

1291

POSTS

FIELD BOOK

No. 385 F

ENGINEERING DEPARTMENT,
CITY OF SAN DIEGO,
CALIFORNIA.

Our Leather Bound Engineers Note Books are carried in the following rulings:

- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
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- No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.
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THE FREDERICK POST CO.
ENGINEERING and DRAFTING SUPPLIES
IRVING PARK STATION
CHICAGO, ILL.

MICROFILMED

DEC 22 1964

TORREY PINES GRADE
 STADIA NOTES
 6% grade P=1500' or more.

10/30/08
 5 hours
 2 hours
 10/1/08
 1 hour

Foot of Torrey Brook	EI
P.C. & Ex. paving = 00	20.0
1	20.0
2 PI = Cop. Tack in 2' Ex. paving = 21.0	20.0
3 A = 4' x 4' LT.	19.3
4 P = 1500'	19.0
5 T = 587.08	18.3
6 Ch = 11.69	17.1
7	16.6
8 = Dry lake bottom	2.8
9 = " " "	2.8
100 EC. 11 + 19.40	37.6
13 + 20	47.1
15 + 77.7 POT	75.3
18 + 15.7 POT	90.7
24 + 09.5 POT	170.1
29 + 53 swale	128.3
31 + 70	147.0
32 + 32.1 POT	168.4
34 + 80	161.4
33 + 70 wash	137.4
34 + 76	166.0
35 + 51	202.9
36 + 09.4 = P.C.	209.0
38 + 13.3 = 2 curve	236.5
39 + 60	234.0

Plotted 11-1-28 TGH

4 = 15° x 9' RT.
 P = 1500
 T = 203.95
 EX = 13.8
 L = 405.35

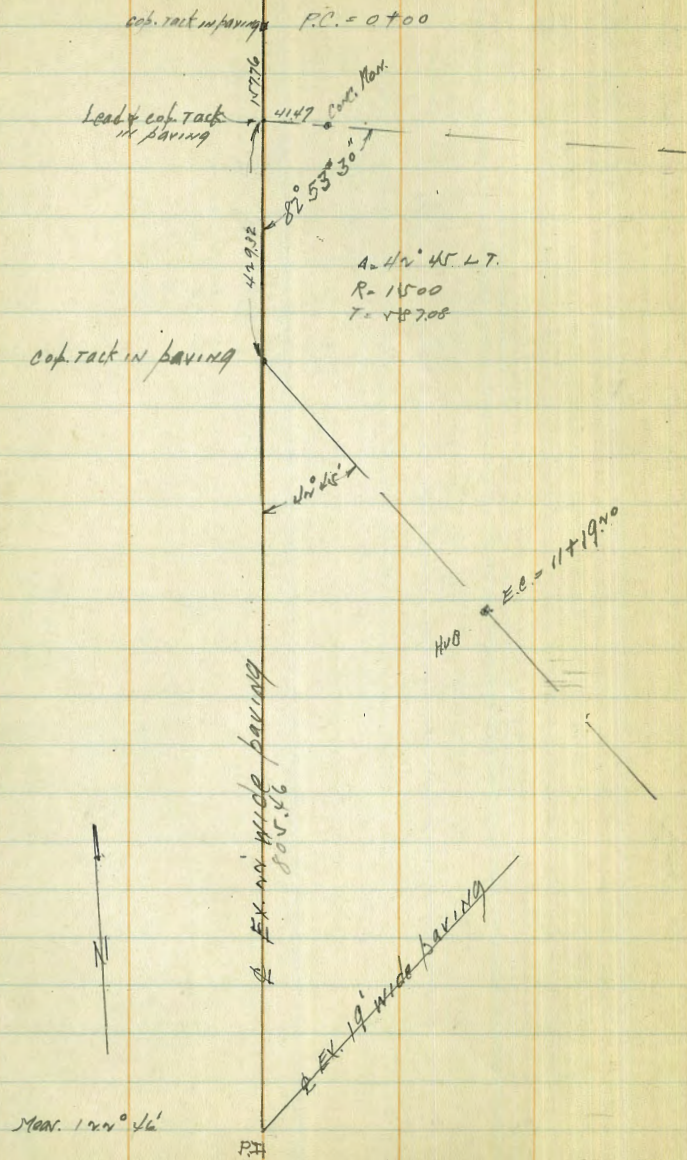
EL

2

40+147 = EC.		201.0
40+54		193.0
40+95		198.0
41+88.5		186.0
43+94		176.5 ✓
45+17		184.3
46+03.5	$\Delta = 9^{\circ}00' RT$	202.5
47+72.3 = PI	$R = 1500 - 75000$	316.0
48+52	$T = 118.5$	291.0
48+90 = EC		311.0
50+62		336.0 ✓
52+10		309.0
53+11 = P.O.T.		352.2
54+03		318.0
55+41		343.2 ✓
60+84 = P.L.	$\Delta = 11^{\circ}00' LT$ $R = 8000$	343.7
63+43 = P.O.T.		376.0
66+90		377.0
68+70		353.0
69+35		369.0
69-45 = P.O.T.		392.5
74+00 P.L.	$\Delta = 26^{\circ}19' RT$ $R = 1500$	405.2
77+57 = HAWK PC of EXPANING		418.0

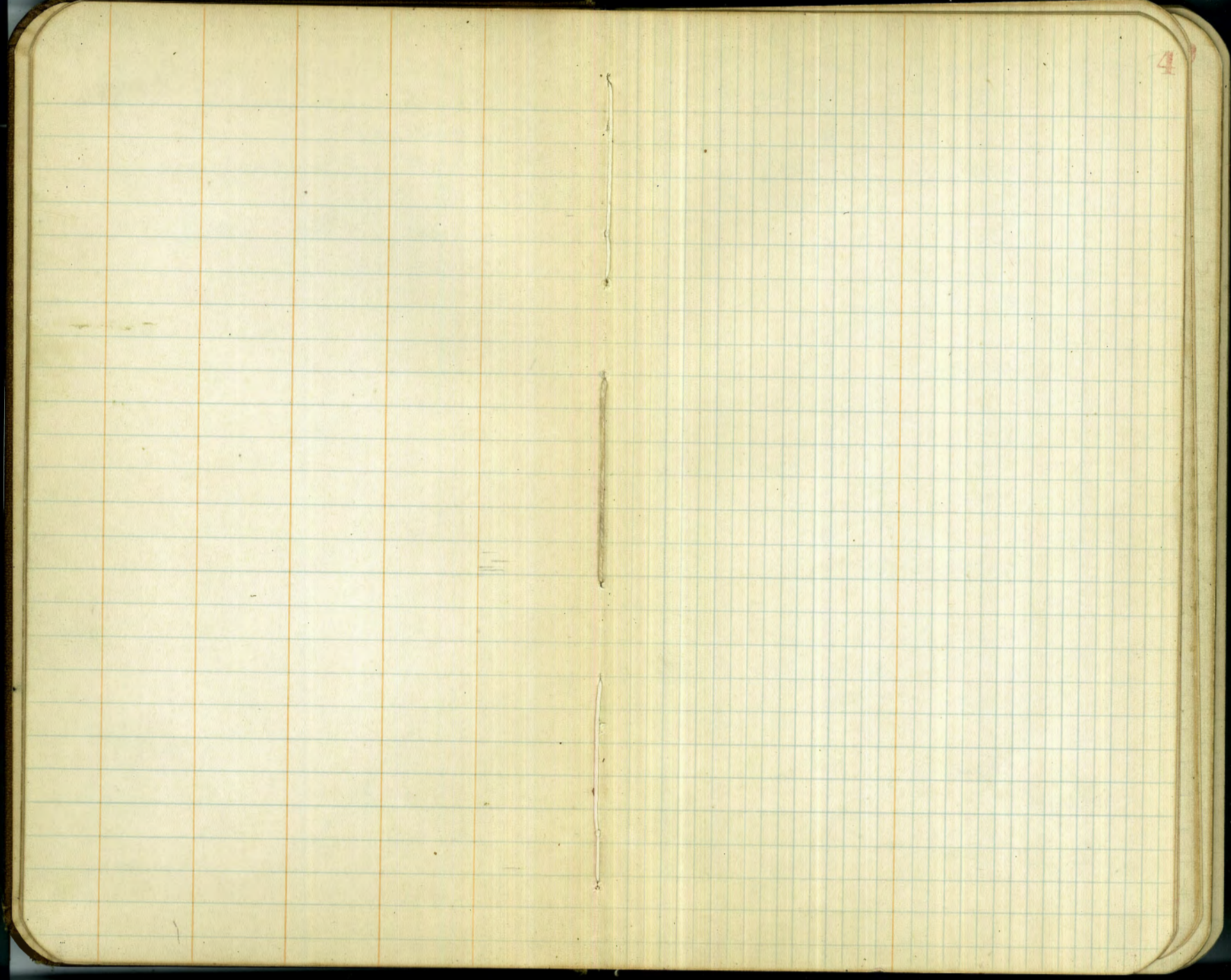
Torrey Pines Grade

11/9/28



$P.C. = 0+00$
 $E.C. = 11+19.20$
 $P.O.T. = 15+80.91$ xx
 $P.O.T. = 18+20.14$ xx
 $P.O.T. = 23+19.64$
 $P.O.T. = 26+17.03$ xx

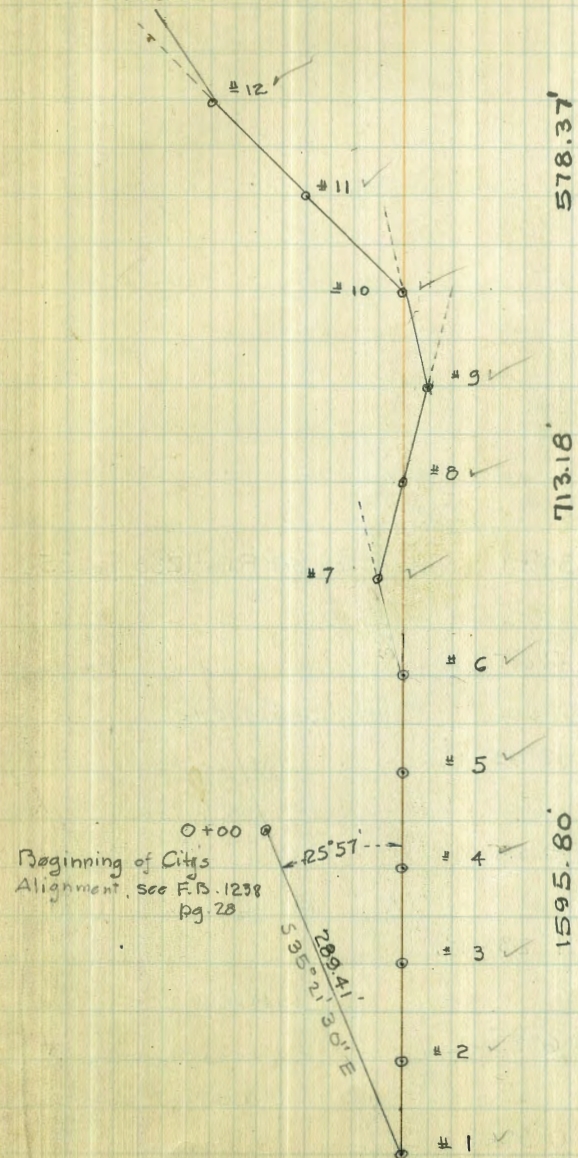
Record $A = 122^{\circ} 50'$ For Torrey Grade
 $R = 125'$
 $T = 229.13$



Control Traverse along Scripps Proposed Alignment and Ties. to City's Alignment
See F.B. 1238, pg. 28

	Bearing	
12	0°59'	
	493.78' ✓	N59°46'30"W ✓
11	P.O.T.	
	84.59' ✓	
10	22°47'-L	
	123.80	N36°53'30"W ✓
9	4°36'-L	
	499.44	
8	P.O.T.	
	213.74'	N32°17'30"W ✓
7	2°17'-R	
	383.92	N34°34'30"W ✓
6	25°10'-L	
	225.77'	
5	P.O.T.	
	101.53'	N9°24'30"W ✓
4	P.O.T.	
	425.09	
3	P.O.T.	
	556.04'	
2	P.O.T.	
	286.77	
1		

JAEGER
Bailey
Clarett
Brooks } Dec. 24th 1928.



578.37'

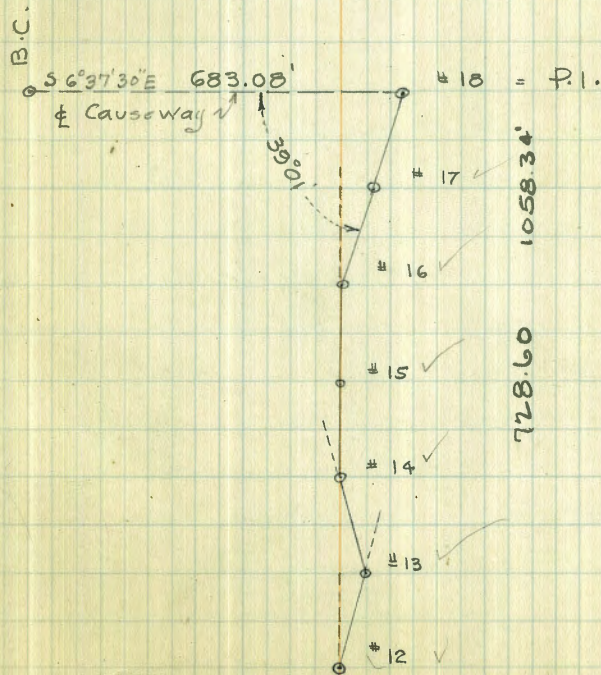
713.18'

1595.80'

Plotted
F.C.L.
Feb 5, 1929

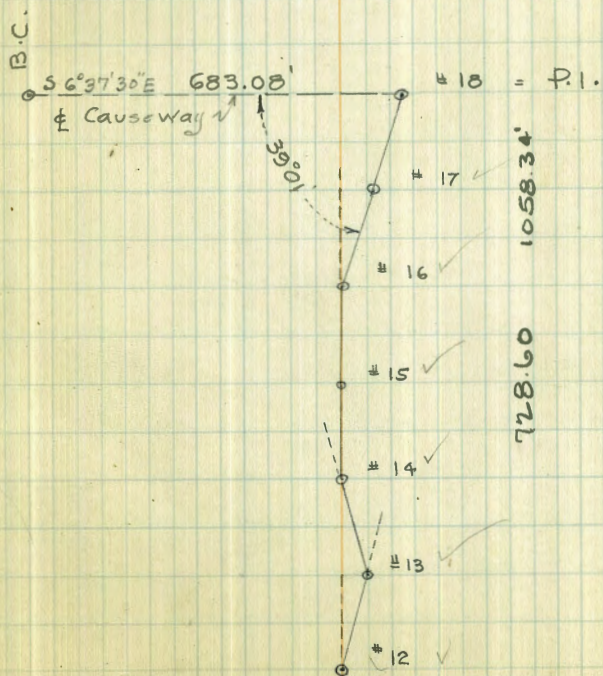
Bearing

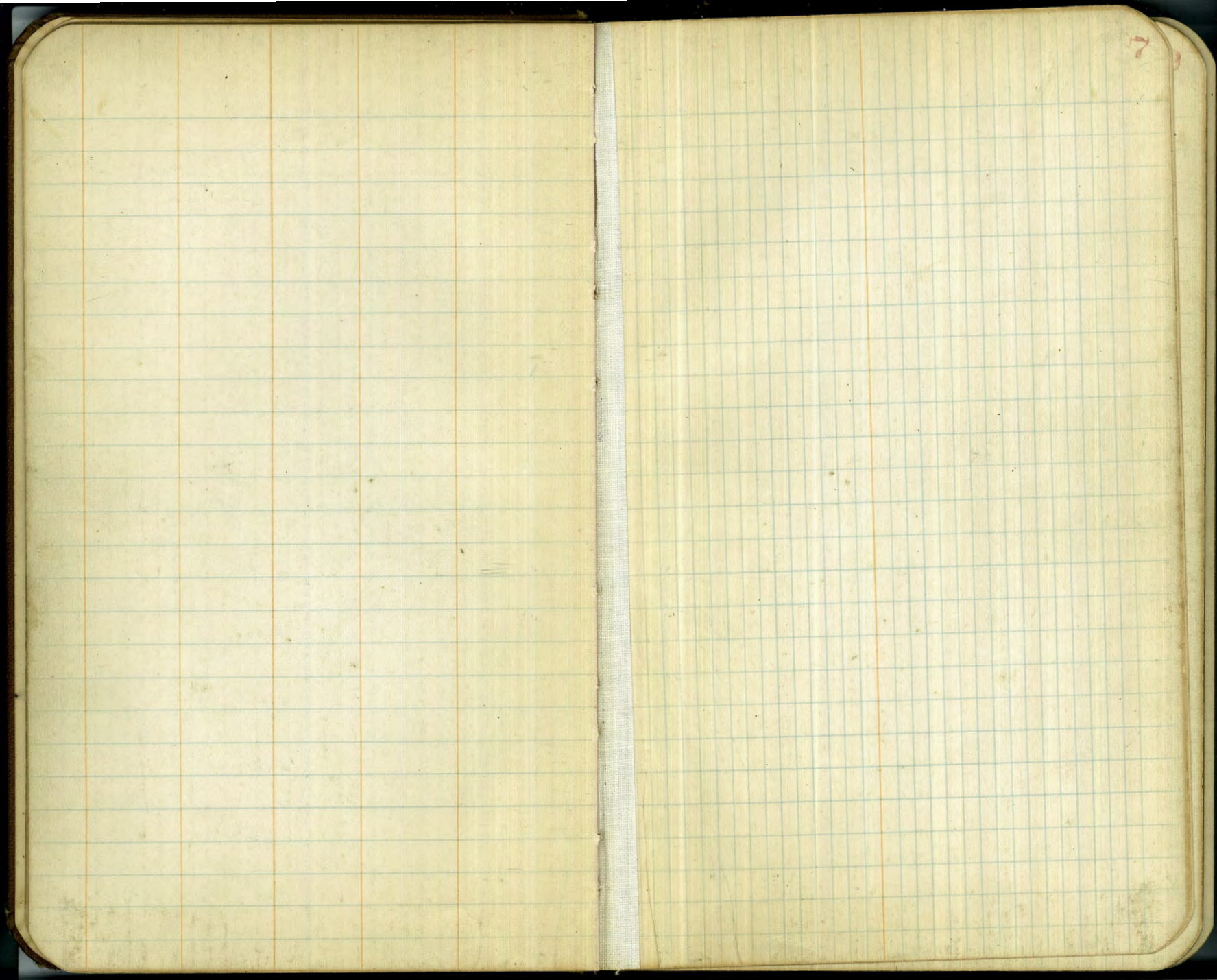
18	39°01'	= P.I. see F.B. 1238, pg. 35
	604.15'	
17	P.O.T.	
	454.19	N45°38'30"W
16	18°03'-R	
	316.03	
15	P.O.T.	
	412.57	N63°41'30"W ✓
14	1°23'-R	
	499.95'	N65°24'30"W ✓
13	6°23'-L	
	340.01'	N58°41'30"W ✓
12	0°59'-R	
		N59°40'30"W ✓

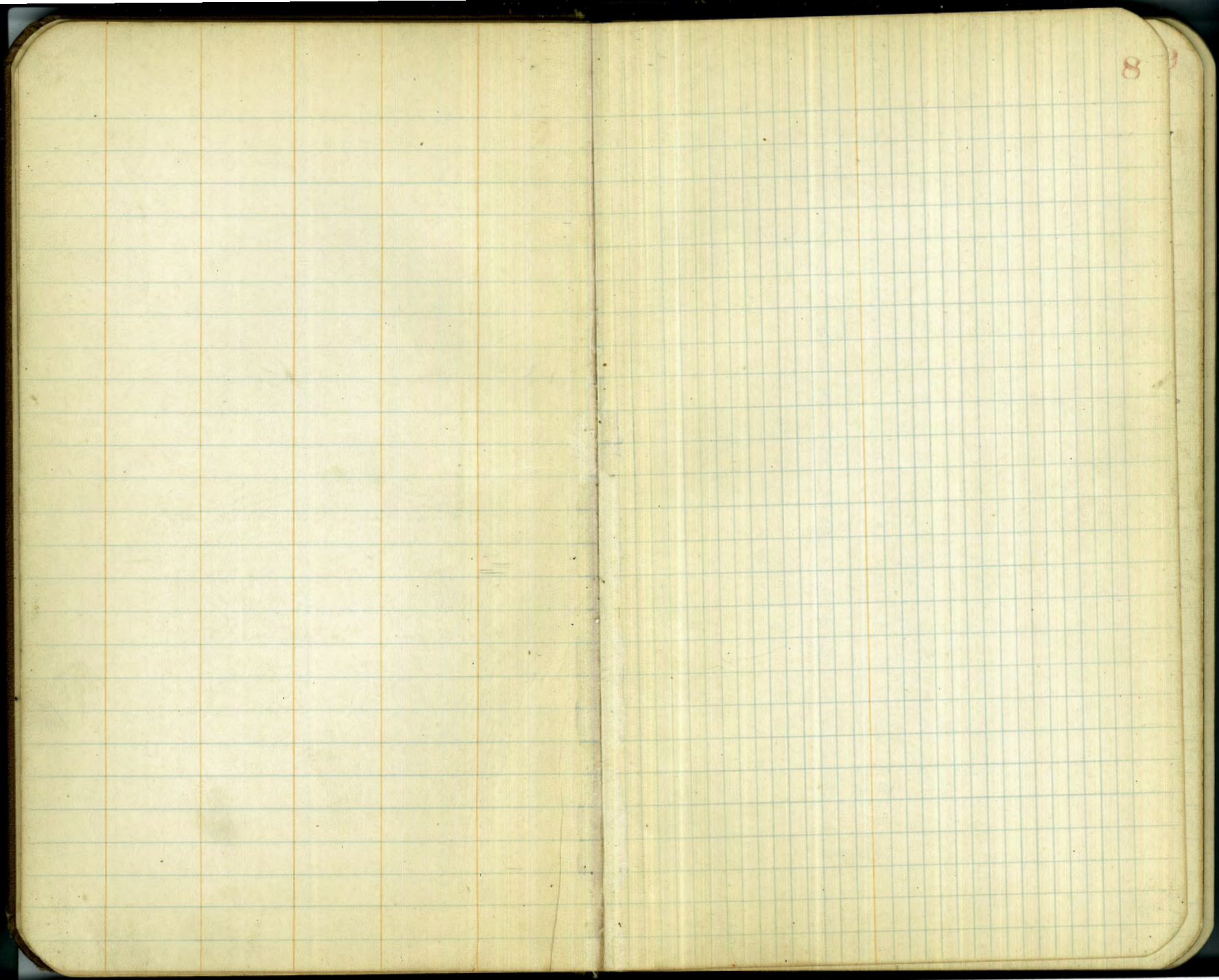


Bearing

18	39°01'	= P.I. see F.B. 1238, pg. 35
	604.15'	
17	P.O.T.	
	454.19	N45°38'30"W
16	18°03'-R	
	316.03	
15	P.O.T.	
	412.57	N63°41'30"W ✓
14	1°23'-R	
	499.95'	N65°04'30"W ✓
13	6°23'-L	
	340.01	N58°41'30"W ✓
12	0°59'-R	
		N59°40'30"W ✓







Levels from B.C. on Pavement (assumed Elev.

350) to Existing City's B.M. at End of Rose Canyon. 9

+	H.I.	-	Elev.
			350.00
12.87	362.87		
		0.09	362.78
11.67	374.45		
		0.40	374.05
13.26	387.31		
		0.12	387.19
12.80	399.99		
		0.39	399.60
12.14	411.74		
		0.99	410.75
12.75	423.50		
		0.60	422.90
10.05	432.95		
		1.20	431.75
7.02	438.77		
		8.38	430.39
1.43	431.82		
		12.60	419.22
1.22	420.44		
		12.75	407.69
1.50	409.19		
		7.75	401.44
7.84	409.28		

+	H.I.	-	Elev.
		1.71	407.87
9.30	417.17		
		0.10	417.07
12.10	429.22		
		1.08	428.14
12.23	440.37		
		10.81	429.56
2.35	431.91		
		10.95	420.96
12.71	433.67		
		1.18	432.49
8.92	441.41		
		1.95	439.46
9.17	448.63		
		9.02	439.61
1.57	441.12		
		12.75	428.37
3.51	431.88		
		3.20	428.68
2.02	430.70		
		6.26	424.44
11.95	436.39		
		1.88	434.51
12.80	447.31		
		7.67	442.64

STA	+	H.I.	-	Elev.
	1.36	444.00		
			9.37	434.63
	3.61	438.24		
			12.52	425.72
	1.15	426.87		
			6.40	420.47
	2.56	423.03		
			11.69	411.34
	0.08	411.42		
			7.15	404.27
	1.77	406.04		

BM. 394.985 City Datum 7.48 398.56

398.56 Assumed Elevation

Subtract 3.57 from Elevations in Book 1238.

Topographic around Scripps Proposed Alignment

JAEGER
Bailey
Claver
Brooks

Dec. 31st 1928.

11

Sta.	Defl. & Dist.	VA.	Horiz. Dist.	Diff. Elev.	Elevation	
1-A	Foresight to STA. ①				354.03	
✓	19°00'-L 105'	+1°50'	105'	+ 3.36	357.39	East Edge Pavement
✓	41-12-L 285'	-3°04'	284'	+ 15.22	369	
✓	39-23-L 112'	-1°15'	112'	- 2.44	352	
✓	57-31-L 235'	-1°44'	235'	- 7.10	347	
✓	91-36-L 260'	-4°52'	259'	- 21.97	332	
✓	66-38-L 102'	-8°29'	100'	- 14.88	339	
✓	94-26-L 135'	-9°10'	132'	- 21.34	333	
✓	75-04-L 53'	-15°21'	49'	- 13.52	340	
✓	68-05-L 25'	-6°15'	25'	- 2.71	351	
✓	150-41-L 95'	-14°40'	89'	- 23.29	331	
	Fore sight to STA ②					
✓	7-45-L 110'	-1°25'	110'	- 2.72	351	
✓	17-45-R 171'	-8°33'	167'	-25.14	329	
✓	9-16-R 267'	-5°59'	265'	- 27.29	327	
✓	7-53-L 207'	-3°41'	206'	- 13.27	341	
✓	16-12-L 270'	-2°55'	269'	- 13.80	340	Edge of Bluff
✓	28-48-L 246'	-1°47'	246'	- 7.65	346	East Edge Pavement
✓	6-48-L 284'	-2°00'	284'	- 9.91	344	Edge of Bluff.
✓	25-55-L 270'	-2°20'	270'	- 10.99	343	
✓	15-20-L 280'	-2°00'	280'	- 9.77	344	
	242'	-4°27'		- 18.72	335.31	STA. ②
2	Fore sight to Sta. 3				335.31	
	5-19-L 12	-28°40'	9.3	- 5.13	330	x
	32-22-L 26	-5°25'	23	- 2.4	333	

Plotted - A.C.L.
Feb. 5, 1929

STA	Defl. g	Dist.	V.A.	Horiz. Dist.	Diff. Elev.	Elev.
✓ 27-57-L	96'	-4°44'	96'	- 8.0	327	
28-18-L	103'	+5°26'	103'	+ 7.94	343.25	STA. 2-A
Z-A	Backsight to		STA 2			
✓ 154-30-R	77'	-33-6	54'	- 35	308	
✓ 123-45-R	105'	-39-55	62'	- 52	291	
✓ 2°-00-R	54'	-0°30'	54'	- 1.4	342	247
✓ 3-30-R	54'	-4°15'	54'	- 4.0	339	7
✓ 108-15-R	136'	-36°45'	88'	- 65.0	278	
✓ 110-30-R	150'	-39-10'	90'	- 74.	269	
✓ 35-15-R	54'	-32-50	39'	- 24	319	
✓ 106-30-R	170'	-33-30	119'	- 78	265	
✓ 95-45-R	35'	-39-30	21'	- 17	326	
✓ 101-15-R	200'	-29-28	151'	- 86	257	
✓ 98-15-R	30'	-48-00	13'	- 17	326	
✓ 106-45-R	246'	-32-17	171'	- 109	234	
✓ 55-15-R	75'	-37-41	47'	- 38	305	
✓ 112-30-R	250'	-33-10	175'	- 114	229	
✓ 70-15-R	120'	-38-35	77'	- 59	284	
✓ 70-15-R	130'	-37-45	82'	- 63'	274	-6'
✓ 67-45-R	175'	-86-43	112'	- 84	259	
✓ 122-45-R	260'	-31-30	113'	- 71	272	
✓ 79-30-R	200'	-37-00	124'	- 96	240	-6.5'
✓ 69-15-R	218'	-35-53	142'	- 102	241	
✓ 64-00-R	255'	-32-05	198'	- 123	220	
✓ 62-15-R	270'	-30-30	200'	- 117	226	

STA	Defl. \angle	Dist	V.A.	Horiz. Dist	Diff. Elev.	Elevation
✓ 63-15-R		280'	-32-05	200'	-126	217
✓ 58-00-R		220'	-33-00	155'	-100	243
✓ 84-00-R		275'	-35-40	181'	-130	213
✓ 51-15-R		225'	-27-45	176'	-96	247
✓ 79-15-R		295'	-35-00	199'	-139	204
✓ 78-45-R		315'	-31-25	236'	-145	198
✓ 58-30-R		350'	-28-47	270'	-148	195
✓ 51-45-R		330'	-27-45	260'	-136	207
✓ 44-30-R		340'	-13-46	325'	-78	265
✓ 36-30-R		377'	-10-30	361'	-67	276
✓ 32-30-R		395'	-7-29	395'	-51	292
✓ 27-00-R		430'	-5-28	430'	-41	302
✓ 23-15-R		445'	-4-15	445'	-33	310
✓ 27-00-R		385'	-10-47	370'	-70	273
✓ 21-15-R		425'	-4-45	425'	-35	308
✓ 30-15-R		360'	-14-11	335'	-85	258
✓ 20-00-R		440'	-2-37	440'	-21	322
✓ 17-15-R		450'	-1°00	450'	-8'	335
✓ 14-45-R		450'	+0-08	450'	+1'	344
✓ 18-15-R		350'	-5-20	350'	-33'	310
✓ 14-30-R		440'	-0-42	440'	-5'	338
✓ 12-30-R		410'	+0-40	410'	+5'	348
✓ 14-30-R		410'	-1-30	410'	-10'	333
✓ 11-30-R		380'	+0°22	380'	+2'	345
✓ 7-30-R		390'	+0°20	390'	+2'	345

Torrey Pine 50' high

Plotted A.C.H.

STA	Defl. \angle	Dist.	V.A.	Horiz. Dist.	Diff. Elev.	Elevation
✓ 8-45-R	312	312	-0-14	312'	- 1	342
✓ 10-00-R	235	235	-0-41	235'	- 3	340
✓ 10-45-R	183	183	-0-26	183'	- 5	338
3	563		+6°00'	+58.55	276.76 ✓	277 ✓
Fore-sight to Sta. 2 all angles to Right.						
✓ 84-00-R	122		+21-10	106'	+ 42'	319
✓ 70-15-R	14		+26-17	13'	+ 6	283
✓ 103-45-R	104		+24-13	90'	+ 41	318
✓ 116-30-R	115		+9-15	112'	+ 18	295
✓ 12-45-R	63		+0-25	63'	+ 0	277
✓ 130-45-R	101		+0-28	101'	+ 1	278
✓ 357-30-R	78		-4-12	78'	- 6	271
✓ 139-15-R	108		-6-40	108'	- 13	264
✓ 340-45-R	107		-12-05	103'	- 22	255
✓ 153-15-R	124		-17-00	116'	- 36	241
✓ 339-15-R	96		-11-15	94'	- 18	259
✓ 329-30-R	141		-15-47	131'	- 37	240
✓ 165-15-R	144		-14-30	135'	- 35	242
✓ 324-30-R	184		-20-28	162'	- 60	217
✓ 171-45-R	141		-11-29	135'	- 28	249
✓ 324-00-R	150		-24-28	125'	- 56	221
✓ 168-00-R	154		-5-45	154'	- 15	262
✓ 170-00-R	198		+0-05	198'	+ 0	277
✓ 168-00-R	203		-1-15	203'	- 4	273
✓ 173-00-R	238		+2-46	238'	+ 12	289

Sta. 2 Elev. 335.31

Torrey Pine 20' high

Torrey Pine 12 "

Torrey Pine 6' high

Sta	Defl. \angle	Dist.	V.A.	Horiz. Dist.	Diff. Elev.	Elevation
✓ 181-15-R		195	+0-05	195'	+ 0	277
✓ 194-30-R		170	-4-30	170'	- 13	264
✓ 189-00-R		154	-6-12	154'	- 17	260
✓ 280-00-R		177	-22-20	150'	- 64	213
✓ 188-45-R		200	-3-44	200'	- 13	264
✓ 279-45-R		138	-22-25	119'	- 49	228
✓ 198-30-R		166	-7-52	166'	- 23	254
✓ 268-30-R		95	-19-35	84'	- 30	247
✓ 206-30-R		177	-12-28	168'	- 39	238
✓ 288-45-R		70	-21-40	61'	- 24	253
✓ 301-30-R		110	-25-28	90'	- 43	234
✓ 203-45-R		205	-11-00	198'	- 39	238
✓ 312-30-R		93	-32-35	68'	- 42	235
✓ 326-15-R		73	-28-20	57'	- 31	246
✓ 166-00-R		286	+7-20	286	+ 36	313
✓ 159-45-R		316	+6-40	316	+ 37	314
✓ 253-30-R		33	-13-36	32'	- 1	276
✓ 149-45-R		337	+11-39	324'	+ 66	343
✓ 218-30-R		40	-41-00	23'	- 20	257
✓ 138-30-R		354	+8-32	354'	+ 52	329
✓ 184-00-R		40	-39-00	24'	- 20	257
✓ 165-00-R		390	+8-17	390'	+ 56	333
✓ 171-30-R		415	+11-45	400'	+ 83	366
✓ 180-00-R		430	+6-17	430'	+ 46.65	323.41
✓ 178-45-R		120	-28-30	96'	-	217

Torrey Pine 25' high

Torrey Pine 30' "

Sta # 4

- 10' Bottom Canger
Plotted A.C.L.

STA	Defl. x	Dist.	V.A.	Horiz. Dist.	Diff. Elevation	Elevation	
✓ 166-00-R	440	+7°53'	440'	+ 59	336		
✓ 154-00-R	400	+7°45'	400'	+ 54	331		
✓ 163-00-R	137	-16°25'	126'	- 37	240	- 12' Bott. Canyon	
✓ 154-45-R	145	-14°35'	136'	- 36	241	Bott. Canyon	
✓ 183-45-R	435	+3°33'	435'	+ 27	304		
✓ 186-00-R	415	+2°15'	415'	+ 16	293		
✓ 148-45-R	174	-9°24'	174'	- 28	249	Bott. "	
✓ 188-30-R	375	+0°42'	375'	+ 5	282		
✓ 145-00-R	210	-4°32'	210'	- 17	260	Bott. "	
✓ 187-15-R	312	-0°13'	312'	- 1	276	Torrey Pine 20' high	
✓ 143-00-R	237	-1°44'	237'	- 7	270	Bott. Canyon	
✓ 181-00-R	290	-0°32'	290'	- 3	274		
✓ 142-15-R	277	+1°10'	277'	+ 6	283	Bott. "	
✓ 179-15-R	255	+0°20'	255'	+ 2	279		
✓ 140-15-R	274	+3°37'	274'	+ 17	294		
✓ 183-45-R	240	-3°30'	240'	- 15	262		
✓ 142-45-R	315	+3°00'	315'	+ 16	293	Bott. "	
✓ 148-00-R	342	+6°32'	342'	+ 38	315		
✓ 159-45-R	230	+2°25'	230'	+ 10	287		
✓ 155-15-R	240	+2°22'	240'	+ 10	287	Two small Torrey Pines	
✓ 144-15-R	360	+7°10'	360'	+ 45	322		
✓ 147-15-R	227	+2°26'	227'	+ 10	287	Torrey Pine 8' high	
✓ 142-00-R	350	+5°40'	350'	+ 34	331		
✓ 138-45-R	314	+6°40'	314'	+ 36	313		
✓ 134-00-R	275	+6°05'	275'	+ 29	306		

STA	Defl. \angle	Dist.	V.A.	Horiz. Dist.	Diff. Elev.	Elevation
✓ 149-30-R		255'	+1°41'	255'	+ 8	285
✓ 131-00-R		215'	+4°52'	215'	+ 18	295
✓ 145-00-R		275'	+4°05'	275'	+ 19	296 X
# 4	Fore sight to STA. 5					323.41
✓ 60-45-R		100'	-23°25'	70'	- 36	287
✓ 9-15-L		64'	-8°00'	63'	- 8.8	314
✓ 95-45-R		100'	-33°30'	70'	- 46	277
		104'	-9°41'		- 17.24	306.17
✓ 89-45-R		140'	-32°10'	100'	- 62	261
✓ 8-00-R		85'	-15°30'	79'	- 22	301
✓ 50-15-R		115'	-24°30'	95'	- 43.5	380 280
✓ 15-45-R		110'	-16°00'	106'	- 29.3	294
✓ 56-45-R		70'	-22°55'	60'	- 25	298
✓ 33-45-R		39'	-18°23'	35'	- 11.5	312
✓ 1-15-R		115'	-11°20'	111'	- 22	301
✓ 33-30-L		34'	+1°35'	34'	+ 0.95	324
✓ 32-45-L		77'	+0°54'	77'	+ 1.13	325
✓ 30-30-L		124'	+1°15'	124'	+ 2.7	326
✓ 32-00-L		137'	+1°21'	137'	+ 3.2	326 X
# 6	Backsight to Sta. 5					242.53 ✓
✓ 177-15-R		158'	+11°41'	154'	+ 31.5	274
✓ 109-45-R		22'	-1°10'	22'	- 0.45	242 ✓
✓ 179-30-R		125'	+10°52'	121'	+ 23	266 ✓
✓ 102-30-R		70'	-10°22'	68'	- 12.4	230 ✓
✓ 165-45-R		105'	+3°20'	105'	+ 6.1	249 ✓

STA. # 5

STA # 5 Elev. 306.17

Torrey Pines 20' high

Torrey Pine 25' high
Plotted A.C.L.

Sta	Defl. \times	Dist.	V.A.	Horiz. Dist	Diff. Elev.	Elevation	
✓ 77-45-R		100'	-7°15'	98'	- 12.2	230	
✓ 157-00-R		87'	-1°30'	87'	- 2.25	240	Torrey Pines 30' high ✓
✓ 66-15-R		136'	-5°30'	136'	- 12.1	230	" " 10' " ✓
✓ 152-30-R		90'	-2°16'	90'	- 3.65	239	" " 35' " ✓
✓ 49-30-R		164'	-3°41'	164'	- 10.56	232	
✓ 31-30-R		216'	-0°36'	216'	- 2.28	240	" " 30' " ✓
✓ 21-30-R		185'	-0°44'	185'	- 2.38	240	
✓ 36-30-R		168'	-0°55'	168'	- 2.70	240	" " 30' " ✓
✓ 44-45-R		150'	-3°00'	150'	- 7.9	234	" " 30' " ✓
× ✓ 84-30-R		60'	+22°06'	52'	+ 2.1	263	
✓ 255-45-R		96'	-5°35'	95'	- 9.2	233	" " 35' " ✓
✓ 51-45-R		73'	+23°30'	62'	+ 2.7	270	
✓ 231-45-R		93'	-4°30'	93'	- 7.3	235	" " 15' " ✓
✓ 28-00-R		125'	+19°00'	112'	+ 3.9	282	
✓ 177-30-R		80'	-9°30'	78'	- 13	229	
✓ 17-15-R		154'	+20°10'	135'	+ 50.5	293	
✓ 148-45-R		35'	-9°30'	34'	- 5.7	237	" " 20' " ✓
128-00-R		50'					" " 20' " ✓
✓ 155-45-R		100'	-12°00'	95'	- 20.5	222	" " 25' " ✓
14-60-R		190'	+19°15'	170'	+ 59.5	302	
153-30-R		167'	-11°15'	160'	- 3.2	210	" " 12' "
# 7 Foresight to Sta # 9 T35			+8°30'		+ 107.46	175.07 177.63 ✓ Correct -	B.M. # 2 285.09
✓ 349-30-R		660'	+0°35'	660'	+ 6.80	185	
✓ 353-00-R		610'	-0°45'	610'	- 8.1	170	Top of Bluff Torrey Pines 7' high ✓
✓ 356-30-R		625'	-1°37'	625'	- 17.8	160	" " "

STA	Defl. x	Dist.	V.A.	Horiz. Dist.	Diff. Elev.	Elevation
✓ 359-30-R	695'	695'	-1°35'	695'	- 19.3	159
✓ 360-00	714'	714'	-1°25'	714'	- 17.63	160.00 ✓
✓ 1-45-R	680'	680'	-3°15'	680'	- 38.5	139
✓ 2-30-R	660'	660'	-4°42'	660'	- 54	124
✓ 359-30-R	630'	630'	-3°58'	630'	- 43.5	134
✓ 357-00-R	610'	610'	-3°50'	610'	- 41	137
✓ 355-00 R	610'	610'	-2°57'	610'	- 31	147
✓ 352-45 R	596'	596'	-2°22'	596'	- 25	153
✓ 351-30 R	560'	560'	-3°30'	560'	- 34.2	144
✓ 350-00 R	515'	515'	-4°50'	515'	- 43.5	134
✓ 358-30 R	535'	533'	-6°00'	533'	- 56	122
✓ 4-30 R	540'	540'	-7°15'	530'	- 68	110
✓ 6-00 R	610'	610'	-6°42'	610'	- 71	107
✓ 5-00 R	500'	500'	-8°15'	490'	- 71	107
✓ 355-45 R	470'	470'	-7°00'	470'	- 57	121
✓ 350-30 R	475'	475'	-5°57'	475'	- 49	129
✓ 0-00	443'	443'	-8°35'	430'	- 65	113
✓ 0-30 R	290'	290'	-9°49'	283'	- 49	129
✓ 350-00 R	410'	410'	-8°00'	400'	- 56.8	121
✓ 343-15 R	423'	423'	-5°55'	423'	- 43.5	134
✓ 344-15 R	455'	455'	-4°05'	455'	- 32.5	145
✓ 337-00 R	420'	420'	-5°35'	420'	- 41	139
✓ 339-15 R	350'	350'	-7°37'	345'	- 46	132
✓ 345-45-R	337'	337'	-4°45'	337'	- 28	150
✓ 358-00 R	310'	310'	-10°45'	301'	- 71	107

STA #9
Torrey Pine 30' high ✓

" " 30' high
2 " " 40' " "

Plotted - A.C.L.

STA	Def. &	Dist.	V.A.	Horiz. Dist.	Diff. Elev.	Elevation
✓	0-00	220'	- 10°58'	214	- 5.2	126
✓	20-45 R	166'	- 2°25'	166	- 7.1	171
✓	18-15 R	190'	- 3°10'	190	- 10.6	167
✓	15-15 R	138'	- 2°30'	138	- 6.1	172
✓	32-30 R	133'	+ 0°40'	133	+ 1.6	180
✓	7-15 R	131'	- 5°45'	131	- 13.1	165
✓	8-15 R	151'	- 5°40'	151	- 14.8	163
✓	5-30 R	161'	- 8°55'	160	- 24.8	153
✓	4-45 R	136'	- 9°37'	132	- 22.4	156
✓	343-45 R	140'	- 13°28'	132	- 31.8	146
✓	330-30 R	166'	- 13°27'	157	- 37.5	140
✓	325-00 R	195'	- 13°30'	186	- 47.5	130
✓	325-00 R	205'	- 13°55'	193	- 47.5	130
✓	307-00 R	200'	- 12°50'	190	- 43	135
✓	305-00 R	195'	- 11°45'	188	- 39	139
✓	304-45 R	130'	- 15°30'	121	- 33.5	144
✓	347-00 R	90'	- 16°35'	82	- 24.7	153
✓	20-00 R	70'	- 11°30'	67	- 13.7	164
✓	327-45 R	45'	- 17°30'	41	- 13	165
✓	44-30 R	21'	- 1°05'	21	- 0.4	178
✓	85-30 R	53'	+ 14°35'	50	+ 13	191
✓	69-00 R	93'	+ 8°00'	89	+ 12.4	190
✓	85-00 R	95'	+ 15°25'	89	+ 24	202
✓	79-30 R	120'	+ 13°15'	114	+ 26.7	208
✓	112-45 R	126'	+ 20°15'	111	+ 41	219

178

20

STA. # 8

2 Torrey Pine 20' high ✓

" " 20' " ✓

" " 14' " ✓

" " 35' " ✓

2 " " 30' " ✓

" " 20' ✓

" " 15' " ✓

" " 50' " ✓

" " 25' " ✓

STA	Defl. α	Dist.	V.A.	Horiz. Dist.	Diff. Elev.	Elevation
✓ 145-00 R		133'	+16°18'	122	+ 35.2	213
✓ 151-30 R		145'	+8°45'	142	+ 22	200
✓ 155-30 R		155'	+12°45'	148	+ 33.5	212
✓ 161-30 R		130'	+7°10'	128	+ 16.3	194
✓ 160-30 R		100'	+10°15'	97	+ 17.6	198
✓ 170-45 R		135'	+3°30'	135	+ 8.25	186
✓ 165-45 R		177'	+6°00'	175	+ 18.6	197
✓ 165-15 R		202'	+10°00'	195	+ 34.8	213
✓ 171-15 R		220'	+12°05'	207	+ 46	224
✓ 179-15 R		220'	+8°40'	218	+ 33	211
✓ 175-45 R		190'	+10°10'	184	+ 33	211
✓ 183-30 R		250'	+6°00'	250	+ 15.7	194
✓ 186-45 R		210'	+6°15'	210	+ 22.3	200
✓ 177-30 R		290'	+9°05'	283	+ 45.5	224
✓ 185-15 R		390'	+8°20'	382	+ 56	234
✓ 197-00 R		300'	+10°00'	292	+ 51.7	230
✓ 196-45 R		335'	+12°00'	322	+ 68.5	247
✓ 203-30 R		325'	+11°30'	314	+ 64	242
✓ 197-00 R		225'	+6°30'	225	+ 31.2	209
✓ 197-30 R		195'	+4°30'	195	+ 15.5	194
✓ 196-45 R		150'	+1°30'	150	+ 3.9	182
✓ 191-30 R		155'	+3°45'	155	+ 10.25	188
✓ 194-15 R		130'	+1°35'	130	+ 1.3	179
✓ 192-45 R		120'	-1°15'	120	- 2.6	175
✓ 168-30 R		175'	+6°28'	175	+ 19.5	198

2 Torrey Pine 40' ✓

" " 12' ✓

" " 12' ✓

" " 20' ✓

" " 35' ✓

" " 14'

STA	Defl. \angle	Dist.	VA.	Horiz. Dist.	Diff. Elev.
	0-00	392'	+10°04'		+ 67.46
# 9	Foresight to STA. 7, All angles to Right.				
✓	2-15 R	770'	+0°40'	770	+ 9.1
✓	5-00 R	800'	+0°28'	800	+ 6.6
✓	7-00 R	830'	+0°32'	830	+ 7.7
✓	7-45 R	860'	+0°45'	860	+11.30
✓	6-15 R	880'	+1°40'	880	+25.5
✓	4-45 R	900'	+2°10'	900	+34.0
✓	3-15 R	865'	+1°20'	865	+20.2
✓	10-30 R	830'	0°00'	830	~
✓	10-45 R	870'	+1°22'	870	+20.9
✓	11-00 R	910'	+2°39'	910	+42
✓	10-00 R	940'	+3°05'	940	+50.5
✓	5-45 R	930'	+2°30'	930	+40.8
✓	4-15 R	935'	+2°35'	935	+42
✓	3-00 R	900'	+1°54'	900	+30
✓	3-00 R	750'	+0°25'	750	+5.6
✓	4-45 R	690'	-0°23'	690	-4.7
✓	8-30 R	660'	-1°16'	660	-14.7
✓	3-45 R	615'	-1°00'	615	-10.8
✓	358-45 R	650'	+0°06'	650	+1.15
✓	356-45 R	550'	-0°20'	550	-3.4
✓	357-15 R	505'	-1°55'	505	-17
✓	354-45 R	480'	-1°40'	480	-14.2
✓	351-00 R	485'	+0°26'	485	+3.7

Elevation

242.53 X

STA. # 6

160.00 ✓

169

167

168

171

185

194 ✓

180 ✓

160 ✓

181

202

210

201

202

190

165

155

145

149

161

157

143

146

164

Bottom Canyon

STA	Defl. x	Dist.	V.A.	Hor. Dist.	Diff. Elev.	Elevation
✓ 348-00 R		430	0°00'	430	~	160
✓ 349-15 R		413	-1°28'	413	-10.8	149
✓ 351-30 R		400	-4°52'	400	-34	126
✓ 353-15 R		370	-7°22'	365	-47.5	112
✓ 346-30 R		335	-8°55'	320	-59	101
✓ 318-45 R		400'	-6°40'	398	-46.5	114
✓ 311-45 R		376'	-6°45'	374	-44	116
✓ 307-45 R		330'	-9°40'	320	-55	105
✓ 316-45 R		340'	-9°28'	330	-56	104
✓ 326-15 R		277'	-12°30'	268	-59	101
✓ 324-30 R		245'	-15°30'	225	-63	97
✓ 312-15 R		204'	-20°55'	178	-69	91
✓ 296-30 R		170'	-24°28'	141	-64	96
✓ 314-00 R		150'	-24°55'	123	-58	102
✓ 321-06 R		125'	-28°30'	97	-53	107
✓ 321-30 R		75'	-36°45'	48	-35	125
✓ 332-45 R		45'	-24°45'	37	-17	143
✓ 258-45 R		35'	-37°30'	22	-17	143
✓ 213-00 R		23'	-27°00'	22	-9	151
✓ 76-15 R		44'	+12°12'	42	+9	169
✓ 74-00 R		94'	+10°20'	91	+16	176
✓ 128-15 R		90	+12°10'	87	+18	178
128-15 R		63'	+12°52'	60	+14	174
15		123'	+2°05'		+4.46	164.46

160

27

Torrey Pine 40'

" " 25'

" " 25'

STA. # 10

STA	Defl. x	Dist.	V.A.	Horiz. Dist.	Diff. Elev.	Elevation
#10	Foreight to STA. #11, all Angles to Right					164.46
✓ 205°30R	88'	-0°25'	88	-0.65	164	
✓ 216-45R	67'	+3°30'	67	+4.1	168	
✓ 228-30R	58'	+6°20'	57	+6.4	171	
✓ 248-45R	23'	+9°40'	22	+3.85	168	
✓ 350°00R	42'	-0°50'	42'	-0.62	162	
✓ 354-30R	20'	-15°39'	18.5	-5.2	159	
✓ 356-30R	70'	-3°50'		-4.7	160	
	85'	-5°25'		-7.99	156.47 ✓	
✓ 304-00R	42'	+11°15'	41	+8.0	172	
✓ 260-30R	75'	+10°53'	74	+14.0	178	
✓ 261-15R	105'	+10°00'	104	+18.2	183	
✓ 7-15R	85'	-8°43'	83	-12.5	152	
✓ 9-15R	85'	-12°20'	82	-17.5	147	
✓ 25-00R	95'	-20°20'	83	-33	131	
✓ 33-45R	95'	-21°52'	82	-33	131	
✓ 38-00R	115'	-26°42'	92	-46	118	
✓ 45-30R	150'	-25°40'	123	-64	100	
✓ 54-30R	198'	-20°10'	175	-67	97	
✓ 68-15R	190'	-22°26'	160	-67	97	
✓ 71-30R	140'	-28°10'	110	-58	106	
✓ 60-30R	105'	-35°17'	70	-50	114	
✓ 89-00R	100'	-39°50'	59	-49.5	115	
✓ 87-30R	137'	-37°00'	98	-61	103	
✓ 78-15R	157'	-24°45'	130	-61	103	

Brink of Cliff

" " "

" " "

" " "

" " "

Bott. " "

Brink " "

STA. #11

Torrey Pine 20 feet

STA	Defl. \angle	Dist	V.A.	Horiz. Dist.	Diff. Elev.	Elevation
✓ 85-00R		196	-21°30'	170	- 67	97
✓ 86-00R		250	-20°46'	218	- 83	81
✓ 86-00R		294	-19°47'	260	- 94	70
✓ 98-15R		320	-19°15'	270	- 100	64
✓ 104-15R		270	-20°38'	238	- 90	74
✓ 99-00R		213	-24°25'	175	- 80	84
✓ 99-30R		185	-27°07'	147	- 75	89
✓ 104-30R		145	-28°35'	113	- 61	103
✓ 110-15R		130	-27°14'	103	- 53	111
✓ 112-30R		100	-28°00'	78	- 42	122
✓ 125-00R		95	-30°18'	71	- 42	122
✓ 151-30R		120	-30°05'	90	- 52	112
✓ 145-30R		155	-27°53'	121	- 64	100
✓ 140-00R		195	-24°04'	163	- 73	91
✓ 154-00R		215	-21°36'	185	- 74	90
✓ 168-30R		190	-21°49'	163	- 66	98
✓ 170-00R		145	-24°35'	120	- 55	109
✓ 176-00R		111	-24°28'	91	- 42	122
✓ 183-00R		86	-24°00'	71	- 32	132
✓ 157-00R		90	-35°12'	60	- 42	122
✓ 147-45R		101	-33°22'	70	- 45	119
✓ 144-30R		103	-37°40'	65	- 50	114
✓ 185-45R		66	-30°22'	49	- 29	135
✓ 212-15R		43	-31°00'	43	- 19	145

Plotted A.C.L.

STA	Defl. \angle	Dist.	V.A.	Horiz. Dist.	Elev. Diff.	Elevation	
✓ 105-15R		55'	-44°16'	28	-27	137	
✓ 97-00R		27'	-42°35'	14.6	-13.5	150	
#11	Fore sight to STA #12, all angles to Right					156.47	✓
		509'	-9°02'		-78.95	77.52	<u>73.82 correct</u>
✓ 284-30R		65'	+1°30'	65'	+1.7	158	Terra Pine #12 ✓
✓ 355-30R		490'	-8°50'	480'	-75	81	
✓ 248-00R		69'	+8°45'	67'	+10.4	167	
✓ 348-30R		470'	-8°10'	460'	-66.5	90	
✓ 247-30R		107'	+9°20'	103'	+17.2	174	
✓ 4-45R		530'	-9°15'	515'	-84.5	72	
✓ 282-30R		130'	+1°55'	130'	+4.3	161	
9-45R		572'	-9°16'	560'	-91	65	
✓ 14-15R		475'	-10°52'	458'	-89	67	
✓ 324-00R		64'	-8°00'	62'	-8.9	147	
✓ 7-30R		460'	-10°18'	445'	-81	75	
✓ 340-00R		37'	-12°18'	35'	-7.7	148	
✓ 0-00		440'	-9°50'	428'	-74.5	82	
✓ 29-15R		35'	-21°16'	30.5'	-12	144	
✓ 353-30R		440'	-9°19'	430'	-71	85	
✓ 354-30R		70'	-15°00'	65'	-17.5	139	
✓ 348-00R		427'	-8°47'	420'	-65	91	
✓ 347-00R		105'	-12°55'	99'	-23	133	
✓ 336-30R		365'	-9°00'	355'	-56.5	100	
✓ 342-45R		365'	-9°30'	355'	-60	96	

Sta	Defl. x	Dist.	V.A.	Horiz. Dist.	Diff. Elevat.	Elevation
✓ 355-00R		355	-11°28'	340	-70	86
✓ 355-30R		345	-12°28'	330	-73	83
✓ 356-15R		330	-12°10'	318	-69	87
✓ 12-00R		328	-14°05'	308	-78	78
✓ 12-30R		335	-14°35'	312	-81.5	75
✓ 13-00R		340	-13°36'	320	-77.5	79
✓ 17-45R		400	-12°19'	385	-84	72
✓ 30-45R		350	-14°40'	325	-86.5	70
✓ 31-30R		350	-15°22'	322	-89	67
✓ 31-30R		340	-15°15'	315	-87	69
✓ 39-45R		330	-15°56'	305	-88	68
✓ 48-15R		300	-16°10'	278	-81	75
✓ 59-00R		290	-14°31'	271	-71	85
✓ 68-15R		285	-17°05'	260	-80	76
✓ 61-45R		236	-18°26'	212	-71	85
✓ 69-00R		235	-19°02'	210	-73	83
✓ 49-30R		190	-20°53'	166	-64	92
✓ 58-15R		143	-25°51'	116	-61.5	94
✓ 54-30R		125	-25°30'	102	-48.5	108
# 12	Foresight to Sta. #11, all angles to Right					73.82
	353-15R	395	+4°00'	395	+27.8	112.00
✓	3-45R	390	+7°30'	380	+51.0	125.00
✓	358-15R	370	+5°07'	370	+33.3	107.00
✓	14-00R	380	+7°16'	375	+48	122.00

STA	Defl. x	Diat.	V.A.	Horiz. Diat.	Diff. Elev.	Elevation
✓ 356-45R		415	+7°10'	405	+52	126
✓ 15°15R		410	+7°54'	400	+56	130
✓ 356-30R		435	+7°47'	425.5	+60	134
✓ 10-45R		420	+8°00'	410	+58.5	132
✓ 3-00R		335	+5°35'	335	+33	107
✓ 5-00R		295	+3°54'	295	+20	94
✓ 20-30R		400	+7°45'	390	+54	128
✓ 25-00R		476	+8°50'	465	+72.21	146
✓ 26-45R		430	+7°15'	420	+54.5	128
✓ 29-00R		290	+6°00'	290	+30.5	104
✓ 31-30R		370	+6°42'	370	+43	117
✓ 37-00R		330	+7°25'	325	+42.5	116
✓ 84-00R		145	+7°31'	142	+19	93
✓ 114-00R		115	+5°00'	115	+10.1	84
✓ 142-00R		110	+2°30'	110	+4.8	79
✓ 180-15R		117	-1°22'	117	-2.8	71
✓ 214-00R		143	-4°55'	143	-12.3	62
✓ 225-30R		190	-5°20'	190	-17.8	56
✓ 220-30R		293	-4°16'	293	-21.8	52
✓ 158-00R		204	+2°50'	204	+10.2	84
✓ 215-30R		335	-2°00'	335	-11.8	62
✓ 146-15R		255	+4°15'	255	+19	93
✓ 145-00R		315	+5°00'	315	+27.5	102
✓ 215-30R		380	-1°00'	380	-6.7	67

Torrey Pine 7'

BM. #3 149.60

- 3.57

146.03 ✓

72.21

73.82

STA	Defl. x	Dist.	V.A.	Horiz. Dist.	Diff. Elevation	Elevation
✓ 153-00R	355	355	+4°20'	355	+27	101
✓ 204-15R	325	325	-0°35'	325	-3.3	71
✓ 160-15R	280	280	+4°00'	280	+19.8	94
✓ 201-30R	295	295	-1°30'	295	-7.8	66
✓ 167-00R	244	244	+2°00'	244	+8.6	83
✓ 200-30R	250	250	-2°10'	250	-9.5	64
✓ 170-15R	315	315	+3°03'	315	+16.8	91
✓ 191-00R	216	216	-1°17'	216	-4.8	69
✓ 171-30R	355	355	+2°23'	355	+14.7	89
✓ 190-30R	293	293	+0°26'	293	+2.2	76
	340		+1°55'		+11.36	85.18
✓ 193-30R	350	350	+0°40'	350	+4.1	78

STA. 13

#13	Foresight	to #14, all angles to Right				
	500'	-0°53'	500'	-7.70	85.18	*
✓ 95-00R	76'	-5°15'	76	-6.9	77.48	
✓ 271-30R	175'	+5°17'	175	+16.3	78	
✓ 79-15R	114'	-5°00'	114	-10.0	101	
✓ 272-00R	115'	+5°10'	115	+10.3	75	
✓ 42-15R	140	-4°09'	140	-10.2	95	
✓ 272-30R	64'	+4°33'	64	+5.1	75	
✓ 20-45R	180'	-3°32'	180	-11.2	90	
✓ 357-15R	160'	-1°52'	160	-5.2	74	
✓ 9-00R	252'	-2°34'	252	-11.5	80	
✓ 336-00R	195'	+0°15'	195	+0.8	74	
					86	

STA. #14

STA	Defl. x	Dist.	V.A.	Horiz. Dist.	Diff. Elevation	Elevation
✓ 6-00 R		330	-2°05'	330	-12.0	73
✓ 322-15 R		220	+1°40'	220	+6.5	92
✓ 10-15 R		360	-2°27'	360	-15.5	69
✓ 326-45 R		340	+2°52'	340	+17.2	102
✓ 4-15 R		390	-1°40'	390	-11.5	73
✓ 336-45 R		374	+1°57'	374	+12.8	98
✓ 0-00		380	-1°10'	380	-7.85	77
✓ 345-30 R		370	+0°50'	370	+5.5	91
✓ 357-15 R		405	-0°45'	405	-5.4	80
✓ 345-15 R		470	+0°50'	470	+6.9	92
✓ 330-00 R		450	+1°22'	450	+10.9	96
✓ 354-15 R		490	-0°15'	490	-2.2	83
✓ 8-15 R		450	-1°52'	450	-14.6	70
✓ 345-15 R		570	+0°48'	570	+8.1	93
✓ 4-15 R		530	-1°20'	530	-12.5	73
✓ 357-00 R		510	-0°35'	510	-5.3	80
✓ 7-15 R		540	-1°45'	540	-16.6	68
#14	Fore sight to Sta. #15, all angles to Right					77.48 77.14
	412	-1°05'			-7.89	69.25
					+7.83	74.21 B.M. #5
✓ 161-30 R	345	-0°50'	345		-5.30	72 + 7.83
✓ 148-30 R	360	-1°29'	360		-9.30	68 - 82.04
✓ 142-30 R	300	-2°28'	300		-13.0	64 - 4.90 H.I.
✓ 132-00 R	375	-4°04'	375		-27	50 77.14 Correct Elev. for Sta. #14

STA. #15

STA	Defl. x	Dist.	V.A.	Horiz. Dist.	Diff. Elev.	Elevation
✓ 130-00R		170	-5°10'	170	- 15.9	61
✓ 149-30R		160	-3°16'	160	- 9.4	68
✓ 127-30R		89	-4°55'	89	- 7.6	69
✓ 104-30R		130	-6°15'	130	- 14	63
✓ 100-45R		204	-6°09'	204	- 22	55
✓ 62-00R		190	-6°22'	190	- 21	56
✓ 314-15R		95	+3°45'	95	+ 6	83
✓ 46-30R		138	-5°38'	138	- 14	63
✓ 301-00R		150	+4°50'	150	+ 13	90
✓ 19-45R		120	-3°46'	120	- 8	69
✓ 309-30R		200	+4°00'	200	+ 14	91
✓ 359-00R		196	-1°53'	196	- 6	71
✓ 322-00R		200	+2°30'	200	+ 9	86
✓ 14-00R		200	-3°00'	200	- 10	67
✓ 326-45R		140	+2°00'	140	+ 5	82
✓ 26-30R		245	-3°50'	245	- 17	60
✓ 340-00R		134	+1°05'	134	+ 2	79
✓ 9-00R		295	-2°04'	295	- 11	66
✓ 357-15R		170	-1°40'	170	- 5	72
✓ 21-00R		340	-3°00'	340	- 18	59
✓ 0-00		290	-1°16'	290	- 6	71
✓ 26-30R		340	-3°27'	340	- 22	55
✓ 354-30R		315	-0°45'	315	- 4	73
✓ 21-15R		360	-2°58'	360	- 19	58

Torrey Pine 9'

STA	Defl. X	Dist.	V.A.	Horiz. Dist.	Diff. Elev.	Elevation
✓ 339-30 R		280	+1°10'	280	+ 6	83
✓ 8-30 R		335	-2°00'	335	- 12	65
✓ 336-30 R		315	+1°47'	315	+ 10	87
✓ 359-00 R		345	-1°10'	345	- 7	70
✓ 330-00 R		300	+2°44'	300	+ 15	92
#15	Foreight	To #16, all angles	To Right			69.25
		314	-1°45'		-9.58	59.67
✓ 89-00 R		50	-6°50'	48	- 5.9	63
✓ 324-30 R		94	+2°45'	94	+ 4.5	74
✓ 91-00 R		104	-6°15'	102	- 11.3	58
✓ 303-15 R		108	+7°41'	106	+ 14.5	84
✓ 89-15 R		155	-6°30'	153	- 17.5	52
✓ 291-00 R		133	+8°54'	131	+ 20.8	90
✓ 88-15 R		205	-5°57'	204	- 21.5	47
✓ 339-30 R		164	+1°18'	164	+ 3.7	73
✓ 73-00 R		216	-7°10'	214	- 27	42
✓ 326-45 R		190	+3°49'	190	+ 12.8	82
✓ 67-45 R		167	-8°16'	165	- 24	45
✓ 321-15 R		216	+7°40'	214	+ 29	98
✓ 56-45 R		114	-8°47'	112	- 17.5	51
✓ 309-45 R		196	+9°03'	190	+ 31	100
✓ 34-15 R		80	-8°18'	78	- 11.5	57
✓ 281-30 R		204	+11°51'	197	+ 41.5	111
✓ 6-30 R		150	-4°14'	150	- 11.2	58

16

Edge Highway

" "

" "

STA	Defl. \angle	Dist.	VA.	Horiz. Dist.	Diff. Elev.	Elevation.	
✓267-30R		220	+11°42'	210	+44	113	Edge Highway
✓23-30R		167	-6°34'	167	-19	50	
✓266-30R		200	+10°05'	193	+34.5	103	
✓36-30R		192	-8°00'	187	-26.8	42	
✓323-45R		236	+6°42'	230	+27.3	96	" "
✓43-30R		240	-8°00'	235	-33.5	36	
✓335-45R		289	+4°43'	289	+24	93	" "
✓48-15R		290	-7°40'	285	-38.5	31	
✓345-00R		360	+2°00'	360	+12.7	82	" "
✓41-30R		335	-7°14'	325	-42	27	
✓348-15R		400	+0°58'	400	+6.9	76	" "
✓32-30R		295	-6°41'	290	-34	35	
✓25-30R		260	-6°04'	258	-27.5	41	
✓5-45R		233	-2°52'	233	-11.7	57	
#16	Fore-sight to STA #17		All angles to Right			59.67	
	489		-5°25'		-43.16	16.51	STA #17
✓67-15-R		59'	-10°33'	57	-10.6	49.	
✓348-30R		385'	-3°18'	385	-22.8	36.8	
✓65-30R		105'	-10°20'	102	-18.6	41.	
✓344-30R		340'	-2°55'	340	-18	41.6	
✓63-15R		156'	-9°35'	151	-25.8	34.8	
✓341-30R		275'	-2°47'	275'	-13.5	46.	
✓63-45R		255'	-8°55'	248	-39.5	20.	
✓334-45R		196'	-2°30'	196	-8.7	51.	

STA	Defl. A	Dist.	V. A.	Hor. Dist	Dif. Elev.
✓ 31-15 R		290	-8°43'	282	-44
✓ 347-00 R		200	-5°23'	200	-19
✓ 353-00 R		230	-6°07'	228	-24.8
✓ 18-00 R		272	-8°27'	265	-40
✓ 354-30 R		290	-5°35'	288	-28.5
✓ 9-00 R		315	-7°15'	310	-39.5
✓ 359-15 R		300	-6°16'	295	-32.5
✓ 16-15 R		350	-7°10'	345	-43.5
✓ 352-15 R		335	-4°35'	335	-26.5
✓ 21-45 R		370	-7°05'	365	-45.5
✓ 337-30 R		340	-0°55'	340	-5.5
✓ 14-45 R		440	-5°53'	438	-45
✓ 340-15 R		320	-0°42'	320	-3.9
✓ 8-00 R		500	-5°10'	500	-45
✓ 336-30 R		265	-0°14'	265	-1.1
✓ 359-15 R		426	-4°55'	435	-37.5
✓ 327-15 R		194	+1°11'	194	+4.0
✓ 353-45 R		380	-4°15'	378	-28
✓ 311-30 R		126	+4°58'	126	+11
✓ 286-00 R		86	+7°43'	84	+11.5
✓ 247-45 R		60	+11°35'	58	+11.7
✓ 296-00 R		55	+5°05'	55	+4.7
✓ 318-15 R		78	-0°00'	78	0.0
✓ 331-45 R		100	-2°47'	100	-4.8

60

34

Elevation

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Edge Highway

Edge Highway

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Plotted A.C.L.

STA	Defl. \angle	Dist.	VA.	Horiz. Dist.	Diff. Elev.	Elevation
	✓ 339-30R	115	-4°25'	115	-8.8	57.
#17	Fore-sight to STA. #18, all angles to Right.					16.51 x
	✓ 10-30R	800	-0°20'	800	-4.7	12
	✓ 13-15R	790	-1°12'	790	-16.6	0
	✓ 68-15R	260	-1°28'	260	-6.7	10
	✓ 25-00R	700	-1°02'	700	-12.8	4 x
	✓ 87-45R	250	-3°20'	250	-14.7	2
	✓ 27-45-R	700	-1°30'	700	-18.5	-2
	✓ 87-00-R	290	-3°14'	290	-16.5	0
	✓ 34-15R	630	-1°45'	630	-19.5	-3
	✓ 40-15R	532	-2°12'	532	-20.6	-4
	✓ 58-00R	274	-4°17'	274	-20.7	-4
	✓ 38-00R	455	-2°35'	455	-20.5	-4
	✓ 46-15R	155	-7°40'	150	-20.5	-4
	✓ 20-00R	510	-2°00'	510	-19.8	-4
	✓ 302-15R	70	-17°45'	64	-20.3	-4
	✓ 16-06R	540	-1°00'	540	-9.5	7
	✓ 269-00R	180	-6°12'	175	-19.5	-3
	✓ 12-00R	555	-1°35'	555	-16.0	0
	✓ 269-45R	280	-3°10'	280	-15.6	1
	✓ 18-30R	580	-1°43'	580	-17.6	-1
	✓ 14-15R	615	-1°10'	615	-12.6	4
	✓ 265-45R	425.	-1°37'	425	-12.1	4
x	✓ 230-00R	615	-0°30'	615	-5.4	11

STA	Defl. α	DIST	V.A.	Hori. Dist	Diff. Elev.	Elevation		
✓ 257-45R		390	-1°05'	390	-7.5	9		
✓ 355-45R		535	-0°35'	535	-5	11 ✓		
✓ 256-15R		320	-0°32'	320	-3	13 ✓		
✓ 356-30R		518	-1°12'	518	-11	5 ✓		
✓ 257-45R		435	+0°31'	435	+4	20 ✓		Edge Pavement
✓ 1°45 R		435	-1°57'	435	-15	1 ✓		
✓ 252-30R		405	+1°19'	405	+9.5	26 ✓	"	"
✓ 5-00 R		404	-1°22'	404	-9.8	7 ✓		
✓ 248-00R		355	+2°26'	355	+15.3	32 ✓	"	"
✓ 10-15 R		355	-2°26'	355	-15.3	1 ✓		
✓ 238-15R		280	+5°00'	279	+24.3	41 ✓	"	"
✓ 15-00R		335	-3°35'	335	-21	-5 ✓		
✓ 232-00R		230	+7°15'	217	+29	45 ✓	"	"
✓ 8-15R		270	-4°20'	270	-20.5	-4 ✓		
✓ 226-00R		200	+9°43'	195	+33.5	50 ✓	"	"
✓ 0-30R		295	-2°25'	295	-12.6	4 ✓		
✓ 350-30R		370	-2°14'	370	-14.5	2 ✓		
✓ 239-15R		215	+4°53'	215	+18.4	35 ✓		Top Edge of Pitt
✓ 344-15R		420	-1°47'	420	-13.3	3 ✓		
✓ 250-00R		245	+1°00'	245	+4.3	21 ✓	"	"
✓ 256-15R		220	-1°30'	220	-5.8	11 ✓	"	"
✓ 330-00R		360	-2°00'	360	-12.7	4 ✓		
✓ 260-15R		220	-2°23'	220	-9.2	7 ✓		
✓ 330-00R		300	-2°49'	300	-14.9	2 ✓		

STA	Defl. &	Dist.	V.A.	Hor. Dist.	Diff. Elev.	Elevation	
✓ 254-15R		220	-1°50'	220	-7.1	9 ✓	Bottom Pitt
✓ 331-30R		220	-2°44'	220	-10.5	6 ✓	" "
✓ 248-45R		230	-1°12'	230	-4.9	11 ✓	" "
✓ 330-45R		180	-6°30'	180	-20.5	-4 ✓	" "
✓ 303-45R		205	-5°46'	205	-20.6	-4 ✓	" "
✓ 257-00R		94	-3°10'	94	-5.2	11 ✓	Edge Pitt
✓ 302°00R		245	-2°53'	245	-12.3	4 ✓	" "
✓ 248-00R		90	+1°53'	90	+2.9	19 ✓	Edge Pitt
✓ 299-15R		345	-2°07'	345	-13	3 ✓	" "
✓ 229-00R		93	+8°42'	91	+14	31 ✓	" "
✓ 282-00R		380	-1°45'	380	-11.7	5 ✓	" "
✓ 225-00R		106	+9°00'	103	+16.5	33 ✓	" "
✓ 276-30R		430	-0°49'	430	-6.2	10 ✓	Edge Highway
✓ 228-45R		155	+7°33'	155	+20.5	37 ✓	" Pitt
✓ 268-45R		425	-1°43'	425	-13	3 ✓	" "
✓ 231-15R		180	+7°30'	180	+23.5	40 ✓	" "
✓ 273-30R		295	-3°00'	295	-15.6	1 ✓	" "
✓ 218-00R		210	+9°45'	205	+3.2	20 ✓	" Highway 20'
✓ 270-15R		445	-0°44'	445	-5.75	11 ✓	" "
✓ 263-45R		445	-0°16'	445	-2.1	14 ✓	" "
258-30R		440	+0°20'	440	+2.6	19 ✓	" "

Plotted - A.C.L.

Sta.	+	π	-	El.	
0+00 \pm Pave.				346.4	
	6.75	353.15			
2+02 \pm	9.80				
Pt #1					
From 0+00 \pm Jaegers Line	8.0	345.1			East edge of Rd. 100' E. of Jaegers Line
Pt #2					
From 1+30	7.0	346.1			East edge of Rd. 115' E. " "
T.P.			6.32	346.83	
	6.90	353.73			
Pt #3					
From 4+50	5.7	348.0			East of \pm 176'
T.P.			14.50	339.27	
	1.2	340.47			
6+10			5.8	334.7	East of Sta. 6+10 (175') El. = 339.3

"A" Line for road in Balboa Park
 From Alabama St. to Park Blvd.

2/6/31
 Loudon R

40

0+00

0+50 B.C.

$$\Delta = 106^{\circ} 10' R$$

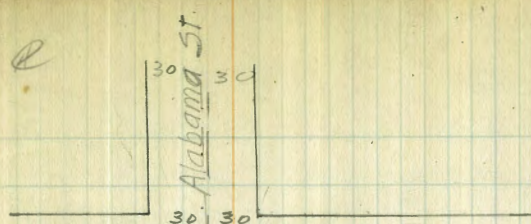
$$R = 500$$

$$T = 665.53$$

$$L = 926.48$$

9+76⁴⁸ EC

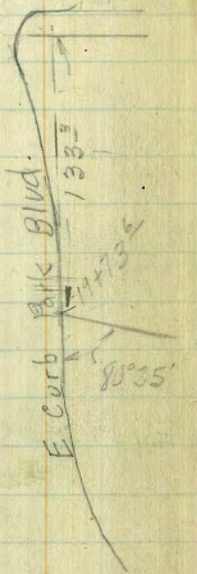
19+73⁵ E curb Park Blvd.



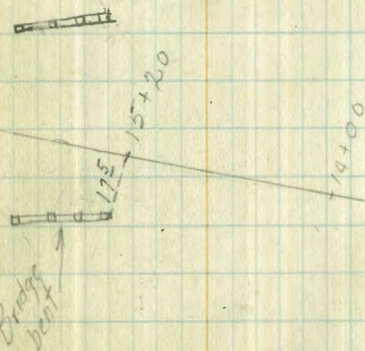
NL Park 0+00

0+50 B.C.

Ubas St.



Does not plot.



19+73⁸

B.M.	3.26	264.76		261.50	Pipe NE Ala. & Upos		215.52
0+00			4.61	260.15		11+00	11.4 204.1
0+50			3.7	261.6		12+00	4.5 211.0
1+50			4.4	260.4		TP 1186	226.44 0.94 214.58
2+50			8.6	256.2		13+00	2.6 223.8
T.P.	1.76	255.90	10.64	254.14		TP 12.79	239.01 0.22 226.22
3+50			7.1	248.8		TP 13.00	251.60 0.41 238.60
TP	0.33	243.43	12.20	243.10		14+00	10.1 241.5
4+50			7.5	235.9		15+00	7.9 243.7
TP	0.30	230.88	12.85	230.58		TP 13.01	263.52 1.09 250.51
TP	0.33	218.28	12.93	217.95		16+00	15.5 248.0
5+50			2.0	216.3		TP 12.90	276.23 0.19 263.33
TP	0.36	206.04	12.60	205.68		17+00	6.6 269.6
6+50			9.5	196.5		18+00	7.6 268.6
T.P.	1.31	194.15	13.20	192.84		18+14	7.6 268.6
7+50			8.3	185.8		18+28	16.5 259.7
8+50			10.9	183.2		18+41	15.5 260.7
8+90			10.4	183.7		TP 12.95	288.98 0.20 276.03
9+10	Stream		14.5	179.6		18+83	5.0 284.0
9+13			10.2	183.9		19+00	1.1 289.9
9+50			3.9	190.2		TP 10.17	298.72 0.43 288.55
T.P.	12.32	203.20	3.27	190.88		19+73 ⁶ cb	4.70 294.02
9+75			15.2	188.0		19+73 ⁶ Pad	5.34 293.38
9+80			10.6	192.6		B.M.	2.96 295.76
10+00			7.9	195.3		S.W. Upos & Park Blvd.	(295.80)
TP	12.60	215.52	0.28	202.92			

"B" Line for road in Balboa Park
 From Alabama at Upos to Park Blvd.

0+00
 1+13⁷² B.C.

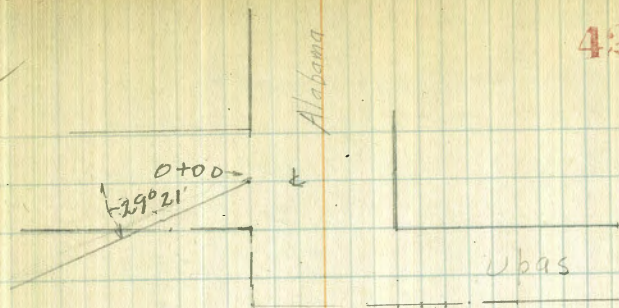
$\Delta = 47^{\circ}55' L$
 $R = 300$
 $T = 133.30$
 $L = 250.89$

3+64⁸¹ E.C.
 4+21⁰⁷ B.C.

$\Delta = 99^{\circ}42' R$
 $R = 300$
 $T = 355.63$
 $L = 522.03$

9+43¹⁰ E.C.
 9+49⁴⁰ 10+00 "A" Line.

Ⓢ



Profile of line shown on
"B" Line

P 42
pipe NE
Up to station.

BM	0.50	262.00		261.50
0+00			2.67	259.33
0+20			6.2	255.8
0+60			8.7	253.3
1+00			9.8	252.2
1+13 ¹² BC			10.2	251.8
1+64 ¹⁰			13.1	248.9
T.P.	0.55	249.47	13.08	248.92
2+14 ²⁸			6.4	243.1
T.P.	0.74	237.25	12.96	236.51
2+64 ⁴⁶			1.7	235.6
3+14 ⁶⁴			10.7	226.6
T.P.	0.44	224.89	12.80	224.45
3+64 ⁸² EC			5.5	219.4
4+21 ⁹⁷ BC			9.3	215.6
5+21 ⁹⁷			20.0	204.9
T.P.	0.25	212.02	13.12	211.77
T.P.	0.76	200.55	12.33	199.79
6+21 ⁹⁷			5.7	194.8
T.P.	1.94	189.28	13.21	187.34
6+41			3.3	186.0
7+21 ⁹⁷			4.9	184.4
8+21 ⁹⁷			4.8	184.5
8+57			5.0	184.3
8+70			8.0	181.3
8+75			4.8	184.5

189.28

T.P.	11.47	199.03	1.72	187.56
9+21+07			7.6	191.4
9+43 ¹² EC			3.8	195.2
9+49 ²⁰ = 10+00 "A" Line			3.6	195.4

Alignment Soledad Road

Rt.

114+65.11 F.C. 19°56.25'

+50 19°04.31'

114 16°12.43'

A 39°52.30'

+50 P 500.0 13°20.54'

T 181.37

113 L 347.98 10°28.66'

D 3.4377

+50 7°36.77'

112 4°44.89'

+50 1°53'

111+17.13 B.C.

Feb. 28. 34
Moore
Silver
Northboro

44



Resort 222 □

8-22-47

See 1324 Page 67

R.

127 + 80.54 E.C.	50° 06'
+50	48° 20.97'
127	45° 29.09'
+50	43° 37.20'
126	39° 45.32'
+50	Δ 100° 12' 26.53.43
125	R 500.0 34° 01.55'
+50	T 598.00 31° 09.66'
124	L 874.41 28° 17.78'
+50	D 343.77 25° 25.89'
123	22° 34.01'
+50	19° 42.12'
122	16° 50.24'
+50	13° 58.35'
121	11° 06.47'
+50	8° 14.58'
120	5° 22.70'
+50	2° 30.81'
119 + 06.13 B.C.	

L1

134+19.26 F.C.

 $15^{\circ}08'25''$

134

 $130^{\circ}16'30''$ $13^{\circ}17'89''$

R 300.0

+50

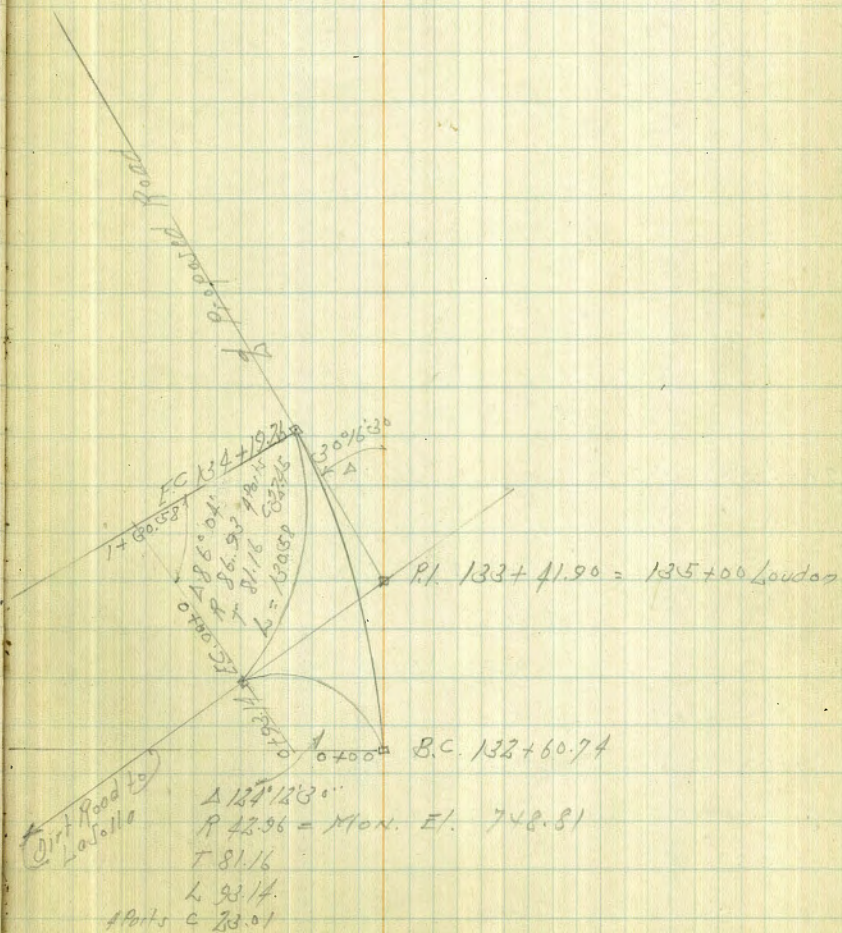
T 81.16 $8^{\circ}31'42''$

L 158.52

133

D 5.7295 $3^{\circ}44'91''$

132+60.74 B.C.



PL

137+64.59 FC

42°34.50'

+50

A 85°09' 38" 23.67

R 100.0

137

T 91.87 24°04.22'

C=1948

L 148.61

+50

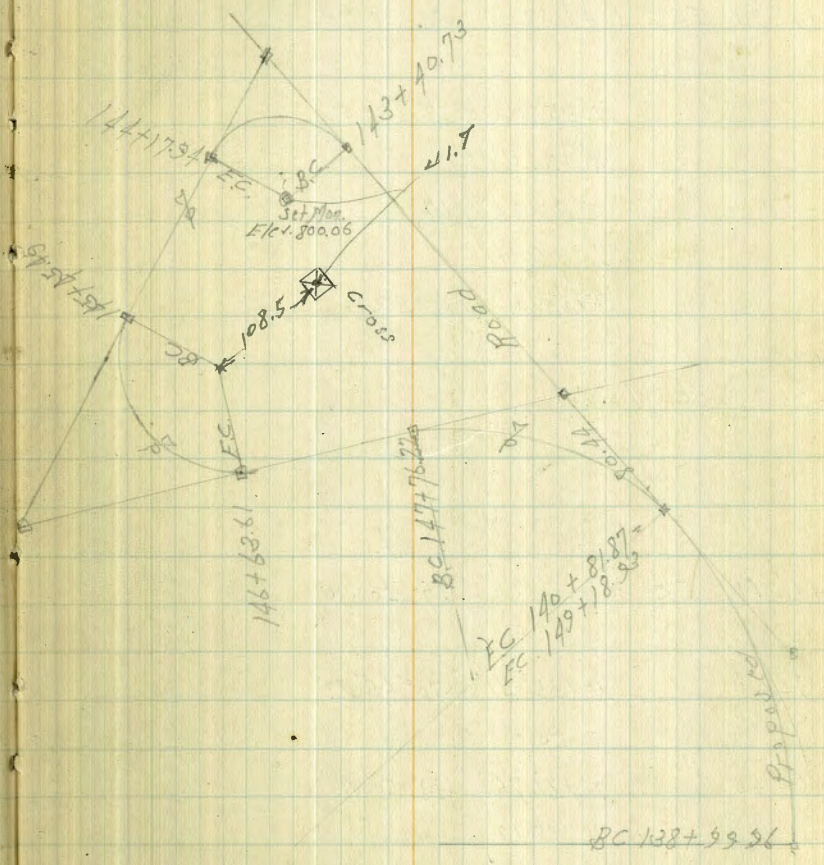
D 171.887 9°44.77'

C=1948

136+15.98 BC

Lt.
 144+17.94 EC. $55^{\circ}17'45''$
 $\Delta 110^{\circ}35'30''$
 143+98.63 R 40.0 $41^{\circ}28'14''$
 T 57.76
 143+79.33 $\Delta 77.21$ $27^{\circ}38'52''$
 C 19.12
 143+60.03 $13^{\circ}49'28''$
 143+40.73 BC Lt.

Lt.
 140+81.87 EC. $20^{\circ}50'75''$
 $\Delta 41^{\circ}41'30''$
 +50 R 250.0 $17^{\circ}11'60''$
 T 95.18
 140 $\Delta 181.91$ $11^{\circ}27'83''$
 D 6.8755
 139+50 $5^{\circ}44'05''$
 138+99.96 BC Lt.



PL

149+18.93 EC = 140+81.87 32° 58.28'

149 Δ 65° 56.30' 28° 36.06'

R 124.0'

+50 T 80.44' 17° 02.91'

L 142.71'

148 D 13.863 5° 22.76'

147+76.22 B.C. PL

LT

146+62.11 EC 67° 10.30'

146+34.08 Δ 135° 21' 50° 45.22'

R 50.0'

146+04.55 T 121.76 33° 50.15'

L 118.12'

145+75.02 C 29.10 16° 55.07'

145+45.49 B.C. LT

± levels on Wye
to Hillside Dr. La Jolla.

50

484 750.99 746.15

B.C. = $\frac{134 + 6074}{0400} =$ S. Leg of Wye

#1 pt. 7.4

#2 pt. 9.3

#3 pt. 11.1

#4 = 04931X = EC. 12.1

1750 14.8

N. Leg of Wye

00 = EC. 12.1

#1 pt. 11.6

#2 pt. 9.5

#3 pt. 7.4

#4 pt = EC = $\frac{134 + 1926}{1730.58}$ 5.1

B.M.^s
Soledad Rd. Loring to
Soledad Park.

Corrected El.^s See 1408-51

51

Indexed
1-24-52
Paw

00-3	33' RT. Contact 1/4 d.	206.85	207.08 ✓
154.88	105' LT. NW Cor. Lower Conc. Step	265.28	265.51
25+06	40' LT. 3/4" pipe	319.56	319.79
41+52.77	40' LT. Conc. Mon.	443.59	443.82 ✓
51+00	45' RT. 1" pipe	513.29	513.52
58+09.89	45' RT. 1" pipe	519.53	519.76
81+00	approx. P.I. Conc. Mon.	560.67	560.90
106+78	P.I. Conc. Mon.	663.56	663.79
119+06.13	40' RT. Conc. Mon.	709.21	709.44
$\frac{124+60.74}{0+00} = 80$	42.96 LT. = R. Mon.	748.81	749.04
143+40.73	40' LT. = R. Mon.	800.06	800.29

Top Ely Peak of Soledad near Easter Cross

Soledad Road Cross Section

Cont From 1324 Page 79

631.50 Ford 1324 Page 79

101+0		
40' Lt	4.2	627.3
20' Lt	3.4	628.1
±	2.8	628.7
20' Pt	1.2	620.3
40' Pt	0.9	630.6
TP	12.33	643.59
0.24 631.26		
101+50		
40' Pt	9.3	634.3
20' Pt	5.9	633.7
±	10.7	632.9
20' Lt	11.9	631.7
40' Lt	14.0	629.6
102+0		
40' Lt	13.0	630.6
20' Lt	10.6	633.0
±	8.0	635.6
20' Pt	5.5	635.1
40' Pt	3.6	640.0
102+50		
40' Pt	0.3	643.3
20' Pt	2.7	640.9
±	5.0	638.6
20' Lt	7.6	636.0
40' Lt	11.5	632.1

643.59

Feb. 23 '34

54

103+0		
40' Lt		6.8
20' Lt		2.2
±		0.8
TP	12.58	656.07
20' Pt		10.6
40' Pt		8.9
103+50		
40' Pt		5.8
20' Pt		6.7
±		8.5
20' Lt		10.4
40' Lt		12.6
103+84.52 85' Lt		
40' Lt		7.1
20' Lt		6.0
± on Hub		4.97
20' Pt		4.0
40' Pt		2.5
104+0		
40' Pt		1.9
20' Pt		3.3
±		4.0
20' Lt		4.3
40' Lt		6.0
TP	12.52	668.46
		0.18

104+49
± on Hub

668.46

104+50		
40 Lt	13.0	655.5
20 Lt	12.8	655.7
1/2	13.4	656.1
20 Pt	11.7	656.8
40 Pt	10.8	657.7

105+50

40 Pt	9.3	659.2
20 Pt	9.0	659.5
1/2	9.0	659.5
20 Lt	9.4	659.1
40 Lt	8.6	658.9

105+50

40 Lt	8.6	659.9
20 Lt	8.4	660.1
1/2	8.4	660.1
20 Pt	7.7	660.8
40 Pt	8.0	660.5

106+50

40 Pt	6.9	661.6
20 Pt	6.5	662.0
1/2	6.8	661.7
20 Lt	7.0	661.5
40 Lt	7.3	661.2

106+50

40 Lt	7.5	661.0
-------	-----	-------

668.46

20 Lt	6.7	661.7
1/2	6.3	662.2
20 Pt	5.8	662.7
40 Pt	5.4	663.1

107+50

40 Pt	3.9	664.6
20 Pt	4.3	664.2
1/2	5.3	663.2
20 Lt	5.3	663.2
40 Lt	6.4	662.1
BM	5.00	663.46

107+50

40 Lt	4.7	663.8
20 Lt	4.4	664.1
1/2	3.8	664.7
20 Pt	4.0	664.5
40 Pt	4.0	664.5

108+50

40 Pt	3.5	665.0
20 Pt	3.3	665.2
1/2	2.8	665.7
20 Lt	3.4	665.1
40 Lt	3.7	664.8

108+50

40 Lt	2.3	666.2
20 Lt	2.1	666.4

Feb. 26-31

Moort

55

07 Pt.
Hub
1064
Reset Max
663.79

668.46

♂		1.4	667.1	
20' Pt		1.4	667.1	
40' Pt		1.1	667.4	
TP	11.68	679.35	0.79	667.67
	109+0			
40' Pt		10.4	669.0	
20' Pt		10.7	668.7	
♂		11.0	668.4	
20' Lt		11.3	668.1	
40' Lt		11.8	668.6	
	109+15.32	EC		
40' Lt		11.6	667.8	
20' Lt		10.8	668.6	
♂ on Hub		10.12	669.23	
20' Pt		9.6	669.8	
40' Pt		9.8	669.6	
	109+50			
40' Pt		8.7	670.7	
20' Pt		8.9	670.8	
♂		9.1	670.3	
20' Lt		9.8	669.6	
40' Lt		10.5	668.9	
	110+0			
40' Lt		9.5	669.9	
20' Lt		8.5	670.9	
♂		7.7	671.7	

679.35

56

20' Pt		7.3	672.1	
40' Pt		7.0	672.4	
	110+50			
40' Pt		5.6	673.8	
20' Pt		5.8	673.6	
♂		6.4	673.0	
20' Lt		6.9	672.5	
40' Lt		7.6	671.8	
	111+0			
40' Lt		6.4	673.0	
20' Lt		5.1	674.3	
♂		4.3	675.1	
20' Pt		4.0	675.4	
40' Pt		3.5	675.9	
	111+17.13	8.C Pt		
40' Pt		2.9	676.5	
20' Pt		3.5	675.2	
♂ on Hub		3.98	675.37	
20' Lt		4.1	675.3	
40' Lt		5.3	674.1	
TP	12.57	687.24	3.98	675.37
	111+50			
40' Lt		12.7	675.2	
20' Lt		12.0	675.9	
♂		11.6	676.3	
20' Pt		11.2	676.7	

07 8.C Hub
111+17.13

687.94

40 Pt 10.8 677.1

112+0

40 Pt 10.1 677.8

20 Pt 10.2 677.7

♂ 10.7 677.2

20 Lt 11.0 676.9

40 Lt 11.4 676.5

112+50

40 Lt 10.3 677.6

20 Lt 9.8 678.1

♂ 9.3 678.6

20 Pt 8.6 679.3

40 Pt 8.7 679.2

113+0

40 Pt 8.2 679.7

20 Pt 8.5 679.4

♂ 8.5 679.4

20 Lt 8.9 679.0

40 Lt 9.8 678.1

113+50

40 Lt 8.2 679.7

20 Lt 8.5 679.4

♂ 8.2 679.7

20 Pt 8.0 680.9

40 Pt 7.4 680.5

687.94

Feb 28-34

57

114+0

40 Pt 6.6 681.3

20 Pt 6.9 681.0

♂ 6.2 681.6

20 Lt 7.4 680.5

40 Lt 7.8 680.1

114+50

40 Lt 6.2 681.7

20 Lt 6.0 681.9

♂ 6.1 681.8

20 Pt 5.5 682.4

40 Pt 4.8 683.1

114+65 H EC

40 Pt 5.2 682.6

20 Pt 5.6 682.3

♂ on Hub 5.62 682.32

20 Lt 5.4 682.5

40 Lt 5.2 682.6

115+0

40 Lt 3.8 684.1

20 Lt 4.0 683.9

♂ 3.5 684.4

20 Pt 2.2 684.7

40 Pt 4.4 683.5

115+50

40 Pt 2.3 685.6

687.94

30' Pt		2.3	685.6
±		2.4	685.5
30' Lt		1.7	686.2
40' Lt		1.1	686.8
TP	12.68	700.46	0.16
	116+0		
40' Lt		11.7	688.8
30' Lt		12.3	688.2
±		11.7	688.8
30' Pt		13.2	682.5
40' Pt		13.5	682.0
	116+50		
40' Pt		10.8	689.7
30' Pt		10.7	689.8
±		10.0	690.5
30' Lt		8.9	691.6
40' Lt		8.4	692.1
	117+0		
40' Lt		5.4	695.1
30' Lt		4.5	696.0
±		5.1	695.4
30' Pt		6.2	694.3
40' Pt		7.3	693.2
	117+50		
40' Pt		2.7	699.8
30' Pt		1.7	698.8

700.46

58

±		0.8	698.7
TP	12.52	712.69	0.29
30' Lt		12.9	689.8
40' Lt		12.6	700.1
	118+0		
40' Lt		9.5	703.2
30' Lt		9.8	702.9
±		10.2	702.5
30' Pt		10.8	701.9
40' Pt		12.0	700.7
	118+50		
40' Pt		8.3	704.4
30' Pt		7.8	704.9
±		7.6	705.1
30' Lt		7.4	705.3
40' Lt		7.8	704.9
	119+06.13	B.C. Pt	
40' Lt		6.1	706.6
30' Lt		5.6	707.1
±	07.46	4.43	708.26
30' Pt		3.5	709.2
40' Pt		3.5	709.2
TP	12.95	725.00	0.64
	119+50		
40' Pt		12.9	712.1
30' Pt		12.8	712.2

(Corr. Elev)
708.49
see pg. 51
Beatty
5/15/55

725.00

1/2	13.0	712.0
20 Lt	12.3	711.7
10 Lt	14.1	710.9
120+0		
40 Lt	14.5	710.5
20 Lt	12.3	712.7
1/2	10.7	714.3
20 Pt	9.7	715.3
40 Pt	10.1	714.9
120+50		
40 Pt	8.4	716.6
20 Pt	9.1	716.9
1/2	9.9	715.1
20 Lt	12.1	712.9
40 Lt	14.4	710.6
121+0		
10 Lt	12.8	712.2
20 Lt	10.0	715.0
1/2	7.5	717.5
20 Pt	6.9	718.1
40 Pt	6.7	718.3
121+50		
10 Pt	4.4	720.6
20 Pt	4.9	720.7
1/2	5.7	719.3
20 Lt	7.2	717.7

725.00

59

40 Lt	10.0	715.0
122+0		
40 Lt	5.8	719.2
20 Lt	4.2	720.8
1/2	3.2	721.8
20 Pt	2.9	722.1
40 Pt	2.9	722.1
122+50		
10 Pt	0.8	724.2
20 Pt	0.3	724.7
1/2	0.3	724.7
20 Lt	0.4	724.6
40 Lt	1.2	726.8
TP	12.55	737.49
123+0		
40 Lt	9.8	727.7
20 Lt	9.4	728.1
1/2	9.9	727.6
20 Pt	10.3	722.2
40 Pt	11.7	725.8
123+50		
40 Pt	11.2	726.3
20 Pt	8.8	728.7
1/2	7.6	729.9
20 Lt	6.1	731.4
40 Lt	6.6	730.9

07 & 8 State
122+50

737.45

124+0

40 Lt	1.8	735.2
20 Lt	3.0	734.5
1/2	4.6	732.9
20 Pt	7.0	730.5
40 Pt	9.2	728.3

124+50

40 Pt	9.6	722.9
20 Pt	7.8	729.7
1/2	4.1	733.4
TP	10.80	747.93 0.36
20 Lt	12.0	735.8
40 Lt	9.2	738.7

125+0

40 Lt	8.1	739.8
20 Lt	12.0	735.9
1/2	14.9	733.0
20 Pt	17.2	730.7
40 Pt	19.7	728.2

125+50

40 Pt	19.8	728.1
20 Pt	15.6	732.3
1/2	13.1	734.8
20 Lt	11.3	736.6
40 Lt	8.7	739.2

747.93

60

126+0

40 Lt	8.3	738.6
20 Lt	11.5	736.4
1/2	13.6	734.3
20 Pt	16.4	731.5
40 Pt	17.4	730.5

126+50

40 Pt	17.2	730.7
20 Pt	15.2	732.7
1/2	12.4	735.5
20 Lt	10.6	737.3
40 Lt	7.4	740.5

127+0

40 Lt	6.1	741.8
20 Lt	8.0	739.9
1/2	11.2	736.7
20 Pt	12.6	735.3
40 Pt	15.4	732.5

127+50

40 Pt	15.7	732.2
20 Pt	9.6	738.3
1/2	7.5	740.4
20 Lt	4.1	743.8
40 Lt	1.9	746.0
TP	9.33	757.18 0.08

757.18

127+80.54 FC

40 Lt	6.5	750.7
20 Lt	10.4	746.5
1/2 on Hub	11.43	745.75
20 Pt	15.6	741.4
40 Pt	20.3	736.9

128+0

40 Pt	19.3	737.9
20 Pt	14.3	742.9
1/2 on Road	10.6	746.6
20 Lt	6.5	750.7
40 Lt	4.0	753.2

128+50

40 Lt	3.6	753.6
20 Lt	5.3	751.9
1/2	7.4	749.8
20 Pt	9.6	747.6
40 Pt	12.1	745.1

129+0

40 Pt	7.9	749.3
20 Pt	6.4	750.8
1/2	4.6	752.6
20 Lt	3.0	754.2
40 Lt	0.9	756.3
TP	10.64	767.75
	0.07	757.11

767.75

129+50

40 Lt	7.4	760.4
20 Lt	8.3	759.5
1/2	8.8	759.0
20 Pt	11.3	756.5
40 Pt	12.6	755.2

130+0

40 Pt	9.4	758.4
20 Pt	7.8	760.0
1/2	6.0	761.8
20 Lt	3.8	764.0
40 Lt	1.7	766.1

130+50 Pt

40 Lt	1.8	766.0
20 Lt	3.3	764.5
1/2 on Hub	6.04	761.71
20 Pt	9.6	758.2
40 Pt	13.1	754.7

TP 6.76 768.47 6.04

131+0

40 Pt	18.3	750.2
30 Pt	17.2	751.3
20 Pt	14.3	754.2
1/2	10.8	757.2
20 Lt	7.8	760.7
40 Lt	5.6	762.9

on 2 Hubs
130+50

768.47

131+50

40' Lt	5.2	763.3
20' Lt	3.0	761.5
5	14.8	753.2
10' Pt	17.0	751.5
12' Pt Nly Road	19.2	749.3
25' Pt Sky	19.5	749.0
40' Pt	24.5	744.0

132+0

40' Pt	27.8	741.7
15' Pt	20.8	742.7
1' Pt	19.8	248.2
5	17.1	751.4
20' Lt	12.6	755.9
40' Lt	10.5	758.0
TP	0.33	756.17
	12.66	755.81

132+50

40' Lt	5.0	756.1
20' Lt	7.0	749.1
5 Road	9.2	746.9
10' Pt	9.0	747.1
40' Pt	16.3	739.8

132+60.74 BCL

40' Pt	16.8	739.3
20' Pt	11.6	744.5
5	9.99	746.15

756.14

62

18' Lt	8.7	747.4
20' Lt	7.0	749.1
40' Lt	7.0	749.4

133+0

40' Lt	12.2	743.9
25' Lt	8.2	747.9
20' Lt	14.6	741.5
5	14.0	742.1
20' Pt	15.4	740.7
40' Pt	19.2	736.9

133+25

40' Pt	20.7	735.7
20' Pt	18.5	737.6
5	16.0	740.1
20' Lt	75.2	740.9
40' Lt	16.8	739.3

133+50

40' Lt	15.0	741.1
20' Lt	14.5	741.6
5	15.2	744.9
20' Pt	17.5	738.6
40' Pt	19.0	737.1

134+0

40' Pt	10.8	745.3
20' Pt	10.7	745.4
5	11.0	745.1

75614

20 Lt	11.8	744.3
40 Lt	13.5	742.6
134+19.28 EC		
40 Lt	12.8	743.3
20 Lt	11.5	744.6
1/2 02 Hub	10.12	745.95
20 Rt	8.8	747.3
40 Rt	7.7	748.4
134+50		
40 Rt	7.2	748.9
20 Rt	8.6	747.5
1/2	10.2	745.9
20 Lt	11.3	744.8
40 Lt	12.2	743.9
135+0		
40 Lt	11.8	744.3
20 Lt	10.5	745.6
1/2	9.4	746.2
20 Rt	8.1	748.0
40 Rt	9.6	746.5
135+50		
40 Rt	12.4	743.2
20 Rt	10.5	745.6
1/2	10.0	746.1
20 Lt	10.4	745.7
40 Lt	11.6	744.5

75614

63

136+0		
40 Lt	10.1	746.0
20 Lt	9.6	746.5
1/2	9.2	746.9
20 Rt	10.0	746.1
40 Rt	12.3	743.8
136+15.98 BE Rt		
40 Rt	11.7	744.4
20 Rt	9.7	746.4
1/2 02 Hub	9.05	747.05
20 Lt	8.9	747.2
40 Lt	9.0	747.1
136+50		
40 Lt	7.2	748.9
20 Lt	8.5	747.6
1/2	8.8	747.3
20 Rt	10.4	745.7
40 Rt	11.4	744.2
137+0		
40 Rt	10.8	745.3
20 Rt	9.0	747.1
1/2	6.7	749.4
20 Lt	6.3	749.8
40 Lt	5.0	751.1
137+50		
40 Lt	7.3	748.8

756.14

20 Lt		2.1	754.0	
♂		2.2	753.9	
20 Pt		4.0	752.1	
40 Pt		5.5	750.6	
137 + 6459 EC.				
40 Pt		5.0	751.1	
20 Pt		2.5	753.6	
♂ on Hub 1211	767.35	0.90	755.24	
20 Lt		12.7	754.7	
40 Lt		19.2	748.2	
138 + 0				
40 Lt		13.5	753.9	
20 Lt		8.5	758.9	
♂		8.1	759.3	
20 Pt		10.2	757.2	
40 Pt		12.8	755.2	
138 + 50				
40 Pt		8.4	759.0	
20 Pt		6.0	761.0	
♂		3.9	763.5	
20 Lt		2.6	764.8	
40 Lt		2.7	764.7	
TP	12.54	779.88	0.01	767.34
138 + 99.96 EC Lt				
40 Lt		11.6	768.3	
20 Lt		11.4	768.5	

779.88

64

♂ on Hub		12.12	767.76
20 Pt		14.3	765.6
40 Pt		16.1	763.8
139 + 50			
40 Pt		14.4	765.5
20 Pt		12.3	767.6
♂		10.7	769.2
20 Lt		10.4	769.5
40 Lt		12.0	769.9
140 + 0			
40 Lt		14.7	765.2
20 Lt		10.4	769.5
♂ - ♀ Road		9.1	770.8
20 Pt		9.8	770.1
40 Pt		12.8	767.6
140 + 50			
40 Pt		11.1	768.8
20 Pt		10.2	769.2
♂		14.7	768.2
20 Lt		14.1	765.8
40 Lt		17.1	762.8
140 + 81.87 EC. = 149 + 18.93 on Return			
40 Lt		17.6	762.3
20 Lt		14.5	765.4
♂		13.3	766.6
20 Pt		15.1	764.8

779.88

40° Pt		17.2	762.7
	141+0		
40° Pt		21.0	258.9
20° Pt		17.2	262.7
♂		13.2	266.7
20° Lt		13.1	266.5
10° Lt		15.0	264.9
	141+50		
40° Lt		7.5	272.4
20° Lt		8.3	271.6
♂		8.2	271.2
20° Pt		13.3	266.6
40° Pt		19.5	260.4
	142+0		
40° Pt		18.3	266.6
20° Pt		5.7	274.2
♂		0.4	279.5
20° Lt - 1/4 Road		0.3	279.6
TP	12.71	792.57	0.02
40° Lt		11.1	281.5
	142+50		
40° Lt		0.6	292.0
20° Lt		2.2	290.4
15° Lt		4.4	288.2
♂		2.7	289.9
20° Pt		6.8	285.8

792.57

65

40° Pt		11.7	780.9
	143+0		
40° Pt		8.8	783.8
20° Pt		3.8	788.8
TP	9.24	801.82	0.09
♂		6.3	795.5
15° Lt		5.2	796.6
20° Lt		1.7	800.1
40° Lt		4.02	802.0
	143+40.73 B.C. Lt		
BM	46° Lt on Mon	1.76	800.06
20° Lt		2.1	799.6
♂		3.5	798.3
20° Pt		6.3	795.5
40° Pt		11.2	790.6
	143+60.03		
40° Pt		4.5	797.3
20° Pt		2.8	799.0
♂		2.7	799.1
20° Lt		2.1	799.2
40° Lt		1.8	800.0
	143+79.33		
40° Lt		1.8	800.0
20° Lt		2.1	799.2
♂		2.7	799.1
20° Pt		2.4	799.4

801.82

2.2' Pt	4.1	792.7
40' Pt	8.4	793.4
1434 98.63		
40' Pt	8.5	793.3
20' Pt	4.5	792.3
⊥	3.9	792.9
20' Lt	2.4	792.4
40' Lt	1.8	800.0

144+17.94 = EC.

40' Lt	1.8	800.0
20' Lt	2.6	792.2
⊥	5.2	796.6
20' Pt	6.8	795.0
40' Pt	9.2	792.6

144+50

40' Pt	12.0	789.5
20' Pt	2.1	792.7
15' Pt	6.8	795.0
⊥ Road	7.0	794.5
10' Lt	4.3	792.6
40' Lt	1.7	800.1

145+0

40' Lt	0.1	801.7
20' Lt	2.9	798.9
8' Lt	7.6	794.2
⊥	7.7	794.1

801.82

66

10' Pt	8.0	793.5
20' Pt	11.2	790.6
40' Pt	14.7	787.1

145+45.42 80 Lt

40' Pt	16.8	785.0
20' Pt	11.5	790.3
8' Pt	5.5	796.3
⊥ - ⊥ Road	5.7	796.1

8' Lt	5.5	796.3
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15' Lt	2.0	799.8
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40' Lt	1.4	800.7
--------	-----	-------

145+75.02

40' Lt	1.7	800.1
--------	-----	-------

15' Lt	3.7	798.1
--------	-----	-------

12' Lt	6.3	795.5
--------	-----	-------

⊥	6.5	795.3
---	-----	-------

10' Pt	9.4	792.4
--------	-----	-------

40' Pt	17.0	784.8
--------	------	-------

146+04.55

40' Pt	13.4	788.4
--------	------	-------

20' Pt	10.9	790.9
--------	------	-------

7' Pt	7.0	794.8
-------	-----	-------

⊥ - ⊥ Road	7.3	794.5
------------	-----	-------

10' Lt	7.0	794.8
--------	-----	-------

15' Lt	5.2	795.6
--------	-----	-------

40' Lt	2.4	799.4
--------	-----	-------

801.82

146+34.08

40 Lt	2.9	298.9
13 Lt	5.9	295.9
8 Lt	8.1	293.7
z	8.2	293.6
20 Pt	9.5	292.3
40 Pt	12.2	289.6

146+63.61 FC

40 Pt	16.5	285.3
20 Pt	11.5	296.3
15 Pt	9.4	292.4
z	10.0	291.8
5 Lt	7.7	284.1
20 Lt	5.4	296.6
40 Lt	2.8	297.0

TP 3.43 798.04 7.21 794.61

147+0

40 Lt	0.6	297.4
20 Lt	4.3	293.7
z	8.0	290.0
20 Pt - 1/4 Pt.	9.3	288.7
25 Pt	12.2	285.8
40 Pt	15.3	282.7

147+50

40 Pt	21.5	276.5
20 Pt	18.0	280.0

798.04

67

15 Pt	15.4	282.6
z	15.3	282.7
20 Lt	10.3	287.7
40 Lt	5.8	292.2

147+76.22 B.C. Pt

40 Lt	10.3	287.7
20 Lt	12.5	284.5
TP 0.94 786.82	12.16	285.88

10 Lt	4.2	282.4
5 Lt	7.2	279.6
z on Herb	7.08	279.74
13 Pt	7.0	279.8
20 Pt	9.3	272.5
40 Pt	13.2	273.5

148+0

40 Pt	14.3	272.5
20 Pt	11.4	275.7
15 Pt	9.9	276.9
z	9.6	277.2
20 Lt	5.6	281.2
40 Lt	3.7	283.1

148+50

40 Lt	15.0	271.8
20 Lt	14.0	272.8
z	15.3	271.5
20 Pt	16.4	270.4

Plotted A.I.B. March 1934

786.82

68

40.81
 TP 20.6 766.2
 12.55 774.27

14970 = 14170 Appx.

TP	1.63	775.90		774.27
TP	0.64	763.50	12.04	762.86
TP	6.72	757.16	12.06	750.44
TP	0.13	751.93	5.86	751.80
TP	0.20	740.95	11.18	740.75
TP	0.24	728.18	13.01	727.94
TP	0.20	715.36	12.02	715.16
TP	0.23	703.37	12.92	702.44
TP	0.34	691.54	12.17	691.20
TP	0.72	680.28	11.98	679.56
TP	0.52	668.75	12.05	668.23
TP	0.13	657.59	11.29	657.46
TP	0.00	644.77	12.82	644.77
TP	0.12	631.85	13.04	631.73
TP	-0.01	619.06	12.78	619.07
TP	0.69	609.08	10.67	608.39
BM	1.12	598.78	11.42	597.66
TP	0.32	586.10	13.00	585.78
TP	0.09	573.81	12.38	573.72
TP			12.91	560.90

1407 587.57
 16 Pt 91.55

Soledad Road Line Change

103+99.42 to 127+04.06

41

6-28-34
Moore

69

109+42.80 E.C.		15° 34'
109		14° 20.397
+50		13° 54.457
108	Δ 31° 08'	11° 28.517
+50	R 1000.0	10° 02.577
107	T 278.58	8° 36.637
+50	L 543.38	7° 10.697
106	D 41.7188	5° 44.757
+50		4° 18.817
105		3° 52.877
104+50		1° 26.937
103+99.42 B.C.		

RT.

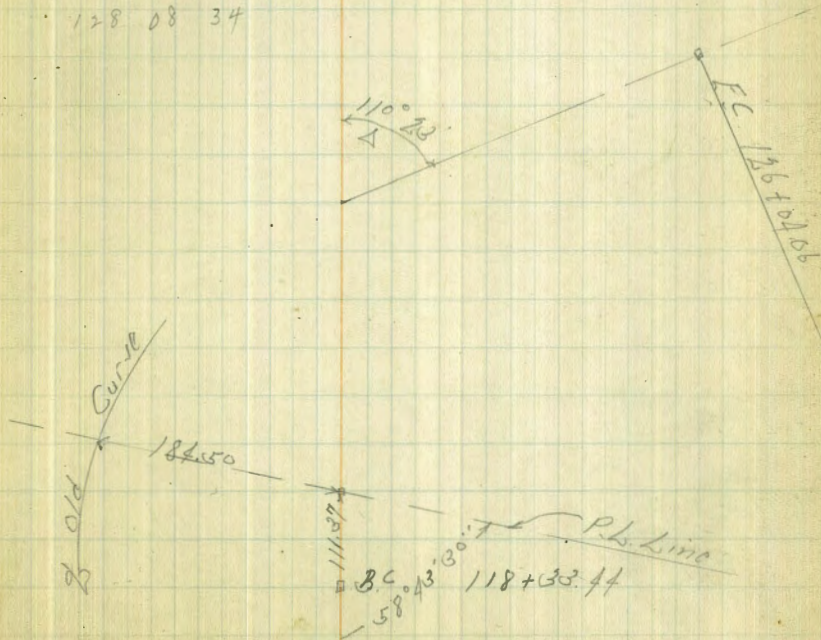
126+0		54° 53' 984"
+50		51° 19' 129" ✓
125+0		47° 44' 274" ✓
+50		44° 09' 419" ✓
124+0	Δ 110° 23'	40° 34' 564" ✓
+46.81		38° 08' 34" ✓
+50	R 400.0	38° 59' 709" ✓
123+0	T 575.35	33° 24' 854" ✓
+184.87		32° 19' 53" ✓
+50	L 770.62	29° 49' 999" ✓
122+0	D 142972	26° 15' 144" ✓
+1581		23° 48' 15" ✓
+50		22° 40' 289" ✓
121+0		19° 05' 434" ✓
+50		15° 30' 579" ✓
120+0		11° 55' 725" ✓
+50		8° 20' 870" ✓
119+0		4° 46' 015" ✓
+50		1° 11' 160" ✓
118+33.44	B.C.	

118 33.44
 109 42.80
 890.64

575.35
 111.37
 464

70

128 08 34



Soledad Road Line Change
 Cross Section
 103+99.42 to 127+84.06

TP 11.02 674.88 0.44 663.56

107+0

+50

106+0

+50

105+0

104+50

103+99.42 B.C.

B.M. 0.44 664.00

663.56

R/M 07
 106+

6-30-24

71

Lt.

L

Rt

<u>663.5</u>	<u>664.9</u>	<u>663.5</u>	<u>663.7</u>	<u>663.0</u>
0.5 40'	+0.4 23'	0.5	0.3 23'	0.1 40'

<u>661.9</u>	<u>662.4</u>	<u>662.8</u>	<u>663.2</u>	<u>663.1</u>
2.1 40'	1.6 23'	1.2	0.8 23'	0.9 40'

<u>661.2</u>	<u>661.7</u>	<u>661.5</u>	<u>661.5</u>	<u>661.8</u>
2.4 40'	2.3 23'	2.5	2.5 23'	2.2 40'

<u>660.1</u>	<u>660.1</u>	<u>660.8</u>	<u>660.3</u>	<u>660.5</u>
3.9 40'	3.9 23'	3.2	3.7 23'	3.5 40'

<u>659.1</u>	<u>659.0</u>	<u>659.3</u>	<u>659.2</u>	<u>659.1</u>
4.9 40'	5.0 23'	4.7	4.8 23'	4.9 40'

<u>654.9</u>	<u>656.1</u>	<u>656.0</u>	<u>656.5</u>	<u>657.4</u>
9.1 40'	7.9 23'	8.0	7.5 23'	6.6 40'

<u>649.7</u>	<u>651.2</u>	<u>652.07</u>	<u>652.90</u>	<u>654.2</u>
14.3 40'	12.8 23'	11.93 07 H 05	11.1 23'	9.8 40'

664.00

111

+50

110

+42.80 F.C.

109

+50

108

107+50

674.88

Lt.

L

Rt

72

Lt.	L	Rt	72
<u>672.9</u>	<u>672.4</u>	<u>671.9</u>	<u>670.8</u>
<u>669.9</u>			
$\frac{2.0}{40}$	$\frac{2.5}{23}$	3.5	$\frac{4.1}{23}$
			$\frac{5.0}{40}$
<u>672.0</u>	<u>670.6</u>	<u>670.3</u>	<u>669.4</u>
<u>668.9</u>			
$\frac{2.3}{40}$	$\frac{4.2}{23}$	4.6	$\frac{5.5}{23}$
			$\frac{6.6}{40}$
<u>669.6</u>	<u>668.7</u>	<u>668.7</u>	<u>668.0</u>
<u>667.7</u>			
$\frac{5.3}{40}$	$\frac{6.2}{23}$	6.2	$\frac{6.9}{23}$
			$\frac{7.2}{40}$
<u>668.1</u>	<u>667.7</u>	<u>667.3</u>	<u>667.5</u>
<u>666.3</u>			
$\frac{6.8}{40}$	$\frac{7.2}{23}$	$\frac{7.61}{0.746}$	$\frac{7.4}{23}$
			$\frac{8.6}{40}$
<u>667.4</u>	<u>667.1</u>	<u>666.6</u>	<u>666.2</u>
<u>666.0</u>			
$\frac{7.5}{40}$	$\frac{7.8}{23}$	8.2	$\frac{8.7}{23}$
			$\frac{8.9}{40}$
<u>666.4</u>	<u>666.1</u>	<u>665.7</u>	<u>665.5</u>
<u>665.4</u>			
$\frac{8.5}{40}$	$\frac{8.8}{23}$	9.2	$\frac{9.4}{23}$
			$\frac{9.5}{40}$
<u>665.1</u>	<u>664.5</u>	<u>665.7</u>	<u>665.5</u>
<u>665.0</u>			
$\frac{9.8}{40}$	$\frac{10.4}{23}$	9.2	$\frac{9.4}{23}$
			$\frac{9.9}{40}$
<u>664.1</u>	<u>664.7</u>	<u>665.5</u>	<u>664.7</u>
<u>664.8</u>			
$\frac{10.8}{40}$	$\frac{10.2}{23}$	9.4	$\frac{10.2}{23}$
			$\frac{10.1}{40}$

674.88

Lt

Z

Pt

73

+50

<u>683.4</u>	<u>682.3</u>	<u>681.3</u>	<u>680.0</u>	<u>678.9</u>
$\frac{26}{40}$	$\frac{3.7}{23}$	$\frac{4.7}{23}$	$\frac{6.0}{23}$	$\frac{7.1}{40}$

114

<u>680.7</u>	<u>680.8</u>	<u>679.6</u>	<u>678.1</u>	<u>677.6</u>
$\frac{53}{40}$	$\frac{5.2}{23}$	$\frac{6.4}{23}$	$\frac{7.9}{23}$	$\frac{8.4}{40}$

+50

<u>679.0</u>	<u>678.2</u>	<u>677.4</u>	<u>676.7</u>	<u>676.6</u>
$\frac{7.0}{40}$	$\frac{7.8}{23}$	$\frac{8.6}{23}$	$\frac{9.3}{23}$	$\frac{9.4}{40}$

113

<u>677.9</u>	<u>677.4</u>	<u>676.7</u>	<u>676.5</u>	<u>676.9</u>
$\frac{8.1}{40}$	$\frac{8.6}{23}$	$\frac{9.3}{23}$	$\frac{9.5}{23}$	$\frac{9.1}{40}$

+50

<u>676.6</u>	<u>676.5</u>	<u>676.8</u>	<u>675.4</u>	<u>675.3</u>
$\frac{9.4}{40}$	$\frac{9.5}{23}$	$\frac{9.2}{23}$	$\frac{10.6}{23}$	$\frac{10.7}{40}$

112

<u>675.8</u>	<u>676.3</u>	<u>674.7</u>	<u>674.1</u>	<u>673.7</u>
$\frac{10.2}{40}$	$\frac{9.7}{23}$	$\frac{11.2}{23}$	$\frac{11.9}{23}$	$\frac{12.3}{40}$

7P

11.95 685.96 0.87 674.81

685.96

11+50

<u>674.6</u>	<u>674.7</u>	<u>673.2</u>	<u>672.5</u>	<u>671.8</u>
$\frac{0.3}{40}$	$\frac{0.2}{23}$	$\frac{1.7}{23}$	$\frac{2.4}{23}$	$\frac{3.1}{40}$

674.88

674.88

kt.

B

Rt

74

118

<u>700.6</u>	<u>700.8</u>	<u>701.4</u>	<u>701.8</u>	<u>701.7</u>
8.6 40	8.4 23	7.8	7.4 23	7.5 40

+50

<u>699.6</u>	<u>698.7</u>	<u>698.7</u>	<u>698.3</u>	<u>698.2</u>
9.6 40	10.5 23	10.5	10.8 23	11.0 40
		709.18		

TP 11.18 709.18 0.65 698.00 1

117

<u>696.7</u>	<u>696.4</u>	<u>696.1</u>	<u>695.9</u>	<u>695.1</u>
2.0 40	2.3 23	2.6	2.8 23	3.6 40

+50

<u>695.1</u>	<u>694.9</u>	<u>694.3</u>	<u>692.9</u>	<u>692.3</u>
3.6 40	3.8 23	4.4	5.8 23	6.4 40

116

<u>692.4</u>	<u>692.4</u>	<u>692.3</u>	<u>691.0</u>	<u>690.2</u>
6.3 40	6.3 23	6.4	7.7 23	8.5 40

+50

<u>688.8</u>	<u>688.2</u>	<u>687.9</u>	<u>686.5</u>	<u>685.4</u>
9.9 40	10.5 23	10.8	12.2 23	13.3 40
		698.65		

TP 12.78 698.65 0.09 685.87

115

<u>685.1</u>	<u>685.4</u>	<u>683.8</u>	<u>682.6</u>	<u>681.2</u>
0.9 40	0.6 23	2.2	3.4 23	4.8 40

685.96

685.96

LH

L

RH

121

<u>721.0</u>	<u>720.0</u>	<u>717.8</u>	<u>716.5</u>	<u>715.7</u>
$\frac{1.2}{40}$	$\frac{2.2}{23}$	4.4	$\frac{5.7}{23}$	$\frac{6.5}{40}$

+50

<u>719.4</u>	<u>719.7</u>	<u>718.7</u>	<u>717.9</u>	<u>715.9</u>
$\frac{2.8}{40}$	$\frac{2.5}{23}$	2.5	$\frac{4.3}{23}$	$\frac{6.2}{40}$

120

<u>720.0</u>	<u>719.3</u>	<u>718.1</u>	<u>717.2</u>	<u>716.5</u>
$\frac{2.2}{40}$	$\frac{2.9}{23}$	4.1	$\frac{5.0}{23}$	$\frac{5.7}{46}$

+50

<u>716.1</u>	<u>715.5</u>	<u>714.2</u>	<u>713.2</u>	<u>712.3</u>
$\frac{6.1}{40}$	$\frac{6.7}{23}$	8.0	$\frac{9.0}{23}$	$\frac{9.9}{40}$

119

<u>711.0</u>	<u>709.8</u>	<u>708.0</u>	<u>706.3</u>	<u>707.3</u>
$\frac{11.2}{40}$	$\frac{12.4}{23}$	14.2	$\frac{15.9}{23}$	$\frac{14.9}{40}$

TP

13.26

722.23

0.21

708.97

^{0.0 Root}
 20.4 118+90

722.23

+50

<u>705.2</u>	<u>704.7</u>	<u>704.2</u>	<u>705.0</u>	<u>704.8</u>
$\frac{4.0}{40}$	$\frac{4.5}{23}$	5.0	$\frac{4.2}{23}$	$\frac{4.4}{40}$

118+03.44 BC

<u>702.8</u>	<u>702.8</u>	<u>703.34</u>	<u>703.5</u>	<u>703.7</u>
$\frac{6.4}{46}$	$\frac{6.4}{23}$	$\frac{5.84}{27.46}$	$\frac{5.7}{23}$	$\frac{5.5}{40}$

709.18

709.18

Lt

S

Pt

76

<u>739.4</u>	<u>737.8</u>	<u>734.9</u>	<u>729.0</u>	<u>724.8</u>
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7.0 40	8.6 23	11.5	17.4 23	21.6 40
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<u>735.4</u>	<u>733.6</u>	<u>732.2</u>	<u>727.1</u>	<u>722.4</u>
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11.0 40	12.8 23	14.2 746.86	19.3 23	24.0 40
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124

TP 12.63 746.86 0.83 733.73

<u>731.9</u>	<u>730.3</u>	<u>727.6</u>	<u>724.8</u>	<u>723.1</u>
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2.7 40	4.3 23	7.0	9.8 23	11.5 40
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+50

<u>728.2</u>	<u>725.6</u>	<u>723.5</u>	<u>722.2</u>	<u>719.7</u>
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6.4 40	9.0 23	11.1	12.4 23	14.9 40
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123

<u>724.8</u>	<u>722.8</u>	<u>721.4</u>	<u>720.6</u>	<u>719.7</u>
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9.8 40	11.8 23	13.2	14.0 23	14.9 40
-----------	------------	------	------------	------------

+50

<u>722.9</u>	<u>720.9</u>	<u>718.6</u>	<u>717.8</u>	<u>716.6</u>
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11.7 40	13.7 23	16.0	16.8 23	18.0 40
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122

TP 12.75 734.56 0.42 721.81

<u>718.2</u>	<u>720.1</u>	<u>718.2</u>	<u>716.4</u>	<u>716.0</u>
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0.0 40	2.1 23	4.0	5.8 23	6.2 40
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121+50

722.23

722.23

Lt

Z

PT

77

126+04.06 EC.

<u>754.0</u>	<u>753.0</u>	<u>751.9</u>	<u>749.6</u>	<u>748.4</u>
$\frac{2.4}{40}$	$\frac{3.4}{23}$	4.5	$\frac{6.8}{23}$	$\frac{8.0}{40}$

450

<u>752.9</u>	<u>751.2</u>	<u>748.2</u>	<u>747.6</u>	<u>746.1</u>	<u>745.9</u>	<u>743.8</u>	<u>741.2</u>
$\frac{3.5}{40}$	$\frac{5.2}{23}$	8.2	$\frac{8.8}{5}$	$\frac{10.3}{7}$	$\frac{11.0}{20}$	$\frac{12.6}{23}$	$\frac{15.2}{40}$

756.36

TP 10.67 756.36 0.67 745.69 ^{07 HOB} 127+8054 EC. 745.75

125

<u>746.2</u>	<u>746.2</u>	<u>745.3</u>	<u>743.2</u>	<u>739.8</u>	<u>731.9</u>
$\frac{0.2}{40}$	$\frac{0.2}{23}$	$\frac{1.1}{15}$	3.2	$\frac{7.6}{23}$	$\frac{14.5}{40}$
			7.45		

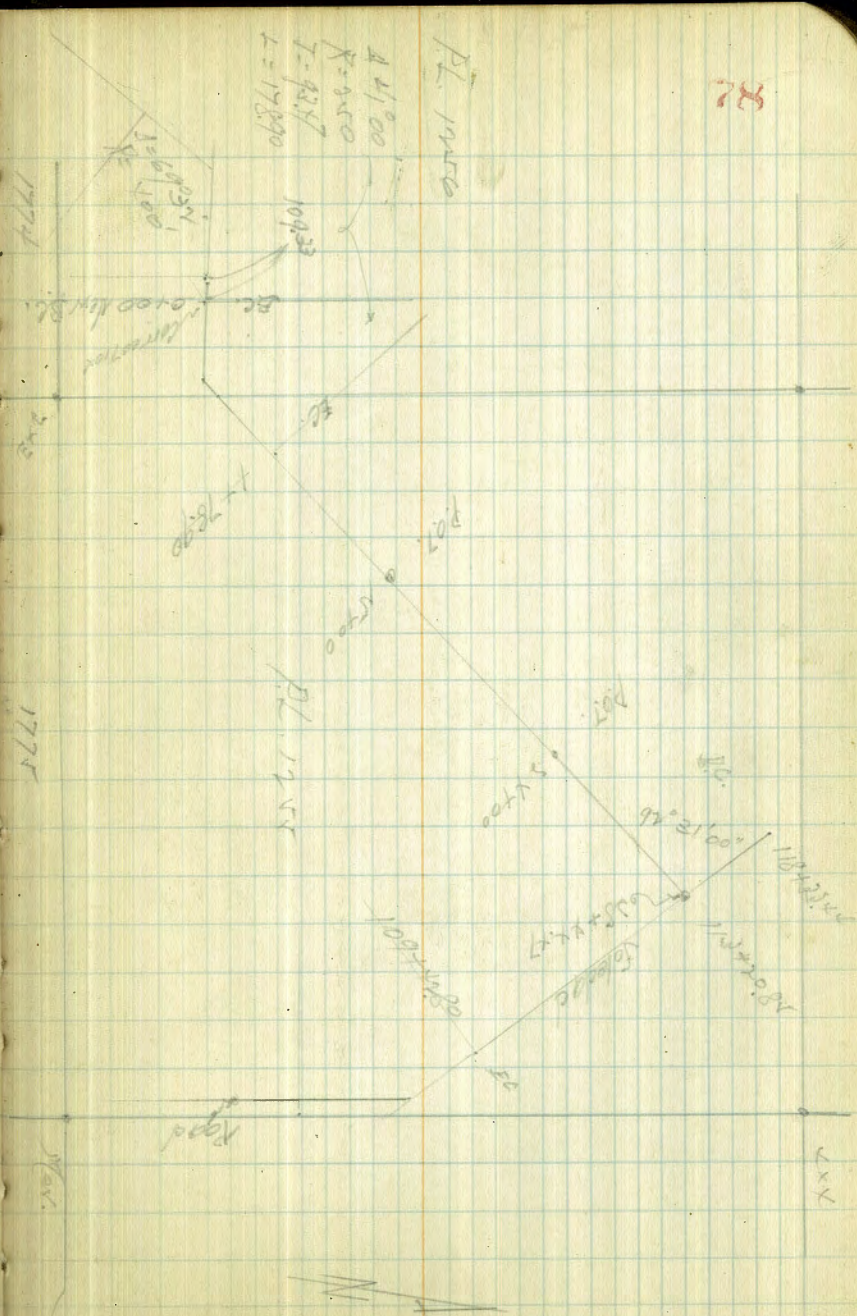
746.36

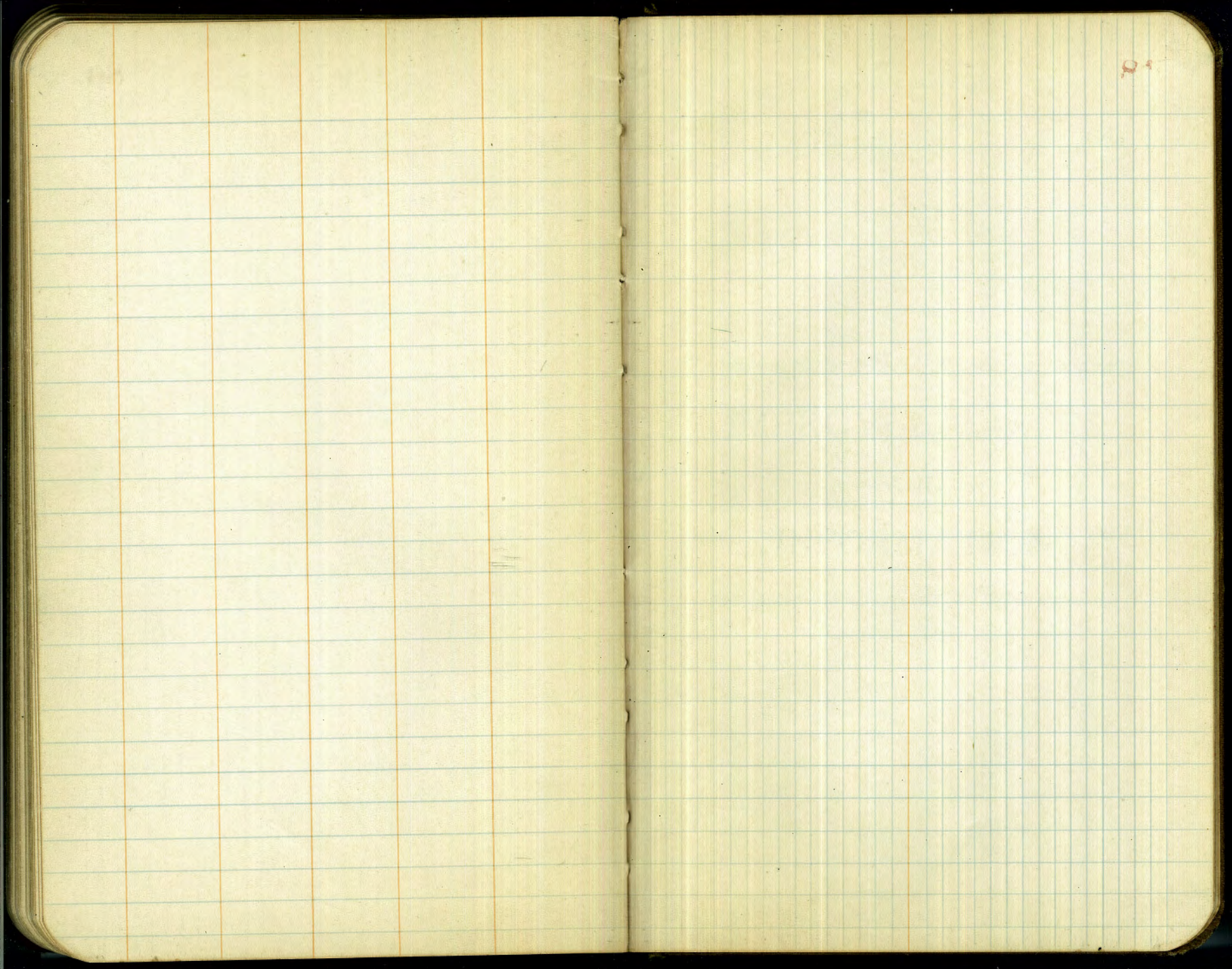
indexed
C.S.N.

Moore
11/22/30

Proposed $\&$ of R.O.W. of the
Ext. of El Camino del Teatro
thru Plot 1255 to connection with
Soledad Rd.

Line thru PL 1256 by JR Comly 2/30





ENGINEERING DEPARTMENT,
CITY OF CALIFORNIA,
SAN DIEGO.

$$\begin{array}{r} 74.21 \\ + 7.83 \\ \hline 82.04 \\ - 4.90 \\ \hline 77.14 \end{array}$$

$$\begin{array}{r} 13.28 \\ + 7.28 \\ \hline 20.56 \\ - 4.80 \\ \hline 15.76 \end{array}$$

$$\begin{array}{r} 3.57 \\ + 9.65 \\ \hline 13.22 \\ - 4.80 \\ \hline 8.42 \end{array}$$

$$\begin{array}{r} 59.67 \\ 16.51 \\ \hline 43.16 \end{array}$$

$$\begin{array}{r} 196 \times 2 \\ \hline 392 \end{array}$$

$$\begin{array}{r} 354.03 \\ - 18.72 \\ \hline 335.31 \end{array}$$

$$\begin{array}{r} 665.53 \\ 50 \\ \hline 715.53 \end{array}$$

$$10.40 \times 563$$

$$\begin{array}{r} 5200 \\ 6240 \\ 3120 \\ \hline 585520 \end{array}$$

$$335.31$$

$$276.76$$

$$\begin{array}{r} 77.48 \\ .34 \\ \hline 77.14 \end{array}$$

$$\begin{array}{r} 306.17 \\ 63.64 \\ \hline 242.53 \end{array}$$

$$\begin{array}{r} 285.66 \\ 3.57 \\ \hline 282.09 \end{array}$$

$$\begin{array}{r} 77.78 \\ 4.90 \\ \hline 82.68 \\ - 7.83 \\ \hline 74.85 \end{array}$$

$$\begin{array}{r} 77.52 \\ 73.82 \\ \hline 3.70 \end{array}$$

$$\begin{array}{r} 77.78 \\ - 3.57 \\ \hline 74.21 \end{array} \text{ BM. } 4 \text{ } 5$$