Our Leather Bound Engineers Note Books are carried in the following rulings:

No. 380 LEVEL BOOK.	Left and Right Hand Page the same as Left Hand Page of this Book.
No. 382 FIELD BOOK.	Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.
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THE FREDERICK POST CO.

ENGINEERING and DRAFTING SUPPLIES

IRVING PARK STATION

CHICAGO, ILL.

x Sec. Alley Blk	45		1
" " " "	44		4
" " " "	43		7
" " " "	42		9
Mechanic St.			13
		c.L. only. See Book 1299	
Meade	Louisana to Utah		15
C St.	30th to 32nd		22
32nd	B. to Boundary.		40
Edgemont.	C to B.		49
31st	C to B		56
Alley 188 CITY HTS			62
" 200	" "		75

Lic. ended Sept 78 7/2/80 HH.

11/3/08 Cross Section of Alley 20' wide
Moore Resub of Blk 44 Fairmont Add.

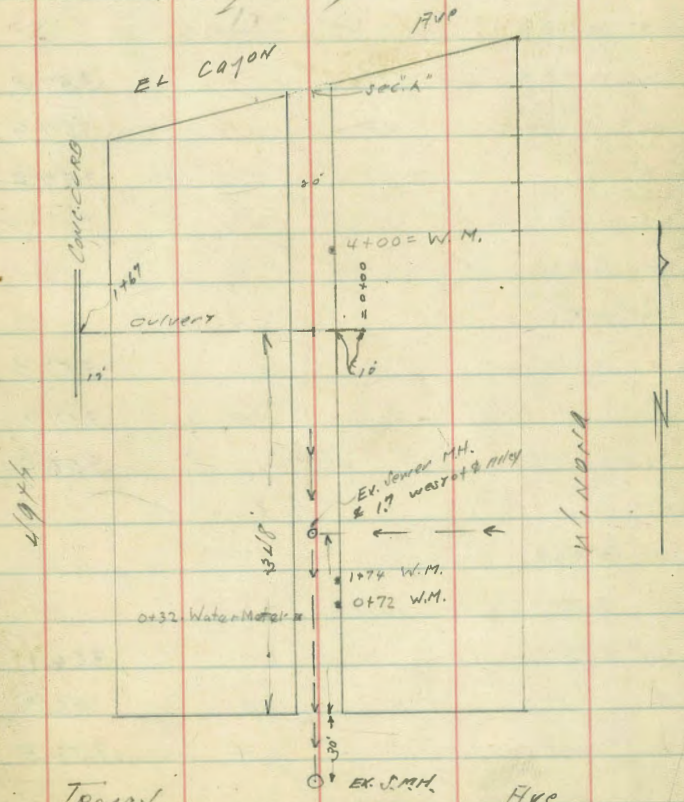
SWBP		355.37	EL Cajon 69th St
	7.57	362.94	
S.M.H 30' South of N.L. Trojan			
Flow line		10.83	352.11
0+00 = N.L. Trojan			
W. Top Cb.		5.17	357.77
gut.		5.9	357.0
℄		5.7	357.2
gut		5.2	357.7
E. Top Cb.		4.40	358.54
0+50			
E.		5.7	357.2
℄		6.2	356.7
W		6.7	356.2
1+00			
W		6.0	356.9
℄		5.8	357.1
E.		5.5	357.4
1+50			
E.		5.7	357.2
℄		5.7	357.2
W.		6.0	356.9
2+00			
W.		5.1	357.8
℄		4.6	358.3
E.		4.7	358.2

Plotted 11-15-28 CBH

1

(4T)

block checks MAP very closely.



	362.94	
2+26.7 = Ex. S.M.H.		
Flow line	8.98	353.96
2+50		
E.	4.1	358.8
℄	4.5	358.4
W.	4.8	358.1
2+75		
-5		
W.	5.5	
℄	5.4	357.5
E.	5.0	357.9
+5	5.0	357.9
3+00	4.7	
-5		
E.	5.4	
℄	5.6	357.3
W.	5.9	357.0
+5	6.0	356.9
3+25	6.4	
-5		
W.	7.2	
℄	6.8	356.1
E.	6.1	356.8
+5	6.4	356.5
3+48 = ℄ of Culvert Location	6.2	

-10			
E			
℄		362.94	6.5
W.			6.6
+5			6.4
3+75			6.9
-5			6.9
W			
℄			6.3
E			6.2
+5			6.1
4+00			5.9
-5			5.8
E.			
℄			2.0
W.			5.3
+5			4.9
4+25			5.8
-5			6.0
W.			
℄			5.5
E.			5.4
+5			4.6
4+50			4.2
-5			3.9
E.			
			3.2
			3.5

356.3
356.5
356.0
356.7
356.8
357.0
357.6
358.0
357.1
357.5
358.3
358.7
359.4

362.94

℄	3.5	359.4	
W	3.6	359.3	
+5	3.6		
4+75			
-5	2.9		
W.	2.8	360.1	
℄	2.3	360.6	
E.	2.1	360.8	
+5	1.5		
5+00			
-5	0.0		
E.	0.2	362.7	
℄	0.7	362.2	
W.	1.2	361.7	
+5	1.3		
T.P.	4.36	358.58	

Sec "A" = S.L. El Cajon. 5+17.20 = W.L. Alley + S.L. El Cajon

5+21.17 = E.L. Alley + S.L. El Cajon.

W. Top Cb.	2.22	360.72	
Gut. on paving	2.39	360.55	
℄	2.24	360.70	
Gut on paving	1.58	361.36	
E. Top Cb.	1.16	361.79	

X sec. of Culvert 348' N. of N.L. Trojan

362.94

0+00 = 10' E. of E.L. Alley			6.5
E.L. Alley			6.6
℄ "			6.4
W.L. "			6.9
0+45			6.5
0+70			7.3
0+95			7.7
1+20			7.6
1+45			7.8
1+67.11 = E. cb of 49th st.			
Top cb.	7.16	365.74	8.60

11/7/28 Cross Section of alley 20' wide
Moore Resub. of Blk 44 Fairmont Add

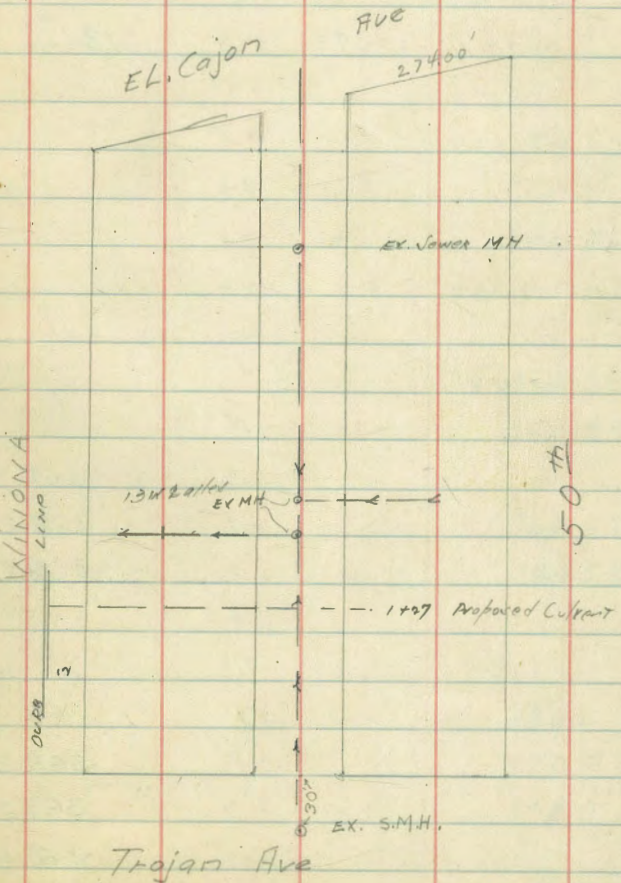
383.13

SWBP	2.59	386.72		~~386.72~~	El. Cajon 50 ft
TP	1.14	376.07	11.79	374.93	
Ex. Sewer MH & alley & Trojan Ave			9.47	366.60	Flowline
	N/L Trojan - 00				
W	Top cem ch		2.1 W	372.95	
℄			2.3	372.8	
E	" " "		1.8 W	373.53	
	0+25 W				
E			2.5	372.6	
C			2.6	372.5	
W			2.9	372.2	
	0+30 W = Ex Water Meter on West				
dirt floor	0+56 = ℄ 8 in. garage on West = Hoover Factory				
W			5.1	370.0	
C			5.4	369.7	
E			4.8	370.3	
	0+75 W				
E			6.0	369.1	
C			6.3	368.8	
W			6.6	368.5	
	1+00				
+5			8.4	367.9	
W			7.9	367.2	
C			7.3	366.8	
E			7.3	366.8	
+5			6.8		

Plotted - 11-16-28 CBH

44

Block checks Map closely



		376.07		
1+47 = proposed culvert				
E -10 = Water			7.0	
0+10 = E for edge			7.7	368.4
0+20 = C " "			7.8	368.3
0+30 = W " "			8.5	366.6
0+35			8.8	
0+50			9.6	
TP	3.04	374.97	6.13	368.84
0+75			7.7	
1			8.8	
+25			9.6	
+50			10.6	
1+67 = curb COM.			10.6	
" " out			11.2	
1+00				
-5			5.2	
W			5.3	367
C			4.8	368.2
E			4.3	368.7
+5			3.9	
1+75				
-5			3.1	
E			3.8	368.2
C			4.3	367.7
W			4.4	368.6
+5			4.9	

		374.97		
1+93 Ex. water Mains both sides				
2+00				
-5			4.7	
W			4.4	368.6
C			3.6	368.4
E			3.0	369.0
+5			2.7	
2+25				
-5			1.9	
E			2.4	369.6
C			3.3	368.7
W			3.6	368.4
+5			4.0	
2+47 = Ex. Sewer MH				
Flowline			9.0±	367.96 ✓
Rim			3.04	368.94
2+43 = Ex Sewer MH				
Flowline			8.5±	365.46 ✓
Rim			2.40	368.58
2+50				
-5			2.7	
W			2.6	369.4
C			1.5	370.5
E			0.2	371.8
2+50 = SL Fence on East & Inverlex				✓
2+77 = NL " " " 3 " "				✓

		377.97		
T P	11.55	380.48	2.04	368.93
	2+77 = SL Double garage cem. floor on line/on east			
E	on cem floor		6.66	372.82
C			7.8	372.7
W			9.0	371.5
	2+86 = Ex water meter on west			
	2+97 = NL of above double garage on east			
	3+00			
W			7.9	372.6
C			7.N	372.5
E			6.7	373.8
	3+03 Ex. water meter on east			
	3+30			
E			.5.8	374.7
C			6.5	374.0
W			7.1	373.4
	3+55 ℄ single garage w/ dirt floor			
- N.S			6.6	373.9
W			6.6	373.9
C			5.8	374.7
E			5.3	375.2
	4+00 Ex. water meter on west			
	4+00			
E			3.5	377.0
C			4.3	376.2
W			4.6	375.9

		381.48		
	4+17	= Ex. Sewer MH		
	4 low line		10.48	370.20
	R. M		3.6N	378.86
	4+50			
W			2.7	378.8
C			2.6	378.9
E			3.4	378.1
T.P.	5.80	384.69	1.59	378.89
	5+00			
E			4.9	379.8
C			5.3	379.4
W			5.7	379.0
	5+40			
W			4.9	379.8
C			4.N	380.5
E			5.3	380.4
	5+75.18 = SL El Cajon on west		5+78.67 on east = Diag.	
E	for ydgo		4.0	380.7
C			4.6	380.1
+1			6.0	378.7
+9			5.8	378.9
W			4.6	379.1
	Same sta. as above			
W	T.P curb & paving		6.48	378.51
C	paving		6.4N	378.25
E	"		6.06	378.63
	Top curb		5.45	379.24

383.3

11/7/28 Cross Section of Alley 20' Wide
Moore Resub of Blk. 43 Fair-mount Add. (383.16)

S.W.I.P.	8.49	391.62		383.13	EL Cajon & 5th
	3.49	388.57	10.54	382.08	

0.0 = N.L. Trojan st.

E.		13.2	377.4
℄		13.4	377.2
W		14.1	370.5

0+50 = S.L. Wirefence .3 IN Alley ON East.

W		10.9	373.7
℄		10.4	374.2
E.		9.5	375.1

0+70 EX. Water Meter ON East

0+85 = N. end of Wirefence ON East 1.0 IN Alley

also S.L. of house ON East 1.0 IN Alley ✓

0+98 = N.L. of above house

1+00

E.		6.7	378.9
℄		7.8	376.8
W		8.2	376.4

1+50

W		6.2	370.4
℄		5.3	379.3
E		4.8	379.9

1+75 = EX. Water Meter ON West

2+00

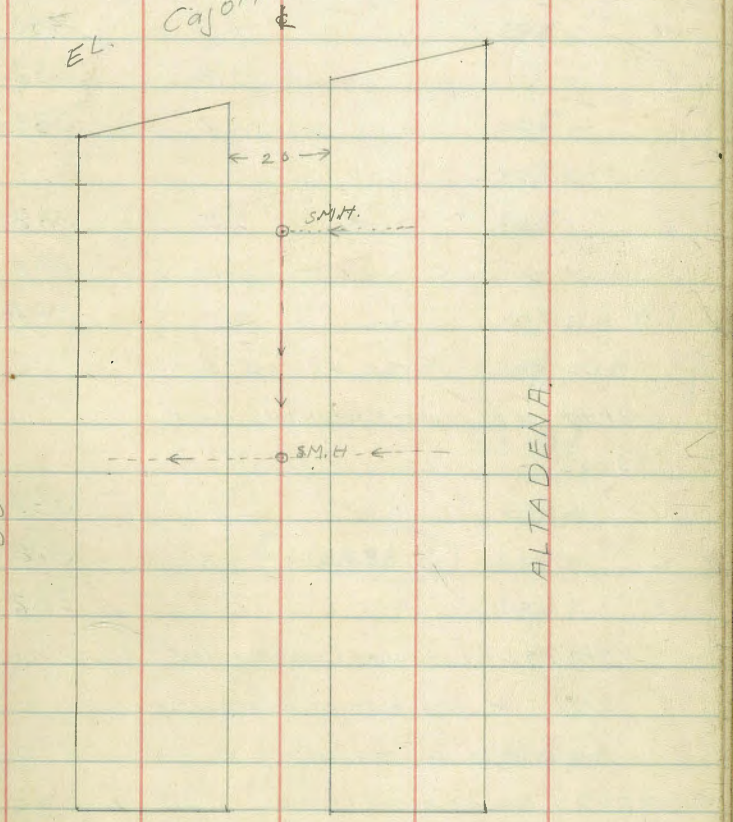
E		3.7	380.9
℄		3.9	380.7

Plotted - 11-16-28 CBH

7

(43)

checks map closely



W.		4.8	389.8
2+47 = EX. S.M.H.			
Flow Line		16.04	368.53
Rim		3.73	380.84
2+50			
W		4.1	380.5
℄		3.4	381.2
E		2.8	381.8
3+00			
E		2.5	382.1
℄		3.1	381.5
W		3.8	380.8
3+25 = S.L. fence on West on line			
3+49 = EX. Water Meter on West			
3+50			
W.		2.7	381.9
℄	36 382.0	6.3	378.3
E		2.0	382.6
3+67 = N.L. of Wire fence on West .7 in Alley			
3+81 = ~~W~~ EX. Water Meter on West			
also S.L. of wire fence on West .5' in Alley			
4+00 = N.L. of above fence .2 in Alley.			
E.		1.3	383.3
℄		1.7	382.9
W		2.5	382.1
T.P.	8.88	391.58	1.87	382.70

4+21 = EX. Water Meter on West.			
4+35 = " " " on East.			
4+50			
W		7.8	383.8
℄		7.3	384.3
E		7.0	384.6
5+00			
E		6.1	385.5
℄		6.2	385.4
W.		6.5	385.1
5+28 = EX. Sewer M.H.			
Flow line		13.96	378.62 ✓
Rim		5.86	382.72
5+40 = ℄ Garage on West		5.8	on dirt floor 5' back
			385.8
5+50			
W		5.2	386.4
℄		5.4	386.2
E		5.3	386.3
5+64 = EX Water Meter on West.			
5+78 = Conc. Walk on West #in Alley S.End.			
Top Conc		4.84	386.74
6+00			
E.		4.4	387.2
℄		4.7	386.9
W Top Conc.		4.90	386.68
6+12 = N.End of Walk on West .4 in Alley			

9-A

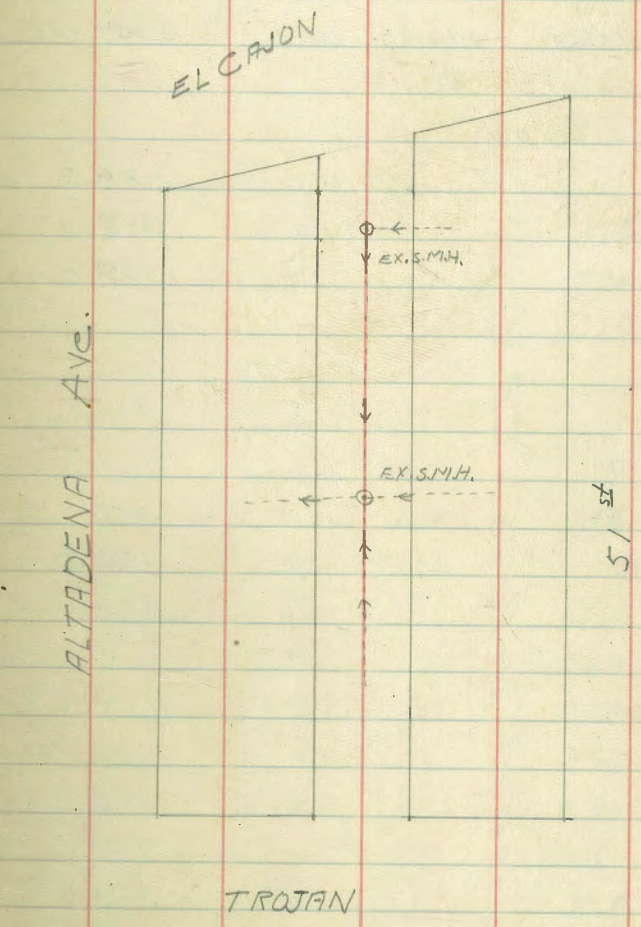
3912.58

W. Top Conn. on	4.81	3886.77
S.L. EL Cajon = 4332.69 on W.L. Alley 6+36.17 on E.L. Alley		
Sec on diagonal		
W. Top Cb.	4.72	3886.86
gut	4.85-	3886.73
E	5.14	3886.44
gut	4.85-	3886.73
E. Top Cb	4.60	3886.98
B.M. 5'0" + EL. Cajon	8.46	3883.12 = .01 error
		3883.13 = ok.

9

(42)

Block Chacks Map Closely



11/8/28
Moore

Cross Section of Alley 20' wide.
Resub of Blk. 42 Fairmount Add.

S.W.B.P.	5.95	398.77		386.82 EL Cajon + 57 ~~387.82~~
			5.92	386.85
	1.46	388.31	12.65	375.66
	0.28	375.94	12.59	363.35
	6.01	370.36		
0+00 = N.L. Trojan				
W.			11.1	358.3
℄			11.7	356.6
E.			12.4	357.0
+5			14.1	
0+05				
-10			11.3	
-3			13.6	
E			12.7	356.7
℄			9.9	359.5
W			8.2	361.2
+5			7.4	
0+25				
-5			3.9	
W			4.8	364.6
℄			6.8	362.6
E			7.6	361.9
+5			7.1	
T.P.	13.05	381.81	0.60	368.76

Plotted 11-16-28 - C.B.H.

381.81

0+50			
-5		11.9	
E		11.9	369.9
℄		13.1	368.7
W		11.6	370.2
+5		10.9	370.9
0+75			
-5		6.1	
W		6.2	375.6
℄		6.6	374.2
E		5.8	376.0
+5		5.9	
1+00			
E		4.0	378.8
℄		4.7	378.1
W		4.0	378.8
1+50			
W		1.8	380.0
℄		1.5	380.3
E		1.6	380.2
T.P.	10.46	392.11	0.16 381.65
2+00			
E.		8.9	383.2
℄		9.1	382.0
W		9.5	382.6

2+35 = Ex Water Meter on West.

2+50 = Ex S.M.H. 1' East of ℄		
W.	6.8	385.3
℄	6.9	385.2
Flow line M.H.	2.20	379.91 ✓
Rim	7.20	384.91
E	6.4	385.7
3+00		
E.	5.0	386.1
℄	4.9	386.2
W	5.3	385.8
3+47 = Ex. Water Meter on East.		
3+50		
W	4.8	386.3
℄	4.3	386.8
E	4.7	386.4
4+00		
E	4.2	386.9
℄	4.1	387.0
W	4.3	386.8
4+50		
W	4.1	387.0
℄	3.9	387.2
E	3.8	387.3
4+83 = Ex W.M. on East		
4+94 = S. Garage 3 in Alley on East.		
5+00		

E	4.1	387.0
℄	3.8	387.3
W.	4.1	387.0
5+50		
W	4.0	387.1
℄	3.8	387.3
E	3.7	387.4
5+77 = Ex S. W.M. on East.		
6+00		
E	3.4	387.7
℄	3.5	387.6
W	3.6	387.5
6+04 = Ex. S.M.H.		
Flow line	10.17	381.94 ✓
Rim	4.13	387.98
6+50		
W	3.2	387.9
℄	2.6	388.5
E	2.8	388.3
6+85		
E	3.2	387.9
℄	3.7	387.4
W.	3.9	387.2
S.L. El Cajon = 6+90.18 on W.L. 6+93.67 on E.L. of Alley on diagonal		
W Top Cb.	4.62	387.49
gut	4.90	387.21

		392.11		
E			5.10	386.01
gut			4.86	386.25
E. Top Cb			4.65	386.46
T.P.	4.34	391.75	4.70	387.41
			4.92	386.83 = S.W.B.P.
B.M. =				~~387.82~~
				386.8

36' wide
5' walks
26' Roadway

Mechanic St. X Sec 11-23-7E Mulli

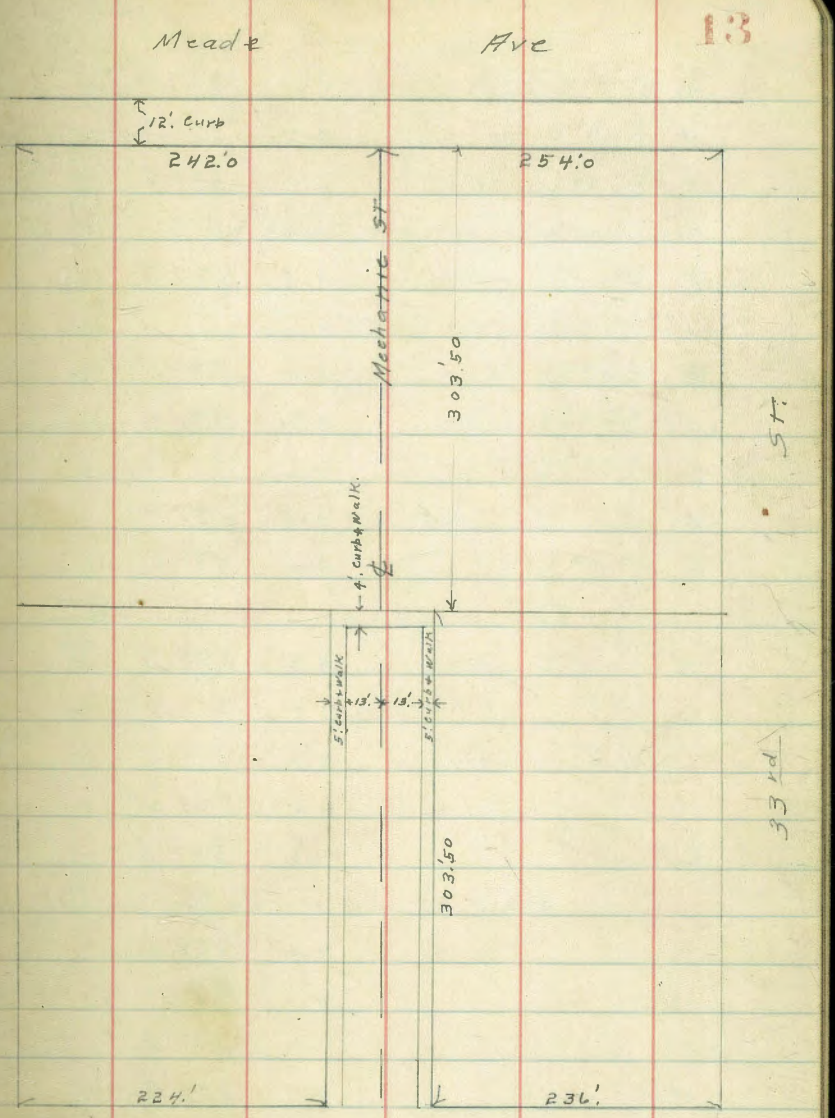
From N. end of Present St to Meade Ave

BM. B.P.	3.76	378.01		374.25	S.W. 33rd St & El Cajon Ave
T.P.	6.44	382.55	1.90	376.11	
00=N. End. Present St. = 303.5 N. of N. Line El Cajon Ave					
W			6.60	375.95	ex cmt walk
el			6.62	375.93	" " "
E			6.62	375.93	" " "
el			6.61	375.94	" " "
E			6.58	375.97	
		50' N.			
E			6.3	376.3	
el			6.4	376.2	
E			6.5	376.1	
el			6.4	376.2	
W			6.4	376.2	
		100' N			
W			5.6	377.0	
el			5.6	377.0	
E			5.6	377.0	
el			5.9	376.7	
E			5.9	376.7	
		150' N.			
E			5.0	377.6	
el			5.1	377.5	
E			5.2	377.4	
el			5.3	377.3	
W			5.4	377.4	

Yardage Tr.
12-10-28
Y. Book 12 Pg 280

Plotted 11/24/28
W.D.S.

13



382.55

200'N

w	4.8	377.7	
cl	4.8	377.7	
c	5.0	377.6	
cl	5.0	377.6	
e	4.9	377.7	

250'N.

e	4.5	378.1	
cl	4.6	378.0	
c	4.6	378.0	
cl	4.7	377.9	
w	4.6	378.0	

298'N

w	4.3	378.3	
cl	4.2	378.4	
e	4.3	378.3	
cl	4.1	378.5	
e	4.0	378.6	

303'.5 N = S. Line Meade Ave

e	4.4	378.2	
cl	4.5	378.1	
c	4.6	378.0	
cl	4.7	377.9	
w	4.7	377.9	

305'. N = S. edge cmt. Walk 4.3 Wide

w	4.64	377.91	on Walk
cl	4.61	377.94	" "

382.55

Mechanic St.

e	4.56	377.99	on walk.
cl	4.42	378.13	" "
e	4.38	378.17	" "

315'.5 N = S. cl. of Meade Ave

e	4.60	377.95	Top cl
cl	4.61	377.94	" "
c	4.73	377.82	" "
cl	4.82	377.73	" "
w	4.84	377.71	" "

314'. N = S. gutter

w	5.7	376.9	
cl	5.7	376.9	
e	5.5	377.1	
cl	5.4	377.2	
e	5.4	377.2	

Meade Ave X S.E. 12-7-28 Miller

Louisiana to Utah.

ck By Walkers Bk Book 2

B.M.	4.67	337.37	332.70	S.E. Meade & Louisiana
		00 = E. line Louisiana		
S. cmt. ch		4.58	332.79 ✓	
S. gutter on pavmt		5.2~	332.15 ✓	
S. ¼ " "		4.60	332.77	
℄ " "		4.34	333.03 ✓	
N. ¼ " "		4.38	332.99	
N. gutter " "		4.77	(~~333.60~~) 332.60	
N. cmt. ch.		4.08	333.29 ✓	
		50' E		
N. cmt. ch		4.40	332.97	
S. " "		5.00	332.37	
		100' E		
S. cmt. ch		5.38	331.99	
N. " "		4.71	332.66	
		140. E. = W. line Alley		
N. line on cmt. ch Return		4.84	332.53	
N. ch " " "		5.08	332.29	
S. ch " " "		5.70	331.67	
S. line " " " Return		5.40	331.97	
		160 E. = E. line Alley		
S. line on cmt. ch. Return		5.51	331.86	
S. ch " " "		5.90	331.47	
N. ch " " "		5.17	332.20	
N. line " " " Return		4.86	332.51	

Curb elev. Plotted 12-11-28 E.B.H.

337.37

200' E.

15

N. cmt. ch		5.43	331.94
S. " "		6.32	331.05
	250' E.		
S cmt. ch		6.52	330.85
N. " "		5.60	331.77
	300' E. = W. line Texas.		
N. cmt. ch.		5.90	331.47 ✓
N. gutter on pavment		6.46	330.91 ✓
N. ¼ " "		6.34	331.03
℄ " "		6.48	330.89 ✓
S. ¼ " "		6.84	330.53
S. gutter " "		7.31	330.06 ✓
S. cmt. ch.		6.86	330.51 ✓
T.P. B.M.	13.13	5.96	331.41 ok. S.E. Meade & Texas.
	00 = E. line Texas.		
S. cmt. ch		13.10	331.44 ✓
S. gutter on pavmt.		13.66	330.88 ✓
S. ¼ " "		13.16	331.38
℄ " "		12.84	331.70 ✓
N. ¼ " "		12.71	331.83
N. gutter " "		12.78	331.76 ✓
N. cmt. ch.		12.11	332.43 ✓
	50' E.		
N. cmt. ch		10.90	333.64
S. " "		12.00	332.54

344.54

100.E.

S. cmt. el		10.87	333.67
N. " "		9.82	334.72
140'S = W. Line Alley			
N. Line on cmt el return		8.74	335.80
N. el cmt. el.		8.91	335.63
S. el " "		10.00	334.54
E. Line on cmt el. return		9.91	334.63
160'E = E. Line Alley			
S. Line cmt. el. ret.		9.24	335.28
S. el cmt. el		9.41	335.13
N. el " "		8.46	336.08
N. Line cmt. el. ret		8.38	(335.16) 336.16
200'E Brk			
N. cmt. el		7.49	337.05
S " "		8.20	336.34
250'E.			
S. cmt. el.		4.04	338.50
N. " "		4.98 ✓	339.56
300'E. = W. Line Arizona.			
N. cmt. el.		2.55	341.99 ✓
N. gutter pavmt.		3.35	~~340.99~~ (341.19)
N. lip	"	3.24	341.30 ✓
℄	"	3.35	341.19 ✓
S. lip	"	3.67	340.87
S. gutter	"	4.22	340.32 ✓
S. cmt. el.		3.52	341.02 ✓

344.54

00 = E Line Arizona

S. cmt el			2.55	341.99 ✓
S. gutter pavmt.			3.10	341.44 ✓
S. lip "			2.15	342.39
℄ "			1.62	342.92 ✓
N. lip "			1.51	343.03
N. gutter "			1.71	342.83 ✓
N. cmt. el.			1.00	343.54 ✓
T.P.	12.65	356.99	0.20	344.34
50'E.				
N. cmt. el			7.77	349.22
S. " "			9.07	347.92
100'E				
S. cmt. el			2.87	354.12
N. " "			2.01	354.98
T.P.	13.06	369.86	0.19	356.80
140'E. = W. Line Alley				
N. Line cmt el. R.t			10.06	359.80
N cmt. el			10.30	359.56
S. " "			10.97	358.89
S. Line cmt el. ret.			10.71	359.15
160'E. = E. Line Alley				
S. Line cmt. el. ret.			8.75	361.11
S. cmt. el			8.79	361.07
N " "			7.69	362.17
N. Line cmt. el. ret			7.61	362.25

		369.86		
		200' E Brk		
N. cmt. el.		3.51	366.35	
S. " "		4.51	365.35	
		220' E. Brk		
S. cmt. el.		2.88	366.98	
N. " "		2.00	367.86	
		240' E. Brk		
N. cmt. el.		0.92	368.94	
S. " "		1.70	368.16	
		260' E Brk		
S. cmt. el.		1.05	368.81	
N. " "		0.25	369.61	
T.P.	8.92	378.61	0.17	369.69
		300' E W. line Hamilton		
N. cmt. el.		8.29	370.32 ✓	
N. gutter	pavmt.	9.02	369.59 ✓	
N 1/4	"	8.85	369.76	
℄	"	8.89	369.72 ✓	
S. 1/4	"	9.25	369.36	
S. gutter	"	9.78	368.83 ✓	
S. cmt el.		9.15	369.46 ✓	
		00 = E. line Hamilton		
S. cmt. el.		7.53	371.08 ✓	
S. gutter	Pavmt.	8.05	370.56 ✓	
S. 1/4	"	7.51	371.10	
℄	"	7.22	371.39 ✓	
N. 1/4	"	7.14	371.47 ✓	

		378.61		
N. gutter	pavmt		7.32	371.29 ✓
N. cmt. el.			6.72	371.89 ✓
		50' E.		
N. cmt. el.			5.38 ✓	373.23
S. " "			5.70	372.91
		80' E. Brk		
S. cmt. el			4.64	373.97
N " "			4.64	373.97
		140' E. = W. line Alley		
N. line	on cmt. el. ret.		3.85	374.76
N. cmt. el.			3.95	374.66
S. " "			3.75	374.86
S. line	" " " "		3.74	374.87
		160' E. = E. line Alley		
S. line	on cmt. el. ret.		3.36	375.25
S. cmt. el.			3.56	375.05
N " "			3.67	374.94
N. line	" " " "		3.54	(374.07) 375.07
		200' E.		
N. cmt. el.			3.20	375.41
S. " "			3.08	375.53
		250' E.		
S. cmt. el.			2.66	375.95
N. " "			2.54	376.07

		378.61		
300'E. = W. line Oregon				
N. cmt. cl.			2.00	376.61 ✓
N. gutter	pavmt.		2.70	? 376.91 375.91
N. 1/4	"		2.31	376.30
℄	"		2.18	376.43 ✓
S. 1/4	"		2.27	376.34
S. gutter	"		2.62	375.99 ✓
S. cmt. cl.			2.00	376.61 ✓
00 = E. line Oregon				
S. cmt. cl.			1.51	377.10 ✓
S. gutter	pavmt.		2.16	376.45 ✓
S. 1/4	"		1.85	376.76
℄	"		1.73	~~374.88~~ ? 376.88
N. 1/4	"		1.85	376.76
N. gutter	"		2.15	376.46 ✓
N. cmt. cl.			1.46	377.15 ✓
T. P. on B/M	3.47	380.70 380.68	1.40	377.21 = 377.23 ✓
		50' E		
N. cmt. cl.			3.76	376.94
S. " "			3.83	376.87
		100' E.		
S. cmt. cl.			4.04	376.66
N " "			3.97	376.73
140'E. = W. line Alley				
N. cmt. cl. No Alley on N.			4.15	376.55
S. cmt. cl.			4.15	376.55
S. line cmt. cl. ret			4.05	376.65

Walker's Book

2k → S.E. Meade

		380.70 380.68		Meade
160' E. = E. line Alley				
S. line cmt. cl. ret			4.11	376.59
S. cmt. cl.			4.18	376.52
N. cmt. cl.			4.25	376.45
200' E.				
N. cmt. cl.			4.42	376.28
S. cmt. cl.			4.40	376.30
250' E				
S. cmt. cl.			4.60	376.10
N. " "			4.63	376.07
300' E. = W. line IDAHO				
N. cmt. cl.			4.78	375.92 ✓
N gutter	pavmt.		5.49	375.21 ✓
N 1/4	"		5.14	375.56
℄	"		5.00	375.70 ✓
S. 1/4	"		5.10	375.60
S. gutter			5.42	375.28 ✓
S. cmt. cl.			4.82	375.88 ✓
00 = E. line Idaho.				
S. cmt. cl.			5.29	375.41 ✓
S. gutter	pavmt.		6.01	374.69 ✓
S. 1/4	"		5.70	375.00
℄	"		5.58	375.12 ✓
N 1/4	"		5.70	375.00
N. gutter	"		6.08	374.62 ✓
N. cmt. cl.			5.31	375.39 ✓

38070

380.68

50' E.

N. cmt. cb.			6.54	374.16
S. " "			6.45	374.25
T.P.	2.94	376.28 376.26	7.36	373.32 4

100' E.

S. cmt cb		3.17	373.11
N. " "		3.24	373.04

140' E. = W. line Alley

N. line cmt. cb. set		3.81	372.47
N. cmt. cb		4.14	372.14
S. " "		4.04	372.24
S. line " " "		3.86	372.42

160' E. = E. line Alley

S. line cmt. cb. set		4.34	371.94
S. cmt. cb		4.55	371.73
N. " "		4.56	371.72
N. line " " "		4.48	371.80

200' E.

N. cmt. cb		5.59	370.69
S. " "		5.53	370.75

250' E

S. cmt cb		6.55	369.73
N. " "		6.75	369.53

Meade

19

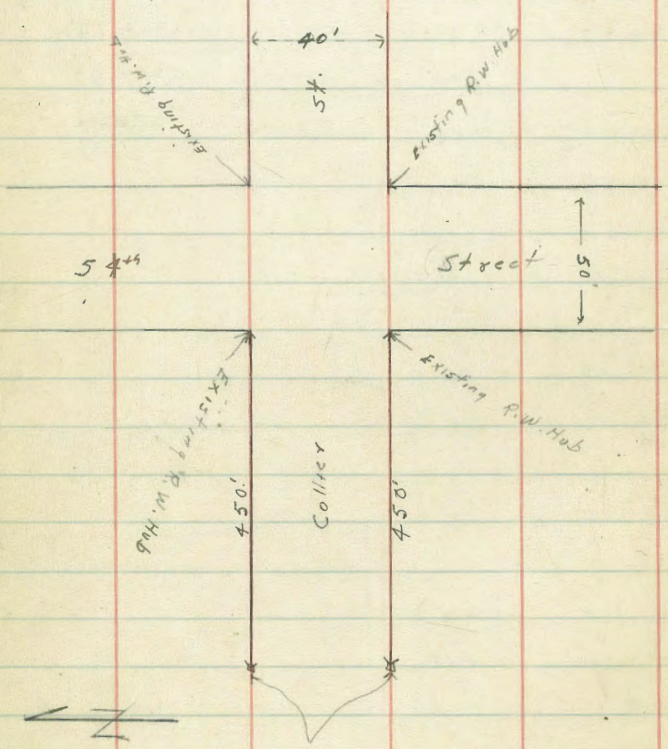
376.28

300' E = W Line Alley

N. cmt. cb,		7.96	368.32 ✓
N. gutter	pavmt.	8.43	367.85 ✓
N. 1/4	"	7.97	368.31
℄	"	7.88	368.40 ✓
S. 1/4	"	8.12	368.16
S. gutter	"	8.31	367.97 ✓
S. cmt. cb.		7.80	368.48 ✓

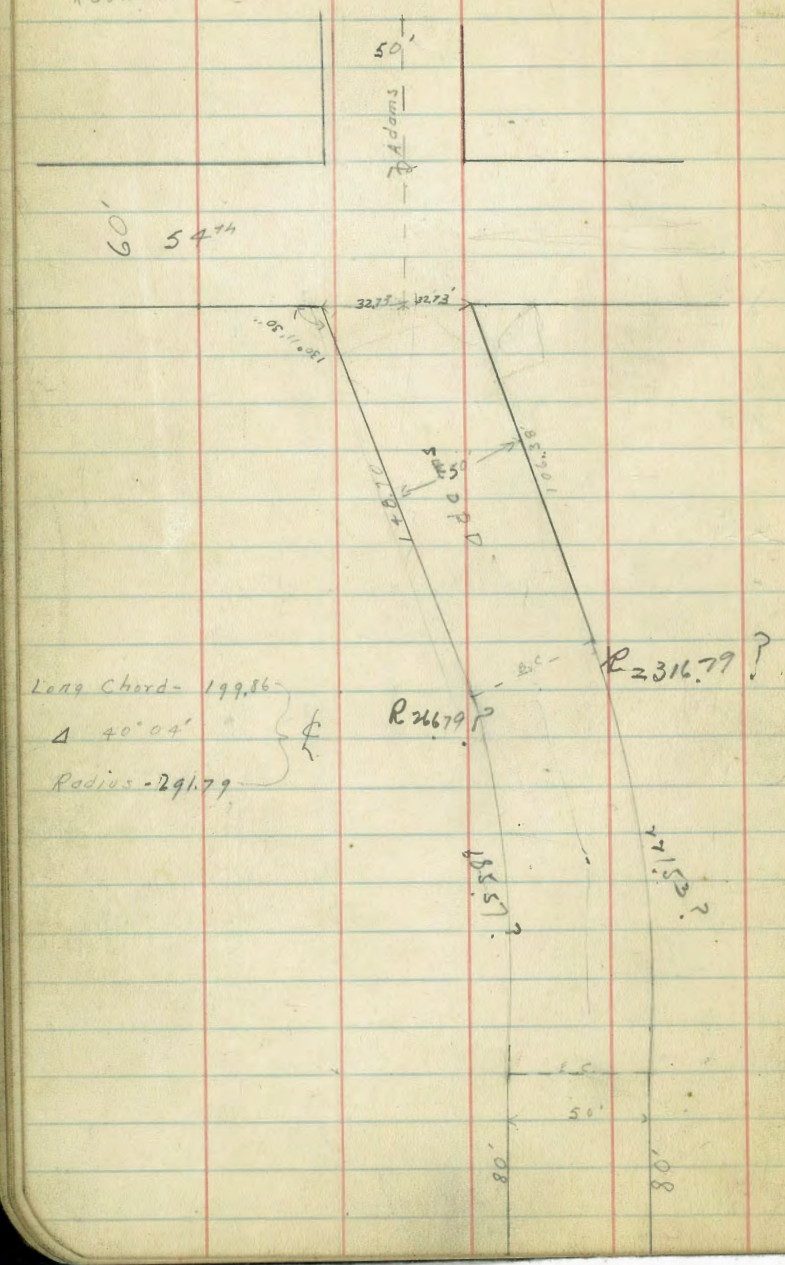
12-18-28
J.C. Bliss
Drebert
Rouner

Extension of Collier St. West of 54th (Radio Road)



12-19-29
J.C. Bliss
Driebert
Rauner

Survey of Extension of Adams Ave West of 54th (Radio Road)



Long Chord - 199.86
Δ 40°04'
Radius - 291.79

R=316.79?

R=291.79?

50.0 / 65.46 = x

7638 ÷ 5

89° 59' 60"
40 - 11 - 60
49 48 10
1 50
49 11
130

X sec V B 11 Pg 37. - 4-1-29 2/25/29

B.P.SW 30th & C — 80' St. 14' cbs 52' Rdway. — 30th to 32nd — Loudon Sec B99 E1

B.M	12.80	20761 ~~20776~~	194.81 ~~194.96~~		
0+00 = EL 30th	Walks & cbs on North		No walks or cbs on South		
Ncb		12.78	194.83		
gut	Pav	13.08	194.53		
1/4	✓	12.74	194.87		
℄	✓	12.62	194.99		
1/4	✓	12.90	194.71		
gut	✓	13.38	194.23		
+1	✓ gut at ret	13.40	194.21		
~~Cb~~+1	top cb end ret	13.01	194.60		
SL		12.8	194.8		
0+25					
SL		10.5	197.1		
+5		10.9	196.7		
+12		11.1	196.5		
cb		11.5	196.1		
1/4		11.5	196.1		
℄		11.5	196.1		
+7		11.7	195.9		
1/4		11.2	196.4		
+6		11.0	196.6		
gut		11.4	196.2		
Ncb		10.96	196.65		

Plotted 3/2-29 -GBH

1.0 ft

		207.61 ~~207.76~~			
0+50					
Ncb			8.83	198.78	
gut			8.8	198.8	
1/4			9.4	198.2	
℄			9.4	198.2	
+6			9.3	198.3	
1/4			9.6	198.0	
+7			9.5	198.1	
cb			9.6	198.0	
+8			9.2	198.4	
+9			8.9	198.7	
SL			9.1	198.5	
0+75					
SL			6.6	201.0	
+11			6.7	200.9	
cb			7.1	200.5	
+1			7.7	199.9	
+7			7.9	199.7	
1/4			7.6	200.0	
℄			7.3	200.3	
1/4			7.4	200.2	
+7			7.0	200.6	
gut			7.0	200.6	
Ncb			6.89	200.72	

		207.61	
1+00			
Neb.		4.98	202.63 ✓
gut		5.2	202.4
¼		5.4	202.2
℄		5.3	202.3
¼		5.4	202.2
+7		5.7	201.9
+12		5.6	202.0
eb		4.9	202.7
+4		4.8	202.8
S.L.		4.5	203.1 ✓
1+25			
S.L.		2.7	204.9
+13		3.0	204.6
eb		3.4	204.2 ✓
+1		3.9	203.7
+7		3.9	203.7
¼		3.5	204.1
℄		3.3	204.3
+10		3.6	204.0
¼		3.4	204.2
+4		3.2	204.4
gut		3.4	204.2
Neb		2.97	204.64 ✓

		207.61 ~~207.76~~		
1+50 = begin inputs on south				
Neb			1.19	206.42 ✓
gut			1.5	206.1
¼			1.7	205.9
℄			1.5	206.1
¼			1.8	205.8
+4			1.9	206.7
+7			2.2	205.4
gut			1.8	205.8
Seb			1.22	206.39
+10			1.0	206.6
S.L.			0.5	207.1
TP	2.75	210.19 ✓ ~~210.34~~	0.17	207.44 ~~207.59~~
1+75				
Seb			2.49	207.70
gut			3.2	207.0
¼			3.1	207.1
℄			2.7	207.5
¼			2.9	207.2
gut			2.7	207.5
Neb			2.41	207.78

		210.19	
2+00			
Ncb		1.60	208.59
gut		1.8	208.3
+12		1.9	208.2
1/4		2.1	208.0
+2		2.2	207.9
℄		1.7	208.5
1/4		2.1	208.1
gut		2.2	208.0
Scb		1.64	208.55
2+25			
Scb		1.14	209.05
gut		1.7	208.5
1/4		1.6	208.6
℄		1.3	208.9
1/4		1.4	208.8
gut		1.5	208.7
Ncb		1.17	209.02

		210.19	
2+50 = end imbuits on South			
Ncb		095	209.24
gut		1.2	209.0
+5		1.1	209.1
1/4		1.4	208.8
+2		1.4	208.8
+12		1.1	209.1
℄		1.2	209.0
1/4		1.6	208.6
+10		1.8	208.4
gut		1.6	208.6
Scb		1.02	209.17
S.L.		0.87	209.4
2+75			
S.L		1.1	209.1
+9		1.2	209.0
cb		1.8	208.3
+5		2.0	208.2
1/4		1.7	208.5
℄		1.2	209.0
1/4		1.5	208.7
gut		1.5	208.7
Ncb		1.17	209.02

210.19

3+00		
Ncb	1.79	208.40 ✓
gut	2.4	207.8
¼	2.1	208.1
℄	1.7	208.5
¼	2.1	208.1
+10	2.7	207.3
cb	2.5	207.7
+3	1.7	208.5
SL	1.4	208.8
3+25		
SL	2.4	207.8
+11	2.7	207.5
cb	3.5	206.7
+3	3.9	206.3
¼	3.2	207.0
℄	2.9	207.3
¼	3.3	206.9
+2	3.4	206.8
+10	3.1	207.1
gut	3.1	207.1
Ncb	2.64	207.55 ✓

210.19

25

3+50		
Ncb	4.36	205.83 ✓
gut	5.0	205.2
+3	4.9	205.3
+9	5.3	204.9
¼	5.1	205.1
℄	4.7	205.5
+10	4.6	205.6
¼	4.8	205.4
+9	5.2	205.0
cb	4.6	205.6
+3	4.3	205.9
SL	4.0	206.2
3+75		
SL	6.4	203.8
+12	6.7	203.5
cb	7.1	203.1
+8	7.7	202.5
¼	7.2	203.0
+8	7.2	203.0
℄	7.3	202.9
+4	7.0	203.2
¼	7.4	202.8
+4	7.6	202.6
+8	7.4	202.8
gut	7.5	202.7
Ncb	6.75	203.44 ✓

4+00	210.19 ~~210.34~~			
Neb		10.06	200.13	
gut		10.5	199.7	
1/4		10.6	199.6	
℄		10.5	199.7	
+5		10.5	199.7	
1/4		10.6	199.6	
+9		11.1	199.1	
eb		10.5	199.7	
+2		10.0	200.2	
+9		10.1	200.1	
S.L.		10.1	200.1	
T.P.	0.07	197.28 ~~197.35~~	13.06	~~197.28~~ 197.13
4+26 = end imbuts on North.				
S.L.		0.3	196.9	
+13		0.8	196.4	
eb		1.1	196.1	
+8		1.6	195.6	
1/4		1.4	195.8	
℄		1.1	196.1	
1/4		1.1	196.1	
+7		1.6	195.6	
gut		1.3	195.9	
Neb		0.71	196.49	
14.10		0.3	196.9	
N.L.		+0.7	197.9	

	197.20		
4+50	~~197.35~~		
N.L.		1.9	195.3
+3		3.6	193.6
+12		4.0	193.2
eb		4.4	192.8
+4		5.1	192.1
1/4		5.0	192.2
℄		4.8	192.4
+6		4.4	192.8
1/4		4.8	192.4
+5		4.7	192.5
+10		5.5	191.7
eb		4.7	192.5
+2		4.2	193.0
S.L.		4.0	193.2
4+75			
S.L.		8.3	188.9
+13		9.0	188.2
eb		9.2	188.0
+3		10.4	186.8
+1		9.4	187.8
1/4		9.5	187.7
+10		9.2	188.0
℄		9.4	187.8
1/4		9.5	187.7
+7		9.3	187.9

197.20

4+75	+97.35		
cb		9.3	187.9
+6		8.0	189.2
+10		8.0	189.2
N.L.		6.9	190.3
5+00			
N.L		11.5	185.7
+6		12.1	185.1
cb		14.8	182.4
+8		14.5	182.7
1/4		14.5	182.7
℄		14.2	183.0
+10		14.0	183.2
1/4		14.6	182.6
+11		15.2	182.0
+12		15.7	181.5
cb		15.4	181.8
+2		14.4	182.8
S.L.		14.0	183.2 ✓
T.P. 0.03	184.15 ✓ +84.30	13.08	+84.27 184.12

184.15

5+20	184.30		
S.L		5.2	179.0 ✓
+4		6.0	178.2
+13		5.6	178.6
cb		6.1	178.1
+1		7.0	177.2
+5		6.7	177.5
1/4		5.2	179.0
+7		3.9	180.3
℄		3.7	180.5
+10		4.0	180.2
1/4		4.1	180.1
+8		4.0	180.2
cb		4.3	179.9
+2		4.2	180.0
+5		3.0	181.2
N.L.		2.6	181.6 ✓
5+40			
N.L.		5.5	178.7 ✓
cb		5.6	178.6
1/4		5.3	178.9
℄		5.2	179.0
+7		5.3	178.9
1/4		5.7	178.5
+9		9.7	174.5
cb		10.0	174.2

5+40		
S.L.	9.8	174.4
5+60		
10's	13.7	170.5
S.L.	13.3	170.9
+2	13.3	170.9
cb	9.8	175.4
+6	7.8	176.4
1/4	6.2	178.0
+3	5.7	178.5
℄	6.1	178.1
1/4	6.2	178.0
+11	6.5	177.7
cb	6.0	178.2
N.L.	6.2	178.0
5+80		
N.L.	8.3	175.9
cb	7.4	176.8
1/4	7.2	177.0
℄	6.8	177.4
+7	6.7	177.5
1/4	6.2	178.0
cb	11.2	173.0
S.L.	14.1	170.1
4's	14.9	169.3
12's	20.5	163.7
20's	19.1	165.1

6+00		
30's	31.0	153.2
15's	24.4	159.8
S.L.	16.6	167.6
cb	10.1	174.1
+9	6.6	175.6
1/4	7.2	177.0
℄	7.4	176.8
+10	6.9	177.3
1/4	7.9	176.3
+3	9.2	175.0
+7	10.0	174.2
cb	9.5	174.7
+6	10.2	174.0
N.L.	12.6	171.6
10'N	14.1	170.1
6+11 = n.c. 31st on North.		
N.L.	14.1	170.1
cb	12.3	171.9
+11	11.0	173.2
1/4	9.5	174.7
+5	6.7	177.5
℄	7.2	177.0
1/4	7.0	177.2
+5	6.7	177.5
+7	8.2	176.0
cb	9.0	175.2

C St.

184.15

6+11		+84.30		
S.L.			19.2	165.0
8'S			24.1	160.1
20'S			26.5	157.7
30'S			30.4	153.8
35S			32.2	151.0
40S			33.1	151.1

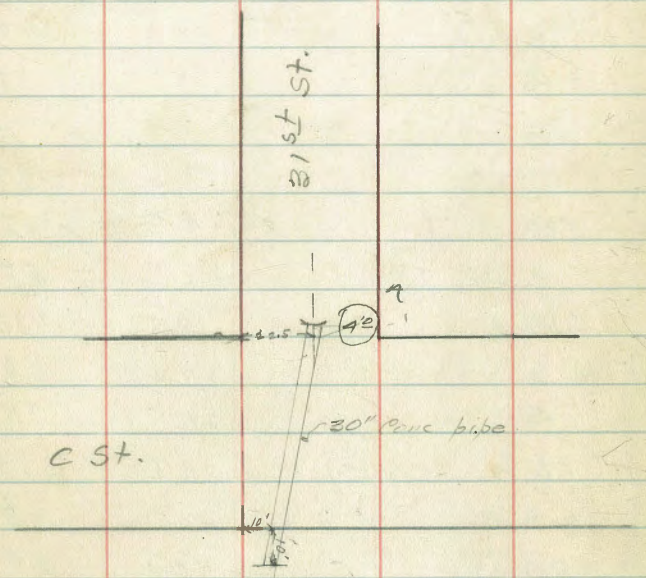
31st 40' wide 3 cbs 30' Rdway.

Web	31st			
40S			33.8	150.4
30'S			32.6	151.6
20'S			28.6	155.6
10'S			26.5	157.7
9'S			22.1	162.1
S.L.			17.7	166.5
cb			9.2	175.0
+7			6.7	177.5
¼			7.1	177.1
℄			7.2	177.0
+7			7.4	176.8
¼			10.7	173.5
+8			15.0	169.2
cb			14.5	169.7
+4			13.4	170.8
N.L.		184.95	14.0	170.2
B.M.	12 99	185.10	12.19	~~172.11~~ 171.96

C St.

30'

Web +5 10'S



Culvert thru C at 31st

C st

18495

W ¼ 31st	185+10		
N.L.		17.7	167.2
+6		18.2	168.8
cb		18.3	166.7
+6		17.8	167.2
¼		14.2	170.8
+10		8.1	176.9
℄		7.8	177.1
¼		7.5	177.5
+10		8.3	176.7
cb		9.7	175.3
S.L.		18.5	166.4
8's		23.2	161.8
9's		29.1	155.9
(F.L. S end culvert)		28.21	156.89 156.74
22 S		32.7	152.3
35 S		34.4	150.6
45 S		35.0	150.0
℄ 31st			
40 S		31.8	153.2
30 S		29.8	155.2
25 S		31.0	154.0
20 S		27.5	157.5
10 S		22.6	162.4
S.L.		16.2	168.7
cb		9.6	175.4
+5		7.4	177.6

18495

A
2.5

℄ 31st	185+10		
¼		7.3	177.7
℄		7.6	177.3
+3		7.9	177.1
¼		15.0	170.0
+3		17.4	167.6
cb		18.4	166.6
+2		17.8	167.2
N.L.		20.6	164.3
(F.L. N end culvert)		25.90	159.05
E ¼ 31st			
N.L.		21.3	163.6
cb		17.9	167.1
¼		13.8	171.2
+5		12.7	172.3
℄		8.0	176.9
+5		7.4	177.6
¼		7.3	177.7
+9		7.3	177.7
cb		8.9	176.1
S.L.		15.3	169.6
10's		21.1	163.9
20's		26.8	158.2
30's		27.0	158.0

C St

184.95

Cb 31st

30'S		25.0	160 0
18'S		24.3	160 8
6'S		16 4	168 6
S.L.		15.0	169.9
		+5	+83.4
Cb		8.6	176 4
+5		2.2	177 8
¼		7.1	177 9
+11		7.3	177 7
℄		7.6	177.3
+8		8.2	176 8
+10		12.6	172 4
¼		13.3	171 7
Cb		15.0	170 0
N.L		21.0	163.9

What ?

E.L 31st = 0+00

NL	21.0	163.9
Cb	14.5	170 5
+6	11.1	173 9
¼	12.6	172 4
+4	12.1	172 9
℄	7.5	177.4
+3	7.1	177 9
¼	6.9	178 1
+10	6 9	178 1
Cb	8 3	176 7

C St

184 95

0+00

S.L.	13.6	171.3
13 S	19.0	166 0
23 S	23.6	161 4
30 S	22.4	162 6

0+10

30 S	19.9	165 1
22 S	19.0	166 0
20 S	20.1	164 9
9 S	15.0	170 0
S.L.	13.0	171.9
+12	7 7	177 3
Cb	7.5	177 5
+3	6.6	178 4
¼	6 7	178 3
℄	7.0	177.9
+4	7 3	177 7
+11	11.1	173 9
¼	11.0	174 0
Cb	11.0	174 0
NL	11.0	173.9

		Cst.			
		184.95			
0+35		+85.10			
N.L			9.0	175.9	
cb			8.8	176.1	
¼			7.1	177.8	
+8			5.6	179.3	
℄			6.0	178.9	
¼			5.9	179.0	
cb			6.2	178.7	
S.L			9.3	175.6	
10's			9.9	175.0	
0+60					
S.L			4.1	180.8	
+4			5.3	179.6	
cb			4.6	180.3	
¼			4.0	180.9	
℄			4.3	180.6	
¼			4.9	180.0	
+5			5.1	179.8	
cb			3.9	181.0	
+6			2.4	182.5	
+12			3.2	181.7	
NL			2.4	182.5	
T.P.	11.97	196.71 196.86	0.21	+84.89	184.74

		Cst.			32
		196.71			
0+85		+96.86			
NL			9.2	187.5	
+2			10.0	186.7	
+9			10.2	186.5	
cb			10.0	186.7	
+6			11.7	185.0	
¼			12.1	184.6	
℄			12.3	184.4	
¼			12.8	183.9	
+3			12.6	184.1	
+7			12.4	184.3	
cb			13.0	183.7	
+1			12.7	184.0	
+2			12.1	184.6	
+11			11.8	184.9	
S.L			9.8	186.9	
1+10					
S.L			5.2	191.5	
+4			6.7	190.0	
+8			7.8	188.9	
+9			7.1	189.6	
+12			7.0	189.7	
+12			8.5	188.2	
cb			8.6	188.1	
+6			7.6	189.1	
¼			7.6	189.1	

C.6+

196.71

1+10		
℄	7.3	189.4
¼	7.2	189.5
+8	6.6	190.1
+9	5.0	191.7
cb	5.0	191.7
+10	4.4	192.3
N.L.	2.7	194.0
1+25 = beg. inputs on North.		
N.L.	2.5	194.2
+4	3.4	193.3
cb +cb	4.05	192.66
gut	4.0	192.7
+5	5.0	191.7
¼	5.3	191.4
℄	5.5	191.2
¼	5.6	191.1
+6	5.5	191.2
cb	5.9	190.8
+1	5.1	191.6
+9	5.1	191.6
SL.	3.6	193.1

C.6+

196.71

1+37		
S.L.	3.5	193.2
+8	4.2	192.5
cb	4.2	192.5
¼	4.6	192.1
℄	4.3	192.4
¼	4.2	192.5
+8	3.9	192.8
gut	3.6	193.1
Ncb	3.17	193.54
1+60		
Ncb	1.5L	195.15
gut	2.0	194.7
¼	1.9	194.9
+10	2.0	194.7
℄	2.3	194.4
+3	2.5	194.2
+10	2.3	194.4
¼	2.6	194.1
+7	3.2	193.5
cb	2.7	194.0
+1	2.4	194.3
SL	2.0	194.7

C. St.

196.71

+96.86

1+82.3 = beg. of inverts on South

S.L.			0.7	196.0
+5			1.0	195.7
cb	top		1.30	195.41
gut			1.7	195.0
+3			2.1	194.6
1/4			1.3	195.4
+8			1.2	195.5
℄			0.8	195.9
1/4			0.5	196.2
gut			0.6	196.1
Ncb			0.37	196.34 ✓
T.P.	4.23	200.88 ✓ 201.03	0.06	196.80 196.65

2+20 = W.L. Edgement on North

Ncb		2.86	198.02
gut		3.3	197.6
+10		3.6	197.3
1/4		3.4	197.5
+5		3.2	197.7
℄		3.4	197.5
1/4		4.1	196.8
+8		4.7	196.2
gut		4.4	196.5
Scb		4.02	196.86

C St.

200.88

2+30 = W.L. Edgement

201.03

Scb		3.75	197.13
gut		4.1	196.8
+5		4.3	196.6
1/4		3.8	197.1
℄		3.1	197.8
+8		2.8	198.1
1/4		2.0	198.9
+5		3.3	197.6
cb		3.2	197.7
gut		2.5	198.4
N.L.	top cb	2.55	198.33 ✓

2+50 = ℄ Edgement on North

N.L	1.6	199.3
cb	2.2	198.7
1/4	2.4	198.5
℄	2.7	198.2
1/4	3.4	197.5
+10	3.8	197.1
gut	3.5	197.4
Scb	3.21	197.67

C

200.88

2+54.99 = W.L Edgemont on South.			
Scb		3.08	197.80
gut		3.4	197.5
+5		3.7	197.2
¼		3.6	197.3
℄		2.6	198.3
¼		2.4	197.5
eb		2.2	198.7
N.L.		1.7	199.2
2+64.99 = W.eb Edgemont on South.			
N.L.		1.7	199.2
eb		2.2	198.7
¼		2.2	198.7
℄		2.5	198.4
+5		2.6	198.3
¼		3.1	197.8
+10		3.6	197.3
eb		3.5	197.4
S.L. gut		2.4	197.5
S.L. top eb		3.10	197.78 ✓

C

200.88

35

2+70	201.03		
S.L.		3.3	197.6 ✓
+5		2.9	198.0
eb		3.5	197.4
¼		3.0	197.9
℄		2.3	198.6
¼		2.3	198.6
eb		2.2	198.7
N.L.	gut	1.7	199.2
N.L.	top eb	1.38	199.50 ✓
B.M.	N.E. Edgemont & C	1.29	~~199.74~~ 199.59
2+80 = E.L. Edgemont on North			
Neb		1.66	199.22
gut		1.9	199.0
¼		2.3	198.6
℄		2.1	198.8
¼		2.7	198.2
+11		3.4	197.5
eb		3.3	197.6
+8		2.6	198.3
S.L.		2.7	198.2

C5+

200.88

2+85 = ℄ Edgemont on South.			
S.L.		2.7	198.2
+6		2.6	198.3
cb		3.2	197.9
+2		3.3	197.6
¼		2.7	198.2
+11		2.1	198.8
℄		2.2	198.7
¼		2.1	198.8
gut		1.7	199.2
Neb		1.57	199.31
3+15 = E.L. Edgemont on South - beg. inputs on South.			
Neb		1.46	199.42
gut		2.0	198.9
¼		2.0	198.9
+8		1.9	199.0
℄		2.0	198.9
¼		2.5	198.4
gut		2.8	198.1
Seb		2.39	198.49
S.L.		2.4	198.5

C5+

200.88

36

3+35			
Seb		2.32	298.56
gut		2.8	198.1
¼		2.3	198.6
℄		1.9	199.0
+6		1.8	199.1
¼		1.9	199.0
gut		2.2	198.7
Neb		1.41	199.47
3+60			
Neb		1.59	199.29
gut		2.2	198.7
¼		2.1	198.8
+9		2.1	198.8
℄		2.3	198.6
¼		2.8	198.1
gut		3.1	197.8
Seb		2.52	198.36
3+75.30 = W.L. Alley on	End of inputs on North. Alley ret in North.		No Alley eb.
Seb		2.71	198.17
gut		3.3	197.6
¼		3.0	197.9
℄		2.5	198.4
¼		2.4	198.5
gut		2.2	198.7
Neb		1.83	199.05
+10		1.6	199.3

		C.S.+	
		200.88	
3+75 30			
N.L.		+0.5	201.4
M.H. on ℄ at 3+82 ℄		2.60	198.28
F.L.		8.35	192.53
3+90 3 = F.L. Alley			
N.L.		0.0	200.88
+5		1.9	199.0
+12		2.2	198.7
eb		2.4	198.5
+3		2.9	198.0
¼		2.8	198.1
+9		2.7	198.2
℄		2.8	198.1
¼		3.2	197.7
+10		3.7	197.2
gut		3.5	197.4
Scb		3.02	197.86
4+10			
Scb		3.53	197.35
gut		4.5	196.4
¼		3.8	197.1
℄		3.5	197.4
¼		3.4	197.5
+10		3.6	197.3
eb		3.2	197.7
+6		2.7	198.2

		C.S.+			37
		200.88			
4+10		201.03			
+10			2.5	198.4	
N.L.			1.4	199.5	
4+45 = N.L. Alley on South				w. Alley 2 rct in. End of Inputs on S.	
N.L.			2.4	198.5	
+5			3.7	197.2	
+12			3.8	197.1	
eb			4.2	196.7	
+3			4.7	196.2	
¼			4.6	196.3	
+9			4.5	196.4	
℄			4.8	196.1	
¼			5.4	195.5	
+7			5.8	195.1	
eb			5.6	195.3	
Scb	top		4.68	196.20	
S.L.	top Alley eb		4.48	196.40	
S.L.	grd.		4.5	196.4	
T.P.			4.33	~~196.70~~ 196.55	
N.E. Elements of					
B.M.	1.93	201.67		199.74	(199.59 V Rec.)
T.P.	8.18	209.49	0.36	201.31	
T.P.	2.67	200.57	11.59	197.90	
B.M.			5.58	194.99	(194.96 Rec.)

Cst

196.76

T.P	0.21	196.91	196.70
4+65 = E.L. Alley			
S.L		0.9	195.9
+4		1.6	195.2
cb		2.0	194.8
+3		2.4	194.4
+5		3.0	193.8
¼		2.6	194.2
+8		2.0	194.8
℄		2.0	194.8
¼		1.8	195.0
+7		1.9	194.9
+8		2.1	194.7
+9		1.9	194.8
cb		1.3	195.5
+7		1.1	195.7
N.L		+0.1	196.9
4+90 = beg. inputs on North.			
N.L		3.3	193.5
N.b		3.41	193.35
gvt		3.4	193.4
+6		4.7	192.1
¼		4.2	192.6
℄		4.4	192.4
¼		4.9	191.9
+11		5.5	191.3
cb		4.4	192.4

Cst

196.76

4+90	196.91	
+1	4.2	192.6
+7	4.2	192.6
+13	3.8	193.0
S.L	3.2	193.6
5+10		
S.L	5.7	191.1
+2	6.3	190.5
+11	6.8	190.0
cb	7.7	189.1
+6	7.4	189.4
¼	6.9	189.9
℄	6.9	189.9
+10	6.6	190.2
¼	6.5	190.3
gvt.	6.0	190.8
Neb	5.98	190.98
5+35		
Neb	9.28	187.48
gvt	9.6	187.2
¼	10.0	186.8
℄	10.3	186.5
¼	10.4	186.4
cb	10.6	186.2
+3	10.8	186.0
+4	9.8	187.0

C st

196.76

5+35	196.91		
S.L.		8.5	188.3
5+50 brk Neb.			
S.L.		11.5	185.3
+9		12.1	184.7
+11		12.7	184.1
eb		12.6	184.2
¼		12.7	184.1
±		12.8	184.0
+10		12.3	184.5
¼		12.5	184.3
+9		12.2	184.6
gut		11.9	184.9
Neb		11.31	185.45
T.P. 0.07	183.81	13.02	183.89 183.74
5 +85	183.96		
Neb		5.32	178.49
gut		5.7	178.1
+11		4.4	179.4
¼		4.4	179.4
±		4.6	179.2
¼		5.1	178.7
eb		5.8	178.0
+6		5.6	178.2
+10		5.5	178.3
S.L.		4.8	179.0

C st

183.81

5+91	183.96		
Neb (brk)		6.43	177.38
6+09.8 = n.c. 32nd		(new ret in 10' R.)	
S.L.		9.3	174.5
+8		8.6	175.2
eb		7.9	175.9
¼		7.2	176.6
±		6.5	177.3
+5		6.2	177.6
+10		7.1	176.7
¼		7.3	176.5
±7		7.3	176.5
+11		9.0	174.8
g.t		9.0	174.8
Neb		9.00	174.81
Bnl Nails show sign nw 32nd c.c.	196.58	6.58	177.38 177.23
T.P. 12.89	196.73	0.07	183.89 183.74
	202.08		
T.P. 5.67	202.18	0.17	196.56 196.41
n.c. Edgemont c.c.			
P.M.		2.45	199.73 (199.79)

office OK. (199.59)

2/27/29 X sec 32nd S + B to Broadway

London 60' wide 10' obs 40' Rdway

slew sixth 32nd sec

BM	9.89	187.12		177.23
		187.27		177.38

see page 39

0+00 = S.L. B St.

N.L.	4.1	183.0
cb	5.0	182.1
1/4	6.0	181.1
+5	6.2	180.9
℄	5.6	181.5
+3	5.7	181.4
1/4	7.0	179.7
cb	8.1	179.0
+6	8.5	178.6
E.L.	9.3	177.8

0+05

E.L.	9.5	177.6
+3	8.5	178.6
cb	7.9	179.2
1/4	6.8	180.3
℄	5.0	182.1
1/4	3.6	183.5
cb	1.6	185.5
N.L.	+0.4	187.5

Plotted 4-5-29 COH

32nd

187.12

187.27

0+30

N.L.	0.2	186.9
+5	2.6	184.5
cb	3.3	183.8
1/4	5.0	182.1
℄	6.3	180.8
1/4	7.7	179.4
cb	9.2	177.9
+2	9.4	177.7
+4	9.0	178.1
E.L.	8.7	178.4
10E	9.0	178.1

0+50

10E	9.9	177.2
3E	9.5	177.6
E.L.	10.2	176.9
+3	10.5	176.6
+8	12.2	174.9
cb	11.8	175.3
+2	11.8	175.3
+5	10.8	176.3
1/4	9.8	177.3
℄	7.8	179.3
1/4	6.9	180.2
cb	5.5	181.6
+8	3.6	183.5
N.L.	2.6	184.5

32nd

187.12

0+75

W.L.	7.1	180.0
+2	8.1	179.0
cb	9.2	177.9
¼	10.6	176.5
℄	12.4	174.7
¼	13.2	173.9
cb	14.4	172.7
EL	16.6	170.5
10E	18.5	168.6
1+00		
15E	25.2	161.9
6E	24.6	162.5
E.L.	22.7	164.4
cb	20.0	167.1
+8	17.0	170.1
¼	16.5	170.6
+5	15.3	171.8
℄	14.8	172.3
¼	13.6	173.5
cb	11.8	175.3
+5	10.9	176.2
WL	9.1	178.0

32nd

187.12

41

1+25

W.L	9.9	177.2
cb	12.8	174.3
¼	14.4	172.7
℄	17.1	170.0
+2 Top 6" vitrified pipe Sewer?	17.4	169.7
¼	19.2	167.9
+2	19.3	167.8
cb	22.8	164.3
+3	25.0	162.1
EL.	28.7	158.4
15E	31.4	155.7
20E	34.6	152.5
1+40 = N.L Alley		
15E	28.0	159.1
E.L.	22.6	164.5
cb	20.2	166.9
+5	18.6	168.5
¼	17.8	169.3
℄	16.6	171.5
¼	13.9	173.2
+4	13.7	173.4
cb	12.2	174.9
W.L.	10.2	176.9

3.2 mg

187.12
+87.27

1+60 = 5 L. Alley

W.L.			9.3	177.8
Cb			11.2	175.9
¼			13.0	174.1
T.P.	6.29	180.42 180.57	12.99	174.13 174.28
℄			8.0	172.4
¼			9.7	170.7
Cb			11.8	168.6
E.L.			14.1	166.3
10 E.			16.2	164.2
1+75				
10 E.			13.5	166.9
E.L.			11.5	168.9
Cb			10.1	170.3
¼			8.5	171.9
℄			7.4	173.0
+5			6.1	174.3
¼			5.5	174.9
Cb			4.5	175.9
+5			2.5	177.9
W.L.			1.0	179.4

3.2 mg

180.42

2+00

W.L.	0.1	180.3
+5	2.5	177.9
Cb	3.4	177.0
¼	5.0	175.4
℄	7.1	173.3
¼	8.5	171.9
Cb	10.5	169.9
+5	11.1	169.3
E.L.	11.3	169.1
10 E.	10.4	170.0
2+25		
10 E.	9.8	170.6
E.L.	10.6	169.8
+4	11.1	169.3
Cb	10.7	169.7
¼	9.4	170.0
℄	7.7	172.7
+4	6.5	173.9
¼	5.4	175.0
Cb	3.5	176.9
+4	2.7	177.7
W.L.	0.2	180.2

32 nd

180.42

2+50

W.L.		0.4	180.0
+5		3.0	177.4
cb		4.0	176.4
¼		6.7	173.7
℄		8.4	172.0
¼		9.7	170.7
cb		10.7	169.7
EL		10.9	169.5
IDE		10.8	169.6

2+75

IDE		9.6	170.6
EL		10.4	170.0
cb		10.1	170.3
¼		9.4	171.0
+5		9.2	171.2
+7		8.6	171.8
℄		8.2	172.2
+6		7.6	172.8
¼		6.7	173.7
cb		4.4	176.0
+3		3.7	176.7
W.L.		0.4	180.0

32 nd

180.42

43

3+00 = N.L C st.

W.L.		4.4	176.0
cb	top cb and ret.	5.58	174.84 ✓
cb		5.8	174.6
+5		6.1	174.3
¼		7.2	173.2
℄		7.7	172.7
¼		7.7	172.5
+3		8.0	172.4
cb		9.5	170.9
EL		10.2	170.2
IDE		10.8	169.6

N cb C

IDE		11.9	168.5
EL		9.4	171.0
cb		8.7	171.7
¼		7.7	172.7
℄		6.9	173.5
¼		6.5	173.9
cb		5.3	175.1
W.L.	prof.	5.6	174.8
W.L.	+ cb cb	5.59	174.83 ✓

32 nd

180.42

N ¼ C

W.L.	3.9	176.5
+7	3.0	177.4
cb	3.9	176.5
¼	5.4	175.0
℄	6.4	174.0
¼	8.1	172.3
cb	8.8	171.6
E.L.	9.5	170.9
5 E	9.7	170.7
10 E	11.5	168.9

℄ C

10 E	11.3	169.1
E.L.	10.6	169.8
+3	10.0	170.4
cb	7.6	172.8
+5	7.1	173.3
¼	7.0	173.4
℄	6.3	174.1
¼	4.7	175.7
+6	4.5	175.9
cb	3.7	176.7
+6	3.3	177.1
W.L.	3.0	177.4

32 nd

180.42

S ¼ C

W.L.	3.8	176.6
cb	4.2	176.2
¼	5.0	175.4
+6	5.6	174.8
℄	6.3	174.1
¼	7.2	173.2
cb	8.8	171.6
+3	10.0	170.4
E.L.	11.1	169.3
10 E	11.9	168.5

S cb C

10 E	11.5	168.9
E.L.	11.0	169.4
cb	9.0	171.4
+6	8.4	172.0
¼	6.6	173.8
+5	6.8	173.6
℄	6.1	174.3
+3	5.7	174.7
¼	5.3	175.1
cb	5.0	175.4
W.L.	4.5	175.9

180.42

S.L. C = 0+00

W.L.	5.9	174.5	
+4	5.7	174.7	
cb	5.7	174.7	
¼	6.1	174.3	
℄	6.4	174.0	
+4	6.5	173.9	
+6	7.0	173.0	
¼	7.7	172.7	
+7	8.5	171.9	
cb	8.8	171.6	
E.L.	10.6	169.8	
10 E	12.0	168.4	
0+10			
10 E	11.6	168.8	
5 E	10.1	170.3	
E.L.	10.4	170.0	
cb	9.2	171.2	
¼	7.8	172.6	
+8	7.1	173.3	
℄	6.8	173.6	
¼	6.8	173.6	
+5	6.5	173.9	
cb	6.8	173.6	
+3	6.6	173.8	
+6	3.7	176.7	
W.L.	3.2	177.2	

32nd

180.42

180.57

177.98

178.12

45

office

Men inside R 32nd sec

B.M.	0.20	2.65	177.78 177.92
0+25			
W.L.	1.3		176.7
+9	2.3		175.7
cb	3.4		174.6
+2	5.2		172.8
¼	5.3		172.7
℄	5.3		172.7
¼	5.4		172.6
+1	5.5		172.5
+6	6.7		171.3
cb	7.3		170.7
E.L.	8.4		169.6
10 E	9.0		169.0
0+50			
10 E	9.2		168.8
7 E	9.2		168.8
E.L.	8.8		169.2
cb	7.1		170.9
+2	6.5		171.5
¼	6.5		171.5
℄	6.8		171.2
+8	6.8		171.2
¼	4.1		173.9
+9	4.1		173.9
cb	3.3		174.7

177.98

0+50.		
w.L	2.0	176.0
0+75		
w.L	3.1	174.9
cb	4.8	173.2
¼	5.0	173.0
+5	6.1	171.9
+7	7.9	170.1
+9	8.2	169.8
℄	8.5	169.5
¼	7.8	170.2
cb	7.7	170.3
+2	7.7	170.3
+5	9.0	179.0
E.L.	9.6	168.4
IDE	10.5	167.5
1+00		
IDE	11.4	166.6
E.L	10.5	167.5
+3	10.1	167.9
+5	8.8	169.2
cb	9.0	169.0
¼	9.3	168.7
+6	10.1	167.9
℄	8.4	169.6
+3	7.0	171.0

32 29

177.98

1+00		
¼	5.8	172.2
cb	5.2	172.8
w.L.	3.8	174.2
1+25		
w.L.	4.4	173.6
cb	6.4	171.6
+5	6.7	171.3
¼	6.7	171.3
℄	8.6	169.4
+8	11.0	167.0
+6	11.5	166.5
¼	11.0	167.0
cb	10.4	167.6
+6	10.4	167.6
+8	11.4	166.6
EL	11.8	166.2
IDE	12.8	165.2
1+50		
IDE	14.5	163.5
E.L	13.1	164.9
+4	12.0	166.0
cb	12.0	166.0
+6	12.2	165.8
¼	12.6	165.4
+3	13.3	164.7
+6	12.4	165.6

177.98

1+50.	178.12			
℄		10.0	168.0	
+7		9.0	169.0	
¼		8.1	169.9	
+1		7.9	170.1	
cb		8.1	169.9	
w.L.		6.0	172.0	
1+75				
	171.45		165.35	
T.P.	6.10 171.59	12.63	165.47	
w.L.		0.1	171.4	
cb		1.4	170.1	
¼		2.7	168.8	
+8		4.3	166.2	
~~cb~~		5.1	166.4	
+5		7.9	163.6	
¼		7.3	164.2	
cb		6.8	164.7	
+6		6.6	164.9	
+9		8.1	163.4	
E.L		8.4	163.1	
10E		9.9	161.6	

32nd

171.45

47

2+00	171.59		
10E		11.7	159.8
E.L.		10.4	161.1
+4		8.5	163.0
cb		8.6	162.9
¼		8.9	162.6
+5		9.5	162.0
℄		6.2	165.3
¼		4.5	167.0
cb		3.6	167.9
+4		2.7	168.8
w.L.		1.5	170.0
2+25			
w.L		2.3	168.7
+4		2.8	168.7
cb		5.0	166.5
+5		5.4	166.1
¼		6.1	165.4
℄		8.6	162.9
+5		10.6	160.9
¼		10.6	160.9
+8		10.9	160.6
cb		10.6	160.9
+6		10.6	160.9
+8		12.3	159.2
E.L.		12.6	158.9
10E		14.0	157.5

171.45

2+50	171.59		
10E		16.3	155.2
E.L.		14.3	157.2
+4		12.3	159.2
eb		12.4	159.1
1/4		12.2	159.3
+4		12.0	159.5
+5		12.5	159.0
℄		10.0	161.5
1/4		7.6	163.9
eb		6.5	165.0
+1		6.2	165.3
+3		5.0	166.5
w.L.		3.7	167.8
2+75			
w.L.		5.8	165.7
+5		6.6	164.9
+9		8.1	163.4
eb		8.4	163.1
1/4		9.6	161.9
+5		10.0	161.5
+7		11.4	160.1
℄		11.7	159.8
+1		12.0	159.5
+3		13.9	157.6
+5		13.6	157.9

32 pl

171.45

2+75	171.59		
1/4		13.8	157.7
+8		14.3	157.2
eb		14.1	157.4
+5		14.0	157.5
+8		16.0	155.5
EL		16.5	155.0
10E		18.7	152.8
3+00 = N.L. Broadway			
10E		19.7	151.8
E.L.		17.6	153.9
+2		17.0	154.5
+5		15.6	155.9
eb		15.5	156.0
1/4		15.7	155.8
+6		15.7	155.8
℄		13.0	158.5
+2		12.1	159.4
1/4		11.3	160.2
eb		10.1	161.4
+3		9.9	161.6
+5		8.9	162.6
w.L.		7.8	163.7
T.P.	10.54	478.56	3.57	168.02
BM.	Beg.		1.19	~~177.37~~	~~177.38~~

Begin page 39 171.23

X sec Edgemont from C to B

60' wide 40' Rdway 10' cbs

see page 39

NE Edgemont
℄ C.
B.M. 11.88 cbs 2 walk in. 211.47 199.59

0+00 = NL. C st.

wcb		13.10	198.37
gut		13.0	198.5
+3		13.3	198.2
¼		12.5	198.9
±		12.2	199.3
¼		12.4	199.1
+4		12.2	199.3
gut		12.2	199.3
Ecb		11.95	199.52
0+20			
Ecb		9.91	201.56
gut		11.0	200.5
+7		10.8	200.7
¼		10.9	200.6
±		10.9	200.6
+5		10.9	200.6
¼		11.1	200.4
+7		11.9	199.6
gut		12.0	199.5
wcb		11.53	199.94

Plotted 5-20-29 T.W.

Edgemont

0+50

wcb		9.57	201.90
gut		10.0	201.5
+4		10.2	201.3
¼		9.4	202.1
±		9.0	202.5
¼		9.2	202.3
gut		8.9	202.6
Ecb		8.35	203.12
0+75			
Ecb		7.33	204.14
gut		8.0	203.5
¼		7.9	203.6
±		7.8	203.7
¼		8.2	203.3
+7		8.8	202.7
gut		8.5	203.0
wcb		8.49	202.98
1+00			
wcb		7.40	204.07
gut		7.7	203.8
+3		7.8	203.7
¼		7.3	204.2
±		6.7	204.8
+6		6.6	204.9
¼		6.8	204.7
gut		6.7	204.8

1+00	211.47 ~~211.62~~		
Ecb		6.26	205.21
1+25			
Ecb		5.38	206.09
q.t		5.9	205.6
¼		5.9	205.6
℄		5.7	205.8
¼		6.1	205.4
+8		6.7	204.8
q.t.		6.5	205.0
Wcb		6.31	205.16
1+51			
Wcb		5.12	206.35
q.t		5.3	206.2
+3		5.5	206.0
¼		5.1	206.4
℄		4.8	206.7
¼		5.0	206.5
q.t.		5.0	206.5
Ecb		4.39	207.08

Edgemont

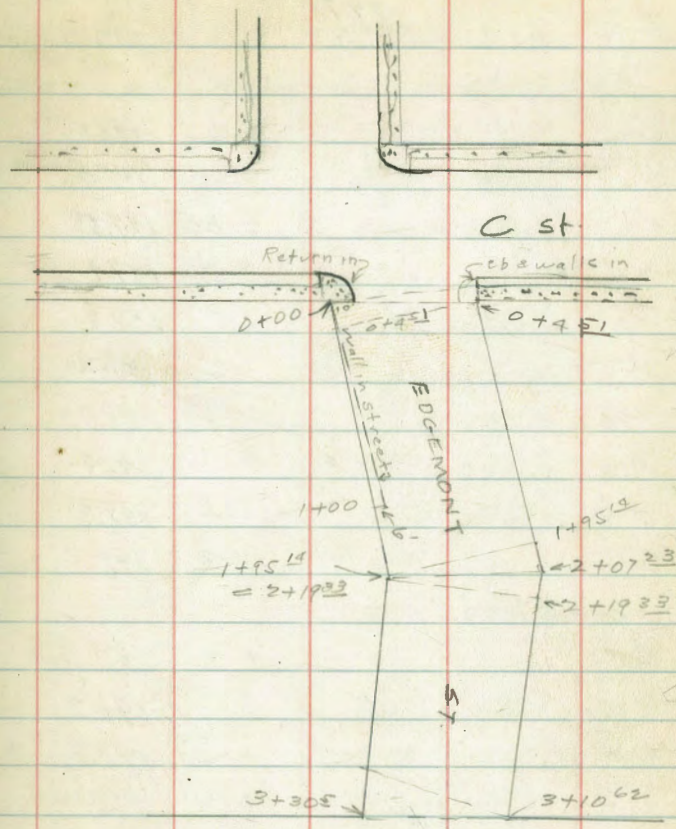
1+75	211.47		
Ecb		3.77	207.70
q.t		4.3	207.2
¼		4.3	207.2
℄		4.1	207.4
¼		4.4	207.1
q.t		4.6	206.9
Wcb		4.28	207.19
2+00			
Wcb		3.44	208.03
q.t		4.0	207.5
¼		3.7	207.8
℄		3.5	208.0
¼		3.6	207.9
q.t		3.6	207.9
Ecb		3.02	208.45
2+25			
Ecb		2.32	209.15
q.t		2.9	208.6
¼		2.9	208.6
℄		2.8	208.7
+5		2.8	208.7
¼		3.0	208.5
q.t		2.9	208.7
Wcb		2.73	208.74

2+50		211.47		
wcb			2.04	209.43
gut			2.1	209.4
¼			2.1	209.4
℄			2.0	209.5
¼			2.1	209.4
gut			2.0	209.5
Ecb			1.47	210.00
2+75				
Ecb			0.75	210.72
gut			1.4	210.1
¼			1.3	210.2
℄			1.3	210.2
¼			1.4	210.1
gut			1.8	209.7
wcb			1.51	209.96
3+00.5 = S.C. Bst				
wcb			0.97	210.50
gut	Paw		1.50	209.97
¼	✓		0.94	210.53
℄	✓		0.56	210.91
¼	✓		0.57	210.90
gut	✓		0.58	210.89
Ecb			0.00	211.47

Edgemont.

0.19

51



Broadway

2/27/29
London

X sec. Edgemont St from C – to Bdway.
60' st. 40' Rdway 10' ebs

199.78
199.59 office Record

B.M	0.19			
0+00 on west = 0+45 on East = St. C St.				
W.L.			1.8	198.0
eb	grd.		2.3	197.5
eb	to b.b		2.00	197.78
+4		5-30-29	2.4	197.4
¼		Plotted	1.9	197.9
℄			1.C	198.2
¼			1.4	198.4
eb			1.4	198.4
+6			1.5	198.3
E.L			1.3	198.5
0+45				
E.L.			1.3	198.5
+4			1.5	198.3
eb			1.5	198.3
¼			1.4	198.4
℄			1.8	198.0
¼			2.2	197.6
+7			2.9	196.9
eb			2.6	197.2
W.L			2.5	197.3

Edgemont

199.78

52

0+25			
W.C		3.8	196.0
+1	wall	3.9	195.9
+1½	bot wall	5.0	194.8
eb		5.3	194.5
+5		5.6	194.2
¼		5.2	194.6
℄		4.8	195.0
¼		4.8	195.0
+5		5.1	194.7
eb		4.5	195.3
+8		4.0	195.8
E.L		2.6	197.2
0+50			
E.L.		7.0	192.8
+3		7.9	191.9
eb		8.6	191.2
+4		8.9	190.8
¼		8.7	191.1
℄		8.5	191.2
¼		8.8	191.0
eb		8.4	191.6
+7	bot wall	7.3	192.5
+7	wall	5.4	194.4
W.L.		5.0	194.8

Edgemont

0 +75		~~199.78~~ ~~199.73~~		
w.l.			6.2	193.6
+8	wall.		7.0	192.8
+5	bot wall		10.9	188.9
eb			11.3	188.5
¼			12.0	187.8
℄			12.0	187.8
+7			11.9	187.9
¼			12.1	187.7
+8			12.1	187.7
eb			11.7	188.1
+7			10.8	189.0
E.L.			9.7	190.1
T.P.	0.03	186.91 ~~187.06~~	12.90	186.88 ~~187.03~~
1+00				
E.L.			0.9	186.0
eb			2.9	184.0
¼			3.6	184.3
℄			2.6	184.3
¼			2.5	184.4
+8			2.0	184.9
eb			2.2	184.7
+4	bot wall		1.4	185.5
+8			+5.0	191.9
w.l.			+5.2	192.1

Edgemont

5:3

1+25		~~186.91~~ ~~187.06~~		
w.l.			0.8	186.1
+8			5.4	181.5
eb			5.9	181.0
+5			6.2	180.7
+6			6.8	180.1
¼			6.8	180.1
℄			6.5	180.4
¼			6.3	180.6
+6			6.3	180.6
eb			6.3	180.6
+4			6.4	180.5
E.L.			4.0	182.9
1+50				
E.L.			7.3	179.6
+4			9.1	177.8
eb			9.6	177.3
+5			9.1	177.8
¼			9.0	177.9
+7			9.2	177.7
℄			9.7	177.2
+2			10.0	176.9
¼			9.9	177.0
+6			9.5	177.4
eb			9.3	177.6
w.l.			3.4	183.5

1+75		186.91 ~~187.06~~		
w.L.			5.1	181.8
+3			6.1	180.8
+8			12.2	174.7
eb			12.6	174.3
+6			12.3	174.6
¼			13.1	173.8
+6			13.0	173.9
℄			12.5	174.4
¼			12.0	174.9
eb			12.0	174.9
+5			11.9	175.0
E.L			10.4	176.5
1+95.14 = L on west				
E.L			12.4	174.5
+5			13.6	173.3
eb			14.0	172.9
T.P	0.61	175.64 ~~175.79~~	11.88	175.03 ~~175.18~~
¼			2.7	172.9
℄			3.8	171.8
+4			3.5	172.1
¼			3.4	172.2
+5			3.8	171.8
eb			3.2	172.4
+5			2.6	173.0
w.L			0.2	175.4

Edgemont

		175.64 ~~175.79~~		
1+95.14 = 2+07.23				
w.L			0.2	175.4
+6			3.3	172.3
eb			3.7	171.9
+3			4.5	171.1
¼			4.2	171.4
℄			4.7	170.9
+5			4.1	171.5
¼			3.8	171.8
eb			3.3	172.3
+8			2.9	172.7
E.L			2.0	173.6
2+19.33 = 1+95.14				
E.L			3.8	172.8
eb			4.4	171.2
+5			5.0	170.6
¼			4.9	170.7
+5			5.3	170.3
℄			5.4	170.2
+6			4.5	171.1
¼			4.4	171.2
+5			4.8	170.8
+8			3.9	171.7
eb			3.7	171.9
+3			3.5	172.1
w.L			0.2	175.4

2+50	175.64 ~~175.77~~		
W.L.		2.3	173.3
+7		6.7	168.7
cb		7.3	~~168~~.3
¼		7.6	168.0
+5		7.5	168.1
℄		7.9	167.7
+8		8.4	167.2
¼		8.2	167.4
+5		8.3	167.3
cb		7.6	168.0
E.L.		7.2	168.4
2+75			
E.L		9.6	166.0
cb		9.8	165.8
¼		10.4	165.2
℄		10.6	165.0
¼		10.4	165.2
cb		9.8	165.8
+5		9.5	166.1
W.L.		6.4	169.2

Edgemont

55

3+00	175.64		
W.L		11.5	164.1
cb		11.9	163.7
¼		12.5	163.1
℄		12.0	163.6
+5		12.1	163.5
+7		13.0	162.6
+9		12.6	163.2
¼		12.4	163.2
+7		12.5	163.1
cb		11.9	163.7
+5		11.6	164.0
+8		12.2	163.4
E.L		11.7	163.9
3+10 62 = W.L Broadway on East.			
E.L		13.5	162.1
+2		14.4	161.2
+6		13.4	162.2
cb		13.3	162.3
+5		16.4	159.2
¼		13.4	162.2
℄		13.3	162.3
¼		13.4	162.2
+5		13.4	162.2
cb		12.8	162.8
W.L		12.3	163.3

175.64

3+80.5 = 3+10.62 = N.L. Broadway		
N.L.	15.1	160.5
+5	16.2	159.4
cb	15.6	160.0
+8	17.4	158.2
¼	16.3	159.3
+5	15.3	160.3
℄	14.6	161.0
¼	14.3	161.3
+6	17.3	158.3
Cb	14.5	161.1
E.L.	13.5	162.1

½ sec 31st from C to B.
10' St. 5' cbs 30' Rdway.

56

	173.15 ~~173.30~~	171.96 ~~172.11~~
BM. 1.17		
3+00.2 = N.L. Cst.		
E.L.	9.8	1634
cb	9.4	1638
+4	8.7	1645
¼	9.7	1635
+5	8.8	1644
℄	8.7	1645
+4	9.2	1640
¼	6.5	1667
+5	3.7	1695
cb	3.1	1701
N.L.	2.9	1703
2+80		
N.L.	6.5	1667
cb	8.3	1649
+4	9.2	1640
¼	10.9	1623
+5	13.3	1599
℄	13.4	1598
¼	13.6	1596
cb	13.2	1600
E.L.	13.3	1599

Plotted 4-22-29 - GM Jam

2+63	173.15			
E.L		13.0	160	2
cb		12.8	160	4
1/4		12.9	160	3
+4		13.3	159	9
℄		12.9	160	3
1/4		12.1	161	1
cb		9.7	163	5
W.L.	173.2	8.6	164	6
2+43				
W.L.		4.6	168	6
cb		8.5	164	7
+6		12.3	160	9
1/4		12.3	160	9
℄		12.4	160	8
1/4		12.1	161	1
cb		12.5	160	7
E.L		12.3	160	9
2+14	✓			
E.L		10.9	162	3
cb		11.2	162	0
+4		11.2	162	0
+5		12.2	161	0
+6		12.2	161	0
1/4		11.0	162	2
℄		11.0	162	2

2+14	173.15			
1/4		11.0	162	2
+4		10.5	162	7
cb		6.2	167	0
+4	173.2	3.4	169	8
W.L.		3.2	170	0
1+89				
W.L.		2.5	170	7
+2		3.9	169	3
cb		9.4	163	8
1/4		9.5	163	7
℄		9.9	163	3
+3		11.7	161	5
+6		11.2	162	0
1/4		9.9	163	3
cb		9.9	163	3
E.L		10.0	163	2
1+63				
E.L		9.0	164	2
cb		9.0	164	2
1/4		8.8	164	4
+3		10.2	163	0
℄		10.4	162	8
1/4		10.6	162	6
cb		10.3	162	9
W.L.		3.8	169	4

1+39		31 ST		
	173.15			
W.L.		6.2	167.0	
+1	(173.2)	7.6	165.6	
+3		8.6	164.6	
cb		8.5	164.7	
+1		8.5	164.7	
+2		9.8	163.4	
+5		10.1	163.1	
+7		8.8	164.4	
1/4		8.5	164.7	
+5		9.3	163.9	
℄		8.6	164.6	
1/4		8.2	165.0	
cb		8.2	165.0	
EL		8.5	164.7	
1+21				
EL.		7.9	165.3	
cb		7.9	165.3	
1/4		8.0	165.2	
℄		7.9	165.3	
1/4		7.8	165.4	
+3		7.7	165.5	
Cb		9.4	164.8	
+2		9.3	163.9	
W.L		9.2	164.0	

1+12		31 ST		
	173.15 ~~173.30~~			
W.L		8.0	165.2	
cb		7.5	165.7	
1/4	(173.2)	7.5	165.7	
℄		7.3	165.9	
1/4		7.1	166.1	
cb		7.4	165.8	
EL.		6.9	166.3	
0+97				
EL.		1.6	171.6	
cb		5.2	168.0	
1/4		5.7	167.5	
℄		5.6	167.6	
1/4		5.8	167.4	
cb		5.1	168.1	
W.L		5.2	168.0	
TP 1232	182.99 ~~183.14~~	2.48	170.67 ~~170.82~~	
0+83				
W.L.	(183.0)	2.4	180.6	
cb		5.0	178.0	
1/4		8.8	174.2	
℄		12.8	170.2	
+2		13.8	169.2	
1/4		13.9	169.1	
cb		6.4	176.6	
+3		5.1	177.9	
+4		2.1	180.9	

		31st		
		182.99		
0+83		~~183.14~~		
E.L			0.8	182.2
0+69		(183.0)		
E.L			0.9	182.1
cb			3.8	179.2
+5			5.7	177.3
¼			8.6	174.4
+5			11.3	171.7
℄			9.1	173.9
¼			4.9	178.1
cb			0.0	183.0
w.L			+3.3	186.3
0+51				
w.L			+9.6	192.6
cb			+5.4	188.4
¼			1.4	181.6
℄			5.0	178.0
+4			5.2	177.8
¼			4.2	178.8
cb			1.0	182.0
E.L.		195.61	+2.2	185.2
T.P.	12.68	~~195.76~~	0.06	182.93 ~~189.08~~

		31st		
		195.61		
0+21		~~195.76~~		
E.L.			6.8	188.8
cb		(195.6)	6.3	189.3
¼			6.3	189.3
℄			5.2	190.4
¼			4.3	191.3
cb			4.2	191.4
w.L			2.5	193.1
T.P.	11.87	207.36 ~~207.51~~	0.12	195.49 ~~195.64~~
0+00 = S.L. B.S+				
w.L			3.7	203.7
cb			4.1	203.3
+5			3.4	204.0
¼			4.7	202.7
℄			3.7	203.7
¼			3.8	203.6
cb			4.7	202.7
E.L			3.5	203.9
0-4e back walls				
E.L		(207.36)	1.36	206.00
cb			1.52	205.84
¼			1.67	205.69
℄			1.70	205.66
¼			1.81	205.55
cb			1.95	205.41
w.L.			2.05	205.31

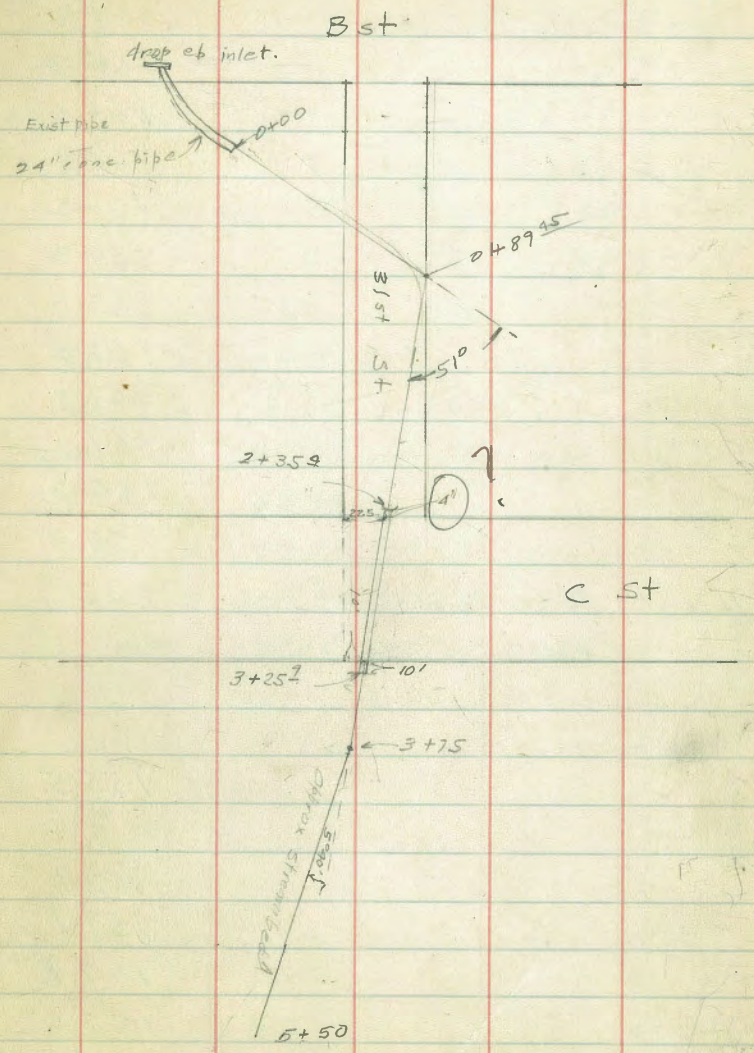
31st St

20136

~~20756~~

0 - 10 = Seb B St

W.L.	to Seb		2.25	205.11	
℄			1.92	205.44	
E.L.			1.60	205.76	10'
B.M.	N.W. 31st & B.		0.62	206.89	(206.74)
T.P	3.76	202.12	9.15	198.36	
			2.36	199.76	(199.74)
S.W. 30th & C.					
B.M	5.01	199.97		194.96	
S.E. 30c & Bdway					
B.M.			4.80	195.17	(195.08)



2/28/21 Profile for storm Drains on B & C
Lowden at 31st See P 60

B.M.	2.22	174.33		172.11
0+00	F.L. pipe		4.61	169.7
0+25			9.1	165.2
0+40			10.3	164.0
0+50			9.7	164.6
+75			9.4	164.9
0+89.45	L.		10.1	164.2
1+00			10.1	164.2
+25			11.0	163.3
+50			12.0	162.3
+65			12.4	161.9
+75			13.2	161.1
2+00			14.0	160.3
+25			14.9	159.4
2+35.4	F.L. 30" pipe		15.21	159.12
B.M.	6.58	178.69		172.11
T.P.	0.52	166.18	13.03	165.66
3+25.9	F.L. 30" pipe		9.43	156.75
+27			10.7	1555
T.P.	0.11	153.51	12.78	153.40
+37			1.4	1521
+50			2.4	1511
3+75	L.		5.7	1478
+93			5.7	1478
4+00			7.7	1458
+12			8.7	1448

			15357	
4+25			8.7	1448
+35			7.6	1459
+50			8.2	1453
+80			12.3	1412
5+00			12.9	1406
+25			14.2	1393
+50 end.			14.8	1387

Note change of Elev following (Elevations deductions)

	Lowden	office	This is high	use?
B.M. 30-C =	194.96,	194.96		194.81
" " Edgemont-C =	199.74	199.59	0.15	
" " 32-C =	177.38			
" " " - " =	177.92	177.78	0.14	
" " 31-B =	206.89	206.74	0.15	
" " 30. Broadway =	195.17	195.08	0.09	

3-12-29. Cross-section Alley - Block 188 -
J.C. Bliss City Heights - Between Wabash + Nile -
Drebert from Wightman to Landis - 20' wide -
Kaufner

O.K. office Records
-0.28 Low according to B.M.'s at Univ. + Nile + University + Boundary

B.M. N.E. B.P. at Boundary + Landis				329.04	
	+0.53	329.57		329.32	
		329.85			
			-11.78	318.07	
	+6.52			317.79	
		329.59			
		H.I. ~~324.31~~			
N.L. Landis = 0+00					
E			6.9	317.7	
℄			6.7	317.9	
W			6.4	318.2	
0+25					
W			5.8	318.8	
℄			6.0	318.6	
+5			5.9	318.7	
E			6.7	317.9	
0+50					
E			6.2	318.4	
℄			5.9	318.7	
W			5.6	319.0	
0+75					
W			5.6	319.0	
℄			5.9	318.7	
E			6.8	317.8	
1+00					
E			6.2	318.4	
+5			5.3	319.3	
℄			5.2	318.4	

3/25/29 T.H. Plotted

H.I. ~~324.31~~ 324.59

W	5.5	319.1
1+25		
W	5.4	319.2
℄	5.3	319.3
+6	5.4	319.2
E	6.6	318.0
1+50		
E	6.8	317.8
+5	5.7	318.9
℄	5.4	319.2
W	5.8	318.8
1+75		
W	5.4	319.2
℄	5.1	319.5
+5	5.7	318.9
E	6.7	317.9
1+93		
℄ 10' · Garage 1.5' Back E.L. · Concrete Floor	6.6	317.97
℄ 12' " 4' Back W.L. Dirt Floor	4.8	319.8
2+00		
E	6.2	~~318.4~~
+5	5.3	319.3
℄	5.3	319.3
W	5.4	319.2

H.I. ~~324.31~~ 324.59

2+25

W	5.5	319.1
℄	5.6	319.0
E	6.3	318.3

2+42

℄ 12' Concrete Garage Apron 2' Back W.L.	5.45	319.14

2+50

E	6.0	318.6
℄	5.7	318.9
W	5.4	319.2

2+75

W	5.6	319.0
℄	5.9	318.7
E	6.1	318.5

3+00

E	6.9	317.7
℄	6.3	318.3
W	5.9	318.7

T.P	-6.62	317.97 ~~317.69~~	
+3.91			

321.88
H.I. ~~321.60~~

3+07

℄ 11' Concrete Apron 5' Back W.L.	2.70	319.18

321.88
H.I. ~~321.60~~

3+24

℄ 2.5' Concrete Walk 45° in Alley from E.L.	4.18	317.70

3+25

W	3.6	318.3
℄	4.1	317.8
E	4.3	317.6

3+50

E	4.8	317.1
℄	4.3	317.6
W	3.8	318.1

3+75

W	4.5	317.4
℄	5.0	316.9
E	5.3	316.6

4+00

E	7.0	314.9
℄	6.3	315.6
++	5.3	316.6
W	4.7	317.2

4+19

Flowline M.H & Alley	17.85	304.03

4+25

W	7.3	314.6
+5	8.9	313.0
+8	11.9	310.0
℄	12.8	309.1

Note Ground breaks down very sharply from E.L. at stations 4+25 and 4+50

		H.I. ~~321.60~~ 321.88		
+6		13.2		308.7
E		15.1		306.8
T.P.			- 13.06	~~308.54~~ 308.82
	+1.51	H.I. ~~310.03~~ 310.33		
		4+50		
E		16.2	294.1	
℄		12.1	298.2	
W		4.8	305.5	
T.P			- 13.13	~~296.92~~ 297.20
	+3.19	H.I. ~~300.11~~ 300.39		
		4+64		
Flow MH & Alley		16.74	283.65	
		4+75 - Base South Bank Large Drain		
W		9.6	290.8	
℄		13.9	286.5	
E		12.3	288.1	
		5+00		
E		12.1	298.3	
℄		12.7	291.7	
W		12.4	288.0	
		5+25		
W		10.0	290.4	
℄		11.1	289.3	

		H.I. ~~300.11~~ 300.39		
E		11.1	289.3	
		5+26		
Flow Plane MH & Alley		18.10	282.29	
		5+50		
E		11.2	289.2	
℄		10.7	289.7	
W		10.3	290.1	
		5765 - Base North Bank Drain		
W		9.6	290.8	
℄		9.7	290.7	
E		8.9	291.5	
		5+75		
E		5.3	295.1	
℄		5.9	294.5	
W		7.0	293.4	
T.P.			-0.34	~~299.44~~ 300.00
	+11.87	H.I. ~~311.64~~ 311.92		
		6+00 = S.L. Wightman		
W		6.0	305.9	
℄		6.3	305.6	
E		7.0	304.9	
T.P.			-0.63	~~311.01~~ 311.29
	+10.94	~~321.95~~ 322.23		

H.I. ~~321.95~~ 322.23

T.P.		-1.29	320.94 320.66
	+2.91	323.91 323.63	
B.M. S.W. B.P. University & Nile		-1.76	322.15 321.87
		Correct	322.15

→ Check to B.M. N.W. B.P. at University & Boundary

B.M. S.W. B.P. University & N.l.c.			322.15
	+7.40	329.55	
T.P.		-2.58	326.97
	+9.90	336.87	
B.M. N.W. B.P. University & Boundary		-3.43	333.44 ✓
		Correct	333.44 ✓

at Office

3-13-29 J.C. Bliss Drebert Rohner

X-section Alley - Resub. by Frink 4 Wide of Block 101 - Between J & K - 31st & Westerly Termination toward 30th - 20' Wide

65

B.M. N.E.B.P. - 31st & K — 78.48 O.K.

33'

H.I. 81.80

W.L. 31st = 0+00

Plotted 4-2-29 - G.M. Tait.

S - Tp existing c.b.		45°	77.3
G		41	77.1
℄		52	76.6
G		47	77.1
N - Tp existing c.b.		46	77.1
	0+25		
N		5.8	76.0
℄		6.0	75.8
S		54	76.4
	0+50		
S		5.8	76.0
℄		6.4	75.4
N		6.0	75.8
	0+75		
N		6.9	74.9
℄		6.6	75.2
S		6.1	75.7

Note - From 0+25 to 0+75 on South side Fence & sheds 9.8' in Alley

0+92

& 12' Garage 4.5' Back S.L. Dirt Floor 5.6 76.2

H.I. 81.80

1400

S	6.5	75 3
℄	7.1	74 7
N	6.9	74 9

1425

N	7.2	74 6
℄	7.3	74 5
S	7.0	74 8

1450

S	7.4	74 4
℄	7.5	74 3
N	7.2	74 6

1467

℄ 16' Double Garage 0.7' in Alley from N.L. Concrete Floor 6.5 75.88

1475

N	7.3	74 5
℄	7.5	74 3
S	7.7	74 1

1490

T.P. -7.39 74 41

+4.75

H.I. 79.16

1490

℄ 18' Double Garage 3.6' Back N.L. - Dirt Floor 4.8 74 4

2+00

S	4.7	74 5

H.I. 79.16

℄	79.2	4.9	74 3
N		4.9	74 3

2+25

N	4.8	74 4
℄	4.8	74 4
S	4.5	74 7

2+50

S	4.6	74 6
℄	5.0	74 2
N	4.9	74 3

2+55

℄ 18' Garage at S.L. - Dirt Floor 4.8 74 4

2+75

N	4.9	74 3
℄	5.0	74 2
S	4.5	74 7

3+00

S	4.9	74 3
℄	4.9	74 3
N	4.7	74 5

3+10

℄ 14' Garage - 9' Back N.L. Concrete Floor 3.49 75 67

3+25

N	4.5	74 7
℄	5.0	74 2

H.I. 79.16

(79R)

S	4.6	74.6
3+50		
S	5.3	73.9
℄	4.9	74.3
N	4.6	74.6
3+75		
N	4.7	74.5
℄	5.3	73.9
S	5.1	74.1
3+91		
℄ 14' Garage - 2.8' Back N.L. - Dirt Floor	4.7	74.5
4+00		
S	5.3	73.9
℄	5.2	74.0
N	5.0	74.2
4+06		
Flow Line M.H. in ℄ Alley	7.80	71.36
4+25		
N	5.0	74.2
℄	5.2	74.0
S	5.2	74.0
4+45		
℄ 8' Garage - 0.5' Back SL - Dirt Floor	5.3	73.9
4+50		
S	5.4	73.8

H.I. 79.16

℄	5.5	73.7
N	5.4	73.8
4+75		
N	5.2	74.0
℄	5.4	73.8
S	5.1	74.1
4+76		
18" Eucalyptus Tree 2' in Alley from S.L.		
4+96		
24" Eucalyptus Tree 2' in Alley from S.L.		
4+95		
℄ 10' Garage at N.L. Dirt Floor	5.4	73.8
5+00		
S	5.1	74.1
℄	5.5	73.7
N	5.6	73.8
5+25		
N	5.6	73.6
℄	5.7	73.5
S	5.5	73.7
5+50		
S	5.8	73.4
℄	6.0	73.2
N	5.6	73.6

H.I. 79.16

5+55

℄ 8' Garage 3' Back S.L. - Dirt Floor 5.8 73.4

5+75

N	5.9	73.3
℄	6.3	72.9
S	5.8	73.4

5+93

℄ 12' Garage 3.5' Back S.L. - Dirt Floor	6.1	73.1
6+00 = Westerly Termination of Alley		
S	6.1	73.1
℄	6.1	73.1
N	6.0	73.2

T.P.	6.06	73.10
+4.61		

H.I. 77.71

Line of Levels for drain along West line Frink + Wilde Sub. of Block 101 from S.L. Alley to K St.

S.L. Alley = 0+00

0+00	4.8	72.9
0+25	4.7	73.0
0+50	4.8	72.9
0+75	4.8	72.9
1+00	5.1	72.6

H.I. 77.71

1+20	5.3	72.4
1+40 = N.L. K	5.6	72.1
1+44 = N cb K St	6.71	71.00
Gutter	7.33	70.38
B.M. N.W. B.P. 30th + K	-.480	72.91
	City Book Elev.	73.07
		O.K.
+ 2.92	75.83	
T.P.	= 2.21	73.62
+ 7.77	81.39	
B.M. N.E. B.P. 31st + K	- 2.88	78.51
	Correct	78.48
	Error	.03

6-25-29 X-section Alley Block 36
J. C. Bliss Ocean Beach - Between Ebers
Drebert + Sunset Cliffs - Santa Cruz to Del Monte
Rouner 20' Wide

B.M. S.E. B.P. Sunset Cliffs + Santa Cruz 54.23
+1.42 T 55.65

E. Gutter Sunset Cliffs

S	10.73	44.92
℄	11.23	44.42
N	11.72	43.93

E.L. Sunset Cliffs = 0+00 - Paved

N Top return	11.07	44.58
G	11.24	44.41
℄	10.93	44.72
G	10.48	45.17
S Top return	10.11	45.54
0+25		
S	11.2	44.5
℄	11.1	44.6
N	11.4	44.3
0+50		
N	10.6	45.1
℄	10.7	45.0
S	10.4	45.3
0+75		
S	9.7	46.0
℄	9.8	45.9
N	9.7	46.0

T 55.65

1+00

N	10.4	45.3
℄	8.7	47.0
S	8.6	47.1

1+07 = ℄ Garage with 8'x12' Concrete Apron at N.L.

West end Apron	8.29	47.36
East end apron	7.87	47.78
Floor Garage at ℄	7.81	47.84
1+25		
S	6.8	48.9
℄	7.2	48.5
N	7.1	48.6
1+40		
℄ 8' Garage 6' Back S.L. - Dirt Floor	4.9	50.8
1+45		
℄ 8' Garage 3' Back N.L. - Dirt Floor	5.5	50.2
T.P.		3.10 52.55

+11.32

T 63.87

1+50

N	12.7	51.2
℄	13.4	50.5
S	12.8	51.1
1+75		
S	10.7	53.2
℄	11.6	52.3

	T 63.87		
N	10 9	53.0	
	2+00		
N	8.8	55.1	
℄	9.1	54.8	
S	8.1	55.8	
	2+25		
S	6.0	57.9	
℄	6.8	57.1	
N	6.8	57.1	
	2+43		
℄ 8' Garage 3.5' Back S.L. - Dirt Floor	3.6	60.3	
	2+50		
N	4.9	59.0	
℄	4.8	59.1	
S	3.7	60.2	
	2+75		
S	1.9	62.0	
℄	2.2	61.7	
N	1.8	62.1	
T.P		-0.37 63.50	
	13.05		
	T 76.55		
	3+00		
Flow line M.H. ℄ Alley	18.83	57.72	
N	12.3	64.3	

	T 76.55		
℄	12.1	64.5	
+8	12.2	64.4	
S	10.5	66.1	
	3+25		
S	8.8	67.8	
℄	9.1	67.5	
+7	9.1	67.5	
N	9.9	66.7	
	3+45		
℄ 8' Garage 7' Back N.L. - Dirt Floor	7.4	69.2	
	3+50		
N	6.7	69.9	
+3	5.9	70.7	
℄	5.7	70.9	
S	5.4	71.2	
	3+75		
S	1.6	75.0	
℄	2.4	74.2	
+7	2.7	74.4	
N	4.3	72.3	
	3+78		
℄ 3' Brick Walk 2' Back S.L.	0.8°	75.8	
	3+90		
℄ 20' Double Garage - 5' Back S.L. - Dirt Floor - Nostent	0.5	76.1	
East end	0.0	76.6	

		π 76.55			
T.P.			0.00	76.55	
	+11.13				
		π 87.68 ✓			
		4+00			
N		17.5	75.2		
℄		10.9	76.8		
℄		11.1	76.6		
S		11.2	76.5		
		4+25			
S		10.5	77.2		
℄		10.1	77.6		
℄		10.1	77.6		
N		11.2	76.5		
		4+45			
℄ 8' Garage 1.5' Back N.L.		Dirt Floor 10.2	77.5		
		4+50			
N		9.6	78.1		
℄		9.5	78.2		
S		9.7	78.0		
		4+75			
S		9.0	78.7		
℄		9.2	78.5		
N		9.0	78.7		
		4+96			
℄ 12' Garage 0.5' Back S.L.		Dirt Floor 8.5	79.2		

		π 87.68			
		5+00			
N		8.3	79.4		
℄		8.6	79.1		
S		8.5	79.2		
		5+25			
S		7.4	80.3		
℄		7.7	80.0		
N		7.7	80.0		
		5+31			
℄ 8' Garage 9' Back S.L.		Dirt Floor 7.0	80.7		
		5+50			
N		6.4	81.3		
℄		6.2	81.5		
S		6.3	81.4		
		5+75			
S		4.7	83.0		
℄		4.9	82.8		
N		4.6	83.1		
		5+87			
N		4.1	83.6		
℄		4.6	83.1		
+7		4.2	83.5		
S		3.8	83.9		
		5+99 = W.L. Ebers - Paved			
S Top return		3.52	84.16		
G		4.26	83.40		

T 87.68

72

E			505	82.63	
N - Top return + Gutter Flush			528	82.40	
		W. Gutter Elevs			
N			590	81.78	
E			511	82.57	
S			444	83.24	
T.P.				-1290	7478
	+0.53	75.31			
				12.71	62.60
	+0.59	63.19			
				12.97	50.22
	0.16	50.38			
				13.26	37.12
				Correct	37.04
				Error	0.08

7-5-29 Levels + Location Otay Pipe

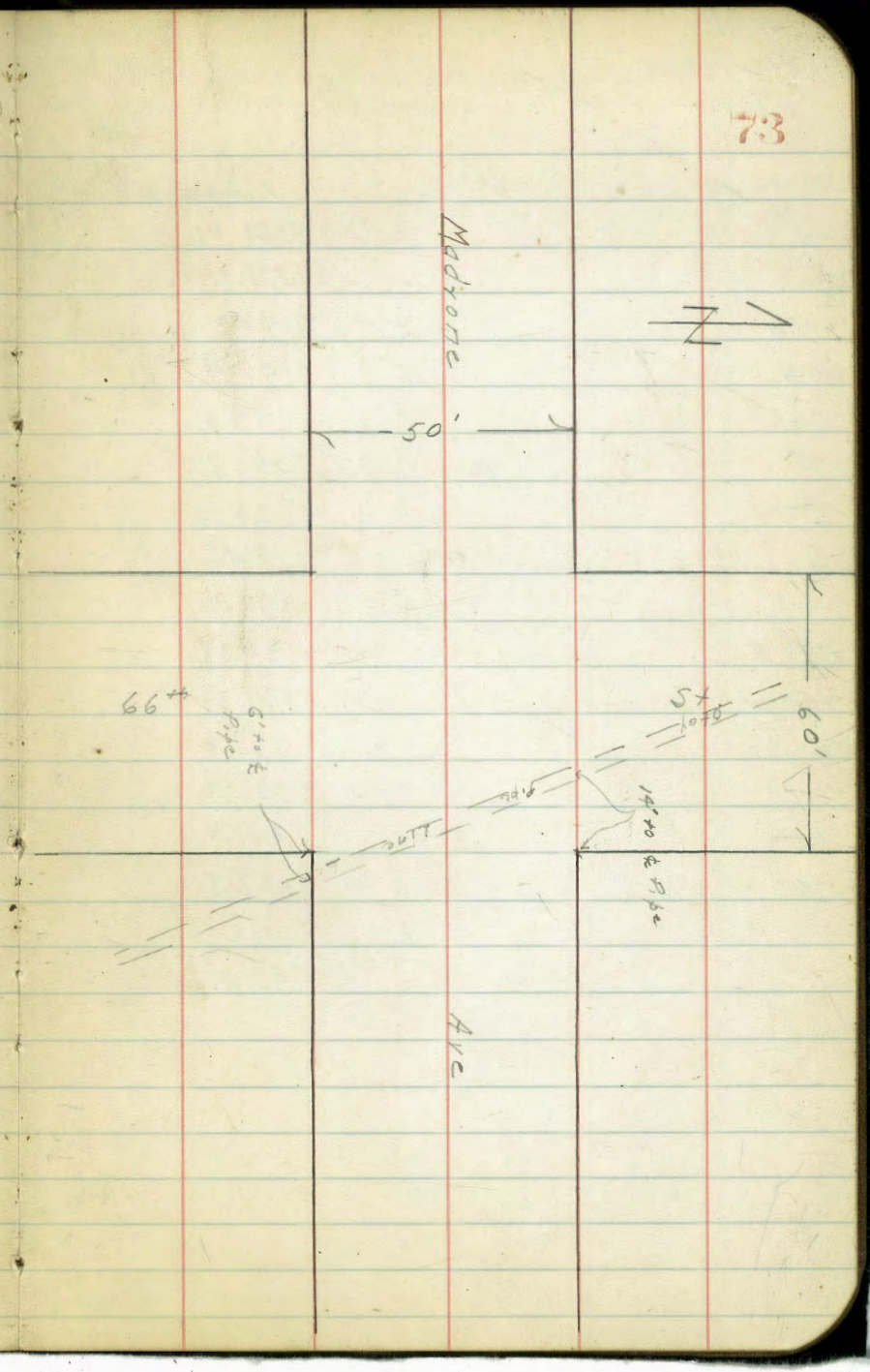
J.C. Bliss

Dr. Ebert Line at 66th + Madrone (Encanto)

Rounex

B.M. S.W. Spike in Pole 66th + Madrone		344.48
0.19	344.67	
	344.67	
Top pipe at S.E. Madrone	5.4	339.27
Top pipe at N.E. Madrone	10.1	334.57

Location - Sketch Next Page



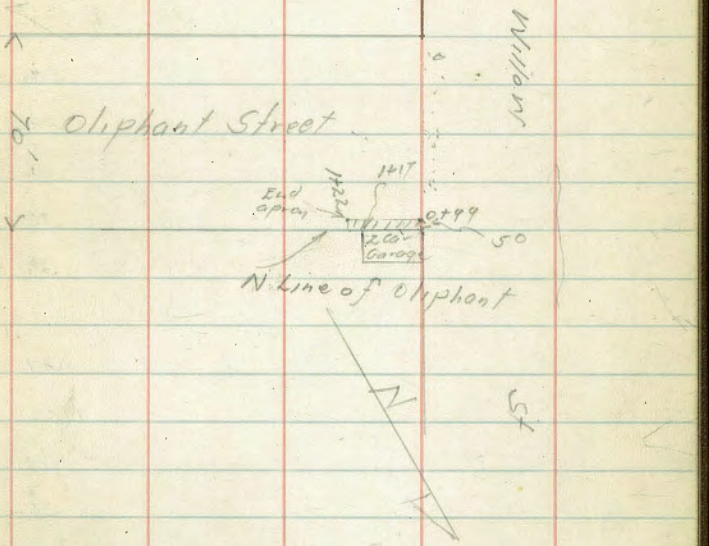
Bill Bliss
July 6 1929

Levels Along the ℄ of Oliphant from the E. Line of Willow 165' East

74

B.M. N.W. Bp	1.06	153.71		152.65
0+00 E. Line of Willow on paving			2.60	151.11
0+03			2.6	151.1
0+16			4.4	149.3
0+40			5.3	148.4
0+85			9.3	144.4
T.P.	1.98	142.86	12.83	140.88
0+87			3.3	139.6
0+99 W End 2 car Garage on N			3.92	139.44
1+05			4.5	138.4
1+17 E. End 2 Car Garage on N			3.99	139.37
1+22 11 " Apron concrete			3.55	139.31
1+28			5.0	137.9
1+38			5.0	137.9
1+50			11.5	131.4
1+65			15.4	127.5
check Mn. Hole to out # 155			9.13	138.73
				138.70
				0.03 error

Willow & Oliphant



8/12/39

Flood Reserve Remitter.

X section Alley Blk 200 C.H.

30' wide Ref - Map 1007
L Stakes 28092
24914

	+	-	+	Elev.
N.W.B.P.	1.62	368.28		366.66
T.P.	0.75	359.91	7.12	359.16
T.P.	1.72	351.45	12.18	349.73
T.P.	3.28	348.04	6.69	344.76

Section A See Sketch

E Top Cb.	5.89	342.15
E Gutter on paving	6.09	341.95
℄ on paving	6.60	341.44
W. ℄ on paving	6.33	341.71
W Top Cb.	6.19	341.85

Section B See Sketch

W. Top Cb.	6.19	341.85
W. on pvmt	6.33	341.71
℄ = Sta 0+00	6.3	341.7
℄ + 8.3 = on rear garage	5.6	342.4

℄ Sta 0+00 = ℄ Garage on E Concrete Floor & Floor

F.L. = Line of Garage	5.15 on Floor	342.89

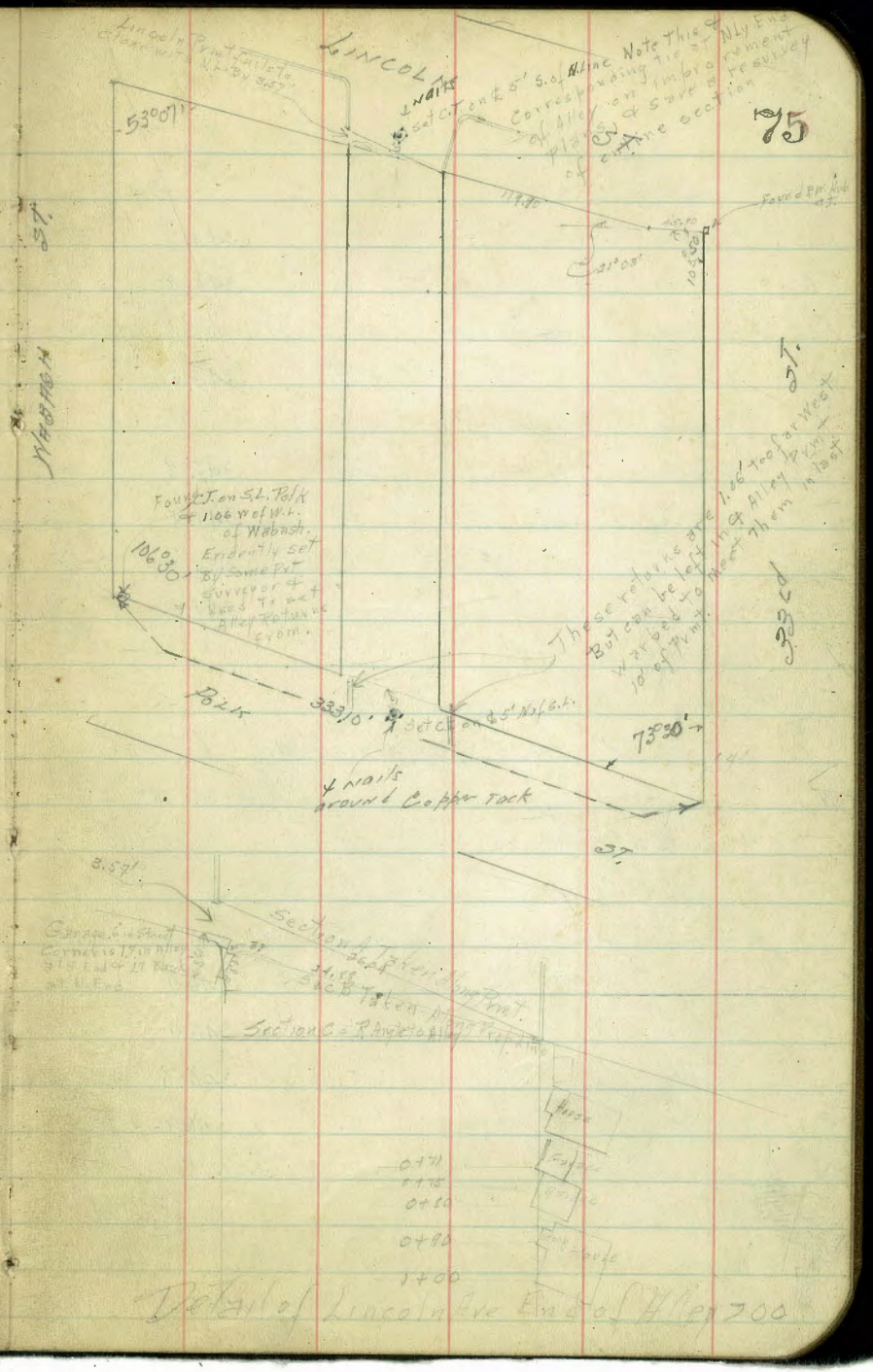
℄ Sta 0+07.1 = Sec. C"

E.L.	5.3	342.7
℄	3.1	342.9
W.L.	6.20	341.84

℄ Sta 0+14 = ℄ Garage on E 1.8' Back

E - 1.8	4.31	343.73
T.P.	7.14	351.89	3.99	344.75

Plotted 8-23-39 CBH



351.89

	+	A	−	Elev
	℄Sta 0+35			
W.L.			7.2	344.7
℄			7.5	344.4
℄+9.6 = Woven Wire Fence 30° Lane				
E.L.			7.4	344.5
	℄Sta 0+52			
E.L.			6.1	345.8
℄			6.4	345.5
W.L.			6.5	345.4
W.L − 4 ℄ Garage dirt floor			6.1	345.8
	℄Sta 0+71			
Nthly Corner of Above Garage, 1 in Alley				
	℄Sta 0+75 = ℄ Garage on W. dirt floor			
W.L = face of Garage			5.9 on floor	345.99 ✓
W	℄Sta 0+80 = Nthly Line of Above Garage		2.3 in Alley	✓
W	℄Sta 0+90 = Nthly Line of porch Frame Residence		0.3 in Alley	✓
E	℄Sta 0+94 = ℄ Garage on E. Cement floor & Apron			
W.L.			5.0	346.9
℄			5.0	346.9
E.L. =			5.1	346.8
E.L. + 0.4 = edge of Concrete Apron			5.0	346.9 ✓
E.L. + 4.8 = face of Garage			1.73	347.16 ✓ on cement floor
E	℄Sta 1+00 = Nthly Corner of House		0.20	in Alley ✓
E	℄Sta 1+06 = ℄ Garage on E Cement floor & Apron			✓
E.L. − 0.5			1.64	347.25 on Apron
E.L. − 5.0 = face of Garage			4.56	347.34 on floor

351.89

	+	T	−	Elev
E	℄Sta. 1+19 ℄ Garage on E 11.8 Back			✓
E.L.			4.4	347.5
℄			4.2	347.7
W.L. − 1.5 = S. End of board Shed			4.0	347.9
	℄Sta 1+65 N.S. Shed on W. 0.50 in Alley			✓
W.L. + 0.5			3.6	348.4
℄			3.5	348.4
E.L.			3.6	348.3
	℄Sta 2+00 ℄ Garage on W. 8.3 Back			✓
E.L.			3.0	348.9
℄			2.6	349.3
W.L.			2.8	349.1
T.P.	9.68	359.40	2.17	349.72
	℄Sta. 2+50			
W.L.			9.1	350.3
℄			8.8	350.6
E.L.			9.0	350.4
	℄Sta 3+00			
E.L.			6.8	352.6
℄			7.0	352.4
W.L.			7.5	351.9
	✓ ℄Sta 3+16 = ℄ Garage on W. dirt floor			
W.L − 5.9 = Face of Garage			5.9	353.5 on Floor
W.L.			5.8	353.6
℄			5.0	354.4

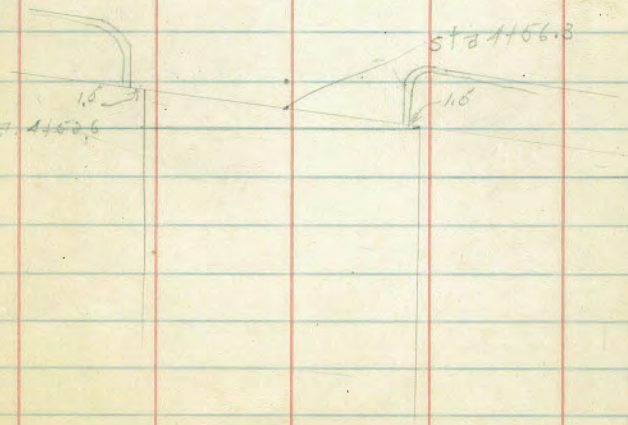
359.10

	+	T	−	Elev
E.L.			5.1	354.3
	℄ Sta 3+78 = St. Apartment on E. Double Garage on ground floor			
E.L. − 1.2			4.1	355.3
E.L.			4.3	355.1
℄			4.1	355.3
W.L.			5.1	354.3
	℄ Sta 3+80 = St. End of cement Apron on E.			
℄ + 9.2 = Edge of Apron			4.15	354.95
E.L.			4.33	355.07
E.L. + 3.1 = Face of Garage under Hob's			3.99	355.41
	℄ Sta 1+03 = N.L. of Hob's on E. & N.L. of Cement Apron			
E.L. − 1.8 = Face of Garage under Hob's			3.96	355.44
E.L. = Edge of cement Apron			4.36	355.04
	℄ Sta. 1+05			
W.L.			4.2	355.2
℄			4.2	355.2
E.L. = So. Corner Picket Fence on line			4.4	355.0
	℄ Sta. 1+30			
E.L.			4.1	355.3
℄			3.6	355.8
W.L.			3.5	355.9
	℄ Sta 1+52.6 = R.A. to Alley Where E.L. fence = Poles			
W.L.			3.7	355.5
℄			3.6	355.8

359.10

77

	+	T	−	Elev
℄ + 9.0 = Prmt			4.95	354.95
℄ + 9.0 Top Cb.			4.36	355.04
E.L.			4.3	355.1
	℄ Sta. 1+56.3 = St. Pole — Section Taken on △ See Sketch Below.			
Top E Cb.			4.36	355.04
E Prmt			4.95	354.95
℄ = Sta 1+56.3			4.63	354.77
W.L. on Prmt			4.61	354.79
W.L. + 1 = Top Cb.			4.44	354.96
T.P.	9.06	365.32	3.14	356.26
T.P.	6.86	368.78	2.40	362.92
			3.13	366.65 = 366.65 B.M.



Walker
Hendricks
Becker
Johnson
11-7-47

Check BMs. & Alley Elevations Blk 44. Between Vhinona & 50th.

	2.28	388.38			386.10
T.P.	5.86	385.13	2.11	379.27	
Chk E. cb 5+77.13	FB 1722 8		5.87	379.26	
				379.18	
				0.08	
Chk. W. Top cb 5+77.13	FB 1722-8		6.58	378.55	
				378.47	
				0.08	
	4+27 This Book				
Check from M.M.	FB 1293 6		8.21	376.92	
			P-6 →	376.86	
				0.06	
	5.69	391.79		386.10	
B.M. brass Plg gone					
Chk Ld Plg. SW	FB 1722 3		8.57	383.22	
				383.12	
				0.10	
		↑ Above 391.79			

Check Alley Block 43 P-9-A

6+32.69	Page 9 W Top cb		4.98	386.81	S.L. El Cajon
				386.85	
				0.04	
	P-9-A		4.81		
6+36.17	E. Top cb S.L. El Cajon			386.98	
			P-9-A =	386.98 ✓	

BM. SE Top Hydt. El Cajon - 50th

Alley Block 42

Check Alley Elevations on S.L. El Cajon

391.79

6+93.67	E Top cb	P-11		4.30	387.49 ✓
6+90.18	= W " "	P-11		4.27	387.52
					387.46
					0.06
T.P.	1.56	380.27		13.08	378.71
T.P.	0.02	367.00		13.29	366.98
T.P.	2.52	356.78		12.54	354.46
Check	N.M. B.P.	Estrella & El Cajon		5.17	351.61
					351.53 Record
					0.08 = Diff.

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1½ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

78.48
3.3
81.80
7.39
74.41
4.75
79.16
6.06
73.10

77.71
4.80
7291

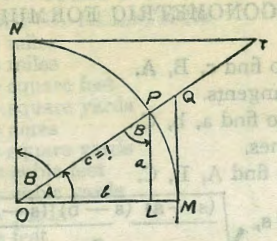


TABLE II

TRIGONOMETRIC FORMULÆ.

$\angle A = \angle MOP \quad \angle B = \angle PON = \angle OPL$

$R = OB = c = 1$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

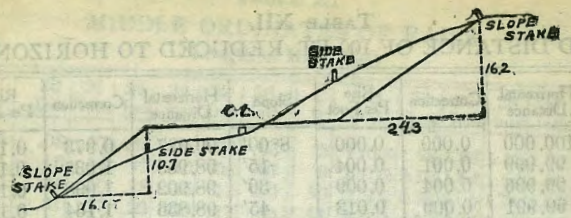
$$\sin \tfrac{1}{2} A = \sqrt{\frac{1 - \text{Cos } A}{2}} \qquad \cos \tfrac{1}{2} A = \sqrt{\frac{1 + \text{Cos } A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \qquad \cos 2A = \cos^2 A - \sin^2 A$$

Law of Sines $\dfrac{\sin A}{a} = \dfrac{\sin B}{B} = \dfrac{\sin C}{C}$

Law of Cosines $c^2 = a^2 + b^2 - 2ab \cos C$

Law of Tangents $\dfrac{a+b}{a-b} = \dfrac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1 65	1 80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3 45	3.60	3 75	3.90	4.05	4.20	4 35	2
3	4.50	4 65	4.80	4.95	5 10	5 25	5 40	5.55	5.70	5.85	3
4	6.00	6 15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7 50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9 00	9 15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10 65	10.80	10.95	11.10	11.25	11.40	11.55	11 70	11.85	7
8	12.00	12 15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13 50	13 65	13 80	13 95	14.10	14.25	14.40	14 55	14.70	14.85	9
10	15.00	15 15	15 30	15 45	15.60	15.75	15.90	16.05	16.20	16 35	10
11	16 50	16 65	16 80	16.95	17 10	17.25	17.40	17.55	17.70	17.85	11
12	18 00	18 15	18.30	18 45	18.60	18 75	18.90	19.05	19.20	19 35	12
13	19 50	19 65	19.80	19.95	20.10	20.25	20 40	20.55	20.70	20.85	13
14	21.00	21 15	21.30	21.45	21 60	21.75	21.90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24 15	24 30	24 45	24.60	24.75	24 90	25 05	25.20	25.35	16
17	25.50	25 65	25.80	25 95	26.10	26 25	26 40	26.55	26.70	26.85	17
18	27.00	27 15	27.30	27 45	27.60	27.75	27.90	28.05	28 20	28.35	18
19	28 50	28 65	28 80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30 00	30 15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31 50	31 65	31.80	31.95	32 10	32 25	32.40	32.55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33.60	33 75	33.90	34.05	34.20	34.35	22
23	34 50	34 65	34.80	34.95	35.10	35 25	35 40	35.55	35.70	35 85	23
24	36.00	36 15	36.30	36 45	36.60	36.75	36.90	37.05	37 20	37.35	24
25	37.50	37.65	37 80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39 00	39 15	39 30	39 45	39 60	39.75	39.90	40.05	40.20	40.35	26
27	40 50	40 65	40 80	40.95	41.10	41.25	41 40	41.55	41.70	41.85	27
28	42 00	42 15	42.30	42.45	42.60	42 75	42.90	43.05	43.20	43.35	28
29	43 50	43 65	43.80	43 95	44.10	44 25	44 40	44.55	44.70	44 85	29
30	45 00	45 15	45.30	45 45	45.60	45.75	45 90	46.05	46 20	46.35	30
31	46.50	46.65	46.80	46 95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48 00	48.15	48.30	48 45	48.60	48 75	48.90	49.05	49 20	49.35	32
33	49.50	49 65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51 00	51.15	51.30	51.45	51.60	51.75	51 90	52.05	52.20	52.35	34
35	52 50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54 00	54 15	54 30	54 45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55 50	55 65	55.80	55 95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57 30	57 45	57.60	57 75	57.90	58.05	58.20	58 35	38
39	58 50	58.65	58 80	58 95	59.10	59 25	59.40	59 55	59.70	59.85	39
40	60 00	60 15	60 30	60 45	60 60	60.75	60 90	61.05	61 20	61.35	40
41	61.50	61 65	61 80	61 95	62 10	62 25	62.40	62 55	62 70	62.85	41
42	63 00	63.15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64.35	42
43	64.50	64 65	64 80	64.95	65.10	65 25	65 40	65.55	65.70	65.85	43
44	66 00	66 15	66 30	66.45	66.60	66 75	66.90	67.05	67.20	67.35	44
45	67 50	67 65	67 80	67 95	68.10	68.25	68 40	68.55	68.70	68.85	45
46	69 00	69 15	69 30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70 50	70 65	70 80	70 95	71.10	71.25	71 40	71.55	71.70	71.85	47
48	72.00	72 15	72.30	72.45	72.60	72.75	72.90	73 05	73.20	73 35	48
49	73 50	73 65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75 15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.

B.M. N.E.B.P. Boundary & Landis

329.04
+ 3.88
334.92
- 7.74
22768
+ 3.37
330.55
- 4.02
326.53
+10.09
336.62
3.43
333.19 - B.M. University & Boundary

336.6
-9.90
326.72
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130° 11'

3423 | 199.86.00
171 15
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130° 11' 30"
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22 98 .58

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583.58
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467264
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52 52 22
17 50 74
40 85 06
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101.48 456 2

266.20
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179° 60'
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5 59 07

3423

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1149.28

1739 | 1,99.8600
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1.5 6 5 1
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1391

5387.05
16.05
3481.0
15
333.10
128.06
135.04

20.07
196.06
2488
119
48
386.91