

1295



UNIVERSITY BOOK

1295

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CITY OF SAN DIEGO,
CALIFORNIA.

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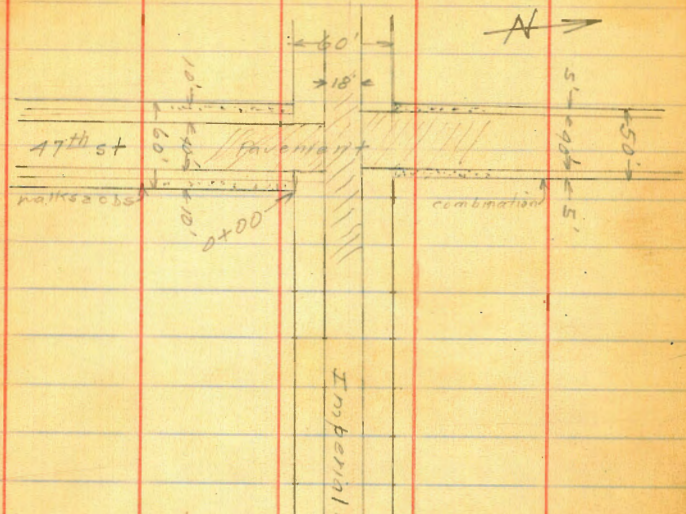
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DEC 22 1964

Imperial Ave from 47th East Page 2

" " " 54th " " 35



X sec. Imperial - 47th
60' St 10' on 47th

new bot.
Pole bolt
40th
Imperial

119.70

2

B.M.	1.34	149.67	148.33
T.P.	0.54	141.75	8.46 141.21
T.P.	0.24	129.04	12.95 128.80
T.P.	2.64	119.70	11.98 117.06
0-60 = ml	47th		
NL	walk	7.66	112.0
cb		8.0	
+3		8.1	
+6		8.9	
1/4		8.82	
+1	N Pav	8.72	110.98
±		8.65	111.05
+9	S Pav	8.76	110.94
1/4		8.7	
+2		8.7	
+5		8.8	
+6		8.5	
cb		8.3	
+2		7.8	
+5		7.5	
SL		7.2	112.5

B.M. Not ck to No. Record.

0-55 = web line 47th on North

SL	walk	7.17	112.5
+4		7.7	
+9		7.8	
cb		8.1	
+3		8.4	
+5		8.7	
+8		8.5	
1/4		8.5	
+1	S Pav	8.57	111.13
±		8.48	111.22
1/4	Pav	8.52	111.18
cb	✓	8.40	111.30
NL	✓	8.44	111.26
NL	Top cb	7.74	111.96
0-50 = web line 47th on South			
NL	Pav	8.29	111.61
cb	✓	8.25	111.45
1/4	✓	8.42	111.28
±	✓	8.36	111.34
1/4	✓	8.46	111.24
cb	✓	8.52	111.18
SL	✓	8.28	111.42
SL	Top cb	7.31	112.39

119.70

0-35 = Φ 47th on North.

SL	Par	8.11	111.59
+6	✓	8.32	
cb	✓	8.19	111.51
1/4	✓	7.92	111.73
Φ	✓	7.90	111.80
1/4	✓	7.94	111.76
cb	✓	7.95	111.75
NL	✓	8.09	111.61

0-30 = Φ 47th on South.

NL	Par	8.21	111.69
cb	✓	7.80	111.90
1/4	✓	7.77	111.93
Φ	✓	7.74	111.96
1/4	✓	7.82	111.88
cb	✓	8.12	111.58
+5	✓	8.27	
SL	✓	8.15	111.55

119.70

3

0-15 = Ecb line 47th on North

SL	Par	8.06	111.64
+3	✓	8.15	
cb	✓	7.87	111.83
1/4	✓	7.44	112.26
Φ	✓	7.26	112.44
1/4	✓	7.25	112.45
cb	✓	7.55	112.15
NL	✓	7.99	111.71
NL	Topcb	7.68	112.02

0-10 = Ecb line 47th on South = EL 47th North

NL		7.4	112.3
cb		7.2	
+5		7.0	
1/4		7.1	112.60
+0.5	N Par	7.18	112.52
Φ	✓	7.18	112.52
1/4	Par	7.36	112.34
cb	✓	7.88	111.82
+5	✓	8.10	
SL	✓	8.12	111.58
SL	Topcb	7.62	112.08

11970

0+00 = EL 47th on south

S.L.	6.8	112.9
cb	7.0	
1/4	7.1	
+15 ^S Pav	6.99	112.73
+	6.86	112.84
+9 ^S N Pav	6.93	112.77
1/4	6.9	
+3	6.7	
cb	7.0	
N.L.	7.1	112.6
0+0.5		
N.L.	6.9	112.8
cb	6.9	
+6	6.6	
1/4	6.8	
+0 ^S N Pav	6.77	112.98
+	6.70	113.00
+8 ^S S Pav	6.80	112.90
1/4	6.8	
cb	6.7	
+5	6.5	
+9	5.6	
S.L.	5.6	114.1

11970

4

0+30

S.L.	5.6	114.1
+3	5.9	
cb	5.9	
1/4	6.1	
+15 ^S S Pav	6.05	113.65
+	5.96	113.74
+9 ^S N Pav	6.05	113.65
1/4	6.1	
+6	5.8	
cb	5.7	
N.L.	5.8	113.9
0+60		
N.L.	5.1	114.6
+3	5.2	
+7	5.0	
cb	5.1	
+4	5.5	
1/4	5.2	
+0 ^S N Pav	5.15	114.55
+	5.25	114.65
+8 ^S S Pav	5.13	114.57
1/4	5.2	
+9	5.1	
cb	5.2	
S.L.	5.3	114.7

119.70

0 + 90

SL	4.7	115.0
+5	4.8	
cb	4.7	
1/4	4.2	
+15 s Pav	4.18	115.52
±	4.11	115.59
+95 N Pav	4.20	115.50
1/4	4.2	
+4	4.3	
+6	4.8	
cb	4.3	
NL	4.3	115.4
1+20		
NL	3.7	116.0
cb	3.6	
+7	3.6	
1/4	3.3	
+105 N Pav	3.28	116.42
±	3.15	116.55
+85 s Pav	3.23	116.47
1/4	3.3	
+6	3.9	
cb	3.8	
SL	4.6	115.1

119.70

1+32¹⁵ = m.L. Alloy

5

SL	4.1	115.6
cb	3.6	
+4	3.5	
1/4	3.0	
+15 s Pav	2.86	116.84
±	2.78	116.92
+95 N Pav	2.88	116.82
1/4	3.0	
+3	3.4	
+6	3.3	
cb	3.4	
NL	3.2	116.50
1+47 ¹⁵ = E.L. Alloy		
NL	2.1	117.6
+3	2.0	
cb	2.3	
+6	2.9	
1/4	2.5	
+105 N Pav	2.42	117.28
±	2.34	117.36
+85 s Pav	2.43	117.27
1/4	2.6	
+7	3.2	
cb	3.1	
+3	3.1	
+8	3.5	

119.70

1+47¹⁵

SL 3.3 116.4

1+80

SL 3.0 116.7

eb 2.1

+6 1.5

1/4 1.4

+1⁵ SPav 1.28 118.42

4 1.17 118.53

+9⁵ N Pav 1.25 118.45

1/4 1.3

+4 1.9

cb 1.3

NL 1.1 118.6

2+10 = mL Manzanilla? st.?

NL 0.1 119.6

+8 0.5

eb 0.6

+2 0.7

+6 0.1

1/4 0.0

+0⁵ N Pav 0.06 119.64

4 0.00 119.7

+8⁵ 0.05 119.65

1/4 0.2

+5 0.3

+8 0.8

6

2+10 119.70

eb 0.6

SL 1.5 118.2

T.P. 1179 131.09 0.35 119.35

2+40

SL 11.5 119.6

+2 11.5

+3 11.0

+6 10.8

eb 10.6

+5 10.3

1/4 10.3

+1⁵ SPav 10.16 120.93

4 10.11 120.98

+9⁵ N Pav 10.21 120.88

1/4 10.2

+4 10.2

+6 10.8

eb 10.6

NL 10.2 120.9

SPK Pole # 7007
B.M. SE 1/4 3. Escucha. 7.14 123.95

13109

2+67

N.L.	6.2	124.9
eb	7.2	
+3	7.7	
+6	9.2	
1/4	8.9	
+0 ^S N Pav	8.86	122.23
±	8.84	122.25
+8 ^S S Pav	8.94	122.15
1/4	9.1	
+5	9.2	
eb	9.5	
S.L.	10.6	120.5
2+79 ³⁰ = v.L. Escuela St.		
S.L.	10.0	121.4
cb	8.6	
1/4	8.3	
+1 ^S S Pav	8.34	122.77
±	8.22	122.87
+9 ^S N Pav	8.28	122.81
1/4	8.3	
+3	8.2	
+7	8.4	
+8	6.9	
eb	6.5	
N.L.	5.3	125.8

13109

2+88

N.L.	4.5	126.6
cb	5.5	
+2	6.1	
+4	7.6	
+7	7.6	
1/4	7.9	
+0 ^S N Pav	7.83	123.26
±	7.80	123.29
+8 ^S S Pav	7.88	124.21
1/4	7.8	
+3	7.8	
+8	8.5	
eb	8.5	
S.L.	8.6	122.5
3+09 ³⁰ = ± Escuela.		
S.L.	7.9	123.2
cb	7.2	
+5	6.9	
1/4	6.8	
+1 ^S S Pav	6.82	124.27
±	6.76	124.33
+9 ^S N Pav	6.82	124.27
1/4	6.8	
+3	6.7	
+6	5.9	
cb	4.8	

131.09

2	3+09 ³⁰		
NL		3.6	127.5
	3+21		
NL		3.6	127.5
cb		5.0	
1/4		6.1	
+0 ⁵	N Pav	6.26	124.83
+	+	6.16	124.93
+8 ⁵	S Pav	6.22	124.87
1/4		6.2	
+3		6.3	
+8		6.8	
cb		7.4	
2	S.L.	7.4	123.7
3	3+39 ³⁰ = E.L. Escudo sl.		
cb	S.L.	6.0	125.1
+	cb	5.7	
+	+5	6.3	
+	+7	5.7	
+	1/4	5.5	
+	+1 ⁵ S Pav	5.43	125.66
+	+	5.34	125.75
+	+9 ⁵ N Pav	5.42	125.67
+	1/4	5.4	
+	+7	4.9	
NL	cb	4.2	
	NL	3.0	128.1

131.09

8

3+60			
NL		2.2	128.9
cb		2.9	
+4		3.6	
+5		4.4	
+6		4.8	
1/4		4.4	
+0 ⁵	N Pav	4.30	126.79
+	+	4.30	126.79
+8 ⁵	S Pav	4.42	126.67
1/4		4.5	
+3		4.6	
+4		5.1	
+6		4.8	
cb		4.6	
+6		4.9	
S.L.		4.6	126.5
3+90			
S.L.		2.9	128.2
+5		2.9	
cb		3.3	
1/4		3.2	
+1 ⁵	S Pav	3.17	128.92
+	+	3.03	128.06
+9 ⁵	N Pav	3.03	128.06
1/4		3.1	

131.09

3790

+4	3.5	
+5	2.2	
+9	+0.2	
cb	+0.2	
+7	+0.4	
+2	+0.7	
+8	+0.7	
NL	+1.3	132.4

4+20

NL	+3.5	134.6
+6	+3.5	
cb	+3.8	
+4	+2.3	
+6	1.6	
1/4	1.7	
+0.5	1.73	129.96
+	1.70	129.39
+8.5	1.82	129.27
1/4	1.9	
+6	2.3	
cb	2.0	
S.L.	1.6	129.5

9

4+50

131.09

S.L.	0.6	130.5		
+5	0.5			
cb	0.7			
1/4	0.5			
+1.5	SPav	0.52	130.57	
+		0.45	130.64	
+9.5	N Pav	0.52	130.57	
1/4		0.6		
+4		0.7		
+5		+0.7		
+8		+3.4		
cb		+4.7		
+2		+5.3		
N.L.		+6.0	137.1	
9.5 box at	+6.5	5.6 + 6		
TP	12.72	143.78	0.03	131.06
+6	30 = w.L	Ally		
NL		5.9	137.9	
+8		6.4		
cb		7.8		
+2		8.0		
+3		10.2		
+5		12.8		
1/4		12.6		
+0.5		12.55	131.23	
+		12.49	131.29	
+8.5		12.62	131.16	

143.78

4+6430

cb	12.7	
S.L.	12.6	131.2
A+79 ³⁰ = EL. Alley		
S.L.	12.1	131.7
cb	12.0	
1/4	12.0	
+1 ⁵ SPav	12.05	131.73
+	11.94	131.86
+9 ⁵ NPav	11.92	131.86
1/4	12.0	
+5	12.1	
+8	8.9	
cb	6.9	
+4	5.4	
N.L.	5.3	138.5
5+10		
N.L.	4.4	139.4
+6	4.8	
+9	6.5	
cb	7.2	
+1	8.7	
+6	11.2	
1/4	10.7	
+0 ⁵ NPav	10.77	132.99
+	10.73	133.05
+8 ⁵ SPav	10.84	132.94

143.78

10

5+10

1/4	10.9	
+5	11.0	
cb	11.2	
S.L.	11.2	132.6
5+40		
S.L.	10.1	133.7
cb	10.0	
1/4	9.7	
+1 ⁵ SPav	9.59	134.19
+	9.49	134.29
+9 ⁵ NPav	9.55	134.23
1/4	9.6	
+5	9.7	
+6	8.6	
cb	6.6	
+4	5.4	
N.L.	4.4	139.4
5+70		
N.L.	4.4	139.4
+1	4.8	
+6	5.3	
cb	6.5	
+4	8.5	
1/4	8.4	
+0 ⁵ NPav	8.35	135.43
+	8.29	135.49

143.78

5+70		
+85 S Pav	8.42	135.36
1/4	8.5	
+5	8.8	
eb	9.0	
+5	9.0	
S.L.	9.3	134.5
6+09 ³⁰ - NL street.		
S.L.	8.0	135.8
eb	7.6	
1/4	7.2	
+15 S Pav	7.13	136.65
+	6.98	136.80
+95 N Pav	7.06	136.72
1/4	7.1	
+5	7.3	
+8	6.2	
eb	5.5	
+1	5.4	
+2	4.8	
+6	4.3	
NL	4.2	139.6

143.78

11

6+34 ³⁰ = 1/4 street.		
NL	5.3	138.5
+5	6.1	
eb	6.3	
1/4	6.1	
+05 N Pav	6.02	137.76
+	5.96	137.82
+85 S Pav	6.06	137.72
1/4	6.2	
eb	6.8	
S.L.	7.2	136.6
6+64 ³⁰ = E.L. street.		
S.L.	6.4	137.4
eb	5.8	
+4	5.8	
1/4	5.2	
+15 S Pav	4.96	138.82
+	4.87	138.91
+95 N Pav	4.94	138.84
1/4	5.0	
+5	5.3	
+7	4.8	
eb	4.8	
NL	4.8	139.0

143.78

6+90

N.L.	4.6	139.2
cb	4.5	
+3	4.8	
+5	4.4	
1/4	4.2	
+0 ⁵ N Pav	4.09	139.69
+	4.03	139.75
+18 ⁵ S Pav	4.16	139.62
1/4	4.4	
+6	5.1	
cb	4.9	
+6	4.7	
S.L.	4.9	138.9
7+10		
S.L.	4.3	139.5
cb	4.6	
1/4	3.7	
+1 ⁵ S Pav	3.47	140.31
+	3.31	140.47
+9 ⁵ N Pav	3.39	140.39
1/4	3.5	
cb	4.5	
N.L.	4.5	139.3

143.78

12

7+39

N.L.	3.7	140.8
+5	3.8	
cb	3.3	
+5	3.1	
1/4	2.7	
+0 ⁵ N Pav	2.53	141.25
+	2.45	141.33
+18 ⁵ S Pav	2.54	141.24
1/4	2.7	
cb	3.5	
+3	3.1	
+8	0.2	
S.L.	+0.1	143.9
7+04		
S.L.	0.3	143.5
+3	0.5	
+8	2.5	
cb	2.6	
1/4	2.0	
+1 ⁵ S Pav	1.83	141.95
+	1.76	142.02
+9 ⁵ N Pav	1.81	141.97
1/4	1.9	
+6	2.4	
cb	2.0	
+6	3.0	

7764	14378		
N.L.		3.3	140.5
7780			
N.L.		2.2	141.6
49		0.8	
cb		1.0	
+2		1.8	
1A		1.5	
+0 ^S N Pav		1.47	142.31
±		1.39	142.39
+8 ^S		1.45	142.33
1A		1.7	
+4		2.2	
cb		2.4	
+4		2.2	
+7		10.8	
SL		1.0	144.8
T.P. 8.11	15048	1.41	142.37
8704			
SL		5.5	145.0
+3		5.7	
+6		8.5	
cb		8.4	
+6		8.4	
1A		7.9	
+1 ^S		7.80	142.60
±		7.77	142.71

8704	15048		
+9 ^S		7.80	142.68
1A		7.7	
+5		8.1	
+7		7.8	
cb		6.0	
N.L.		5.4	145.1
8+1A			
N.L.		5.4	145.1
cb		5.5	
+3		7.8	
1A		7.7	
+0 ^S N Pav		7.66	142.82
±		7.60	142.88
+8 ^S S Pav		7.69	142.79
1A		7.8	
+5		8.2	
cb		8.2	
+3		8.2	
+6		6.3	
SL		5.9	144.6

150.48

8+25		
S.L	6.0	144.5
+5	6.4	144.1
+6	8.0	142.5
cb	8.0	142.5
'A	7.7	142.8
+15 S Pav	7.57	142.91
±	7.50	142.98
+9 ^S N Pav	7.57	142.91
'A	7.6	
+6	7.8	
+7	7.7	
cb	6.5	
N.L.	6.5	144.0
8+55		
N.L.	4.7	145.8
+2	4.2	
+5	4.0	
+8	4.7	
cb	5.9	
+2	7.2	
'A	7.4	
+0 ^S N Pav	7.30	143.14
±	7.23	143.25
+8 ^S S Pav	7.26	143.22
'A	7.3	

150.48

14

6+55		
+5	7.5	
+8	7.4	
cb	7.6	
+ 4	7.7	
+6	6.9	
+6	5.7	
S.L.	5.7	144.8
8+70		
S.L.	5.7	144.6
+3	5.8	
+5	7.3	
cb	7.6	
'A	7.3	
+15 S Pav	7.17	143.31
±	7.12	143.36
+9 ^S N Pav	7.18	143.30
'A	7.3	
+8	7.4	
cb	6.8	
+2	5.7	
+9	6.1	
N.L.	6.5	144.0

150.48

9+00		
N.L.	7.1	143.4
+8	6.4	
cb	7.1	
+2	7.0	
1/4	7.1	
+0 ^S N Pav	7.13	143.35
±	7.09	143.39
+8 ^S S Pav	7.20	143.28
1/4	7.3	
cb	7.9	
+4	8.0	
S.L.	7.4	143.1
9+29		
S.L.	8.0	142.5
+2	8.4	
T6	8.5	
cb	8.1	
1/4	7.3	
+1 ^S S Pav	7.10	143.38
±	6.99	143.49
+9 ^S N Pav	7.03	143.45
1/4	7.1	
T6	7.2	
cb	7.7	
+5	8.1	
N.L.	7.9	142.6

150.48

15

9+59		
N.L.	8.3	142.2
+8	8.2	
cb	7.6	
+2	7.3	
1/4	6.9	
+0 ^S N Pav	6.92	143.56
±	6.83	143.65
+8 ^S S Pav	6.93	143.55
1/4	7.1	
+5	7.8	
cb	7.9	
+5	8.1	
S.L.	9.2	141.3
9+89		
S.L.	8.3	142.2
cb	7.7	
1/4	7.1	
+1 ^S S Pav	6.89	143.59
±	6.78	143.70
+9 ^S N Pav	6.84	143.64
1/4	6.9	
+7	7.3	
cb	8.4	
+6	8.5	
N.L.	7.9	142.6

150.48

10+06 = cutvert 12" conc Pipe

N.L.		8.3	142.2
+9 ⁵	FL Culvert	9.20	141.28
cb		7.6	
1/4		6.8	
+0 ⁵	N Pav	6.77	143.71
±		6.71	143.77
+8 ⁵	S Pav	6.82	143.66
1/4		7.1	
+5		7.6	
+8		7.6	
cb		8.0	
+5	FL Culvert	9.60	140.88
S.L.		9.2	141.3
10+20			
S.L.		8.9	141.6
+5		7.7	
cb		7.5	
+5		7.5	
1/4		6.9	
+1 ⁵	S Pav	6.73	143.75
±		6.66	143.82
+9 ⁵	N Pav	6.74	143.74
1/4		6.8	
cb		7.5	
+5		7.8	
N.L.		7.7	142.8

150.48

16

10+50

N.L.		6.2	144.3
+5		6.8	
+8		7.3	
cb		7.1	
+5		6.6	
1/4		6.6	
+1	N Pav	6.56	143.92
±		6.49	143.99
+9	S Pav	6.59	143.89
1/4		6.7	
+5		7.2	
+9		7.4	
cb		7.2	
+5		7.5	
S.L.		7.8	142.7
10+80			
S.L.		7.3	143.2
cb		6.9	
+4		6.9	
1/4		6.3	
+1	S Pav	6.26	144.22
±		6.18	144.30
+9	N Pav	6.28	144.20
1/4		6.3	
+6		6.4	

150.48

10+80

cb	6.6	
+4	6.9	
N.L.	7.0	143.5
11+10		
N.L.	6.3	144.2
cb	6.1	
+2	6.3	
+4	5.9	
1/4	5.9	
+1 N Pav	5.91	144.57
±	5.83	144.65
+7 S Pav	5.92	144.56
1/4	6.0	
+5	6.4	
cb	6.5	
+3	6.6	
SL	8.5	142.0
11+36		
SL	7.5	143.0
+3	7.2	
+7	6.3	
cb	6.1	
1/4	5.7	
+1 S Pav	5.61	144.87
±	5.50	144.98

150.48

17

11+36

+9 N Pav	5.56	144.92
1/4	5.6	
+6	5.6	
cb	5.9	
+3	6.3	
+8	6.4	
N.L.	6.2	144.3
11+70		
N.L.	5.2	145.3
+1	5.7	
cb	5.5	
+4	5.2	
1/4	5.2	
+1 N Pav	5.17	145.31
±	5.08	145.40
+9 S Pav	5.18	145.30
1/4	5.3	
cb	5.7	
+3	5.9	
+6	7.1	
SL	7.2	143.3

15048

12+00		
SL	7.4	143.1
+4	7.0	
+8	5.5	
cb	5.5	
1/4	4.9	
+1 S Pav	4.77	145.69
±	4.70	145.78
+9 N Pav	4.78	145.70
1/4	4.8	
+6	4.8	
cb	5.2	
+7	5.3	
NL	4.5	146.0
12+30		
NL	5.0	145.5
+4	5.4	
+9	4.5	
cb	4.6	
1/4	4.4	
+1 N Pav	4.29	146.19
±	4.20	146.28
+9 S Pav	4.30	146.18
1/4	4.4	
+5	4.9	
cb	5.5	
SL	7.1	143.4

15048

18

12+60		
SL	6.2	144.3
+5	5.6	
cb	4.5	
+5	4.3	
1/4	4.0	
+1 S Pav	3.77	146.71
±	3.69	146.79
+9 N Pav	3.82	146.66
1/4	3.9	
cb	4.1	
+8	4.7	
NL	4.3	146.2
12+85		
NL	3.5	147.0
+5	3.7	
cb	3.5	
1/4	3.4	
+1 N Pav	3.28	147.28
±	3.19	147.29
+9 S Pav	3.28	147.20
1/4	3.3	
cb	4.1	
SL	4.6	145.9

150.48

12+95 ⁶⁰ = w.L. 49 th St.			
S.L. walls		2.60	147.88
+5		3.0	
+7		3.4	
cb		3.2	
+6		3.0	
'A		3.1	
+1 S Pav		3.06	147.42
±		2.99	147.49
+7 N Pav		3.08	147.40
'A		3.1	
cb		3.4	
+8		3.5	
N.L.		3.0	147.5
13+0060 = w cb 49 th			
N.L.		3.3	147.2
cb		3.3	
'A		3.0	
+1 N Pav		2.91	147.57
±		2.83	147.65
+9 S Pav		2.92	147.56
'A		2.9	
cb		3.0	
S.L.		3.2	147.3
S.L. top cb		2.65	147.83

150.48

19

13+0810 = w 'A 49 th			
S.L.		3.0	147.5
cb		2.7	
+5		3.0	
'A		2.8	
+1 S Pav		2.75	147.73
±		2.65	147.83
+9 N Pav		2.74	147.74
±		2.8	
cb		3.1	
N.L.		3.5	147.0
13+1560			
N.L.		3.4	147.1
cb		3.0	
'A		2.6	
+1 N Pav		2.57	147.91
±		2.50	147.98
+9 S Pav		2.59	147.89
'A		2.6	
+6		2.8	
cb		2.7	
S.L.		2.8	147.7

150.48

13+23 ¹ = E'A 49 th		
S.L.	2.6	147.9
+8	2.7	
cb	2.8	
+3	2.8	
1/4	2.4	
+1 S Pav	2.40	147.08
±	2.30	147.18
+9 N Pav	2.33	147.15
1/4	2.4	
cb	2.8	
N.L.	3.3	147.2
13+30 ⁶ = E'cb 49 th		
N.L.	3.1	147.4
cb	2.5	
1/4	2.2	
+1 N Pav	2.18	148.30
±	2.14	148.34
+9 S Pav	2.24	148.24
+8	2.7	
cb	2.6	
S.L.	2.7	147.8
S.L. top cb	1.99	148.49

150.48

20

13+3560 = E.L 49 th		
S.L. walls	1.98	148.60
S.L. grad	2.2	148.3
+6	2.4	
cb	2.7	
1/4	2.2	
+1 S Pav	2.13	148.35
±	2.02	148.46
+9 N Pav	2.06	148.42
1/4	2.1	
cb	2.4	
N.L.	3.0	147.5
13+80		
N.L.	2.0	148.5
cb	1.4	
1/4	1.0	
+1 N Pav	0.91	149.57
±	0.82	149.66
+9 S Pav	0.90	149.58
1/4	1.1	
+8	1.9	
cb	1.6	
+2	1.8	
+6	2.7	
S.L.	2.6	147.9

14+10	150.48		
S.L.		1.9	148.6
+9		0.9	
cb		0.9	
+4		0.8	
1/4		0.1	
+1 SPav		0.05	150.43
+		0.00	150.48
+9 NPav		0.14	150.34
1/4		0.1	
cb		0.6	
+4		1.0	
N.L.		1.2	149.3
NE. 49 th imp. B.M.		2.10	148.38 (148.33)
	150.43		
T.P. 12.82	163.01	0.24	150.19
14+40			
N.L.		12.2	150.8
+6		11.9	
cb		12.2	
+5		11.9	
1/4		12.0	
+1 NPav		11.94	151.07
+		11.78	151.23
+9 SPav		11.83	151.18
1/4		12.0	

14+40	163.01		
+8		12.7	
cb		12.7	
+3		12.8	
+7		13.5	
S.L.		13.9	149.1
14+70			
S.L.		12.9	150.1
+2		12.9	
+8		11.4	
cb		11.5	
1/4		11.0	
+1 SPav		10.85	152.16
+		10.78	152.23
+9 NPav		10.86	152.15
1/4		10.9	
+8		11.1	
cb		10.9	
+5		10.8	
N.L.		11.0	152.0

		163.01	
15+00			
N.L.		9.9	153.1
cb		10.3	
+5		10.4	
+7		10.0	
'A		9.8	
+1	N Pav	9.76	153.25
+		9.70	153.31
+9	S Pav	9.81	153.20
'A		9.9	
+5		10.4	
cb		10.6	
+1		10.1	
+3		10.5	
+6		11.8	
S.L.		11.9	151.1
15+30			
S.L.		9.9	153.1
+5		10.4	
+9		9.3	
cb		9.3	
'A		8.7	
+1	S Pav	8.64	154.37
+		8.52	154.49
+9	N Pav	8.61	154.40
'A		8.6	

		163.01	22
15+30			
cb		9.4	
+3		9.1	
+7		8.5	
N.L.		8.2	154.8
15+60			
N.L.		6.5	156.5
+8		7.0	
cb		7.5	
+3		7.8	
'A		7.3	
+1	N Pav	7.24	155.77
+		7.21	155.81
+9	S Pav	7.33	155.68
'A		7.4	
cb		8.1	
+5		7.3	
S.L.		7.0	154.0
15+90			
S.L.		7.7	155.3
+5		7.5	
cb		6.7	
'A		6.1	
+1	S Pav	5.99	157.02
+		5.90	157.11
+9	N Pav	5.95	157.06
'A		6.1	

163.01

15+90

+8	6.5	
cb	6.3	
+2	6.2	
+4	5.6	
N.L.	5.2	157.8
16+18 ⁸⁵	OZARK W.L. 50 th on North.	
N.L.	3.9	159.1
+6	4.1	
cb	4.4	
+5	4.9	
1/4	4.6	
+1 N.Pav.	4.56	158.45
±	4.54	158.47
+9 S.Pav.	4.64	158.37
1/4	4.7	
cb	5.3	
S.L.	6.2	156.8
16+28 ⁸⁵	= W.L. 50 th ST on South.	
S.L.	5.1	157.9
cb	4.8	
1/4	4.3	
+1 S.Pav.	4.23	158.78
±	4.11	158.90
+9 N.Pav.	4.14	158.84
1/4	4.1	

163.01

23

16+28⁸⁵

+8	4.3	
cb	4.0	
N.L.	4.0	159.0
16+48 ⁸⁵	= ± 50 th on South	
N.L.	3.3	159.7
cb	3.2	
1/4	3.3	
+1 N.Pav.	3.27	159.74
±	3.20	159.81
+9 S.Pav.	3.23	159.78
1/4	3.1	
cb	3.3	
S.L.	3.5	159.5
2+68 ⁸⁵	= F.L. 50 th ST.	
S.L.	2.8	160.2
cb	3.0	
+6	2.5	
1/4	2.4	
+1 S.Pav.	2.32	160.69
±	2.25	160.76
+9 N.Pav.	2.33	160.68
1/4	2.3	
cb	2.6	
N.L.	3.0	160.0

17+10	163.01		
NL	0.9	162.1	
+4	1.1		
cb	0.9		
+5	1.2		
1/4	0.7		
+1 N Pav	0.49	162.52	
±	0.38	162.63	
+9 S Pav	0.48	162.53	
1/4	0.6		
cb	1.1		
+5	1.3		
S.L.	1.1	161.9	
T.P. 12.68	175.52	0.17	162.84
17+40			
S.L.	12.1	163.4	
cb	12.2		
1/4	11.7		
+1 S Pav	11.67	163.85	
±	11.54	163.98	
+9 N Pav	11.58	163.94	
1/4	11.7		
cb	12.1		
+2	12.5		
NL	12.5	163.0	

17+70	175.52		
NL	11.1	164.4	
cb	10.8		
1/4	10.2		
+1 N Pav	10.24	165.28	
±	10.18	165.34	
+9 S Pav	10.30	165.22	
1/4	10.4		
+7	10.9		
cb	10.8		
+5	10.6		
S.L.	10.4	165.12	
18+00			
S.L.	8.7	166.8	
cb	9.1		
1/4	8.8		
+1 S Pav	8.89	166.63	
±	8.82	166.70	
+9 N Pav	8.89	166.63	
1/4	9.0		
+6	9.5		
cb	9.4		
NL	9.3	166.2	

175.52

18+30

NL		7.9	167.6
+2		7.7	
+8		7.8	
cb		8.1	
+6		7.8	
1/4		7.6	
+1	N Pav	7.51	168.01
±		7.48	168.04
+9	S Pav	7.60	167.92
1/4		7.6	
+3		7.6	
+6		8.1	
cb		7.9	
+5		7.9	
S.L		7.4	168.1
18+60			
S.L	walk to house	5.07	170.45
+3 ^S	end walk	5.30	
+5		6.4	
cb		6.5	
1/4		6.1	
+1	S Pav	6.13	169.39
±		5.98	169.54
+9	N Pav	6.07	169.45
1/4		6.1	

175.52

25

18+60

cb		6.6	
N.L. Drive		6.54	168.98
18+90			
NL		5.2	170.3
+8		5.0	
cb		5.2	
+6		4.9	
1/4		4.7	
+1	N Pav	4.73	170.79
±		4.69	170.83
+9	S Pav	4.81	170.71
1/4		4.8	
+8		5.2	
cb		5.2	
S.L		4.7	170.8
19+20			
S.L		3.6	171.9
+3 ^S		3.9	
+4		4.2	
cb		4.1	
1/4		3.5	
+1	S Pav	3.53	171.99
±		3.41	172.11
+9	N Pav	3.41	172.11
1/4		3.4	
cb		4.0	

175.52

19+20

NL 4.4 171.1

19+50

NL 3.2 172.3

+8 2.9

cb 2.9

+5 2.4

1/4 2.3

+1 N Pav 2.27 173.25

± 2.15 173.37

+9 S Pav 2.29 173.23

1/4 2.3

cb 2.9

+5 3.0

SL 3.0 172.5

19+80

SL 1.4 174.1

+3 1.5

cb 2.0

1/4 1.1

+1 S Pav 1.06 174.46

± 0.99 174.53

+9 N Pav 1.07 174.45

1/4 1.1

+4 1.1

+8 1.7

cb 1.6

19+80

175.52

26

NL 2.0 173.5

T.P. 10 27 125.48 0.33 175.19

20+10

NL 10.7 174.8

+5 10.8

cb 10.5

+3 10.6

+6 10.1

1/4 10.0

+1 N Pav 9.99 175.49

± 9.86 175.62

+9 S Pav 9.92 175.56

1/4 10.1

+5 10.7

cb 10.8

+5 10.9

SL 10.4 175.1

20+10

SL 9.5 176.0

cb 9.9

+5 9.9

1/4 9.2

+1 S Pav 8.97 176.51

± 8.92 176.56

+9 N Pav 8.99 176.49

185.48

20+40

1/4	9.1	
+5	9.5	
cb	9.5	
N.L.	9.5	176.0

20+70 = w.l. street 20 North (Winnona?)

N.L.	8.7	176.8
cb	8.8	
1/4	8.2	
+1 N Pav	8.10	177.38
±	8.01	177.47
+9 S Pav	8.07	177.41
1/4	8.2	
+5	9.0	
cb	8.7	
SL	8.7	176.8

21+00

SL	7.7	177.8
cb	7.6	
+6	7.7	
1/4	7.3	
+1 S Pav	7.22	178.26
±	7.14	178.34
+9 N Pav	7.18	178.30
1/4	7.3	
cb	8.1	
+2	8.1	

185.48

27

21+00

+3	7.9	
N.L.	7.9	177.6

21+19.90 = E.L. Street on North.

N.L.	7.2	178.3
------	-----	-------

+8	7.0	
cb	7.3	
+4	7.4	
1/4	6.8	
+1 N Pav	6.66	178.82
±	6.62	178.86
+9 S Pav	6.73	178.75
1/4	6.9	
+5	7.3	
cb	7.1	
SL	7.3	178.2

21+60

SL	6.5	179.0
+8	5.7	
cb	5.8	
+6	5.9	
1/4	5.6	
+1 S Pav	5.60	179.88
±	5.57	179.91
+9 N Pav	5.67	179.81
1/4	5.8	

185.48

21+60
+5 6.3
cb 5.9
NL 5.7 1798

21+90
NL 5.0 1805

+5 5.4
cb 5.4
+6 5.5
1/4 5.2
+1 N Pav 5.11 18037

4 4.80 18068

+9 S Pav 4.69 18079

1/4 4.7

cb 4.8

SL 4.3 1802

L L = 2746' R = 530 - 470 = 5002
curve stationed on inside equation for outside
22+04.42 = B.C. arc at E.C.

SL 4.8 1807

+3 4.2

cb 4.1

+5 4.5

1/4 4.2

+1 S Pav 4.19 18129

4 4.37 18111

+9 N Pav 4.73 18075

185.48

22+04.40 = SL Churchward

1/4 4.8

cb 5.0

+5 4.5

NL 4.5 1810

22+29.42

NL 3.6 181.9

+7 3.4

+8 4.1

cb 4.1

+4 4.5

1/4 4.1

+1 N Pav 4.02 181.46

4 3.67 181.81

+9 3.41 182.07

1/4 3.4

+8 3.4

cb 3.1

+4 3.3

+8 3.8

SL 3.8 181.7

28

185.48

22+54⁴⁰

S.L.	2.5	1830
+5	2.5	
cb	2.5	
+3	2.8	
+8 S Pav	2.68	18280
1/4	2.70	18278
±	2.96	18252
+9 N Pav	3.37	18211
1/4	3.4	
+4	3.7	
+7	3.6	
cb	3.0	
+3	2.6	
A.L.	2.7	1828
22+79 ⁴⁰		
N.L.	2.3	1832
cb	2.0	
+1	2.0	
+4	3.0	
+7	3.1	
1/4	2.9	
+1 N Pav	2.77	18261
±	2.38	18310
1/4	2.10	18338
+6 S Pav	2.07	18341

185.48

29

22+79⁴⁰

cb	2.3	
+3	1.8	
+6	1.5	
S.L.	1.8	183.7
23+04 ⁴⁰		
S.L.	1.2	184.3
cb S Pav	1.60	184.88
1/4	1.61	184.67
±	1.85	183.63
+9 N Pav	2.24	183.24
1/4	2.3	
+2	2.5	
cb	1.5	
+4	1.3	
N.L.	1.4	184.1
23+29 ⁴⁰		
N.L.	0.8	184.7
cb	1.0	
+5	1.8	
1/4	1.9	
+1 N Pav	1.90	183.58
±	1.53	183.95
1/4	1.23	184.25
cb	1.16	184.32
+7 ^S S Pav	1.18	184.30
S.L.	1.2	184.3

185.48

~~23+54⁴⁰~~

s.l. on Pav	0.71	184.77
cb	0.85	
+2 ² N Pav	0.91	184.57
+8	0.90	184.58
1/4	1.0	184.48
+1 S Pav	1.06	184.42
±	1.26	184.22
+9	1.66	184.82
1/4	1.7	
+3	1.9	
+6	1.7	
cb	1.1	
+2	0.9	
NL	0.6	184.9

~~23+79⁴⁰~~

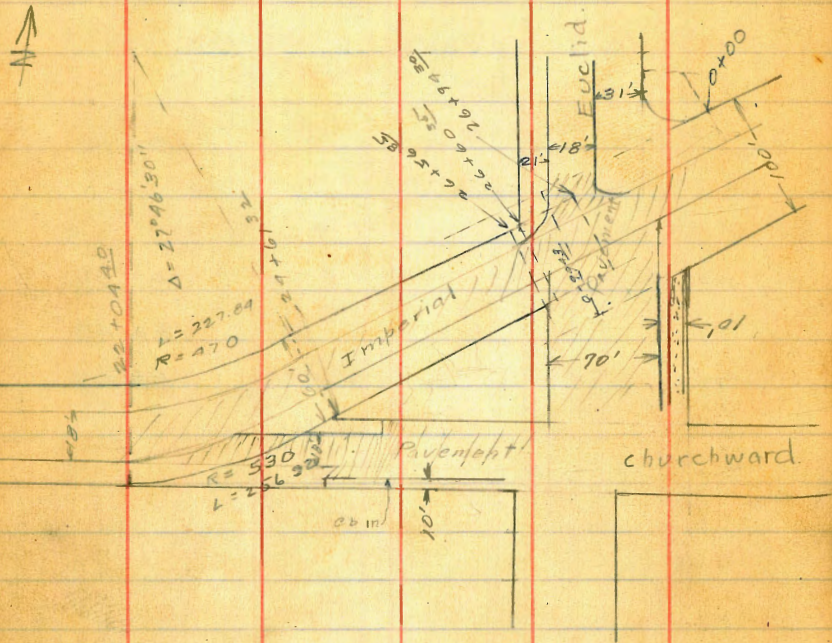
NL	0.5	185.0
+9	0.6	
cb	1.2	
+4	2.1	
1/4	1.6	
+1 N Pav	1.50	183.98
±	1.10	184.38
+9 S Pav	0.84	184.64
1/4	0.8	
cb	0.8	

30

~~23+79⁴⁰~~

185.48

0+7 ⁸ N Pav	0.70	184.78	
s.l. on Pav	0.60	184.88	
T.P. 1.53	186.56	0.45	185.03
29+04 ⁴⁰			
s.l.	1.8	184.8	
cb	1.9		
1/4	1.9		
+1 S Pav	1.95	185.61	
±	2.13	184.43	
+9 N Pav	2.47	184.07	
1/4	2.6		
+5	2.9		
cb	2.1		
+4	1.4		
NL	1.1	185.5	
24+32 ⁴⁸ = 24+61 ³²	= E.C.	Progress from 24+61 ³²	
NL	1.7	184.9	
+7	2.1		
cb	2.8		
+2	3.0		
+5	2.8		
1/4	2.7		
+1 N Pav	2.66	183.90	
±	2.28	184.28	
+9 S Pav	2.05	184.51	
1/4	2.0		



$= 247613 \pm$
 $27+3298$

186.56

eb		2.0	
S.L.		1.8	184.8
24+70			
S.L.		1.8	184.8
eb		2.0	
1/4		2.1	
+1	S Pav	2.11	184.45
+		2.31	184.25
+9	N Pav	2.59	183.99
1/4		2.6	
eb		2.7	
NL on Drive		2.45	184.11
24+90			
NL		2.5	184.1
+8		2.4	
eb		2.5	
1/4		2.7	
+1	N Pav	2.72	183.84
+		2.51	184.05
+9	S Pav	2.39	184.17
1/4		2.4	
eb		2.2	
S.L.		1.9	184.7

186.56

25+20

S.L.	2.4	184.2
eb	2.7	
1/4	2.9	
+1 S Pav	2.93	183.63
+	2.89	183.67
+9 N Pav	2.97	183.59
1/4	3.0	
+5	3.1	
eb	2.9	
N.L.	2.7	183.9
25+50		
N.L.	3.9	182.7
+5	3.5	
+8	3.8	
eb	3.5	
+1	3.4	
+6	3.7	
1/4	3.5	
+1 N Pav	3.37	183.17
+	3.42	183.14
+9 S Pav	3.54	183.02
1/4	3.5	
eb	3.1	
S.L.	2.8	183.8

50 ft 20' from +
 1.3 in st. 25+40 to 25+100 on South.

Wall 6.5' in st on South 25+80 to 26+80

186.56

32

25+80

S.L.	3.4	183.2
eb	3.9	
+5	4.1	
1/4	4.0	
+1 S Pav	4.14	182.42
+	4.05	182.51
+9 N Pav	4.08	182.48
1/4	4.1	
+5	4.4	
+6	4.2	
eb	4.2	
+8	3.9	
N.L.	4.1	182.5
26+10		
N.L.	5.9	180.7
eb	5.2	
+3	5.0	
+6	5.3	
1/4	5.0	
+1 N Pav	4.90	181.64
+	4.88	181.68
+9 S Pav	4.98	181.58
1/4	4.9	
eb	4.4	
S.L. = eb + 33	4.1	180.5

186.56

26+40

S.L. = S.L. + 6.8

eb

+7

1/4

+1 S Pav

+

+9 N Pav

1/4

+4

cb

N.L.

26+56.85 = W.L. Euclid on South

N.L.

+3

+4

cb

+5

1/4

+10² N Pav

+

+9 S Pav

1/4

+5

+7

cb

S.L. = cb + 3.5

5.6

5.7

6.1

6.0

5.91

5.85

5.87

5.9

6.3

5.8

6.3

7.4

7.3

7.0

6.9

6.6

6.5

6.48

6.46

6.64

6.6

6.5

6.2

6.1

6.0

181.0

180.65

180.71

180.69

180.3

179.2

180.08

180.10

179.92

180.6

186.56

26+60³⁵ = W.L. Euclid on North

S.L. on Pav

+6 N Pav

+6² well

cb

+3

1/4

+1 S Pav

+

1/4

+10² N Pav

+5

cb

+6

N.L.

26+71

N.L.

+4

+7

cb

+1 N Pav

1/4

+

1/4 on Pav

cb ✓

S.L. ✓

5.86

6.19

6.0

6.1

6.0

6.6

6.58

6.57

6.55

6.57

6.5

7.0

7.1

7.4

8.5

7.5

7.2

7.1

7.23

7.16

7.13

7.22

6.91

6.48

180.70

180.37

179.98

179.99

180.01

179.99

179.2

178.1

179.33

179.40

179.43

179.34

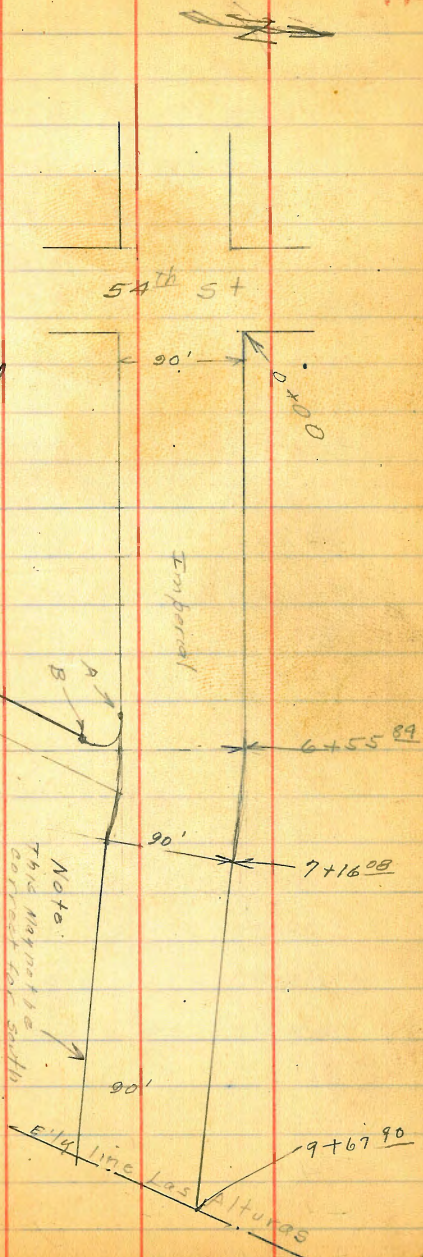
179.65

180.08

33

26+81		186.56		
S.L.	on Pav		6.79	179.77
cb	✓		7.18	179.38
Dist. used in way.	✓		7.46	179.10
1/4	✓		7.51	179.05
eb	✓		7.58	178.98
B.L. = w.c. Euclid Pav.			7.84	178.72
26+94 ³⁰	Euclid Paving			
N.L.	on Pav		8.23	178.33
eb	✓		8.02	178.54
1/4	✓		7.9	178.66
S 1/4	✓		7.99	178.57
eb+1	✓		7.70	178.86
S.L.	✓		7.20	179.36
Nails Pole on imp. = Euclid.				
B.M.			4.80	181.26
TP	0.01	183.09	3.48	183.08
TP	0.42	171.48	12.03	171.06
TP	0.76	159.29	12.95	158.53
B.M.	Beginning		10.88	148.41 (148.33)

go check back this B.M.
 should be 181.68 for levels ahead
 See pages this book & Book 1300 pages 26



Nov 15-28
 Imperial
 1900
 1901

X sec. Imperial Ave From
 EL 54th Easterly. to EL Las Alturas N^o 3
 90' st 15' cbs 60' Rdway.

Min's file
 540 Imperial
 x 1/2 lid.

B.M	0.93	182.19		181.76
T.P	0.80	169.93	13.06	169.13
T.P	6.12	163.18	12.87	157.06
T.P.	3.95	160.29	6.84	156.34
BM Hub N.E 53 rd & Imperial.			6 ⁰¹	154.28
T.P	6.75	164.58	2.46	157.83
0+00 = EL 54 th				
N.L.			6.2	158.4
cb			6.0	
+10			5.9	
1/4			5.2	
+4			5.0	
+11 N Pav			5.08	159.50
±			5.04	159.46
+5 ± Pav			5.01	159.49
+14 S Pav			5.10	159.40
1/4			5.0	
cb			5.4	
T.P			5.6	
S.L.			5.4	159.2
0+30				
S.L.			5.6	159.0
cb			5.6	
+13			5.3	
1/4			5.0	
+1 S Pav			4.90	159.60
+10 ± Pav			4.81	159.69

0+30		164.58		
±			4.85	159.65
+4 N Pav			4.90	159.60
+10			5.1	
1/4			5.4	
+10			5.6	
cb			5.9	
N.L.			6.4	158.1
S.N			6.7	157.9
0+65				
S.N			7.3	157.3
N.L.			6.7	157.9
+7			5.7	
cb			5.8	
+6			5.6	
1/4			5.5	
+2			5.4	
+6			5.1	
+11 N Pav			4.67	159.83
±			4.64	159.86
+5 ± Pav			4.62	159.88
+14 S Pav			4.72	159.78
1/4			4.8	
+3			5.2	
cb			5.3	
+2			5.6	
+4			5.6	

164.58⁰

0 + 6.5			
+6	5.2		
S.L.	5.2	159.4	
1 + 0.0			
S.L.	5.0	159.6	
+10	4.9		
+12	5.2		
cb	5.1		
+7	5.2		
+12	5.0		
1/4	4.7		
+1 S.Pav	4.57	159.93	
+10 &	4.44	160.06	
&	4.47	160.03	
+4 N.Pav	4.50	160.00	
+9	4.5		
1/4	5.0		
+5	5.0		
+6	5.2		
+8	4.9		
cb	5.7		
+5	6.2		
N.L.	7.3	157.2	
5'N	7.5		

164.58⁰

1 + 3.0			
5N	7.0		
N.L.	6.8	157.7	
+5	6.6		
+10	6.7		
cb	6.4		
+4	6.3		
+8	5.6		
1/4	5.2		
+4	5.1		
+7	4.7		
+11 N.Pav	4.40	160.10	
&	4.32	160.18	
+5 & Pav	4.31	160.19	
+14 S.Pav	4.38	160.12	
1/4	4.5		
+3	4.7		
cb	4.5		
+4	5.0		
+5	4.5		
S.L.	4.8	159.7	

164.58

1+65		
S.L.	4.5	160 0
+10	4.4	
eb	4.3	
+2	4.2	
+9	4.4	
14	4.3	
+1 SPav.	4.25	160 25
+10 ± Pav	4.13	160 37
±	4.11	160 39
+4 NPav	4.15	160 35
+8	4.8	
+13	7.3	
14	7.5	
eb	7.8	
+2	7.6	
N.L.	7.9	156 6
10'N	8.3	
2+00.		
10N	7.6	
N.L.	7.8	156 7
+5	8.1	
+10	8.0	
eb	8.1	
+12	7.8	
14	7.4	
+5	4.6	

164.58

37

2+00		
+11 NPav	4.02	160 48
±	3.96	160 54
+5 ± Pav	3.94	160 56
+14 SPav	4.06	160 44
14	4.2	
+6	4.5	
eb	4.6	
+4	5.0	
+5	4.5	
SL	4.5	160 0
2+30		
SL	4.4	160.1
+10	4.5	
+12	4.8	
eb	4.4	
+5	4.6	
+11	4.2	
14	4.0	
+1 SPav	3.94	160 56
+10 ± Pav	3.81	160 69
±	3.82	160 68
+4 NPav	3.89	160.61
+9	4.0	
14	6.3	
+5	7.2	

2+30

104.58⁰

cb 7.8 1567

+5 7.8

N.L. 8.3 1562

10'N 8.1

T.P. 9.38 166.50^{.42} 7.46 157.12^{.04}

2+65

10'N 9.0

N.L. 9.5 1569

cb 9.9

+8 9.4

1/4 7.0

+5 6.4

+11 N Pav 5.81 160.61

4 5.71 160.71

+5 4 Pav 5.64 160.78

+14 SPav 5.70 160.72

1/4 5.8

+6 6.2

cb 6.5

+4 6.8

+6 6.4

S.L. 6.4 1600

2+75

S.L. 6.4 160.0

+1 6.6

+10 6.5

+11 6.7

+13 6.4

cb 6.4

+8 6.2

1/4 5.8

+1 SPav 5.66 160.76

+10 4 Pav 5.60 160.82

4 5.65 160.77

+4 N Pav 5.75 160.67

+8 6.4

+9 6.2

1/4 6.6

cb 7.3

+9 7.0

N.L. 7.3 159.1

3+00

N.L. 6.7 159.7

cb 6.4

+7 6.6

1/4 6.2

+6 6.0

+7 6.2

166.42

38

166.42

3+00			
+11 N Pav	5.69	160 73	
¢	5.60	160 82	
+5 ¢ Pav	5.55	160 87	
+14 S Pav	5.64	160 78	
1/4	5.7		
+3	6.0		
+7	6.2		
+13	6.5		
eb	6.4		
+4	6.4		
+6	6.1		
+11	6.1		
S.L	6.2	160 2	
3+30			
S.L	6.2	160 2	
+1	6.5		
+10	6.3		
+12	6.5		
eb	6.5		
+8	6.4		
1/4	5.7		
+1 S Pav	5.60	160 82	
+10 ¢ Pav	5.46	160 96	
¢	5.50	160 92	
+4 N Pav	5.56	160 86	
+8	6.0		

166.42

39

3+30			
+10	5.8		
1/4	6.1		
+10	6.3		
eb	6.2		
N.L.	6.3	160.1	
3+65			
N.L	6.5	159.9	
+10	6.1		
eb	6.4		
+5	6.6		
+13	6.4		
1/4	6.1		
+7	5.7		
+11 N Pav	5.51	160.91	
¢	5.44	160.98	
+5 ¢ Pav	5.40	161.02	
+14 S Pav	5.51	160.91	
1/4	5.7		
+3	5.9		
+5	5.8		
+10	7.1		
+13	7.0		
eb	6.6		
+4	6.6		
+7	6.2		
+14	6.5		

166.42

3+65

S.L.	6.1	160.3
1+00		
S.L.	5.8	160.6
+1	6.2	
+10	6.0	
eb	6.0	
+3	6.3	
+10	5.9	
1A	5.9	
+1 SPav	5.29	161.13
+10 4 Pav	5.24	161.18
4	5.28	161.14
+4 NPav	5.35	161.07
+10	5.31	161.11
1A	5.6	
+5	5.9	
eb	6.0	
+5	6.0	
N.L.	6.2	160.2

166.42

40

H450

N.L.	5.7	161.7
eb	5.5	
1A	5.5	
+4	5.5	
+11 NPav	5.16	161.26
4	5.08	161.34
+5 4 Pav	5.06	161.36
+14 5 Pav	5.19	161.23
1A	5.3	
+3	5.6	
+5	5.6	
+12	6.3	
eb	6.0	
+4	6.1	
+7	5.7	
+14	5.8	
S.L.	5.5	160.9
5+00		
S.L.	5.4	161.0
+1	5.6	
+10	5.5	
+12	5.6	
eb	5.5	
+7	5.5	
1A	5.1	
+1 SPav	4.95	161.47

166.42

5700

+10	± Pav	4.84	161.58
±		4.86	161.56
+4	N Pav	4.92	161.50
+9		5.0	
+13		5.2	
1/4		5.2	
+5		5.2	
cb		5.4	
+6		5.1	
NL		5.2	161.2

5730

NL		4.9	161.5
cb		5.2	
1/4		5.1	
+8		4.7	
+11	N Pav	4.74	161.68
±		4.65	161.77
+5	± Pav	4.62	161.80
+14	S Pav	4.72	161.70
1/4		4.9	
+2		5.3	
cb		5.0	
+4		5.4	
+6		5.1	
+8		4.9	
+13		4.9	

166.42

41

+14		5.3	
SL		4.8	161.6
5765			
SL		4.3	162.1
+2		4.9	
+4		4.5	
+10		4.6	
+12		4.8	
cb		4.5	
+10		4.9	
1/4		4.5	
+1	S Pav	4.38	162.04
+10	± Pav	4.26	162.16
±		4.29	162.13
+4	N Pav	4.36	162.06
+10		4.4	
1/4		4.7	
cb		4.7	
NL		4.8	161.6

166.42

b+00		
NL	4.3	162.1
cb	4.4	
+12	4.4	
1/4	4.4	
+11 N Pav	3.88	162.54
+	3.83	162.59
+5 E Pav	3.82	162.60
+14 S Pav	3.86	162.46
1/4	4.0	
+6	4.3	
+10	4.6	
cb	4.5	
+4	4.7	
+5	4.3	
+13	4.5	
+14	4.8	
SL	4.4	162.0
6+30		
SL	4.1	162.3
+1	4.3	
+2	4.1	
+9	4.0	
+11	4.5	
cb	4.1	
1/4	3.9	
+0 ³ S Pav	3.77	162.65

42

166.42

6+30		
+9 ² E Pav	3.54	162.88
+	3.48	162.84
+3 ² N Pav	3.43	162.99
+7	3.7	
+10	3.7	
1/4	3.9	
+10	3.9	
cb	4.0	
+10	4.2	
+12	4.0	
NL	4.1	162.3
Drive on Northbat ⁶⁺⁰⁶	4.16	162.26
Walk on North _{3.5 miles at 6+28}	4.10	162.32
6+55 ⁸⁹ = B.C.		
NL	4.4	162.0
cb	3.9	
1/4	3.9	
+13 ¹ N Pav	3.18	163.24
+	3.21	163.21
+7 ¹ E Pav	3.29	163.13
1/4	3.51	162.91
+1 S Pav	3.55	162.87
+5	3.7	
cb	3.7	
+4	3.9	
+6	3.4	

6+55⁸⁹
 +13 3.8
 +14 4.0
 S.L. 3.7 162.7
 (A) Scep 3a 3.6
 (B) r v 3.5
 6+85⁹⁶ - cot curve
 S.L. 3.5 162.9
 +10 3.4
 +12 3.7
 cb 3.4
 +8 3.3
 +9 3.5
 +13^S SPav 3.27 163.15
 1/4 3.24 163.18
 +17^S $\frac{1}{2}$ Pav 3.05 163.37
 $\frac{1}{2}$ 2.96 163.46
 +1^S N Pav 2.96 163.46
 +8 3.1
 1/4 3.4
 cb 3.8
 N.L. 3.7 162.7

166.42

Sta. on outside of curve

16642

43

7+16⁸⁸ = E.C.
 N.L. 3.4 163.0
 +4 3.2
 cb 3.4
 1/4 2.9
 +5 2.9
 +7 2.7
 +12^S N Pav 2.70 163.72
 $\frac{1}{2}$ 2.71 163.71
 +8^S $\frac{1}{2}$ Pav 2.80 163.62
 1/4 2.98 163.44
 +10^S SPav 2.99 163.43
 +6 3.1
 +10 3.4
 cb 3.4
 S.L. 3.4 163.0
 7+30
 S.L. 2.9 163.5
 cb 3.0
 +5 3.2
 +11 2.8
 +10 3.0
 1/4 2.9
 +11 SPav 2.84 163.58
 +10 $\frac{1}{2}$ Pav 2.59 163.83
 $\frac{1}{2}$ 2.49 163.93
 +4 N Pav. 2.47 163.95

16642

7730		
+10	2.7	
1/4	2.7	
cb	3.0	
+7	3.1	
+11	2.9	
N.L.	3.0	163.4
7+65		
N.L.	2.6	163.8
cb	2.3	
1/4	2.1	
+5	2.0	
+9 ⁵ N Pav	2.06	164.36
±	2.13	164.29
+3 ⁵ ± Pav	2.20	164.22
+12 3 Pav.	2.45	163.97
1/4	2.5	
cb	3.1	
S.L.	3.4	163.0
8+00		
S.L.	1.1	165.3
+3	2.0	
cb	2.6	
+5	2.4	
1/4	2.8	
+4 ⁶ 5 Pav	2.45	163.97

16642

44

8+00		
+13 ² ± Pav	2.10	164.32
±	2.06	164.36
+7 ⁶ N Pav	2.00	164.42
1/4	2.1	
+5	2.0	
cb	2.0	
+7	1.7	
N.L.	1.9	164.5
8+30		
N.L.	1.4	165.0
cb	2.0	
1/4	2.2	
+3	2.3	
+6 ⁸ N Pav	2.17	164.25
±	2.30	164.12
+0 ⁸ ± Pav	2.31	164.11
+9 ⁸	2.61	163.81
1/4	2.9	
1/4	2.7	
+10	2.9	
cb	3.1	
+5	2.8	
+10	2.7	
+14	0.7	
S.L.	0.7	165.7

8+65

166.^{.42}₅₀

S.L.	0.4	166 0
+5	0.6	
+7	2.4	
cb	2.4	
+2	2.3	
+5	1.6	
+10	1.6	
1/4	3.2	
+4 ³ S Pav	2.80	163 62
+13 ³ S Pav	2.51	163 91
±	2.47	163 95
+7 ³ N Pav	2.40	164 02
+11	2.4	
1/4	2.2	
cb	1.7	
+5	1.4	
N.L.	1.0	165 4
T.P. 6.21	171. ^{.38} ₄₆	165. ^{.17} ₂₅
9+00		
N.L.	5.7	175.7
+2	5.7	
cb	6.4	
+8	6.6	
1/4	7.0	
+5	7.2	
+7	7.6	

171.38

45

9+00

cb+8 ² N Pav	7.66	163.72
±	7.70	163 68
+2 ² S Pav	7.71	163 67
+11 ² S Pav	7.90	163 48
1/4	8.1	
+2	8.1	
+4	5.9	
cb	5.5	
+10	4.5	
S.L.	4.5	166 9
9+13		
S.L.	2.6	168 8
cb	3.4	
+7	5.3	
+10	5.9	
13	8.2	
1/4	8.1	
+2 ⁵ S Pav	7.91	163 47
+11 ² S Pav	7.85	163 53
±	7.82	163 56
+5 ⁵ N Pav	7.82	163 56
+7	7.8	
+8	7.4	
+14	6.6	
1/4	6.5	

	171.38	
9+13		
+10	6.2	
cb	6.4	
NL	5.7	165.7
9+30		
NL	5.9	165.5
+5	5.8	
cb	6.2	
+10	6.1	
14	6.3	
+3	6.5	
+8	7.4	
+9	7.8	
+9 ^B N Pav	8.00	163.38
±	7.97	163.41
+3 ^B ± Pav	8.00	163.38
+12 ^B 3 Pav	8.09	163.29
14	8.1	
+3	7.9	
+5	5.5	
cb	4.7	
+5	3.8	
S.L.	3.6	167.8

	171.38	46
9+40		
S.L.	4.4	167.0
cb	4.8	166.6
+9	5.3	166.1
+12	8.0	163.4
±	8.2	163.2
+1 ^B S Pav	8.12	163.26
+10 ^B ± Pav	8.05	163.33
±	8.03	163.35
+4 ^B N Pav	8.06	163.32
+7	7.4	164.0
+14	5.9	165.5
14	5.8	165.6
cb	5.8	165.6
+8	5.5	165.9
NL	5.6	165.8
Sec on EL Las Alturas N ^o 3 = 9+67 ²⁵ on North.		
NL	5.3	166.1
cb	5.7	165.7
14	6.1	165.3
+4	6.1	
+10	8.1	
+10 ² N Pav	8.20	163.18
±	8.18	163.20
+4 ² ± Pav	8.14	163.24
+14 S Pav	8.26	163.12

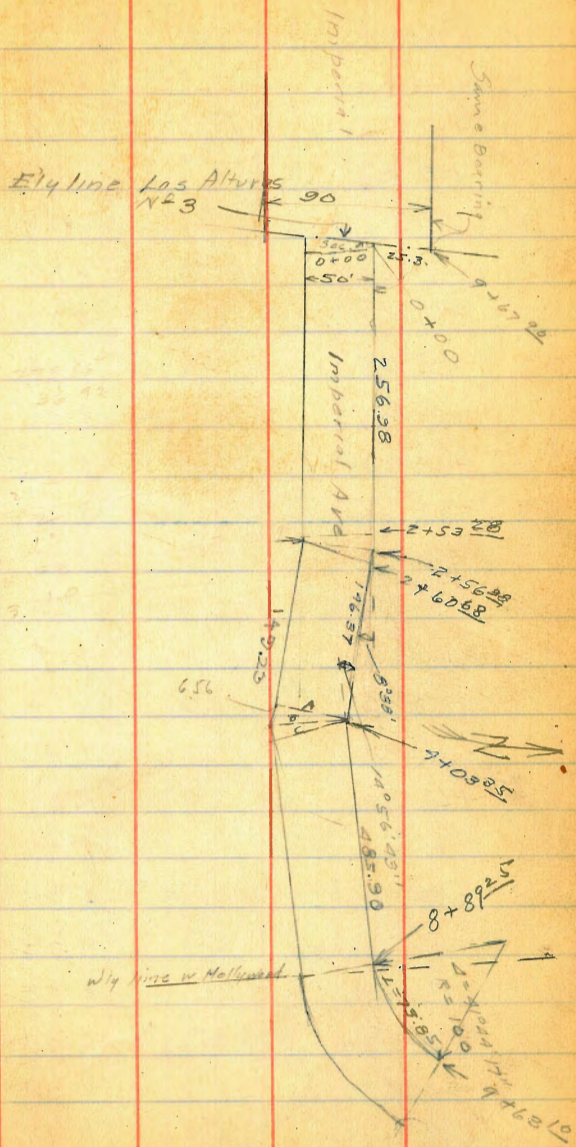
Sec on E.L. Las Alturas

1/4	8.3	
+3	8.0	
+7	4.5	166.9
cb	4.4	167.0
S.L.	4.1	167.3

X Sec Imperial Ave from Ely
line of Las Alturas N#3 Easterly
50' st 10' chs 30' Rdway.

Sec on E.L. Las Alturas = 0+00 on North

S.L.	4.4	167.0
+7	4.5	
cb	5.9	165.5
+7	8.1	163.3
+6 ^S s Pav	8.27	163.11
1/4	8.23	163.15
±	8.13	163.25
+0 ^S ± Pav	8.14	163.24
1/4	8.17	163.19
+2 ^S N Pav	8.20	163.18
+3	8.1	163.3
cb	6.1	165.3
N.L.	5.8	165.6



Imperial.

171.38

0+00		
N.L.	5.8	1656
+9	6.0	
cb	6.3	1651
+5	8.2	1632
+6 N.Pav	8.19	16319
1/4	8.19	16319
± E.Pav	8.18	16320
1/4	8.25	16313
+15 S.Pav	8.25	16313
+65	8.2	1632
cb	5.8	1656
+3	4.3	
S.L.	3.9	167.5
0+30		
S.L.	1.4	170.0
+6	1.8	
cb	7.3	1641
+2	8.3	1631
+5 S.Pav	8.32	16306
1/4	8.32	16306
+65 ± Pav	8.21	16317
±	8.21	16317
1/4	8.31	16307
+05 N.Pav	8.33	16305
+15	8.4	
+25	7.9	

171.38

48

0+30		
+4	7.7	1637
cb	6.1	1653
N.L.	5.7	1657
0+49		
N.L.	5.3	1661
+5	5.5	
cb	6.1	1653
+3	7.5	1639
1/4 N.Pav	8.34	16304
±	8.31	16307
+15 ± Pav	8.30	16308
1/4	8.31	16307
+3 S.Pav	8.35	16303
cb	8.7	1627
+3	4.1	1673
S.L.	3.9	167.5
0+65		
S.L.	4.0	1674
+7	4.3	1671
+9	8.7	1627
cb	8.8	1626
+4 S.Pav	8.45	16293
1/4	8.41	16297
55 ± Pav	8.40	16297
±	8.40	16298

171.38

0+65			
±77	N Pav	8.45	162 93
1A		8.5	
+35		7.8	163 6
cb		5.8	165 6
+1		5.5	
+8		4.9	
N.L.		5.0	166 4
0+81			
10' N		8.7	
N.L.		5.2	166 2
+5		5.0	
cb		5.5	165 9
+2		6.0	165 4
+5		8.7	162 7
1A		8.7	
+1	N Pav	8.58	162 80
±		8.49	162 89
+25	± Pav	8.50	162 88
1A		8.52	162 86
+4	S Pav	8.62	162 76
cb		9.0	162 4
+1		9.0	162 4
+4		3.9	167 5
S.L.		3.8	167.6

171.38

49

1+00			
S.L.		3.8	167 6
+4		4.9	166 5
+8		9.3	162 1
cb		9.2	
+25	S Pav	8.93	162 45
1A		8.83	162 55
±4	± Pav	8.79	162 59
±		8.80	162 58
+55	N Pav	8.88	162 50
1A		9.1	
+25		9.0	162 4
+55		5.5	165 9
cb		5.4	
+6		5.6	
N.L.		6.4	165 0
1+30			
^{15' N} N.L.		^{18.80} 10.5	161.9
+6		6.5	
cb		6.4	
+3		6.7	164 7
+55		9.4	162 0
1A		9.7	
+25	N Pav	9.44	161.94
±		9.34	162 04
+4	± Pav	9.30	162 08

171.38

1+30		
1/4	9.35	162 03
+55 S Pav	9.47	161.91
cb	9.7	161 7
+3	9.5	161 9
+8	3.2	168 2
S.L	2.6	168 8
1+65		
S.L	2.1	169 3
71	2.2	
+65	10.5	160 9
cb	10.3	
+05 S Pav	10.27	161 11
1/4	10.39	160 99
+2 ± Pav	10.35	161 03
±	10.34	161 04
+35	10.37	161 01
1/4	10.9	160 5
+3	8.2	163 2
cb	8.9	
N.L	13.0	158.4
13'N	17.4	
25'N	22.0	

171.38

50

2+00		
^{20'N} N.L	20.4	156.8
cb	14.6	
+7	10.4	
1/4	9.8	161 6
+05	11.3	160 1
+5 N Pav	12.1	159 3
±	11.77	159 61
+65 ± Pav	11.75	159 63
1/4	11.74	159 64
cb	11.74	159 64
+05 S Pav	11.76	159 72
+5	11.77	159.61
+9	11.6	159.77
S.L	7.6	163 8
2+30	4.0	167.4
S.L	5.7	165.7
+4	13.3	
+8 S Pav	13.09	158.29
cb	13.11	
+9 ± Pav	12.99	158.39
1/4	12.99	158.39
±	13.03	158.35
+15 N Pav	13.09	158.29
+55	14.1	
+7	10.9	
1/4	10.9	

2+30			
+6 ^E		7.2	
cb		7.6	
NL		15.8	155.58
25W		23.8	
T.P.	0.10	13.01	158.45
2+65			
25N		13.6	
NL		6.6	151.8
cb		3.5	
'A		1.0	
+2 ^S		0.7	
+3		1.8	
+4		2.0	
+4 ^S		1.5	
+6		1.4	
+6 ^S		1.8	
⊕ N.Pav		1.75	156.72
'A		1.70	156.77
+1 ^S ⊕ Pav		1.69	156.78
cb		1.67	156.80
3 ^S s Pav		1.83	156.64
+7		2.2	156.3
+8		2.2	156.3
SL		0.3	158.2

cont on P. 68

158.55

~~2+82⁸⁴~~ = 2+87⁵

SL		2.0
+1		3.0
+2		2.3
+4		2.6
+6 ^S s Pav		2.64
cb		2.60
+5 ^S ⊕ Pav		2.56
'A		2.57
+7 N Pav		2.69
⊕		2.67
+3		2.3
+5		2.7
'A		3.8
cb		6.6
NL		9.0
15N		12.0
2+86 ⁸⁰ = 2+82 ⁸⁴		
15N		12.3
NL		9.6
cb		7.3
'A		4.2
+3		2.8
⊕		2.7
+1 N Pav		2.68
'A		2.64
+2 ^S ⊕ Pav		2.62

Void to P

51

$$2+86^{80} = 2+82^{84}$$

cb	2.65
+4 S Pav	2.67
+6	2.7
+8	2.3
+9	2.9
S.L.	3.0
$2+90^{76} = 2+82^{84}$	
S.L.	3.0
+1	3.0
+2	2.4
+4	2.7
+6 ^S S Pav	2.70
cb	2.66
+5 ^S Par	2.67
'4	2.68
+7 N Pav	2.78
4	2.8
+4	3.1
+5	2.9
'4	4.3
cb	7.6
NL	10.0
15'N	12.5

$$3+00$$

15'N	12.9
NL	10.8
cb	7.3
'4	3.9
+1	3.3
+2	3.8
+6 ^S N Pav	3.20
4	3.16
'4	3.08
+0 ^S Par	3.08
cb	3.06
+2 S Pav	3.08
+6	2.9
+9	3.0
S.L.	3.7
$3+30$	
S.L.	5.5
+1 ^S	5.5
+2	5.1
+4	4.6
+6	4.9
+8	5.0
cb	4.8
+1 ^S S Pav	4.57
'4	4.46
+3 Par	4.45

3+30

±

4.45

+4⁵ N Pav

4.56

1/4

4.8

+1⁵

5.0

+2⁵

4.8

cb

7.7

N.L.

11.8

15'N

13.2

3+65

15'N

14.1

N.L.

12.8

+3

12.0

cb

7.4

+1

6.6

+2

6.9

+6^L N Pav

6.12

1/4

6.06

± ± Pav

6.04

1/4

6.12

+2^L S Pav

6.15

cb

6.3

+3

6.9

S.L.

7.1

See 47
A+00²⁵ (A)

S.L.

8.5

+7

8.8

cb

8.7

+4

7.7

+6

7.9

1/4

7.8

+2 S Pav

7.76

±

7.65

3⁵ ± Pav

7.65

1/4

7.64

+5 N Pav

7.79

cb

8.1

+2

8.4

+3

8.2

N.L.

12.9

15'N

16.3

A+00²⁵ (B)

N.L.

12.9

+7

8.2

+8

8.4

cb

8.4

+2 N Pav

7.90

1/4

7.77

+3⁵ ± Pav

7.80

±

7.83

4+00²⁵ (B)

+5 S Pav	7.98
'A	8.0
+3	7.9
+6	8.9
cb	8.9
+2	9.1
S.L.	8.6
4+00 ²⁵ (C)	
S.L.	8.7
+8	9.2
cb	9.0
+4	8.2
'A	8.2
+2 ^A S Pav	8.10
E	7.94
+3 ^B E Pav	7.88
'A	7.86
S.L.	7.98
cb	8.3
+2	8.5
+3	8.3
N.L.	13.0
15N	16.2

4+30

15N	16.3
5N	15.9
N.L.	14.8
+4	13.4
cb	10.1
+1	9.4
+2	9.6
+6 N Pav	9.43
'A	9.34
E E Pav	9.12
'A	9.18
+1 ² S Pav	9.19
+5	9.4
cb	9.2
+3	10.1
S.L.	10.2
4+65	
S.L.	10.2
+5	9.7
+8	10.2
cb	10.1
+1 ³ S Pav	10.09
'A	10.05
+2 ³ E Pav	10.10
E	10.22
+4 ⁵ N Pav	10.51

A+65	158.55		
1/4		10.6	
+1		10.6	
+2 ^S		10.3	
cb		12.7	
N.L.		16.0	
10N		16.5	
T.P. 5.53	153.15	10.93	147.62
5+00			
10N		11.3	
N.L.		10.4	
cb		7.6	
+5		5.6	
1/4		5.6	
+0 ^S		5.8	
+1 ^S N Paw		5.50	
⊕		5.36	
+6 ³ ⊕ Paw		5.17	
1/4		5.16	
cb		5.16	
+0 ³ S Paw		5.16	
+4		5.2	
+4 ^S		4.9	
+6		5.0	
S.L.		6.4	

5+30			
5'S		7.0	
S.L.		6.4	
+4		5.4	
+5		5.6	
+9 ³ S Paw		5.50	
cb		5.49	
1/4		⊕ 4.4	
+0 ³ ⊕ Paw		5.45	
⊕		5.56	
+2 ³ N Paw		5.65	
+6		6.2	
1/4		6.0	
+1		5.8	
+4		6.5	
cb		7.0	
N.L.		10.5	
10N		10.9	
5+65			
10N		10.9	
N.L.		10.0	
cb		7.3	
1/4		6.4	
+1		6.6	
+5 N Paw		5.81	
⊕		5.72	

5+65	
+6 ^S ± Pav	5.70
1/4	5.72
eb	5.86
+0 ^S S Pav	5.90
+4 ^S	6.1
+5	5.8
S.L.	7.0
5'S	7.6
6+00	
5'S	7.6
S.L.	7.2
+5	6.1
+5 ^S	6.4
eb S Pav	6.09
1/4	5.95
+1 ^S ± Pav	5.95
±	5.99
+3 N Pav	6.06
+7	6.4
1/4	6.3
eb	7.5
+5	7.8
N.L.	9.3
10'N	10.0

18" Conc Pipe
Culvert 91' long at 6+07 on North
6+13 on South 5' in from N.L.

FL Nord	5.66
FL S end	8.70

Head walls 6" x 3' x 4'

6+30	
10'N	9.6
N.L.	8.7
+4	8.7
+7	7.9
eb	7.7
1/4	6.6
+4 ^S N Pav	6.13
±	6.05
+6 ± Pav	6.07
1/4	6.05
eb S Pav	6.19
+4	6.4
+5	6.1
S.L.	7.2
5'S	7.5

6+65

SL	6.1
+5	5.7
+6	6.1
eb	6.0
+0 ^S S Pav	5.99
1/4	5.85
+2 € Pav	5.85
€	5.87
+3 ^S N Pav	5.98
1/4	6.3
+3	6.3
+6 ^S	5.7
eb	6.0
+7	7.5
N.L	8.5
10'N	9.5
7+00	
10N	9.3
3N	8.8
N.L	7.4
+3	6.8
eb	6.3
+6	5.8
1/4	6.0
+3 ^S N Pav	5.78
€	5.78

7+00

+5 € Pav	5.65
1/4	5.66
+6 ^S S Pav	5.75
eb	5.8
+3	6.0
+4	5.8
SL	5.9
7+30	
SL	5.5
+5 ^S	5.4
+6	5.5
ob	5.6
+1 S Pav	5.56
1/4	5.47
+2 ^S € Pav	5.46
€	5.50
+4 N Pav	5.56
1/4	5.6
+2	5.4
eb	5.6
+5	5.7
+7	5.9
N.L	6.0
5'N	8.6
10'N	9.0

57

7+65

10N

8.5

6N

8.1

NL

6.0

+3

5.5

+5

5.8

cb

5.3

+3

5.4

+5

5.2

1A

5.4

+3 N Pav

5.40

+

5.34

+4.5 & Pav

5.32

1A

5.38

+6 S Pav

5.46

cb

5.5

+4

5.2

SL

5.1

8+00

SL

5.1

+6

4.8

+8

5.1

cb

5.1

+1.5 S Pav

5.15

1A

5.15

+3 & Pav

5.20

8+00

+

5.31

+4.5 N Pav

5.47

1A

5.4

+1

5.4

+2

5.2

cb

5.5

+4

5.3

+7

5.0

NL

5.8

3N

7.4

10N

7.8

8+30

10N

8.2

NL

7.4

cb

5.5

+5

5.5

1A

5.6

+2 N Pav

5.52

+

5.28

+3.5 & Pav

5.13

1A

4.97

+5 S Pav

4.84

cb

4.9

+3

4.8

+6

5.1

SL

4.8

8+65

S.L	3.7
+4	4.8
+8	4.1
cb	4.4
+25 ^S S Pav.	4.44
'A	4.62
+A b Pav	4.83
+	5.05
+6 ^S N. Pav	5.59
'A	5.6
+5	5.1
cb	5.1
+5	6.8
N.L	7.2
3 ^S N	8.6
4N	12.1
10N	12.8

$$\angle L = 41^{\circ}44'17'' \quad R=100 \quad L=73.85$$

8+86¹⁵ = BC

10N	13.3
6N	13.2
5 ^S N	9.7
N.L	6.7
+4	5.6

8+86¹⁵

cb	5.5
+5 N Pav	5.66
'A	5.45
+	4.87
'A	4.43
+A ^B S Pav	4.21
cb	3.3
+6	5.0
S.L	5.1

culvert of 5+99 on South
5+97 on North
24" conc pipes 48' long 3' not N.L.

FL Sand	10.03
FL Nord	11.39

9+22⁵² = C of Curve

5'S	5.5
S.L	6.5
+4	3.8
cb	4.0
+A ² S Pav	4.09
'A	4.16
+	4.52
'A	5.00

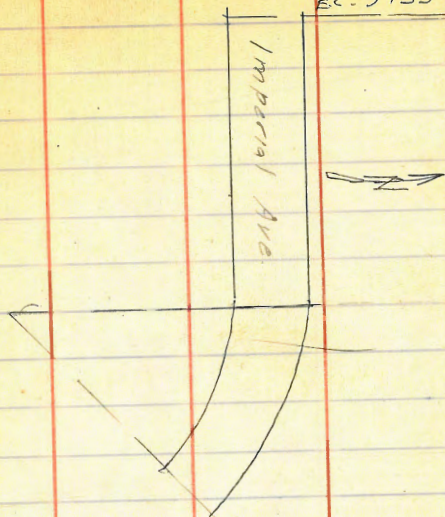
9+22⁵⁷

+6 ² N Pav	5.52
eb	5.6
N.L.	5.5
4'N	5.7
8 ^E N	8.3
9'N	11.9
9+59 = EC	
11'N	11.0
10 ^E N	7.9
7'N	5.7
N.L.	5.0
+8	4.9
eb	5.1
+4 ² N Pav	5.11
1/4	4.86
±	4.46
1/4	4.17
+2 ⁵ S Pav	4.10
eb	4.1
S.L.	3.9

60

EC. 9+59²²

Imperial Ave



9+79		
S.L.		4.2
+7		4.1
cb		4.2
+5	S Pav	4.10
1/4		4.18
⊕		4.45
1/4		4.80
+1	N Pav	4.82
+4		5.0
cb		4.7
N.L.		4.7
5'N		5.1
8 ^E N		7.9
9N		9.4
10+00		
11N		7.3
3N		4.0
N.L.		4.2
cb		4.4
+6 ^B	N Pav	4.60
1/4		4.56
⊕		4.26
+10 ^B	⊕ Pav	4.24
1/4		4.10
+12 ^B	S Pav	4.09
cb		4.2

61

10+00		
+5		3.9
S.L.		4.1
10+30		
S.L.		4.1
cb		4.2
+15 ^B	S Pav	4.20
1/4		4.20
+16 ^B	⊕ Pav	4.28
⊕		4.30
1/4		4.47
+10 ^B	N Pav	4.48
+6		4.1
cb		4.3
+7		4.4
N.L.		4.2
4'N		4.6
5 ^E N		6.0
6N		9.3
10+65		
7'N		9.3
4'N		7.8
3'N		6.1
N.L.		4.8
+3		4.2
cb		4.0

10+65		
cb + 6 ⁵	N Pav	4.33
1/4		4.30
+		4.21
+0 ⁵	± Pav	4.20
1/4		4.21
+2	s Pav	4.21
cb		4.2
+5		3.8
S.L.		4.7
11+00		
S.L.		4.5
+4		3.9
cb		4.0
+5	s Pav	4.12
1/4		4.02
+6 ⁵	± Pav	4.02
+		4.02
1/4		4.17
+1	N Pav	4.19
cb		4.0
+5		4.3
48		4.1
N.L.		4.5
2 ⁵ N		5.1
3N		8.6
6N		8.7

11+30	153.15	
7 ¹ N		8.8
3 ⁵ N		8.5
3N		6.0
N.L.		4.1
+3		3.4
cb		3.4
+1		3.6
+6 ⁵	N Pav	3.84
1/4		3.77
+		3.74
+0 ⁵	± Pav	3.74
1/4		3.82
+1 ⁵	s Pav	3.86
cb		3.8
+1		3.5
S.L.		4.0
T.P.	7.50	158.22
		2.43
		150.72
11+65		
S.L.		8.8
+7		8.8
cb		8.4
+1		8.3
+2		8.7
+6	s pav	8.64
1/4		8.64

11+65		158.22
1/4	1/4 Pav	8.55
1/4		8.64
+15	N Pav	8.70
+6		8.8
+6		8.5
cb		8.6
+8		8.8
NL		9.3
6'N		13.3
10'N		13.4
12+00		
10'N		13.2
5'N		13.2
9'N		10.0
NL		8.9
cb		8.2
+2		8.4
+6	N Pav	8.21
1/4		8.16
1/4	1/4 Pav	8.16
1/4		8.24
+15	S Pav	8.24
+4		8.5
cb		8.2
+2		8.2
+8		8.4

63

12+00		
5L		7.6
12+30		
5L		5.2
+2		7.2
+5		7.7
+5		8.0
+7		8.0
+7		7.8
cb		7.7
+2		8.1
+6	S Pav	8.00
1/4		7.90
1/4	1/4 Pav	7.64
1/4		7.53
+15	A Pav	7.55
+6		7.6
cb		7.4
NL		7.4
3'N		9.5
35'N		12.9
7'N		12.9
15'N		12.4

12 + 65

10N	11.6
9N	11.2
8N	8.9
2N	5.8
N.L.	6.0
cb	6.3
+2	6.6
+6 ³ N Pav	6.34
1/4	6.33
±	6.56
+0 ³ ± Pav	6.58
1/4	6.98
+1.8 S Pav	7.08
+6 ³	7.4
cb	7.1
+1	7.1
+2	6.7
+6	7.3
+7	7.0
+9	6.8
SL	6.0

12 + 77 48 = BC.

SL	6.9
+2	6.9
+3	7.1
+6	6.4
+7	6.7
+9	6.7
cb	7.1
+2	7.2
+4.2 S Pav	6.75
1/4	6.50
+6 ³ ± Pav	6.15
±	6.09
1/4	5.82
+0 ³ N Pav	5.83
+4.5	6.1
+5	5.9
cb	6.0
+4	6.0
N.L.	5.4
4N	5.9
12N	9.3
13N	11.9

13 + 11 ³⁰

10N	11.7
9N	12.3
8N	8.8
N.L.	6.3
+3	4.9
+8	4.2
cb	4.6
+4	4.7
+5	4.9
1/4	4.8
+15 N Pav.	4.68
+	4.92
+3 + Pav	5.04
1/4	5.24
+45 S Pav	5.62
cb	5.8
+2	6.1
+3	5.7
+7	5.8
+8	5.5
S.L.	5.8

13 + 45 ¹²

S.L.	4.6
+1	4.9
+6	4.6
+6.5	4.8
cb	4.5
+2 S Pav	4.41
1/4	4.04
+3.5 + Pav	3.83
+	3.65
+5 N Pav	3.45
1/4	3.5
+2.5	3.6
cb	3.2
+5	3.6
N.L.	6.1
3 ^E N	8.2
4N	12.5
10N	11.0
15N	7.2

65

13+78⁹⁴

5N	4.4
11N	5.9
10N	5.6
3N	8.1
N.L.	5.6
+7	2.1
eb	1.8
+5	2.5
1/4	2.4
+2 N Pav	2.42
±	2.40
+3 ⁵ ± Pav	2.52
1/4	2.78
+6 s Pav	3.26
eb	3.30
+4	3.3
+7	3.7
sL	4.0
14+12 ⁷⁶	
S.L	1.6
+1	2.1
+2	3.5
+4	3.4
+7	2.1
+9	2.3
eb	2.3

66

14+12⁷⁶

15822

eb+3 ⁵ s Pav	2.10
1/4	1.82
+5 ± Pav	1.47
±	1.29
1/4 N Pav	0.88
+4	1.2
+5	0.8
eb	0.7
+5	0.6
N.L.	3.1
5N	1.1
10N	4.1
T.P. 7.42	16525 0.39 157.83
14+12 ⁵⁸	
13N	9.5
11N	10.3
4N	7.0
2N	7.5
N.L.	6.7
+2	6.2
+6	6.3
+8	6.6
eb	6.3
+1	6.6
+4 N Pav	6.78

14+4658

1/4	6.95
+5 ^S E Paw	7.21
E	7.32
+7 S Paw	7.86
1/4	7.9
+3	8.1
+5 ^S	8.3
+6	8.1
eb	8.4
+2	9.1
+3	7.8
+6	5.4
S.L.	5.3

14+80⁴⁴ = E.C.

S.L.	2.9
+6	3.2
eb	7.0
+2	8.2
+4	7.4
+6 ^S	6.7
1/4	6.8
+5 S Paw	6.79
E	6.60
+6 ^S E Paw	6.11
1/4	6.06

14+80⁴⁴

165.25

67

eb	5.74
+10 ^S N Paw	5.73
+4	5.8
+8	5.2
N.L.	5.2
8 N	5.3

~~VOID~~
 Hd. bottom bolt Pale
 B.N. sur 1 imp. Merlin. 0.90 164.35

10.25 174.60 164.35

B.M. Hub. E.L. Marked on both. 2.61 171.99 171.90

Imperial Cont from P 51

	.41	.37
T.P.	3.01	161.49
2+53 ²⁸		158.45
S.L.	+1.8	163.2
+2	4.3	
+5	4.4	
+7 S Pav	3.98	157.43
cb	3.93	
+6 2	3.87	157.52
1/4	3.87	157.52
2	4.10	157.31
+0 ^S N Pav	4.13	157.28
+2 ^S	4.5	
+4	4.5	
+5	2.5	
1/4	2.4	
+3	2.3	
cb	4.1	
A.L.	8.1	153.3
15N	12.6	

161.41

2+56⁹⁸ = 4 on North

15N	13.0	
NL	8.3	153.1
cb	4.2	
+5	2.4	
1/4	2.5	
+3	2.7	
+3	4.5	
+7 N Pav	4.21	157.20
2	4.18	157.23
1/4	3.91	157.50
+1 ^S 2 Pav	3.88	157.53
cb	4.00	157.41
+3 S Pav	4.04	157.37
+5	4.4	
+8	4.4	
S.L.	+1.8	163.2
2+60 ⁶⁸		
S.L.	+1.8	163.2
+2	4.4	
+4	4.5	
+6	4.1	
+6 ³ S Pav	4.07	157.34
cb	3.99	157.42
+6 2 Pav	3.98	157.43
1/4	3.99	157.42
2	4.23	157.18

Imperial

2+60 ⁶⁸			
¢+0 ⁴	N Pav		
+4		4.26	
+5		4.6	
1/4		2.9	
+2		2.7	
cb		2.5	
N.L.		5.1	
1.5N		8.9	152.5
3+00		13.1	
1.5N		15.2	
N.L.		12.3	149.1
cb		8.2	
+3		6.3	
+4		6.7	
1/4		6.4	
+1 ⁵	N Pav	6.12	155.29
¢		6.00	155.41
+2 ⁵	¢ Pav	5.98	155.43
1/4		6.00	155.41
+4 ⁵	S Pav	6.06	155.35
cb		6.0	
+4		5.9	
+5		6.6	
+6		6.0	
+8		5.7	
+9		5.0	

3+00			
5L		4.6	156.8
3+30			
5L		7.0	154.4
+1		7.9	
+2		7.8	
+3		8.5	
+4		8.5	
+5		8.1	
+8		7.5	
cb		7.9	
+5	S Pav	7.47	153.94
1/4		7.40	154.01
+7	¢ Pav	7.38	154.03
¢		7.38	154.03
1/4		7.47	153.94
+0 ⁶	N Pav	7.51	153.90
+1 ⁵		7.9	
+5 ⁵		7.7	
cb		6.3	
+4		11.0	
N.L.		13.6	147.8
4W		15.7	
1.5N		16.0	
T.P.	7.13	8.69	152.80

Imperial.

3+65	.65		
	153.93		
15N	9.2		
AN	8.0		
1N	7.3		
NL	6.9	146.9	
+7	2.1		
+8	2.3		
eb	1.9		
+2 ^z N Pav	1.49	152.36	
'4	1.37	152.48	
+A E Pav	1.39	152.46	
E	1.36	152.49	
+5 ¹ S Pav	1.50	152.35	
'4	1.5		
+5	1.7		
+6	2.2		
eb	2.2		
+7	2.5		
S.L	0.6	153.2	

153.85

70

Seeb 47

A+D3³⁵ (A) = 4 on North

S.L	3.3	150.5
+1	3.9	
cb	4.1	
+4	3.9	
+7	3.1	
'A	3.2	
+5 ^z S Pav	3.25	150.60
E	3.29	149.56
+9 ^z E Pav	3.16	150.69
'A	3.16	150.69
cb	3.21	150.64
+2 N Pav	3.30	150.55
+6	3.8	
+7	3.7	
NL	5.7	148.1
LN	8.8	
12N	10.8	
15N	11.3	

A+D3³⁵ (B)

NL	5.7	148.1
+3	3.7	
+4	3.9	
+8 N Pav	3.38	150.47
eb	3.28	150.57
+6 ^z E Pav	3.26	150.59
'A	3.26	150.59

153.85

A+03³⁵ (B)

⊕	3.39	15046
+1 ^L 3 Pav	3.43	15042
+7	3.5	
1/4	3.8	
+2	4.4	
+5	4.5	
cb	4.4	
+4	4.0	
+9	4.0	
s.L.	3.2	1506

A+03³⁵ (C)

s.L.	4.1	149.7
+7	3.8	
cb	4.3	
+3	4.4	
1/4	3.9	
+1	3.5	
+2	3.7	
+6 ^S 5 Pav	3.55	15030
⊕	3.53	15032
1/4	3.35	15050
+0 ³ 1/2 Pav	3.35	15050
cb	3.32	15053
+2 ^L N Pav	3.42	15043
+6	3.9	
+7	3.7	

153.85

A+03³⁵ (C)

N.L.	5.7	1481
A+30		
15N	11.5	
7N	11.0	
3N	9.4	
N.L.	8.6	145.2
+6	4.8	
+7	5.0	
cb	4.9	
+1 ^L A/Pav	4.76	149.09
1/4	4.48	149.37
+2 ^S 1/2 Pav	4.42	149.43
⊕	4.46	149.39
+4 ³ 5 Pav	4.53	149.32
1/4	4.7	
+1	4.7	
+3	4.5	
+5	5.3	
cb	5.3	
+4	5.3	
s.L.	5.3	148.6

71

Imperial

153.85

4+65

S.L	6.3	147.6
cb	5.1	
+2	5.5	
+6 S Pav	5.41	148.44
1/4	5.38	148.47
cb & Pav	5.46	148.39
1/4	5.74	148.11
+1 ⁴ N Pav	5.86	147.99
+6 ^E	6.0	
+7	5.6	
cb	6.0	
+5	8.6	
N.L.	9.8	144.0
4N	11.1	
15N	11.7	
5+00		
15N	12.0	
7N	11.6	
N.L.	10.3	143.5
+5	9.8	
cb	6.5	
+2	6.3	
+4	6.6	
1/4	6.4	
+0 ² N Pav	6.29	147.56

153.85

5+00

cb	6.00	147.85
+6 ² & Pav	5.96	147.89
1/4	5.96	147.89
+2 ^E S Pav	5.91	147.94
cb	5.9	
+1	5.7	
+3	5.9	
+6 ^E	7.3	
S.L	5.5	148.3
5+30		
S.L.	7.8	146.0
+8	6.1	
+9	6.4	
cb	6.3	
+2 ² S Pav	6.20	147.65
1/4	6.18	147.67
+4 & Pav	6.16	147.69
cb	6.22	147.63
+5 ² H Pav	6.38	147.47
1/4	6.6	
+3	6.9	
+5	6.7	
cb	7.4	
+4	8.1	
N.L.	10.2	143.6

72

153.85

5+30

5A	11.6	
15N	11.8	
5+65		
15N	11.7	
3N	10.6	
N.L.	9.6	144.2
+5	8.2	
cb	7.8	
+3	7.1	
+5	7.3	
1/4	6.8	
+1 1/2 N Pav	6.59	147.26
1/2	6.47	147.38
+2 1/2 1/2 Pav	6.46	147.39
1/4	6.52	147.33
+4 1/2 S Pav	6.66	147.19
cb	6.9	
+1	6.9	
+2	6.6	
+5	7.4	
+8	8.4	
S.L.	8.5	145.4
5'S	8.4	

153.85

73

6+00

10'S	8.0	
S.L.	8.4	145.5
+4	8.1	
+9	7.0	
cb	7.1	
+3 1/2 S Pav	6.83	147.02
1/4	6.70	147.15
+5 1/2 Pav	6.69	147.16
1/2	6.70	147.15
+6 1/2 N Pav	6.83	147.02
1/4	6.9	
+3	7.1	
+4	7.0	
cb	7.7	
+3	8.3	
+9	8.6	
N.L.	9.0	144.8
6N	10.5	
13N	10.7	
15N	11.2	
Culverts at 6+07 1/2 on North ^{North} 1/2 S of NL		
18" conc pipe ^{6" 1/2 S} on ^{Southly} 6" N of S.L.		
FL. Nend	10.43	143.42
FL. send	9.50	144.35

153.85

6+30

15N	10.2	
3N	10.1	
N.L.	9.4	144.4
+4	8.7	
cb	8.1	
+4	7.3	
¹ / _A	7.1	
+1 ¹ / _A N Pav	6.90	146.95
+	6.81	147.04
+2 ⁶ / _A + Pav	6.81	147.04
¹ / _A	6.83	147.02
+4 ¹ / _A S Pav	6.96	146.89
cb	7.2	
+1	6.8	
+7	8.0	
S.L.	8.2	145.6
5's	8.1	
6+65		
5's	6.0	
1's	6.2	
S.L.	6.9	146.9
+3	6.8	
+8	6.6	
+9	6.9	
cb	6.8	
+3 ³ / _A S Pav	6.76	147.09

153.85

74

6+65

¹ / _A	6.66	146.19
+5 + Pav	6.63	147.22
+	6.64	147.21
+6 N Pav	6.72	147.13
¹ / _A	6.9	
+3	7.1	
+7	7.0	
cb	6.7	
+1	6.5	
+7	8.1	
N.L.	8.3	145.5
4'N	9.7	
8'N	10.2	
15N	10.4	
7+00		
15N	10.1	
6N	9.6	
1N	7.8	
N.L.	7.6	146.3
cb	6.9	
+3	6.7	
¹ / _A	6.6	
+0 ² / _A N Pav	6.55	147.30
+	6.41	147.44
+2 ¹ / _A + Pav	6.42	147.43
¹ / _A	6.45	147.40

153.85

7+00		
+4 ¹ S Paw	6.53	147.32
eb	6.8	
+1	6.6	
S.L.	6.6	147.2
7+30		
S.L.	6.3	147.5
+8	6.2	
eb	6.3	
+3 ² S Paw	6.36	147.49
1/4	6.28	147.57
+5 ¹ E Paw	6.27	147.58
⊕	6.27	147.58
+6 ² N Paw	6.37	147.48
1/4	6.4	
+6	6.2	
eb	6.4	
N.L.	6.3	147.5
5N	9.2	
12N	9.8	

Imperial.

153.85

75

7+65		
10N	9.2	
7N	8.6	
3N	7.1	
N.L.	6.5	147.3
+8	6.1	
eb	6.2	
+3	6.1	
+4	6.2	
1/4	6.2	
+1 N Paw	6.21	147.64
⊕	6.08	147.77
+2 ³ E Paw	6.09	147.76
1/4	6.12	147.73
+3 ² S Paw	6.21	147.64
eb	6.2	
+2	5.9	
S.L.	5.9	148.0
8+00		
S.L.	5.8	148.1
+8	5.6	
eb	5.9	
+3 ² S Paw	5.90	147.95
1/4	5.91	147.94
+4 ¹ E Paw	6.00	147.85
⊕	6.06	147.79

153.85

8+00		
4 +6 ^E N.Pav	6.25	147.60
1/4	6.2	
+3	6.2	
+4	6.0	
cb	6.3	
+7	5.7	
N.L.	6.0	147.8
5 ^N	8.2	
8+30		
5 ^N	8.1	
N.L.	8.2	145.6
+2	8.1	
+8	6.2	
cb	6.2	
1/4	6.3	
+0 ² N.Pav	6.28	147.57
4	5.98	147.87
+2 ^L 4 Pav	5.90	147.95
1/4	5.68	
+3 ^E S.Pav	5.60	148.25
cb	5.6	
S.L.	5.4	148.4

153.85

76

8+65		
S.L.	4.9	148.9
+4	5.8	
cb	5.1	
+4 ^L S.Pav	5.24	148.61
1/4	5.35	
+5 ^E 4 Pav	5.63	148.22
4	5.73	148.12
1/4	6.31	
0 ^E H.Pav	6.40	147.45
+2	6.4	
+6	5.9	
cb	5.8	
+4	6.3	
+6	7.3	
N.L.	7.6	146.2
5 ^N	9.2	
5 ^E N	12.9	
15 ^N	13.4	
8+89 ²⁵ = B.C. see P 97		
15 ^N	12.5	
11 ^N	13.5	
7 ^N	12.9	
6 ^E N	10.8	
N.L.	6.8	147.0
+3	6.2	

153.85

8+89²⁵

eb	6.3	
+3 ⁵ N Pav	6.43	147.42
'A	6.10	147.75
+5 E Pav	5.69	148.16
E	5.59	148.26
'A	5.15	148.70
+3 S Pav	4.99	148.86
+6	4.0	
cb	4.2	
+5	4.9	
+8	6.1	
S.L.	5.8	148.0

Culvert at 8+98 on North 9+00 on South

S end 75' N of S.L. 24" conc Pipe
17' 30" Armo on North end.

N end 5' N of N.L. 22" long 30" dia conc pipe

FL S end	10.80	143.05
FL N end	12.4	141.4

9+26¹⁷ = c curve

S.L.	6.7	147.1
+1	6.7	
+6	4.5	
cb	4.7	
+6 ⁵ S Pav	4.79	149.06

153.85

9+25⁶⁷

'A	4.80	149.05
E	5.15	148.70
+3 ⁹ E Pav	5.24	148.61
'A	5.61	148.24
cb	6.27	147.58
+0 ³ N Pav	6.27	147.58
N.L.	6.2	147.6
G.N.	6.5	
10 ⁵ N	9.0	
11 N	12.8	
9+63 ¹⁹ = EC		
12 ⁵ N	11.9	
12 N	8.6	
7 N	5.6	
N.L.	5.7	148.1
+6	5.6	
cb	5.9	
+2 ⁹ N Pav	5.89	147.96
'A	5.50	148.35
+5 ⁷ E Pav	5.25	148.60
E	5.17	148.68
'A	4.89	148.96
+0 ⁵ S Pav	4.88	148.97
cb	4.8	
S.L.	4.7	149.1
2'S	4.5	

77

Imperial.

.85
153.93

9+63 ¹⁰ E.C.

7 1/2		6.0	
10'S		5.7	
TP	8.76	159.96	2.65
		160.04	151.28

20' rail rate south at 9+63

Alignment as per Map of West Hollywood.

9+80

5B		11.6	148.3
3B		11.2	
S.L.		11.2	148.7
cb		11.0	
+7	S Pav	11.00	148.96
1/4		11.01	
±		11.27	148.69
+0 ⁸	± Pav	11.31	148.65
1/4		11.60	
+2 ²	N Pav	11.72	148.24
cb		11.8	
+3		11.6	
N.L.		11.6	148.4
6N		11.6	
10 ⁵ N		14.4	
11N		17.2	142.8

159.96

78

10+00

15N		12.8	142.2
5N		11.0	
N.L.		11.2	148.7
cb		11.4	
+5 ¹	N Pav	11.47	148.49
1/4		11.39	
+6 ⁵	± Pav	11.14	148.82
±		11.11	148.85
1/4		10.96	
+0 ⁵		10.97	
cb		11.0	
+3		10.8	
+7		10.8	
S.L.		11.1	148.8
A S		11.4	
5S		12.0	148.0

10+30

5S		10.9	149.1
S.L.		11.7	148.2
+2		12.9	
cb		11.1	
+6 ²	S Pav	11.10	148.86
1/4		11.09	
±		11.15	148.81
+0 ⁸	± Pav	11.17	148.79

159.96

10+30

'A	11.30	
+2 ³ N Pav	11.39	148.57
cb	11.0	
N.L.	11.1	148.8
6N	11.4	
8N	12.7	
9N	16.3	
18N	17.6	142.4
10+6.5		
10N	16.1	143.9
5N	12.6	
N.L.	11.0	148.9
cb	11.0	
+5 ³ N Pav	11.22	148.74
'A	11.19	
+6 ² E Pav	11.10	148.86
E	11.10	148.86
'A	11.10	
+0 ² S Pav	11.10	148.86
cb	11.1	
+5	10.8	
+9	11.6	
S.L.	11.1	148.8

159.96

79

11+00

S.L.	11.4	148.5
+3	11.0	
cb	11.0	149.0
+6 ⁵ S Pav	10.98	148.98
'A	10.96	149.00
E	10.94	149.02
+0 ² E Pav	10.94	149.02
'A	11.09	148.92
+1 ² N Pav	11.09	148.87
+7	11.1	148.9
cb	11.0	149.0
+9	10.9	
N.L.	11.4	148.5
AN	11.3	
AN	15.3	
12N	16.2	143.8
11+30		
10N	15.9	144.1
AN	15.6	
AN	12.5	
N.L.	10.6	148.3
+2	10.2	
cb	10.4	149.6
+5 ³ N Pav	10.78	149.18
'A	10.70	149.26

Imperial.

159.96

160.00

11+30

+72 $\frac{1}{2}$ Pav

10.70

149.26

$\frac{1}{4}$

10.70

149.26

1/4

10.77

149.19

+1 S. Pav

10.78

149.18

e b

10.6

149.4

+2

10.6

+9

11.0

S.L.

11.3

148.6

B.M

9.33

150.71

Can't in Book 1300

Page 1.

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 $\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body

IMPROVED TABLES AND INFORMATION

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add connection found in column of connections. Degree of curve with a given T may be found by dividing tangent (or external), opposite T by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

37.3
20.7
80
52.15
32.85

5.930
7.067
1.863
7.067
4.800
1.863
6.741

ENGINEERING DEPARTMENT
CITY OF
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