

1299

EAST

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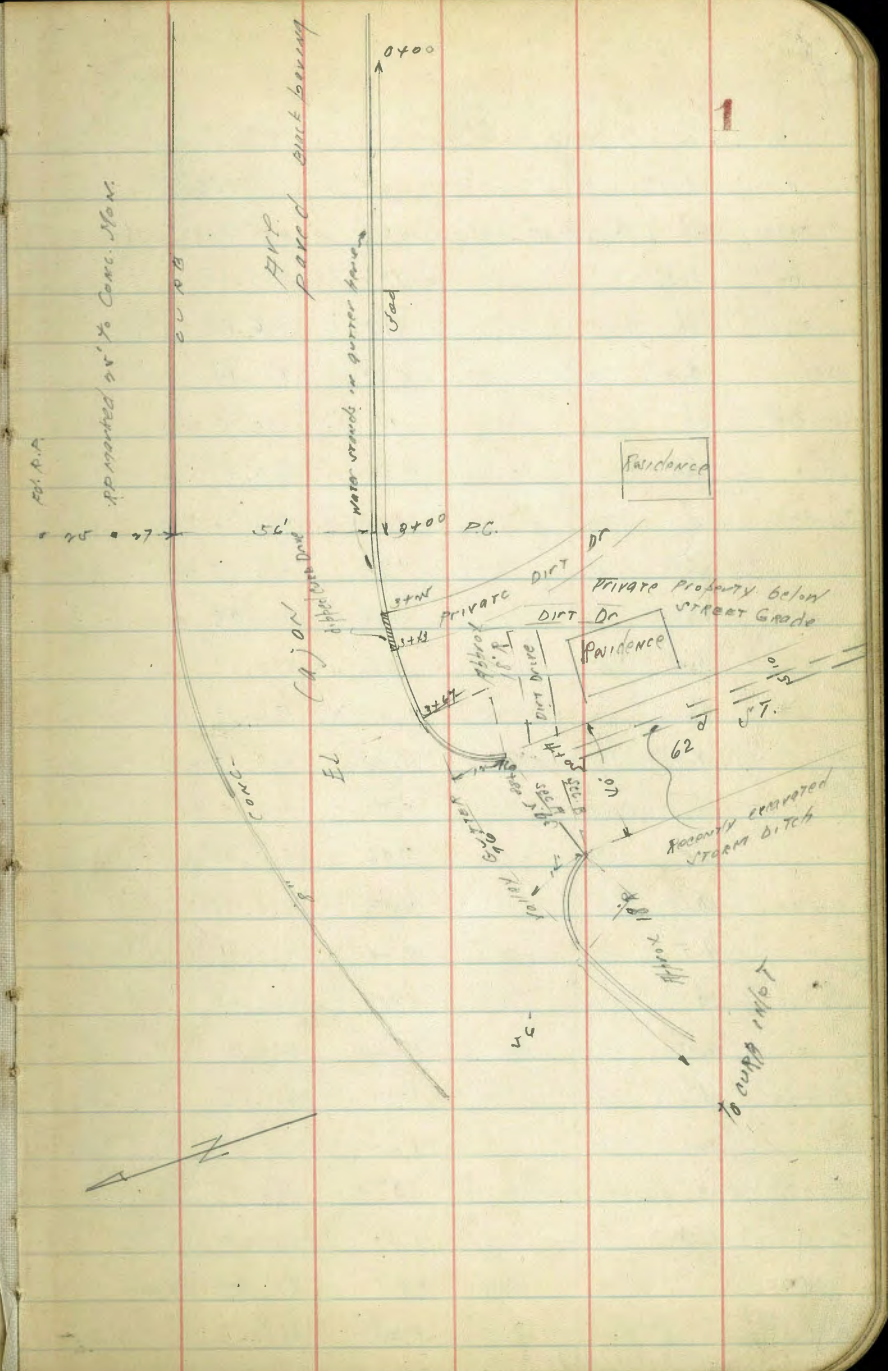
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Moore Levels on paving at 6th & El Cajon Ave

11/6/88	+	π	-	el	NOTE LINE EL RETIRO SUB.
Top COM. CURB N. Side El Cajon Ave	474	468.74		464.00	
T.P.	650	470.31	4.93	463.81	
00=300' E of P.C. or S of Live El Cajon Ave			4.85 = CURB DRIVE	465.46	Top of
" "	" "	" "	5.00	465.31	90T
-0+10	Top of		4.25	466.06	
" "	90T		4.88	465.43	
0+20	Top of		4.20	466.11	
" "	90T		4.84	465.47	
0+30	Top of		4.10	466.21	
" "	90T		4.75	465.56	
0+40	Top of		4.06	466.25	
" "	90T		4.72	465.59	
0+50	Top of		4.04	466.29	
" "	90T		4.72	465.59	
0+60	Top of		4.01	466.30	
" "	90T		4.65	465.66	
0+70	Top of		3.94	466.37	
" "	90T		4.63	465.68	
0+80	Top of		3.88	466.43	
" "	90T		4.58	465.73	
0+90	Top of		3.91	466.40	
" "	90T		4.57	465.74	
1+00	Top of		3.93	466.38	
" "	90T		4.59	465.72	
1+10	Top of		3.99	466.32	
" "	90T		4.63	465.68	



1+20	cb = cb Drive	4.55	465.76	
"	gut	4.67	465.84	
1+30	cb = cb Drive	4.56	465.75	
"	gut	4.73	465.58	.58-
1+40	cb	4.13	466.18	
"	gut	4.80	465.89	.57-
1+50	cb	4.18	466.13	
"	gut	4.86	465.45	.56
1+60	cb	4.20	466.11	
"	gut	4.84	465.47	.54
1+70	cb	4.25	466.06	
"	gut	4.82	465.47	.53
1+80	cb	4.27	466.04	
"	gut	4.88	465.43	.52
1+90	cb	4.20	465.99	
"	gut	4.96	465.35	.51-
2+00	cb	4.22	465.99	
"	gut	5.00	465.31	.49
2+10	cb	4.20	465.99	
"	gut	5.00	465.31	.48
2+20	cb	4.30	465.96	
"	gut	5.00	465.29	.47
2+30	cb	4.37	465.94	
"	gut	5.04	465.27	.46
2+40		4.37	465.94	
"		5.05	465.26	.44

2+50	cb	4.44	465.87	
"	gut	5.06	465.25	.43
"	N'S	4.7	465.6	
2+60	cb	4.46	465.85	
"	gut	5.09	465.22	.42
"	N'S	4.7	465.6	
2+70	cb	4.46	465.85	
"	gut	5.08	465.23	.41
"	N'S	4.8	465.5	
2+80	cb	4.46	465.85	
"	gut	5.08	465.23	.39
"	N'S	4.8	465.5	
2+90	cb	4.43	465.88	
"	gut	5.06	465.25	.38
"	N'S	4.9	465.9	
3+00 = PC	cb	4.43	465.88	
"	gut	5.11	465.20	.37
"	N'S	5.0	465.3	
3+10	cb	4.41	465.90	
"	gut	5.06	465.25	.36
"	N'S	5.0	465.3	
3+20	cb	4.38	465.93	
"	gut	5.01	465.30	.34
"	N'S	5.3	465.0	
3+25	cb CURB DRIVE	4.90	465.91	
"	gut	5.05	465.26	

3+30	cb	CURB Drive	4.55	465.76	
"	gut		5.00	465.31	.33
"	N'S		5.00	465.31	
3+40	cb	CURB Drive	4.86	465.45	
"	gut		4.99	465.32	.32
"	N'S		4.8	465.5	
3+43	cb	CURB Dr	4.58	465.93	
"	gut		5.02	465.29	
3+50	cb		4.39	465.92	
"	gut		5.07	465.28	.31
"	N'S		5.00	465.31	
3+60	cb		4.44	465.89	
"	gut		5.06	465.25	.29
"	N'S		5.1	465.2	
3+67 = PC	CURB RETURN	CURB	4.44	465.89	
"	gut		5.04	465.27	.28
"	N'S		5.2	465.1	
"	25'S	Center private Dr	5.2	465.1	Front of House
3+72	curb		4.39	465.92	
"	gut		5.06	465.25	
3+77	cb		4.60	465.91	
"	gut		5.03	465.28	
3+82	cb		4.31	466.00	
"	gut		4.92	465.35	
3+87	cb		4.45	466.06	
"	gut		4.88	465.45	

3+88 = end	curb	curb	4.15	466.16	
"	gut		4.59	465.42	
Sec A = S edge paving = $\frac{1}{4} = 9.9$			4.67 = E 1/4	465.64	on paving
E 6W			4.45	465.76	" "
W 1/4			4.23	465.58	" "
W gut			5.15	465.16	" "
W cb	Tot cb		4.29	465.82	
Elev. of valley gutter					
3+67 = PC of RETURN = 00			5.04	465.27	.28
0 + 0.95			5.01	465.30	.27
0 + 1.9			4.90	465.41	.26
0 + 4.85			4.89	465.42	.25
0 + 3.8 = E 6W			4.89	465.42	.24
0 + 4.75			4.99	465.32	.23
0 + 5.7			5.03	465.28	.21
0 + 6.5			5.04	465.27	.20
				465.19	.19
0 + 7.6 = PC RETURN on WAST			5.14	463.2	in 5' parts
Lead top curb & paving on SW RETURN					
end cb on W + SLEI Cajan			4.89	465.92	
" " gutter			5.15	465.16	
#1 curb			4.40	465.91	
" gut			5.05	465.25	
#2 curb			4.35	465.96	
" gut			5.03	465.28	
#3 curb			4.39	465.92	
" gut			5.06	465.25	

#1	cb	4.44	465.89		3+40	E	5.8	464.5	4
"	gut	5.11	465.20			C	6.0	464.3	
#2	cb = RC of Putnam +	4.46	465.85	end of		W	5.7	464.6	
"	gut	5.11	465.19	valley gutter	3+40	W	5.4	464.9	
	Lorals J on 62 md ST approx. 40' wide					C	5.6	464.7	
	Sec B = 40					E	5.6	464.7	
W	gut on paving	5.15	465.16			E	4.8	465.8	
C		4.8	465.5		3+40				
E		5.7	464.6			E	5.4	465.8	
+10	private prop.	5.5	464.8			C	5.4	464.9	
	0+50					W	5.8	464.5	
E		5.7	464.6		4+40				
C		5.6	464.7			W	5.7	464.6	
W		5.7	464.6			C	5.1	465.2	
	1+40					E	5.6	464.7	
W		6.0	464.3		4+50				
C		5.8	464.5			E	5.4	465.9	
E		5.8	464.5			C	5.2	465.1	
	1+50					W	5.5	464.8	
E		5.8	464.5		5+40				
C		5.9	464.4			W	5.3	465.0	
W		6.4	464.1			C	5.5	464.8	
	2+00					E	5.7	464.6	
W		6.4	463.9		5+50				
E		5.9	464.4			E	6.9	465.4	
E		6.0	464.3			C	5.7	464.6	

N+50

W

N.V 464.8

0+00

W

N.V 464.9

C

N.V 464.9

E

N.V 464.4

I suggest skin patching on paving of El Cajon
and the grading & paving of Grand St

Filling in of private drives & property is
necessary in any event.

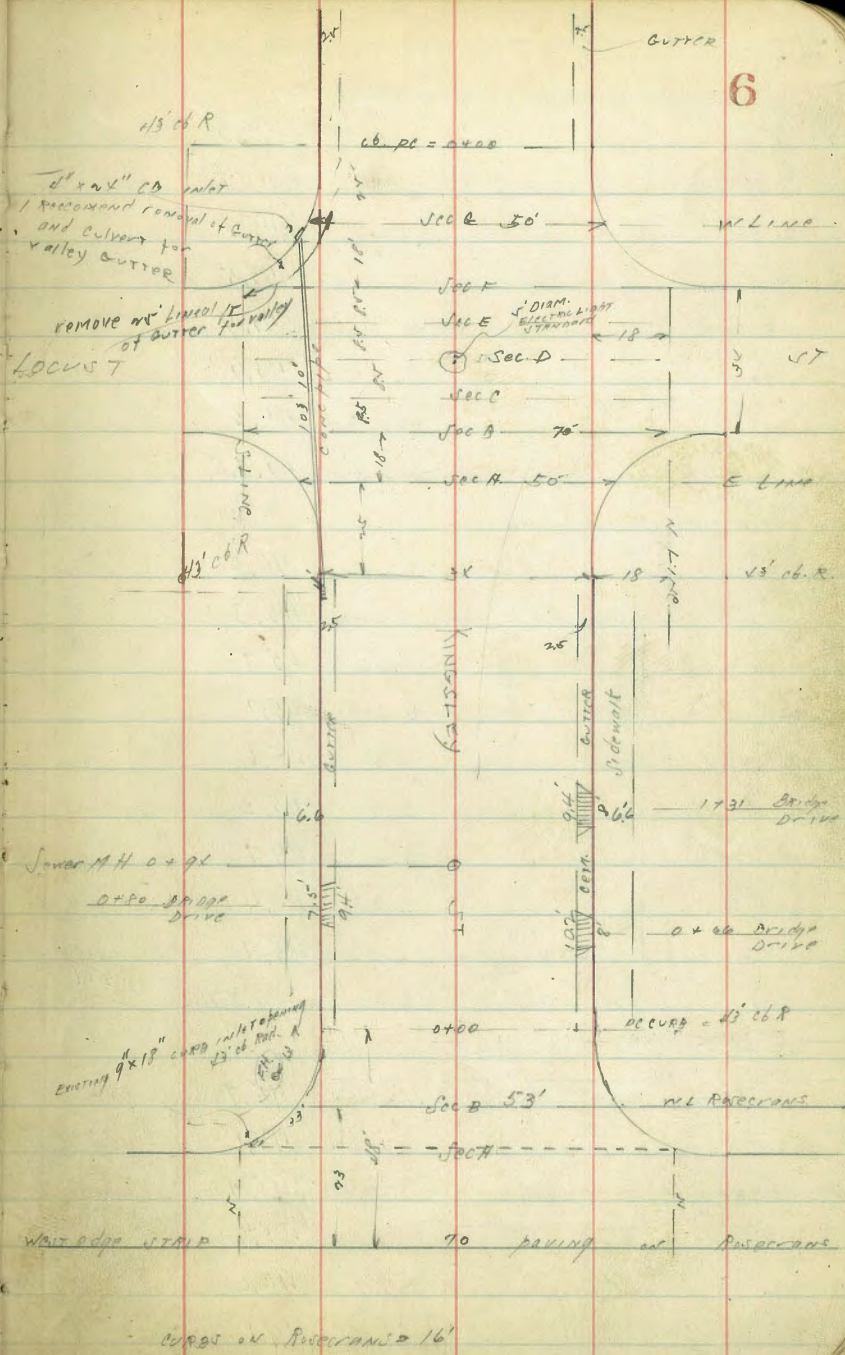
11/19/18 Cross Section of Kingsley st.
Moore from Rosecrans to Chatsworth

47.3

SW.P.P. Rosecrans Lytton	5.52	4.727	41.75
W. Edge Paving on Rosecrans			
N.L.	3.47	43.80	
cb.	2.16	44.1	
1/4	3.03	44.3	
1/2	2.88	44.39	
3/4	2.74	44.6	
cb	2.59	44.7	
s.L.	2.29	44.98	
Sec. "A"			
s.L. Top cb.	1.64	45.63	
gut	2.61	44.86	
outside edge of gut	2.17	45.1	
cb	2.1	45.2	
1/4	2.0	45.3	
1/2	2.2	45.1	
3/4	2.4	44.9	
cb	2.8	44.5	
edge of gut	3.56	43.7	
gut	3.88	43.39	
N. top Cb.	2.87	44.40	
Sec. "B" = W.L. Rosecrans			
N. top Cb.	2.61	44.66	
gut	3.62	43.7	
edge	3.28	44.0	

C.B. Plotted - 12.3-28 - C.B.H.

gutters 1 - 4 - 29 T.G.H.

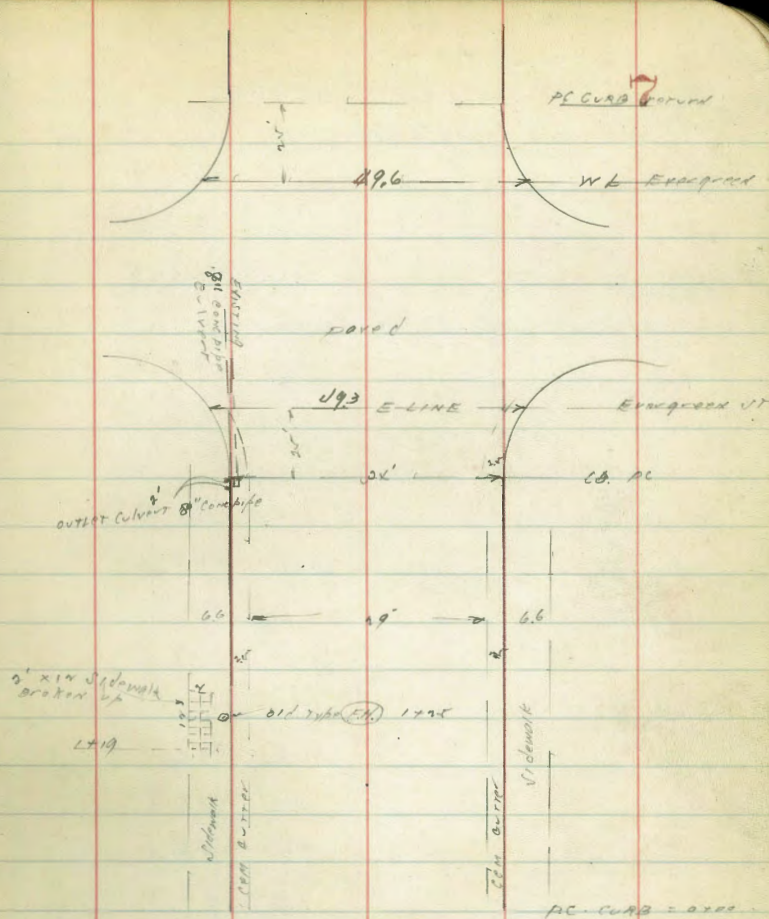


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47.27

47.3

cb.	3.0	44.3			
$\frac{1}{4}$	2.4	44.9			
$\frac{1}{2}$	2.0	45.3			
$\frac{3}{4}$	1.8	45.5			
cb	1.9	45.4			
edge	2.15	45.1			
gut	2.69	44.6			
S. Top cb.	1.62	45.85			
0+00 = P.C. of Return					
s top cb.	1.26	46.0			
gut	2.03	45.3			
edge	1.62	45.7			
$\frac{1}{4}$	1.6	45.7			
$\frac{1}{2}$	1.7	45.6			
$\frac{3}{4}$	2.3	45.0			
edge	2.61	44.7			
gut	2.93	44.4			
N. top cb.	2.22	45.1			
T.P.	11.02	55.89	240	44.87	<u>55.9</u>
0+25					
N. Top cb.	10.16	45.7			
gut.	10.83	45.1			
edge	10.55	45.4			
$\frac{1}{4}$	10.3	45.6			
$\frac{1}{2}$	9.9	46.0			
$\frac{3}{4}$	9.8	46.1			



Cross Section of Kingsley st.

From Chatsworth to Rosecrans

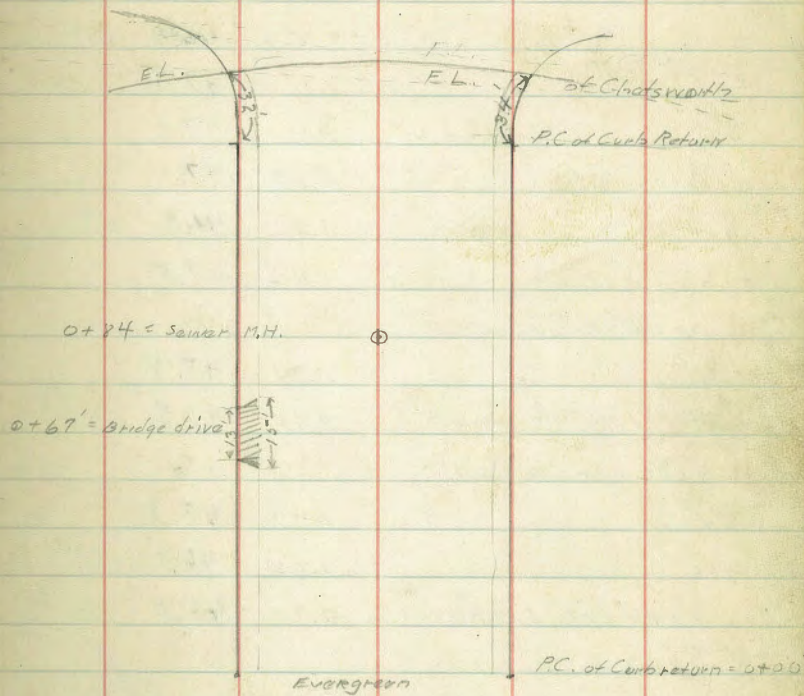
55.89

55.9

edge	9.82	46.1
gut	10.00	45.8
s cb.	9.44	46.5
0+42 = Break in cb. on South. sunken cb.		
Top cb.	9.21	46.7
gut.	9.77	46.1
0+42 = Break in cb. on North. - cb. has sunk.		
Top cb.	10.47	45.4
gut	9.78	46.1
0+50		
s cb.	9.03	46.9
gut	9.62	46.3
edge	9.35	46.6
1/4	9.2	46.7
1/2	9.4	46.5
3/4	9.6	46.3
edge	9.91	46.0
gut	10.21	45.7
N Top cb.	9.52	46.4
0+65 = B. on South.		
Top cb.	8.49	47.4
gut.	9.11	46.8
0+75		
N. cb.	8.78	47.0
gut	9.47	46.4

8

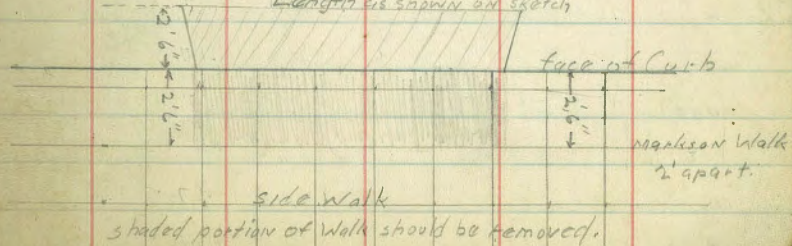
Chatsworth - Paved



Detail showing walk to be removed to
make runways.

Bridged gutter drain should be removed

Length is shown on sketch



55.89

55.9

edge	9.20	46.7	
$\frac{1}{4}$	9.0	46.9	
$\frac{1}{2}$	8.6	47.3	
$\frac{3}{4}$	8.8	47.1	
edge	8.77	47.1	
gut	9.02	46.9	46.57
s. cb.	8.42	47.5	
0+84 = Br. on South.			
Top cb.	8.37	47.5	
gut	8.98	46.9	46.91
0+82 = Br. on North			
Top cb.	8.57	47.3	
gut.	9.25	46.7	46.64
0+94 = Ex. S.M.H. on Rim.			
1+00	7.93	48.0	
s. cb.	7.88	48.0	
gut	8.48	47.4	
edge	8.22	47.7	
$\frac{1}{4}$	8.1	47.8	
$\frac{1}{2}$	7.9	48.0	
$\frac{3}{4}$	8.3	47.6	
edge	8.52	47.4	
gut	8.74	47.2	
N. cb.	8.08	47.8	

1+16 = B. on South

55.89

55.9

9

Top cb.	7.47	48.4	
gut.	8.04	47.9	
1+25			
N. cb.	7.63	48.3	
gut	8.30	47.6	
edge	8.07	47.8	
$\frac{1}{4}$	7.7	48.2	
$\frac{1}{2}$	7.5	48.4	
$\frac{3}{4}$	7.5	48.4	
edge	7.67	48.2	
gut	7.94	48.6	
s. cb.	7.33	48.6	
1+39 = Br. on South.			
Top cb.	7.02	48.9	
gut.	7.68	48.2	
1+50			
s. cb.	6.62	49.3	
gut	7.24	48.7	
edge	7.00	48.9	
$\frac{1}{4}$	6.9	49.0	
$\frac{1}{2}$	6.8	49.1	
$\frac{3}{4}$	7.1	48.8	
edge	7.39	48.5	
gut	7.62	48.3	
N. cb.	6.95	49.0	

55.89

1+63 = BRION South

Top cb	6.15	49.7
gut	6.79	49.1

1+64 = BRION North

Top cb	6.41	49.5
gut	7.09	48.8

1+75-

N. cb	6.05	49.9
gut	6.73	49.2
edge	6.58	49.3
$\frac{1}{4}$	6.3	49.6
E	6.1	49.8
$\frac{1}{4}$	6.1	49.8
edge	6.18	49.7
gut	6.44	49.5
S. cb	5.86	50.1

1+76 = BRION South

Top cb	5.48	50.4
gut	6.10	49.8

2+00

S. cb	5.23	50.7
gut	5.84	50.1
edge	5.54	50.4
$\frac{1}{4}$	5.4	50.5
E	5.5	50.4
$\frac{1}{4}$	5.7	50.2

55.9

edge	5.94	50.0
gut	6.11	49.8
N. cb	5.42	50.5

2+25

N. cb	4.85	51.1
gut	5.53	50.4
edge	5.33	50.6
$\frac{1}{4}$	5.1	50.8
E	4.8	51.1
$\frac{1}{4}$	4.9	51.0
edge	5.07	50.8
gut	5.52	50.4
S. cb	4.71	51.2

2+45.5 = outlet of culvert on South

Top cb	4.19	51.7
gut	4.53	51.4
Flow line of pipe	5.44	50.5

2+50 = P.C. of Curb Returns

S. cb	4.09	51.8
gut	4.51	51.4
edge	4.33	51.6
$\frac{1}{4}$	4.2	51.7
E	4.2	51.7
$\frac{1}{4}$	4.3	51.4
edge	4.57	51.3
gut	4.83	51.1

55.9

10

55.89

55.9

N. cb.	4.18	51.7
Sec. "A" = E.L. Locust. See Sketch		
N. Top cb.	3.68	52.21
gut	4.34	51.55
edge	4.07	51.8
cb.	3.9	52.0
$\frac{1}{4}$	3.9	52.0
$\frac{1}{2}$	3.8	52.1
$\frac{3}{4}$	3.8	52.1
cb	3.8	52.1
edge	4.00	51.9
gut	4.17	51.72
s. Top cb	3.53	52.36

Sec. "B"

s. Top cb	3.24
gut	3.88
edge	3.66
cb. line	3.5
$\frac{1}{4}$	3.6
$\frac{1}{2}$	3.5
$\frac{3}{4}$	3.6
cb	3.5
edge	3.92
gut	4.19
N. Top cb.	3.53

55.89

55.9

Sec. "B" = cut line of Locust

11

N.L.	3.7	52.2
cb	3.3	52.6
$\frac{1}{4}$	3.3	52.6
$\frac{1}{2}$	3.4	52.5
$\frac{3}{4}$	3.4	52.5
cb	3.4	52.5
s.L.	3.2	52.7
Sec. "C" = E. $\frac{1}{4}$		
s.L.	2.9	53.0
cb	3.2	52.7
$\frac{1}{4}$	3.1	52.8
$\frac{1}{2}$	3.1	52.8
$\frac{3}{4}$	3.1	52.8
cb	3.1	52.8
N.L.	3.3	52.6

Sec. "D" = E

N.L.	2.9	53.0
cb.	2.8	53.1
$\frac{1}{4}$	2.8	53.1
+ 6' = N. edge of base of Okn. lamp post.	2.8	53.1
Top corn.	2.34	53.6
$\frac{1}{2}$ on corn.	2.34	53.6
+ 2 $\frac{1}{2}$ = S. edge of lamp post on corn.	2.34	53.6
on ground.	2.8	53.1
$\frac{1}{4}$	3.0	52.9

55.89

55.9

55.89

55.9**12**

cb.	3.1	52.8
s.l.	2.7	53.2
Seci "E" = W.L. $\frac{1}{4}$		
s.l.	2.5	53.4
cb.	2.9	53.0
$\frac{1}{4}$	2.8	53.1
$\frac{1}{2}$	2.7	53.2
$\frac{1}{4}$	2.7	53.2
cb.	2.8	53.1
N.L.	2.9	53.0
Seci "F" = cb. line of locust		
N.L.	2.8	53.1
cb.	2.6	53.3
$\frac{1}{4}$	2.6	53.3
$\frac{1}{2}$	2.6	53.3
$\frac{1}{4}$	2.6	53.3
cb.	2.7	53.2
s.l.	2.5	53.4
Seci "G" = W.L. of locust		
s Top cb.	2.52	53.31
gut	2.22	52.69
edge	2.79	53.1
$\frac{1}{4}$ cb.	2.5	53.4
$\frac{1}{4}$	2.3	53.6
$\frac{1}{2}$	2.3	53.6
$\frac{1}{4}$	2.3	53.6

cb.	2.5	53.4
edge	2.69	53.20
gut.	2.06	52.83
N. Top cb.	2.43	53.5
0+00 = P.C. at Returns		
N cb.	1.87	54.0
gut	2.53	53.4
edge	2.25	53.7
$\frac{1}{4}$	2.0	53.9
$\frac{1}{2}$	1.9	54.0
$\frac{1}{4}$	2.1	53.8
edge	2.35	53.7
gut	2.67	53.2
s cb.	2.05	53.9
T.P.	11.83	65.79
0+25		
s cb.	11.19	54.6
gut.	11.81	54.0
edge	11.53	54.3
$\frac{1}{4}$	11.4	54.4
$\frac{1}{2}$	11.2	54.6
$\frac{1}{4}$	11.3	54.5
edge	11.45	54.3
gut	11.68	54.1
N. cb	11.02	54.8
0+50		

65.8

65.79

65.8

65.79

65.8

13

N. cb	1030	55.5
gut	10.96	54.9
edge	10.73	55.1
$\frac{1}{4}$	10.5	55.3
ϵ	10.4	55.4
$\frac{1}{4}$	10.6	55.2
edge	10.73	55.1
gut	11.02	54.8
scb.	12.42	55.4
0+75-		
scb	9.67	56.1
gut	10.28	55.5
edge	10.04	55.8
$\frac{1}{4}$	9.8	56.0
ϵ = P.M. of B.M.H.	9.39	56.4
$\frac{1}{4}$	9.8	56.0
edge	9.96	55.8
gut	10.23	55.6
N. cb.	9.57	56.2
1+00		
N. cb.	8.85	57.0
gut	9.53	56.3
edge	9.30	56.5
$\frac{1}{4}$	9.1	56.7
ϵ	9.0	56.8
$\frac{1}{4}$	9.2	56.6

edge	9.32	56.5
gut	9.57	56.2
scb.	8.92	56.9
1+25-		
scb	8.20	57.6
gut	8.83	57.0
edge	8.58	57.2
$\frac{1}{4}$	8.4	57.4
ϵ	8.3	57.5
$\frac{1}{4}$	8.5	57.3
edge	8.56	57.2
gut	8.84	57.0
N. cb.	8.17	57.6
1+50		
N. cb.	7.39	58.4
gut	8.06	57.7
edge	7.83	58.0
$\frac{1}{4}$	7.6	58.2
ϵ	7.6	58.2
$\frac{1}{4}$	7.7	58.1
edge	7.85	58.0
gut	8.12	57.7
scb.	7.50	58.3
1+75-		
scb.	6.74	59.1
gut.	7.37	58.4

65.79

edge	7.09	58.7
$\frac{1}{4}$	6.8	59.0
$\frac{1}{2}$	6.9	59.0
$\frac{3}{4}$	6.9	58.9
edge	7.13	58.7
gut	7.39	58.4
N cb.	6.72	59.1
2+00		
N cb.	6.04	59.8
gut	6.70	59.1
edge	6.42	59.4
$\frac{1}{4}$	6.1	59.7
$\frac{1}{2}$	6.0	59.8
$\frac{3}{4}$	6.1	59.7
edge	6.41	59.4
gut	6.61	59.2
scb	5.96	59.8
2+25		
scb	5.26	60.5
gut	5.98	59.8
edge	5.66	60.1
$\frac{1}{4}$	5.6	60.2
$\frac{1}{2}$	5.4	60.4
$\frac{3}{4}$	5.5	60.3
edge	5.78	60.0
gut	5.98	59.8

65.8

N. cb.	5.32	60.5	14
2+48 = outlet of Culvert on South			
Top cb.	4.57	61.2	
gut	5.01	60.8	
Flow line of pipe	5.77	60.1	
2+50			
N cb.	4.62	61.2	
gut	5.28	60.5	
edge	5.00	60.8	
$\frac{1}{4}$	4.8	61.0	
$\frac{1}{2}$	4.7	61.1	
$\frac{3}{4}$	4.8	61.0	
edge	4.73	61.1	
gut	4.95	60.9	
scb.	4.52	61.3	
E. L. of Evergreen st on paving			
S. top cb.	3.87	61.9 P	
gut	4.53	61.2 O	
cb. line	4.15	61.6	
$\frac{1}{4}$	3.87	61.9	
$\frac{1}{2}$	3.83	61.9 B	
$\frac{3}{4}$	3.96	61.9	
cb. line	4.25	61.6	
gut	4.70	61.0 B	
N. top cb.	4.07	61.7 P	
T.P.	9.16	72.98	1.97 63.82

65.79

65.8

72.98

73.0

72.98

73.0

15

W.L. Evergreen st. on paving
 N. Top cb. 9.62 63.86
 gut 10.31 62.67
 cb line 9.88 63.1
 $\frac{1}{4}$ 9.67 63.3
 2 9.60 63.38
 $\frac{1}{4}$ 9.54 63.5
 cb line 9.68 63.3
 gut 9.72 63.26
 S Top cb. 9.08 63.90

0+00 = P.C. of Returns

s cb. 9.10 63.9
 gut 9.72 63.3
 edge 9.49 63.5
 $\frac{1}{4}$ 9.3 63.7
 2 9.2 63.8
 $\frac{1}{4}$ 9.3 63.7
 edge 9.55 63.5
 gut 9.21 63.2
 N cb. 9.15 63.8

0+25

N cb. 8.60 64.4
 gut 9.24 63.8
 edge 8.94 64.1
 $\frac{1}{4}$ 8.7 64.3
 2 8.6 64.4

$\frac{1}{4}$
 edge
 gut
 s cb
 0+50

s cb
 gut
 edge
 $\frac{1}{4}$
 2

$\frac{1}{4}$
 edge
 gut
 N cb.

0+75

N cb.
 gut
 edge
 $\frac{1}{4}$
 2

$\frac{1}{4}$
 edge
 gut
 s cb.

0+84 = S.M.H. ON P.M.

1+00

8.6 64.4
 8.71 64.3
 8.94 64.0
 8.29 64.7

7.57 65.4
 8.20 64.8
 7.96 65.0
 8.0 65.0
 7.9 65.1

8.1 64.9
 8.28 64.7
 8.58 64.4
 7.94 65.1

7.23 65.8
 7.89 65.1
 7.62 65.4
 7.3 65.7
 7.1 65.9

7.2 65.8
 7.20 65.8
 7.48 65.5
 6.83 66.2
 6.67 66.3

72.98

73.0

s cb	6.02	67.0
gut	6.68	66.3
edge	6.48	66.5
$\frac{1}{4}$	6.4	66.6
2	6.4	66.6
$\frac{1}{4}$	6.8	66.2
edge	7.02	66.0
gut	7.23	65.8
N cb.	6.55	66.5
1+25		
N cb.	5.97	67.0
gut	6.63	66.4
edge	6.38	66.6
$\frac{1}{4}$	6.0	67.0
2	5.7	67.3
$\frac{1}{4}$	5.7	67.3
edge	5.73	67.3
gut	5.93	67.1
s cb	5.28	67.7
1+50		
s cb	4.48 4.8	68.5
gut	5.13	67.9
edge	4.96	68.0
4	5.0	68.0
2	5.0	68.0
$\frac{1}{4}$	5.4	67.6

72.98

73.0

16

edge	5.75	67.3
gut	5.99	67.0
N cb.	5.33	67.7
1+75 - P.C. of Returns		
N cb.	4.78	68.2
gut	5.43	67.6
edge	5.18	67.8
$\frac{1}{4}$	4.1	68.2
2	4.3	68.7
$\frac{1}{4}$	4.2	68.8
edge	4.20	68.8
gut	4.40	68.6
s cb.	3.75	69.2

E.L. of Chatsworth on Paving. See sketch for distance

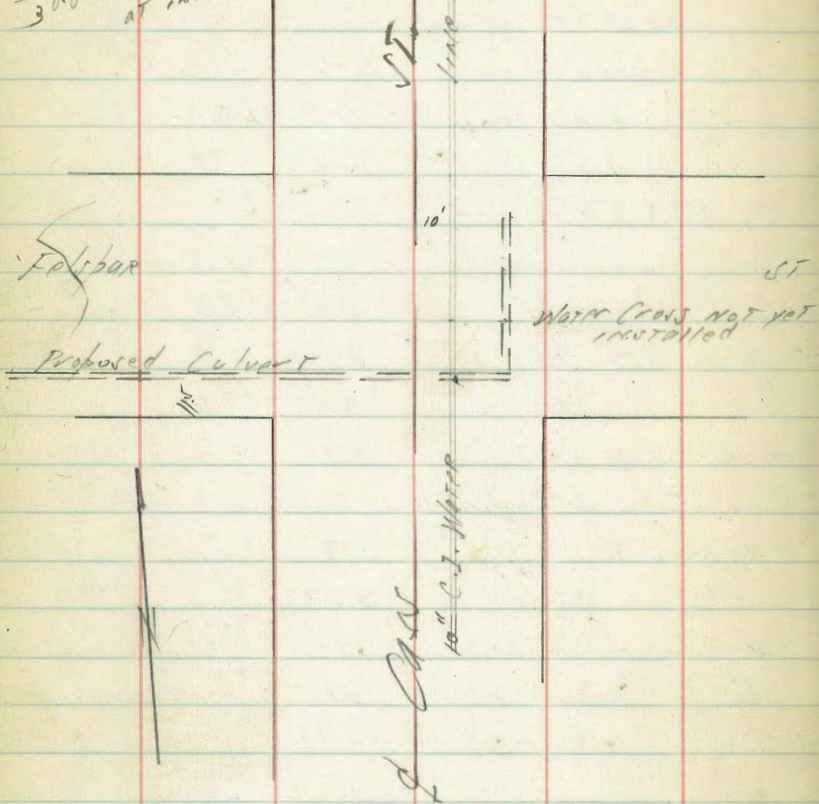
s. Top of cb.	3.13	72.98	69.9
gut	3.99	$\frac{0.12}{72.86}$	69.0
curve line produced	3.71	$\frac{0.26}{72.60}$	69.3
$\frac{1}{4}$	3.75	$\frac{0.26}{72.84} = \text{BM Chats. James}$	
2	3.90	$\frac{0.12}{74.00}$	
$\frac{1}{4}$	4.22	$\frac{1.263}{61.37}$	69.08
curve line	4.63	$\frac{0.49}{61.86}$	68.4
gut	5.30	$\frac{13.02}{48.44}$	67.68
N. top cb.	4.39	$\frac{0.50}{49.34}$	68.6
		$\frac{7.64}{41.70}$	
		$\frac{41.75}{41.75} = \text{correct elev.}$	

benches .05 in error.

Elev. of WATER MAIN
Folger & Cass

11/9/04
Mosco

28.5
8.20
36.7
5.93
30.81 = Elev. of Top of 10" water pipe
at intersection of culvert



$$30.81 = \text{Top}$$

$$\frac{30.81}{10} = \text{Bottom of 10" MAIN}$$

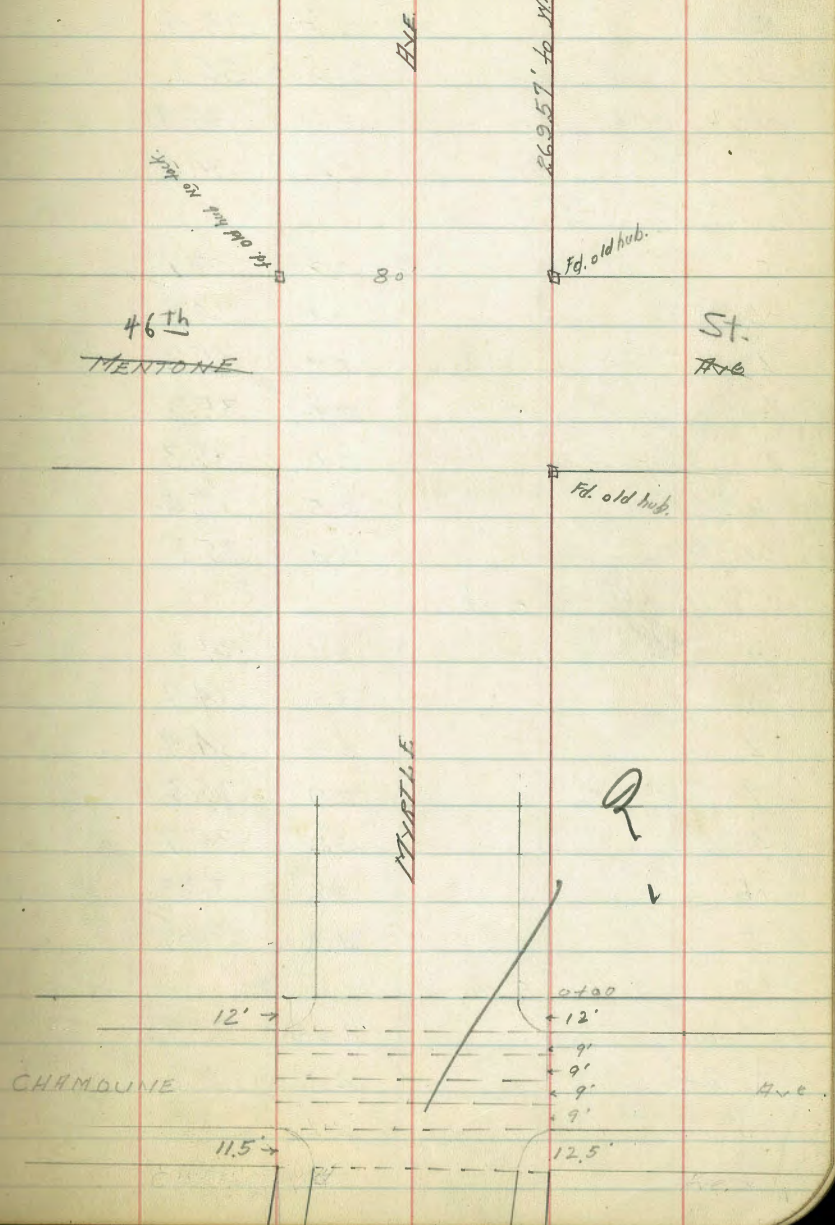
Walker
Rupinger
Leaky
No. 1000
11-11-28

Cross Section MYRTLE Ave
Bet. Chamoune and Mentone
80' wide 22' cbs. 9' 1/2 s. Bet. E. L. Mentone
And N. L. 47th St.

2.05 337.94 335.89 N.W. B.P. Myrtle
Chamoune

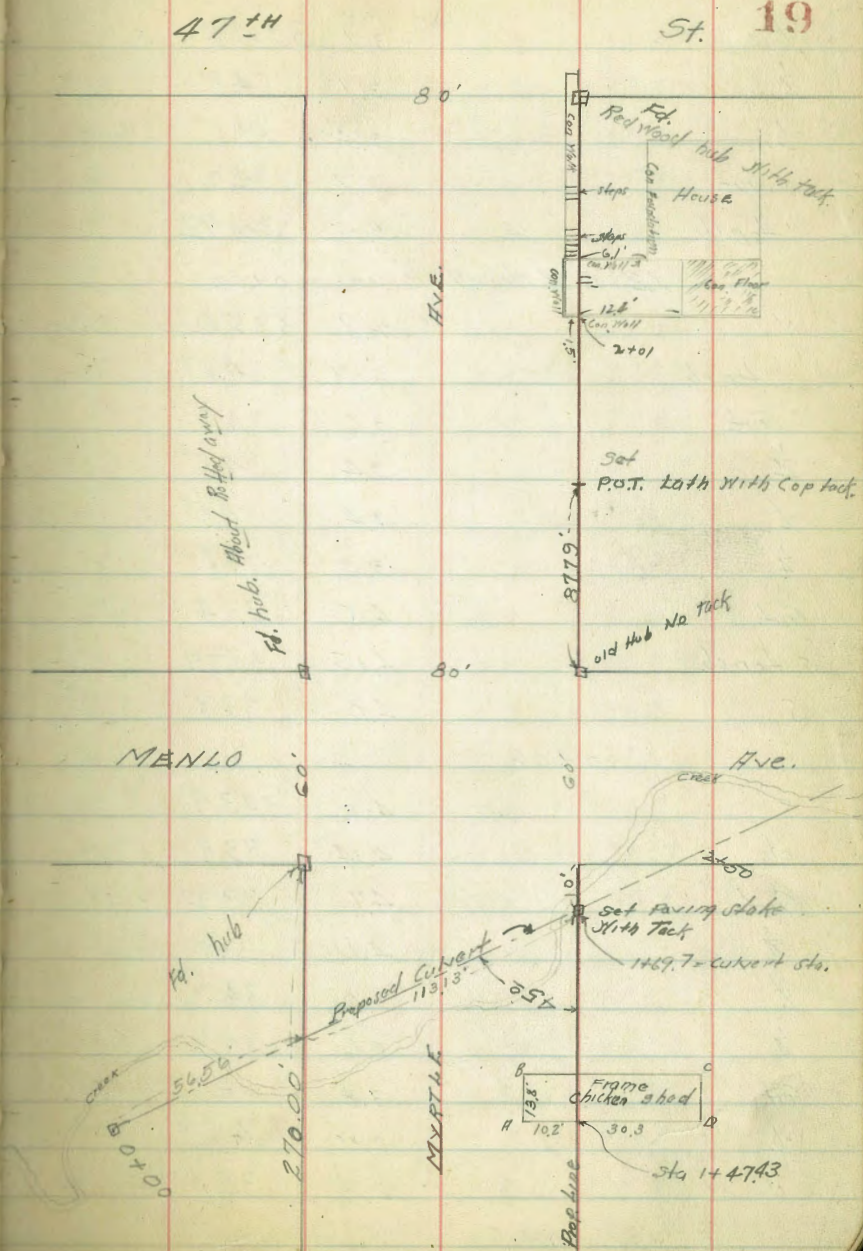
N.L. Chamoune

N	1.9	336.0
N top cb	2.15	357.9
" Gut. on Pav.	2.78	335.16
" 1/2 " "	2.64	35.30
1/2 " "	2.75	35.19
S 1/2 " "	3.12	34.82
" Gut. " "	3.71	34.23
" top cb	3.04	34.90
S	2.8	35.1
N. L. cb. Chamoune		
S top cb	3.01	34.93
S Gut.	3.8	34.1
cb	3.0	34.9
1/2	3.9	35.0
1/2	3.6	35.3
1/2	2.4	35.5
cb	3.7	35.2
N Gut.	2.8	35.1
" top cb	2.10	35.8
N 1/2		
N	2.6	35.3
cb	2.6	35.3



337.94

$\frac{1}{4}$	2.4	
$\frac{1}{2}$	2.5	35.4
$\frac{1}{4}$	2.8	35.1
cb.	3.0	34.9
S	3.4	34.5
S		
S	3.7	34.7
cb.	3.1	34.8
$\frac{1}{2}$	2.7	35.2
$\frac{1}{2}$	2.6	35.3
$\frac{1}{4}$	2.6	35.3
cb.	2.5	35.4
N	2.4	35.5
N		
E $\frac{1}{2}$		
N	3.1	34.8
cb.	3.0	34.9
$\frac{1}{4}$	3.0	34.9
$\frac{1}{2}$	2.9	35.0
$\frac{1}{4}$	3.2	34.7
cb.	3.6	34.3
S	4.0	34.9
S		
E cb.		
S top cb.	4.03	33.91
" Gut.	4.5	33.4
cb.	4.1	33.8
$\frac{1}{4}$	3.4	34.5



2	3.1	334.8
2	3.1	34.8
cb.	3.4	34.5
N Gut.	3.7	34.2
" top cb.	3.02	34.92
12' E Ecb. Chamoune - 0+00		
N	2.9	335.0
" top cb.	3.07	34.87
" Gut.	3.6	34.3
2	3.4	34.5
2	3.4	34.5
2	3.8	34.1
Gut.	4.5	33.4
S top cb.	4.15	33.79
S	4.0	33.9
0+08		
S	4.0	333.9
cb.	4.14	33.8
Gut.	4.7	33.2
2	4.1	33.8
2	3.6	34.3
2	3.6	34.3
Gut.	3.8	34.1
cb.	3.11	34.83
N	2.8	35.1

0+50

N	4.3	333.6
cb.	4.54	333.40
Gut.	5.2	32.7
2	5.0	32.9
2	4.8	33.1
2	5.4	32.5
Gut.	6.0	31.9
cb.	5.52	32.42
S	5.2	32.7
1+00		
S	6.7	331.2
cb.	7.19	30.75
Gut.	7.9	30.0
2	7.1	30.8
2	6.7	31.2
2	6.8	31.1
Gut.	7.0	30.9
cb.	6.27	31.67
N	5.8	32.1
1+32.57 = 116. Alley = End East. cb. + Walk		
N on top cb. (Alley Return)	6.92	331.02
" cb " " " "	7.24	30.70
" Gut.	7.6	30.3
2	7.5	30.4
2	7.6	30.3
2	8.1	29.8

Ent.		8.3	329.6
S top cb.	(Alley Return)	8.16	29.78
S on top cb.	(Alley Return)	7.83	30.11
T.P.	3.07	332.81	8.20
	1+50		329.74
S		3.3	329.5
cb.		3.2	29.6
$\frac{1}{4}$		3.0	29.8
$\frac{1}{2}$		2.7	30.1
$\frac{3}{4}$		2.5	30.3
+10		2.3	30.5
+12		2.7	30.1
cb.		2.4	30.4
N		1.8	31.0
1+72 = $\frac{1}{2}$ Con Walk on N 1' in st.		2.00	30.8
	1+93		
N		3.2	329.6
cb.		3.5	29.3
$\frac{1}{4}$		4.0	28.8
$\frac{1}{2}$		4.2	28.6
$\frac{3}{4}$		4.4	28.4
cb.		4.6	28.2
S		4.6	28.2
	2+00		
S		5.2	327.6
cb.		4.9	27.9

$\frac{1}{4}$		4.6	328.2
$\frac{1}{2}$		4.4	28.4
$\frac{3}{4}$		4.2	28.6
cb.		3.7	29.1
N		3.4	29.4
2+18 = $\frac{1}{2}$ Con Walk on N 2' in st.		3.64	29.2
	2+25		
N		3.8	329.0
cb.		4.0	28.8
$\frac{1}{4}$		4.4	28.4
$\frac{1}{2}$		4.9	27.9
$\frac{3}{4}$		5.2	27.6
cb.		5.5	27.3
S		5.8	27.0
	2+50		
S		6.2	326.6
cb.		5.7	27.1
$\frac{1}{4}$		5.4	27.4
$\frac{1}{2}$		5.1	27.7
$\frac{3}{4}$		4.7	28.1
cb.		4.8	28.0
N		5.3	27.5
2+56 = $\frac{1}{2}$ Con Walk on N		5.52	25.29
	2+77.69 ^{on N} = 2+78.93 on S = Nlu Mentone		15' in st. 5' in st. 12' cb. 9' $\frac{1}{4}$ S
N		6.4	326.4
+2		7.0	25.8

cb.	6.6	326.2
$\frac{1}{2}$	6.0	26.8
$\frac{2}{2}$	5.5	27.3
$\frac{1}{2}$	5.7	28.1
cb.	5.6	28.2
S	6.3	26.5

M cb.

S	6.3	326.5
cb	6.1	26.7
$\frac{1}{2}$	5.8	27.0
+8	6.0	26.8
$\frac{1}{2}$	6.4	26.4
$\frac{1}{2}$	7.2	25.6
cb	8.2	24.5
N	9.3	23.5
+5	10.0	22.8

M $\frac{1}{2}$ Mentore

-5	10.4	322.4
N	9.7	23.1
cb	8.4	24.4
$\frac{1}{2}$	8.4	24.4
$\frac{1}{2}$	7.2	25.6
$\frac{1}{2}$	6.7	26.6
cb.	6.3	26.5
S	6.4	26.4

E

S	6.6	326.2
cb	6.8	26.0
$\frac{1}{2}$	7.0	25.8
$\frac{1}{2}$	8.2	24.6
$\frac{1}{2}$	8.8	24.0
cb	9.7	23.1
N	10.4	22.4
+10	10.5	22.3

E $\frac{1}{2}$

-10	12.1	320.7
N	11.2	21.6
cb	10.2	22.6
$\frac{1}{2}$	9.6	23.2
$\frac{1}{2}$	9.3	23.5
$\frac{1}{2}$	8.4	24.4
cb	7.4	25.4
S	7.2	25.6

E cb.

S	8.1	324.7
+8	8.0	24.8
cb	8.8	24.0
$\frac{1}{2}$	9.3	23.5
$\frac{1}{2}$	10.1	22.7
$\frac{1}{2}$	10.9	21.9
cb	11.6	21.2
N	12.3	20.5

332.81

+10		13.2	319.6
		Note: From here to 47th st	
		E.L. Mentage = 0+00 22 cbs 9' 75.	
-10		12.5	318.3
N		14.2	18.6
cb		12.7	20.1
$\frac{1}{2}$		12.2	20.6
$\frac{1}{2}$		12.0	20.8
$\frac{1}{4}$		11.3	21.5
cb		10.8	22.0
+10		9.7	23.1
S		9.6	23.2
	0+25		
-5		11.8	321.0
S		12.0	20.8
+12		12.2	20.6
cb		13.0	19.8
$\frac{1}{2}$		13.8	19.0
$\frac{1}{2}$		14.2	18.6
$\frac{1}{2}$		15.0	17.8
cb		15.2	17.6
+10		15.7	17.1
N		16.8	16.0
+10		18.1	14.7
T.P.	1.05	320.95	18.91 319.90
	0+50		
-15		10.4	310.6

320.95

23

N		9.5	311.5
cb		7.0	14.0
$\frac{1}{4}$		5.8	15.2
$\frac{1}{2}$		4.7	16.3
$\frac{1}{2}$		4.0	17.0
cb		3.5	17.5
+12		2.3	18.7
S		2.4	18.6
+5		2.0	19.0
	0+75		
-5		4.2	316.8
S		4.3	16.7
cb		6.4	14.6
$\frac{1}{4}$		8.1	12.9
$\frac{1}{2}$		9.6	11.4
$\frac{1}{2}$		11.6	309.4
cb		12.9	07.1
+9		15.4	05.6
N		17.7	03.3
+20		20.5	300.5
	0+85		
-20		23.7	297.3
N		20.9	300.1
$\frac{1}{2}$		19.4	01.6
$\frac{1}{4}$		14.6	06.4
$\frac{1}{2}$		12.6	88.4

32095

1/2		10.0	311.0
cb		84	12.6
+10		64	14.6
5		52	15.8
+5		4.8	16.2
	1+00		
-10		6.0	315.0
5		7.4	13.6
+15		97	11.3
cb		11.4	09.6
+5		12.8	08.2
T.P.	0.99 308.97	12.97	307.98
1/4		2.3	06.7
1/2		5.3	03.7
1/2		7.4	01.6
cb		10.3	298.7
+17		14.9	294.1
N		15.8	293.2
+15		18.5	90.5
+30		21.0	88.0
	1+30		
-45		29.1	279.9
-30		29.0	280.0
-15		27.5	281.5
N		24.9	284.1
+9		23.3	285.7

30897

cb		50.1	288.9
1/2		16.3	92.7
1/2		13.0	96.0
1/2		9.5	98.5
cb		6.8	302.2
+12		2.8	06.2
5		0.5	08.5
+10		+1.3	10.3
	Location chicken shed. Page 19		
A on Ground		7.3	301.7
A on Roof		+8.3	17.3
B on Ground at chicken shed		10.1	298.9
B on Roof of " "		+10.3	319.3
C on Ground at " "		3.0	306.0
C on Roof		+10.3	19.3
D " "		+8.3	17.3
D on Ground		+2.0	11.3
	1+43		
-10		+0.4	309.4
-6		0.6	08.4
5		2.9	06.1
+4		3.9	05.1
+10		6.1	02.9
cb		9.2	299.8
1/2		12.3	296.7
1/2		15.8	293.2

24

z		19.5	289.5
cb.		22.7	286.3
+11		25.8	283.2
N		27.7	81.3
+11		30.9	78.1
+20		31.6	77.4
+45		29.7	79.3
	1+52		
-45		29.3	279.7
-20		31.6	77.4
N		32.7	76.3
+10		32.7	76.3
+13		28.7	80.3
cb.		26.2	82.8
z		22.9	86.1
z		19.4	89.6
z		15.1	93.9
cb.		11.7	97.3
+11.8 at oblique shed		8.2	300.8
S under shed on ground		6.7	02.3
+10 " " " "		5.7	03.3
TP	0.59	297.23 ^v	12.33 296.64
	1+62		
-10		+4.6	301.8
S		+3.0	300.2
+17		0.6	296.6

cb		2.6	294.6
z		6.0	91.2
z		11.0	86.2
z		15.4	81.8
cb.		18.2	79.0
+6		21.8	75.4
+13		21.6	75.6
N		20.4	76.8
+20		19.0	78.2
+22		19.9	77.3
+45		18.8	78.4
	Levels For Proposed Culvert Location Page 19		
-52 in Creek Bed		17.0	280.2
-43 on Bank		15.6	81.6
0+00 on stub		17.44	79.8
+13 = N edge creek		19.3	77.9
+27 = S " "		20.0	77.2
+29 = on Bank at S edge creek		19.0	78.2
+50		19.3	77.9
+70		21.0	76.2
+25 = N edge Creek		22.8	74.4
+35 = in " "		23.4	73.8
+39 = S edge creek on Bank		22.8	74.4
+50		23.1	74.1
+69.7 = Intersection of culvert and S edge Myrtle on stub		23.56	73.67
+100		24.5	72.7
+50 = End of line		26.4	70.8

z Creek
30' to E

creek 20' W

" 15' W

creek 5' E

" " "

creek 15' E

creek 35' E

297.23

	1+75		
-40		16.6	280.6
-30		15.1	82.1
-12		18.6	78.6
N		19.7	77.5
+8		20.7	76.5
+15		21.5	75.7
+20		22.1	75.1
cb.		22.3	74.9
$\frac{1}{4}$		19.1	78.1
$\frac{1}{4}$		15.3	81.9
$\frac{1}{4}$		10.3	86.9
cb.		5.2	92.0
+8		2.6	94.6
+9		1.6	95.6
5		+0.7	96.5
+15		+3.4	300.6
	1+90		
-15		+0.1	297.3
5		3.4	93.8
+6		5.5	91.7
+14		8.6	88.6
cb.		12.2	85.0
$\frac{1}{4}$		15.9	81.3
+2		21.0	76.2
$\frac{1}{4}$		21.9	75.3

297.23

26

$\frac{1}{4}$		22.1	275.1
cb.		21.9	75.3
+3		20.7	76.5
+14		19.2	78.0
N		18.6	78.6
+30		13.0	84.2
	1+95		
-30		12.6	284.6
N		18.1	79.1
+8		19.2	78.0
cb.		20.5	76.7
+7		21.6	75.6
$\frac{1}{4}$		22.3	74.9
$\frac{1}{4}$		22.3	74.9
$\frac{1}{4}$		22.1	75.1
+4		21.1	76.1
+5		16.2	81.0
cb.		14.6	82.6
+8		10.1	87.1
+16		5.3	91.9
5		4.7	92.5
+15		1.0	96.2
	2+07		
-20		2.5	294.7
-12		4.4	92.8
-5		9.7	87.5

297.23

S	11.7	285.5
+5	14.2	83.0
+10	14.7	82.5
+20	21.7	75.5
cb	22.1	75.1
+6	22.6	74.6
$\frac{1}{4}$	22.0	75.2
$\frac{1}{2}$	22.0	75.2
$\frac{3}{4}$	21.2	76.0
cb	20.5	76.7
N	18.2	79.0
+30	11.6	85.6
21.87		
-30	7.0	290.2
-10	14.6	82.6
N	16.2	81.0
cb	19.5	77.7
$\frac{1}{4}$	21.2	76.0
$\frac{1}{2}$	21.7	75.5
$\frac{3}{4}$	22.8	74.4
+4	23.4	73.8
cb	23.1	74.1
+8	20.9	76.3
+17	18.4	78.8
S	14.6	82.6
+8	12.0	85.2

297.23

+20	9.0	
21.45		
-25	14.8	282.4
-9	18.4	78.6
S	21.4	75.8
+8	21.2	76.0
cb	22.9	74.3
+4	23.5	73.7
$\frac{1}{4}$	22.8	74.4
$\frac{1}{2}$	21.5	75.7
$\frac{3}{4}$	20.4	76.8
cb	18.2	79.0
N	14.9	82.3
+13	11.2	86.0
+30	4.0	93.2
21.62		
N-20	5.4	281.8
N	13.2	84.0
+9	15.8	81.4
cb	17.9	79.3
$\frac{1}{4}$	20.1	77.1
$\frac{1}{2}$	21.4	75.8
$\frac{3}{4}$	22.1	75.1
+7	22.8	74.4
cb	23.8	73.4
+10	14.0	73.2

27

S	23.8	273.4
+8	23.6	73.6
+20	23.0	74.2
+35	18.5	78.7
	2+69.57 = N.H. Mendel Ave	12' cbs 9' 7/8
S-40	19.9	277.3
S-29	22.8	74.4
S-10	24.3	72.9
S	24.2	73.0
+15	23.7	73.5
cb	23.0	74.2
$\frac{1}{2}$	22.0	75.2
$\frac{1}{2}$	21.0	76.2
$\frac{1}{2}$	19.4	77.8
cb	17.5	79.7
N	13.2	84.0
	N cb.	
N	11.9	85.3
+7	14.1	83.1
cb	17.7	79.5
$\frac{1}{2}$	18.3	78.9
$\frac{1}{2}$	19.5	77.7
$\frac{1}{2}$	20.8	76.4
cb	21.6	75.6
+15	24.1	73.1
S	24.9	72.3

Note: For arts on
North 500 N. School
Notes for Mendel

+9	25.9	271.3
+10	27.2	70.0
+20	26.3	70.9
+21	25.3	71.9
+40	24.5	72.7
	N $\frac{1}{2}$	
-45	25.3	271.9
-25	24.9	72.3
-23	26.8	70.4
-20	26.9	70.3
-18	26.9	70.3
-17	25.8	71.4
-5	25.6	71.6
S	24.1	73.1
+10	23.5	73.7
cb	21.0	76.2
$\frac{1}{2}$	20.0	77.2
$\frac{1}{2}$	18.3	78.9
$\frac{1}{2}$	18.0	79.2
cb	15.9	81.3
+11	14.3	82.9
N	11.0	86.2
	N $\frac{1}{2}$	
N	9.0	89.2
+15	13.3	83.9
cb	13.4	83.8

1/2	15.8	281.4
1	17.4	79.8
1	18.7	78.5
cb.	20.0	77.2
+14	23.3	73.9
5	24.0	73.2
+20	26.9	70.3
+25	26.1	71.1
+28	24.1	73.1
+45	24.3	72.9
	E 1	
-45	24.3	272.9
-37	25.9	72.3
-26	27.9	69.3
-20	27.0	70.2
-15	26.2	71.0
5	23.9	73.3
+19	19.6	77.6
cb.	19.1	78.1
1/2	17.6	79.6
1	15.8	81.4
1/2	14.3	82.9
cb.	12.4	84.8
N	6.5	90.7
	E cb	
N	4.0	293.2

cb.	9.3	287.9	29
1/2	11.4	85.8	
1	13.1	84.1	
1/2	15.1	82.1	
+4	15.9	81.3	
cb.	16.8	80.4	
5	22.6	74.6	
+22	27.2	70.0	
+28	28.6	68.6	
+36	26.1	71.1	
+45	26.3	70.9	
	E.L. MENLO AVE. - 0+00		
-45	27.3	269.9	
-37	27.2	75.0	
-31	27.6	69.6	
-28	24.1	73.1	
-27	27.6	74.6	
-20	24.3	72.9	
5	20.1	77.1	
+10	16.0	81.2	
cb.	12.8	84.4	
1/2	10.6	86.6	
1	8.8	88.4	
1/2	7.0	90.2	
cb.	5.0	92.2	
N	0.2	97.0	

297.83

0+15

-15	+10.0	307.2
N	+6.0	303.2
cb.	+12	298.4
$\frac{1}{4}$	0.5	296.7
$\frac{1}{2}$	1.8	95.4
$\frac{3}{4}$	-4.0	93.2
cb.	7.0	90.2
S	14.0	83.2
+35	22.0	75.2
+45	28.9	68.3

0+30

-35	12.2	285.0
-15	10.0	87.2
S	7.4	89.8
T.P.	12.15	307.84 ✓ 1.54 295.69 ✓
+15	13.6	294.2
cb.	11.8	96.0
$\frac{1}{4}$	10.3	97.5
$\frac{1}{2}$	8.4	99.4
$\frac{3}{4}$	6.1	301.7
+6	4.1	03.7
cb.	3.8	04.0
N	+0.4	08.2
+15	+3.8	11.6

0+42

307.84

-15	+5.7	313.5
N	+2.6	10.4
cb.	14	06.4
$\frac{1}{4}$	2.7	05.1
$\frac{1}{2}$	3.4	04.4
$\frac{3}{4}$	5.3	02.5
cb.	7.4	00.4
+12	9.1	296.7
S	11.9	95.9
+8	13.8	94.0
+35	15.0	92.8
	18.1	89.7

0+53

-25	15.3	292.5
-5	13.3	94.5
S	12.3	95.5
+8	10.1	97.7
cb.	7.0	300.8
$\frac{1}{4}$	6.2	01.6
T.P.	11.82	319.66 ✓ 0.00 307.84
$\frac{1}{2}$	14.6	305.1
$\frac{3}{4}$	12.6	07.1
cb.	11.5	08.2
✓	8.0	11.7
+10	6.0	13.7

0+72

319.66

-10		4.4	315.3
N		6.0	13.7
cb.		9.6	10.1
$\frac{1}{2}$		10.7	09.0
$\frac{1}{2}$		12.1	07.6
$\frac{1}{2}$		13.6	06.1
+4		14.1	05.6
cb.		16.0	03.7
S		21.0	298.7
+25		26.3	93.4
	0+88		
-25		27.4	292.3
-10		22.0	97.7
S		19.8	299.9
+20		14.0	305.7
cb.		13.4	06.3
$\frac{1}{2}$		12.1	07.6
$\frac{1}{2}$		10.9	08.8
$\frac{1}{2}$		9.8	09.9
cb.		8.3	11.4
+10		6.4	13.3
N		4.6	15.1
+5		3.6	16.1
T.P.	8.31 323.42	4.55	315.11
	1+00		
-5		6.1	317.3

On Lot 6
on North
Approx. 1+00

323.42

31

N		7.2	316.2
cb.		11.0	12.4
$\frac{1}{2}$		12.9	10.5
$\frac{1}{2}$		14.0	09.4
$\frac{1}{2}$		15.1	08.3
cb.		16.6	06.8
+10		18.8	04.6
S		24.0	299.4
+15		30.5	292.9
+30		38.6	84.8
+35		40.6	82.8
+20		42.0	81.4
	1+20		
-40		41.0	282.4
-35		41.8	81.6
-35		42.5	80.9
-30		42.6	80.8
-14		34.5	88.9
S		29.2	94.2
+11		22.7	300.7
cb.		17.9	05.5
$\frac{1}{2}$		16.4	07.0
+4		14.4	09.0
$\frac{1}{2}$		13.4	10.0
$\frac{1}{2}$		11.5	11.9
cb.		10.1	13.3

N	5.7	317.7
+5	5.0	18.4
	1+35	
-5	4.8	318.6
N	5.3	18.1
+4	6.2	17.2
+15	9.2	14.2
cb.	10.8	12.6
$\frac{1}{4}$	13.6	09.8
$\frac{1}{2}$	16.2	07.2
$\frac{3}{4}$	19.2	04.2
cb.	22.2	01.2
S	33.5	289.9
+19	40.0	283.4
+25	40.5	82.9
+35	38.0	85.4
+40	35.3	88.1
	1+50	
-35	31.2	292.2
-18	33.6	89.8
-9	37.0	86.4
S	37.0	86.4
+10	31.5	91.9
cb.	27.4	86.0
$\frac{1}{4}$	22.9	300.5
$\frac{1}{2}$	19.7	303.7

$\frac{1}{4}$	16.2	307.2	32
cb.	13.0	10.4	
+15	8.0	15.4	
N	6.0	17.4	
+10	3.7	19.7	
	1+60		
-10	4.3	319.1	
N	7.2	16.2	
+15	11.2	12.2	
cb.	14.5	08.9	
$\frac{1}{2}$	18.9	04.5	
$\frac{3}{4}$	23.7	299.7	
$\frac{1}{4}$	27.3	296.1	
cb.	30.5	292.9	
+7	33.4	290.0	
+17	34.6	288.8	
S	34.0	289.4 ^v	
+16	29.2	294.2	
+30	27.1	296.3	
	1+71		
-30	22.1	301.3	
-20	24.1	299.3	
S	27.6	295.8 ^v	
+6	29.2	294.2	
cb.	30.0	293.4	
+6	30.0	293.4	

32342

$\frac{1}{2}$	29.7	293.7
+4	29.7	93.7
$\frac{1}{2}$	26.6	96.8
$\frac{1}{2}$	22.1	301.3
cb.	17.9	05.5
+10	13.2	10.2
N	9.3	14.1
+6	7.5	15.9
+10	6.3	17.1
	1+83	
-15	7.3	316.1
N	12.1	11.3
+5	13.7	09.7
+12	16.5	06.9
cb.	22.0	01.4
+5	24.8	98.6
$\frac{1}{4}$	25.2	98.2
$\frac{1}{2}$	25.5	97.9
+6	24.1	99.3
$\frac{1}{4}$	24.2	99.2
cb.	22.7	300.7
S	20.3	03.1
+10	20.9	02.7
+20	18.5	04.9
	1+93	
-20	14.2	09.2

32342

33

S	15.4	308.0	
+10	16.0	07.4	
cb.	17.0	06.4	
$\frac{1}{4}$	18.8	04.6	
$\frac{1}{2}$	20.9	02.5	
$\frac{1}{4}$	21.1	02.3	
cb.	22.0	01.4	
+10	20.3	03.1	
+15	15.7	07.7	
N	13.4	10.0	
+20	6.3	17.1	
	See sketch R.19		
	5'01" on top Con. Wall	9.93	13.49
	2+01" at Base " " on Ground	14.5	10.9
	2+05		
-20	9.2	314.2	
N	15.6	07.8	
+8	17.3	06.1	
cb.	16.4	07.0	
+1	14.4	09.0	
$\frac{1}{2}$	13.5	09.9	
$\frac{1}{4}$	12.6	10.8	
cb.	11.6	11.8	
+5	9.8	13.6	
	+20.5 on top Con. Wall	9.68	13.74
S	9.7	13.7	
+15" " Gen. floor.	9.58	13.84	

Sketch P-19				
R+12	on top on Wall on Skine	6.89	316.53	
2+12	at " " " Ground	9.8	13.6	
2+21	on top on Wall on Sk	5.30	18.12	
2+21	" Ground at "	6.6	16.8	
T.P.	888 327.01	529	318.13	
	2+16			
-6.1	at house	10.5	316.5	
S		10.3	16.7	
+1.5	= N edge Wall	10.33	16.68	
+2		11.5	15.5	
cb.		11.2	15.8	
$\frac{1}{4}$		10.4	16.6	
$\frac{1}{2}$		10.0	17.0	
$\frac{3}{4}$		10.3	16.7	
cb.		10.1	16.9	
N		11.7	15.3	
+80		10.8	16.2	
	R+23			
-15		8.5	318.5	
N		7.6	19.4	
+5		7.7	19.3	
cb.		5.6	21.4	
$\frac{1}{4}$		5.9	21.1	
$\frac{1}{2}$		6.2	20.8	
$\frac{3}{4}$		8.5	18.5	
cb.		9.3	17.7	

+20.5	= on N edge Wall	8.80	18.2	
S		8.7	18.3	
+6.1	at house	8.7	18.3	
R+15	= Pepper tree on S	11.5	15.5	
R+23	" " " " "	9.4	17.6	
R+32	" Pepper " " "	8.4	18.6	
R+47	" " " " "	6.8	20.2	
	R+32			
-6.1	at house	7.7	19.3	
S		8.2	18.8	
+1.5	on N edge Wall	8.20	18.81	
cb.		8.0	19.0	
+5		6.2	20.8	
$\frac{1}{4}$		5.8	21.2	
$\frac{1}{2}$		5.3	21.7	
$\frac{3}{4}$		5.2	21.8	
cb.		5.0	22.0	
N		4.0	23.0	
+5		3.7	23.3	
	R+60 = End exist. cb. Returns			
N		3.5	323.5	
N top cb.		4.11	22.90	
" Gut. on ground		4.4	22.6	
$\frac{1}{4}$		4.7	22.3	
$\frac{1}{2}$		4.8	22.2	
$\frac{3}{4}$		5.4	21.6	

16" inst
3" dia, 10" tall
11.5 inst.
2" " 5" "
16" inst.
3" dia 10" tall
16" inst.

S Gut.	6.1	320.9
" top ch	5.59	21.42
S	6.4	20.6
+5	6.4	20.6
R+70		
S	6.2	20.8
+19 on top ch	5.77	21.24
+19 " Gut on Porosity	6.24	20.77
ch " "	6.02	20.99
$\frac{1}{2}$ " "	5.35	21.66
$\frac{1}{2}$ " "	4.91	22.10
$\frac{1}{2}$	4.65	22.36
cb	4.58	22.43
+2 on Gut " "	4.59	22.42
+2 " top ch	3.89	23.12
X	3.3	23.7
BR in File		
chk. on SW. Spk. Myrtle 147 $\frac{1}{2}$	2.67	322.34'
T.P. 11.73	335.90'	3.44 323.57'
T.P. 4.50	339.25'	0.55 334.75'

← This Mt. used on Cross Section Notes Page 38 For check out see
see levels pages 36 to 40

Walker
Rup. 11/19/28
J. 11/19/28

Cross Section Mendo Ave. 60' wide 12' obs 9' AS
From S.L. Dwight to N.L. Myrtle Ave

339.25

36

339.25 = π from Page 35

E	1.2	338.1	
" top cb.	1.38	37.87	
" Gut. on Pav.	1.82	37.43	
$\frac{1}{4}$ " "	1.68	37.57	
$\frac{1}{2}$ " "	1.71	37.54	
$\frac{1}{4}$ " "	1.94	37.31	
Gut " "	2.36	36.89	
π top cb.	1.90	37.35	
π	1.8	37.5	
0+10			
π	2.2	37.1	
cb.	1.7	37.6	
$\frac{1}{4}$	1.8	37.5	
$\frac{1}{2}$	1.6	37.7	
$\frac{1}{4}$	1.3	38.0	
cb.	1.3	38.0	
E	1.2	38.1	
0+20 = $\frac{1}{2}$ Cor. Walk on π	2.08	37.17	4' side on line
0+50			
E	2.0	37.3	
cb.	2.4	36.9	
$\frac{1}{4}$	2.2	37.1	
$\frac{1}{2}$	2.3	37.0	
$\frac{1}{4}$	2.4	36.9	
cb.	2.5	36.8	

π	2.7	336.6	
	1+00		
π	4.0	335.3	
+6	4.3	35.0	
cb.	4.0	35.3	
$\frac{1}{2}$	4.0	35.3	
$\frac{1}{2}$	3.4	35.9	
+3	3.1	36.2	
$\frac{1}{4}$	3.2	36.1	
cb.	3.2	36.1	
E	3.0	36.3	
1+15 = $\frac{1}{2}$ Euc. tree on E	2.9	36.4	
+31 = " " " "	3.4	35.9	
1+18			
E	3.3	36.0	
cb.	3.6	35.7	
$\frac{1}{4}$	3.4	35.9	
+7	3.3	36.0	
$\frac{1}{2}$	3.5	35.8	
$\frac{1}{4}$	4.3	35.0	
+3	4.6	34.7	
cb.	4.5	34.8	
π	4.4	34.9	
1+50			
π	5.6	33.7	
cb.	5.6	33.7	

2' Buck.
15 dia 35' high.
2' Buck.
2' dia 40' high.

33925

z	5.1	334.2
L	4.7	34.6
z	4.6	34.7
cb.	4.6	34.7
E	4.1	35.2
1+63		
E	4.7	334.6
cb.	5.0	34.3
z	5.0	34.3
L	4.8	34.5
z	5.0	34.3
cb.	5.7	33.6
W	5.8	33.5
2+00		
W	7.0	332.3
cb.	6.8	32.5
z	6.7	32.6
L	6.6	32.7
z	6.3	33.0
cb.	6.1	33.2
E	5.7	33.6
2+50		
E	7.2	32.1
cb.	7.7	31.6
z	7.8	31.5
L	8.2	31.1

33925

37

z	8.2	331.1
cb.	8.3	31.0
W	8.3	31.0
2+62		
W	8.3	331.0
cb.	8.2	31.1
+6	8.9	30.4
z	8.7	30.6
L	8.6	30.7
z	8.5	30.8
cb.	8.2	31.1
E	7.7	31.6
2+80		
E	8.4	330.9
cb.	8.8	30.5
z	8.9	30.4
L	9.2	30.1
z	9.6	29.7
cb.	9.6	29.7
W	9.6	29.7
3+00		
W	10.5	28.8
cb.	10.6	28.7
+8	10.5	28.8
z	10.2	29.1
L	9.4	29.9

z		9.4	329.9
cb		9.5	29.8
E		9.0	30.3
	3+20		
E		9.8	329.5
cb		10.2	30.1
z		10.4	29.9
z		10.5	29.8
z		10.8	28.5
cb		11.2	28.1
Y		11.3	28.0
	3+50		
Y-5'		12.5	326.8
Y		12.5	26.8
cb		12.3	27.0
z		12.0	27.3
z		11.6	27.7
z		11.3	28.0
cb		11.0	28.3
E		10.7	28.6
TP	0.30	11.58	327.67
	4+00		
E		1.2	326.8
cb		1.6	26.4
z		1.9	26.1
z		2.4	25.6

z		2.7	325.3
cb		3.2	24.8
Y		3.7	24.3
+5		4.2	23.8
4+21=2	Con. Y 1/4 W E	1.40	26.57
4+47=8	Upper face on Y	5.8	22.2
	4+50		
-5		7.5	320.5
Y		7.2	20.8
+6		6.6	21.4
cb		6.3	21.7
z		5.8	22.2
z		5.2	22.8
z		4.7	23.3
cb		4.2	23.8
E		3.4	24.6
	4+75		
E		5.3	322.7
cb		6.2	21.8
z		6.8	21.2
z		7.4	20.6
z		8.0	20.0
+3		8.9	19.1
cb		9.2	18.8
Y		9.2	18.8
+10		10.0	18.0

3' wide
on line
6" dia
3' 10" sf.

4+95

-10	12.6	315.4
11	11.5	16.5
+6	12.4	15.6
cb	11.8	16.2
$\frac{1}{2}$	10.7	17.3
2	9.7	18.3
$\frac{1}{2}$	8.7	19.3
cb	8.1	19.9
+7	7.7	20.3
E	6.0	22.0

5+00

E	6.7	321.3
+5	7.6	20.4
cb	8.7	19.3
$\frac{1}{2}$	9.5	18.5
2	10.5	17.5
$\frac{1}{2}$	11.2	16.8
cb	12.5	15.5
11	13.8	14.2
+15	15.6	12.4

5+15

-20	18.3	309.7
11	16.3	11.7
cb	15.2	12.8
$\frac{1}{2}$	14.3	13.7

2	13.1	314.9
$\frac{1}{2}$	12.2	15.8
cb	10.7	17.3
+7	9.3	18.7
E	8.0	20.0

5+30

-5	10.7	317.3
E	12.1	15.
TP	144	317.42
+5	3.9	13.5
cb	5.0	12.4
$\frac{1}{2}$	6.3	11.1
2	7.3	10.1
$\frac{1}{2}$	8.1	09.3
cb	8.7	08.7
11	9.4	08.0
+7	10.0	07.4
+20	12.8	04.6

5+45

-20	17.2	00.2
11	15.5	01.9
cb	14.4	03.0
$\frac{1}{2}$	13.4	04.0
2	12.2	05.2
$\frac{1}{2}$	10.9	06.5
cb	10.1	07.3

317.42

E		7.2	310.2
+5		5.3	12.1
+10		3.9	13.5
	5463		
-20		7.2	10.2
E		12.5	04.9
TP	0.69	305.88	12.23 305.19
cb		5.0	300.9
4		6.3	299.6
L		8.3	97.6
i		9.4	96.5
cb		10.2	95.7
N		10.2	95.7
+25		14.7	91.2

5 + 87.5 = N.H. Myrtle

Note: For X Section
Intersection Sec
Pages 28-29

-35		24.0	281.9
N		21.9	84.0
cb		20.6	85.3
4		19.7	86.2
L		17.9	88.0
i		14.9	91.0
cb		12.4	93.5
E		8.9	97.0
+20		0.6	305.3
TP	12.16	317.86	0.18 305.70
TP	11.55	328.24	1.17 316.69

328.24

TP	9.55	337.08	0.71	327.53
chk. w. B.M. N.H. Myrtle + Chamaunt			1.21	335.87

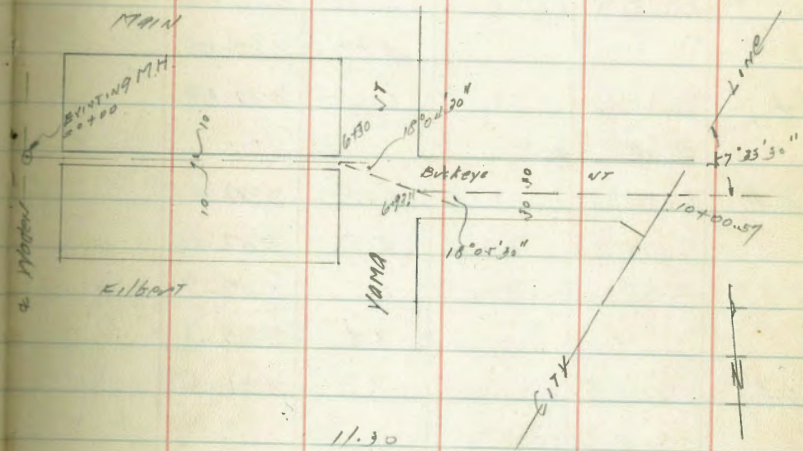
Page 18
 $335.87 - 335.85 = 0.02$
 0.02 = Error

40

1/30/94
Moore
Sewer Levels & alley between MAIN & Filbert from
Wagon to Yama thence east on 2 of Buckeye to Division

NWSP	S.N.P.	12.74	10.26	MAIN WAGON
00 = Ex. MH & Wagon & alley		12.55	0.19	Flankline
" " " " " " " "	RTM	5.14	7.59	RIM
0 + 20 = in cut of line Wagon		5.3	7.4	
0 + 30 = " " " " " "		4.9	7.8	
0 + 50		4.4	8.3	
1		4.2	8.5	
+ 50		5.5	7.2	
✓		5.8	6.9	
+ 30		6.7	6.0	
+ 57		6.5	6.2	
+ 85		5.5	7.2	
2 + 20		6.8	5.9	
+ 50		7.0	5.7	
+ 60		7.1	3.6	
+ 70		8.6	4.1	
4 + 00		9.7	3.0	
+ 40		11.3	1.4	
✓		11.4	1.3	
+ 55		14.2	1.5	
+ 82		10.5	2.2	
6 + 30 = in l. Yama = A		10.3	2.4	
T.P.	8.85	11.30	10.29	✓ 4.5
6 + 30 = EL	" = A	9.4	2.1	
7 + 50		9.6	1.7	
8		9.7	1.6	

Platted 1-21-29
S.P.N.



11.30			
9 + 50	9.8	1.5	
9	9.6	1.7	
+ 50	9.8	1.5	
10 + 00.57 = CITY LINE	9.5	1.8	
cut to NWSP MAIN & Div.	5.40	8.90	8.88
			0.04 error

Walker
Massey
Lee Ky
No. 1000
2-10-29

X. Section of Roadway MEADE Ave 52' wide
Bet. Louisiana and Utah Sts.
FOR YARDAGE ONLY

33919
Sec. Book 1293 for cb Et.

42

778	339.19	331.41	SE. B.P. Mo. & Texas
E. Louisiana = 0+00			
S. Gutter on Pav.	6.98	332.21	
" 1/4 "	6.43	332.76	
" 1/2 "	6.17	333.02	
" 3/4 "	6.18	333.01	
" Gut "	6.60	332.59	
0+50			
N. Gut	6.8	332.4	
1/4	6.7	332.5	
1/2	6.5	332.7	
3/4	7.1	332.1	
S. Gut	7.7	331.5	
1+00			
S "	8.0	331.2	
" 1/4 "	7.3	331.9	
1/2	7.0	332.2	
N 1/4	6.9	332.3	
" Gut	7.6	332.0	
1+50			
N. Gut	7.1	332.1	
" 1/4 "	7.3	331.9	
1/2	7.4	331.8	
S 1/4	7.8	331.4	
S. Gut.	8.4	330.8	

2700	S. Gut	8.8	330.4
	" 1/4 "	8.1	331.1
	1/2	7.6	331.6
	N 1/4	7.7	331.5
	" Gut "	7.9	331.3
2+50	N "	8.0	331.2
	" 1/4 "	7.9	331.3
	1/2	8.0	331.2
	3/4	8.5	330.7
	Gut	8.9	330.3
3+00 = Y.L. Texas St	S. Gut. on Pav.	7.17	330.02
	" 1/4 "	8.64	330.55
	1/2 "	8.32	330.87
	3/4 "	8.16	331.03
	N. Gut "	8.28	330.91
4+00 = Y.L. Texas St = 0+00	N " " "	7.46	331.73
	" 1/4 " "	7.36	331.83
	1/2 " "	7.59	331.66
	S 1/4 " "	7.78	331.41
	" Gut " "	8.28	330.91
0+50	S. Gut.	7.4	331.8

337.19

S 1/2	6.6	332.6
L	6.3	332.9
N 1/2	6.3	332.9
" Gut.	6.4	332.8

1+00

N Gut.	5.2	334.0
" 1/2	5.1	334.1
L	5.1	334.1
S 1/2	5.5	333.7
" Gut.	6.3	332.9

1+50

S Gut.	5.2	334.0
" 1/2	4.3	334.9
L	5.6	335.6
N 1/2	3.8	335.4
" Gut.	4.3	334.9

E+00

N "	3.0	336.2
" 1/2	2.3	336.9
L	2.8	337.0
S 1/2	2.7	336.5
" Gut.	3.6	335.6

E+50

S "	1.4	337.8
" 1/2	0.8	338.4
L	0.3	338.9

339.19

N 1/2	0.4	338.8
N Gut.	0.4	338.8
T.P.	12.50 351.18	0.51 338.98

3+00 = N.H. Arizona st

N Gut. on Av.	10.00	341.18
" 1/2 " "	9.89	341.29
L " "	10.00	341.18
S 1/2 " "	10.37	340.91
" Gut. " "	10.86	340.32

E.L. Arizona = 0+00

S " " "	9.76	341.42
" 1/2 " "	8.78	342.40
L " "	8.25	342.93
N 1/2 " "	8.13	343.05
N Gut " "	8.36	342.82

0+50

N Gut.	2.6	348.6
" 1/2	2.8	348.5
L	2.9	348.3
1/4	3.3	347.8
S Gut.	3.9	347.3
T.P.	12.72 363.67	0.23 350.95

1+00

S Gut.	10.2	353.5
S 1/2	9.9	353.8
L	9.4	354.3

43

N 1/4		9.4	354.3
N Gut.		9.6	354.1
	1A50		
N "		3.9	359.8
" 1/4		3.7	360.0
1/2		3.7	360.0
S 1/4		4.2	359.5
" Gut.		4.6	359.1
	1A75		
S "		1.8	361.9
" 1/2		1.3	362.4
1/2		0.7	363.0
N 1/4		0.7	363.0
" Gut.		0.9	362.8
IP	13.07 376.65	0.09	362.58
	2+00		
N Gut		11.1	365.5
" 1/4		11.2	365.4
1/2		11.1	365.5
1/2		11.8	364.8
S Gut.		12.1	364.5
	2+25		
S "		10.2	366.4
" 1/4		9.9	366.7
1/2		9.3	367.3
N 1/4		7.2	367.4

N Gut.		9.3	367.3
	2+50		
N "		7.9	368.7
" 1/4		8.0	368.6
1/2		8.0	368.6
1/4		8.5	368.1
S Gut.		8.8	367.8
	3+00 = Y.L. Hamilton St.		
S " on Pav.		7.84	368.81
" 1/4 "		7.20	369.45
1/2 "		6.93	369.72
N 1/4 "		6.90	369.75
N Gut. "		7.07	369.58
	E.L. Hamilton St. = 0+00		
N Gut. on Pav.		5.36	371.29
" 1/4 "		5.16	371.49
1/2 "		5.27	371.38
S 1/2 "		5.59	371.06
" Gut. "		6.09	370.56
	0+50		
S Gut.		4.5	372.1
" 1/4		4.0	372.6
1/2		3.8	372.8
1/4		3.9	372.7
N Gut.		4.2	372.4
	0+75		

N. Gut.	3.6	373.0
" $\frac{1}{2}$	3.3	373.3
$\frac{1}{2}$	3.2	373.4
$\frac{1}{4}$	3.5	373.1
S Gut.	3.6	373.0
1+00		
S "	3.1	373.5
" $\frac{1}{2}$	2.9	373.7
$\frac{1}{2}$	2.6	374.0
N $\frac{1}{4}$	2.7	373.9
" Gut.	3.6	373.4

1+50

N Gut.	2.6	374.0
" $\frac{1}{2}$	2.2	374.4
$\frac{1}{2}$	1.7	374.9
S $\frac{1}{4}$	2.0	374.6
" Gut.	2.4	374.2

E+00

S Gut.	1.8	374.8
" $\frac{1}{2}$	1.5	375.1
$\frac{1}{2}$	1.2	375.4
N $\frac{1}{4}$	1.7	374.9
" Gut.	2.0	374.6

E+50

N "	1.2	375.4
" $\frac{1}{2}$	0.8	375.8

$\frac{1}{2}$	0.8	375.8
$\frac{1}{4}$	1.1	375.5
S Gut.	1.2	375.2
E+00 = 1/4 Oregon St.		
S Gut. on Pav.	0.67	375.98
" $\frac{1}{2}$ " "	0.81	376.34
$\frac{1}{2}$ " "	0.23	376.42
N $\frac{1}{4}$ " "	0.35	376.30
N Gut. " "	0.74	375.91
T.P.	4.00	380.47
E.L. OREGON = 0+00		
N Gut. on Pav.	4.00	376.47
" $\frac{1}{2}$ " "	3.72	376.75
$\frac{1}{2}$ " "	3.59	376.88
$\frac{1}{4}$ " "	3.70	376.77
S Gut. " "	4.00	376.47

0+50

S Gut.	4.3	376.2
" $\frac{1}{2}$	4.1	376.4
$\frac{1}{2}$	4.0	376.5
N $\frac{1}{4}$	4.1	376.4
" Gut.	4.3	376.2

1+00

N "	4.4	376.1
N $\frac{1}{2}$	4.3	376.2
$\frac{1}{2}$	4.1	376.4

38047

z	41	376.4
S Gut.	46	375.9
1+50		
S Gut.	16	375.9
" z	23	376.2
L	41	376.4
N z	42	376.3
N Gut.	46	375.9
2+00		
N "	51	375.4
" z	44	376.1
L	43	376.2
S z	45	376.0
" Gut.	48	375.7
6+50		
S "	50	375.5
" z	46	375.9
L	44	376.1
z	47	375.8
N Gut.	51	375.4
3+00 = W.L. IDH40 St.		
N Gut. on Pav.	525	375.22
" z " "	493	375.54
L " "	478	375.69
S z " "	489	375.58
" Gut. " "	520	375.27

38047

46

E.L. IDH40 St. = 0+00		
S Gut. on Pav.	582	374.65
S z " "	549	374.98
L " "	535	375.12
N z " "	548	374.99
" Gut. " "	587	374.60
0+50		
N Gut.	74	373.1
z	68	373.7
L	66	373.9
S z	67	373.8
S Gut.	69	373.6
1+00		
S Gut.	81	372.4
z	77	372.8
L	75	373.0
z	77	372.8
N Gut.	85	372.0
1+50		
N "	95	371.0
" z	91	371.4
L	84	372.1
z	88	371.7
S Gut.	94	371.1
6+00		
S "	102	370.3

S 1/2	99	370.6
1/2	99	370.6
N 1/2	102	370.3
" Gut.	111	369.4
E+50		
N Gut	121	368.4
" 1/2	113	369.2
1/2	111	369.4
S 1/2	114	369.1
S Gut.	115	369.0
3+00 = W.L. Utah St		
S Gut. on Pring	1255	367.92
" 1/2 " "	1233	368.14
1/2 " "	1210	368.37
N 1/2 " "	1219	368.28
N Gut. " "	1265	367.82
chk. on top base Form + Meade	503	375.44

X. Section Alleys West Prop. lines
in MEADE AVE. West Louisiana St and
UTAH ST.

9.96 341.37

10' West of Sta 1+50 P. 42 = W.L. Alley. ^{at Louisiana} _{St. Texas St}

S	10.0	331.4
scb.	10.4	331.0
Ncb.	9.5	331.9

N.L.	9.5	331.9
1+60 = E.L. Alley	West Louisiana + Texas	
N.L.	9.3	332.1
Ncb.	9.7	331.7
scb.	10.6	330.8
S.L.	10.2	331.2
West. Line Alley <u>West</u> Texas + Arizona		
S.L.	7.1	334.3
scb.	7.5	333.9
Ncb.	6.6	334.8
N.L.	6.0	335.4
E.A. Alley <u>West</u> Texas + Arizona		
N.L.	5.5	335.9
Ncb.	6.1	335.3
scb.	6.8	334.6
S.L.	6.5	334.9
TP	1570	353.71
TP	1252	366.00
West Line Alley <u>West</u> Arizona + Hamilton St.		
S.L.	6.9	359.1
+3	7.2	358.8
scb.	7.8	358.2
Ncb.	6.9	359.1
N.L.	6.4	359.6
E.L. Above Alley		
N.L.	4.3	361.7

Ncb. 4.8 361.2

Scb. 5.7 360.3

S.L. 5.4 360.6

T.P. 12.12 378.10 0.02 365.98

West Line Alley Bet Hamilton & Oregon St.

S.L. 3.6 374.5

Scb. 4.0 374.1

Ncb. 4.2 373.9

N.L. 3.8 374.3

E.L. House Alley

N.L. 3.5 374.6

Ncb. 3.9 374.2

Scb. 3.6 374.5

S.L. 3.3 374.8

T.P. 3.86 381.02 0.94 377.16

W.L. Alley Bet Oregon & IDAHO St. Alley stops on Sch Line

S.L. 4.8 376.2

Scb. 5.0 376.0

E.L. Alley Bet Oregon & IDAHO

S.L. 5.0 376.0

Scb. 5.1 375.9

W.L. Alley Bet IDAHO & Utah St

S.L. 9.1 371.9

Scb. 9.6 371.4

Ncb. 9.8 371.2

N.L. 9.2 371.8

E.L. Alley Bet IDAHO & Utah

N.L. 9.5 371.5

Ncb. 9.9 371.1

Scb. 10.0 371.0

S.L. 9.4 371.6

Cht. on top ch. S.E. Trade & IDAHO 5.65 375.37

375.44 = p-47.

0.07 = Error.

Moore
3/2/29
Y.S.P. of 11/24 20' wide
BIR 54 FAIRMONT AVE

NWBP	5.47	358.03		352.56
T.P.	5.21	357.39	5.85	352.18
T.P.	4.85	358.44	3.84	353.57

WL 40 1/2' N of cb line of Polk Ave

Top cb 4.43 353.99

on paving 358.42 4.85 353.57

EL Highland + N of cb line of Polk

Top cb 5.14 353.28

on paving 5.60 352.82

0+00 - 6.5 = N of cb line of Polk

W Top cb 4.84 353.58

E " " 4.79 353.63

0+00 - 1.5 = inside edge sidewalk

E Top sidewalk 4.67 353.75

W 4.76 353.64

0+00 = NL

W 4.7 353.7

C 4.9 353.5

E 4.6 353.8

0+01 4 W METERS ON EL

0+27 1 " " " WL

0+30 1 " " " "

0+43

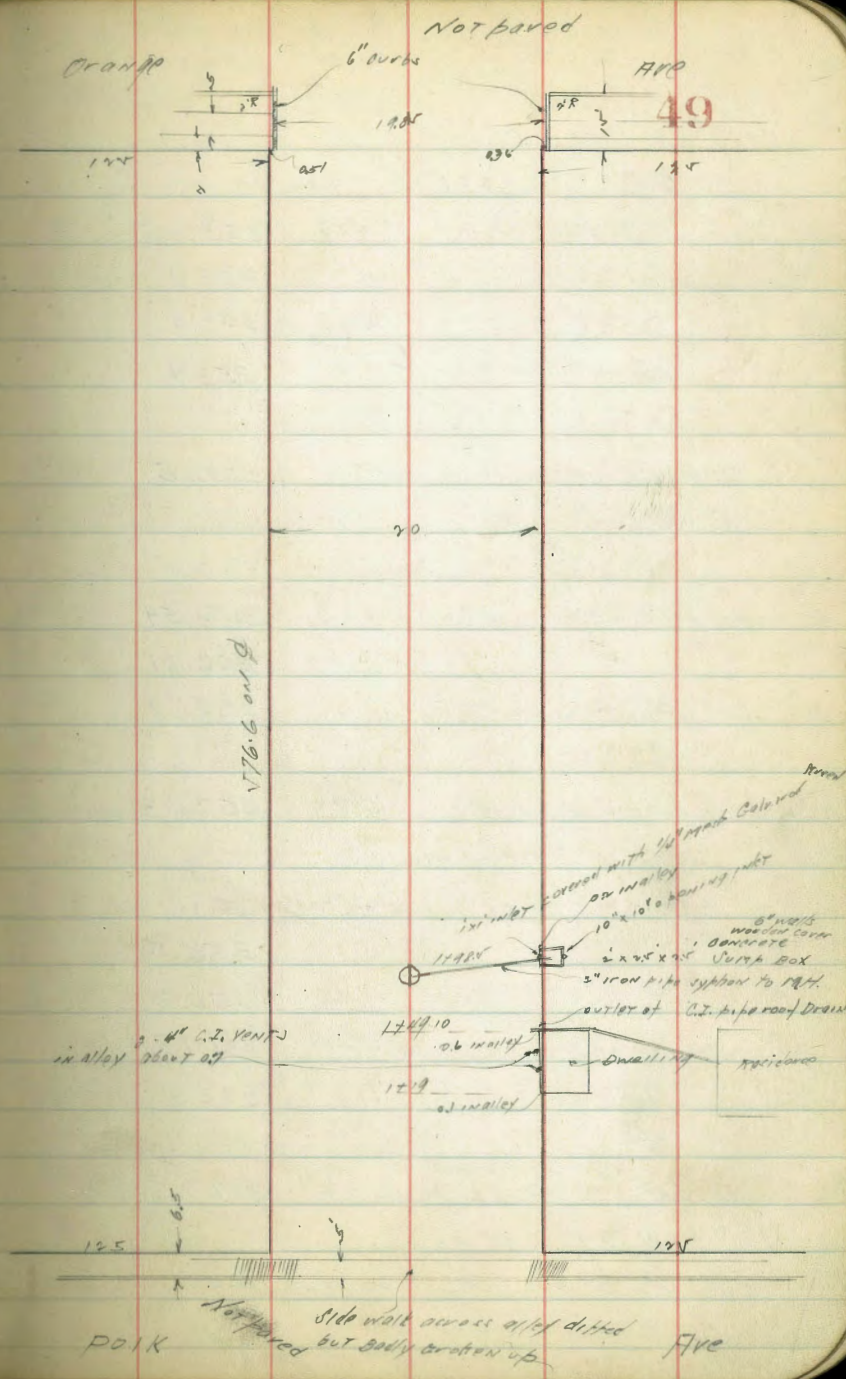
E Sid Car Apron 7' wide on line 4.81 353.61

C 5.4 353.0

W 5.0 353.4

+2.8 Sid Car dirt floor 4.9 353.5

Plotted 3/5/29 - G.M.J.



T.P.	473	358.50 357.61	554	357.88
0455 = W Metre EL				
on alley	0463	357.61		
W 8' wide Jan. Gar. Approx. Pers.	456	353.05		
C	457	352.9		
E	458	353.2		
+9 Jan Gar. det. floor	459	353.4		
0477				
W E comparison 73' wide online	456	353.05		
0487 = W Metre on WL				
1406				
E Jan Gar. corr. floor online	507	352.54		
C	500	352.61		
W 10th fence 1" alley	500	352.61		
1416				
E 8' wide corr. walk off alley	518	352.43 = W Metre EL		
1427 W Metre on WL				
1491 = N Cor. of Dwelling on east 0.6' alley				
W	511	352.5		
C	514	352.2		
+8 = outlet ^{4" diam. CP into} Flowline Roof drain from	580	351.79		
E	513	352.3		
1457				
E Jan Gar. Cor. floor ^{on east} EL-10	526	352.35		
1474 W Metre on EL				
1475 " " " WL Nord of 10th fence on fire				
1477 " " " EL				

				357.61
1492.5				
-8 Jan Gar. corr. floor	563	351.98		
E	63	351.3		
+9	57	351.9		
C	58	351.8		
W	54	352.2		
+07 Jan Gar. corr. floor	510	352.57		
1495				
1495 Jan Gar. M.H. R.M.	580	351.79		
" " " Flowline	10.75	346.86		
" ^{OUTLET IN P.H.} Flowline 2" pipe drain	8.2	349.4		from Sump
1498.5				
Top of Sump	500	351.79		
Flowline of 2" inlet to M.H.	739	350.22		
Bottom of Sump	70	350.0		
2433 W Metre on WL				
2443 " " on EL				
2458				
W	57	351.9		
C	60	351.6		
E	59	351.7		
2476 W Metre on WL				
2487 " " " EL				
3414				
E	58	351.8		
C	58	351.8		

50

35761

3+14				
W	E of double Car dirt floor	5.4	352.2	
3+40	W Metre on EL			
3+42	" " " " wt serves to house			
T.P.	6.00 358.18	5.43	352.18	
3+50				
W		5.9	352.3	
C		6.1	352.1	
E		6.0	352.2	
4+00				
E		5.8	352.4	
C		5.8	352.4	
W		5.7	352.5	
4+05	W Metre on WL			
4+11				
E	Double Car dirt floor 13' back	5.2	353.0	
4+51	W Metre on EL			
4+59	" " " "			
4+35				
W		5.4	353.0	
C		5.7	352.5	
E		5.7	352.5	
4+61	W Metre on EL			
4+66	" " " WL			
4+70				
E	Sim Car wood floor of alley	5.0	353.1	

35818

51

4+75				
E		5.2	353.0	
C		5.4	352.8	
W		5.1	353.1	
4+95.2				
W		4.9	353.3	
C		5.1	353.1	
E	Sedge of wide Cor. Apron	4.97	353.21	0.3 back
4+00	W Metre on WL			
4+01	" " " EL			
4+08				
E	E Cor. Apron	4.81	353.37	0.4 back
4+20.9				
E	Slope Cor. Apron	4.90	353.28	0.4 back
C		4.9	353.3	
W		4.9	353.3	
4+6	Sim Car Cor. floor	4.51	353.67	
4+27	W Metre on WL			
4+31.5				
E	Sim Car dirt floor	4.9	353.3	2' back
4+41	W Metre on EL			
4+48	" " " "			
4+56				
W		4.9	353.3	
C	Sewer MH R.M.	4.76	353.42	
"	" " Flouline	4.14	349.04	
E		4.9	353.3	

V+76.6 = St Orange

E Top cb	469	353.49	
" on ground	5.0	353.23	
C	5.2	353.0	
W " "	4.8	353.4	
W Top cb	457	353.61	
T.D. 5.5	358.66	5.07	353.15

EL of Highland + Subline of Orange

Top cb	451	353.67	
on paving	5.13	353.05	
Wk alley + Subline of ^{Orange}	5.41	352.77	
EL " " " "	5.50	352.68	

Wk of 4th + Subline Orange

Top cb	6.30	351.88	
on paving	6.90	351.28	
check NW/SE Orange + Highland	451	354.15	354.16

error

20' wide

X Sec. Alley BIK 18 Fairmont
Univ. to Polk Bet. 46th + Menlo.

5-19-29
Mills.

352.48

B.M.	9.39	352.48	343.09
00 = N. Line Univ. Ave			
N. cmt. cl.		4.98	347.50
W. parmt.		5.37	347.11
φ parmt		5.63	346.85
E "		5.67	346.81
E. cmt. cl.		5.62	346.86
	5' N		
E		4.8	347.7
C		4.4	348.1
+5		4.1	348.4
W		2.9	349.6
	15' N		
W		3.3	349.2
C		3.8	348.7
+8		4.3	349.2
E		4.7	347.6
	60' N		
E		5.2	347.3
+3		4.2	348.3
C		4.0	348.5
W		4.0	348.5
	100' N		
W		4.7	347.8
C		4.7	347.8
+8		4.7	347.8
E		6.0	346.5

Plotted 3/30/29

n.w. Univ
& Menlo.

E	158' N Garage on W. cmt. floor 15' Back	6.6	345.9
C		5.7	346.8
W		5.7	346.8
+15		4.6	347.9 floor
	188' N garage on W. cmt. floor 15' Back		
-15		5.2	347.3 floor
W		5.9	346.6
C		6.1	346.4
C		6.7	345.8
	215' N garage on W. cmt. floor 14.2 Back		
E		6.8	346.7
C		6.2	346.3
W		6.2	346.3
+14.2		5.5	347.0 floor
	223' N. Door into Planing Mill. 1/2 Back dirt floor		
1/2 E. of E. line		6.7	345.8 floor
	236' N. garage on W. cmt. floor 14' Back		
N-14		5.6	346.9 floor
	250' N		
W		6.1	346.4
C		6.2	346.3
E		6.4	346.1
	265' N		
E		6.4	346.1
C		6.6	345.9
W		6.2	346.3

352.48

295' N

W	6.0	346.5 ^{ok}
C	6.5	346.0 ^{ok}
E	6.4	346.1 ^{ok}

300' N

E	6.7	345.8	346.2 New Dirt
+3		45.8	395.8
C	6.7	345.8 ^{ok}	
W	-7.3	345.2	345.0

325' N

W	6.7	345.8 ^{ok}
C	6.8	345.7 ^{ok}
E	6.5	346.0 ^{ok}

3.50' N

E	6.9	345.6 ^{ok}
C	7.3	345.2 ^{ok}
W	4.9	345.6 ^{ok}

400' N

W	6.8	345.7 ^{ok}	345.1
+5			
C	7.3	345.2 ^{ok}	
E	6.8	345.7 ^{ok}	

T.P.	7.54	353.36	6.66	345.82
------	------	--------	------	--------

457' N = double garage on W dirt floor 3.7 Back

E	7.3	346.1	
C	7.2	346.2	
W	7.3	346.1	
+37	7.3	346.1	floor

409' N S side House 8.5 E of Alley

347.50 Floor Elev

353.36

500' N

W	6.5	346.9
C	6.8	346.6
E	6.6	346.8

520' N. garage on E, dirt floor 7' Back

-7	5.9	347.5	floor
E	6.1	347.3	
C	6.1	347.3	
W	6.2	347.2	

from 525' N. to 545' N. Back on W. side in Alley

537' N. garage on E, dirt floor 4' Back

W	5.9	347.5	
C	5.6	347.8	
E	5.3	348.1	
+4	5.1	348.3	floor

540' N

on M. H.

5.38, 347.98

555' N. garage on W, dirt floor 3.8 Back

E	5.1	348.3	
C	5.1	348.3	
W	5.4	348.0	
+3.8	5.5	347.9	floor

582' N

W	4.6	348.8
C	4.4	349.0
E	4.2	349.2

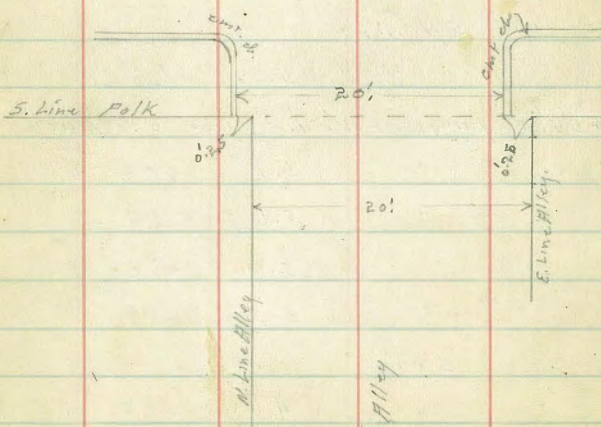
54

Alley Blk 18 Fairmont

353.36

594'.N

E	4.3	349.1
+3	5.3	348.1
e	5.6	347.8
W	5.8	348.1
599'.N. = S. Line Polk Ave		
W. dirt	6.0	347.4
W. emt. cl	5.97	347.39
W. pavmt	6.40	346.96
4" "	6.68	346.68
4" dirt	6.5	346.9
E. "	5.8	346.6
E. emt. cl	6.08	347.28
E. pavmt	6.53	346.83
chk. on R.M. Top Hydt	1.63	351.73 = 351.73



H. Hooley
W. McCarty

140 B.M.

0+03

0+06

0+09

0+12

0+15

0+18

W+10

W+20

Hand Levels Around
Return & sidewalk, NW Cor Menlo's Chain
H.I.

2.27 345.36

2.21

2.2

2.2

2.25

2.25

1.85

1.65

1.30

Alley 131K18. Fairmont.

55

Fairmont.

NW Cor
Menlo's Univ.

Top curb

" "

" "

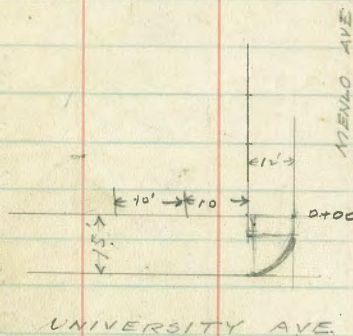
" "

" "

Property
Line Intersection

" "

" "



4/13
 Moore
 Fl...
 Col...
 Pearce
 on original stations see BM 1240 pages 58
 26.127 Nide
 of Ocean St
 E.L. Coast Blvd No.

5.24 41.11 35.87

Section 3462

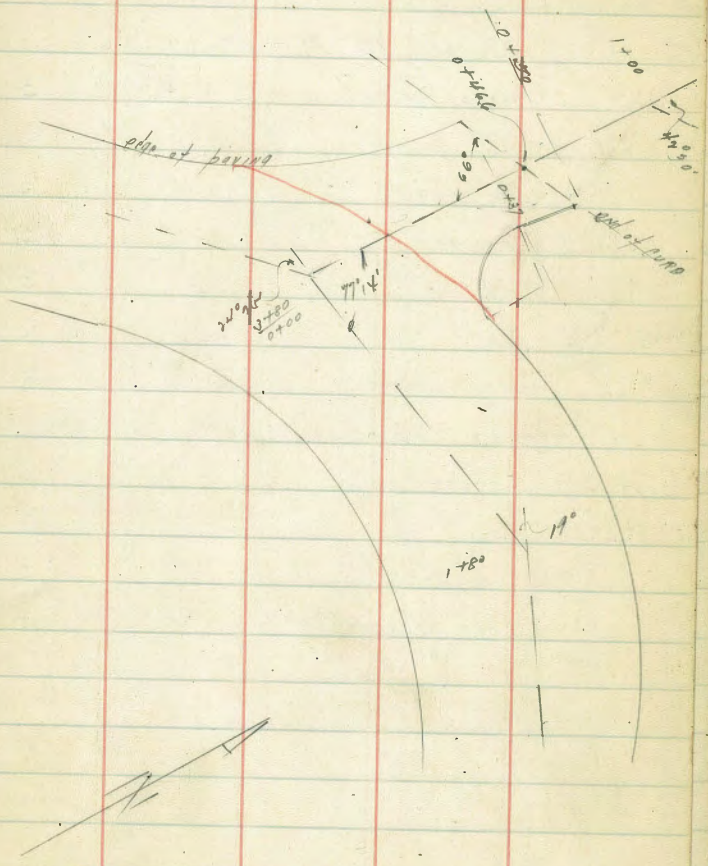
19.75 LT Top of	4.66	36.45
" " paving curb	5.63	35.48
10' LT "	5.3	35.8
R.L. "	5.23	35.88
16.5 RT "	6.03	35.08
4N RT "	6.20	35.91
30' RT "	6.35	35.76
40' RT "	6.60	35.51
50' RT	6.8	34.3

Sec 3480-A

56' RT	7.1	34.0
36' RT paving	6.97	34.72
16' RT "	5.87	35.24
6' RT "	5.56	35.57
4' LT "	5.43	35.68
14' LT "	5.47	35.64
24.05 LT grating	5.71	35.40
" " Top of	4.66	36.45

Sec 4730

25.65 LT Top curb	7.78	33.33
" " gutter on paving	5.12	35.69
15' LT	5.30	35.81
5' LT	5.33	35.78



5 RT.	5.51	35.57
13 RT = edge of New Paving	5.85	35.26
15 RT	5.8	35.8

See 0+37 page of BK 1240

13.5 RT = Top of New curb	5.90	35.21
" gutter paving	6.48	34.63
12.5 RT old cob gene	6.48	34.63
4.8 RT paving	6.37	34.74
7' LT "	6.36	34.75
17' LT edge	6.63	34.48
19' LT natural ground	6.2	34.9

New Sec 46.6 = diagonal line = edge of paving

17.5 LT paving	6.70	34.41
R.L. "	6.60	34.51
15.4 RT " gutter	7.15	33.96
" " Top new curb and	6.61	34.50

Ellison Place X Sec
Mt. View Drive North.

5-7-29
mills

B.M.	6.22	397.29		391.07	S.E. 32 nd + Copley
T.P.	3.42	394.21	6.50	390.77	N.W. Ellison
T.P. B.M.	4.43	394.01	4.43	389.58	+ Mt. View Drive 87.59

N. Line Mt. Drive on Curve.

n. cont. ch.		4.46		389.55
gutter		4.8		389.2
1/4		4.6		389.4
c		4.6		389.4
1/4		5.0		389.0
gutter		5.2		388.8
e. cont. ch.		4.94		389.03

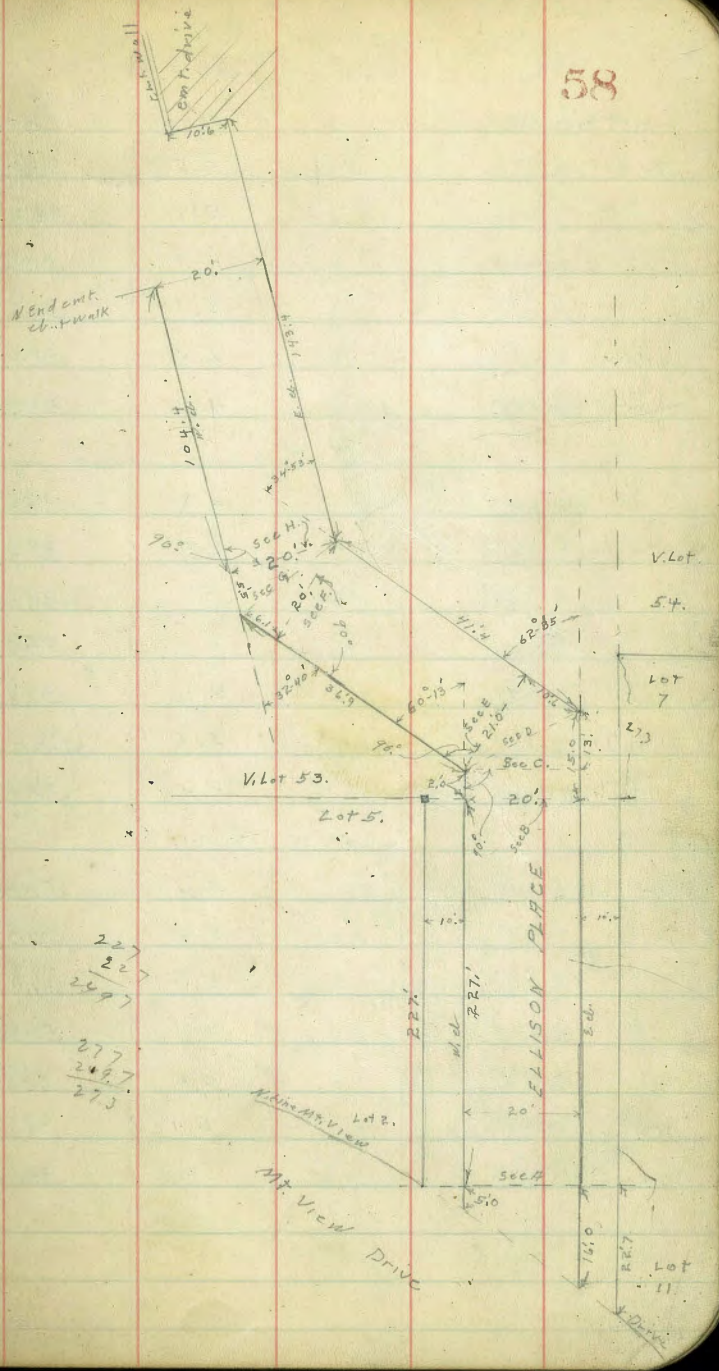
Sec. A. at 90° from N.W. Cor.

e. cont. ch.		5.05		388.96
gutter		5.2		388.8
1/4		5.0		389.0
c		4.2		389.3
1/4		4.6		389.4
gutter		4.8		389.2
n. cont. ch.		4.46		389.55

Plotted 5-11-29 CBH

R.S.N.

n. cont. ch.		4.58		389.43
gutter		5.1		388.9
1/4		4.8		389.2
c		4.9		389.1
1/4		4.9		389.1
gutter		5.2		388.8
e. cont. ch.		5.14		388.83



227
227
2297

277
2497
273

394.01
50' N. of Sec. A.

E. ent. cl	5.32	388.69
gutter	5.5	388.5
"4	5.2	388.8
e	4.9	389.1
"4	5.1	388.9
gutter	5.4	388.6
W. ent. cl	4.78	389.23
75' N.		
W. ent. cl	4.91	389.10
gutter	5.4	388.6
"4	6.1	388.9
e	5.2	388.8
"4	6.3	388.7
gutter	5.6	388.4
E. ent. cl in drive figured	5.41	388.60
100' N.		
E. ent. cl	5.47	388.54
gutter	5.8	388.2
"4	5.4	388.6
e	5.4	388.6
"4	5.5	388.5
gutter	5.4	388.6
W. ent. cl	5.04	388.97

Ellison Place

394.01
125' N

59

W. ent. cl	5.19	388.82
gutter	5.6	388.4
"4	5.4	388.6
e	5.3	388.8
"4	5.6	388.4
gutter	5.7	388.3
E. ent. cl	5.60	388.41
150' N.		
E. ent. cl	5.68	388.33
gutter	5.9	388.1
"4	5.7	388.3
e	5.4	388.6
"4	5.5	388.5
gutter	5.8	388.2
W. ent. cl	5.26	388.75
175' N.		
W. ent. cl	5.48	388.53
gutter	5.9	388.1
"4	5.2	388.3
e	5.6	388.4
"4	5.8	388.2
gutter	6.1	387.9
E. ent. cl	5.43	388.18

394.01
200' N

S. ent. ch	5.90	388.11
gutter	6.2	387.8
"4	5.9	388.1
e	5.9	388.1
"4	6.0	388.0
gutter	6.2	387.8
W. ent. ch.	5.60	388.41
R22' N. = S. End ch. inlet on W.		
W. ent. ch.	5.66	388.35
gutter on Lip ch. inlet	6.66	387.35
R27' N. of Sec A = Sec B. = 90° 00' from N.E. Cor. Lot. 5		
W. ent. ch	5.66	388.35
gutter on grading	6.69	387.32
"4	6.2	387.8
e	5.9	388.1
"4	5.5	388.5
gutter on Lip. S. End. ch. inlet	6.94	387.07
E. ent. ch.	5.94	388.07
E'N. of Sec B. = Sec C. = Δ in W' ch.		
E. ent. ch	5.93	388.08
gutter. ch. inlet Lip.	6.94	387.07
"4	5.6	388.4
e	5.8	388.2
"4	6.1	387.9
gutter on N. end ch. inlet on W	6.66	387.35
W. ent. ch at A.	5.67	388.34

394.01

Elison Place

Δ on W. ch 13' N. of sec C on E. ch = Δ on E. ch. = sec D R3.8 on Diagonal

N. ent. ch at A	5.67	388.34
gutter ch. inlet lip.	6.66	387.35
"4	6.2	387.8
e	5.7	388.3
"4	6.1	387.9
gutter Lip. at N. End. ch. inlet on E.	6.95	387.06
E. ent. ch. at A	5.93	388.08
(2) 10' Rdw. Δ on W. ch + 10' 6" N.W. on N.E. ch line = Sec. E. at 90° from S.W. ch.		
N.E. ent. ch	5.83	388.18
gutter	6.6	
"4	6.3	
e	6.0	388.0
"4	6.3	
gutter Lip. ch. inlet	6.66	
S.W. ent. ch. at A	5.67	388.34
30.8' NW. of Sec. E. = Sec. F. = Δ on N.E. ch. at 90° from S.W. ch. (20' Rdw.)		
S.W. ent. ch. in drive Plev Figured	5.80	388.21
gutter	6.3	
"4	6.2	
e	6.1	387.9
"4	6.2	
gutter	6.2	
N.E. ent. ch. at A	5.56	388.45

394.01

Δ on N.E. cb. = 2.1' W.W. of Sec F, on S.W. cb. = Sec. G. A on W. cb. (20.7 Rdy)

E. cont. cb at Δ	5.56	388.45
gutter	6.1	
"	6.1	
c	6.2	387.8
"	6.3	
gutter driveway No d	6.45	
W. cont. cb elev figured	5.83	388.18

5.5' N. on W. cb. + Δ on S. cb. = Sec H. at 90° to curbs (20' Rdy)

W. cont. cb.	5.92	388.09
gutter	6.4	
"	6.4	
c	6.1	387.9
"	6.1	
gutter	6.1	
E. cont. cb at Δ	5.56	388.45

25' N. of Sec H.

E. cont. cb	5.98	388.03
gutter	6.4	
"	6.3	
c	6.2	387.8
"	6.5	
gutter	6.8	
W. cont. cb.	6.34	387.67

394.01

50' N

W. cont. cb	6.84	387.17
gutter	7.4	
"	6.9	
c	6.6	387.4
"	6.8	
gutter	7.0	
E. cont. cb	6.57	387.44

75' N.

E. cont. cb in drive elev. figured.	6.87	387.14
gutter in driveway	7.4	
"	7.0	
c	6.9	387.1
"	7.2	
gutter	7.8	
W. cont. cb.	7.29	386.72

104.4' N. of Sec H. = N. cont. cont. walk cb. on W. (20' Rdy)

10' W. of N. cb	10.1	
W. of N. cb. = N. edge cont. walk	7.7	
W. cont. cb	7.78	386.23
gutter	8.1	
"	7.4	
c	7.5	386.5
"	7.6	
gutter	7.4	
E. cont. cb.	7.79	386.82

Ellison Place

61

394.01

110' N. of Sec. H.

S. ent. cl.	7.24	386.77
gutter	7.6	
"	7.7	
c	7.6	386.4
"	7.7	
W. cb. line	7.9	386.1
+ 7	8.6	
+ 10	10.4	
+ 15	11.5	

130' N. of Sec. H. (20' Rdw)

12' W. of W. cb. line	14.6	
3 " " " "	9.1	
W. cb.	8.9	385.1
"	8.2	
c	7.9	386.1
"	7.8	
gutter	7.7	
S. ent. cl.	7.35	386.66

143' 4" N. of Sec. H. = S. end. ent. drive at N. End. St.

S. ent. cl.	7.22	386.79
gutter on ent. drive	7.75	386.26
" " " "	7.75	
W. end. ent. drive	7.73	386.28
Top. ent. wall extending North.	5.55	388.46
+ 1 ground.	8.0	
"	8.6	
W. cb. line	10.4	383.6

394.01

Elison Place

10. W. of W. cb. line	17.2	62
150' N. of Sec. H.		
W. cb. line	13.5	380.5
W. "	10.7	
+ 4' = 1' W. of 4	8.5	
chk on B.M.	4.43	389.58

NW. Ellison

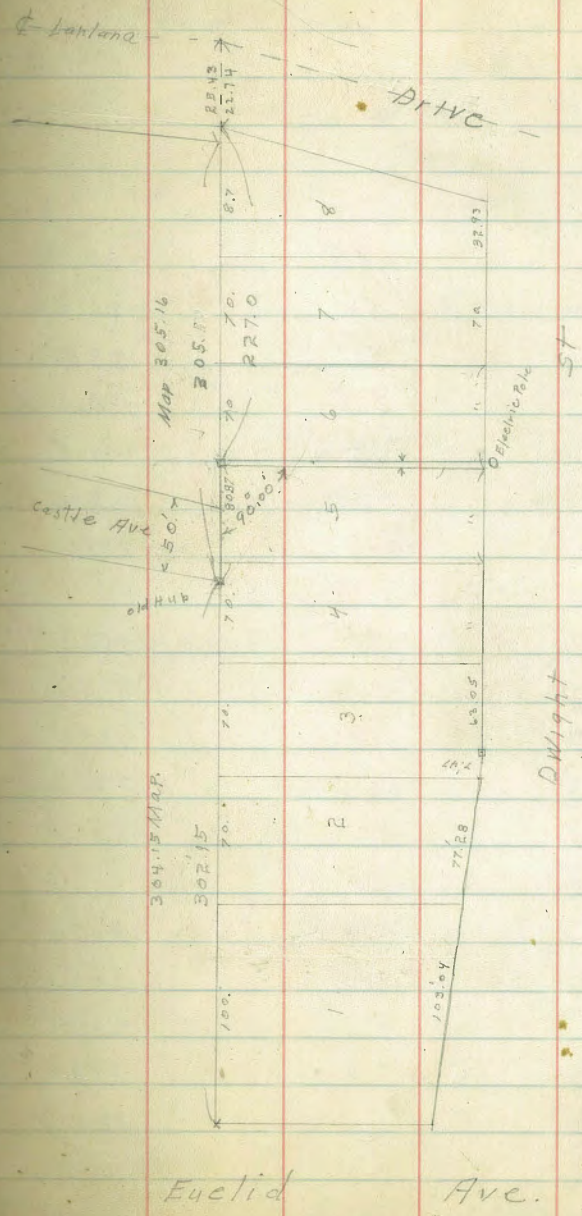
+ Mt. View Drive

8-9-29 Survey of W. line of Lot 5 Fairhaven Acres.

Müller
Levels for Drain on a line 2' N. of N. Boundary of Fairhaven Acres
From W. line Castle Ave. E. to a line 2' E. of E. Line Lot 5, Fairhaven Acres
Thence S. to Dwight St.

B.M. B.P.	7.79	
T.P.	7.60	4.05
		2' N. of N. line of
op W. line Castle Fairhaven Acres		5.3
+41		4.6
or 42 $\angle 90^{\circ}00'$ RT.		4.3
1+00		5.1
1+25		5.6
1+50		6.3
1+75		6.6
1+84 ⁸⁷ = N. Line Dwight		7.4
1+89 ⁸⁷		8.2
1+94 ⁸⁷		8.7
T.P.	3.33	8.25
Ch. Kon B.M.		3.42

at 1+87 Electric Pole R.E. of E. Line Lot 5. Pole to be Moved or
Culvert placed 4' E. of E. line Lot 5.



J. C. Bliss X-section Ash St. Edgemont to
 Ryan Dyer + 32nd. - 60' wide 15' above 9' x 1/2
 Chas. Palmer 0+00 = P.C. of East Returns on Edgemont.
 11-12-29 20' off East of line Edgemont

B.M. N.W. B.P. 31st & Ash		235.07	S
+6.67	241.74		cb
	+		14
	0+00		ϕ
N	5.9	235.9	14
+4 = 1p existing return	5.8	235.93	cb
cb	5.9	235.8	N
ϕ	5.5	236.2	T.P.
cb	5.2	236.5	
+11 = 1p existing return	4.74	237.00	
S	4.7	237.0	
	0+25		N
S	5.4	236.3	cb - edge fill
cb	6.0	235.7	14
ϕ	6.2	235.5	ϕ
cb	6.8	234.9	14
N	6.6	235.1	cb
	0+50		S
N	9.0	233.7	
cb	9.0	232.7	S
ϕ	8.0	233.7	cb
cb	7.8	233.9	14
S	7.1	234.6	ϕ

Plotted T.I.
11/29/29

241.74

64

	0+75		
	9.5		232.2
	9.8		231.9
	9.8		231.9
	10.8		230.9
	11.2		230.5
	11.4		230.3
	12.5		229.5
		13.12	228.62
1.54	230.16		
	π		
	1+00		
	10.4	219.8	
	2.9	227.3	
	2.9	227.3	
	3.4	226.8	
	2.7	227.5	
	2.3	227.9	
	0.8	229.4	
	1+25		
	8.3	221.9	
	8.0	222.2	
	7.9	222.3	
	7.6	222.6	
	8.3	221.9	
	12.5	217.7	

14 = edge fill

230.16

N		17.0	213.2
T.P.			13.09 217.07
	+0.97	218.04	
		+	
		1+52	
N		15.7	202.3
cb		12.2	205.8
1/4		9.1	208.9
ϕ		5.3	212.7
1/4		2.1	215.9
+3 = edge Fill		0.7	217.3
cb		0.5	217.5
S		1.8	216.2
		1+67 = S.L. Edge of Fill	
S		4.3	213.7
cb		7.3	210.7
1/4		10.0	208.0
ϕ		13.0	205.0
T.P.			12.65 205.39

+0.32

205.71

1/4		38	201.9
cb		59	199.8
N		78	197.9

205.71

65

2+00

N		19.7	186.0
cb		17.9	187.8
1/4		16.7	189.0
ϕ		15.8	189.9
1/4		14.9	190.8
cb		12.7	193.0
S		11.0	194.7
T.P.			-12.69 193.02
	+0.53	192.55	
		+	
		2+25	
S		10.2	193.3
cb		11.6	181.9
ϕ		13.0	180.5
cb		13.6	179.9
N		14.8	178.7
T.P.			13.03 180.52
	+0.31	180.83	
		+	
		2+50	
N		10.5	170.3
cb		9.8	171.0
ϕ		8.0	172.8
cb		7.0	173.8
S		5.5	175.3

180.83

66

2475

S	141	166.7
cb	161	164.7
♀	17.5	163.3
cb	18.7	162.1
N	19.6	161.2

3400

N	26.6	154.2
cb	26.0	154.8
♀	25.3	155.5
cb	24.4	156.4
S	22.7	158.1

T.P. -0.13 180.7

+13.09 193.79

T.P. 0.16 193.63

+12.98 206.61

-0.04 206.57

+12.95 219.52

T.P. -0.22 219.30

+12.72 232.02

T.P. -0.06 231.96

+9.50 241.46

B.M. N.W.B.P. 31st x Ash

(?)
6.39

235.07

25c. Sidewalks on El Cajon Ave
for New Cmt. walks Euclid To Boundary

S. side El Cajon Bet. 47th + Menlo

B.M. B.P. 5.97 353.17 347.20 + El Cajon

0+00 = W. end Existing cmt. walk 63.5 W. of S.W. cor 47th + El Cajon

S. cmt. cl. 5.18 347.99

+9.3 = N. edge cmt. walk 4.99 348.18

+14 = S. " " 4.96 348.21

+14 = S. line 4.9 348.3

0+15 West.

S. cmt. cl. 5.01 348.16

+9 4.8 348.4

+14 4.6 348.6

+15 = S. line 4.4 348.8

0+20 West

S. cmt. cl. 4.92 348.25

+9 4.7 348.5

+14 4.5 348.7

S. 3.7 349.5

0+40 W

S. cmt. cl. 4.75 348.42

+9 4.6 348.6

+14 4.4 348.8

S. 3.7 349.5

0+58' W

S. cmt. cl. 4.53 348.64

+9 4.4 348.8

+14 3.9 349.3

+15 = S. line 2.0 351.2

353.17

0+63 3W = E. line Alley on S. line

67

S. cmt. cl. on Alley Production 4.49 348.68

S. line on cmt. cl. 4.20 348.97

N. side El Cajon Bet Chamoun + Highland.

B.M. B.P. 5.22 361.36 356.14 + Highland

W. end cmt. walk 414.5 W. of

0+00 = N.W. cor Chamoun + El Cajon

N. cmt. cl. 4.35 357.01

+5 = S. edge cmt. walk 4.30 357.06

+10 = N. " " 4.20 357.16

+15 = N. 3.0 358.4

0+30 West

N. cmt. cl. 4.49 356.87

+5 4.4 357.0

+10 4.3 357.1

+15 3.0 358.4

0+50' W

N. cmt. cl. 4.57 356.79

+5 4.5 356.9

+10 4.2 357.1

+11 4.1 357.2

+13 2.9 358.5

+15 2.9 358.5

361.36
0+75' W.

N. end cl	4.68	356.68
+5	4.7	356.7
+10	4.5	356.8
+12	3.9	357.4
+15	3.0	358.4

0+93⁶⁰ W = E. end emt. walk

N. emt. cl	4.79	356.57
+5 = S. edge emt. walk	4.63	356.73
+10 = N " " "	4.53	356.83
+15	3.7	357.7

1+63⁴⁵ W = W. end emt. walk

N. emt. cl	5.08	356.28
+5 = S. edge emt. walk	4.97	356.39
+10 = N " " "	4.87	356.49
+15	4.1	357.3

1+90' W

N. emt. cl	5.20	356.16
+5	5.1	356.3
+10	4.9	356.4
+15	4.4	357.0

R+29³⁰ W = N.E. Cor El Cajon + Highland

N. emt. cl	5.29	356.07
+5	5.2	356.1
+10	5.2	356.1
+15	4.9	356.4

N. line El Cajon }
E. cl. Highland } on emt. cl.

5.32 356.04

S. side El Cajon bet H3. rd & Van Dyke

B.M. B.P. 7.23 364.96 357.73

S.W. 43rd

68 + El Cajon

0+00 = N. line 43rd St

S. emt. cl	7.20	357.76
+10	7.0	357.9
+20 = S.	6.7	358.2

0+65 West

S. emt. cl	4.20	360.76
+10	4.0	360.9
+20 = S	3.0	361.9

0+75^E = E. end walk. N.G.

S. emt. cl	3.71	361.25
+6 = N. edge walk	3.1	361.8 dirt
+6 = " " "	2.78	362.18 walk
+11 = S " "	2.76	362.20 walk + dirt
S.	2.8	362.1

1+10^E W = W. end walk

S. emt. cl	2.2	362.74
+6 = N. edge walk	1.90	363.06 walk + dirt
+11 = S " "	1.87	363.09 " " "
+20 = S.	1.5	363.4

1+25^E W = E. line Alley

S. emt. cl	1.71	363.25
+10	1.62	363.34
+20 = S. line	1.52	363.44

See page 72 for work as done

1/27/30
Flood Peavee
Bailey

Measurements & Levels for Sidewalk

E. Side of Louisiana St Wightman to Landis

S.E.P. 0.28 290.19 289.91 Louisiana St Wightman

T.P. 1.74 283.07 8.84 281.35

0+00 = S. Wightman

Sta 1+77.2

Prmt 1.77

Top Cb. 1.14

+2.75 = Edge walk 0.98

+8 = " " 0.75

+10 = F.L. 0.8

Sta. 2+05.4

Prmt 3.13 279.96

Top Cb. 2.45 280.64

+2.75 2.20 280.89

+8 2.01 281.02

+10 1.9 281.2

2+22 Cb broken down at this pt

Prmt 3.74 279.15

Top Cb. 3.14 279.95

+2.75 dirt 2.7 280.4

+8 3.0 280.1

+10 2.9 280.2

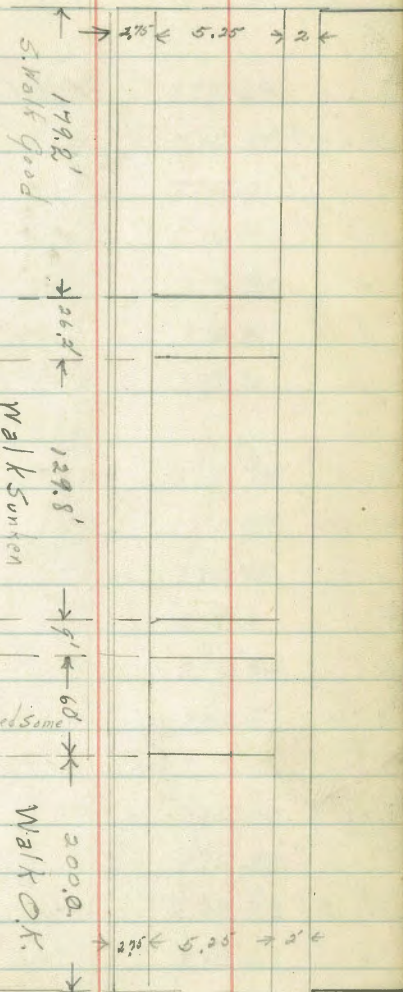
2+40

Prmt 4.95 278.14

Top Cb. 4.37 278.72

Wightman St

69



near Landis St.

283.09

+2.75 dirt (dug 25' & found no walk)	3.8	279.3
+8	3.7	279.4
+10	3.6	279.5

2 + 60

prmt	5.90	277.19
Top cb	5.91	277.88
+2.75 walk	5.07	277.62
+2.75 dirt	5.0	278.1
+8	5.0	278.1
+10	5.0	278.1

2 + 90

prmt	6.68	276.41
Top cb	6.09	277.09
+2.75 walk	6.27	276.82
Same dirt	5.7	277.4
+8 walk	6.57	276.52
Same dirt	5.5	277.6
+10	5.6	277.5

3 + 00

prmt	7.22	275.87
Top cb	6.42	276.67
+2.75 walk	6.57	276.58
Same dirt	6.2	276.9
+8 walk	6.80	276.29
Same dirt	5.8	277.3
+10	5.8	277.3

283.09

Chinlet Needed Here $3 + 0.8.5 = 4$ 2' x 2' Grating inlet
 This is inadequate for drainage 7.43 on Grating

3 + 20

prmt	7.40	275.69
Top cb	6.71	276.38
+2.75 walk	6.68	276.41
dirt	6.4	276.7
+8 walk	7.23	275.86
dirt	6.3	276.8
+10	6.1	277.0

3 + 35.2

prmt	7.30	275.79
Top cb	6.87	276.27
+2.75	6.90	276.19
Same dirt	6.7	276.4
+8 walk - dirt level	6.55	276.54
+10	6.6	276.5

3 + 44.2

prmt	7.06	276.03
Top cb	6.60	276.49
+2.75 } walk	6.56	276.53
+8 }	6.48	276.61

3 + 77 brk in grade

prmt	6.80	
Top cb	6.30	
+2.75 walk	6.26	

28369

71

+ 8

619

4+04

prmt

614

Top C6

536

+275 } walk

540

+ 8

527

T.P.

11.33

291.81

308

280.01

SE.B.P.

143

289.91

Louisiana
Wightman

A3rd West to El Cajon Ave S.W. Notes
 Alley- June 19-30

Page 68

	HI	Sedg	SWL	OK	SWL	OK
0+00	6.7	$\frac{6.4}{11.0}$	$\frac{6.3}{15.5}$	+1.3	$\frac{5.2}{15.5}$	$\frac{1.8}{20}$
0+6.5	6.9	$\frac{6.6}{15.0}$	$\frac{6.4}{15.0}$	+0.2	$\frac{6.4}{15.0}$	$\frac{1.2}{5.5}$
0+7.5	7.2	6.7				$\frac{1.0}{6.0}$
1+10	6.2	5.9				$\frac{1.5}{5.5}$

72

Walker
Bliss
Drebert
10-17-30

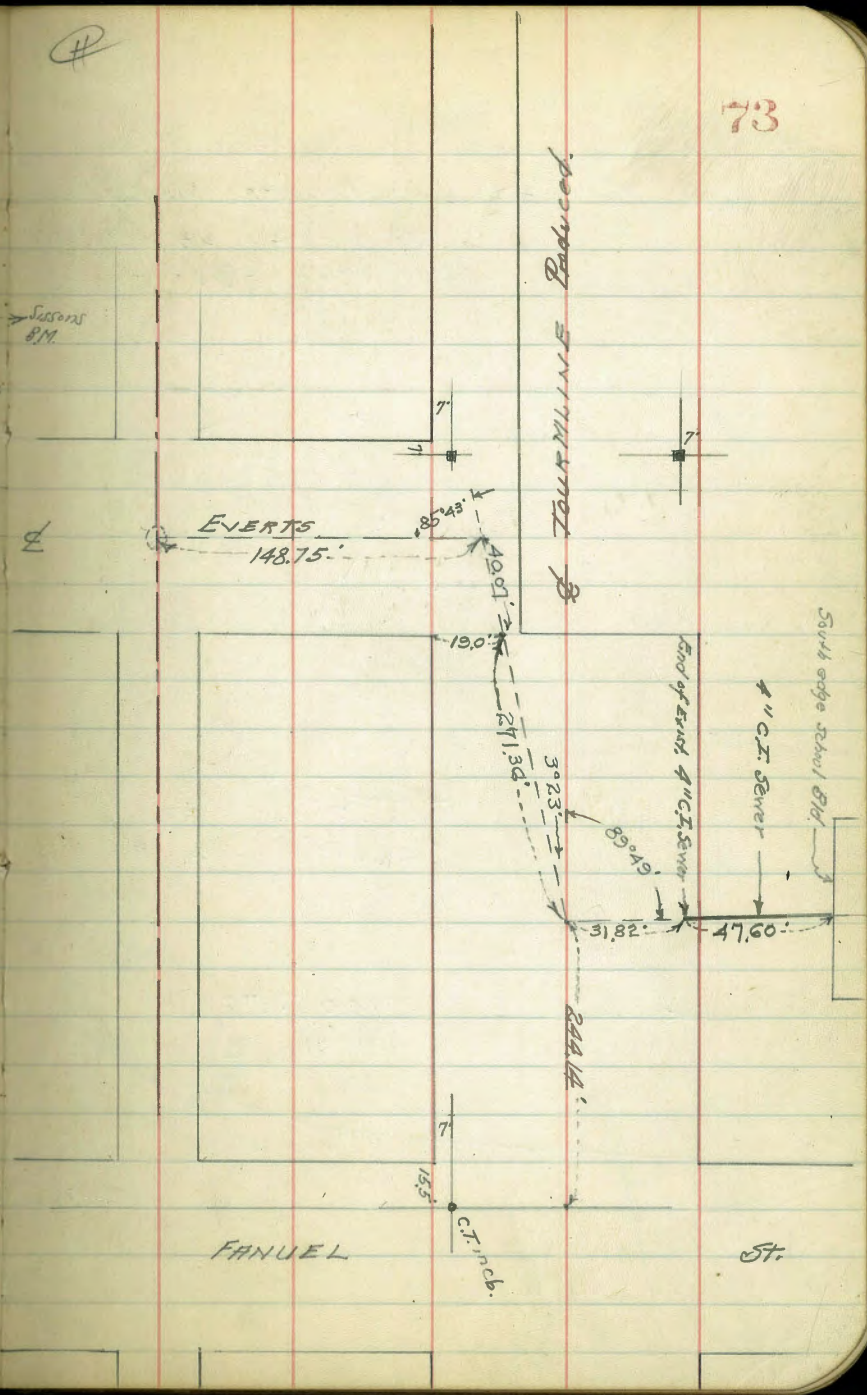
PRELIMINARY LOCATION
AND LEVELS FOR SEWER
IN TOURMALINE AND EVERTS, etc.

(#)

73

	4.11	162.66		158.55	S.W. C.T. 1066 FANUEL & Tourmaline
T.P.	6.70	158.08	11.28	151.38	S.E. Hydr. Stake
			15.65	142.43	S.W. 7' Hub. Everts & Tourmaline
T.P.	18.96	158.08	18.96	139.12	S.W. 7' Hub. Everts & Tourmaline
			18.16	139.92	S.W. 7' Hub. Everts & Tourmaline
0+00 - 47.6' Top 4" C.I. of Sid.		6.96		151.12	
0+00 on ^{top} End Exit 4" C.I. Pipe		7.81		150.27	
0+00 on Ground		6.2		151.9	
+31.82 = Δ 84° 32' 12"		6.4		151.7	
+50		7.1		151.0	
1+00		8.4		149.7	
+50		10.6		147.5	
2+00		12.1		146.0	
+50		14.0		144.1	
3+00 = Everts St.		19.7		143.4	
+43.25 = Δ Lt. 85° 43'		17.3		140.8	
4+00		18.1		140.0	
T.P.	0.47	146.26	12.39	145.79	
4+50		7.2		139.1	
+92 = Δ Exist. M.H. or Rim.		7.65		138.61	
4+92 - " " " Flow		14.73		131.53	

131.58 Prec. Beh. Sewer
Profile



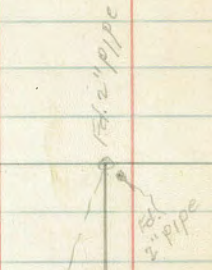
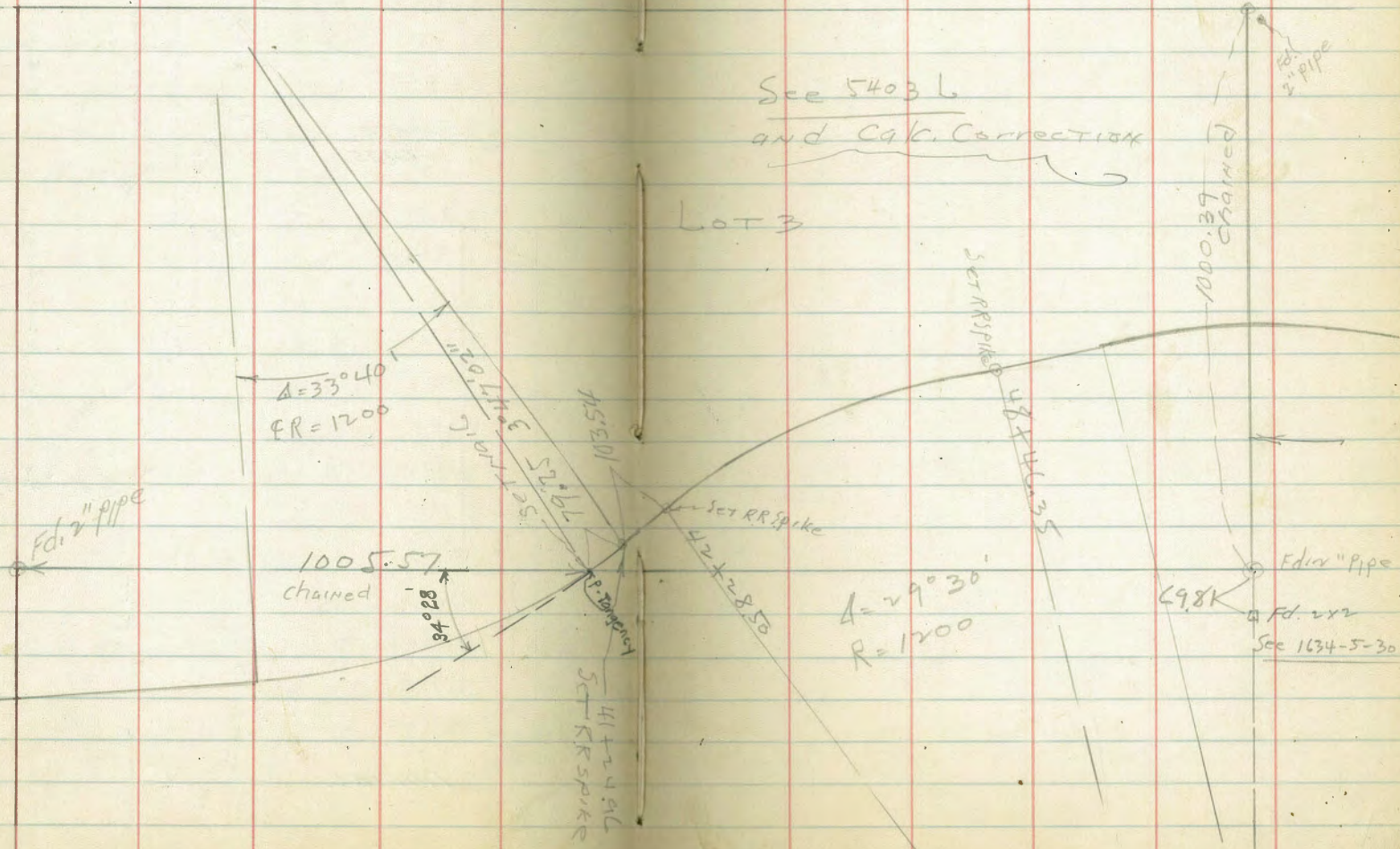
FANUEL

ST.

cam Check Survey Lot 3
 C.S.
 W.M.
 6-14-75. Marchena Tract Map # 828
 See Co. E.B. 749 - 237-7, p7
 " also " 1498-49, City.

See 5403 L
 and Calc. Correction

LOT 3



Fd. 2" pipe
 69.81
 Fd. 2" pipe
 See 1634-5-30

1153.01
 SET RR SPIKE
 412.49
 SET RR SPIKE

$\Delta = 33^\circ 40'$
 $R = 1200$

$\Delta = 29^\circ 30'$
 $R = 1200$

1000.37
 CHAINED

Fd. 2" pipe

1005.57
 CHAINED

1120.14
 SET RR SPIKE

SET RR SPIKE
 487.43

SET RR SPIKE
 422.85

94.28

69.81

75

DIRECTIONS FOR USE OF TABLES

30897
13.18
29579
003
297 2/3
295 2/3

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 1/2 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body

1.41 = Transit.

IMPROVED TABLES
AND
INFORMATION

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given T may be found by dividing tangent (or external), opposite T by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

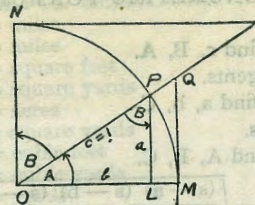


TABLE II

TRIGONOMETRIC FORMULAE.

$$\angle A = \angle MOP \quad \angle B = \angle PON = \angle OPL$$

$$R = OB = c = 1$$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

$$\sin \frac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \quad \cos \frac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \quad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Sines} \quad \frac{\sin A}{a} = \frac{\sin B}{b} = \frac{\sin C}{c}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$$

TABLE II—Continued
TRIGONOMETRIC FORMULAE (continued)

In any triangle:

Given a, b, C; to find c, B, A.

Use Law of Tangents.

Given A, B, c; to find a, b, C.

Use Law of Sines.

Given a, b, c; to find A, B, C.

$$\text{Let } \frac{a+b+c}{2} = s, \sqrt{\frac{(s-a)(s-b)(s-c)}{s}} = r$$

$$\cos \frac{1}{2} A = \sqrt{\frac{s(s-a)}{bc}}$$

$$\tan \frac{1}{2} A = \frac{r}{s-a}$$

$$\tan \frac{1}{2} B = \frac{r}{s-b}$$

$$\tan \frac{1}{2} C = \frac{r}{s-c}$$

Area of a triangle:

$$\text{Area} = \frac{1}{2} ab \sin C$$

$$\text{Area} = \sqrt{s(s-a)(s-b)(s-c)}$$

PRISMOIDAL FORMULA.

$$\text{Vol} = \frac{h}{6} (E+b+4M)$$

h = altitude: b, B = bases; M = midsection

TABLE III
INCHES AND FRACTIONS OF AN INCH IN DECIMALS OF A FOOT

	0	1	2	3	4	5	6	7	8	9	10	11
$\frac{1}{16}$.0052	.0885	.1719	.2552	.3385	.4219	.5052	.5885	.6719	.7552	.8385	.9219
$\frac{1}{8}$.0104	.0938	.1771	.2604	.3438	.4271	.5104	.5938	.6771	.7604	.8438	.9271
$\frac{3}{16}$.0156	.0990	.1823	.2656	.3490	.4323	.5156	.5990	.6823	.7656	.8490	.9323
$\frac{1}{4}$.0208	.1042	.1875	.2708	.3542	.4375	.5208	.6042	.6875	.7708	.8542	.9375
$\frac{5}{16}$.0260	.1094	.1927	.2760	.3594	.4427	.5260	.6094	.6927	.7760	.8594	.9427
$\frac{3}{8}$.0313	.1146	.1979	.2813	.3646	.4479	.5313	.6146	.6979	.7813	.8646	.9479
$\frac{7}{16}$.0365	.1198	.2031	.2865	.3698	.4531	.5365	.6198	.7031	.7865	.8698	.9531
$\frac{1}{2}$.0417	.1250	.2083	.2917	.3750	.4583	.5417	.6250	.7083	.7917	.8750	.9583
$\frac{9}{16}$.0469	.1302	.2135	.2969	.3803	.4635	.5469	.6302	.7135	.7969	.8802	.9635
$\frac{5}{8}$.0521	.1354	.2188	.3021	.3854	.4688	.5521	.6354	.7188	.8021	.8854	.9688
$\frac{11}{16}$.0573	.1406	.2240	.3073	.3906	.4740	.5573	.6406	.7240	.8073	.8906	.9740
$\frac{3}{4}$.0625	.1458	.2292	.3125	.3958	.4792	.5625	.6458	.7292	.8125	.8958	.9792
$\frac{7}{8}$.0677	.1510	.2344	.3177	.4010	.4844	.5677	.6510	.7344	.8177	.9010	.9844
$\frac{15}{16}$.0729	.1563	.2396	.3229	.4063	.4896	.5729	.6563	.7396	.8229	.9063	.9896
$\frac{1}{1}$.0781	.1615	.2448	.3281	.4115	.4948	.5781	.6615	.7448	.8281	.9115	.9948
	.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167	1.0000
	0	1	2	3	4	5	6	7	8	9	10	11

TABLE IV
USEFUL RELATIONS

Lineal feet $\times .00019$ = miles
 Lineal yards $\times .0006$ = miles
 Square inches $\times .007$ = square feet
 Square feet $\times .111$ = square yards
 Square yards $\times .0002067$ = acres
 Acres $\times 4840$ = square yards
 Cubic inches $\times .00058$ = cubic feet
 Cubic feet $\times .03704$ = cubic yards
 Links $\times .22$ = yards
 Links $\times .66$ = feet
 Feet $\times 1.5$ = links

$$360^\circ = 21600' = 1296000''$$

$$\text{Radius} = \text{arc of } 57.2957790^\circ$$

$$\text{Arc of } 1^\circ (\text{radius} = 1) = .017453292$$

$$\text{Arc of } 1' (\text{radius} = 1) = .000290888$$

$$\text{Arc of } 1'' (\text{radius} = 1) = .000004848$$

$$\pi = 3.141592654 \quad \sqrt{\frac{1}{4}} = 0.564190$$

$$\frac{\pi}{4} = 0.785398163 \quad \sqrt[3]{\frac{6}{\pi}} = 1.240700982$$

$$\frac{\pi}{6} = 0.523598776 \quad \pi^2 = 9.869604401$$

$$\sqrt{\frac{4}{\pi}} = 1.128379167 \quad \frac{1}{\pi^2} = 0.101321184$$

$$\frac{\pi}{6} = 0.523598776 \quad \sqrt{\pi} = 1.772453851$$

$$\frac{4\pi}{3} = 4.188790205 \quad \frac{1}{\pi} = 0.3183099$$

Curvature of Earth's surface = about 0.7 feet in 1 mile

Curvature in feet = $0.667 (\text{Dist. in miles})^2$

Difference between arc and chord length, 0.05 feet in $11\frac{1}{2}$ miles

$$\text{Probable error of a single observation} = 0.6754 \sqrt{\frac{Mv^2}{n-1}}$$

Error in chaining of 0.01 feet in 100 feet:

Due to—

1. Length of tape error of 0.01 feet
2. Alignment. One end 1.4 feet out of line
3. Sag of tape at centre of 0.61 feet.
4. Temperature difference of 15°
5. Difference of pull of 15 lbs.

STADIA REDUCTION FORMULAE.

$$\text{Horizontal Distance} = R - R \sin^2 a + C \cos a$$

$$\text{Vertical Distance} = R \frac{1}{2} \sin 2a + C \sin a$$

distance from Object glass to cross hairs

$$R = \text{Reading} \times \frac{\text{distance from Object glass to cross hairs}}{\text{distance between cross hairs}}$$

C = distance from Object glass to cross hairs + distance from Object glass to center of instrument.

a = angle of elevation for mid Reading

0.0104
A20
208°

TABLE X.
MIDDLE ORDINATES OF RAILS
Length of Rail (feet)

C	R	30	28	26	24	22	20	C	R	30	28	26	24	22	20
o /	Feet	Inch	Inch	Inch	Inch	Inch	Inch	o	Feet	Inch	Inch	Inch	Inch	Inch	Inch
0-20	17189	.08	.07	.06	.05	.04	.03	8	716.8	1.88	1.64	1.42	1.20	1.01	.84
0-40	8594	.16	.14	.12	.10	.08	.07	9	637.3	2.12	1.84	1.60	1.35	1.14	.94
1-0	5730	.24	.20	.18	.15	.13	.10	10	573.7	2.36	2.05	1.78	1.50	1.27	1.04
1-20	4297	.31	.27	.23	.20	.17	.13	11	521.7	2.59	2.26	1.95	1.65	1.39	1.15
1-40	3438	.39	.34	.29	.25	.21	.17	12	478.3	3.83	2.47	2.15	1.81	1.54	1.26
2-0	2865	.47	.41	.35	.30	.25	.20	13	441.7	3.05	2.66	2.30	1.96	1.66	1.36
2-20	2456	.55	.48	.41	.35	.29	.23	14	410.3	3.30	2.87	2.48	2.10	1.78	1.46
2-40	2149	.63	.55	.47	.40	.33	.27	15	383.1	3.54	3.08	2.68	2.26	1.91	1.57
3-0	1910	.71	.62	.53	.45	.38	.31	16	359.3	3.76	3.28	2.83	2.40	2.04	1.67
3-20	1719	.78	.68	.59	.50	.42	.35	17	338.3	4.00	3.48	3.02	2.57	2.16	1.78
3-40	1563	.86	.75	.65	.55	.46	.38	18	319.6	4.21	3.67	3.18	2.70	2.28	1.87
4-0	1433	.94	.82	.71	.60	.50	.42	19	302.9	4.45	3.89	3.36	2.86	2.41	1.98
4-20	1323	1.02	.89	.77	.65	.55	.45	20	287.9	4.70	4.09	3.55	3.00	2.54	2.09
4-40	1228	1.10	.96	.83	.70	.59	.48	22	262.0	5.16	4.44	3.84	3.30	2.80	2.29
5	1146	1.18	1.03	.89	.75	.63	.52	24	240.5	5.64	4.92	4.20	3.59	3.04	2.50
6	955.3	1.41	1.23	1.06	.90	.76	.62	26	222.3	6.07	5.29	4.58	3.88	3.29	2.70
7	819.0	1.65	1.44	1.24	1.05	.89	.73								

TABLE XI.
SHORT RADIUS CURVES

Radius Feet	Chord Feet	Central Angle	Deflection Angle	Deflection for 1 Foot
35	10	16-26	8-13	49.3
45	10	12-46	6-23	38.3
50	15	17-16	8-38	34.5
60	15	14-22	7-11	28.8
75	15	11-30	5-45	23.0
100	20	11-30	5-45	17.3
120	20	9-34	4-47	14.3
150	20	7-39	3-49	11.5
190	25	7-32	3-46	9.15
200	25	7-10	3-35	8.6
225	25	6-25	3-12	7.7
240	25	5-58	2-59	7.2
250	25	5-44	2-52	6.9
275	25	5-12	2-36	6.2
288	50	9-58	4-59	6.0
300	50	9-32	4-46	5.7
350	50	8-12	4-06	4.9
376	50	7-40	3-50	4.6
400	50	7-10	3-35	4.3
410	50	7-00	3-30	4.2

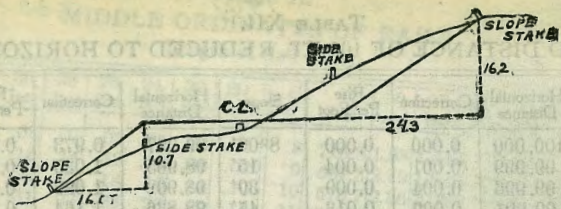
To find length of curve divide angle from P. C. to P. T. by central angle of chord, and multiply by length of chord.

TABLE XII.
INCLINED DISTANCE OF 100 FT. REDUCED TO HORIZONTAL

Slope	Horizontal Distance	Correction	Rise Per Foot	Slope	Horizontal Distance	Correction	Rise Per Foot
0°00'	100.000	0.000	0.000	8°00'	99.027	0.973	0.139
15'	99.999	0.001	0.004	15'	98.965	1.035	0.143
30'	99.996	0.004	0.009	30'	98.903	1.098	0.148
45'	99.991	0.009	0.013	45'	98.836	1.164	0.152
1 00	99.985	0.015	0.017	9 00	98.769	1.231	0.156
15	99.976	0.024	0.022	15	98.700	1.300	0.161
30	99.966	0.034	0.026	30	98.629	1.371	0.165
45	99.953	0.047	0.031	45	98.556	1.444	0.169
2 00	99.939	0.061	0.035	10 00	98.481	1.519	0.174
15	99.923	0.077	0.039	15	98.404	1.596	0.178
30	99.905	0.095	0.044	30	98.325	1.675	0.182
45	99.885	0.115	0.048	45	98.245	1.755	0.187
3 00	99.863	0.137	0.052	11 00	98.163	1.837	0.191
15	99.839	0.161	0.057	15	98.079	1.921	0.195
30	99.813	0.187	0.061	30	97.992	2.008	0.199
45	99.786	0.214	0.065	45	97.905	2.095	0.204
4 00	99.756	0.244	0.070	12 00	97.815	2.185	0.208
15	99.725	0.275	0.074	15	97.723	2.277	0.212
30	99.692	0.308	0.078	30	97.630	2.370	0.216
45	99.657	0.343	0.083	45	97.534	2.466	0.221
5 00	99.619	0.381	0.087	13 00	97.437	2.563	0.225
15	99.580	0.420	0.092	15	97.338	2.662	0.229
30	99.540	0.460	0.096	30	97.237	2.763	0.233
45	99.497	0.503	0.100	45	97.134	2.866	0.238
6 00	99.452	0.548	0.105	14 00	97.030	2.970	0.242
15	99.406	0.594	0.109	15	96.923	3.077	0.246
30	99.357	0.643	0.113	30	96.815	3.185	0.250
45	99.307	0.693	0.118	45	96.705	3.295	0.255
7 00	99.255	0.745	0.122	15 00	96.593	3.407	0.259
15	99.200	0.800	0.126	15	96.479	3.521	0.263
30	99.144	0.856	0.131	30	96.363	3.637	0.267
45	99.087	0.913	0.135	45	96.246	3.754	0.271

TABLE XIII.
MINUTES IN DECIMALS OF A DEGREE.

0 30"	.00833	10 30"	.17500	20 30"	.34167	30 10"	.50833	40 30"	.67500	50 10"	.84167
1 00	.01667	11 00	.18333	21 00	.35000	31 00	.51667	41 00	.68333	51 00	.85000
30	.02500	30	.19167	30	.35833	30	.52500	30	.69167	30	.85833
2 00	.03333	12 00	.20000	22 00	.36667	32 00	.53333	42 00	.70000	52 00	.86667
30	.04167	30	.20833	30	.37500	30	.54167	30	.70833	30	.87500
3 00	.05000	13 00	.21667	23 00	.38333	33 00	.55000	43 00	.71667	53 00	.88333
30	.05833	30	.22500	30	.39167	30	.55833	30	.72500	30	.89167
4 00	.06667	14 00	.23333	24 00	.40000	34 00	.56667	44 00	.73333	54 00	.90000
30	.07500	30	.24167	30	.40833	30	.57500	30	.74167	30	.90833
5 00	.08333	15 00	.25000	25 00	.41667	35 00	.58333	45 00	.75000	55 00	.91667
30	.09167	30	.25833	30	.42500	30	.59167	30	.75833	30	.92500
6 00	.10000	16 00	.26667	26 00	.43333	36 00	.60000	46 00	.76667	56 00	.93333
30	.10833	30	.27500	30	.44167	30	.60833	30	.77500	30	.94167
7 00	.11667	17 00	.28333	27 00	.45000	37 00	.61667	47 00	.78333	57 00	.95000
30	.12500	30	.29167	30	.45833	30	.62500	30	.79167	30	.95833
8 00	.13333	18 00	.30000	28 00	.46667	38 00	.63333	48 00	.80000	58 00	.96667
30	.14167	30	.30833	30	.47500	30	.64167	30	.80833	30	.97500
9 00	.15000	19 00	.31667	29 00	.48333	39 00	.65000	49 00	.81667	59 00	.98333
30	.15833	30	.32500	30	.49167	30	.65833	30	.82500	30	.99167
10 00	.16667	20 00	.33333	30 00	.50000	40 00	.66667	50 00	.83333	60 00	1.00000



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING

SLOPE 1 1/4 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

30784
1004
29780
591
29875 = T Transit.
57
2933
150
59
91
71966
732
763

1398
978
2356

To find

27863 - dist from 17' E. S. 1/4. Channing to 11th Mentone

ENGINEERING DEPARTMENT
CITY OF SAN DIEGO,
CALIFORNIA.

15 = 273
30 = 290

126
14.03
025

+44
12122/20
113.13680
56.56
169.69

29723
1403
28320
025
28345

987
615
722

29723
28345
1378 below
+35
18.13

319.66
922
274

13.8
78
216

740

10.8 x .014

1.745
0524

570.8

2701
12516

457.35416

BM 100 667	45.60
7 106.67	13.09
13.12	58.69
7.093.52	0.16
1.54	58.53
7 95.06	12.98
13.09	71.51
7.081.97	0.04
0.97	71.47
7 82.94	12.95
12.65	84.20
7.070.29	0.22
10.32	84.20
7.070.61	12.22
12.69	96.92
7.057.92	0.06
0.53	96.86
7 58.43	9.50
13.23	106.36
7.045.42	6.47
0.31	99.89
45.73	
0.13	
45.60	