.38	9.89	227.88
0+00 Sline Pringle				
E		1.4		228.0
E Top cb		1.50		227.88
G		2.29		
1/4		2.60		
1/2		2.90		226.48
3/4		3.50		
G		4.78		
N Top cb		9.32		225.06
VY		4.4		225.0
0+19				
N-10		6.4		
N		5.5		223.9
cb		9.6		
1/4		4.0		
1/2		3.4		226.0
3/4		2.8		
cb		2.7		
TP		1.9		
E		1.9		227.5
0+25				
E		4.0		225.4
cb		3.8		
1/4		3.8		

Plotted Jan-10-29 CBH



H.I.
22938

+

H.I.
22938

Elev 51

E	4.1	225.3
1/4	4.5	
cb	5.4	
W	6.3	223.1
+10	7.1	
	0.50	
-10	10.9	
W	9.5	219.9
cb	7.9	
1/4	7.9	
E	6.9	222.5
1/4	6.6	
cb	6.4	
+6 Fence	7.0	
E	7.2	222.2
	0.63	
E	8.5	220.9
+6	8.5	
cb	8.5	
1/4	8.9	
E	9.4	220.0
1/4	10.4	
+5	11.7	
cb	11.7	
+2	11.4	
W	12.6	217.8

+10	13.3	
TP	0.98	217.07
		12.79
		0.75
W-10		3.8
W		3.0
+5		2.5
cb		2.5
1/4		2.4
E		1.8
1/4		1.3
cb		0.8
+6 Fence		0.1
E		0.1
		0.94
E		5.5
		6.3
+6 Wall's Fence		6.3
+6		7.0
cb		7.5
1/4		7.6
E		8.0
1/4		9.0
cb		9.3
+4		9.3
+8		7.0
W		6.8
+10		7.0

216.59 -

214.1

215.3

217.0

211.6

209.1

210.3

H.I.
217.07

0198

W-10		8.0	
-4		7.4	
-3		8.9	
N		9.9	207.2
cb		10.9	
1/4		10.5	
2		9.8	207.3
1/4		9.5	
cb		9.2	
+6 Bottom well		9.2	
+6 Top well		6.0	
E		6.0	211.1
	11.00		
E		10.3	206.8
+6		10.1	
cb		10.1	
1/4		10.2	
2		10.5	206.6
1/4		11.2	
cb		11.6	
N		12.0	205.1
+10		12.5	
T.P.	0.08	204.29	12.86
		11.25	204.21
-10		7.6	
N		7.7	196.6

H.I.
209.29

52

cb		7.6	
1/4		7.6	
2		7.3	197.0
1/4		7.0	
cb		7.0	
E		6.6	197.7
T.P.	0.58	192.12	12.75
		11.50	191.59
E		2.2	189.9
cb		2.5	
1/4		2.8	
2		2.9	189.2
1/4		3.4	
cb		3.5	
N		3.7	188.4
+10		3.9	
		11.53	
-10		5.0	
N		5.8	186.3
cb		5.7	
1/4		5.5	
+2		5.8	
+3		4.2	
2		4.0	188.1
1/4		3.9	
cb		3.6	

	H.I	-	E/ey
	192.12		
+8		3.2	
E		3.1	189.0
	1470		
E		9.0	183.1
Ob		9.1	
1/4		9.9	
Ø		10.1	182.0
1/4		10.5	
Ob		10.7	
+10		11.0	
+11		9.9	
W		10.9	181.2
+10		10.0	
T.P.	0.33	12.98	179.14
		1485	
-10		2.9	
W		2.6	176.9
Ob		2.6	
1/4		2.5	
E		2.2	177.3
1/4		2.0	
+1		1.6	
Ob		1.4	
E		1.1	178.4
	2+00		
E		1.5	175.0

	H.I		
	179.47		53
	2+00		
cb	5.2		
1/4	5.6		
Ø	5.8		173.7
1/4	5.9		
Ob	5.8		
W. Ground	6.6		172.9
W. Top Wall	4.0		175.5
+10 Ground	7.4		
+10 Top Wall	4.3		
	2+20		
-10	11.5		
W.	11.0		168.5
Ob	10.9		
1/4	11.1		
Ø	10.8		168.7
+2	10.5		
+3	12.2		
1/4	11.8		
Ob	11.5		
+8	10.6		
+9	10.0		
E	10.1		169.4
T.P.	0.16	12.98	166.99
		2+32	
E		1.2	166.0
+8		0.9	
+9		2.0	

HZ
167.15

cb	2.3	
1/4	2.3	
+6	1.6	
1/4	0.7	1665
1/4	0.6	
cb	0.8	
W	1.5	165.7
+10	1.8	
	21.34	
-10	2.6	
W	2.2	165.0
+7	1.9	
+8	2.8	
cb	3.6	
1/4	3.7	
1/4	3.4	163.8
1/4	3.0	
cb	3.0	
F2	2.7	
+3	1.2	
E	2.6	165.6
	21.37	
E	8.2	159.0
+3	8.3	
+4	3.1	
+8	1.9	

+

HZ
167.15

+9	3.0	
cb	3.3	
1/4	3.2	
1/4	3.2	164.0
1/4	9.0	
cb	4.3	
+7	2.3	
W	2.9	164.8
	21.52	
W-10	5.9	
W	5.6	161.6
cb	5.4	
1/4	6.1	
1/4	5.8	161.4
1/4	6.3	
cb	6.7	
+2	6.5	
+7	7.8	
+8	8.9	
E	9.4	10.90
	21.62	157.8
		21.62 ⁵ Porch of Residence
	7.8	159.4
	21.65	
E	10.4	156.8
cb	10.8	
1/4	10.2	

Elk House 54.
2793.23 Back
82 Rod

25 Back

27.1 End
15 Back
4.0 105

	H.I. 167.15	-	Elev		H.I. 155.07	
2		9.7	157.8	+10	2.6	
1/4		8.8			2790	
cb		8.6		-10	5.0	
W		9.1	158.1	W	5.1	150.0
+10		8.8		+4	5.5	
		2771 S. End Residence on East		+5	5.9	
	7.5 Back	10.8	156.4	cb	5.9	
		2775		1/4	6.7	
-10		11.9		2	6.8	148.3
W		12.2	155.0	1/4	6.5	
cb		12.5		cb	5.9	
1/4		13.0		+8	5.2	
2		13.0	154.2	+9	4.4	
1/4		12.8		E	3.6	151.5
cb		12.9			2798	
E		11.3	155.9	E	7.8	147.3
TP	0.62	12.70	154.45	+2	7.8	
		2783		+3	10.1	
E		0.5	154.6	+8	10.9	
+8		1.9		cb	9.9	
cb		2.4		1/4	9.5	
1/4		3.2		2	9.3	145.8
2		4.1	151.0	1/4	9.3	
1/4		4.4		cb	9.2	
cb		3.5		W	7.9	147.2
1X		2.4	152.7	+10	8.1	

	+	H.I. 155.07	-	E/64
			3+00	
W			9.2	145.9
cb			9.7	
1/4			10.0	
1/4			10.9	144.7
1/4			10.8	
cb			11.0	
E			11.2	143.9
T.P.	0.38	142.61	12.84	142.23
		S. Line Keating = 00		
E-10			12.7	
E			13.1	129.5
cb			13.3	
1/4			13.2	
1/4			13.2	129.4
1/4			13.8	
cb			13.3	
+7			12.8	
W			12.6	130.0
+10			11.8	
T.P.	0.89	130.66	12.84	129.77 -
			0+13	
-10			4.4	
W			4.9	126.3
+5			4.8	
cb			5.5	

	H.I. 130.64	5P
1/4	6.9	
1/4	5.5	125.2
1/4	5.1	
cb	5.2	
+7	5.1	
E	5.1	125.6
+10	5.0	
	0+26	
E-15	8.4	
E	8.4	122.3
cb	9.4	
1/4	10.1	
1/4	11.2	119.4
+5	12.1	
1/4	11.6	
cb	11.0	
+5	9.4	
+10	8.2	
W	8.0	122.7
+15	7.7	
T.P.	0.14	118.13
	12.67	117.99
	0+34	
W-25	1.9	
W-7	2.5	
W	1.2	116.9
+9	1.1	

H.I
118.13

cb			2.1	
1/4			2.8	
£			1.9	116.2
1/4			1.5	
+4			0.6	
cb			0.4	
T.P.	3.92	124.14	0.91	117.72
+6			2.3	
E			1.8	119.3
+15			2.1	
+25			1.7	3
T.P.	0.41	118.13	3.42	117.14
			0+50	
-30			3.8	
-15			3.7	
E			5.4	112.7
cb			6.4	
1/4			6.6	
£			6.9	111.2
1/4			7.5	
cb			7.9	
+5			8.8	
N			9.1	109.0
+27			9.4	
+30			8.4	

H.I
118.13

57

				0+65	
-30				11.6	
N				11.0	107.1
cb				9.7	
1/4				9.2	
£				8.1	110.0
1/4				7.9	
cb				7.4	
E				6.2	111.9
-30				5.7	
				0+70	
-40				9.6	
-18				9.6	
-17				6.5	
E				6.7	111.4
cb				7.7	
1/4				8.3	
£				8.8	109.3
1/4				9.4	
cb				10.2	
+1				12.7	
N				13.6	104.5
+17				14.6	
+18				11.4	
+30				11.8	
				10+77	
-30				12.2	

H.I
11813

0-28	12.3	
1-27	14.5	
2-20	14.7	
1-8	13.8	
1-7	11.4	
011	10.1	1080
7+7	9.9	
+8	13.5	
006	13.2	
+3	13.2	
+14	12.8	
7+3	12.4	
+4	9.8	
-2	9.0	1091
-14	8.6	
06	8.1	
0E	7.1	1110
+8	7.3	
+9	10.5	
+20	10.3	
+21	8.4	
+30	7.0	
+35	6.0	
	0+86	
+35	5.2	
-23	6.4	

H.I
11813

58
0+93 114
84

-15	8.5	
-13	9.6	
-5	11.1	
-1	11.3	
E	8.0	110.1
06	8.6	
+3	9.2	
+4	12.3	
1/4	12.6	
2	12.2	105.9
12	12.1	
+3	9.4	
1/4	9.1	
06	9.3	
W	10.2	107.9
-30	12.5	
-32	12.8	
	0+90	
-30	12.5	
W	10.1	108.0
06	9.2	
1/4	8.8	
2	9.1	109.0
+3	11.0	
+5	12.3	
1/4	12.1	

H.I.
118.13

cb	11.2	
E	11.3	106.8
F10	9.9	
+20	6.9	
+30	5.6	
	0493. Sewer Mouth Rim	
κ.	8.9	109.73
	1400	
-30	5.0	
-10	6.7	
-2	7.5	
E	10.0	108.1
cb	11.5	
+4	11.6	
+5	7.2	
1/4	7.1	
κ	7.6	110.5
1/4	8.2	
cb	8.5	
N	9.2	108.9
+12	11.2	
+20	12.4	
+30	13.3	
	1403	
-30	13.3	
-20	12.0	

H.I.
118.13

59

-10	10.5	
N	8.8	109.3
cb	7.7	
1/4	7.3	
κ	7.0	111.1
1/4	6.6	
cb	6.9	
E	6.2	111.9
+30	4.7	
	1420	
-30	1.5	
-25	1.4	
-20	0.8	
-10	0.4	
E	0.6	117.5
cb	0.9	
+5	2.1	
1/4	2.1	
κ	2.5	115.6
1/4	2.8	
cb	3.5	
N	5.9	112.7
+10	7.2	
+18	8.5	
+28	12.4	
+30	13.2	

H.I.
118.131+29

N-25		7.7		
-15		5.9		
N		3.2	114.9	
cb		1.2		
1/4		0.2		
T.P.	12.03	129.44	0.72	117.41
ϕ		10.5		119.0
1/4		9.3		
cb		8.7		
E		8.3		121.1
+10		8.4		
+20		9.4		
+30		11.3		
		114.5		
-30		6.8		
-20		4.0		
-10		2.6		
E		2.6		126.8
cb		3.5		
1/4		4.4		
ϕ		5.9		124.0
1/4		6.3		
cb		7.5		
N		9.2		119.8
+10		12.2		
+18		14.2		

H.I.
129.44

60

N-25		14.7		
		14.57		
-20		10.9		
-13		10.1		
N		6.9	122.5	
+7		4.6		
cb		3.6		
1/4		2.8		
ϕ		2.3	127.1	
1/4		1.7		
cb		0.7		
T.P.	10.22	138.37	1.29	128.15
+6		8.6		
E		8.0		130.4
+10		7.1		
		117.1		
-10		4.6		
E		4.8		133.6
cb		6.3		
1/4		7.2		
ϕ		8.4		130.0
1/4		9.6		
cb		10.6		
N		13.3		125.1
+7		14.8		
+15		15.9		

H.I.
138.37

+20		159	
		1178	
-20		132	
-7		128	
W		120	126.4
cb		9.6	
1/4		8.3	
E		6.9	131.5
1/4		5.8	
cb		4.8	
+7		3.7	
E		3.3	135.1
+10		2.9	
TP	13.12	150.93	0.56
		1196	137.81
-10		10.9	
E		10.9	140.0
+10		12.0	
cb		12.5	
1/4		13.7	
E		14.8	136.1
1/4		15.8	
cb		17.0	
+5		17.9	
+8		19.1	
KV		19.8	131.1

H.I.
150.93

61

+10		19.9	
+20		20.1	
		2105	
-20		18.1	
-6		16.9	
W		16.7	134.2
+5		16.6	
cb		15.4	
1/4		14.3	
E		13.0	137.9
1/4		11.6	
cb		10.0	
E		9.2	141.7
+10		9.2	
		2120	
E		7.0	143.9
cb		7.9	
1/4		9.1	
E		10.2	140.7
1/4		11.1	
cb		12.1	
+8		12.8	
W		12.7	138.2
+15		13.7	
		2134	
-15		7.2	

H.I.
150.93

N	7.1	143.8
+9	7.2	
cb	7.9	
1/4	7.9	
¢	6.8	144.1
1/4	5.5	
+5	9.4	
cb	9.2	
E	3.7	147.2
	2+40	
E	2.0	148.9
+6	2.0	
cb	2.6	
1/4	3.9	
¢	4.4	146.5
1/4	5.2	
cb	5.4	
+8	5.1	
N	4.9	146.0
+10	4.5	
TP	0.95	150.48
	2+61	
-10	8.4	
N	9.2	153.9
cb	8.7	
1/4	8.4	

H.I.
16314

62

¢	8.7	154.4
1/4	8.2	
cb	7.9	
E	7.1	156.0
	2+72	
E	2.8	160.3
cb	3.1	
1/4	3.4	
¢	2.9	160.2
1/4	2.9	
cb	2.9	
+5	2.8	
N	3.8	159.3
+10	3.2	
TP	13.09	175.10
	1.13	162.01
	2+82	
-10	11.0	
N	11.0	164.1
+3	10.9	
cb	9.9	
1/4	9.5	
¢	9.5	165.6
+3	9.2	
1/4	9.7	
cb	9.9	
E	9.7	165.4

H.I.
175.10

E	10.0	165.1
	2790	
-10	6.1	
E	5.9	169.7
+9	5.5	
cb	5.8	
1/4	6.0	
E	5.1	170.0
1/4	4.5	
cb	5.0	
+6	5.5	
N	6.3	168.8
+10	6.0	
	2199	
-10	4.3	
N	4.9	170.7
+9	3.6	
cb	2.2	
1/4	1.8	
E	2.7	172.4
1/4	3.4	
cb	3.2	
E	3.2	171.9
+10	3.8	
TP	10.83	184.25 1.68 173.42

3100 N. Line Andrews

H.I.
184.5

63

E	8.2	176.0
cb	7.9	
1/4	7.3	
E	7.4	176.8
1/4	8.0	
cb	7.9	
+6	8.8	
+7	9.8	
N	10.9	173.3
TP	12.38	195.90 0.73 183.52
T.P.	12.95	208.77 0.08 195.82
T.P.	5.56	213.69 0.64 208.13
Set B.M. 13' Point	Andrews & Torrence	4.30 209.39

W Bliss
 Duermit
 Jacobson
 12/7/28
 8 W TOP
 N. Pringle
 Torrence

X Sections Torrence St from the
 South line of Pringle to the North
 Line of Andrews
 + 2.00 238.27
 H.I. Elev 237.27
 50' st 12 cbs 65' 1/45

0435 Tree 65
 off Peopline 69

S. Line Pringle = 00
 on paving

W	4.3	235.0
W Top cb	4.38	234.89
G	4.82	234.5
1/4	4.14	235.2
¢	3.66	235.61
1/4	3.31	236.0
G	3.16	236.1
E Top cb	2.35	236.92
E	2.2	237.1

Curb put in for 10' walks 30' roadway. JLB

0414²⁰ North End Single Garage on East

1st Back concrete floor 3.15 236.12

0422⁵⁰ South End Single Garage on East

1st Back concrete floor 3.15 236.12

0425

E	3.4	235.9
cb	3.8	235.5
1/4	4.1	235.2
¢	4.4	234.9
1/4	4.6	234.7
cb	4.7	234.6
W	4.9	234.4

0431

W	5.3	234.0
+3	5.9	233.4

Plotted Jan-10-1929 C.H.H.

	HI 23927	-	E/cv
cb		57	233 6
1/4		55	233 8
2		49	234 4
1/4		42	235 1
cb		42	235 1
E		35	235 8
	0+37		
E		58	233 5
cb		51	234 2
1/4		52	234 1
2		53	234 0
22		57	233 6
23		63	233 0
1/4		66	232 7
cb		69	232 4
210		69	232 4
W		59	233 4
	0+50		
-10		75	231 8
W		76	231 7
22		90	230 3
cb		95	229 8
1/4		93	230 0
22		87	230 6
24		67	232 6
2		66	232 7

	HI 23927	-	E/cv	65
1/4		65	232.8	
cb		73	232.0	
26		66	232.7	
E		62	233.1	
	0+62			
E		93	230.0	
26		95	229.8	
cb		98	229.5	
25		98	229.5	
1/4		94	229.9	
25		80	231.3	
2		76	231.7	
25		96	229.7	
1/4		10.7	228.6	
22		11.7	227.6	
cb		121	227.2	
210		11.7	227.6	
W		95	229.8	
210		100	229.3	
	0+68			
-10		11.5	227.8	
W		14	227.9	
TP	2.63	228.73	13.17	226.10
24		2.7	226.0	
cb		3.1	225.6	
1/4		2.7	226.0	

228.73

£	2.9	225 8
1/4	7.9	226 8
cb	1.3	227 4
E	0.3	228 4
0175		
E	2.2	226 5
cb	3.6	225 1
+3	9.2	224 5
1/4	4.2	224 5
£	4.2	224 5
1/4	4.6	224 .1
cb	4.8	223 9
+8	5.0	223 7
1/4	3.0	225 7
+10	1.8	226 9
0190		
-10	6.1	222 6
W	7.8	220 9
+6	9.8	218 9
cb	9.7	219 0
1/4	9.1	219 6
£	8.9	219 8
1/4	8.1	220.6
cb	7.0	221 7
E	5.0	223.7

H.
22873

66

1400		
E	7.4	221.3
cb	9.7	219.0
1/4	10.9	217.6
£	11.8	216.9
1/4	12.3	215.6
cb	12.9	215.8
+6	13.2	215.5
+8	12.7	216.0
W	13.1	215.6
+10	12.2	216.5
T.P.	0.23	216.78
	12.18	216.55
1710		
-10	6.8	210.0
W	5.3	211.5
+3	4.7	212.1
cb	4.0	212.8
1/4	3.5	213.3
£	3.3	213.5
1/4	2.1	214.7
cb	1.2	215.6
E	0.1	216.7
1725		
E	3.7	213.1
cb	5.2	211.6
1/4	6.5	210.3
£	7.5	209.3

H.1
216.78

1+25

1/4	8.2	208.6
cb	8.7	208.1
W.	9.5	207.3
+10	11.5	205.3

1+35

-10	15.0	201.8
W	13.0	203.8
cb	11.7	205.1
1/4	11.5	205.3
E	11.2	205.6
1/4	10.2	206.6
cb	9.3	207.5
E	7.5	209.3

T.P.	0.13	204.32	12.59	204.19
------	------	--------	-------	--------

1+53

E	0.9	203.4
cb	2.6	201.7
1/4	3.3	201.0
E	4.0	200.3
1/4	4.7	199.9
cb	4.8	199.4
W.	6.4	197.9
+10	7.7	196.9

1+80

-10	14.2	
W.	13.2	191.1

204.32

67

cb	11.7	
1/4	10.8	
E	10.9	193.4
1/4	9.9	
cb	9.1	
E	7.0	197.3

2+00

E	11.9	192.4		
T.P.	0.43	191.74	13.01	191.31
cb	1.6			
1/4	2.4			
E	3.4	188.3		
1/4	4.2			
cb	5.2			
W.	6.8	184.9		
+10	7.9			

2+25

-10	13.3	
W	12.1	179.6
cb	10.0	
1/4	8.8	
E	8.2	183.5
1/4	7.7	
cb	6.7	
E	5.2	186.5

191.74
2+50

E		10.2	181.5
cb		11.4	
1/4		11.8	
£		12.5	179.2
1/4		13.1	
T.P.	0.66	13.02	178.72
cb.		2.2	
W.		4.5	174.9
+10		6.3	
		2+75	
-10		11.3	
W		9.6	169.8
cb		7.5	
1/4		6.3	
£		5.6	173.8
1/4		4.7	
cb		4.0	
E		2.7	176.7
		3+00	
E		7.4	172.0
cb		8.6	
1/4		9.7	
£		10.8	168.6
1/4		11.7	
cb		12.8	
+8		14.0	

HZ.
179.38

68

W		15.0	164.4
T.P.	0.52	167.58	12.32
T.P.	3.90 3.70	158.80	12.68
			154.90 -
		S Line Keating = 00	
W		10.0	148.8
+9		9.7	
cb		9.2	
1/4		7.9	
£		7.4	151.4
+3		6.0	
1/4		5.2	
+3		3.9	
cb		3.2	
+6		1.6	
E		0.9	158.4
		0+13	
E		6.2	152.6
+6		7.3	
cb		9.1	
1/4		10.6	
£		12.1	146.7
+5		13.5	
1/4		14.2	
+4		14.8	
cb		15.4	
W		17.5	141.3

H.Z.
15880

+15		18.2	
		0+25	
-15		24.0	
W		23.4	135.4
cb		20.2	
1/4		18.1	
¢		16.2	142.6
1/4		14.5	
cb		13.2	
+7		12.4	
E		11.6	147.2
TP	0.95	146.16	13.04
		0+36	145.71
E		3.8	142.4
cb		5.8	
1/4		7.2	
¢		7.8	138.4
1/4		9.3	
cb		11.7	
W		15.2	131.0
+15		16.6	
		0+56	
W-25		24.4	
-15		23.0	
W		21.6	124.6
+7		20.0	

+
H.I.
14616

-
Elev
69

cb		18.9	
1/4		17.8	
¢		16.2	130.0
1/4		15.1	
cb		13.9	
+6		13.3	
E		12.1	134.1
+15		10.7	
TP	0.79	134.46	12.44
		0+74	133.67-
E-25		3.7	
-15		5.1	
E		7.0	127.5
cb		9.6	
1/4		10.7	
¢		12.0	122.5
1/4		12.7	
cb		13.5	
W		14.8	119.7
+15		15.9	
+30		16.8	
		0+87	
W-30		20.5	
-15		20.5	
-5		20.1	
-4		17.0	

H.I.
134.46

W		16.2	118.3
cb		15.3	
1/4		14.6	
Φ		13.6	120.9
1/4		12.6	
cb		11.9	
E		10.7	123.8
+10		9.2	
+20		7.5	
+30		6.0	
		0+93	
E-30		7.3	
-15		9.9	
E		10.9	123.6
cb		12.9	
T.P.	2.97	125.71	11.72 122.79
1/4		4.9	
Φ		5.9	119.8
1/4		6.8	
cb		7.5	
+1		10.9	
W Bottom		11.3	114.4
+11		11.7	
+12		8.2	
+30		8.9	

H.I.
125.71

70

		14.00	
W-30		7.7	
W		7.9	118.3
+8		7.8	
+9		9.5	
cb		10.5	
1/4		10.4	
+4		10.5	
+5		7.1	
Φ		6.8	118.9
1/4		6.0	
cb		5.1	
E		3.6	122.1
+15		1.9	
130		0.2	
		14.13	
-30		1.8	
-15		3.6	
E		5.9	120.3
cb		6.5	
+3 Top		6.9	
+3 Bottom		9.2	
1/4		10.2	
+5		10.1	
Φ. Top Mn. Hole		6.0	119.7
1/4		5.9	
cb		5.9	

	+	H.I. 125.71	-	Elev
N			5.2	1205
+5			4.9	
+15			3.6	
+30			2.6	
TP.	6.35	131.15	0.91	124.80
			14.25	
-30			2.7	
-15			4.3	
N			5.8	1254
+8			5.7	
06			6.1	
14			7.0	
⊕			7.9	1233
14			10.1	
+4			11.0	
+5			15.1	
06			15.1	
+5			14.9	
+6			12.3	
E			11.3	1199
+15			9.8	
+30			8.1	
			14.3	
-30			8.4	
-15			10.0	
E			11.1	1200

	+	H.I. 131.15	-	Elev	71	
+1					14.9	
+7					15.0	
+10					11.1	
06					10.8	
+3					9.9	
+5					7.7	
14					7.2	
⊕					5.9	125.3
+3					5.2	
14					5.0	
+3					4.8	
06					4.1	
+5					3.2	
N					2.8	126.4
+15					1.3	
+25					0.3	
TP.	8.75	138.64			12.4	129.91
					14.39	
-30					5.4	
-15					6.9	
N					8.7	129.9
06					9.3	
14					10.4	
⊕					11.4	127.2
+5					12.6	
14					12.8	

HI
138.64

+5	13.4	
cb	15.8	
+8	18.0	
E	22.4	116.2
+4	22.4	
+5	19.3	
+30	17.0	
	174.4	
-30	21.8	
-10	22.3	
E	18.6	120.0
+4	15.7	
+5	13.1	
cb	12.4	
+v	10.6	
1/4	9.6	
1/4	8.8	129.8
1/4	8.3	
cb	7.8	
W	6.8	131.8
+15	5.0	
+30	3.9	
	175.0	
-20	2.9	
-10	3.3	
W	4.8	133.8

HI
138.64

72

cb	6.1	
1/4	6.6	
1/4	6.9	131.7
1/4	7.6	
cb	8.4	
+7	9.8	
+8	10.7	
E	13.4	125.2
+15	16.5	
+30	15.6	
	145.6	
-30	13.9	
-15	12.4	
E	8.0	130.6
+4	6.5	
cb	4.8	
1/4	3.8	
1/4	3.3	135.3
1/4	3.2	
cb	2.9	
W	2.1	136.5
+20	0.8	
TP	12.72	149.95
	1.91	137.23
	170	
-20	5.1	
W	7.4	142.5

HI.
149.95

cb		8.0	
1/4		8.1	
\$		8.6	141.3
1/4		9.0	
cb		9.2	
+8		9.8	
E		10.9	139.0
+10		13.6	
+20		17.6	
+30		19.5	
		1480	
-30		12.8	
-20		12.0	
-15		11.6	
E		7.6	142.3
cb		5.8	
1/4		4.9	
\$		4.2	145.7
1/4		3.6	
cb		3.9	
N		2.7	147.2
+10		0.7	
T.P.	12.98	162.50	0.43
			149.52
+20		11.4	
		1190	
-20		6.6	

HI.
162.50

73

N		8.7	153.8
+5		9.0	
cb		10.0	
1/4		10.6	
\$		11.5	150.9
1/4		12.2	
cb		13.1	
+8		15.4	
E		16.6	145.9
+15		21.0	
+30		21.1	
		2100	
-30		16.4	
-15		17.1	
-7		15.5	
E		12.3	150.2
+6		9.4	
cb		7.7	
1/4		7.2	
\$		6.2	156.3
1/4		5.3	
cb		4.4	
+5		3.6	
N		3.3	159.2
+15		1.8	
T.P.	12.59	173.36	1.73
			160.77

H.I.
173.36

2+15

W-15	7.9	
W	6.2	167.2
+8	6.7	
cb	7.3	
1/4	8.8	
2	9.8	163.6
1/4	11.3	
cb	12.9	
+5	14.8	
E	17.1	156.3
+15	19.6	
+30	17.5	

2+25

-30	14.2	
-15	14.0	
E	12.3	161.1
+6	11.9	
cb	9.3	
1/4	6.9	
2	4.6	168.8
1/4	3.6	
cb	3.1	
+5	2.6	
W	2.3	171.1
+10	1.8	

13.20 186.16 0.90 172.96

H.I.
186.16

74

2+35

W-10	10.7	
W	11.8	174.4
cb	12.9	
1/4	13.6	
2	14.5	171.7
1/4	15.9	
cb	17.6	
+8	20.7	
E	21.3	164.9
+15	22.6	
+30	23.1	

2+45

-30	18.3	
-15	17.8	
E	16.2	170.0
+8	15.3	
cb	14.2	
1/4	13.3	
2	12.9	173.8
1/4	11.5	
cb	10.1	
W	8.1	178.1
+10	7.9	

2+55

-10	5.3	
W	6.3	179.9

	+	HI.	-	Elev
		18616		
cb			7.3	
1/4			8.6	
⊕			9.9	176.8
1/4			10.3	
cb			10.8	
E			12.8	173.4
+20			12.8	
			2+7.5	
-15			5.5	
E			9.9	181.8
cb			4.3	
1/4			3.5	
⊕			2.5	183.7
1/4			1.8	
cb			0.9	
T.P.	12.41	198.10	0.47	185.69
W			11.1	187.0
+10			9.8	
			2+9.0	
-10			5.8	
W			6.6	191.5
cb			8.0	
1/4			8.2	
⊕			8.7	189.4
1/4			9.3	
cb			9.8	

	+	HI.	-	Elev
		19810		75
E			9.6	188.5
+15			11.2	
			3+0.0	Nline Andrews
			7.2	
			5.3	
E			5.5	192.6
cb			5.7	
1/4			5.6	
⊕			5.4	192.7
-1/4			5.2	
cb			4.6	
W			2.9	195.2
T.P.	13.28	211.27	0.11	197.99
check out on BM	13 rd Point Andrews		1.88	209.39
	2 Torrence			
B.M.	4.44	213.83		209.39
TP	6.29	207.29	12.83	201.00
Set BM	3 Nails in fence post		10.63	196.61
	N.E. Nealey Andrews			

5 Nails on this BM in
 Neale St.
 Book 1307 page 12
 45 Etc. 196.72

Couts St. Cross Section

West Atlantic to Mainline of Santa Fe RR

Correction see Page 79

3-7-59
S.S. son
Replinger
Hubbard
Osborn

BM	251	7.00 7.50	6d 122-34 85' wide 13' Chs. 13' 9" dia 1 SE Top Hat Couts	cb	700	91	-1.9 -2.4
				78		82	-0.7 -1.2
				74		86	+1 -1.6
S		7.4	2.1 2.6	2		10.0	-2.5 -3.0
+9 - Existing cb		4.97	2.13 2.63	2		84	-0.9 -1.4
Gutter on Parap		5.08	2.42 1.92	cb		90	+1.5 -2.0
cb		4.88	2.68 2.18	N		98	-2.3 -2.8
7/4		4.49	2.01 2.51	TP	817	994	-1.4 -2.94
8		4.38	2.12 2.62		35 F		
7/4		4.15	3.05 2.55	N		88	-2.8 -3.3
cb		4.93	2.77 2.27	cb		86	-2.5 -3.1
Gutter		4.91	2.59 2.09	7/4		85	-2.5 -3.0
+5 - Existing cb		4.28	3.22 2.72	2		86	-2.5 -3.1
N		4.3	3.5 2.7	7/4		87	-2.7 -3.2
				cb		86	-2.5 -3.1
N		4.8	2.7 2.2	S		85	-2.5 -3.0
cb = End of Existing cb		4.11	2.36 2.86		65 F		
Gutter		4.9	2.6 2.1	S		63	-0.3 -0.8
7/4		4.8	2.7 2.2	cb		64	-0.4 -0.9
2		5.0	2.5 2.0	7/4		65	-0.5 -1.0
7/4		5.1	2.9 1.9	2		65	-0.5 -1.0
Gutter		5.1	2.4 1.9	7/4		66	-0.6 -1.1
cb = End of Existing cb		4.36	3.14 2.64	cb		68	-0.8 -1.3
S		4.7	2.8 2.3	N		70	-1.0 -1.5
					100 F		
S		9.7	2.2 -2.7	N		51	+0.9 +0.4

Plotted 3-19-59
T.L.

5.53
~~6.03~~

Cb	55	+0.5	00
1/4	55	0.5	00
8	54	0.5	+0.1
1/4	50	+0	+0.5
Cb	53	0.7	+0.2
S	48	+1.2	+0.7

150'F

S	57	0.9	0.4
Cb	52	0.8	0.3
1/4	50	1.0	0.5
8	50	1.0	0.5
1/4	50	1.0	0.5
Cb	50	1.0	0.5
H	50	+0	0.5

100'F

H	43	1.7	1.2
Cb	43	1.7	1.2
1/4	43	1.7	1.2
8	43	1.7	1.2
1/4	43	1.7	1.2
Cb	43	1.7	1.2
S	43	1.7	1.2

250'F

S	35	2.5	2.0
Cb	36	2.4	1.9
1/4	34	2.6	2.1

5.53
~~6.03~~

77

8	34	2.6	2.1
1/4	33	2.7	2.2
Cb	36	2.4	1.9
1/4	33	2.7	2.2

300'F - N L Karteg 75' N L 125' Cb 125' S L

H	35	2.5	2.0
Cb	31	2.4	1.9
1/4	36	2.4	1.9
8	35	2.5	2.0
1/4	36	2.7	1.9
Cb	35	2.5	2.0
S	34	2.6	2.1

N Cb

S	37	2.3	1.8
Cb	37	2.3	1.8
1/4	33	2.7	2.2
8	39	3.1	2.6
1/4	38	2.8	2.3
H	38	2.8	2.3

N 1/4

H	38	2.8	2.3
Cb	38	2.8	2.3
1/4	38	2.8	2.3
8	38	2.8	2.3
1/4	34	2.6	2.1
S	35	2.5	2.0

~~603~~

Kurtz

S	29	3.7	2.6	2.7
Cb	27	3.3	2.8	2.8
H	26	3.4	2.9	2.9
S = Rim of Moat	468	2.85		
		3.35		
H	26	3.4	2.9	2.9
Cb	27	3.3	2.8	2.8
H	28	3.2	2.7	2.7
H	27	3.3	2.8	2.8
Cb	27	3.3	2.8	2.8
H	27	3.3	2.8	2.8
S	27	3.2	2.7	2.7
Cb	27	3.1	2.6	2.7
S	29	3.1	2.6	2.7
S	26	3.4	2.9	3.1
Cb	24	3.6	3.1	3.3
H	23	3.7	3.2	3.4
S	22	3.8	3.3	3.2
H	22	3.8	3.3	3.2
Cb	22	3.7	3.2	3.1
H	24	3.6	3.1	3.2
H	20	4.0	3.5	3.5

Book 1309-10
M.H. 2.9

A/H

ECb

EL Party

~~603~~

Cb = Grabbing of Catch Basin

Cb	242			
H	23			
S	18			
H	16			
Cb	11			
S	17			
TP	122	10.01	14.32	
S	82			
Cb	88			
H	103			
S	100			
H	111			
Cb	113			
H	100			
H	94			
Cb	93			
H	93			
S	90			
H	92			
Cb	86			
S	82			
S	84			
Cb	86			

325 of F.L. Kurtz

37E

15E

Book 1309 - page 10
E.L. of Kurtz = 307

	3.11			
	3.1			
	3.2			
	3.7			3.3
	3.7			
	3.2			3.7
	3.9			
	4.1			4.0
	4.4			
	4.9			4.2
	3.9			
	4.3			3.8
	4.31			
	4.4			
	6.0			
	6.0			
	5.5			
	6.0			
	4.0			
	4.5			
	4.3			
	4.8			
	3.2			
	3.7			
	3.0			
	4.3			
	4.8			
	5.4	4.9		
	5.5	5.0		
	5.5	5.0		
	5.8	5.3		
	5.9	5.1		
	6.7	5.7		
	6.4	6.1		
	6.8	5.9		
	6.2	5.7		

Couts St.

14.32

~~11.83~~

69.83

1/4	8.7	8.1	5.6
1/2	8.6	6.2	5.7
3/4	9.2	5.4	5.1
cb	9.3	5.5	5.0
H	9.3	5.5	5.0
58 F			
H	2.8	11.9	10.5
cb	4.0	10.8	10.3
1/4	4.0	10.8	10.3
1/2	4.0	10.8	10.3
3/4	3.9	10.9	10.4
cb	3.9	10.9	10.4
S	3.9	10.9	10.4
62.2 E = 2 Main Lvs Sable Fe RR on S.			
S on Top Rail	3.7	11.65	11.15
Ground	3.6	11.2	10.7
cb	3.7	11.1	10.6
1/4	3.7	11.1	10.6
1/2	3.8	11.2	10.5
3/4	3.8	11.0	10.5
cb	3.8	11.0	10.5
H Ground	3.8	11.0	10.5
Top Rail	3.32	11.0	11.50
BM	9.84	4.48	4.46

SE Top Hyd
Couts of Atlantic
4.46

B.M. levels Couts - Wetherby & 3-15-29
N. Atlantic miller. 79

B.M. Top Hyd.	2.38	7.34	4.96	5.8 Couts 4 Atlantic
T.P. B.M. Top Hyd.	2.53	7.81	4.31	5.8 Atlantic 4 Wetherby Book 1309 P. 14
Hydts on Atlantic on fill possibility of settlement.				
B.M. Top Hyd.	2.53	6.84	4.31	5.2 Atlantic 4 Wetherby
T.P.	12.00	14.57	4.27	2.57
T.P.	12.94	26.81	0.74	13.23
T.P.	12.23	38.14	0.90	25.91
chk on B.M.			10.40	27.74 = 27.73 5.2. Moore 4 Wetherby
T.P.	12.75	50.49	0.40	37.74
T.P.	13.09	63.15	0.43	50.06
T.P.	11.52	73.18	1.49	61.66
chk on B.M.			3.35	69.83 = 69.83 N. Wetherby 4 La Jolla Blvd
B.M. Top Hyd	SE Atlantic + Wetherby		4.31	Not 4.38
" " "	SE Atlantic + Couts		4.46	Not 4.96

Correction.

20' ch. on Ivy Levels on Return + Curb.
 10' ch. on Baker S.E. Cor. Ban Croft + Ivy sts.
 20' Radius Return

3-15-29
 Miller.

B.M. BP	0.44	294.02		293.58	S.E. Juniper + Bancroft
S. line Ivy, 10' W. of E. line Bancroft		10.27		83.75	S. end. Return
Center Return		9.56		84.46	
S. end. ch. Ivy 10' E. of E. line Bancroft		9.03		84.99	P.C. 20' Radius Return
25' E. of E. line Bancroft		8.96		85.06	ons. ent. ch.
50' " " " "		8.86		85.16	" " " "
75' " " " "		8.81		85.21	" " " "
100' " " " "		8.71		85.11	E. end S. end. ch. N.C. Ivy
chk on B.M. BP		7.13	286.89 =	286.94	+ Bancroft
T.P.	0.74	283.37	11.39	282.63	
chk on B.M. BP		4.80	278.57 =	278.61	N.W. Ivy + 33 rd St.

B.M.s at Ivy + Bancroft + Ivy 32nd St
 are in a 2" Walk Both might have settled
 B.M. at Juniper + Bancroft in cent. ch.

Plotted
 TGH
 3-27-29

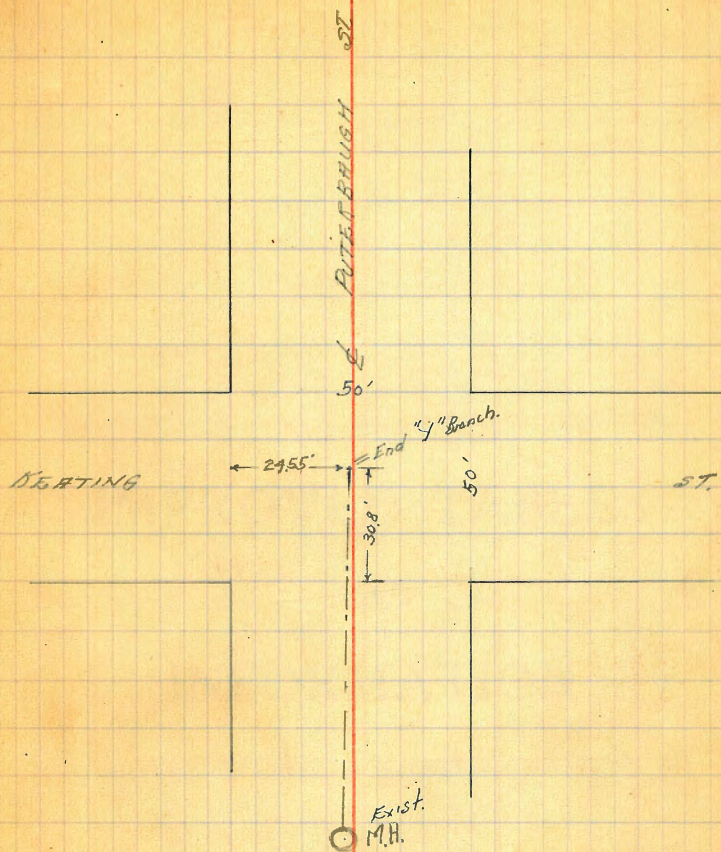
Walker
 No 149 m
 No 100 m
 Rem. 100 m
 9-10-29

Location of Existing Sewer
 in the Intersection of Ruterbaugh
 and Heating St.

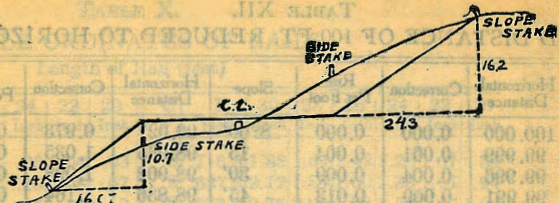
Bottom of M.H.
 0.493 Page 59
 this Book.
 1

	12.96	122.69		109.73
Elvd line of floor 1911			18.63	104.06
T.P.	12.81	135.40	0.10	122.59
T.P.	11.23	146.02	0.61	134.79
Flow line "Y" Branch			11.81	134.21
T.P.	12.47	158.24	0.25	145.77
T.P.	3.59	161.12	0.71	157.52
Chk on Arch 2+62.5 Page 54 this Book			1.77	159.35
				$\frac{159.35}{0.05} = \text{Pitch.}$

81



C	R
o 7	Feet
0-20	17189
0-40	8594
1-0	5730
1-20	4297
1-40	3438
2-0	2865
2-20	2456
2-40	2149
3-0	1910
3-20	1719
3-40	1563
4-0	1433
4-20	1323
4-40	1223
5	1146
6	955.3
7	819.0



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

To find length

12.55
24.55

67-48 Ver (6-25-00 = Cos 99374)

34-48 Back

1025	1.86
1025	1.86
5125	11.16
2050	1488
	186

ENGINEERING DEPARTMENT
CITY OF SAN DIEGO
CALIFORNIA

1050625 (1024.99)

202	10500
	404
2049	1024
	8176
	204554
20489	184401
204989	2015300

120.75	573.91
100.00	59
100.00	59
57.00	22
573.59	

cos 21°-14'-00" = 98.90

2719.16	99374
	6748
	794992
	397496
	698618
	596244
	670675750
	3448
	7258

15725	2)31.19	1690	390	2129
35			261.50	2.37
42112	1559		643.50	
30.00	37.16		26150	7150
391.12	310		382.00	420
	4001		643.50	7192
285	4-27-00		4001	
			391	
			9.10	

30	100x cos 9° 27' =	100.0999699	1
30			81
900			9.81
82.8	9.10		
9.0	9.10		
782.8	8990		
	828100		
3			
953.00	29038		
9	57-16-		
83			

#42-24	42 23.30	1.4	6.80
	-184.47		6.15
8.89			69 60
	45°-12"-00"	15	73-53
29653			16.07
30			16 31
8.89590	17.45	17.45	
	15.59	15.59	
8.90	2)31.19	1.86	

28929		95874
30		30
852870	log sin = 16° 31' x .30	2876220
7792.11		41.81
285		50292
7489.06	16-31	401.736
		276150
	Tan 16°-31	401.936

147.25	901.96
65	41.81
5025	443.75
	211.50
	182.25
	35.00
	147.25