

1298

LEVEL BOOK

No. 380 F

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CITY OF SAN DIEGO,
CALIFORNIA.

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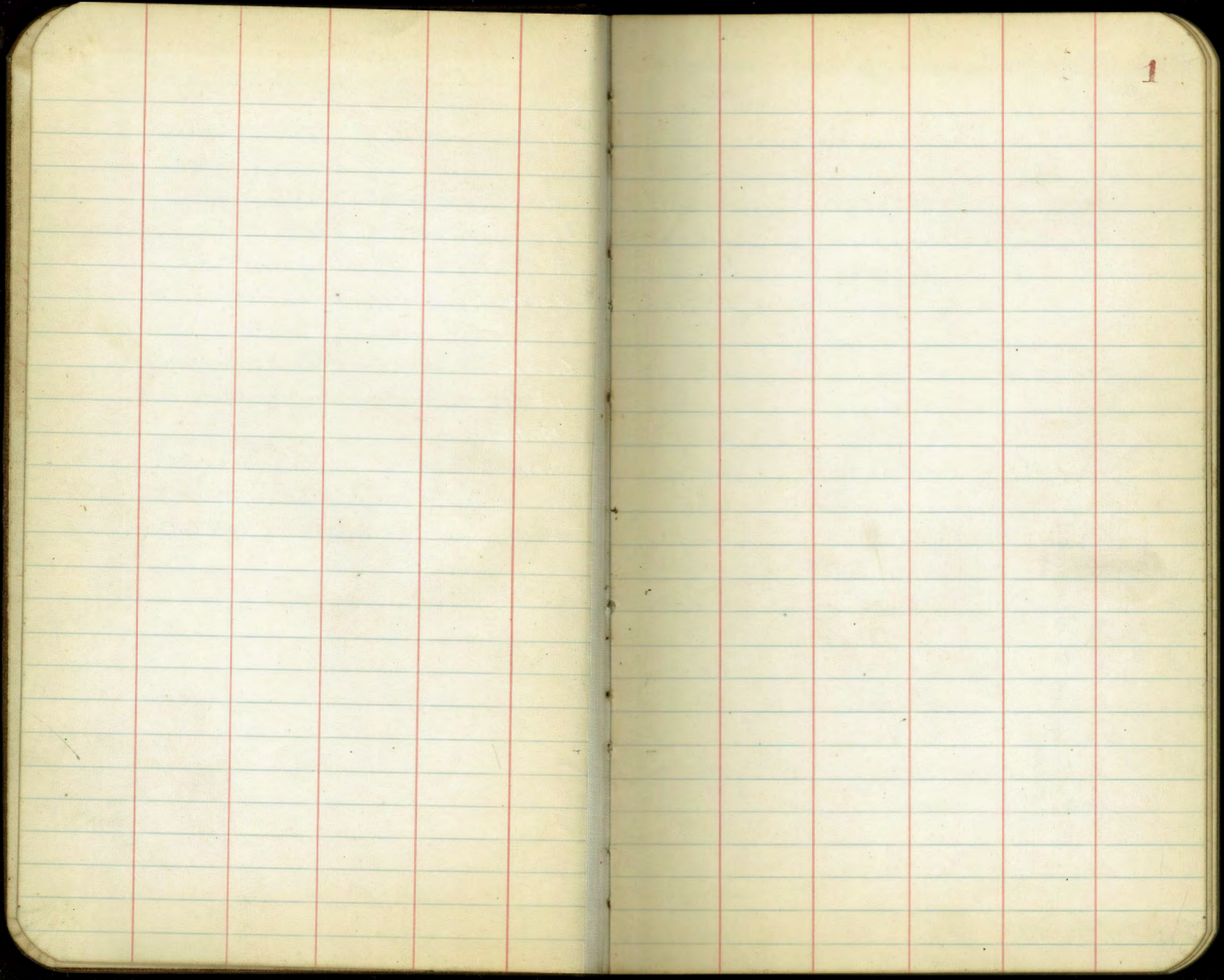
MICROFILMED

DEC 28 1964

The pointer indicated by 11/11/64

The points indicated by 7/1/11

Cross Sec.	Olyphant	Rosecrans to Willow	2
"	"	Locust Olyphant to Quimby	11
"	"	Poe Rosecrans to Willow	15
"	"	Evergreen Olyphant to Quimby	24
"	"	Rosecrans Newell to "	27
Topog.	Florida St	inlet and outlet 36" drain	36
X section	Tuna Lane	Soldado Terrace	48-52
X "	Alley	Block 59 city Hts	53-59
Location of Poles + Fire Hydrants Newton Ave. 16 th to			
13 th Location Poles + Fire Hydrants 13 th Newton to			
National			61
Cross Sec.	Alley Blk 18	Teralta 42 nd Van Dyke Orange + Polk	62
"	"	California St. Beech to Grape	66
"	"	Catalina + Navagansett intersection	76



1

11-17-28

X-section Olyphant Street

J.C. Bliss

Drebert

Rauver

Rosecrans to Willow.

70' wide

10' cbs

12 1/2' H/S

N 15.60

2

B.M. S.W. 7' + Prop. Marr. Rosecrans + Olyphant 6.68

+ 8.92

West edge

N 15.60

Section along Rosecrans paving which is 23' from W.L. Rosecrans

0+50

S	9.85	5.75	N	7.3	8.3
cb	9.89	5.71	cb	7.5	
1/2	9.95		1/4	7.5	
1/2	10.01	5.59	1/2	7.3	8.3
1/2	10.10		1/4	7.3	
cb	10.17	5.43	cb	7.2	
N	10.21	5.39	S	7.2	8.4

W.L. Rosecrans = 0+00

0+75

N	9.2	6.4	S	6.6	9.0
cb	8.5		cb	6.8	
7/8	7.5		1/4	6.8	
1/4	8.7		1/2	6.8	8.8
1/2	8.3	7.3	1/4	7.0	
1/4	8.0		cb	6.9	
cb	8.2		N	6.9	8.7
S	8.1	7.5			
	0+75		N	6.5	9.1
S	7.6	8.0	cb	6.6	
cb	7.7		1/4	6.5	
1/4	7.3		1/2	6.2	9.4
1/2	7.5	8.1	1/4	6.2	

Plotted 12-10-28. C.B.H.

B.M. at notch 2. Not recorded C.B.H.

π 15.60

cb	6.3	
S	5.7	9.9
0+86 - \$ 18 Garage 4' 5" x 5.1'		
Concrete floor at \$	6.06	9.54 ✓
	14.25	
S	4.9	10.7
cb	5.4	
1/4	5.7	
\$	5.5	10.1
1/4	5.9	
cb	6.4	
N	6.2	9.4
	14.50	
N	5.8	9.8
46	6.1	
1/4	5.5	
\$	5.4	10.2
1/4	5.2	
cb	5.0	
S	4.6	11.0
	14.15	
S	4.6	11.0
cb	4.8	
1/4	5.0	
\$	5.2	10.4

π 15.60

3

1/4	5.2	
cb	5.9	
N	5.5	10.1
	2+00	
N	4.9	10.7
cb	5.0	
1/4	5.0	
\$	4.8	10.8
1/4	4.5	
cb	4.2	
S	4.2	11.4
	2+25	
S	3.7	11.9
cb	3.7	
1/4	4.0	
\$	4.2	11.4
1/4	4.4	
cb	4.5	
N	4.3	11.3
	2+50	
N	3.6	12.0
cb	3.7	
1/4	4.0	
\$	3.8	11.8
1/4	3.7	

π 15.60

cb	3.3	
S	3.2	12.4
	2.75	
S	2.8	12.8
cb	2.7	
1/4	2.8	
⊕	3.1	12.5
1/4	3.4	
cb	3.0	
N	3.2	12.4
	3 + 100 = E.L. Locust - 70' wide 10' cbs 12/12/143	
N	2.7	12.9
cb	2.6	
1/4	2.5	
⊕	2.4	13.2
1/4	2.2	
cb	1.9	
S	2.0	13.6
	E cb	Locust
S	1.8	13.8
cb	1.8	
1/4	2.0	
⊕	2.4	13.2
1/4	2.4	
cb	2.6	

π 15.60

4'

N	2.4	13.2
	Locust	
N	2.0	13.6
cb	2.1	
1/4	1.6	
⊕	1.6	14.0
1/4	1.3	
cb	1.5	
S	1.7	13.9
	W cb . Locust	
S	0.5	15.1
cb	0.9	
1/4	1.1	
⊕	1.0	14.6
1/4	1.4	
cb	1.6	
N	1.6	14.0
	W.L. Locust = 0.100	
N	1.4	14.2
cb	1.3	
1/4	1.2	
⊕	1.1	14.5
1/4	1.0	
cb	0.5	
S	0.3	15.3

T. 15.00

T.P

+ 1289

- 0.51 15.09

T 27.98

0425

S 123 15.7

cb 12.1

1/4 123

¢ 12.6 15.4

1/4 12.6

cb 12.8

N 12.9 15.1

0450

28.0

N 11.8 16.2

cb 12.0

1/4 12.0

¢ 11.7 16.3

1/4 11.7

cb 11.7

S 11.3 16.7

0425

S 10.6 17.4

cb 10.6

1/4 10.5

¢ 10.9 17.1

1/4 10.8

T 27.98

5

cb 10.9

N 10.7 17.3

1400

N 8.8 19.2

cb 9.0

1/4 9.1

¢ 9.1 18.9

1/4 9.2

cb 9.2

S 9.3 18.7

1425

S 7.1 20.9

cb 7.1

1/4 7.1

¢ 7.2 20.8

1/4 7.0

cb 6.8

N 6.6 21.4

1450

N 1.4 26.6

cb 2.0

1/4 2.7

¢ 3.4 24.6

1/4 4.2

cb 4.1

∑ 27.98

S	4.6	23.4
T.P		-0.02 27.96
+12.83		

∑ 40.79

1475

S	11.3	29.5
cb	11.2	
H	10.6	
¢	9.8	31.0
H	9.0	
cb	7.6	
N	7.3	33.5

2400

N	0.3	40.5
cb	0.7	
H	1.5	
¢	1.7	39.1
H	2.3	
cb	3.1	
S	3.9	36.9

-0.05 40.74

∑ 53.80

2425

S	10.0	43.8
cb	9.3	

+13.06

∑ 53.80

6

H	8.6	
¢	8.0	45.8
H	7.7	
cb	7.2	
N	6.0	47.8

2460

N	4.0	54.8
cb	4.5	
H	0.2	
¢	0.9	52.9
H	2.1	
cb	3.0	
S	3.5	50.3

T.P. -0.37 53.43

+12.72

∑ 66.15

2475

S	9.5	56.7
cb	8.1	
H	7.2	
¢	6.6	59.6
H	5.6	
cb	5.1	
N	4.6	61.6

T.P. -0.28 65.67

+12.81

78.68

7868

3400 = E.L. Evergreen

N	8.9	69.8
cb	9.1	
1/2	7.5	
♀	10.1	68.6
1/4	11.0	
cb	12.2	
S	13.0	65.7
E. cb Evergreen		
S	10.7	68.0
cb	9.5	
1/2	8.2	
♀	7.0	71.7
1/4	6.0	
cb	5.5	
N	5.7	73.0
T.P		-0.00 78.68

+1301

791.69

♀ Evergreen

N	10.6	81.1
cb	10.7	
1/4	11.0	
♀	12.4	78.3
1/4	13.3	
cb	14.5	

91.69

7

S	15.7	75.0
♀ Locust + 20		
S	6.0	85.7
cb	5.1	
1/4	4.3	
1/2	5.7	
♀	6.3	85.4
1/4	6.1	
cb	5.4	
N	4.8	86.9
B.M. N.W. Block Corner Evergreen + Olives 1.2.3 90.46		
W.L. Evergreen = 0 + 00		
N	1.2	80.5
cb	1.8	
1/4	2.6	
♀	3.1	88.6
1/4	3.1	
1/2	1.6	
1/4	1.8	
cb	3.5	
S	4.5	87.2
T.P		-0.02 91.67

+12.92

7104.65

104.65

0431

S	9.7	95.0
cb	7.5	
14	9.0	
¢	9.3	95.4
14	8.5	
cb	8.9	
N	8.2	96.5

0450

N	14	103.3
cb	1.6	
14	2.1	
¢	2.8	101.9
14	4.1	
cb	4.1	
S	4.1	100.6

T.P.

-0.09 104.56

+1268

117.24

0475

S	8.7	108.5
cb	9.6	
14	8.9	
¢	8.0	109.2
14	6.6	
cb	5.6	

117.24

8.

N	5.3	117.9
T.P.		-0.11 117.13

+1298

130.11

+100

N	11.2	118.9
cb	11.6	
14	12.2	
¢	13.0	117.1
14	14.1	
cb	15.0	
S	15.1	115.0

+1225

S	7.5	122.6
cb	8.2	
14	7.7	
+3	6.3	

¢	5.7	124.4
---	-----	-------

14	4.5	
----	-----	--

cb	4.0	
----	-----	--

N	3.6	126.5
---	-----	-------

T.P.

+13.16

+13.04

-0.23 129.88

Σ 143.04

1450

N	7.0	137.0
cb	8.7	
1/4	10.7	
¢	11.9	131.1
1/4	13.3	
+2.5	13.5	
+5	15.4	
cb	15.3	
S	14.4	128.6

1462

S	11.1	132.0
cb	11.9	
+2	11.6	
1/4	8.0	
+7.5	5.4	
¢	5.3	137.7
1/4	5.5	
cb	5.4	
N	5.3	137.7

1475

N	3.8	139.2
cb	4.6	
1/4	5.0	
¢	5.2	137.8
1/4	5.5	

Σ 143.04

9

+8	5.7	
+10	7.2	
cb	8.0	
S	8.4	134.6
2+00		
S	4.7	138.3
cb	4.5	
1/4	4.4	
¢	4.7	138.3
1/4	4.4	
cb	3.8	
N	3.4	139.6

1490 = 18' Stucco Garage With concrete apron
 that extends 5' into st. from N.L.
 Concrete floor at ¢. on N.L. 3.76 139.28
 Edge concrete apron at ¢ of Garage 3.89 139.15
 T.P. -0.22 142.82

+1307

Σ 155.89

2+03

N	8.4	147.5
cb	10.2	
+3	11.7	
+4	16.7	
1/4	17.0	
¢	17.1	138.8

π 155.89

1/4	169	
cb	170	
S	174	138.5
	2+17	
S	156	140.3
cb	152	
1/4	154	
+6	152	
+7	117	
¢	110	144.9
1/4	82	
cb	71	
N	61	149.8
	2+25	
N	50	149.9
cb	60	
1/4	75	
¢	101	145.8
+7	111	
+10	145	
1/4	145	
cb	143	
S	151	140.8
	what station	
S	130	142.9

π 155.89

10

cb	120	
1/4	115	
+3	113	
+5	98	
¢	77	148.2
+8	57	
1/4	48	
cb	37	
N	25	153.4
	2+75	
N	05	155.4
cb	17	
1/4	27	
¢	66	149.3
+6	87	
1/4	93	
cb	100	
S	115	144.4
	2+97	
S	85	147.4
cb	77	
1/4	62	
¢	48	151.1
1/4	34	
+10	23	

15589

cb	0.8	
N	+1.0	156.9
+100 = E.L. Willow - Paved		
N	1.7	154.2
+9.2 Trog cb	26.6	153.23
Gutter	3.48	152.41
1/4	4.03	
♀	4.85	151.04
+7 = Gutter	5.43	
Tp cb	4.63	151.26
1/4	5.7	
cb	7.0	
S	8.3	147.6
B.M. N.W.B.P. Willow & Olyphant - 3.28 152.61		

This BM in office Record BM Book 152.81
Also in Jorgenson BM Book.

11-19-28 X-section Locust-Olyphant
J.C. Bliss to Quimby - 70' wide
Drebert 10' cbs
Raney 17' 4" cbs

11

T.P. at Locust Olyphant		15.09
	+12.23	
	X	27.82
K.L. Olyphant = +100		
W		13.6 14.2
cb		13.8
1/4		14.1
♀		14.5 13.3
1/4		14.4
cb		14.7
E		15.0 12.8
E		15.3 12.5
cb		15.1
1/4		15.1
♀		14.6 13.2
1/4		14.5
cb		14.3
W		14.0 13.0
W		14.2 13.6
cb		14.7
1/4		15.0
♀		14.8 13.0
1/4		15.4

Plotted by T.G.H. 5-16-28
Book 420 x 1236
Ground line Chs at Olyphant
" " " 54' POC.
" " " low N.W. POC.
" " " low S.W. Quimby

+25
+50

T 27.82

cb	15.6	
E	15.8	12.0
	0+75	
E	15.5	12.3
cb	15.4	
1/4	15.4	
♀	14.9	12.9
1/4	14.6	
cb	14.5	
W	14.1	12.7
	14.0	
W	14.6	13.2
cb	15.1	
1/4	15.4	
73	14.6	
♀	15.4	12.4
1/4	15.4	
cb	15.7	
E	16.1	11.7
	14.25	
E	15.8	12.0
cb	15.7	
1/4	15.4	
♀	15.2	12.6
1/4	15.1	

T 27.82

12

cb	14.8	
W	14.4	13.4
	14.50	
W	13.8	14.0
cb	14.5	
1/4	15.0	
♀	15.0	12.8
1/4	15.0	
cb	15.6	
E	15.4	12.4
	14.75	
E	15.3	12.5
cb	15.3	
1/4	14.9	
♀	14.7	13.1
1/4	14.5	
cb	14.3	
W	13.9	13.9
	2400 E S L. P. C. K 70' W	
W	13.3	14.5
cb	13.5	
1/4	13.7	
E	14.0	13.8
1/4	14.1	
cb	14.4	

T 27.82

E		15.0	12.8
	S	cb	Poe
E		14.8	13.0
cb		14.6	
1/4		14.1	
£		14.1	13.7
1/4		13.7	
cb		13.1	
W		12.9	14.9
	£	Poe	
W		11.9	15.9
cb		12.1	
1/4		12.5	
£		12.8	15.0
1/4		13.0	
cb		13.5	
E		13.8	14.0
	A	cb	Poe
E		13.0	14.8
cb		12.5	
1/4		12.1	
£		11.7	16.1
1/4		11.3	
cb		10.9	
W		10.7	17.1

T 27.82

13

B. M. N. W. Prop. Hub	Poe	10.16	17.66
	N. L. Poe	20.00	
W		10.2	17.6
cb		10.5	
1/4		10.7	
£		11.2	16.6
1/4		11.6	
cb		12.0	
E		12.4	15.4
	0+25		
E		11.3	16.5
cb		10.9	
1/4		10.4	
£		9.9	17.9
1/4		9.4	
cb		8.9	
W		8.6	19.2
	0+50		
W		7.2	20.6
cb		7.6	
1/4		8.1	
£		8.6	19.2
1/4		9.3	
cb		9.8	
E		10.2	17.6

π 2782

0475

E	8.9	18.9
cb	8.4	
1/4	7.7	
♀	7.2	20.6
1/4	6.8	
cb	6.1	
W	5.6	22.2

1400

W	4.3	23.5
cb	4.8	
1/4	5.2	
♀	5.8	22.0
1/4	6.3	
cb	7.2	
E	8.0	19.8

1425

E	6.9	20.9
cb	6.3	
1/4	5.6	
♀	4.9	22.9
1/4	4.0	
cb	3.3	
W	2.7	25.1

1450

W	1.4	26.4
---	-----	------

π 2782

14

cb	1.9	
1/4	2.7	
♀	3.6	24.2
1/4	4.4	
cb	5.0	
E	5.6	22.2

1475

E	4.4	23.4
cb	3.6	
1/4	2.7	
♀	2.0	25.8
1/4	1.6	
cb	0.5	
T.O.		-0.69 27.13

+ 2.85

π 29.98

W		28.0
	2.0	
	0	
W	0.2	28.8
cb	0.8	
1/4	1.7	
E	2.1	27.3
1/4	3.5	
cb	4.3	

29.98

E 5.0 5.25.0
 B.M. N.W. Prop Hub Locust & Poe -12.32 17.66
 → 17.66

11-23-28 X-section Poe Street - Rosecrans
 J.C. Bliss
 Drebert to Willow - 70' Wide - 10' cbs 12" 1/45 **15**
 Ranner

B.M. S.W. 7' x Prop Mon Rosecrans & Poe 565
 +8.25 13.90
 W.L. Rosecrans = 0.00

s	7.8	61
cb	7.5	
14	7.4	
6	7.4	65
14	7.5	
+9.5 Flow ^{line} 8" Culvert	10.09	
cb	8.4	
N	7.7	62
N	7.4	65
cb	7.7	
14	7.4	
6	7.0	69
14	7.5	
cb	7.4	
s	7.2	67

Plotted 12-10-28
 SBH
 BM Notched
 what section

0+26

4x3' Culvert Box 19' from S.L.
 Top wall 7.44 6.46
 Flow line 12" Culvert 7.87 4.03

1390

0+50

S	6.9	70
cb	7.4	
1/4	7.3	
¢	7.3	66
1/4	7.2	
cb	7.1	
N	7.1	68

0+75

N	6.4	75
cb	6.3	
1/4	6.3	
¢	6.4	75
1/4	6.6	
cb	6.6	
S	6.7	72

1+00

S	6.3	76
cb	6.1	
1/4	5.9	
¢	5.8	81
1/4	5.7	
cb	5.5	
N	5.2	87

T 1390

1+25

N	4.7	92
cb	4.7	
1/4	5.1	
¢	5.3	86
1/4	5.3	
cb	5.5	
S	5.6	83

1+50

S	4.8	91
cb	4.8	
1/4	4.6	
¢	4.6	93
1/4	4.5	
cb	4.1	
N	4.0	99

1+75

N	3.1	108
cb	3.4	
1/4	3.7	
¢	3.9	100
1/4	4.1	
cb	4.7	
S	4.0	99

2+00

S	3.3	106
---	-----	-----

16

T 13,90

cb	3.4	
1/4	3.4	
¢	3.0	10.9
1/4	2.7	
cb	2.6	
N	2.7	11.5
+0.5 Concrete Driveway	1.91	11.99 ✓
	2+07	
Concrete Driveway at S.W.	3.03	10.87 ✓
	2+25	
N	1.3	12.6
cb	1.5	
1/4	1.9	
¢	2.2	11.7
1/4	2.6	
cb	2.8	
S - Concrete Walk	2.97	11.93
†		
	2+28	
Concrete Walk 1' North of N.L.	0.95	12.95
	2+50	
S	2.3	11.6
cb	2.2	
1/4	1.9	
¢	1.3	12.6

T 13,90

17

1/4	1.0	
cb	0.6	
N	0.3	13.6
T.P		-0.02 13.88
	+12.77	
	T 26.65	
	2+75	
N	1.20	14.6
cb	1.23	
1/4	1.27	
¢	1.32	13.4
1/4	1.40	
cb	1.43	
S	1.45	12.1
	3+00 = E.L. Locust	
S	1.36	13.0
cb	1.34	
1/4	1.30	
¢	1.25	14.1
1/4	1.20	
cb	1.19	
N	1.13	15.3
	W.L. Locust = 0+00	
¢	0.90	17.6
cb	0.75	

$\pi 26.65$

1/4	10.0	
¢	10.6	16.0
1/4	11.1	
cb	11.6	
S	12.0	14.6
	0+05	
S	11.0	15.6
cb	10.6	
1/4	10.1	
¢	9.8	16.8
1/4	9.3	
cb	8.8	
N	8.3	18.3
	0+50	
N	7.0	19.6
cb	7.3	
1/4	7.7	
¢	8.0	18.6
1/4	8.5	
cb	9.0	
S	9.5	17.1
	0+75	
S	8.0	18.6
cb	7.7	
1/4	7.5	

 $\pi 26.65$

18

¢	6.9	19.7
1/4	6.5	
cb	5.9	
N	5.4	21.2
	1+00	
N	3.5	23.1
cb	3.9	
1/4	4.4	
¢	4.8	21.8
1/4	5.3	
cb	5.7	
S	5.9	20.7
	1+25	
S	0.4	26.2
T.P.		-0.41 26.24
	1+236	
	π 38.60	
cb	12.7	
1/4	11.6	
¢	10.5	28.1
1/4	11.0	
cb	10.5	
N	10.0	28.6
	1+50	
N	4.5	34.1

T 3860

cb	4.2	
1/4	4.0	
q	4.6	34.0
1/4	5.5	
cb	5.4	
S	5.8	32.8
T.P		-0.44 38.16

+12.87

T 51.03

	+175	
S	11.6	39.4
cb	11.0	
1/4	10.3	
q	10.0	41.0
1/4	9.6	
cb	9.3	
N	8.5	42.5
	2+00	
N	2.0	49.0
cb	2.8	
1/4	3.5	
q	3.6	47.4
1/4	4.0	
cb	4.0	
S	4.4	47.6
T.P		-0.40 50.63

T 50.63

19

f 12.96

	T 63.59	
	2+25	
S	7.3	54.3
cb	7.4	
1/4	7.7	
q	7.4	54.2
1/4	7.8	
cb	7.4	
N	7.5	54.1
T.P		-0.11 63.43

+12.62

T 76.05

	2+50	
N	11.2	64.8
cb	10.7	
1/4	10.5	
q	10.6	65.4
1/4	10.8	
cb	10.9	
S	11.2	64.8
	2+75	
S	1.6	74.4
cb	1.0	
1/4	0.6	

76.05

♀	0.4	75.6
1/4	0.6	
cb	0.9	
N	1.4	74.6
T.P		-0.10 75.95
+1287		

88.87

3400 = E.L. Evergreen - ^{70' wide} _{10' obs} 124' 145

x	3.8	85.0
cb	3.5	
1/4	3.4	
♀	3.0	85.8
1/4	3.3	
cb	4.0	
S	4.7	84.1
Ecb Evergreen		
S	1.6	87.2
cb	1.3	
1/4	0.8	
♀	0.4	88.4
1/4	0.1	
cb	0.2	
N	0.1	88.7
T.P.		-0.23 88.59

+1251

101.10

101.10

20

♀ Evergreen

N	2.5	98.6
cb	2.7	
1/4	2.3	
♀	4.0	97.1
1/4	5.0	
cb	5.9	
S	6.6	94.5
T.P.		-0.29 100.81

+1290

113.71

Wcb Evergreen

S	10.7	103.0
cb	9.6	
1/4	8.2	
♀	7.3	106.4
1/4	6.8	
cb	6.1	
N	5.8	107.9
B.M. N.W. Prop. Hub Evergreen x Bee	-2.73	110.98
W.L. Evergreen = 0700		
N	2.7	111.0
cb	3.8	
1/4	4.3	
♀	5.2	108.5
1/4	6.1	

113.71

cb	6.8	
S	7.9	105.8
	0.25	
S	1.2	112.5
cb	0.6	
T.P.		-0.32 113.39

+130.2

126.41

1/4	12.5	
¢	11.4	115.0
1/4	10.1	
cb	9.7	
N	8.8	117.6

0.50

N	4.0	122.4
cb	4.5	
1/4	5.2	
¢	5.7	120.7
1/4	6.4	
cb	7.2	
S	8.0	118.4

0.75

S	3.0	123.4
cb	1.7	
1/4	0.9	

126.41

21

¢	0.2	126.2
T.P.		-0.12 126.29

+12.66

138.95

1/4	11.6	
cb	10.8	
N	10.0	128.9

14.00

N	3.4	135.5
---	-----	-------

cb	4.6	
----	-----	--

1/4	5.5	
-----	-----	--

¢	6.7	132.2
---	-----	-------

1/4	7.2	
-----	-----	--

cb	7.3	
----	-----	--

S	8.0	130.9
---	-----	-------

T.P.		-0.31 138.64
------	--	--------------

+12.45

151.09

S	10.5	140.6
---	------	-------

cb	9.6	
----	-----	--

1/4	8.4	
-----	-----	--

¢	8.8	142.3
---	-----	-------

1/4	8.1	
-----	-----	--

cb	6.7	
----	-----	--

N	5.7	145.4
---	-----	-------

T

\bar{x} 151.09

T.P.

+13.04

-0.62 150.47

 \bar{x} 163.51

1+50

N

82

155.3

cb

T.1

1/4

10.4

♀

11.4

152.1

1/4

12.5

cb

13.0

S

13.9

149.6

1+75

S

7.6

155.9

cb

6.4

1/4

5.2

♀

4.1

159.4

1/4

2.7

cb

1.2

N

0.4

163.1

T.P.

+12.64

 \bar{x} 175.76

-0.39 163.12

2+00

N

6.7

169.0

cb

7.8

1/4

9.0

 \bar{x} 175.76

22

♀

10.0

165.7

1/4

11.0

cb

12.5

S

13.7

162.5

2+25

S

6.1

168.0

cb

6.1

1/4

5.1

♀

3.6

172.2

1/4

2.7

cb

2.0

N

1.3

174.5

T.P.

-0.23 175.53

+10.83

 \bar{x} 186.36

2+50

N

6.6

179.7

cb

7.0

1/4

7.7

♀

8.6

177.7

1/4

9.2

cb

9.9

S

10.4

176.0

2+75

S

5.2

181.2

cb

4.4

186.36

23

1/4	4.2	
2	3.5	182.8
1/4	3.2	
cb	3.4	
N	3.2	183.1
2 + 96		
N	1.2	185.1
cb	1.5	
1/4	1.2	
2	0.8	185.5
1/4	1.4	
cb	2.5	
S	2.7	183.6

3 + 00 = E.L. Willow - Pared

S	7.3	179.0
Top cb	7.26	179.10
G	7.99	178.37
1/4	7.61	
2	7.31	179.05
1/4	7.15	
G	7.12	179.24
Top cb	6.37	179.99
N	5.9	180.5

B.M. S.W.B.P. Pac & Willow

-8.66 } 177.70

} 177.79

B.M. S.W.B.P. Pac & Willow

177.79

+ 0.53 178.12

T.P.

-13.31 164.81

+ 0.11 164.92

B.M. N.W. B.P. Willow & Olyphant

-12.28 152.64

Office Record, also Walkers. Book = 152.81

N.W. B.P. Willow & Olyphant

11-26-28

J.C. Bliss

Raney

Kierston

X-section Evergreen Olyphant

to Quimby - 70' wide

10' cbs

12 1/2 1/5

B. N. W. Black Cor Hub - Olyphant + Evergreen 90.46

+11.76 T 100.22

N. L. Olyphant = 0+00

W	11.8	90.4
cb	13.9	88.3
1/4	16.8	85.4
2	20.7	81.5
1/4	25.0	77.2
cb	29.3	72.9
E	32.1	70.1
0+25		
E	31.0	71.2
cb	28.1	74.1
1/4	23.4	78.8
2	19.0	82.2
1/4	15.2	87.0
cb	12.0	90.2
W	10.0	92.2
0+50		
W	8.3	93.9
cb	10.0	92.2
1/4	12.9	89.3
2	16.5	85.7
1/4	20.5	81.7
cb	24.8	77.4

Note - For cuts on lower side - slope continues about the same as on the Street

24

T 102.22

E	28.2	74.0
0+75		
E	26.3	75.9
cb	23.0	79.2
1/4	19.1	83.1
2	15.1	87.1
1/4	11.2	91.0
cb	8.1	94.1
W	5.6	96.6
1+00		
W	3.5	98.7
cb	6.3	95.9
1/4	9.6	92.6
2	13.2	89.0
1/4	17.2	85.0
cb	21.6	80.6
E	24.5	77.7
1+25		
E	23.0	79.2
cb	19.8	82.4
1/4	15.8	86.4
2	12.5	89.7
1/4	8.8	93.4
cb	4.7	97.5
N	1.6	100.6

Plotted - 12-11-28 C.B.H.
BM notches % no records

π 102.22

1450

W	0.7	101.5
cb	2.7	98.5
1/4	7.7	94.5
E	10.9	91.3
1/2	14.6	87.6
cb	19.0	83.2
E	21.7	80.5
1475		
E	20.5	81.7
cb	17.6	84.6
1/4	13.5	88.7
E	9.5	92.7
1/2	5.8	96.4
cb	1.8	100.4
T.P.		

+986

-023 101.99

 π 111.85

W	8.3	103.5
2+00 = S.L. Poe		
W	6.3	105.5
cb	8.9	102.9
1/4	12.0	98.8
E	17.3	94.5
1/2	20.9	90.9

 π 111.85

25

cb	24.5	87.3
E	28.0	82.8
A.L. Poe = 0+00		
E	26.4	85.4
cb	23.3	88.5
1/4	19.0	92.8
E	13.0	98.8
1/4	8.7	103.1
cb	4.1	107.7
W	1.0	110.8
0+25		
W	0.5	111.3
cb	3.9	107.9
1/4	7.6	104.2
E	13.0	98.8
1/4	18.0	93.8
cb	22.7	89.1
+5	24.5	87.3
+8	27.0	84.8
E	28.0	83.8
0+50		
E	31.5	80.3
cb	26.3	85.5
+5	24.6	87.2

111.85

1/4	229	88.9
♀	143	97.5
1/4	9.5	102.3
cb	4.3	107.5
W	1.1	110.7

1+25

W	2.8	109.0
cb	6.4	105.4
1/4	11.1	100.7
♀	16.0	95.8
40	19.6	92.2
1/4	21.6	90.2
cb	26.0	85.8
E	29.5	82.3

1+00

E	30.0	81.8
cb	27.0	84.8
1/4	21.7	90.1
♀	16.9	94.9
1/4	12.4	99.4
cb	7.5	104.3
W	3.5	108.3

1+25

W	4.8	107.0
cb	8.4	103.4

111.85

26

1/4	12.5	99.3
♀	16.6	95.2
1/4	22.0	89.8
cb	26.2	85.6
E	29.5	82.3

1+50

E	30.2	81.6
cb	26.2	85.6
1/4	21.6	90.2
♀	18.0	93.8
1/4	13.5	98.3
cb	7.4	102.4
W	6.2	105.6

1+75

W	4.6	107.2
cb	8.5	103.3
1/4	13.2	98.6
♀	17.9	93.9
1/4	22.3	89.5
cb	26.5	85.3
E	31.0	80.8

2+00 = S. L. Quimby

E	30.3	81.5
cb	26.3	85.5
1/4	21.2	90.6

T 11.85

11-26-28

J.C. Bliss

Romer

Kiernan

X-section Rosecrans Ave

Newell to Quimby - 100' wide

20' cbs

15' 1/2s

27

B.M. S.W. 7 1/4 Prop. Men-Rosecrans clyphant 6.68

+388

T 10.56

N.L. Newell = 0 + 66 1/2

£	16.5	95.3
1/4	11.7	100.1
cb	6.5	105.3
w	1.8	1100 ✓
B.M. N.W. Prop. Peet Evergreen	0.93	110.92
		110.98

E	32	7.0
cb	5.7	
+6	32	
+8	2.5	
+13	1.9	
+14	2.8	
+2	4.5	
To E. Rail	3.51	7.05
To W "	3.50	7.06
+18	4.4	
£	2.6	8.0
+2	2.0	
+7 - E edge paving	3.28	7.28
+4	3.24	
+12 W edge paving	3.35	7.21
cb	3.5	
+5	3.4	
+6	2.4	
w	2.0	8.6
	0 + 25	
w	2.1	8.5
+17	2.7	

Plotted 12-8-28 - CBH

Bench etc. Not at 7% recorded date
CBH

Note - West edge of paving on Rosecrans
is 23' East of W.L. Rosecrans. East edge is
of curbside
43' East of W. Line. West Rail is 55.7'
East of W. Line of Rosecrans and East
Rail is 5' from West Rail

T 10.56

18	3.7	
cb	3.7	
180 W edge paring	3.55	7.01
1/4	3.46	
+85 E edge paring	3.49	7.07
Q	2.3	8.3
+2	4.7	
W Rail-Top	3.70	6.86
E Rail-Top	3.59	6.87
+12	4.7	
1/4	2.8	
+2	2.0	
+7	3.4	
cb	4.0	
E	3.8	6.8
	+50	
E	3.5	7.1
cb	4.3	
+8	4.1	
+13	2.1	
1/4	3.0	
+3	4.8	
E Top Rail	3.89	6.67
W " "	3.89	6.67
+13	4.8	

T 10.56

28

Q	3.6	7.0
+3	2.8	
E edge paring	3.66	6.90
1/4	3.59	
W edge paring	3.77	6.79
cb	4.0	
+3	3.8	
+5	2.8	
W	2.5	8.1
	+100	
W	2.1	8.5
+14	3.4	
+15	4.0	
cb	4.2	
W-edge Paring	4.13	6.43
1/4	3.98	
E-edge Paring	4.02	6.54
+14	3.2	
Q	3.4	7.2
+2	5.3	
W Rail	4.21	6.35
E Rail	4.20	6.36
+13	5.1	
+14	4.1	
1/4	5.9	

T. 10.56

+3	2.5	
+7	3.7	
cb	4.4	
+10	4.8	
E	4.0	6.6
	1+30	
E	4.7	5.9
cb	4.4	
+10	4.0	
+13	3.1	
1/4	4.2	
+3	5.5	
E Rail	4.55	6.01
W ii	4.57	5.99
+14	5.6	
¢	3.9	6.7
+2	3.2	
+5	4.0	
E-edge Paving	4.35	6.21
1/4	4.31	
W-edge Paving	4.49	6.07
cb	4.4	
+5	4.0	
W	2.6	8.0

T 10.56

2+00 = S.L. Olyphant ^{70' wide} ^{10' obs} ^{12/20/44} 29

W	2.8	7.8
+15	3.7	
+16	4.4	
cb	4.6	
wedge paving	4.76	5.80
1/4	4.68	
E-e.p.	4.73	5.83
+13	3.6	
¢	4.2	6.4
+2	5.9	
W Rail	4.9✓	5.64
E "	4.9✓	5.64
+13	5.9	
1/4	4.7	
+3	4.5	
+6	4.4	
cb	4.8	
E	4.8	5.8
	5 cb olyphant	
E	4.6	6.0
cb	5.1	
+9	4.5	
+13	3.2	
1/4	4.3	
+2	6.0	

π 10.56

E Rail	4.99	5.57
W "	4.99	5.57
+13	5.9	
♀	4.2	6.4
+5	4.6	
E-c.p.	4.82	5.74
1/4	4.73	
W-c.p.	4.83	5.73
cb	4.6	
+5	3.7	
W	3.1	7.5

♀ Olyphant

W	3.3	7.3
+15	4.3	
cb	4.8	
W-c.p.	4.98	5.58
1/4	4.88	
E-c.p.	4.93	5.63
♀	4.5	6.1
W Rail	5.16	5.40
E "	5.14	5.42
1/4	4.8	
cb	5.1	
E	5.7	4.9

π 10.56

30

N cb Olyphant

E	5.8	4.8
cb	5.5	
+8	4.7	
+12	3.4	
1/4	4.6	
+2	6.3	
E Rail	5.33	5.23
W "	5.36	5.20
+13	6.3	
♀	4.2	6.4
+4	4.6	
E-c.p.	5.09	5.47
1/4	5.05	
W-c.p.	5.16	5.40
cb	5.0	
+7	4.6	
W	3.8	6.8

N, L Olyphant

W	4.1	6.5
+6 = Edge of 24x6 strip of sidewalk	3.89	
Shot on 1 edge of strip of walk	3.88	6.48
cb	5.0	
W-c.p.	5.22	5.34
1/4	5.12	

T 10.56

E-e.p.	5.12	5.44
+10	5.0	
♀	4.4	6.2
+3	6.4	
W Rail	5.42	5.14
E "	5.40	5.16
+13	6.4	
14	4.7	
+3	3.2	
+6	4.8	
cb	5.5	
E	5.8	4.8
	0.60	
E	6.0	4.6
cb	5.6	
+8	5.1	
+13	3.9	
14	5.0	
+2	6.6	
E Rail	5.64	4.92
W "	5.65	4.91
+13	6.6	
♀	5.0	5.6
+2	4.4	
+5	5.2	

T 10.56

31

E-e.p.	5.27	5.29
14	5.27	
W-e.p.	5.47	5.09
cb	5.3	
W	3.7	6.9
T.P.		-5.55 5.01
	+4.68	
	T 9.69	
	1.00	
N	2.9	6.8
cb	4.8	
W-e.p.	4.78	4.91
14	4.60	
E-e.p.	4.63	5.06
+13	3.7	
♀	4.1	5.6
+1	5.9	
W Rail	5.04	4.65
E "	5.02	4.67
+13	6.1	
14	4.1	
+3	2.9	
+7	4.5	
cb	5.2	
E	5.3	4.4

9.69

1450

E	5.7	4.0
cb	4.9	
+10	4.6	
+14	3.7	
1/4	4.4	
+v	6.2	
E Rail	5.23	4.46
W "	5.24	4.45
+13	6.1	
E	4.5	5.2
+v	3.8	
E - e.p.	4.77	4.92
1/4	4.74	
W - e.p.	4.88	4.81
cb	4.8	
W	4.1	5.6

1475

60x30 - Culvert box 5' W of W edge of paving

Shot on 16" Culvert flowline 6.15 3.54

2+00 = 5.6 P.O.C.

W	3.7	6.0
cb	4.5	
W - e.p.	5.03	4.66
1/4	4.92	
E - e.p.	4.75	4.74

9.69

32

113	4.1	
Q	4.7	5.0
+v	6.4	
W. Rail	5.45	4.24
E "	5.46	4.23
+13	6.3	
1/4	4.8	
+3	4.1	
+10	5.1	
cb	5.5	
E	5.7	4.0
S - cb. P.O.C.		
E	6.4	3.3
cb	5.5	
+1	5.2	
+1v	3.4	
1/4	4.7	
+v	6.5	
E Rail	5.53	4.16
W "	5.52	4.17
+1v	6.5	
Q	4.1	5.6
E - e.p.	5.02	4.67
1/4	4.98	
W - e.p.	5.08	4.61

969

cb	42	
W	34	63
Flowline 16" Culvert located on S 1/2 cb + 10 + 21 West		
50 ft E.L. Rosecrans	9.43	
\$ Poe		
W	3.5	62
+14	3.8	
cb	46	
W-e.p.	529	440
1/4	515	
E-e.p.	519	450
+10	4.7	
+12	3.8	
1/2	4.8	4.9
+2	66	
W Rail	564	405
E "	563	406
+13	66	
1/4	4.0	
+3	32	
+10	5.2	
cb	5.7	
E	6.3	3.4

969

33

N. cb Poe		
E	64	3.3
+15	60	
Flowline 8" Culvert under Rosecrans		
Small ditch dug for Culvert outlet	8.15	1.54
cb	5.5	
+12	3.5	
1/4	5.1	
+2	6.2	
E Rail	575	394
N "	574	395
+13	6.7	
1/2	4.5	5.2
E-e.p.	540	429
1/4	5.34	
W-e.p.	548	421
cb	5.6	
+2 Flowline 8" Culvert	6.80	2.89
+10	2.6	
W	4.2	5.5
N.L. Poe = 0400		
W	3.4	6.3
+10	2.7	
+17	3.9	
cb	5.5	
W-e.p.	5.51	4.18

969

114	5.36	
E-e.p.	5.43	4.26
+10	5.0	
♀	4.7	5.0
+2	6.9	
W-Rail	5.79	3.90
E- "	5.79	3.90
+13	6.8	
14	4.6	
+5	3.6	
+8	4.8	
cb	5.6	
E	6.2	3.5
	0+50	
E	6.0	3.7
cb	5.7	
+7	5.2	
11	3.5	
14	4.8	
+2	6.8	
E Rail	5.82	3.87
W "	5.81	3.88
+13	6.8	
♀	4.8	4.9
+3	4.3	

969

31

F-e.p.	5.32	4.37
14	5.27	
W-e.p.	5.44	4.25
cb	5.0	
+3	4.2	
W	3.4	6.3
	1700	
W	3.6	6.1
e 13	4.3	
cb	4.6	
W-e.p.	5.33	4.36
14	5.18	
E-e.p.	5.20	4.49
♀	4.6	5.1
+2	6.5	
W Rail	5.70	3.99
E "	5.72	3.99
+13	6.5	
14	4.8	
+3	3.6	
+11	5.0	
cb	5.5	
E	5.5	4.2

969

1450

F	5.6	4.1
cb	5.4	
+7	5.3	
+12	4.0	
1/4	4.7	
+2	6.5	
E Rail	5.59	4.10
W "	5.58	4.11
+13	6.5	
♀	4.1	5.6
E-e.p.	5.06	4.63
1/4	5.00	
W-e.p.	5.15	4.54
cb	4.6	
W	3.5	6.2
2+00 = S.L. Quimby		
W	3.7	6.0
cb	4.6	
W-e.p.	5.03	4.66
1/4	4.86	
E-e.p.	4.90	4.79
♀	4.2	5.5
+2	6.4	
W Rail	5.45	4.24
E "	5.45	4.24

969

35

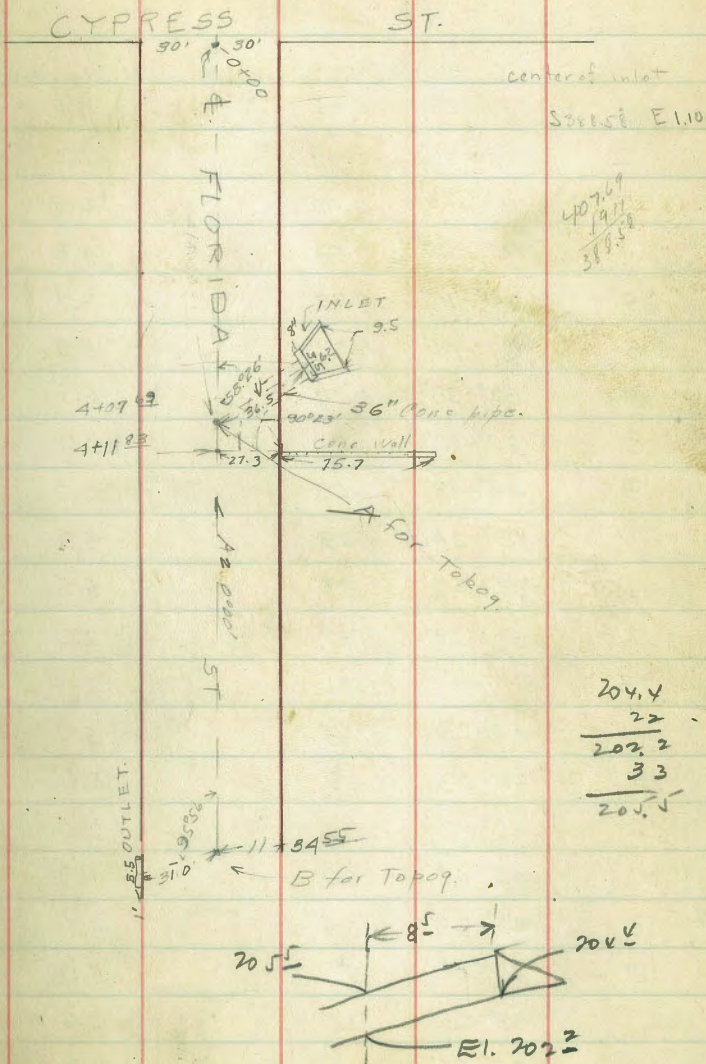
+13	6.4	
1/4	5.0	
+2	4.3	
+12	6.0	
cb	6.2	
E	5.6	4.1
B.M. S.W. 7' x Drop Man - Pic + Reservoirs -409		
		5.60
		5.65

Location & Topog on Storm Drain (Walker) south of Cypress.

Dec 21-28

Loudon
Isbell
Moran

B.M.	+	x	-	EI.
	0.08	261.61		261.53
T.P.	0.17	248.87	12.91	248.70
T.P.	0.22	236.22	12.87	236.00
T.P.	0.08	223.37	12.91	223.31
B.M.	1.77	212.51	12.65	210.74
Top Headwall inlet.		4.28		208.23
FL inlet		8.09		204.42
Apron smooth inlet		7.22		205.29
"A" for topog.		5.24		207.27
Top cb opp. con. Wall		5.40		207.11
Top W. end con Wall		3.87		208.64
Top. con. Wall 24.1'-E. of West End		3.35		209.16
Top. con. Wall E. end.		3.16		209.35
Top cb. opp. Inlet.		4.76		207.75
T.P.	2.25	201.93	12.83	199.68
T.P.	3.88	198.76	7.05	194.88
'B' for topog		5.25		193.51
FL outlet.		10.36		188.40
top Headwall outlet		4.67		194.09
B.M.	12.98	223.72		210.74
T.P.	12.78	236.43	0.07	223.65
T.P.	12.87	249.25	0.05	236.38
T.P.	12.91	262.12	0.04	249.21
B.M. Beginning		0.59		261.53



Stadia Topog around inlet storm
Drain on Florida south of Cypress.

Station	Az.	Stadia	V.A.	rod	H.I	Elev.
"A"	See P 36.					207.27
Ht. inst = 5.2.					242.5	
Inst of A oriented on \pm Florida Az $0^{\circ}00'$ North.						
1	51°-30'	0.45		4.4		209.1
2	54°-30'	0.44		7.2		206.3
3	64°-23'	0.45		6.8		205.7
4	72°-20'	0.45		4.8		207.7
5	69°-17'	0.78		3.7		205.8
6	67°-40'	0.78		5.9		206.6
7	62°-38'	0.78		6.5		207.0
8	60°-12'	0.78		4.0		208.5
9	48°-43'	1.28		2.7		209.8
10	49°-24'	1.29		5.0		207.5
11	52°-25'	1.33		5.5		207.0
12	53°-17'	1.35		2.0		210.5
13	43°-42'	1.41		2.4		210.1
14	44°-23'	1.43		5.0		207.5
15	46°-03'	1.49		5.0		207.5
16	46°-46'	1.51		2.0		210.5
17	42°-48'	1.60		1.9		210.6
18	42°-38'	1.56		4.7		207.8
19	40°-57'	1.52		5.0		207.5
20	38°-25'	1.38		2.6		209.9
21	25°-55'	1.20		3.3		209.2
22	15°-54'	1.12	+2°-32'			212.2
23	25°-42'	0.65		3.2		209.3

Station	Az.	Stadia	Vert. L	Rod	H. I.	Elev.
Ht. Inst. 5.2	Inst. at "A" Oriented on to Florida				212.5	
24	39°-25'	0.77		4.0	208	208.5
25	58°-52'	0.31		4.6		207.9
26	71°-46'	0.35		5.3		207.2
27	97°-14'	0.28		4.8		207.7
28	83°-50'	0.33		4.4		208.1
29	92°-05'	0.66	/	4.5		208.0
30	91°-44'	1.01		3.4		209.1
31	90°-22'	1.40	+2°-09'			212.6
32	91°-09'	1.80	+2°-49'			216.6
33	76°-52'	1.84	+3°-14'			217.7
34	70°-58'	1.40		0.6		211.9
35	76°-25'	0.94		4.1		208.4

Tobag around Outlet

"B" set P 36						193.51
Ht. Inst = 5.2	Inst at "B" oriented on to Florida. Az 0°00'				2198.7	
1	319°58'	0.45		4.4		194.3
2	320°45'	0.43		6.4		192.3
3	330°57'	0.36		4.6		194.1
4	292°14'	0.23		4.8		193.9
5	284°10'	0.28		7.4		191.3
6	267°34'	0.18		7.0		191.7
7	270°51'	0.15		5.6		193.1
8	246°45'	0.24		4.8		193.9
9	259°47'	0.28		6.9		191.8

Station	AZ	Stod	Vert L	Pod	H.I	Elev
10	276°42'	0.34		7.9		190.8
11	279°31'	0.36		6.2		192.5
12	268°24'	0.37		9.2		189.5
13	256°21'	0.39		8.9		189.8
14	247°07'	0.42		5.6		193.1
15	250°50'	0.62		5.6		193.1
16	262°06'	0.59		8.5		190.2
17	271°20'	0.63	+1°45'	^{4P} 3.0		192.4
18	261°00'	1.21		6.7		192.0
19	259°31'	1.18		9.6		189.1
20	255°00'	1.15		9.3		189.4
21	251°56'	1.16		6.4		192.3
22	253°44'	1.00		6.0		192.7
23	256°28'	0.96		9.3		189.4
24	257°40'	0.93		8.0		190.7
25	246°05'	0.65		7.8		190.9
26	242°47'	0.66		5.7		193.0
27	227°55'	0.43		5.2		193.5
28	231°57'	0.40		7.3		191.4
29	234°54'	0.36		5.2		193.5
30	194°25'	0.22		6.0		192.7
31	242°29'	1.52		7.9		190.8
32	244°00'	1.55		9.9		188.8
33	246°01'	1.61		10.7		188.0
34	248°26'	1.68		8.0		190.7

Station	AZ	Stad	Vert L	Pod	H.Z	Elev	Hor. Dist.
35	237°00'	195		9.7	196.7	189.0	
36	236°25'	190		11.7		187.0	
37	236°07'	182		11.5		187.2	
38	234°04'	180		8.5		190.2	
39	223°13'	203		9.5		189.2	
40	223°23'	208		12.5		186.2	
41	223°33'	215		12.2		186.5	
42	223°38'	217		9.5		189.2	
43	203°57'	220		10.8		187.9	
44	203°17'	270		13.8		184.9	
45	203°69'	268	+0°35'	^{HP} 8.0		188.2	
46	203°09'	256		10.8		187.9	
47	196°33'	230		9.2		189.5	
48	197°42'	233		10.6		188.1	
49	198°45'	233		9.7		189.0	
50	201°00'	201	+0.55'	^{HP} 7.0		193.2	
51	199°22'	201		10.7		188.0	
52	195°07'	203		6.4		192.3	
53							
"C"	102°25'	0.56	+11°43'			204.6	
H.Z. 5.1	Inst at "C"	0.56	-11°44'		209.7	193.5	54
1	336°58'	0.70	-8°25'			193.6	68
2	3°20'	0.50	-10°15'			195.8	45.5
3	30°42'	0.43	-7°57'			198.8	42
4	50°00'	0.32		3.3		206.4	

H.I. = 209.7

41

Station	AZ	Stad	Vert L	Rod	Vertical Hts	Elev	Hn. Dist
5	263°43'	0.30		12.4		197.3	
6	269°47'	0.36	-12°15'		7.4	197.2	35'
7	235°28'	1.06	-6°20'		11.6	193.0	
8	233°03'	1.01	-7°22'		12.5	191.8	
9	216°32'	0.83	-5°42'		8.2	196.4	
10	212°18'	1.66	-3°58'		11.4	193.2	
11	215°12'	1.72	-4°54'		14.6	190.0	
12	224°14'	1.80	-4°20'		13.4	191.2	
13	239°06'	1.47	-4°49'		12.3	192.3	
14	217°44'	3.10	-3°05'		16.6	188.0	
15	226°37'	3.18	-0°25'	4 P 10.0	2.3	192.3	
16	232°30'	2.93	-1°35'		8.1	196.5	
17	232°24'	2.76	-3°00'		14.4	190.2	
18	246°09'	2.60	-2°34'	4 P 1.0	11.6	192.0	
19	255°02'	2.30	-2°11'	4 P 5.0	8.8	190.8	
20	255°13'	2.38	-2°10'		9.0	195.6	
21	257°05'	2.54		9.9		199.8	
22	262°37'	2.07	-2°51'		10.3	194.3	
23	267°37'	2.28		7.5		202.2	
24	278°46'	2.13		5.0		204.7	
25	283°44'	1.68	-3°50'		11.2	193.4	
26	300°15'	1.69	-3°33'		10.2	194.4	
27	293°32'	1.19	-4°30'		8.1	196.5	
28	201°24'	0.86		11.5		198.2	
29	194°50'	2.10	-2°04'	4 P 3.0	7.5	194.1	

Dec 22-28
Landon
Lohell
Wierman.

BPSE
Chastworth
& Elliot.

X Sec. Azalea St. from
Wisteria Dr to 100' beyond Nord.
13' cbs 34' Roadway.

42

B.M. 1.55 129.68 128.13

TP 2.14 116.82 1300 116.68

TP 0.04 103.76 1310 103.72

Sec on NL Wisteria Prod. = 0+00 on East.
= 0-292 on West.

wL 7.1 96.6

+5 8.4

+8 backwalk 7.99 95.77

cb topcb 8.22 95.54

cb gut. 9.04 94.72

1/4 Pav 8.82

± ✓ 8.77 94.99

1/4 ✓ 8.90

cb Pav 9.32 94.44

+9 ^{end NE return.}
gut 9.55

+4 topcb 9.06 94.70

+7 backwalk 9.02

EL 9.00 94.76

0+00

EL 9.0 94.7

cb 9.2

1/4 9.2

± 9.1 94.7

1/4 8.4

+2 8.5

+3 9.5

+4 8.5

cb 8.5

Azalea

0+00	103.76		
w.L.	7.6	96.2	
0+15			
w.L.	8.4	95.4	
eb	8.7		
+7	8.8		
1/4	10.9		
+2	10.6		
+3	8.6		
±	8.9	94.9	
1/4	8.9		
+6	8.3		
eb	8.4		
E.L.	8.7	95.0	
0+37			
E.L.	9.2	94.5	
eb	10.1		
1/4	10.0		
+3	10.0		
±	14.5	89.3	
+4	16.6		
+7	9.4		
1/4	9.2		
eb	8.9		
w.L.	8.7	94.9	

Azalea

43

0+51	103.76		
w.L.	9.2	94.6	
+1/2	11.0		
eb	12.6		
+5	17.5		
1/4	16.6		
+2	15.2		
+6	15.6		
±	18.7	85.1	
+3	18.9		
+5	16.6		
+7 ^E	18.7		
1/4	18.3		
+6 ^S	17.4		
eb	16.3		
+3	15.4		
+7	16.2		
E.L. Cor retain. wall.	15.9	87.9	
T.P. 0.44	91.96	12.29	91.52
0+57			
10E	4.0		
E.L.	4.2	87.7	
+4	4.2		
+8	6.1		
+9	5.4		
eb	7.2		
1/4	8.1		

0+57	91.96		
±	7.5	84.4	
'A	6.6		
+5	4.2		
eb	2.9		
w.L.	+1.7	93.7	
0+63			
w.L.	1.7	90.2	
cb	6.4		
'A	7.8		
+5	8.9		
±	9.0	82.9	
'A	9.1		
cb	9.1		
+3	8.5		
EL	4.3	86.7	
10E	4.1		
12'E at 0+57 bottom back door	3.56	88.40	✓

0+73	91.96		
15E	4.0		
8E	4.2		
EL	7.8	84.1	
+3	9.2		
cb	10.6		
'A	10.8		
±	10.5	81.4	
'A	9.8		
cb	8.2		
w.L.	5.5	86.4	
10W	4.2		
0+92			
15W	8.1		
w.L.	9.8	82.1	
cb	11.5		
'A	12.7		
±	13.6	78.3	
'A	13.6		
cb	13.9		
EL	12.2	79.7	
5E bet. wall	11.0	80.9	
5E top wall	9.4	82.5	✓
15E	8.4		
18E bottom back door on E.L. ± to st. pen wall at 0+89 top	6.76	85.20	✓
	9.91	82.05	

1+11	91.96		
20E		11.1	
E.L.		14.8	77.1
T.P.	0.39	82.43	99.2
			82.04
+A		5.9	
cb		6.3	
1/4		6.2	
±		5.9	76.5
1/4		5.3	
cb		3.9	
w.L.		2.3	80.1
75W		0.2	
1+18			
13W		0.8	
8W		2.0	
w.L.		5.5	76.9
+6		4.0	
cb		4.8	
1/4		6.0	
±		7.0	75.4
1/4		7.5	
cb		7.4	
E.L.		6.2	76.2
20E		2.7	

1+24¹² = boundary on East

	82.43		
20E		3.3	
E.L.		7.3	75.1
+11		8.5	
cb		8.2	
1/4		8.2	
±		7.8	74.6
1/4		7.1	
cb		5.0	
w.L.		2.8	79.6
13W		0.4	

1+36⁶⁰ = boundary on West.

15W		+0.4	
w.L.		1.8	80.6
cb		3.8	
1/4		5.6	
±		7.6	74.8
1/4		9.2	
+5		10.4	
cb		9.9	
+8		10.2	
E.L.		9.1	73.3
20E		5.4	

1+50

82.43

20E	8.7	
FL	11.6	70.8
+6	12.1	
+8	13.9	
+9	11.9	
cb	11.2	
1/4	9.0	
±	6.7	75.7
1/4	4.5	
cb	2.6	
w.L	0.4	82.0
13W	+2.2	

1+75

10W	+3.6	
w.L	+1.6	84.0
cb	1.8	
1/4	4.1	
±	6.6	75.8
1/4	8.8	
cb	11.5	
FL	15.1	67.3
2E	16.9	
6E	18.5	
7E	14.8	
20E	13.5	

2+00

82.43

20E	18.0	
18E	18.3	
17E	22.0	
19E	18.3	
5E	17.3	
E.L.	15.7	66.7
cb	11.3	
1/4	8.6	
±	6.3	76.1
1/4	4.2	
cb	2.2	
w.L	+1.0	83.4

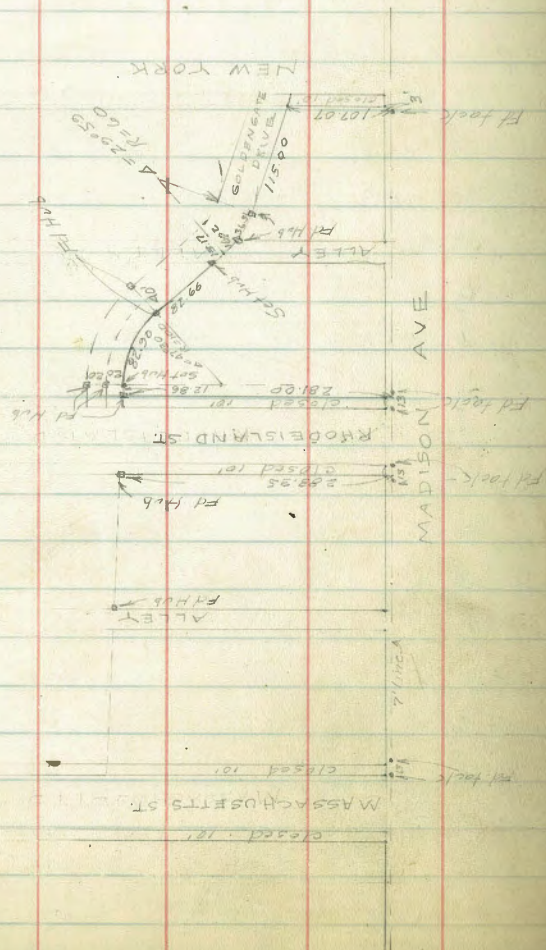
2+25

10W	+1.7	
w.L	0.9	81.5
cb	3.7	
1/4	5.1	
±	7.4	75.0
1/4	9.3	
cb	11.8	
E.L.	15.8	66.6
5E	17.3	
20E	19.6	
T.P.	12.31	94.70
	0.04	82.39
T.P.	3.86	95.09
	3.47	91.23
BM	S.E. Homer & Chatsworth	11.52
		83.57
		83.53

46

Dec 29-28
London
Isbell
Morgan.

Survey of Blocks 30, 31 & 32
Univ. Hts to replace Hubs on south
Line of Golden Gate Drive.



Elevations top of 36" C.P. in Florida St.
B.M. SW Cor Myrtle & Florida 198.01
Myrtle 60' St. 4.63 ^{BS} _{FS} 202.64 ^{HI}

Tp Pipe N.H. of Myrtle 6.16 196.44 ✓
M.H. & " " 7.33 195.31 ✓

Sample B.M. 3.19 201.70

Tp Pipe 1455' S of L. of Myrtle 7.13 194.07 ✓

105' S. & of Cork Outlet.

Tp Pipe 329' S of S. of Myrtle 8.77 192.43 ✓

M.H. Upper Pipe F.L. 12.24 188.96 ✓

" Lower Pipe Top of Pipe. 12.44 188.36 ✓

Bill Bliss
Joe Duermitt
J. Jacobszoon
3/6/99

X Section Tuna Lane Saledad Terrace

BM	3.69	249.03	245.34	sewer stub 120' E of 1011
check	onssewer Stub Mn. Hole. Tied West 62	868	240.35	1/2 Malden Collingswood Drive
T.P.	5.82	245.72	913.	239.90

Set BM 8.05 237.67 SW Top Hydrant Loring & Tuna Lane

of 0004 N =

Sec. A. See sketch Page 48 (copy)

S. line	5.2	240.5
+10	5.6	240.1
+20	4.8	240.9
+30	5.5	240.2
+45 Bottom	6.9	238.8
+95 Top N line	4.6	241.1
	Sec. B 11.3	379
-37 th N line	3.1	242.6
-30	4.6	241.1
-20	4.6	241.1
-10	5.5	240.2
-8	5.1	240.6
S line	5.2	240.5
	Sec. C 32.6	
S.	5.2	240.5
+8	5.1	240.6
+10	5.6	240.1
+17	5.1	240.6
+20	4.2	241.5
+30	3.7	242.0

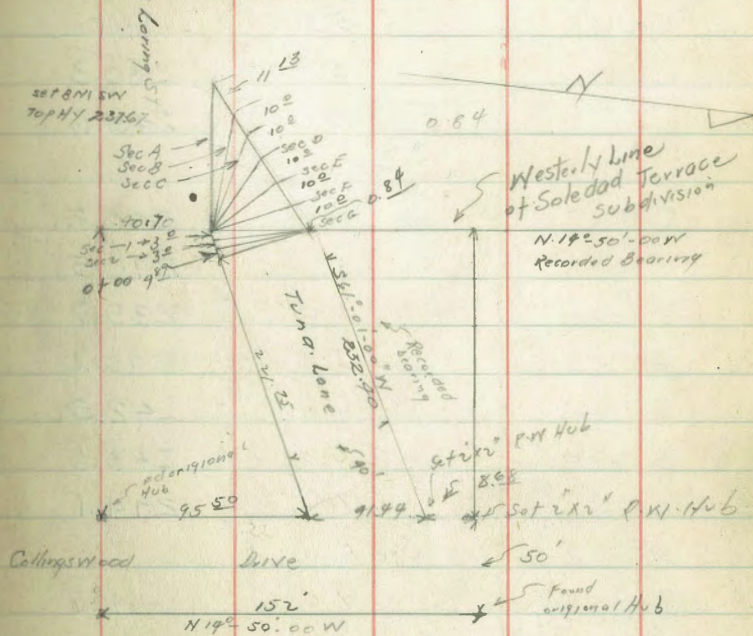
Plotted A-28-29-C.B.H.

6/9
10:89075

48

1195wood drive to Malden D.E. See page 20 Sewer Code Book 139. Walker's Notes

Collingswood Drive



6/13 4106

	+	HI 245.72	-	Elev
+32.6 N Line			2.5	243.2
			Sec D	30.2
-30.2 N Line			2.2	243.5
-18			3.4	242.3
-16			5.0	240.7
-8			5.5	240.2
-5			5.4	240.3
S Line			5.2	240.5
			Sec E	31.3
S Line			5.2	240.5
+3			5.2	240.5
+5			6.0	239.7
+10			5.7	240.0
+19			2.8	242.9
+25			2.2	243.5
+31.3 N Line			1.8	244.1
			Sec F	35.1
-35.1 N Line			1.0	244.7
-20			2.7	243.0
-18			3.1	242.6
-10			5.7	240.0
-5			6.3	239.4
-3			5.2	240.5
S Line			5.2	240.5
			Sec G	40.60
S Line			5.2	240.5

	+	HI 245.72	-	Elev
			7.3	240.3
			+5	239.3
			+9	239.7
			+12	240.5
			+18	242.7
			+30	243.9
			+40 ⁵⁶ N Line	244.5
			Sec 1	38 ⁴⁰ 41 ⁴⁰
			N Line = 00	244.6
			+15	243.7
			+24	242.5
			+30	240.3
			+38	239.2
			+41 ⁴⁰ S Line	240.3
			+56	239.3
			Sec 2	90.8
			-56	237.3
			-40 ⁸⁰ S Line	238.8
			-30	240.2
			-24	242.7
			-15	243.7
			N	244.6
			0100 Seosketch	
			N	244.6
			+15	243.6
			+24	242.8

	HZ.	-	5/6/1
	245.72		
+27		50	240.7
+35		6.2	239.5
+40 Sline		7.3	238.4
+42		8.1	237.6
+45		10.2	235.5
+55		14.9	230.8
	0125		
-60		18.8	226.9
-50		13.9	231.8
-40 Sline		8.5	237.2
-37		6.3	239.4
-25		5.1	240.6
-23		2.2	243.5
-10		2.0	243.7
N		2.0	243.7
	0150		
N		2.3	243.4
+10		2.3	243.4
+21		2.3	243.4
+23		4.5	241.2
+25		5.6	240.1
+35		6.4	239.3
+40 Sline		10.1	235.6
+43		11.5	234.2
+20		19.4	226.3

	HZ.	-	5/6/1
	245.72		
	0175		
-60		19.7	226.50
-45		13.3	232.4
-40 Sline		11.6	234.1
-35		8.8	236.9
-32		6.6	239.1
-29		5.8	239.9
-29		5.1	240.6
-20		3.4	242.3
-10		3.0	242.7
N		3.0	242.7
J.P.	1.29	245.77	1.19
			244.53
	0188		
N		3.0	242.8
+2		3.3	242.5
+10		3.7	242.1
+15		4.0	241.8
+20		4.0	241.8
+22		5.1	240.7
+29		5.7	240.1
+40 Sline		12.8	233.0
+45		14.4	231.4
+60		19.8	226.0
+65		21.4	224.4
	1700		
-65		21.3	224.5
-55		18.6	227.2

+	HZ 245.77	-	Elev
-40 S Line		12.5	233.3
-37		11.9	225.9
-28		5.8	240.0
-20		5.2	240.6
-15		4.4	241.4
-2		3.9	241.9
N		3.3	242.5
	111		
N		3.3	242.5
r		4.0	241.8
+15		4.6	241.2
r-0		5.0	240.8
+27		5.4	240.4
+40 S. Line		12.2	233.6
+48		15.6	230.2
+60		19.2	226.6
	1125		
-60		19.5	226.3
-50		15.6	230.2
-40 S. Line		12.0	233.8
-27		5.5	240.3
-20		5.2	240.6
-15		4.9	240.9
-2		4.4	241.4
N		3.8	242.0

+	HZ 295.77	-	Elev
		1150	
		5.2	240.6
		5.9	240.4
		5.9	239.9
		6.2	239.6
		6.2	239.6
		6.5	239.3
		10.3	235.5
		15.2	230.6
		18.5	227.3
	1143		
		21.1	224.7
		18.1	227.7
		15.4	230.4
		12.3	233.5
		10.9	235.4
		8.3	237.5
		7.2	238.6
		5.7	240.1
		5.7	240.1
		5.5	240.3
		5.4	240.4
	1175		
		5.6	240.2
		5.5	240.3
		5.7	240.1
		11.6	234.2

	H.I. 295.77	Elev
+40 S. line	14.5	231.3
+50	17.8	228.0
+60	20.4	225.4
+65 Bottom	21.3	224.5
	187	
-60 Bottom	20.4	225.4
-50	19.0	226.8
-40 S. line	16.3	229.5
-32	14.3	231.5
-27	11.7	234.1
-18	5.6	240.2
-10	5.4	240.4
N	5.4	240.4
	2100	
N	5.7	240.1
+10	5.6	240.2
+15	5.8	240.8
+17	5.7	240.1
+28	14.7	233.1
+33	14.5	231.3
+40 S. line	15.6	230.2
+50	18.0	227.8
+55 Bottom	19.8	226.0
	2121 75	
-47	15.6	230.2
-43	18.3	227.5

	H.I. 245.77	Elev
-40 S. line	18.3	227.5
-37	14.9	230.9
-30	13.2	232.6
-25	11.6	234.2
-15	5.5	240.3
-10	5.5	240.3
N	5.7	240.1
	Sec. A. 2121 25 = 2132 ²⁰ on N	
N	5.7	240.1
+10	5.5	240.3
+13	5.5	240.3
+17	6.0	239.8
+25	10.6	235.2
+28	12.6	233.2
+35	14.4	231.4
+41 ⁴ S. line	18.3	227.5
+43	18.3	227.5
+49	16.0	229.8
TP	7.79 247.74	5.82 239.95
	check out on Starting 8 M. Sewer Stub & Callingswood	2.40 245.34

Bill Bliss
Ducemit
Jacobson
Kierman

X. Section Alley Block 59 City Blk
Between Wilson + 36th, University + Whitman

April 2, 1929

+ H.I - Elev

BM 3.89 364.50 360.61 NWBR Univ + Wilson

Section Curbside of Univ

E-15 Topcb	5.30	359.20
E-15 Gutter	5.65	359.85
E on Topcb	5.15	359.35
" in Gutter at PC Curb Return	5.97	359.03
E Alley Produced North	5.92	359.08
W in Gutter at PC of Cb Return	5.33	359.17
W Top Cb	5.03	359.47
W+15 Topcb	4.98	359.52
W+15 Gutter	5.37	359.13

0100. Skine of Univ on Paving

W Topcb	4.89	359.61
G	4.97	359.53
E	5.18	359.32
G	5.06	359.44
E Topcb	4.94	359.56

0106

E	5.0	359.5
E	4.8	359.7
76	4.7	359.8
78	4.5	360.0
7X	4.7	359.8

0125

W	4.5	360.0
---	-----	-------

Plotted 4/26-29 - CBH

No sketch
that can see

+	HZ 36950	-	Elev
15		4.8	359.7
Φ		4.8	359.7
13		4.7	359.8
17		4.8	359.7
E		5.2	359.3
		0750	
E		5.3	359.2
15		5.1	359.4
Φ		4.9	359.6
16		4.6	359.9
N		4.6	359.9
		0775	
N		5.7	358.8
16		5.3	359.2
Φ		5.5	359.0
18		5.5	359.0
E		5.8	358.7
		1400	
E		5.8	358.7
16		5.8	358.7
Φ		6.1	358.4
12		5.9	358.6
N		5.7	358.8
		1425	
N		5.8	358.7
17		5.7	358.8

+	HZ 36950	-	Elev
		5.8	358.7
		5.8	358.7
		5.8	358.7
		1450	
		6.2	358.3
		6.1	358.4
		6.0	358.5
		6.1	358.4
		1466 Single Garage on West ✓	
		12 in Alley concrete floor 5.91	358.59
		1475	
		6.0	358.5
		6.1	358.4
		6.2	358.3
		6.6	357.9
		6.6	357.9
		2100	
		6.5	358.0
		6.5	358.0
		6.7	357.8
		6.6	357.9
		6.5	358.0
		6.7	357.8
		2108 Single Garage on East ✓	
		7.4 back dirt floor 6.8	357.7

54
1430 Blk on West
12 in Alley
1450 S. End
1460
1480

	H.I		Elev
	364.50		
	2415		
W	7.2		357.3
ϕ	6.8		357.7
E	6.9		357.6
	2433		
E	7.4		357.1
ϕ	7.2		357.3
W	7.5		357.0
	2443	Single Garage on East	
W	7.9		356.6
ϕ	7.9		356.6
E	7.8		356.7
	7 th Back concrete floor ϕ	7.97	357.03 ✓
T.P.	1.20	357.79	7.91 356.59
	2450		
E	1.2		356.6
ϕ	1.3		356.5
W	1.1		356.7
	2463		
N	1.6		356.2
+5	1.7		356.1
ϕ	1.7		356.1
+5	1.6		356.2
E	1.4		356.4
	2475		
E	1.5		356.3

	H.F	
	357.79	
	1.9	355.9
ϕ	2.0	355.8
+3	2.0	355.8
+5	2.2	355.6
W	2.3	355.5
	2485	
N	2.6	355.2
+4	2.6	355.2
+6	2.3	355.5
ϕ	2.2	355.6
+7	2.1	355.7
E	1.4	356.4
	3700	
E	2.6	355.2
ϕ	2.7	355.1
+3	2.6	355.2
+7	2.5	355.3
W	2.7	355.1
	3708	
W	3.1	354.7
+4	3.2	354.6
ϕ	3.1	354.7
+3	2.9	354.9
+8	3.1	354.7
E	3.3	354.5

	HZ 357.79	
E	3725	
E	3.3	354.5
W	3.4	354.4
±3	3.4	354.4
E	3.4	354.4
	3740	
E	3.3	354.5
±5	3.7	354.1
±	3.8	354.0
±3	3.5	354.3
E	3.8	354.0
	3753	
E	3.8	354.0
±	4.0	353.8
±3	3.9	353.9
W	4.0	353.8
	3766	Single Garage on West
	0.8 Back Wood floor	± 3.22 ✓
W	4.2	354.57
±5	4.1	353.6
±	4.1	353.7
E	4.2	353.6
±	4.4	353.4
	3773	
E	4.5	353.3
±	4.3	353.5
±5	4.2	353.6
W	4.1	353.7

	HZ 357.79	
	3783	
W	4.3	353.5
±	4.3	353.5
±8	4.3	353.5
E	4.8	353.0
	4700	
E	4.9	352.9
±3	4.6	353.2
±	4.6	353.2
±5	4.5	353.3
N	4.6	353.2
	4710	
W	4.8	353.0
±5	4.9	352.9
±	5.0	352.8
	47	352.9
±6	5.0	352.8
E	5.2	352.6
	4725	
E	5.3	352.5
±5	5.3	352.5
±	5.5	352.3
W	5.3	352.5
	4737	
W	5.6	352.2
±5	5.7	352.1

+ HI
357.79

Elev

+8	6.0	351.8
♀	5.7	352.1
+5	5.8	352.2
E	5.5	352.3
9+51 N End Db/ Garage on East		
Lip 1.3 Back concrete floor	5.8	351.97 ✓
E	5.8	352.0
+4	5.5	352.3
♀	5.7	352.1
+8	5.7	352.1
W	5.8	352.0
4+56 Single Garage on West		
1.3 Back concrete floor	♀ 5.35	352.44 ✓
4+65		
W	5.9	351.9
♀	5.9	351.9
E	5.9	351.9
9+71 S End Db/ Garage on East		
Lip 1.3 Back concrete	5.89	351.90 ✓
E	5.9	351.9
+4	5.8	352.0
+7	5.7	352.1
♀	5.8	352.0
+5	5.7	352.1
W	5.8	352.0

+ HI
357.79

Elev

57

4+80	6.0	351.8
♀	6.2	351.6
+8	5.9	351.9
♀	6.0	351.8
+5	6.1	351.7
+6	5.8	352.0
E	5.8	352.0
9+8 N End Db/ Garage on East		
Lip 1.4 Back concrete	6.15	351.64 ✓
4+85		
E	6.2	351.6
+5	6.1	351.7
♀	6.1	351.7
+5	6.1	351.7
W	5.9	351.9
5+00 S End Db/ Garage on East ✓		
W	6.3	351.5
+4	6.4	351.4
♀	6.4	351.4
+4	6.5	351.3
E	6.4	351.4
Lip 1.3 Back concrete	6.25	351.54 ✓
5+08		
E	6.8	351.0
+9	6.8	351.0
♀	6.5	351.3

	+	HZ	-	Elev
		357.79		
T5			6.7	351.1
N			6.7	351.1
		5125		
W			6.3	351.5
T4			6.6	351.2
T8			7.0	350.8
Φ			6.9	350.9
T5			7.0	350.8
E			7.~	350.6
		5133	Single Garage on West	
	4.5 Back Drift floor	Φ	6.8	351.0 ✓
		514.0		
E			7.4	350.4
T4			7.3	350.5
T6			7.0	350.8
Φ			6.9	350.9
T6			7.1	350.7
N			7.1	350.7
		5149	Walk on West 2" wide	
	1 st m alley	Φ	7.39	350.40
		5155		
N			7.6	350.2
T6			7.5	350.3
Φ			7.4	350.4
T5			7.4	350.4
E			7.6	350.2

	+	HZ	-	Elev
		357.79		
		5175		
			8.1	349.7
			7.9	349.9
			8.0	349.8
			8.1	349.7
		5190		
			8.9	349.4
			8.7	349.1
			8.6	349.2
			8.6	349.2
			8.6	349.2
		5199 ²⁰	N Line of 1	
			9.2	348.6
			9.1	348.7
			9.1	348.7
			9.3	348.5
			9.3	348.5
			9.0	348.8
		Sec A. See sketch		
			8.97	348.82
			9.25	348.54
		Sec B.		
			9.31	348.48
			9.10	348.69
		Sec. along oblique Wagon		
			9.3~	348.47
			9.37	348.42

+

HI

-

Elev

357.79

59

E Top cb

9.47

348.32

E+15 Top cb. Wrightman is Not paved

9.55

348.24

T.P.

7.3

369.29

0.82

356.97

check BM. NWBP 36 B. Univ

476

359.53

359.50

0.01 ✓

check starting

BM. Wilson 0 Univ NWBP

3.68

360.61

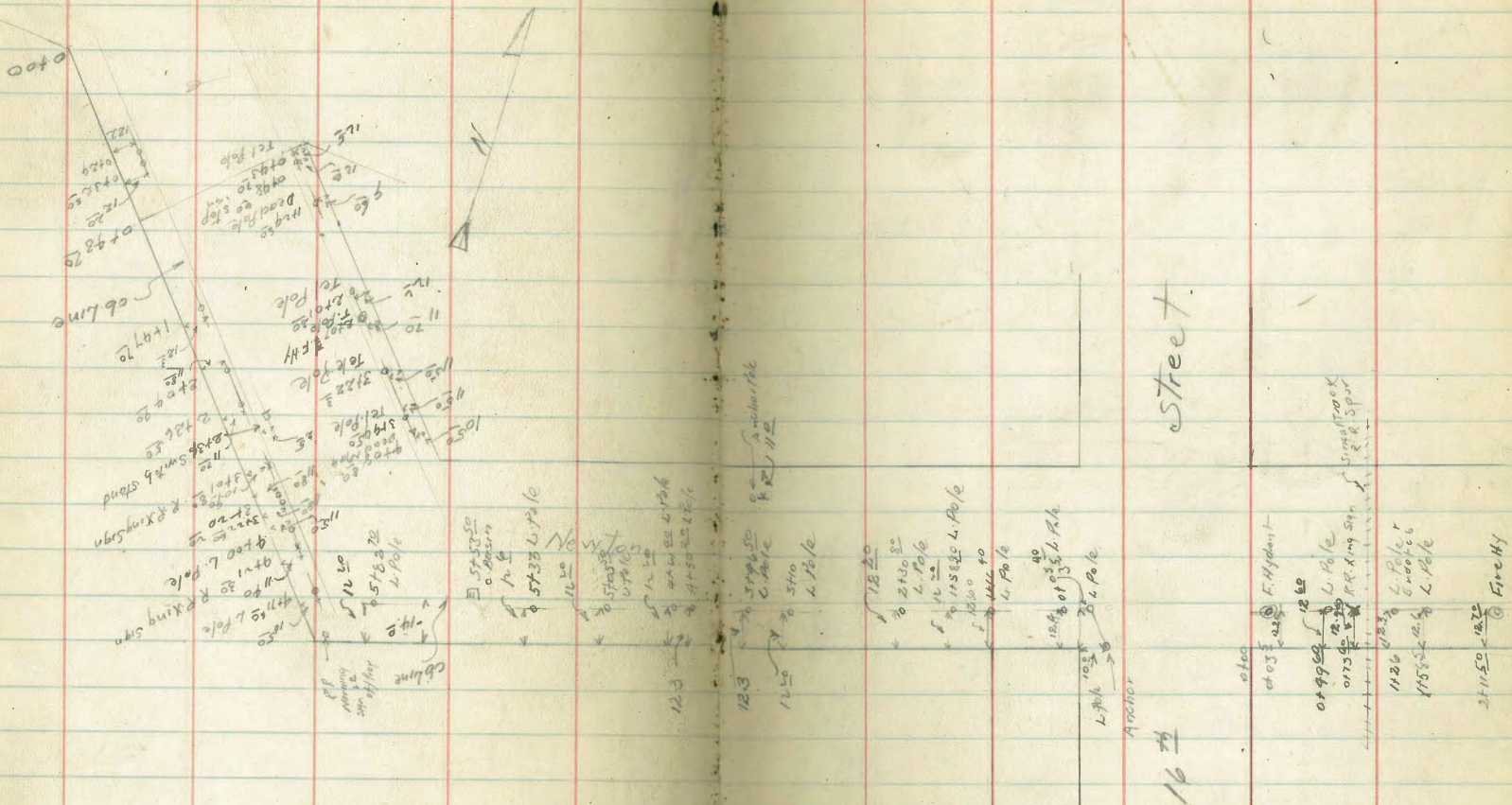
360.61

00 ✓

60

Bill Bliss
April 3, 1929

Location of Poles + Hydrants Newton Ave
from 200' SE of 12th to 13th + 13th St Newton to
National



Street

16th

0100
0103
0105 F. Hydrant
0149
0175
1126
1155
21150
Fire Hy

Curb & Pavmt. Levels
S.E. Cor 12th St & Bdw

4-16-29
Miller

ALLEY
BOUNDARY

X Sec Alley BIK 18 Teralta.
Between 42 & Van Dyke Orange to Polk.

62

B.M. 5.48 76.22 70.74 5 W. 11th St & Bdw.

S. line Bdw

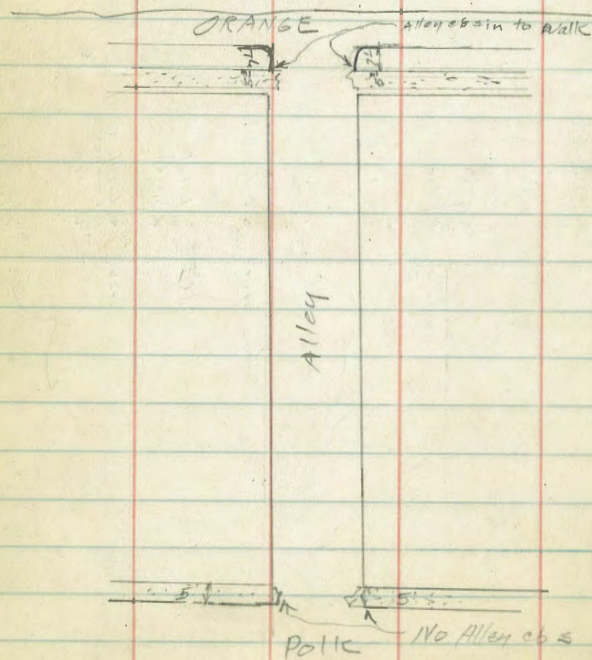
e. curb pavmt 5.11 71.11

gutter v F.A. Culvert 6.41 69.81

100.5

ch 6.12 70.10

gutter 7.02 69.20



B.M. 4.62 369.14 364.52 S.P. NW Copeland & Meade

or E. curb pavmt B.M. 4.44 367.40 6.18 362.96

T.P. 5.89 367.19 6.10 361.30

3rd line orange

EL top ret 5.59 361.60

W.L. top ret 5.57 361.62

0-15

W.L. backwalk 5.40 361.79

EL v v 5.35 361.84

0+00 = s.l. Orange

EL 5.1 362.10

E 5.3 361.9

W.L. 5.2 362.0

0+25

W.L. 4.4 362.8

E 4.5 362.7

EL 4.6 362.6

0+50

EL 4.9 362.3

E 4.7 362.5

W.L. 4.4 362.8

Plotted 5/10-1929
C.H.

0+58

W.L.	4.8	362.4
±	5.0	362.2
E.L.	5.5	361.7
2E floor garage (earth)	5.5	361.7
0+81 = ± Single garage 5 ¹ / ₂ W	4.95	362.34

Abbrn to 0±W.
Conc floor

0+80

E.L.	5.7	361.5
±	5.5	361.7
W.L.	5.5	361.7

1+00

W.L.	5.7	361.5
±	6.0	361.2
E.L.	6.1	361.1

1+10 = ± Single garage 1¹/₂ E earth floor

5.8 361.4

1+20

E.L.	5.6	361.6
±	5.6	361.6
W.L.	5.8	361.4

1+40

367.19

W.L.	5.9	361.3
±	5.8	361.4
E.L.	5.9	361.3

1+60

E.L.	6.0	361.2
±	5.9	361.3
W.L.	5.8	361.4

1+68 = ± garage 4¹/₂ West abrn to 0±W.

5.18 362.01

2+00

W.L.	5.6	361.6
±	5.9	361.3
E.L.	6.0	361.2

T.P. 536 367.35 520 361.99

2+10 = ± garage 8' E. Conc floor.

5.63 362.72

2+19 = ± garage 3¹/₂ W Conc floor.

5.24 362.11

2+20

E.L.	5.7	361.7
±	5.5	361.9
W.L.	5.3	362.1

2+50

367.35

w.L	57	361.7
+5	57	361.5
+7	56	361.8
±	58	361.6
+4	57	361.7
E.L	6.1	361.3

2+75

EL	5.5	361.9
±	5.6	361.8
w.L	5.4	362.0

3+00

w.L	5.1	362.3
±	5.5	361.9
EL	5.3	362.1

(2+98 = N end double garage 5⁶ West Conc floor.

5.01 362.34

3+22 send same garage

5.10 362.25

3+25

EL	5.8	361.6
+5	5.3	362.1
±	5.3	362.1
w.L	5.2	362.2

367.35

64

3+47 = ± garage 6⁵ West Conc floor.

5.1 362.3

3+50

w.L	5.2	362.2
±	5.1	362.3
EL	5.4	362.0

3+75

EL	5.1	362.3
±	5.3	362.1
w.L	5.6	361.8

4+00

w.L	5.5	361.9
±	5.5	361.9
EL	5.9	361.5

4+25 (shed 02 in on East)

EL 5.6 361.8

± 5.6 361.8

w.L 5.4 362.0

4+34 = ± garage 3' East earth floor.

5.5 361.9

4+46 = ± garage 18' East Conc floor.

5.65 361.70

A+50 367.35

w.L.	5.5	361.9
±	5.4	362.0
E.L.	5.6	361.8

A+67 = 4 garage 2⁵ West earth floor.

T.P.	5.15	367.22	5.28	362.07
------	------	--------	------	--------

A+75 5.5 361.7

E+75

EL	5.4	361.8
±	5.4	361.8
w.L.	5.5	361.7

A+81 = Nord double garage 7' East conc. floor.

	5.58	361.64
--	------	--------

5+05 = Sord. same garage

	5.61	361.61
--	------	--------

A+96 = 4 garage 1⁸ West conc. floor.

	5.36	361.86
--	------	--------

5+00.

w.L.	5.6	361.6
±	5.1	362.1
E.L.	5.2	362.0

65

5+25 367.22

EL	5.6	361.6
±	5.4	361.8
w.L.	5.5	361.7

5+34 = 4 garage 2' East earth floor

	5.5	361.7
--	-----	-------

5+50

w.L.	5.7	361.5
±	5.6	361.6
E.L.	5.6	361.6

5+70

E.L.	5.5	361.7
±	5.8	361.4
w.L.	5.8	361.4

5+77⁸ = NL Polk

w.L. back walk	6.06	361.16
±	6.1	361.1
E.L. back walk	5.86	361.36

Neb line Polk

E.L. top cb	6.02	361.20
w.L. ✓✓	6.19	361.03

T.P.	5.15	367.22	5.28	362.07
T.P.	5.53	367.39	5.36	361.86
T.P.	5.35	367.77	4.97	362.42

BM Sur El Polans Copeland 4.81 362.96

6-26-29 X-section California Street
 J.C. Bliss Beech to Grape - 75' wide 12' cbs
 Drabert 12.75' 1/4 S - Conforming to R.R. Alignment - E.L.
 Rauner California 25' East of R.R. Right of Way
 1995 corr.
 1999

B.M. N.W.B.P. Beech + Kettner
 +0.63 20.67
 T.P. -6.47 14.18
 +5.12
 +19.27

N.L. Beech = 0+00 - Paved - Flush with top rail
 E.L. Santa Fe R of W - Top existing cb. 4.75 14.51
 G-Flush

Note Track Numbers sketch next page

+20 = Top east rail track #1	5.02	14.24
+25 = " west " " "	5.03	14.23
+33 = " east " " #2	5.01	10.25
+38 = " west " " "	4.99	14.27
+47 = " east " " 3	5.13	14.13
+52 = " west " " 3	5.09	14.17
+67 = " East rail Spur Track	5.09	14.17
+67 = " West " " "	5.15	14.11
+76.5 = " east " " "	5.90	13.36
+81.5 = " West " " "	5.85	13.41

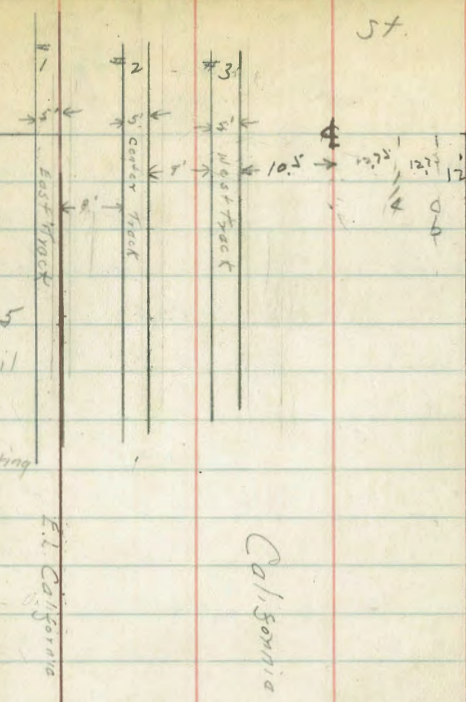
+100 = West line P of W cb +aving flush 6.43 12.83
 Paving breaks down to road bed at N.L. Beech

X-section is only from West rail of #3 West as road bed follows grade of track

W	6.7	12.6
cb	6.4	12.9

Beech

Location of 3 Principal Santa Fe Tracks.
 Road bed is 0.5' below top of rail between Property lines of intersecting streets.



ST.

66

19.27⁶

1/4	5.9	13.4	
¢	5.5	13.8	
+10.5 - Base West rail #3	5.4	13.9 + A	14.3 Top rail
	0 + 50		
B. West rail #3	5.3	14.0	+ A Top rail
¢	5.5	13.8	
1/4	5.5		
cb	6.1		
W	6.3	13.0	
	0 + 75		
W	5.8	13.5	
cb	6.0		
1/4	5.3		
¢	5.3	14.0	
+10.5 - B. W. R. #3	5.2	14.1	
	1 + 00		
B. W. R. #3	5.0	14.3	
¢	5.1	14.2	
1/4	5.6		
cb	5.8		
W	5.8	13.5	
	1 + 25		
W	5.7	13.6	
cb	5.7		
1/4	5.5		

19.29⁶

67

¢	5.0	14.3	
+10.5 - Base West rail #3	4.9	14.4	
Top rail - Eng. Main Line + Spur Track	4.37		
	1 + 50		
B. W. R. #3	4.7	14.6	
¢	4.8	14.5	
1/4	5.4		
cb	5.4		
W	5.4	13.9	
	1 + 75		
W	4.7	14.6	
cb	5.3		
1/4	5.2		
¢	5.0	14.3	
+10.5 - B. W. R. #3	4.6	14.7	California
			2 + 03.8 = 80 - 41 Ports - 120' 13' - R = 3892.04
B. W. R. #3	4.5	14.8	
¢	4.6	14.7	
1/4	5.4		
cb	5.2		
W	4.9	14.4	
	#1		
W	4.8	14.5	
cb	5.2	14.1	
1/4	5.3		

π 19.27⁶

⊥		4.9	14.4
410.5-B.W.R #3		4.4	14.9
	#2		
B.W.R #3		4.1	15.2
⊥		4.8	14.5
1/4		5.3	
cb		5.6	
W		5.7	13.16
	#2 + 30.3 = S.L. Cedar		
W		6.2	13.1
cb		6.0	
1/4		4.7	
⊥		4.0	15.3
410.5 - Top West rail #3		3.52	15.74
1/4 + 2.75 " East " "		3.41	15.85
1/4 + 2 " West " #2		3.22	15.99
cb + 4.5 " East " "		3.22	16.04
E " West " #1		3.02	16.24
4.5 " East " "		3.05	16.21
Section across existing paving on Cedar ^{50' wide} _{13' high}			
Which is 7' East of E.L. California-			
S		3.5	15.8
cb + Gutter Flush		3.03	
1/4		3.00	
⊥		2.93	16.33

π 19.29⁶

68

1/4		2.95	
cb + Gutter Flush		2.97	
X.		3.2	16.1
	#4		
B.W.R #3		3.4	15.9
⊥		3.9	15.4
1/4		4.8	
cb		5.7	
W		7.1	12.2
X.P.			-4.74 14.58 ²
	+ 5.78		
	π 20.31 ⁰		
Flowline 1' x 2' Wooden Culvert on North cb line Cedar + 2.5'			
East of E. California 7.10 13.20			
Flowline similar culvert on South cb			
line Cedar + California 7.20 13.10			
#5 + 8.5 = N.L. Cedar			
W		7.2	13.1
cb		6.8	
1/4		6.4	
⊥		5.1	15.2
Top West rail #3		4.26	16.04
" E " "		4.18	16.12
" W " #2		4.03	16.27
" E " "		3.96	16.34

π 20.31°

Top West rail #1 396 16.34

" E " " 386 16.44

Note - Black stagg flush with top of rail across
Intersection of Cedar

Concrete Walks 2' in St. from W.L. California

N.L. Cedar = 0+00

0+12 - 2' 6" Walk 7.17 13.13

0+36 - 2' 3" " 7.36 12.94

0+61 - 2' 3" " 7.36 12.94

0+72 - 2' 2" " 7.37 12.93

0+88 - 2' 4" " 7.40 12.90

1+02 - 2' 3" " 7.25 13.05

1+12 - 2' 4" " 7.20 13.10

1+31 - 2' 4" " 7.47 12.83

1+45 - 2' 4" " 7.69 12.61

#6

B.W.R.#3 4.8 15.5

2 5.4 14.9

1/4 7.0 13.3

cb 7.0 13.3

W 7.1 13.2

#7

W 7.5 12.8

cb 7.4 12.9

π 20.31°

29

1/4 7.2

2 6.0

2 5.5 14.8

110.5 = B.W.R.#3 4.6 15.7

#8

B.W.R.#3 4.6 15.7

2 5.7 14.6

1/4 7.2

cb 7.4

W 7.4 12.9

#9

W 7.5 12.8

cb 7.6

1/4 7.0

2 5.3 15.0

110.5 = B.W.R.#3 4.4 15.9

#10

B.W.R.#3 4.4 15.9

2 5.5 14.8

1/4 6.6

cb 7.7

W 8.2 12.1

#11

W 8.1 12.2

cb 7.8

π 20.3⁰

1/4	7.2	
♀	5.1	15.2
+10.5 = B.W.R.#3	4.2	16.1
#12		
B.W.R.#3	4.1	16.2
♀	5.0	15.3
+5	6.4	
1/4	6.9	
cb	7.5	
W	8.2	12.1
#13		
W	8.1	12.2
cb	7.6	
1/4	7.0	
+7	6.8	
♀	4.4	15.9
+10.5 = B.W.R.#3	4.1	16.2
#14 + 88 = J.L. Date		
East Rail #1	3.05	17.25
West " "	3.16	17.14
E " #2	3.31	16.99
W " "	3.40	16.90
E " #3	3.50	16.80
W " #3	3.53	16.77
Base West Rail #3	4.0	16.3

π 20.3⁰

70

+8.5	4.1	
♀	4.7	15.6
+5	6.8	
1/4	6.9	
cb	7.4	
W	8.4	11.9
Flow line 2'12" Wooden Culvert on South cb line		
Date + ♀ California	7.83	12.47
#15		
W	8.2	12.1
cb	7.2	
+5	6.1	
1/4	7.7	
+7	7.3	
♀	4.8	15.5
+4	4.0	
+10.5 = B.W.R.#3	3.9	16.4
#16		
B.W.R.#3	3.9	16.4
♀	4.4	15.9
+9	7.8	
1/4	8.7	
+5	9.3	
cb	6.8	
W	8.5	11.8

π 20.31

Flow line 2' x 2' Wooden Culvert on North

cb line Date & California 794
 T.P. -4.13 16.18
 +5.47

π 21.65

#16 + 22 = N.L. Date

W	10.1	11.5
cb	8.3	
+8	11.0	
114	10.2	
+5	9.4	
¢	5.8	15.8
B.W.R. #3	5.2	16.4
Top West Pair #3	4.7	16.97
" E " "	4.4	17.03
" W " #2	4.50	17.14
" E " "	4.43	17.21
" W " #1	4.16	17.48
" E " "	4.06	17.58

Section on existing Paving on Date St.

N.L. 41' E of E.L. California - S.L. 29' E of E.L.
 California - Cedar - 80' wide 14' cbs 13' 1/2 S
 S 4.0 17.6
 cb 4.75
 G 5.15

π 21.65

71

14	4.76	
¢	4.53	17.11
14	4.65	
G	5.12	
To cb	4.60	
1	4.1	17.5
#18		
B.W.R. #3	5.1	16.5
+8	5.4	
¢	6.5	15.1
+10	10.4	
114	10.6	
+5	11.8	
cb	9.7	
W	10.5	11.1
#19		
W	9.9	11.7
+7	12.2	
cb	10.3	
114	9.4	
+3	11.0	
¢	7.1	14.5
+5	5.4	
+10.5 = B.W.R. #3	5.0	16.6

π 21.65^d

20

B.W.R. #3	48	16.8
+5	55	
⊥	71	14.5
+7	99	
1/4	10.5	
cb	10.9	
+9	111	
W	121	9.5

21

W	11.0	10.6
cb	10.8	
1/4	10.3	
+5	91	
⊥	59	15.7
+2	51	
#10.5 = B.W.R. #3	47	16.9

21 + 18 and 2.5 W of California = Flowline

2' x 2' Wooden Culvert 10.56 11.08

22

B.W.R. #3	46	17.0
+5	50	
⊥	64	15.2
+8	94	
1/4	10.2	
cb	10.4	

π 21.65^d

72

23

W	10.9	10.7
W	10.5	11.1
cb	10.6	
1/4	10.2	
+5	94	
⊥	64	
+5	48	

710.5 = B.W.R. #3 44 17.2

23 + 30 = S.L. Fir

B.W.R. #3	43	17.3
+8	46	
⊥	65	15.1
+8	84	
1/4	93	
cb	10.2	

W. 10.3 11.3

Top E Rail #1 283 18.81

" W " " 293 18.71

E " #2 326 18.38

" W " #2 340 18.24

" E " #3 367 17.97

" W " #3 378 17.86

T.P. Top M.H. 5' West W. Rail #3 S.L. Fir - 423 17.42

+5.37 22.78

8
 π 22.74

#25

W	11.3	11.5
cb	10.9	
1/4	9.5	
+7	8.5	
¢	6.2	16.6
+2	5.5	

+10.5 = B.W.R #3

#26+10 = N.L. Fir

E-Top rail #1	360	19.18
W " " "	366	19.12
E " " #2	408	18.70
W " " "	413	18.65
E " " #3	436	18.42
W " " #3	449	18.29
B.W.R #3	5.0	17.8
+6	5.4	17.4
¢	6.4	16.4
+4	7.5	15.3
1/4	9.2	13.6
cb	9.6	13.2
W	9.4	13.4'

Section across paving West end Fir St - 80' wide 14' cbs 12' to

S Top cb	437	18.41
G	487	
1/4	425	

8
 π 22.74

73

¢	4.16	18.62
1/4	4.34	
G	4.68	
N Top cb	4.24	18.54

Paving Line West end of Fir approximately 39' E of E.L.
 California

#27

W-¢ Concrete Walk at W.L.	8.59	14.19
cb	8.2	
1/4	6.7	
+5	5.6	
¢	5.7	17.1
+2	6.8	
+7	5.7	
+10.5 = B.W.R #3	4.9	17.9

#28

B.W.R #3	4.7	18.1
+3	5.2	
+8	6.2	
¢	5.4	17.4
+5	4.7	
1/4	5.8	
cb	7.2	
W-¢ Concrete Walk at W.L.	7.70	15.08

π 22.79⁶

#28+18

⊕ 4' Concrete Walk at W.L. 6.80 15.98

#28+31

⊕ 5' Concrete Walk at W.L. 6.82 15.96

#29

W 6.8 16.0

cb 6.1

14 5.2

⊕ 4.3 18.5

+4 5.9

+7 5.1

B.W.R.#3 4.6 18.2

#30

B.W.R.#3 4.5 18.3

+3 4.7

+7 5.6

⊕ 4.8 18.0

14 5.2

cb 5.5

W 6.2 16.6

#31

W 5.7 17.1

cb 5.2

14 4.7

⊕ 4.2 18.6

+4 5.4

π 22.79⁶

74

+7 4.7

10.5 B.W.R.#3 4.3 18.5

#32

B.W.R.#3 4.2 18.6

+3 4.5

+7 5.3

⊕ 4.9 17.9

+2 4.5

14 4.3

cb 4.2

W-Base ⊕ 3.2' Concrete Wall 4.8 18.0

Top Wall - Wall Level 4.30

#33

W 4.0 18.8

cb 4.2

14 3.9

11 3.9

⊕ 4.6 18.2

+2 5.1

+5 5.2

+8.5 B.W. 4.3

B.W.R.#3 4.2 18.6

#33+5

⊕ 3' Concrete Walk at W.L. 4.27 18.51

T 22.79^b

T.P - 4.02 18.77^b
+ 7.74

T 26.74^a

#34

B.W.P #3 80 18.7

+2 -8.2

+5 8.9

+8 8.8

£ 7.8 18.9

17L 7.2

cb 7.1

W 7.5 19.2

#35 + = S.L. Grabe^{pared} - across entire curve

W Top cb 8.18 18.52

G - Paving 8.40

cb 8.05

11+ 7.82

£ 7.64 19.06

Top W rail #3 7.63 19.07

" E " " 7.47 19.23

" W " #2 7.30 19.40

" E " #2 7.25 19.45

" W " #1 7.08 19.62

" E " #1 7.02 19.68

11V

T 26.74^o

75

EL. California - Paving 7.04 19.66

+25 - Gutter 6.25 20.45

16. Top - cb - EL. of P of W. 5.93 20.77

T.P -2.17 24.54³

+ 8.11 32.65^a

B.M. W.B.P. Grabe + Netter -1.59 31.06⁵

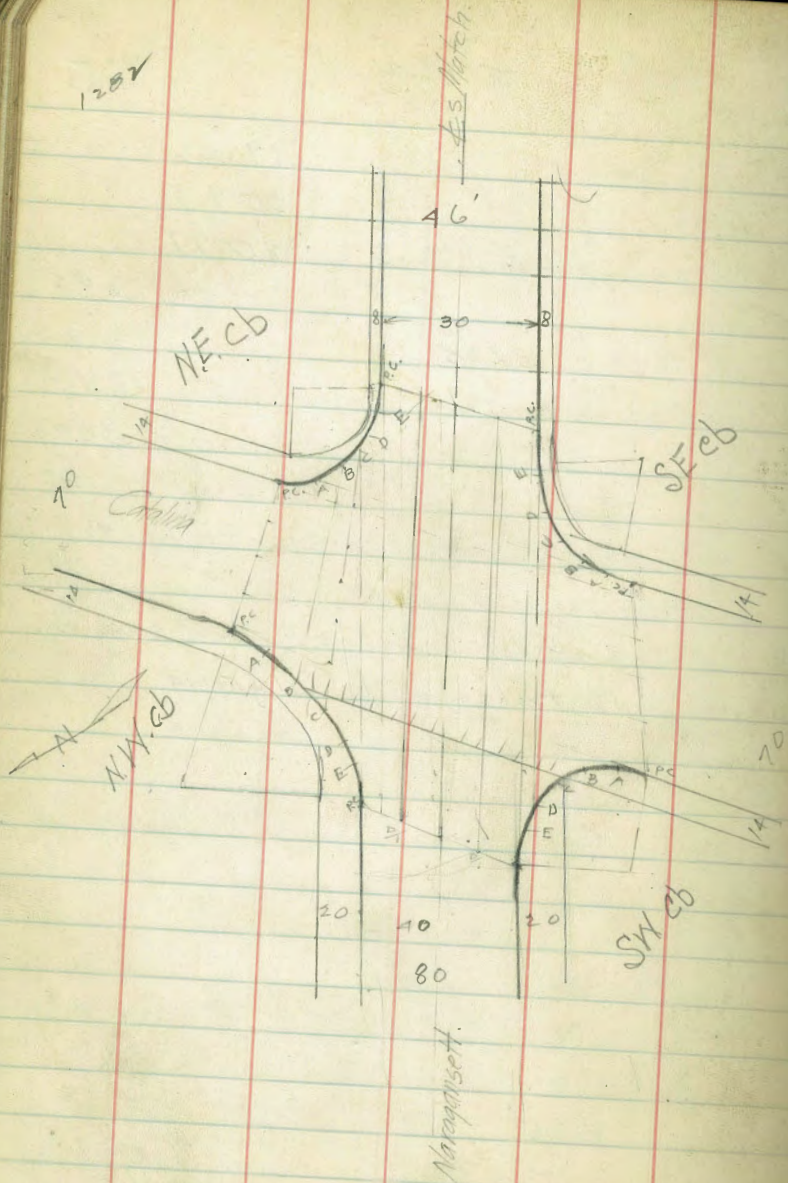
Correct 30.99

Error 0.07

Note - Improved intersections - Paving is
Flush with top of rails
Ties to radial lines between sections on
curve are taken on £ California

Taken

1282



X Sec Intersection of
Catalina & Narragansett.
7/31/29 Loudon. **76**
Curb levels on returns - 6 equal parts.
Return.

PC on Narragansett	4.73	157.41
E	5.35	156.79
D	5.99	156.15
C	6.19	155.95
B	6.04	156.10.
A	5.96	156.18
PC on Catalina	5.96	156.18
S.W. return.		
PC on Catalina	5.61	156.53
A	5.42	156.72
B	4.93	157.21
C	4.19	157.95
D	3.30	158.84
E	3.32	158.82
PC on Narragansett	1.36	160.78
N.W. return.		
PC on Narragansett	2.46	159.68
E	3.28	158.86
D	4.00	158.14
C	4.78	157.36
B	5.66	156.48
A	6.46	155.68
PC on Catalina	7.33	154.81

162.14

N.E. return

PC on Catalina	7.83	154.31
A	7.58	154.56
B	7.40	154.74
C	7.16	154.98
D	6.38	155.76
E	5.58	156.56
PC on Narragansett	4.59	157.55

Section S Across Catalina 22' relay

Sec from sw. PC. to SE PC.		
web	5.63	156.51
qtz	6.25	155.89
1/4	6.53	155.61
1/4	6.69	155.45
1/4	6.64	155.50
qtz	6.59	155.55
Ecb	5.96	156.18

Section B-B

Ecb + 5 top ebs	6.03	156.11
qtz	6.68	155.46
eb Pav	6.82	155.32
1/4	6.90	155.24
1/4	6.90	155.24
1/4	6.65	155.49
eb	6.33	155.81
web + 6.6 qtz	5.59	156.55
web + 6 top eb	4.93	167.21

162.14

Sections on 1/4 S ebs taken
Parallel to 1/4 of Narragansett.

Section on Seb Narragansett Produced from West

WL-31E top eb PC	1.36	160.78
" " qtz	2.0	160.1
WL. Catalina	4.73	157.41
eb	6.51	155.63
1/4	6.88	155.26
1/4	7.15	154.99
1/2	7.13	154.99
eb	7.09	155.05

E.L.	6.71	155.43
+2 Int with ret	6.67	155.47
+2 top eb ret	6.08	156.06

Section on Seb line of Narragansett Produced from East

EL-20 PC ret	4.74	157.40
" " qtz	5.29	156.85
E.L.	6.73	155.41
eb	7.20	154.94
1/4	7.22	154.92
1/4	7.24	154.90
1/4	6.95	155.19
eb	6.62	155.52
WL. F. 19 Pav	4.68	157.46
+31 Int. with 1/4 top eb PC.	1.9	160.2

162.14

Sec on S 1/4 line Narragansett Produced from West.

wL-30	2.0	160.1
wL. Edg Pav	4.67	157.47
cb	6.71	155.43
1/4	7.04	155.10
±	7.30	154.84
1/4	7.31	154.83
cb	7.30	154.84
E.L.	6.75	155.39
+22	5.02	157.12

Sec on ± Narragansett.

EL-25	4.63	157.51
E.L.	6.70	155.44
cb	7.40	154.74
1/4	7.46	154.68
±	7.47	154.67
1/4	7.20	154.94
cb	6.86	155.28
wL. Edg Pav	4.70	157.44
+28 ²	2.2	159.9

Int of wL. Catalina & SW. return

top eb	4.15	157.99
getter	4.82	157.32

162.14

78

Sec on N 1/4 line Narragansett Produced from West.

wL-26	2.8	159.3
wL. Edg. Pav	4.76	157.38
cb	7.01	155.13
1/4	7.39	154.75
±	7.60	154.54
1/4	7.63	154.51
cb	7.57	154.57
E.L.	6.91	155.23
+28 ²	4.80	157.34

Sec on N 1/4 line Narragansett Produced from East.

FL-30 ³ top eb Pe. ret.	4.59	157.55
" " gutter	5.02	157.12
E.L.	7.10	155.04
cb	7.65	154.49
1/4	7.74	154.40
±	7.70	154.44
1/4	7.47	154.67
cb	7.06	155.08
wL. Edg. Pav.	4.88	157.26
+24	3.1	159.0

Int. of wL. Catalina & NW. ret.

top eb	4.43	157.71
getter	5.06	156.08

162.14

Sec on Neb line N. Mansueti Produced from West.

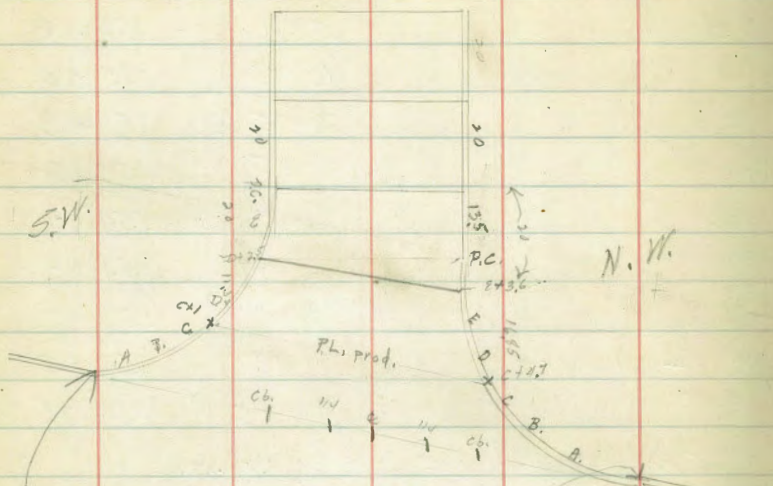
WL-23 ^E	pc. ret top cb	2.46	159.68
" "	gut	3.2	158.9
W.L.	Edg Paw	4.96	157.18
cb		7.14	155.00
1/4		7.56	154.58
±		7.80	154.34
1/4		7.80	154.34
cb		7.78	154.41
E.L.		7.30	154.84
+11	top NE. ret gutter	6.59	155.55
"	top cb	6.16	155.98
Sec. C-C - NE-NW rets.			
EL 10 ^S		7.15	154.99
11	gutter	7.57	154.57
cb		7.89	154.25
1/4		7.95	154.19
±		7.94	154.20
1/4		7.70	154.44
cb		7.19	154.95
+11 ^E	gutter	5.50	156.64
11	top cb	4.78	157.36

162.14

79

Sec B-B	NE-NW rets		
WL 17 ^Z	top cb	5.66	156.48
"	gutter	6.48	155.66
cb		7.25	154.89
1/4		7.85	154.29
±		8.09	154.05
1/4		8.11	154.03
cb		8.07	154.07
+6 ^Z	gutter	7.97	154.15
+6 ^Z	top cb	7.41	154.73
Sec between NE & NW. P.C.s.			
Feb	top	7.85	154.29
	gutter	8.48	153.66
1/4		8.56	153.58
±		8.54	153.60
1/4		8.29	153.85
	gutter	7.96	154.18
Web	top	7.32	154.82

157.52
5.98
163.50



P.C. Cb.	6.98	156.52	P.C. Cb.	8.70	154.80
P.C. point	7.61	155.89	P.C. point	9.33	154.17
A. Cb.	6.78	156.72	A.	7.83	158.67
B. Cb.	6.30	157.20	B.	7.03	156.47
C. Cb.	5.55	157.95	C.	6.15	157.35
C + 1 = 7.48	5.48	159.02	C + 4.7 = 7.48	5.78	157.70
D.	4.66	158.84	D.	5.36	158.14
D + 2.5 = 11.30	4.44	159.06	E.	4.64	158.86
E.	3.69	159.51	E + 3.6 = 11.30	4.36	159.14
P.C. on Nav.	2.70	160.80	P.C. on Nav.	3.83	159.67
+ 20	0.76	162.74	+ 13.5 = 0.76 P.C.	2.67	160.80
			+ 20	0.89	162.64
S. Cb. on Cb. line	7.87	155.63	N 1/4	8.27	155.21
S 1/4	5.04	155.46	N Cb.	8.46	155.04
Q	8.16	156.34			

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 1/2 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body

of table in same row and column gives distance from side stake to slope stake. If ground is not

level, the side stake and slope stake, lower table by this amount if cut, elevation of fill. Add this amount

to cut or fill and find distance in table. Set up rod at this point and line of sight should cut

target.

necessary.

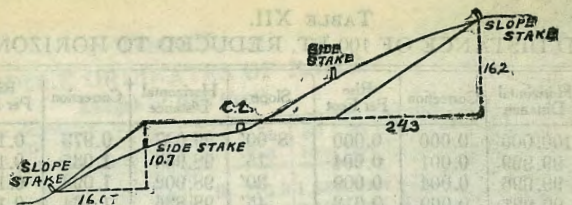
IMPROVED TABLES AND INFORMATION

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING

SLOPE 1 1/4 TO 1. ROADWAY OF ANY WIDTH.

C	R
o /	Feet
0-20	17189
0-40	8594
1-0	5730
1-20	4297
1-40	3438
2-0	2865
2-20	2456
2-40	2149
3-0	1910
3-20	1719
3-40	1564
4-0	1437
4-20	132
4-40	122
5	114
6	954
7	819

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	72 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

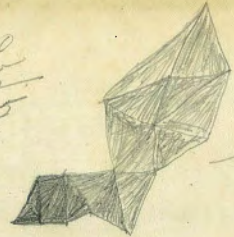
Computed by L. Leland Locke.

2.75.
4
58.00

To fir

J.W.B.P Grape Weather SW BP 30.99

15.50
12.75
2.75



375
10.5
27

ENGINEERING DEPARTMENT
CITY OF CALIFORNIA
SAN DIEGO

225

1425

16

17

E

cb

35 1/4

14 + 43

+ 93

♀ N Top cb - 3.67

+7 G 4.11

1/4 3.77

41 W ♀ 3.59

cb 1/4 3.68

W 3.80

Top

366

257

4.25

J.M. SW. B.P. Lowell Reservoir 806

35/23 NW BP 3.11
46 434 - 5.95

8.73

+ 3.19

11.92

S.W. 7' 4" Prop Map of - 5.24

6.68

163.01

60.46

223.47

80

224.27

11.15

11.92

- 6.06

5.86

+ 8.04

13.90

- 8.25

04362

163.17

04362

32634

97902

48951

65268

1174

99905

63.7

699335

49905

299715

599430

99905

631099885

99905

163009

99905

16317

699335

99905

299715

599430

99905

1630199885

B.M. 1107 5.65

390454

12.5

389204

437

437

380

57