

1300

PASTS

LEVEL BOOK

No. 330-F

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No. 380 to 385 6/20/64

MAY 21-28

X. Sec. Imperial	from Book 1295-80	-	1
" " Alley. BIK 407-	Helpingstone Add	37 th St & 38 th St.	69
" " Park Ave	Hamilton to Oregon		72
side walks on Kettner Blvd-	Kalmia & Laurel		76

Imperial

Cont from Book 1295 P 80
 159.96
 160.04

Nov. 21-28
 Loudon
 15bell
 Morgan.

11+65

5L	10.7	149.2
+8	10.6	149.4
cb	10.2	149.8
+1	10.2	149.8
+2	10.6	149.4
+7 S Pav	10.48	149.48
1/4	10.48	149.48
+	10.39	149.57
#0 ⁸ & Pav	10.39	149.57
1/4	10.42	149.54
+1 ⁵ N Pav	10.48	149.48
+6	10.6	149.4
cb	10.4	149.6
NL	10.8	149.1
4N	11.5	148.5
5N	15.2	144.8
12N	15.2	144.8
12+00		
6N	15.0	145.0
5N	11.8	148.2
NL	10.7	149.2
cb	10.0	150.0
+1	10.3	149.7
+5 ⁸ N Pav	10.03	149.93

12+00

159.96
160.04

1/4	9.96	150.00
+7 ³ & Pav	9.97	149.99
1/4	9.97	149.99
1/4	10.05	149.91
+0 ⁸ S Pav	10.09	149.87
+5	10.3	149.7
eb	9.9	150.1
+8	10.2	149.8
SL	9.4	150.5
12+30		
SL	7.2	152.7
+2	8.7	151.3
+5	9.0	151.0
+6	9.9	150.1
eb	9.5	150.5
+2	10.0	150.0
+6 ³ S Pav	9.83	150.13
1/4	9.77	150.19
1/4	9.51	150.45
+0 ⁸ & Pav	9.49	150.47
1/4	9.40	150.56
+2 N Pav	9.41	150.55
+6 ⁵	9.5	150.5
eb	9.3	150.7
NL	9.3	150.6
1N	9.2	

12+30

159.96

2

1N	10.8	149.2
5N	14.9	145.1
12+65		
8N	13.2	146.8
2N	7.6	152.4
NL	7.7	152.2
eb	8.3	151.7
+2	8.6	151.4
+6 ³ N Pav	8.25	151.71
1/4	8.26	151.70
1/4 & Pav	8.48	151.48
1/4	8.87	151.09
+1 ⁵ S Pav	8.96	151.00
7	9.5	150.5
eb	9.0	151.0
+3	8.6	151.4
+6	9.2	150.8
+8	8.8	151.2
+9	8.7	151.3
SL	8.0	151.9

Imperial.
159.96

$\angle R = 42^\circ 17'$ $R = 275$ $L = 202.96$

$12 + 80^{57} = B.C$

SL	8.6	151.3
+2	9.0	151.0
+6	8.2	151.8
cb	8.9	151.1
+A ⁵ S Paw	8.50	151.46
$\frac{1}{4}$	8.27	151.73
+5 ² $\frac{1}{4}$ Paw	7.92	152.04
$\frac{1}{4}$	7.84	152.12
$\frac{1}{4}$ N Paw	7.61	152.35
+4	8.0	152.0
+5	7.8	152.2
cb	7.7	152.3
NL	7.4	152.5
6N	7.7	152.3
12N	10.9	149.1
13N	13.8	146.2
13 + 14 ³⁹		
8N	14.3	145.7
8N	10.3	149.7
NL	8.5	151.4
+3	6.8	153.2
cb	6.3	153.7
+5	6.5	153.5
cb	6.6	153.4

Imperial.
159.96

3

6 Parts

13 + 14³⁹

cb + 2 ³ N Paw	
$\frac{1}{4}$	
+3 ⁶ $\frac{1}{4}$ Paw	
$\frac{1}{4}$	
+5 ² S Paw	
cb	
+3	
+4	
SL	
1's	
2's	
3's	
5's	
13 + 14 ²¹	
6's	
5's	
4's	
3's	
SL	
+5	
cb	
+0 ² S Paw	
$\frac{1}{4}$	
+1 ⁶ $\frac{1}{4}$ Paw	

6.49	153.47
6.67	153.29
6.83	153.13
7.00	153.0
7.39	152.57
7.6	152.4
7.9	152.1
7.6	152.4
7.5	152.4
7.7	152.3
8.5	151.5
7.8	152.2
7.6	152.4
6.6	153.4
7.4	152.6
7.5	152.5
6.7	153.3
6.4	153.5
6.4	153.6
6.3	153.7
6.21	153.75
5.75	154.25
5.66	154.30

Imperial
159.96

13+48²¹

+	5.33	154.63
+4 N. Pav	5.25	154.71
'A	5.4	154.6
eb	5.2	154.8
+2	5.2	154.8
+5	5.6	154.4
N.L.	8.6	151.3
3N	10.2	149.8
3N	14.1	145.9
13N	9.9	150.1
13+82 ⁰³		
13N	6.2	153.8
3N	9.2	150.8
N.L.	9.6	150.3
+8	3.9	156.1
eb	3.7	156.3
+6	4.4	155.6
'A	4.3	155.7
+3 N. Pav	4.25	155.71
+	4.20	155.76
+4 ² & Pav	4.33	155.63
'A	4.52	155.48
eb s Pav	5.08	154.88
+5	5.2	154.8
5L	5.6	154.3
35	6.4	153.6

Imperial

159.96

4

13+82⁰³

160.04

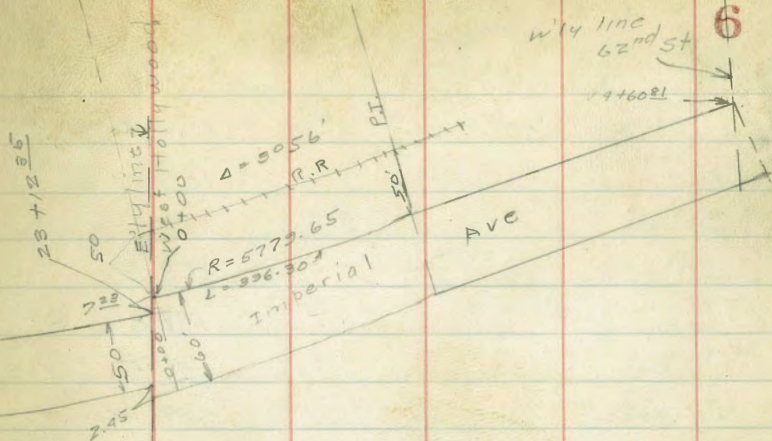
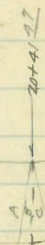
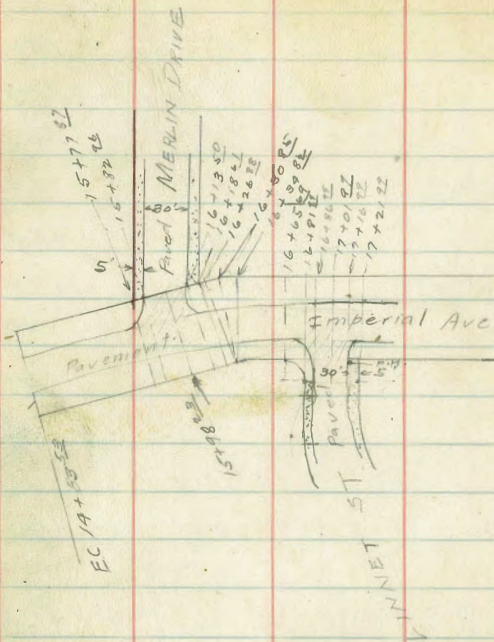
5's	5.5	154.5
14+15 ⁸⁵		
5.L.	4.5	155.4
+1	5.3	154.7
+2	5.2	154.8
+5	4.0	156.0
eb	3.8	156.2
+1 ⁸ S Pav	3.94	156.02
'A	3.49	156.57
+4 & Pav	3.24	156.72
+	3.00	156.96
+6 N. Pav	2.70	157.26
'A	2.8	157.2
+3	3.0	157.0
+3	2.6	157.4
eb	2.3	157.7
+4	2.6	157.4
+9	5.2	154.8
N.L.	4.4	155.6
3N	3.1	156.9
10N	6.7	153.3
T.P.	8.23	167.45
		37
		14
	0.82	159.22

14 + 4967 167.37
167.45

12N	11.5	155.9
N.L	9.3	158.1
+4	8.5	158.9
eb	8.8	158.6
+2	8.6	158.8
+5 ⁸ N Pav	9.01	158.36
1/4	9.05	158.32
± ± Pav	9.42	157.95
1/4	9.92	157.45
+1 S Pav	10.05	157.32
eb	10.6	156.8
+1	10.2	157.0
+4	11.3	156.1
+5	9.6	157.8
+8	7.4	160.0
S.L	7.5	159.9
14 + 8353 = F.C.		
S.L	5.5	151.9
+3	5.4	162.0
+9	10.4	157.0
eb	10.4	157.0
+1	9.6	157.8
+5	9.0	158.4
1/4	9.1	158.3
+2 ⁸ S Pav	9.00	158.37

14 + 8353 167.37

±	8.62	158.75
+4 ³ ± Pav	8.31	159.06
1/4	8.16	159.21
+5 ⁸ N Pav	7.95	159.42
eb	8.0	159.4
+3	7.8	160.6
N.L	7.5	159.9
7N	7.9	159.5
15N	6.7	160.7
15+00		
10N	6.8	160.6
2N	6.7	160.7
N.L	7.3	160.1
eb N Pav	7.54	159.83
1/4	7.81	159.56
+1 ± Pav	7.89	159.48
±	8.30	159.07
+2 ⁶ S Pav	8.50	158.87
1/4	8.8	158.6
+3	8.8	158.6
eb	10.1	157.3
+1	7.9	159.5
+9	5.2	162.2
S.L	5.1	162.3



	37	
15+30	167.45	
S.L	3.0	164.4
+8	7.5	159.9
+9	8.9	158.5
cb	8.9	158.5
+1	8.6	158.8
1/4	7.9	159.5
± S. Pav	7.71	159.66
1/4	7.21	160.16
+2 ² ± Pav	7.14	160.23
cb	6.87	160.50
+2 ⁵ N Pav	6.79	160.58
N.L.	6.9	160.5
15+65		
N.L.	6.2	161.2
+7 ² N Pav	6.27	160.10
cb	6.29	161.08
+6 ² ± Pav	6.53	160.83
1/4	6.57	160.80
±	6.97	160.40
+0 ⁵ S Pav	7.02	160.35
1/4	6.9	160.5
+5	7.0	160.4
cb	7.7	159.7
+1	8.2	159.2
+2	7.4	160.0
S.L	1.5	165.9

	37	7
B.M	3.10	164.35
15+77 ⁸² = w L Merlin Dr on North		
S.L	1.8	165.6
+8	6.2	161.2
+9	7.9	159.5
cb	7.2	160.2
+5	6.7	160.7
1/4	6.7	160.7
+6 ⁵ S Pav	6.81	160.56
±	6.71	160.66
1/4	6.35	161.02
+0 ⁵ ± Pav	6.32	161.05
cb	6.15	161.22
+3 N Pav	6.20	161.17
+7	5.6	161.8
N.L. walk	5.27	162.10
15+82 ²⁶ = w cb Merlin.		
N.L. top cb	5.30	162.07
N.L. put	6.06	161.31
cb Pav	6.12	161.25
1/4 v	6.32	161.05
±	6.63	160.74
1 ² S Pav	6.76	160.61
1/4	6.6	161.8
+7	7.0	160.4
cb	7.6	159.8

15+82⁹⁶37
167.45

+1	7.8	159.6
S.L.	1.4	166.0
15+98 ²³	= ♀ Merlin	
S.L.	1.5	165.9
+9	7.2	160.2
cb	7.1	160.3
+5	6.5	160.9
1/4	6.4	161.0
+3 ⁵ S Pav	6.56	160.81
♀	6.41	160.96
+5 ♀ Pav	6.23	161.14
1/4 Pav	6.13	161.24
cb Pav	5.93	161.44
NL ✓	5.83	161.54
16+135 ⁰	= E. cb Merlin	
N.L. gut	6.08	161.29
N.L. top cb	5.26	162.11
+4 ⁵ N Pav	5.91	161.46
cb Pav	5.99	161.38
1/4 ✓	6.05	161.32
♀ ✓	6.21	161.16
+6 S Pav	6.46	160.91
1/4	6.5	161.9
+5	6.6	160.8
cb	7.0	160.4
S.L.	0.5	167.0

37
167.4516+18⁶¹ = E.L. Merlin.

8

S.L.	1.4	165.9
+6	4.7	162.7
+9	6.9	160.5
cb	6.9	160.5
+4	6.4	161.0
1/4	6.5	160.9
+0 ⁵ S Pav	6.42	160.95
♀	6.15	161.22
1/4	6.02	161.35
+4 ⁷ N Pav	6.01	161.36
cb	5.7	161.5
+4	5.5	161.9
N.L. wall T	5.26	162.11
16+26 ⁸⁸	= Len. South	
N.L.	5.2	162.2
+9	5.4	162.0
cb	5.6	161.8
+9	6.0	161.4
+6 N Pav	6.05	161.32
1/4	6.04	161.35
♀ ♀ Pav	6.12	161.25
1/4	6.31	161.06
+1 ⁷ S Pav	6.37	161.00
+6	6.4	161.0
cb	6.8	160.6
+9	6.8	160.6

16737

~~16+26⁸⁸~~

S.L.	1.2	166.2
16+30 ⁸⁵ = 16+26 ⁸⁸ = L on North.		
S.L.	1.2	166.2
+8	6.8	160.6
cb	6.8	160.6
+15	6.4	161.0
+6 s Pav	6.36	161.01
1/4	6.31	161.06
1/4	6.12	161.25
1/4	6.01	161.36
+1 N Pav	6.01	161.36
+5	6.4	161.3
cb	5.7	161.7
N.L.	5.2	162.2

~~16+34⁸² = 16+26⁸⁸~~

N.L.	5.2	162.2
+3	5.2	162.2
cb	5.9	161.5
+5	6.1	161.3
+6 N Pav	6.04	161.33
1/4	6.01	161.36
1/4	6.13	161.24
1/4	6.31	161.06
+1 s Pav	6.34	161.03
+6 ⁸⁵	6.4	161.0
cb	6.9	160.5

16737

9

~~16+34⁸² = 16+26⁸⁸~~

cb+2	6.8	160.6
S.L.	1.2	166.2
16+65 ⁶⁴ = B.C. sw. ret. Linnat st.		
S.L.	0.1	167.3
+7	3.7	163.7
+9	6.2	161.2
cb	6.5	160.9
+3	6.0	161.4
+6 s Pav	6.12	161.25
1/4	6.17	161.20
1/4	5.98	161.39
1/4	6.05	161.32
+1 N Pav	6.07	161.30
cb	5.5	162.9
N.S.L.	5.0	162.4

~~16+81⁹⁹ = w.L. Linnat Pav.~~

N.S.L.	5.2	162.2
+5	5.2	162.2
cb	5.4	162.0
+6 N Pav	6.05	161.32
1/4	6.04	161.33
1/4	6.04	161.33
1/4	5.99	161.38
cb Pav	5.85	161.52
+1 ³ s Pav	5.84	161.83
S.L.	5.6	161.8

16737

16+72 (out of Place)

SL	4.9	162.5
+7	6.0	161.1
+5 ⁵ Pav	6.05	161.32
'A	6.05	161.32
+ + Pav	5.96	161.41
'A	6.02	161.35
+1	6.04	161.34
cb	5.5	161.9
NL	5.1	162.3

16+86⁹⁹ = wcb Linnet

SL on Pav	5.60	161.77
cb ✓	5.87	161.50
'A ✓	5.96	161.41
+ ✓	6.01	161.36
'A ✓	6.01	161.36
+1 N Pav	6.04	161.33
cb	5.5	161.9
+5	5.2	162.2
NL	5.1	162.3

16737

10

17+01⁹⁹ = ~~+~~ Linnet

NL	5.0	162.4
+5	5.0	162.4
cb	5.4	162.0
+6 N Pav	5.99	161.38
'A	5.98	161.39
+	5.96	161.41
'A	5.90	161.47
cb on Pav	5.77	161.60
SL ✓	5.43	161.94

17+16⁹⁹ = Fcb Linnet

^s NL top cb	5.27	162.10
^s NL gut	5.80	161.57
cb Pav	5.96	161.41
'A ✓	5.95	161.42
+ ✓	5.95	161.42
'A ✓	6.04	161.33
+1 ⁵ N Pav	6.05	161.32
cb	5.5	161.9
+2	5.4	162.0
+5	6.5	160.9
NL	6.4	161.0

167.37

17+21⁹⁹ = EL Linnet

5N	8.4	159.0
N.L.	8.5	158.9
+4	7.9	159.5
+8	5.7	161.7
cb	5.7	161.7
+6 N Pav	6.01	161.36
1/4	5.97	161.40
1/4 1/2 Pav	5.97	161.40
1/4	6.00	161.37
+5 S Pav	5.99	161.38
+6	5.8	161.6
cb	5.5	161.9
+4	5.3	162.1
+5	4.7	162.7
S.L.	5.0	162.4
17+30		
S.L.	3.7	163.5
cb	5.2	162.2
+6 S Pav	5.91	161.46
1/4	5.97	161.40
1/4 1/2 Pav	5.86	161.51
1/4	5.96	161.41
+15 N Pav	6.02	161.35
cb	5.8	161.6
N.L.	6.3	161.1
5N	7.7	

167.37

11

17+65

5N	6.5	160.9
N.L.	6.1	161.3
cb	5.8	161.6
+6 N Pav	5.89	161.48
1/4	5.88	161.49
1/4 1/2 Pav	5.87	161.50
1/4	5.87	161.50
+0 ⁶ S Pav	5.86	161.51
cb	5.5	161.9
+4	5.4	162.0
+6	5.5	161.9
+8	5.3	162.1
S.L.	3.6	163.8
18+00		
S.L.	6.2	161.2
+8	5.6	161.8
cb	5.7	161.7
+6 S Pav	5.71	161.66
1/4	5.70	161.67
1/4 1/2 Pav	5.71	161.66
1/4	5.82	161.55
+0 ⁸ N Pav	5.89	161.48
+5	6.2	161.2
cb	5.8	161.6
+2	5.9	161.5
+5	7.0	160.4

	167.37	
13+00		
NL	8.5	158.9
12'N	9.1	158.3
18+30		
12N	9.0	158.4
NL	9.0	158.4
+5	8.2	159.2
cb	5.7	161.7
+6 N Pav	5.79	161.58
1/4	5.73	161.64
± ± Pav	5.63	161.74
1/4	5.69	161.68
+1 ^S S Pav	5.80	161.57
cb	6.1	161.3
+3	6.3	161.1
S.L.	6.8	160.6
18+65		
10S	9.5	157.9
S.L.	9.4	158.0
+2	9.2	158.2
+8	6.2	161.2
cb	5.8	161.6
+5 ^S S Pav	5.82	161.55
1/4	5.75	161.62
+7 ± Pav	5.61	161.76
±	5.61	161.76
1/4	5.69	

	167.37	12
18+65		
+1 N Pav	5.74	161.63
cb	6.0	161.4
+5	8.1	159.3
+8	8.5	158.9
NL	8.5	158.9
3N	8.2	159.2
10N	8.4	159.0
14' conc culvert at 18+93 ^S		
Nend 6' s of N.L. 91' long		
FL Nend	11.70	165.67
FL Sand.	10.60	156.77
18+87		
10N	8.0	159.4
N.L.	8.1	159.3
+4	8.1	159.3
cb	6.1	161.3
+6 N Pav	5.65	161.72
1/4	5.61	161.76
± ± Pav	5.56	161.81
1/4	5.65	161.72
+1 ^S S Pav	5.75	161.62
cb	6.1	161.3
+5	9.0	158.4
S.L.	9.5	157.9
10S	9.5	157.9

167.37

18+93

105	9.6	157.8
S.L.	9.5	157.9
+3	9.7	157.7
+4	8.6	158.8
cb	6.0	161.4
+6 S Pav	5.74	161.63
1/4	5.69	161.68
1/4 & Pav	5.59	161.78
1/4	5.70	161.67
+1 N Pav	5.72	161.65
cb	6.1	161.3
+3	9.4	158.0
NL	10.5	156.9
10N	10.3	157.1
19+00		
10N	7.8	159.6
NL	7.6	159.8
+5	7.5	159.9
cb	5.8	161.6
+6 ³ N Pav	5.65	161.72
1/4	5.61	161.76
1/4 & Pav	5.61	161.76
1/4	5.64	167.73
+2 S Pav	5.71	161.76
+7	6.1	161.3
cb	5.8	161.6

167.37

13

19+00

cb +5	8.2	159.2
S.L.	9.0	158.4
10's	9.2	158.2
19+30		
105	8.6	158.8
S.L.	8.1	159.3
+5	7.6	159.8
cb	5.8	161.6
+1	6.1	161.3
+5 ³ S Pav	5.67	161.70
1/4	5.52	161.85
1/4 & Pav	5.49	161.88
1/4	5.58	161.79
+1 N Pav	5.61	161.76
cb	5.8	161.6
+3	7.3	160.1
NL	7.2	160.2
10N	7.2	160.2
19+65		
10N	8.9	158.5
NL	8.8	158.6
+5	8.4	159.0
cb	5.8	161.6
+6 ³ N Pav	5.55	161.82
1/4	5.50	161.87
1/4 & Pav	5.41	161.96

167.37

19+65		
1/4	5.46	161.91
+1 ⁸ S Pav	5.53	161.84
+7	5.0	162.4
cb	5.8	161.6
+4	7.8	159.6
S.L.	7.9	159.5
3s	8.5	158.3
10s	8.7	158.7
20+00		
10s	8.1	159.3
2s	7.9	159.5
S.L.	7.4	160.0
+7	7.2	160.2
cb	5.5	161.9
+1	5.9	161.5
+6 ³ S Pav	5.46	161.91
1/4	5.42	161.95
± ± Pav	5.32	162.05
1/4	5.36	162.01
+1 ⁶ N Pav	5.45	161.92
cb	5.5	161.9
+5	7.2	160.2
NL	7.2	160.2
10N	6.7	160.7

167.37

14

20+41²⁷ (A) = L on North

10N	7.3	160.1
8N	7.7	159.5
3N	7.9	159.5
NL	7.3	160.1
+8	5.5	161.9
cb	5.4	162.0
+4 N Pav	5.30	162.07
1/4	5.20	162.17
+5 ⁵ ± Pav	5.16	162.21
±	5.16	162.21
+6 ⁸ S Pav	5.25	162.12
1/4	5.3	162.1
+4	5.6	161.8
+5	5.2	162.2
cb	5.9	161.5
+2	5.7	161.7
S.L.	6.4	161.0
4s	6.6	160.8
10s	8.1	159.3

16737

20+41⁴² (B) = L on South

10 S	8.0	157.4
4 S	7.6	159.8
S.L.	6.5	160.9
+1	6.3	161.1
+9	6.4	161.0
cb	5.8	161.6
+3	5.2	162.2
+4	5.6	161.8
1/4	5.3	162.1
+0 ² S Pav	5.23	162.14
±	5.15	162.25
+2 ± Pav	5.15	162.22
1/4	5.19	162.18
+3 ² N Pav	5.30	162.07
cb	5.4	162.0
+3	5.5	161.9
N.L.	7.3	160.1
20+41 ⁴² (C)		
N.L.	7.3	160.1
+7	5.5	161.9
cb	5.3	162.1
+3 ² N Pav	5.31	162.06
1/4	5.20	162.17
+5 ⁵ ± Pav	5.16	162.21
±	5.15	162.22
+6 ² S Pav	5.25	162.12

20+41⁴² (C) 167.45

37

15

1/4	5.3	162.1
+3	5.6	161.8
+4	5.2	162.2
cb	5.9	161.5
+1	6.5	160.9
S.L.	6.3	161.1
4 S	7.7	159.7
10 S	8.0	159.4
T.P. 8.17	170.36 ^{.28}	5.26 ^{.11} 162.19
20+7.0		
10 S	10.4	159.9
S.L.	8.6	161.7
cb	8.2	162.1
+2	7.9	162.4
+6 ² S Pav	8.09	162.19
1/4	8.05	162.23
±	7.96	162.32
+0 ² ± Pav	7.97	162.31
1/4	8.01	162.27
+2 ² N Pav	8.07	162.21
cb	8.0	162.3
+3	8.1	162.2
N.L.	9.6	160.7
10 N	10.3	160.0

21+00

10N	8.9	161.4
NL	9.2	161.1
+3	9.1	161.2
cb	7.6	162.7
+6 ² N Pav	7.87	162.41
1A	7.85	162.43
1A 1A Pav	7.67	162.61
1A	7.80	162.48
+1 ² S Pav	7.89	162.39
+5	8.0	162.3
cb	7.7	162.6
+1	8.1	162.2
SL	8.5	161.8
2S	8.9	161.4
3S	9.5	160.8
10S	10.2	160.1
21+30		
10S	9.7	160.6
SL	8.0	162.3
cb	7.4	162.9
+1	7.8	162.5
+5 ⁵ S Pav	7.53	162.75
1A	7.43	162.85
6 ⁸ 1A Pav	7.35	162.93
1A	7.35	162.93

21+30

1A	7.45	163.83
+0.8 N Pav	7.48	162.80
cb	7.4	162.9
+2	7.4	162.9
+5	8.9	161.4
NL	8.7	161.6
10N	8.7	161.6
21+65		
10N	7.2	163.1
1N	7.2	163.1
NL	7.4	162.9
+2	8.0	162.3
cb	6.7	163.6
+3	7.3	163.0
+6 ² N Pav	7.03	163.25
1A	6.97	163.31
1A	6.88	163.40
+0 ⁸ 1A Pav	6.88	163.40
1A	6.99	163.29
+1 ² S Pav	7.08	163.20
+6	7.5	162.8
cb	7.2	163.1
SL	7.7	162.6
7S	7.7	162.4
10S	8.8	161.5

16

22+00

10S	8.6	161.7
2S	7.1	163.2
S.L.	7.1	163.2
+7	7.0	163.3
cb	6.7	163.6
+1	7.1	163.2
+5 ² S Pav	6.73	163.55
1/4	6.63	163.65
+7 $\frac{1}{2}$ Pav	6.55	163.73
$\frac{1}{2}$	6.55	163.73
1/4	6.66	163.68
+1	6.65	163.63
+4	6.8	163.5
cb	6.3	164.0
+5	6.4	163.9
N.L.	7.1	163.2
10N	7.6	162.7

22+30

10N	6.9	163.4
N.L.	7.0	163.3
cb	6.0	164.3
+6 ² N Pav	6.20	164.08
1/4	6.17	164.11
$\frac{1}{2}$	6.10	164.18
+0. ³ $\frac{1}{2}$ Pav	6.10	164.18

22+30

1/4	6.18	164.10
+12 S Pav	6.26	164.02
+6	6.7	163.6
cb	6.3	164.0
+5	6.7	163.6
S.L.	6.8	163.5
5S	6.7	163.6
7S	7.5	162.8
10S	7.5	162.8

22+65

10S	6.5	163.8
S.L.	6.4	163.9
+8	6.4	163.9
cb	5.6	164.7
+1	6.0	164.3
+5 ⁶ S Pav	5.83	164.45
1/4	5.80	164.48
+7 $\frac{1}{2}$ Pav	5.72	164.56
$\frac{1}{2}$	5.70	164.58
1/4	5.72	164.56
+1 ² N Pav	5.75	164.53
+4	5.9	164.4
cb	5.4	164.9
+4	5.7	164.6
N.L.	7.0	163.3
10N	7.0	163.3

17

Nov 22-28
Lowdon
15 Bell
Morgan.

		28 170.36 17.65	6.58	70 163.78	Hub Fl w. Holly wood. NL Imp.
B.M	12.95	17.65	6.58	163.78	
22 + 65	Probably 23 + 00				
10 N			13.2	163.5	
N.L.			13.3	163.4	
+2			13.3	163.4	
+6			12.0	164.7	
cb			11.6	165.1	
+4			12.2	164.5	
+6 ²	N Pav		12.03	164.62	
1/4			12.06	164.59	
1/4	± Pav		12.03	164.62	
1/4			12.14	164.51	
+2	S Pav		12.15	164.50	
+5 ²			12.4	164.3	
cb			12.0	164.7	
+4			12.7	164.0	
S.L.			12.7	164.0	
10 S			12.8	163.9	
Sec on EL W Holly wood = 23 + 12 ³⁵ on North.					
2L			11.6	165.1	
+6			11.8	164.9	
cb			11.3	165.4	
+1			11.6	165.1	
+5 ²	S Pav		11.12	165.53	
1/4			11.03	165.62	
+7	± Pav		10.90	165.75	

176.65

18

see on EL W Holly wood

±		10.88	165.77
1/4		10.89	165.76
+1	N Pav	10.88	165.77
+5		11.4	165.3
cb		11.0	165.7
+4		11.2	165.5
+7		12.2	164.5
N.L.		12.7	164.0
X sec Imperial from EL W Holly wood to NW 62 nd st. 60' at 10' cbs 90' Runway (See P 6)			
Sec on EL W Holly wood = 0 + 00 on North			
10 N		13.5	163.2
8 N		13.4	163.3
5 N		13.0	163.7
N.L.		12.9	163.8
+7		12.7	164.0
cb		12.4	164.3
+4		11.3	165.4
+7		10.9	165.8
1/4		11.4	165.3
+3 ³	N Pav	10.88	165.77
±		10.87	165.78
+2 ²	± Pav	10.90	165.75
1/4		11.04	165.61
+1 ²	S Pav	11.10	165.55

176.65-

Sec on E. & W Hollywood.

+6	11.6	165.1
+7	11.3	165.4
eb	11.6	165.1
SL	11.7	165.0
0+00 (Radial)		
SL	11.1	165.6
+2	11.6	165.1
+8	11.8	164.9
eb	11.3	165.4
+3	11.3	165.4
+4	11.5	165.2
+8 ^S S Pav	12.98	165.67
1/4	10.91	166.74
+7 ^S S Pav	10.81	165.84
+	10.79	165.86
+6 ^S N Pav	10.81	165.84
1/4	11.3	165.4
+2	11.0	165.7
+4	10.9	165.8
eb	12.3	164.4
+4	12.8	163.9
NL	12.8	163.9

176.65-

19

0+30

10 N	13.3	163.4
7 N	13.1	163.6
5 N	12.4	164.3
NL	12.3	164.4
+4	12.3	164.4
+9	12.7	166.0
eb	10.4	166.3
+5	10.4	166.3
+8	10.9	165.8
1/4	10.4	166.3
+2 N Pav	9.97	166.68
+	9.86	166.79
+1 S Pav	9.86	166.79
1/4 S Pav	10.07	166.58
+5	10.7	166.0
+6	10.3	166.4
eb	10.5	166.2
+1	11.0	165.7
+3	10.9	165.8
+4	10.6	166.1
+5	10.9	165.8
SL	8.0	168.7

	176.65	
0 + 60		
S.L.	6.2	170.5
+5	7.3	169.4
eb	10.0	166.7
+2	10.0	166.7
+6	9.3	167.4
+7	9.7	167.0
1/4	9.3	167.4
+2 S Pav	9.16	167.49
±	8.98	167.67
+1 ± Pav	8.98	167.67
1/4 N Pav	9.11	167.54
+5	9.7	167.0
+6	9.0	167.7
eb	9.4	167.3
+5	10.0	166.7
+8	11.4	165.3
N.L.	11.8	164.9
6N	12.0	164.7
12N	13.0	163.7
0 + 90		
10N	12.2	164.5
6N	11.2	165.5
N.L.	11.0	165.7
+2	10.6	166.1
+7	8.5	168.2
eb	8.1	168.6

	176.65	20
0 + 90		
+3	8.1	168.6
+3 ^S N Pav	9.0	167.7
+8 ^S N Pav	8.24	168.41
1/4	8.18	168.47
+7 ^S ± Pav	8.13	168.52
±	8.14	168.51
+6 ^S S Pav	8.30	168.35
1/4	8.7	168.0
+1	8.7	167.8
+2	8.4	168.3
+3	8.3	168.4
+5	8.9	168.8
eb	6.4	170.3
S.L.	4.0	172.7
1 + 20		
S.L.	0.8	175.9
eb	3.3	173.4
+3	4.0	172.7
+8	7.4	169.3
1/4	7.9	168.8
+5 S Pav	7.40	169.25
±	7.29	169.36
+4 ± Pav	7.25	169.40
1/4	7.30	169.35
+3 N Pav	7.35	169.30

	176.65	
1+20		
+8	8.1	168.6
+9	7.4	169.3
cb	7.2	169.5
+4	7.3	169.4
NL	9.2	167.5
7N	9.6	167.1
10N	10.8	165.9
1+50		
10N	8.2	168.5
6N	7.2	169.3
NL	6.9	169.8
+3	6.3	170.4
+7	6.4	170.3
+9	6.9	169.8
cb	6.9	169.8
+6 N Paw	6.49	170.16
1/4	6.41	170.24
+5 1/4 Paw	6.30	170.29
1/4	6.38	170.27
+4 B Paw	6.54	170.11
+8	7.2	169.5
1/4	6.6	170.1
+8	1.3	175.4
cb	1.0	175.7
S.L.	10.9	177.6

	176.65	21
1+80		
S.L.	+1.2	177.9
+9	0.2	176.5
cb	0.8	175.9
+5	4.0	172.7
1/4	5.5	171.2
+2	5.7	171.0
+3	6.4	170.3
+7 S Paw	5.68	170.97
1/4	5.62	171.03
+6 1/4 Paw	5.56	171.09
1/4	5.53	171.12
+5 N Paw	5.60	171.05
cb	5.6	171.1
+6	6.0	170.7
NL	6.1	170.6
8N	5.9	170.8
10N	6.0	170.7
2+10		
10N	4.8	171.9
NL	4.5	172.2
cb	4.9	171.8
+2	4.9	171.8
+4 ^L N Paw	4.74	171.91
1/4	4.62	172.03
+3 ^L 1/4 Paw	4.61	172.04

2+10

176.65

±	4.71	171.94
+2 ^L S Pav	4.80	171.85
+6	5.5	171.2
+9	4.2	172.5
1/4	3.9	172.8
+6	0.3	176.4
cb	+0.2	176.9
S.L.	+1.6	178.3

2+40

S.L.	+1.6	178.3
cb	+0.6	177.3
+5	0.0	176.7
1/4	3.4	173.3
+4	4.6	172.1
8 ^S S Pav	3.95	172.76
±	3.90	172.75
+7 ^S ± Pav	3.78	172.87
1/4	3.76	172.89
+6 ^S N Pav	3.85	172.80
cb	4.2	172.5
+1	4.2	172.5
+5	3.8	172.9
N.L.	3.8	172.9
5N	3.9	172.8

2+70

176.65

5N	3.0	173.7
N.L.	3.1	173.6
+7	2.8	173.9
cb	2.9	173.8
+1	3.1	173.6
+2 ^S N Pav	2.98	173.67
1/4	2.90	173.75
+1 ^S ± Pav	2.91	173.74
±	3.04	173.61
+0 ^S S Pav	3.06	173.59
+5	3.8	172.9
+7	3.1	173.6
+8	3.3	173.4
1/4	2.5	174.2
+3	0.0	176.7
cb	+0.2	176.9
S.L.	+1.0	177.7
3+00		
S.L.	+2.0	178.7
cb	+0.3	177.0
+7	0.4	176.3
1/4	2.1	174.6
+3	2.4	174.3
+5	3.0	173.7
+9 ^S S Pav	2.16	174.49
±	2.15	174.50

3+00			
¢ + 8 ⁸	¢ Pav	2.08	174.62
1/4		2.02	174.63
+7 ⁸	N Pav	2.15	174.50
cb		2.4	174.3
+2		2.4	174.3
+4		1.8	174.9
NL		1.9	174.8
7N		2.5	174.2
3+30			
7N		1.5	175.2
NL		1.6	175.1
+3		1.5	175.2
+6		1.1	175.6
+8		2.2	174.5
cb		1.9	174.8
+2	N Pav	1.45	174.20
1/4		1.32	175.33
+1	¢ Pav	1.33	175.32
¢	S Pav	1.52	175.13
+5		2.3	176.4
+9		1.5	175.2
1/4		1.1	175.6
+2		11.5	178.2
cb		+2.1	178.8
S.L		+2.8	179.5
T.P.	8.10	0.77	175.76

.65
176.73

3.98
184.06

3+60			
S.L		5.3	178.7
cb		6.1	177.9
+9		6.6	177.4
1/4		7.3	176.7
+5		8.1	175.9
¢	S Pav	8.20	175.78
+9	¢ Pav	8.12	175.86
1/4		8.11	175.87
+8	N Pav	8.23	175.75
cb		8.7	175.3
+2		9.1	174.9
+4		7.8	176.2
+7		8.4	175.6
NL		8.4	175.6
3+96 ³⁰	= E.C.		
NL		7.8	176.2
+6		7.3	176.7
+8		8.5	175.5
cb		8.2	175.8
+2	N Pav	7.87	176.11
1/4		7.73	176.25
+1	¢ Pav	7.75	176.23
¢	S Pav	7.90	176.08
+5		8.7	175.3
+9		7.8	176.2
1/4		6.2	177.8

183.98
184.06

23

3+96³⁰

183.98

eb	5.6	178.4
S.L.	4.8	179.2
4+30		
S.L.	4.1	179.9
cb	4.8	179.2
+9	5.5	178.5
1/4	6.4 ^h	177.6
+5	8.3	175.7
+7.8 S Pav	7.64	176.34
+	7.62	176.36
+8.8 + Pav	7.42	176.56
1/4	7.44	176.54
+7.6 N Pav	7.58	176.40
cb	7.8	176.2
+2	8.0	176.0
+3	7.1	176.9
+5	16.9	177.1
N.L.	7.0	177.0
4+65		
N.L.	6.4	177.6
+3	6.6	177.4
+7	6.4	177.6
+8	7.5	176.5
eb	7.4	176.6
23 N Pav	7.23	176.75

4+65

24

1/4	7.14	176.84
+1 ³ + Pav	7.13	176.85
+	7.27	176.71
+0 ³ S Pav	7.28	176.70
+5	7.90	176.08
+7	7.0	177.0
+9	6.7	177.3
1/4	6.1	177.9
+2 ⁵	4.6	179.4
cb	3.8	180.2
S.L.	3.3	180.7
5+00		
S.L.	3.0	181.0
cb	3.2	180.8
+8	3.3	180.7
1/4	4.8	179.2
+4	6.8	177.2
+5	7.5	176.5
+9 ² S Pav	6.94	177.04
+	6.94	177.04
+8 ^h + Pav	6.71	177.27
1/4	6.70	177.28
+7.5 N Pav	6.92	177.06
cb	7.0	177.0
+1	7.1	176.9

5+00

+4

6.1 177.9

NL

5.9 178.1

5+30

NL

5.2 178.8

+7

5.9 178.1

+9

6.8 177.2

cb

6.8 177.2

+2² N Pav

6.61 177.37

1/4

6.43 177.55

+12 1/2 Pav

6.43 177.55

1/2

6.60 177.38

+0² S Pav

6.61 177.37

+5

7.1 176.9

+6

6.3 177.7

+9

5.6 178.4

1/4

4.7 178.3

+2

3.2 180.8

cb

2.7 181.3

S.L.

2.1 181.9

5+65

S.L.

2.1 181.9

cb

2.4 181.6

+7

2.8 181.2

1/4

4.4 179.6

+5

6.6 177.4

+9 S Pav

6.25 177.73

1/2

6.23 177.75

+8 1/2 Pav

6.11 177.87

1/4

6.12 177.86

+7 N Pav

6.46 177.72

cb

6.4 177.6

+1

6.5 177.5

+3

5.6 178.4

NL

5.2 178.8

6+00

NL

4.8 179.2

+6

5.4 178.6

+9

6.1 177.9

cb

6.1 177.9

+3 N Pav

5.96 178.02

1/4

5.77 178.21

+2 1/2 Pav

5.77 178.21

1/2

5.89 178.09

+1 S Pav

5.93 178.05

+5

6.3 177.7

+6

5.4 178.6

25

Imperial

183.98

6+00

1/4	4.0	180.0
+3	2.1	181.9
cb	1.6	182.4
SL	1.4	182.6
6+30		
SL	.09	183.1
cb	1.2	182.8
+7	1.8	182.2
1/4	3.8	180.2
+4	5.3	178.7
+4 ^S	5.8	178.2
+9 S Pad	5.66	178.32
±	5.63	178.35
+8 ± Pad	5.48	178.50
1/4	5.50	178.48
+7 N Pad	5.68	178.30
cb	5.7	178.3
+1 ^S	5.7	178.3
+3 ^S	5.1	178.9
N.L.	5.2	178.8

183.98

26

6+65

7N	5.5	178.5
N.L.	5.2	178.8
+4	4.9	179.1
+8	5.1	178.9
+9	5.3	178.7
cb	5.4	178.6
+3 ^S N Pad	5.32	178.66
1/4	5.19	178.78
+2 ^S ± Pad	5.19	178.78
±	5.30	178.68
+1 ^S S Pad	5.28	178.70
+6	5.7	178.3
+7	4.9	179.1
+9	4.6	179.4
1/4	3.4	180.6
+4	1.5	182.5
cb	0.7	183.3
SL	+0.5	184.5
7+00	+0.8	
SL	+0.8	184.8
cb	0.4	183.6
+7	2.1	181.9
1/4	3.9	180.1
+3	5.1	178.9
+4	5.4	178.6

	183.98	
7+00		
1/4 + 8 ³ S Pav	4.87	179.11
¢	4.91	179.07
+ 7 ³ ¢ Pav	4.86	179.12
1/4	4.86	179.12
+ 6 ³ N Pav	4.99	178.99
¢	5.1	178.9
+ 1	5.0	179.0
+ 2	4.7	179.3
NL	5.8	178.2
7N	6.7	177.3
7+30		
10N	7.2	176.8
NL	6.3	177.7
+ 8	4.5	179.5
+ 9	4.4	179.6
¢	4.9	179.1
+ 3 ⁶ N Pav	4.67	179.31
1/4	4.54	179.44
+ 2 ⁶ ¢ Pav	4.54	179.44
¢	4.69	179.29
+ 1 ⁶ S Pav	4.68	179.30
+ 4	5.0	179.0
+ 4 ⁵	4.6	179.4
+ 8	4.6	179.4
+ 9	5.2	178.8
1/4	4.5	179.5

	183.98		27
7+30			
+ 5	3.7	180.1	
¢	2.0	182.0	
+ 5	1.0	183.0	
SL	0.5	183.5	
7+65			
SL	1.4	182.8	
+ 5	1.9	182.1	
¢	3.8	180.2	
+ 4	4.0	180.0	
+ 7	4.6	179.4	
+ 8	4.6	179.4	
+ 9	5.2	178.8	
1/4	4.7	179.3	
+ 3	4.4	179.8	
+ 8 ⁵	4.5	179.5	
+ 8 ¹ S Pav	4.35	179.63	
¢	4.32	179.66	
+ 7 ¹ ¢ Pav	4.16	179.82	
1/4	4.16	179.82	
+ 6 ¹ N Pav	4.32	179.66	
¢	4.5	179.5	
+ 7	4.4	179.6	
+ 6	6.0	178.0	
NL	6.5	177.5	
7N	7.3	177.7	

8+00

183.98

10N	8.2	175.8
NL	6.1	177.9
+4	5.3	178.7
+7	4.8	179.2
+9	4.0	180.0
cb	4.3	179.7
+4 N Pav	4.03	179.95
1/4	3.83	180.15
+3 & Pav	3.85	180.13
&	4.01	179.97
+2 s Pav	4.02	179.96
+7	4.3	179.7
+8	4.1	179.9
1/4	4.8	179.2
+2	5.2	178.8
+5	5.3	178.7
cb	4.7	179.3
+4	3.9	180.1
SL	1.7	182.3
8+30		
SL	1.6	182.4
+8	4.3	179.7
cb	4.6	179.4
+5	4.9	179.1
1/4	4.6	179.4
+2	3.9	180.1

8+30

183.98

+3	4.2	179.8
+7 ⁵ s Pav	3.81	180.17
&	3.76	180.22
+6 ⁵ & Pav	3.58	180.40
1/4	3.59	180.39
+5 ⁵ N Pav	3.74	180.24
cb	4.20	179.78
+1	3.9	180.1
+3	4.6	179.4
+8	5.1	178.9
NL	5.4	178.6
6N	7.9	176.1
10N	7.8	176.2
8+65		
10N	7.2	176.8
NL	5.8	178.2
+9	3.4	180.6
cb	3.6	180.4
+4 ³ N Pav	3.36	180.62
1/4	3.28	180.60
+3 ² & Pav	3.27	180.71
&	3.41	180.57
+2 ³ s Pav	3.44	180.54
+7	3.9	180.1
+9	3.9	180.1
1/4	4.4	179.6

28

8+65

183.98
184.06

4+3	5.1	178.9
+6	5.2	178.8
cb	5.1	178.9
S.L.	2.5	181.5
8+88 = 24" conc pipe Culvert		
S.L.	4.1	179.9
+7	5.9	178.1
cb	6.1	177.9
+2	6.0	178.0
+6 send culvert. FL	7.09	176.89
1A	3.8	180.2
+1	3.4	180.6
+6 ⁶ SPav	3.08	180.90
+	3.06	180.92
+5 ⁶ + Pav	3.01	180.97
1A	3.03	180.95
+4 ⁶ N Pav	3.09	180.89
+9	3.5	180.5
cb	3.1	180.9
+6	3.4	180.6
N.L.	6.6	177.4
0 ⁵ N Road culvert FL	7.96	176.02
10N	7.1	176.9
T.P. 6.03	187.38	2.71 181.35

9+30

187.30
187.38

29

10N	9.4	177.9
6N	9.7	177.6
3N	9.3	178.0
N.L.	8.2	179.1
+6	8.0	179.3
+9	6.4	180.9
cb	6.3	181.0
+4 ⁵ N Pav	6.04	181.26
1A	5.96	181.34
+3 ⁵ + Pav	5.90	181.40
+	6.02	181.28
+2 ⁵ SPav	6.04	181.26
+8	6.5	180.8
1A	7.2	180.1
+4	8.3	179.0
cb	8.4	178.9
+4	8.7	178.6
S.L.	7.9	179.4
9+65		
S.L.	7.2	180.1
cb	7.9	179.4
+8	7.2	179.1
1A	6.1	181.2
+1	6.0	181.3
+7 SPav	5.75	181.55
+	5.66	181.70

9+65

187.30

+6	± Pav	5.55	181.75
1/4		5.59	181.71
+5	N Pav	5.62	181.68
+9		6.0	181.3
eb		5.8	181.5
+1		5.8	181.5
+5		8.1	179.2
NL		9.2	178.1
10N		9.1	178.2
10+00			
10N		9.6	177.7
NL		8.1	179.2
+5		7.5	179.8
eb		5.7	181.6
+5	N Pav	5.35	181.95
1/4		5.28	182.02
+4	± Pav	5.28	182.02
±		5.30	182.00
+3	S Pav	5.39	181.91
+9		5.7	181.6
1/4		5.9	181.4
+3		6.6	180.7
eb		7.4	179.9
S.L		7.7	179.6

10+30

187.30

30

S.L.		7.4	179.9
eb		7.1	180.2
+5		7.4	179.9
+7		7.0	179.3
1/4		5.7	181.6
+5		5.1	182.2
+3		5.4	181.9
+7	S Pav	5.12	182.18
±		5.02	182.28
+6	± Pav	4.98	182.32
1/4		4.98	182.32
+5	N Pav	5.04	182.26
+9		5.5	181.8
eb		5.3	182.0
+1		5.2	182.1
+7		8.3	179.0
NL		8.4	178.9
6N		8.9	178.4
14N		10.6	176.7
10+65			
10N		8.7	178.6
8N		8.3	179.0
NL		8.6	178.7
+3		8.1	179.2
+9		5.2	182.1
eb		5.0	182.3

	187.30	
10 + 65		
cb + 5 N Pav	4.80	182.50
1/4	4.65	182.65
+ 4c 1/2 Pav	4.67	182.63
1/4	4.70	182.60
+ 3 S Pav	4.82	182.48
+ 7	5.1	182.2
+ 9	5.0	182.3
1/4	5.6	182.7
+ 6	6.7	180.6
cb	6.6	180.7
S.L.	6.7	180.6
10 S	6.7	180.6
11 + 00		
10 S	3.3	184.0
S.L.	6.2	181.1
cb	6.1	181.2
+ 4	6.1	181.2
1/4	4.7	182.6
+ 2	4.7	182.6
+ 6 ² S Pav	4.44	182.86
1/4	4.33	182.97
+ 5 ² 1/2 Pav	4.28	183.02
1/4	4.31	182.99
+ 4 ² N Pav	4.44	182.86

	187.30	31
11 + 00		
+ 8	4.9	182.4
cb	4.7	182.6
+ 6	7.2	180.1
N.L.	7.2	180.1
10 N	7.9	179.4
11 + 30		
10 N	8.0	179.3
N.L.	7.0	180.3
+ 3	6.9	180.4
+ 8	4.6	182.7
cb	4.2	182.1
+ 2	4.4	182.9
+ 5 ² N Pav	4.15	183.15
1/4	4.06	183.24
+ 4 ² 1/2 Pav	4.03	183.27
1/4	4.08	183.22
+ 3 ² S Pav	4.15	183.15
+ 8	4.3	183.0
1/4	4.4	183.1
+ 3	4.5	182.8
+ 6	5.5	181.8
cb	5.4	181.9
S.L.	5.5	181.8
S.S.	3.5	183.8

	187.30	
11 + 65		
10 S	3.3	184.0
6 S	4.7	182.6
3 L	4.5	182.8
cb	4.7	182.6
+6	4.3	183.0
1/4	3.4	183.9
+1	3.8	183.5
+6 S Pav	3.73	183.57
+	3.64	183.66
+5 + Pav	3.61	183.69
1/4	3.64	183.66
+4 N Pav	3.75	183.55
+8	3.8	183.5
+9	3.5	183.8
cb	3.6	183.7
+5	6.0	181.3
N.L.	6.5	180.8
10 N	7.1	180.2
12 + 00		
10 N	6.1	181.2
2 N	4.3	183.0
N.L.	4.5	182.8
+5	4.7	182.6
+9	2.9	184.4
cb	3.1	184.2
+1	3.2	184.1

	187.30	
12 + 00		
cb + 5 ⁸ N Pav	3.12	184.18
1/4	3.01	184.29
+4 ⁸ + Pav	3.00	184.30
+	3.02	184.28
+3 ⁸ S Pav	3.11	184.19
+8	3.1	184.2
+9	2.6	184.7
1/4	3.1	184.2
cb	3.7	183.6
S.L.	3.9	183.4
3's	4.1	183.2
9s	0.6	186.7
12 + 30		
S.L.	2.5	184.8
cb	2.5	184.8
1/4	2.3	185.0
+1	2.7	184.6
+5 ⁸ S Pav	2.38	184.92
+	2.25	185.05
+4 ⁸ + Pav	2.20	185.10
1/4	2.23	185.07
+3 ⁸ N Pav	2.31	184.99
+8	2.4	184.9
+9	2.0	185.3
cb	2.2	185.1

12+30	187.30	
+6	2.4	184.9
N.L.	3.5	183.8
10N	6.2	181.1
12+65		
10N	5.3	182.0
5N	4.8	182.5
N.L.	2.2	185.1
+7	1.2	186.1
cb	1.1	186.2
+2	1.7	185.6
+6 ⁵ N Pav	1.12	186.18
1/4	1.15	186.15
+5 ⁵ S Pav	1.16	186.14
4	1.12	186.18
+4 ⁵ S Pav	1.17	186.13
+9	1.7	185.6
1/4	1.5	185.8
cb	1.6	185.7
+9	2.2	185.1
S.L.	1.7	185.6

13+00	187.38	30	33
5L		+3.6	190.9
+6		0.3	187.0
cb		0.5	186.8
+4		0.4	186.9
+7		0.0	187.3
+8		0.4	186.9
1/4		0.2	187.1
+1		0.6	186.7
+5 ⁵ S Pav		0.10	187.20
T.P. 11.53	.49	0.34	187.04
4	198.57	11.17	187.32
+4 ³ S Pav		11.09	187.40
1/4		11.10	187.39
+3 ³ N Pav		11.11	187.38
+8		11.8	186.7
cb		11.2	187.3
4L		11.0	187.5
N.L.		12.0	186.5
10N		16.3	182.2
15N		16.4	182.1

13+30

198.49

~~188.57~~

13N	15.0	183.5
8N	14.9	183.6
N.L.	10.8	187.7
+4	9.7	188.8
Cb	10.1	188.4
+2 ⁵	10.7	187.8
+6 ⁸ N Pav	10.04	188.45
1/4	9.84	188.65
+5 ⁸	9.95	188.54
+	10.03	188.46
+4 ⁸ S Pav	10.20	188.29
1/4	10.3	188.2
+3	9.6	188.9
+5	9.4	189.1
+6	10.8	187.7
+7	10.8	187.7
+8	9.7	188.8
+9	9.4	189.1
Cb	8.3	190.2
SL	3.5	195.0

13+65

198.49

34

SL	+1.0	199.5
Cb	4.8	193.7
+4	8.3	190.2
+5	8.3	190.2
+6	9.2	189.3
+7	9.2	189.3
+7	8.7	189.8
1/4	9.0	189.5
+5 S Pav	8.47	190.02
+	8.53	189.96
+4 $\frac{1}{2}$ Pav	8.51	189.98
1/4	8.56	189.93
+3 N Pav	8.66	189.83
+7	9.5	189.0
+9	8.7	189.8
Cb	8.8	189.7
+4	8.7	189.8
+6	8.3	190.2
N.L.	8.9	189.6
9N	13.5	185.0
15N	13.4	185.1

198.49

14+00

15N	11.3	187.2
8N	12.7	187.8
3N	7.4	191.1
NL	7.0	191.5
+3	7.0	191.5
+5	7.5	191.0
cb	7.6	190.9
+2	7.6	190.9
+2 ^E	7.9	190.6
+7 N Pad	7.16	191.33
'4	7.00	191.49
+6 & Pad	6.87	191.52
'4	6.90	191.59
+5 S Pad	7.09	191.40
+9	7.6	190.9
'4	7.3	191.2
+2	8.1	190.4
+3 ^E	7.7	190.8
+4	6.2	192.3
cb	2.0	196.5
S.L.	+5.1	203.6

198.49

14+30

S.L.	+7.6	206.1
cb	+0.4	198.9
+7	4.0	194.5
+8	5.7	192.8
'4	6.4	192.1
+4 ^S S Pad	5.79	192.76
cb	5.55	192.94
+3 ^S & Pad	5.52	192.97
'4	5.60	192.89
+6 ^E N Pad	5.72	192.77
+8	6.4	192.1
cb	6.0	192.5
+1	5.9	192.6
+3	6.2	192.3
+5	6.2	192.3
+7	5.5	193.0
NL	5.8	192.7
1N	5.8	192.7
7N	8.8	189.7
10N	8.4	198.1

35

.49
198.57

14460⁸¹ = w.l. 62nd on North

10N	7.3	191.2
7N	6.9	191.6
N.L.	3.7	194.8
H	3.7	194.8
+3	4.4	194.1
cb	4.7	193.8
+7 ² N Pav	4.39	194.10
1/4	4.28	194.21
+6 ² E Pav	4.14	194.35
E	4.15	194.34
+5 ² S Pav	4.20	194.29
1/4	4.9	193.6
+2	2.3	196.2
+6	0.3	198.2
cb	+5.5	204.0
+7	+10.5	209.0
S.L.	+11.5	210.0
Nails PN#70157 NW Imp 2		195.89
B.M.	2.60	195.99
T.P.	1.13	186.83 ⁷⁵ 12.87 185.90 ⁶²
T.P.	1.32	180.87 ⁷⁹ 7.28 179.55 ⁴⁷
T.P.	0.12	168.66 ⁵⁸ 12.33 168.54 ⁴⁴
B.M.	4.27	164.31 ³¹ 164.35
	1.54	165.87 ⁸⁵ 164.35 ⁸¹
B.M.	4.10	161.79 ⁷⁵
Set Nail in lead plug in cb		161.71 Correct El.
NE Imperial and Merlin Dr.		

X sec Imperial from EL Euclid
100' st 20' cbs 60' Roadway.

Correct from Book
1295 Page 3A
36

HI
181.93

181.68
181.76

Nails Pole
SW Imp
2 Euclid

0-99⁴³ - E Euclid on South

B.M.	0.25	182.01	181.76
S.L. on Pav		1.24	180.69
cb	✓	2.24	179.69
1/4 Pav dug out			
+6	✓	3.04	178.89
E	✓	2.98	178.95
1/4	✓	3.06	178.87
cb	✓	3.36	178.57
+3 N Pav		3.50	178.43
+10		4.1	177.8
N.L. Prod.		6.3	175.6
0-46 ²⁷ EL Euclid on South			
10N		8.3	177.6
N.L.		7.2	174.7
+10		6.4	175.5
cb		5.6	176.3
+5		5.2	176.7
+10		5.2	176.7
1/4		5.1	176.8
+6 N Pav		4.92	177.01
E E Pav		4.87	177.06
1/4 on Pav		4.95	176.98
cb S Pav		4.73	177.20
+7		3.7	178.2

Nov 23-28
Loudon
Lobell
Morgan

Las Alturas N^o 4
Map N^o 2052



37

181.93

0-46²²

eb +10	3.6	178.3
S.L.	3.2	178.7
top Ecb Euclid on south.	3.36	178.57
0 + 00 = BC. NE Ret Euclid on North.		
S.L.	5.0	176.9
+10	5.3	176.6
eb	5.3	176.6
+4	5.4	176.5
+10	6.0	175.9
1/4	6.5	175.4
+5	6.7	175.2
+6 S Pav	6.70	175.23
⊕ ⊕ Pav	6.63	175.30
+9 N Pav	6.71	175.22
+10	6.8	175.1
1/4	6.7	175.2
+5	7.2	174.7
eb	7.3	174.6
+10	7.9	174.0
N.L.	8.1	173.8
10N	9.4	172.5
Ⓐ see P 37 EC. Ret.	10.4	171.5

181.93

38

0+30

10N	10.2	171.7
N.L.	10.0	171.9
+10	9.3	172.6
eb	8.5	173.4
+10	7.9	174.0
1/4	7.9	174.0
+3	8.0	173.9
+5	8.0	173.9
+6 N Pav	7.84	174.09
⊕ c Pav	7.77	174.16
+9 S Pav	7.79	174.14
+10	7.8	174.1
+12	8.0	173.9
1/4	7.5	174.4
+5	7.4	174.5
eb	7.1	174.8
+10	6.6	175.3
S.L.	6.3	175.6
0+60		
S.L.	8.6	173.3
+5	8.1	173.8
+10	8.5	173.4
eb	8.9	173.0
+10	8.9	173.0
+13	9.2	172.7
1/4	8.7	173.2

0 + 60

181.93

+5		8.9	173.0
+6	S Pav	8.88	173.05
±	c Pav	8.82	173.11
+9	N Pav	8.90	173.03
+10		9.0	172.9
+13		9.2	172.7
'4		9.2	172.7
+5		9.1	172.8
+10		9.5	172.4
cb		9.5	172.4
+10		10.0	171.9
NL		10.8	171.1
10N		11.4	170.5
1 + 02 ⁵⁵	= W.L. Alley		
10N		11.8	170.1
N.L.		11.0	170.9
+10		10.8	171.1
cb		10.5	171.4
+10		10.6	171.3
'4		10.6	171.3
+5		10.5	171.4
+6	N Pav	10.41	171.52
±	c Pav	10.31	171.62
+9	S Pav	10.39	171.54
+10		10.3	171.6

181.93

39

1 + 02⁵⁵

1/4		10.0	171.9
+2		10.5	171.4
+5		10.5	171.4
cb		10.5	171.4
+10		10.4	171.5
SL		10.0	171.9
1 + 25 ^{LS}	= E.L. Alley		
SL		10.5	171.4
+10		10.8	171.1
cb		10.7	171.2
+10		10.9	171.0
+13		11.0	170.9
'4		10.5	171.4
+5		11.1	170.8
+6	S Pav	11.14	170.79
±		11.10	170.83
+9	N Pav	11.19	170.74
+10		11.3	170.6
'4		11.4	170.5
+5		11.3	170.6
cb		11.2	170.7
+10		11.4	170.5
NL		11.5	170.4
10N		12.3	169.6

	181.93		
1750	182.01		
10N		14.1	167.8
NL		13.0	168.9
+10		12.6	169.3
cb		12.3	169.6
+10		12.2	169.7
1/4		12.3	169.6
+5		12.1	169.8
+6 N.Pav		11.98	169.95
+		11.89	170.04
+9 S.Pav		11.95	169.98
+10		11.8	170.1
1/4		11.6	170.3
+2		12.0	169.9
+5		11.8	170.1
cb		11.1	170.8
+10		11.0	170.9
+15		11.1	170.8
SL		11.3	170.6
T.P. 0.73	170.09 170.12	12.62	169.39

	170.04		
1780	170.12		
SL		0.0	170.0
+10		+0.1	170.1
cb		1.0	169.0
+10		1.0	169.0
+13		1.1	168.9
1/4		0.4	169.6
+5		1.0	169.0
+6 S.Pav		0.97	169.07
+		0.88	169.16
+9 N.Pav		0.93	169.11
+10		1.1	168.9
1/4		1.3	168.7
+1		0.9	169.1
+5		0.9	169.1
cb		1.5	168.5
+10		2.3	167.7
NL		3.0	167.0
10N		3.7	166.3

170.04

2+10

10N	5.0	165.0
NL	4.1	165.9
+7	3.0	167.0
+10	3.0	167.0
cb	2.6	167.4
+10	2.0	168.0
+14	1.8	168.2
14	2.0	168.0
+2	2.1	167.9
+5	2.0	168.0
+6 N Pav	1.95	168.09
4	1.89	168.15
+9 S Pav	1.96	168.08
+10	2.0	168.0
+11	1.6	168.4
14	1.5	168.5
+2	1.9	168.1
+5	1.8	168.2
+10	1.5	168.5
cb	1.8	168.2
+5	1.7	168.3
+10	1.2	168.8
S.L	1.2	168.8

170.04

2+40

S.L. 5.01	2.5	167.5
+10 5.01	2.5	167.5
cb 5.01	2.6	167.4
+10 5.01	2.6	167.4
+13 5.01	2.7	167.3
14 5.01	2.1	167.9
+5 5.01	2.6	167.4
+6 S Pav	2.86	167.18
4 5.01	2.77	167.27
+9 N Pav	2.83	167.21
+10 5.01	2.9	167.1
14 5.01	3.2	166.8
+5 5.01	3.3	166.7
cb 5.01	4.0	166.0
+10 5.01	4.5	165.5
N.L. 5.01	5.3	164.7
10N 5.01	6.0	164.0
5.01		
5.01		

41

170.04

2+70

10N.	6.7	163.3
N.L.	6.2	163.8
+10	5.6	164.4
+14	5.3	164.7
cb	5.1	164.9
+6	4.7	165.3
+10	4.4	165.6
1/4	4.1	165.9
+5	3.9	166.1
+6 N Pav	3.83	166.21
+	3.71	166.33
+9 S Pav	3.82	166.22
+10	3.8	166.24
1/4	3.4	166.6
+1	3.7	166.3
+5	3.8	166.2
cb	4.0	166.0
+10	3.8	166.2
S.L.	3.3	166.7

170.04

42

3+00

S.L.	3.6	166.4
+10	4.1	165.9
+12	4.0	166.0
cb	4.2	165.8
+10	4.7	165.3
+14	4.7	165.3
1/4	4.3	165.7
+5	4.8	165.2
+6 S Pav	4.77	165.27
+	4.69	165.35
+9 N Pav	4.80	165.24
+10	4.9	165.14
+13	4.9	165.1
1/4	4.6	165.4
+5	4.7	165.3
cb	5.3	164.7
+10	5.7	164.3
N.L.	6.2	163.8
10N	6.6	163.4

170.09

3+30

10N	6.3	163.7
N.L.	5.9	164.1
+10	5.8	164.2
+15	5.3	164.7
Pb	5.5	164.5
+7	5.6	164.4
+10	5.4	164.6
+12	5.2	164.8
1/4	5.5	164.5
+2	5.7	164.3
+5	5.7	164.3
+6 N Pav	5.73	164.31
±	5.64	164.44
+9 S Pav	5.70	164.34
+10	5.8	164.2
1/4	5.5	164.5
+1	5.9	164.1
+5	5.2	164.8
+7	5.0	165.0
+11	2.7	167.3
eb	2.8	167.2
+10	3.1	166.9
S.L.	2.8	167.2

170.04

+70.14

3+60

SL	2.0	168.0
+10	1.9	168.1
eb	1.8	168.2
+4	1.9	168.1
+10	6.5	163.5
+14	6.8	163.2
1/4	6.4	163.6
+5	6.7	163.3
+6 S Pav	6.64	163.40
±	6.54	163.50
+9 N Pav	6.64	163.40
+10	6.7	163.3
1/4	6.5	163.5
+5	6.3	163.7
+12	6.0	164.0
eb	6.1	163.9
+10	6.1	163.9
N.L.	6.3	163.7
10N	6.7	163.3
T.P. 0.40	⁵⁶ 163.64	6.88 163.24

43

3+90
 10N
 NL
 +10
 cb
 +5
 1/4
 +3
 +5
 +1 N Pav
 E
 +9
 +10
 1/4
 +2
 +3
 +5
 cb
 +6
 +10
 SL

163.56
~~163.64~~
 1.2
 0.8
 0.6
 0.7
 0.6
 0.8
 1.1
 1.1
 1.09
 0.98
 1.06
 1.1
 1.1
 1.5
 1.1
 0.9
 +0.5
 +1.8
 +2.2
 +2.2

162.4
 162.8
 163.0
 162.9
 163.0
 162.8
 162.5
 162.5
 162.47
 162.58
 162.50
 162.5
 162.5
 162.1
 162.5
 162.7
 164.1
 165.4
 165.8
 165.8

4+20
 SL
 +10
 cb
 +4
 +10
 +13
 1/4
 +5
 +6 S Pav
 E
 +9 N Pav
 +10
 +12
 1/4
 +1
 +5
 cb
 +5
 +10
 +13
 NL
 10N

163.56
 0.4
 0.2
 0.3
 0.6
 2.0
 2.4
 1.8
 2.0
 1.96
 1.86
 1.96
 2.1
 2.4
 1.9
 1.7
 1.7
 1.7
 1.7
 1.7
 1.8
 1.9
 2.4
 2.5

163.2
 163.4
 163.3
 163.0
 161.6
 161.2
 161.8
 161.4
 161.60
 161.70
 161.60
 161.5
 161.2
 161.7
 161.9
 161.9
 161.7
 161.9
 161.8
 161.7
 161.2
 161.1

163.56		
A+50		
10N	3.7	159.9
NL	3.3	160.3
+10	3.3	160.3
cb	3.1	160.5
+6	2.7	160.9
+10	2.7	160.9
1/4	2.9	160.7
+2	3.1	160.5
+5	2.9	160.7
+6 N Pad	2.86	160.70
±	2.81	160.75
+9 S Pad	2.90	160.66
+10	2.7	160.9
+12	2.5	161.1
1/4	2.4	161.2
+2	2.9	160.7
+5	2.9	160.7
+8	3.0	160.6
+13	1.7	161.7
cb	2.2	161.4
+10	2.5	161.1
+18	2.3	161.3
S.L.	2.6	161.0

163.56			45
A+80			
S.L.		4.1	159.5
+10		4.0	159.6
cb		3.7	159.9
+10		3.6	160.0
+13		3.8	159.8
+14		3.5	160.1
1/4		3.5	160.1
+3		3.3	160.3
+5		3.8	159.8
+6 S Pad		3.85	159.71
±		3.73	159.83
+9 N Pad		3.86	159.70
+10		4.0	159.6
+12		4.2	159.4
+14		3.9	159.7
1/4		4.1	159.5
+5		4.3	159.3
cb		4.3	159.3
+10		4.5	159.1
N.L.		4.6	159.0
10N		5.0	158.6

163.56

5+10

10N	8.0	155.6
NL	7.4	156.2
+10	7.4	156.2
cb	6.8	156.8
+10	6.8	156.8
+12	6.8	156.8
1/4	5.3	158.3
+1	4.9	158.7
+3	5.1	158.5
+5	4.9	158.7
+6 N Pav	4.78	158.78
±	4.67	158.89
+9 S Pav	4.79	158.77
+10	4.8	158.8
+12	4.6	159.0
1/4	4.4	159.2
+1	4.7	158.9
+5	4.7	158.9
+12	5.0	158.6
cb	4.6	159.0
+7	4.6	159.0
+10	4.8	158.8
+14	4.6	159.0
SL	4.9	158.7

163.56

5+21

10S	7.0	156.6
SL	7.3	156.3
+10	5.9	157.7
+15	5.6	158.0
cb	5.6	158.0
+7	5.6	158.0
+10	5.5	158.1
1/4	4.5	159.1
+5	5.1	158.5
+6 S Pav	5.09	158.47
±	5.00	158.56
+9 N Pav	5.16	158.40
+10	5.2	158.4
+12	5.4	158.2
1/4	5.3	158.3
1/4	5.5	158.1
+4	8.2	155.4
+5	8.2	155.4
cb	8.0	155.6
+10	8.7	154.9
NL	9.7	153.9
10N	9.9	153.7
15N	10.0	153.6

46

163.56

5+46 ²⁵ = B.C.

15N	9.9	153.7
N.L.	9.5	154.1
+10	9.8	153.8
7/8	10.0	153.6
+17	10.7	152.9
cb	10.7	152.9
+6	10.7	152.9
+10	9.7	153.9
1/4	6.2	157.4
+1	6.0	157.6
+5	6.1	157.5
+6 N Paw	5.98	157.58
±	5.77	157.79
+9 S Paw	5.77	157.79
+10	5.8	157.8
1/4	5.4	158.2
+4	8.0	155.6
+5	8.1	155.5
cb	8.7	154.9
+5	9.2	154.4
+10	9.2	154.4
S.L.	10.0	153.6
3B	9.8	153.8
10 S	8.8	154.8
20.5	9.8	153.8

Stations to be
on island this summer
EAB

163.56

5+81 ³¹

47

15S	10.5	153.1
SL	10.6	153.0
+10	10.4	153.2
cb	10.3	153.3
+9	10.0	153.6
+10	9.6	154.0
±	6.8	156.8
+1	6.2	157.4
+5	6.6	157.0
+6 S Paw	6.51	157.05
±	6.58	156.98
+9 N Paw	6.84	156.72
+10	6.9	156.7
+13	6.9	156.7
1/4	7.5	156.1
+5	10.8	152.8
+9	12.3	151.3
cb	12.8	150.8
+10	13.0	150.6
N.L.	13.1	150.5
15N	13.4	150.2

6+15 82

163.56

15N	13.4	150.2
NL	13.2	150.4
+10	13.2	150.2
eb	13.3	150.3
+5	13.0	150.6
+10	11.2	152.4
+12	10.6	153.0
14	8.2	155.4
+1	8.0	155.6
+2	7.3	156.3
+5	7.6	156.0
+6 N Pav	7.68	155.88
E	7.31	156.25
+9 S Pav	7.15	156.41
+10	7.1	156.5
+13	6.8	156.8
14	7.5	156.1
+5	10.4	153.2
+8	10.9	152.7
eb	11.4	152.2
+10	11.1	152.5
S.L.	11.0	152.6
13 S	10.8	152.8
15 S	10.3	153.3

163.56

48

Culvert at 6+27 Bend 36' N of S.L.

12" Conc pipe 37' long		
FL send	13.17	149.49
FL Nend.	13.60	149.96
6+50 ⁹³		
10 S	8.4	155.2
S.L.	8.8	154.8
+10	8.9	154.7
eb	9.9	153.7
+4	10.9	152.7
+10	10.9	152.7
+11	10.9	162.7
14	8.9	154.7
+4	7.6	156.0
+5	7.6	156.0
+6 S Pav	7.77	155.79
E	7.90	155.66
+9 N Pav	8.30	155.26
+10	8.3	155.3
+14	8.4	155.2
19	9.0	154.6
+5	9.1	154.5
eb	10.2	153.4
+9	11.3	152.3
+10	11.7	151.9
N.L.	13.0	150.6
15N	13.8	149.8

163.56

(B) Sec P 37 EC Ret	12.7	150.9
6 + 89 29		
15N	12.6	151.0
3N	12.5	151.1
N.L.	12.2	151.4
+10	12.0	151.6
+17	11.5	152.1
+18	10.4	153.2
cb	10.0	153.6
+10	8.7	154.9
+14	8.1	155.5
1/4	8.2	155.4
+6 N Pav	8.66	154.90
±	8.31	155.25
+9 S Pav	8.19	155.37
+10	7.8	155.8
+12	7.8	155.8
1/4	8.4	155.2
+5	8.6	155.0
cb	8.5	155.1
+10	8.2	155.4
5L	7.9	155.7
10 S	7.8	155.8
(C) Sec P 37	7.1	156.5

163.56

49

6 + 92 el		
10 S	7.5	156.1
5L	7.6	156.0
+10	8.3	155.3
cb	8.4	155.2
+10	8.4	155.2
1/4	8.4	155.2
+1	8.4	155.2
+4	7.5	156.1
+5	7.7	155.9
+6 S Pav	8.24	155.32
±	8.36	155.20
+9 N Pav	8.66	154.90
+10	8.7	154.9
1/4	8.3	155.3
+3	8.7	154.9
+5	9.1	154.5
+8	9.4	154.2
+9	10.3	153.3
+14	10.7	152.9
cb	9.1	154.5
+10	10.4	153.2
+15	11.6	152.0
N.L.	12.0	151.6
+1	11.5	152.1
12N	11.5	152.1

7+19⁵⁵

163.56

15N	12.2	151.4
12N	12.7	150.9
5N	12.0	151.6
N.L	10.3	153.3
+10	9.5	154.1
+15	8.9	154.7
cb	8.9	154.7
+13	8.4	155.2
1/4	8.6	155.0
+6 N Pad	8.66	155.90
+	8.43	155.13
+9 S Pad	8.40	155.16
+10	8.2	155.4
1/4	8.0	155.6
+5	8.0	155.6
cb	8.0	155.6
+10	7.8	155.8
S.L	7.5	156.1

163.56

50

7+54¹⁵ = E.C.

S.L	7.5	156.1
+10	7.8	155.8
cb	8.1	155.5
+10	8.2	155.4
1/4	8.2	155.4
+5	8.4	155.2
+6 S Pad	8.39	155.17
+	8.33	155.23
+9 N Pad	8.45	155.11
+10	8.5	155.1
1/4	8.7	154.9
+5	8.9	154.7
+10	8.7	154.9
cb	9.0	154.0
+10	9.6	154.0
N.L	10.1	153.5
10N	10.6	153.0
① See P. 37	11.1	152.5

8+02⁹⁶

163.56

10N	10.4	153.2
N.L.	9.2	154.4
+10	8.8	154.8
cb	8.4	155.2
+5	8.2	155.4
+10	8.2	155.4
1/4	8.1	155.7
+5	8.1	155.5
+6 N Paw	8.06	155.50
+	7.97	155.59
+9 S Paw	8.05	155.51
+10	8.1	155.5
1/4	7.9	155.7
+5	8.1	155.5
cb	8.1	155.5
+10	7.8	155.8
S.L.	7.4	156.2
(E) See p37	6.7	156.9

163.56

51

8+30

SL	7.2	156.4
+10	7.2	156.4
cb	7.8	155.8
+10	8.0	155.6
1/4	8.0	155.6
+5	7.8	155.8
+6 S Paw	7.77	155.79
+	7.70	155.86
+9 N Paw	7.80	155.76
+10	7.9	155.7
1/4	8.1	155.5
+5	8.1	155.5
cb	8.4	155.2
+10	8.7	154.9
N.L.	9.1	154.5
10'N	9.1	154.5
8+60		
10N	8.8	154.8
N.L.	8.3	155.3
+10	8.3	155.3
cb	8.0	155.6
+10	7.5	156.1
1/4	7.4	156.2
+5	7.5	156.1
+6 N Paw	7.41	156.15

	16356		
8+60	16364		
±		7.29	156.27
+9 S.Pav		7.34	156.22
+10		7.3	156.3
1/4		7.6	156.0
+5		7.6	156.0
cb		7.4	156.2
+10		7.1	156.5
S.L.		6.9	156.7
9+20			
S.C.		5.1	158.5
+10		5.7	157.9
cb		6.4	157.2
+10		6.8	156.8
1/4		6.6	157.0
+5		6.5	157.1
+6 S.Pav		6.49	157.07
±		6.40	157.16
+9 N.Pav		6.49	157.07
+10		6.6	157.0
1/4		6.6	157.0
+5		6.5	157.1
cb		6.8	157.8
+10		7.3	156.3
N.L.		7.7	155.9
10N		8.0	156.89
T.P.	7.67	6.67	156.97

16456
~~16464~~

	16456		52
9+50	16464		
10N 821		8.7	155.9
N.L. 721		8.1	156.5
+10 721		7.7	156.9
cb 721		7.4	157.2
+10 721		7.1	157.5
+12 721		6.9	157.7
1/4 721		7.1	157.5
+5 721		7.1	157.5
+6 N.Pav		6.98	157.58
± 721		6.88	157.68
+9 S.Pav		6.98	157.58
+10 721		6.9	157.7
1/4 721		7.1	157.5
+5 721		6.9	157.7
+10 721		6.5	158.1
cb 721		6.5	158.1
+10 721		6.1	158.5
S.L. 721		5.4	159.2

169.56

9+80

SL	6.0	158.6
+10	6.2	158.4
cb	6.1	158.5
+10	6.2	158.4
1/4	6.2	158.4
+5	6.3	158.3
+6 S Pav	6.44	158.12
+	6.36	158.20
+9 1/4 Pav	6.47	158.09
+10	6.5	158.1
1/4	6.6	158.0
+5	6.7	157.9
cb	6.7	157.9
+10	7.1	157.5
N.L.	7.6	157.0
10N	8.0	156.6
10+10		
10N	7.9	156.7
N.L.	7.6	157.0
+10	7.1	157.5
cb	6.6	158.0
+10	6.4	158.2
1/4	6.3	158.3
+5	6.2	158.4
+6 N Pav	6.01	158.55

169.56

53

10+10

+	5.93	159.63
+9 S Pav	6.00	158.56
+10	6.0	158.6
1/4	6.0	158.6
+5	6.0	158.6
cb	5.7	158.9
+10	5.7	158.9
SL	6.0	158.0
10+40		
SL	4.7	159.9
+10	5.1	159.5
cb	5.2	159.4
+10	5.3	159.3
1/4	5.2	159.4
+5	5.7	158.9
+6 S Pav	5.71	158.85
+	5.56	159.00
+9	5.58	158.98
+10	5.7	158.9
1/4	5.8	158.8
+5	6.2	158.4
cb	6.5	158.1
+10	6.9	157.7
N.L.	8.0	156.6
10N	8.7	155.9

10+59

164.56

10N	10.2	154.4
NL	9.3	154.3
+5	8.7	155.9
+10	7.2	157.4
+13	6.5	158.1
cb	6.4	158.5
+5	5.8	159.1
+10	5.5	159.1
1/4	5.5	159.1
+5	5.4	159.2
+6 N.Pav	5.34	159.22
±	5.37	159.19
+9 S.Pav	5.53	159.03
+10	5.5	159.1
1/4	5.1	159.5
+5	5.1	159.5
cb	4.6	160.0
+10	5.0	159.6
5L	5.0	159.6

10+70

164.56

54

3.6	5.1	159.5
+10	5.1	159.5
cb	5.0	159.6
+10	5.2	159.4
1/4	5.2	159.4
+5	5.4	159.2
+6 S.Pav	5.41	159.15
±	5.25	159.31
+9 N.Pav	5.25	159.31
+10	5.3	159.3
1/4	5.5	159.1
+5	5.7	158.9
cb	6.1	158.5
+10	6.6	158.0
NL	7.1	157.5
10N	7.7	156.9

10+97³¹ = B.C. 169.56

*Stationing mounted
the same 8/23*

10N	8.8	155.8
NL	7.2	157.4
+10	6.6	158.0
cb	5.9	158.7
+10	5.7	158.9
1/4	5.5	159.1
+5	5.3	159.3
+6 N Pav	5.31	159.25
±	5.34	159.22
+9 S Pav	5.47	159.09
+10	5.5	159.1
1/4	5.5	159.1
+5	5.2	159.4
cb	5.2	159.4
+10	5.2	159.4
S.L.	4.9	159.7
11+34 ⁸⁵		
S.L.	4.5	160.1
+10	5.3	159.3
cb	5.4	159.2
+10	5.7	158.9
1/4	5.9	158.7
+5	6.2	158.4
+6 S Pav	6.14	158.52

11+34⁸⁵ 169.56 55

±	5.71	158.85
+9 N Pav	5.50	159.06
+10	5.6	159.0
1/4	5.7	158.9
+5	5.8	158.8
cb	6.1	158.5
+10	6.9	157.7
NL	7.1	157.5
10N	7.9	156.7
11+72 ⁵⁹		
10N	8.0	156.6
NL	7.3	157.3
+10	6.9	157.7
cb	6.3	158.3
+10	5.9	158.7
1/4	5.9	158.7
+5	6.0	158.6
+6 N Pav	6.05	158.51
±	6.31	158.25
+9 S Pav	6.79	157.77
+10	6.4	158.2
1/4	6.4	158.2
+5	6.4	158.2
cb	6.2	158.4
+10	5.7	158.9
S.L.	5.0	159.6

12+09 23

164.56

S.L.	5.8	158.8
+10	6.2	158.9
cb	6.4	158.2
+10	6.6	158.0
1/4	7.0	157.6
+5	7.3	157.3
+6 S Pav	7.34	157.22
±	6.99	157.57
+9 N Pav	6.77	157.79
+10	6.8	157.8
+5	7.0	157.6
cb	7.2	157.4
+10	7.5	157.1
N.L.	7.9	156.7
10N	8.7	155.9
12+47 47		
10N	9.3	155.3
N.L.	8.5	156.1
+10	8.3	156.3
cb	7.8	156.8
+10	7.6	157.0
1/4	7.6	157.0
+5	7.6	157.0
+6 N Pav	7.55	157.01
±	7.76	156.80

164.56

56

12+47 47

±9 S Pav	8.16	156.40
+10	8.0	156.6
1/4	7.6	157.0
+5	8.1	156.5
+10	7.8	156.8
cb	7.8	156.8
+10	6.8	157.8
S.L.	6.0	158.6
12+85 01		
S.L.	7.7	156.9
+10	8.5	156.1
cb	8.8	155.8
+10	8.7	155.7
1/4	8.7	155.9
+5	8.7	155.9
+6 S Pav	8.75	155.81
±	8.41	156.15
+9 N Pav	8.24	156.32
+10	8.3	156.3
1/4	8.0	156.6
+5	8.0	156.6
cb	8.3	156.3
+10	8.7	155.9
N.L.	9.5	155.1
10N	9.7	154.9

13+22⁵⁸ = E.C

164.56

10N	10.6	154.0
NL	9.7	154.9
+10	9.1	155.5
cb	8.7	155.9
+10	8.4	156.2
1/4	8.5	156.1
+5	8.7	155.7
+6 N Paw	8.90	155.66
+	8.90	155.66
+9 S Paw	9.06	155.50
+10	9.0	155.6
1/4	9.1	155.5
+5	9.2	155.4
+cb	9.1	155.5
+10	8.9	155.7
S.L	8.5	156.1

13+60

S.L	9.4	155.2
+10	9.4	155.2
cb	9.5	155.1
+10	9.5	155.1
1/4	9.4	155.2
+5	9.4	155.2
+6 spaw	9.39	154.17

13+60

164.56

57

+	9.29	155.27
+9 N Paw	9.39	155.17
+10	9.5	155.1
1/4	9.6	155.0
+5	9.5	155.1
cb	10.0	154.6
+10	10.0	154.6
NL	10.7	153.9
10N	11.0	153.6
13+94 ²⁸ = w. 53 ^d on South		
10N	10.6	154.0
NL	10.7	153.9
+10	10.5	154.1
cb	10.2	154.4
+10	9.8	154.8
1/4	9.7	154.9
+5	9.6	155.0
+6 N Paw	9.50	155.06
+	9.39	155.17
+9 S Paw	9.50	155.06
+10	9.5	155.1
1/4	9.5	155.1
+5	9.5	155.1
cb	9.6	155.0
+10	9.5	155.1
+12	9.4	155.2

13 + 94⁹⁸164.56
164.64

S.L. 9.8 154.8

(G) See P 37 10.1 154.5

14 + 194²

S.L. 9.9 154.7

+10 9.7 154.9

cb 9.7 154.9

+10 9.5 155.1

1/4 9.6 155.0

+5

+6 S Pau 9.55 155.01

+ 9.47 155.09

+9 N Pau 9.56 155.00

+10 9.7 154.9

+12 10.0 154.6

1/4 9.7 154.9

+5 9.8 154.8

cb 10.6 154.0

+10 10.6 154.0

N.L. 10.9 153.7

10N 11.2 153.4

(E) See P 37 11.6 153.0

B.M. 7.25 161.22
+61.30 154.17 HUB NE
154.25 Imp. 5319 + 71²² = 53 on North
161.22
161.30

N.L. Prod. 7.4 153.8

+10 7.0 154.2

cb 6.9 154.3

+10 6.7 154.5

1/4 6.4 154.8

+5 6.4 154.8

+6 N Pau 6.39 154.83

+ 6.28 154.94

+9 S Pau 6.33 154.89

+10 6.4 154.8

1/4 6.5 154.7

+5 6.7 154.5

cb 7.0 154.2

+10 6.8 154.4

S.L. Prod. 6.7 154.5

58

X sec Imperial from 53^d to
 54th 80' st 10' cbs 60' Roadway
 161.22
 161.30

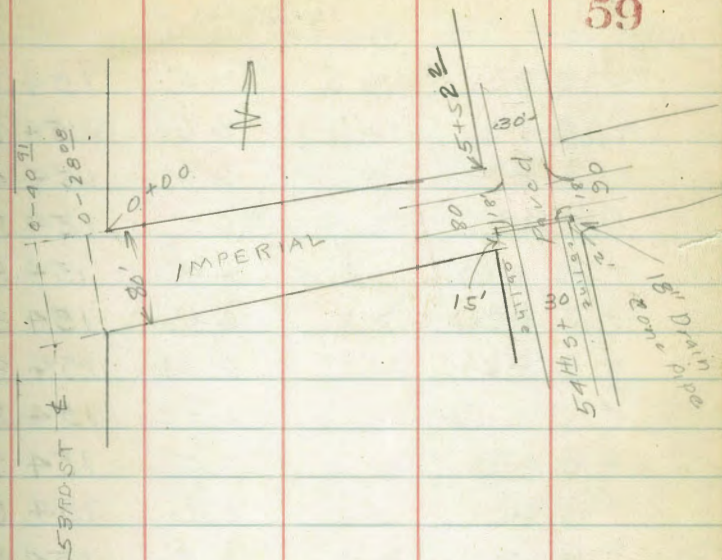
0-40²¹ = \pm 53^d on South

SL	Prod.	6.6	154.6
cb		6.8	154.4
+10		6.6	154.6
'4		6.3	154.9
+5		6.3	154.9
+6	S Pav	6.29	154.93
\pm		6.23	154.99
+9	N Pav	6.37	154.85
+10		6.4	154.8
'4		6.7	154.5
+5		6.9	154.3
cb		7.6	153.6
+5		7.2	153.0
NL		7.3	153.9

0-2808 = E.L. 53^d on South

NL		7.1	154.1
cb		6.9	154.3
+10		6.6	154.6
'4		6.3	154.9
+6	N Pav	6.37	154.85
\pm		6.27	154.95
+9	S Pav	6.35	154.87
+10		6.4	154.8
'4		6.6	154.6
+5		6.7	154.5

59



0-2808 161.30

cb		6.7	154.5
SL		6.5	154.7

0+00 = E.L. 53 = ^{161.22} ~~161.30~~ on North.

S.L.	6.5	154.7
cb	6.6	154.6
+10	6.7	154.5
'4	6.5	154.7
+5	6.4	154.8
+6 S Pav	6.40	154.82
+	6.33	154.89
+9 N Pav	6.42	154.80
+10	6.5	154.7
'4	6.6	154.6
+5	6.8	154.4
+8	7.2	154.0
+10	6.7	154.5
cb	6.7	154.5
N.L.	7.0	154.2
S'N	7.2	154.0
0+30		
S'N	7.1	154.1
N.L.	7.0	154.2
cb	6.8	154.4
+10	6.3	154.9
'4	6.1	155.1
+5	6.4	154.8
+6 N Pav	6.40	154.82

0+30

^{161.22}
~~161.30~~

60

+	6.31	154.91
+9 S Pav	6.40	154.82
+10	6.4	154.8
'4	6.5	154.7
+5	6.6	154.6
cb	6.8	154.4
S.L.	6.4	154.8
0+60		
S.L.	6.3	154.9
cb	6.6	154.6
+10	6.4	154.8
'4	6.5	154.7
+5	6.4	154.8
+6 S Pav	6.31	154.91
+	6.24	154.98
+9 N Pav	6.35	154.87
+10	6.4	154.8
'4	6.5	154.7
+5	6.5	154.7
cb	6.7	154.5
N.L.	7.1	154.1
S'N	7.3	153.9

	161.22	
1+00		
5N	7.4	153.8
NL	7.4	153.8
cb	7.0	153.2
+10	6.8	154.4
1/4	6.5	154.7
+5	6.2	155.0
+6 N Pav	6.19	155.03
+	6.09	155.13
+9 S Pav	6.19	155.03
+10	6.2	155.0
1/4	6.3	154.9
+5	6.5	155.7
cb	6.4	154.8
+1	6.7	154.5
SL	6.5	154.7
1+30		
S.L	6.4	154.8
cb	6.5	154.7
+10	6.1	155.1
1/4	6.2	155.0
+5	6.1	155.1
+6 S Pav	6.07	155.15
+	5.99	155.23
+9	6.06	155.16
+10	6.1	155.1
1/4	6.2	155.0

	161.22	61
1+30		
+5	6.6	154.6
cb	6.9	154.3
NL	7.3	153.9
5N	7.5	153.7
1+65		
NL walk to house	6.54	154.68
+6	7.2	154.0
cb	7.1	154.1
+10	6.7	154.5
1/4	6.2	155.0
+5	6.0	155.2
+6 N Pav	5.89	155.33
+	5.82	155.40
+9 S Pav	5.92	155.30
+10	5.9	155.3
1/4	5.9	155.3
+5	6.1	155.1
+10	6.1	155.1
+12	6.4	154.8
+13	5.9	155.3
cb	5.9	155.3
S.L.	5.9	155.3

161.22

2+00

SL	6.1	155.1
cb	5.9	155.3
+2	6.0	155.2
+4	6.3	154.9
+6	5.8	155.4
+10	5.7	155.5
1/4	5.8	155.4
+5	5.7	155.5
+6 S Pav	5.69	155.53
+	5.63	155.59
+9 N Pav	5.74	155.48
+10	5.8	155.4
1/4	6.1	155.1
+5	6.5	155.7
cb	6.8	154.4
NL	6.6	154.6
Drive at 1+93 on NL	6.31	154.91
Drive at 2+11 on NL	6.38	155.84
walk to house at 2+32 ^{on NL}	6.01	155.21

161.22

2+30

62

NL	6.0	155.2
+5	6.4	154.8
cb	6.4	154.8
+10	5.9	155.3
1/4	5.5	155.7
+5	5.6	155.6
+6 N Pav	5.50	155.72
+	5.40	155.82
+9	5.46	155.76
+10	5.5	155.7
1/4	5.6	155.6
+5	5.5	155.7
+11	6.5	155.7
+13	5.9	155.5
cb	5.8	155.4
SL	5.9	155.3
2+65		
SL	5.6	155.6
cb	5.2	155.0
+4	6.3	154.9
+6	5.6	155.6
+10	5.2	156.0
1/4	5.2	156.0
+5	5.2	156.0
+6 S Pav	5.17	156.05

161.22

2+65

4	5.05	156.17
+9 N Pav	5.17	156.05
+10	5.3	155.9
1/4	5.7	155.5
+5	5.9	155.3
ob	6.2	155.0
N.L.	6.3	154.9
3+00		
N.L.	6.0	155.2
cb	5.6	155.6
+1	5.9	155.3
+4	5.4	155.8
+10	5.4	155.8
1/4	5.3	155.9
+5	4.9	156.3
+6 N Pav	4.79	156.43
4	4.72	156.50
+9 S Pav	4.83	156.39
+10	4.9	156.3
1/4	4.9	156.3
+5	5.0	156.2
+9	4.9	156.3
+11	6.1	155.1
+12	5.8	155.4
ob	4.9	156.3
+5	4.9	156.3

161.22

63

3+00

5L 22	5.3	155.9
3+30		
5L 221	4.6	156.6
cb 22	4.6	156.6
+4 22	5.9	155.3
+6 22	5.9	155.3
+8 22	5.0	156.2
+10	4.9	156.3
1/4 22	4.7	156.5
+5 22	4.5	156.7
+6 S Pav	4.46	156.76
4 22	4.36	156.86
+9 22	4.49	156.73
+10 22	4.7	156.5
1/4 22	5.3	155.9
+1 22	5.2	156.0
+5 22	5.3	155.9
+8	5.4	155.8
cb	5.2	156.0
N.L.	5.1	156.1

161.22

3+65

NL	4.6	156.6
cb	4.8	156.4
+10	4.9	156.3
1/4	4.8	156.4
+5	4.3	156.9
+6 N Pav	4.09	157.13
⊕	4.01	157.21
+9 S Pav	4.09	157.13
+10	4.2	157.0
1/4	4.2	157.0
+5	4.1	157.1
+7	4.7	156.5
+8	5.9	155.3
+10	5.8	155.4
+13	4.2	157.0
cb	4.0	157.2
S.L.	3.9	157.3

161.22

4+00

64

S.L.	4.1	157.1
cb	3.5	157.7
+6	5.9	155.3
+8	4.4	156.8
+10	4.3	156.9
1/4	4.0	156.2
+5	3.8	157.4
+6 S Pav	3.73	157.49
⊕	3.63	157.59
+9 N Pav	3.73	157.49
+10	3.9	157.3
1/4	4.2	157.0
+5	4.4	156.8
cb	4.3	156.9
NL	4.5	156.7
4+30		
NL	4.1	157.1
cb	4.1	157.1
+10	3.8	157.4
1/4	3.8	157.4
+5	3.5	157.7
+6 N Pav	3.41	157.81
⊕	3.32	157.90
+9 S Pav	3.41	157.81
+10	3.4	157.8
1/4	3.6	157.6

161.22

4+30

+5	3.8	157.4
+7	4.1	157.1
+10	5.8	155.4
cb	3.3	157.9
+7	3.6	157.6
+8	4.1	157.1
SL	3.8	157.4

4+65

SL	3.4	157.8
+5	3.1	158.1
+9	2.3	158.9
+cb	2.6	158.6
+4	4.2	157.0
+5	5.8	155.4
+7	3.4	157.8
+10	3.4	157.8
4	3.1	158.1
+5	3.0	158.2
+6. S Pav	2.96	158.26
+	2.87	158.35
+9 N Pav	2.99	158.23
+10	3.0	158.2
4	3.1	158.1
+5	3.2	158.0
cb	3.5	157.7
NL	3.6	157.6

161.22

5+00

65

AL	3.3	157.9
cb	3.3	157.9
+10	3.1	158.1
4	2.9	158.3
+5	2.8	158.4
+6 N Pav	2.70	158.52
+	2.56	158.66
+9 S Pav	2.63	158.59
+10	2.6	158.6
4	3.0	158.2
+5	3.4	157.8
+8	4.0	157.2
+7	5.8	155.4
+10	5.7	155.5
+11	4.1	157.1
cb	2.3	158.9
+2	1.9	159.3
+6	2.9	158.3
SL	3.0	158.2

5+30

101.22

SL.	2.8	158.4
+H	2.7	158.5
+8	1.8	159.4
eb	2.2	159.0
+4	4.0	157.2
+5	5.5	155.7
+7	5.6	155.6
+8	3.4	157.8
H0	2.9	158.3
1/4	2.6	158.6
+5	2.5	158.7
+6 S Pav	2.42	158.80
±	2.31	158.91
+9 N Pav	2.40	158.82
+10	2.4	158.8
1/4	2.5	158.7
+5	2.6	158.6
eb	3.1	158.1
N.L.	3.2	158.0

161.22

5+57² = N.L. 59th 5+

66

N.L.	3.7	157.5
eb	3.1	158.1
+10	2.1	159.1
1/4	2.1	159.1
+5	2.2	159.0
+6 N Pav	2.24	158.98
±	2.16	159.06
+9 S Pav	2.27	158.95
+10	2.3	158.9
1/4	2.1	159.1
+5	2.6	158.6
+8	3.2	158.0
+9	5.3	155.9
+11	5.4	155.8
+11 F.L. Five	5.95	155.27
+13	2.7	158.5
eb	2.2	159.0
+5	2.7	158.5
S.L.	2.6	158.6

161.22

5+62² = web 54th

S.L.	2.8	158.4
cb	2.5	158.7
+10	2.2	159.0
1/4	2.2	159.0
+5	2.2	159.0
+6 S Pav	2.20	159.02
+	2.16	159.06
+10	2.17	159.05
+13 N Pav	2.15	159.07
1/4	2.2	159.0
+5	2.1	159.1
+10	2.0	159.2
cb	2.2	159.0
N.L.	2.7	158.5
5+67 ² = Wedge Pav. on 54 th		
N.L.	2.63	158.59
cb	2.42	158.80
+10	2.23	158.99
1/4	2.17	159.05
+5	2.13	159.09
+	2.09	159.13
+10	2.17	159.05
1/4	2.22	159.00
+5	2.30	158.92
cb	2.38	158.84
S.L.	2.49	158.73

161.22

5+82² = + 54th

67

S.L.	2.29	158.93
cb	2.21	159.01
+10	2.15	159.07
1/4	2.11	159.11
+	1.96	159.26
+10	2.04	159.18
1/4	2.07	159.15
+5	2.10	159.12
cb	2.30	158.92
N.L.	2.48	158.74
2+99 ² = E edge Pav on 54 th		
N.L.	2.65	158.57
cb.	2.38	158.84
+10	2.19	159.03
1/4	2.08	159.14
+5	1.99	159.23
+	1.87	159.35
+10	1.96	159.26
1/4	2.05	159.27
+5	2.19	159.03
cb	2.32	158.92
S.L.	2.44	158.78

161.22

6 + 0.22 = Ecb 54th

S.L.	2.6	158.6
eb	2.2	159.0
+10	2.0	159.2
1/4	2.1	159.1
+2 S Pav	1.98	159.24
+10	1.93	159.29
4	1.85	159.37
+10	1.95	159.27
+13 N Pav	2.01	159.21
1/4	2.1	159.1
+5	1.9	159.3
eb	2.2	159.0
NL	2.1	159.1
FL. End Drain	5.68	155.54

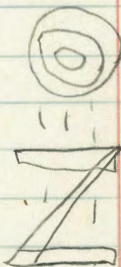
See Book 1295 Pg. 34

68

12/4/28
Stoore

CROSS SECTION of Alley = 16' wide
815 407 HELPBINDING AVE

	12.93	59.82	4689	54764 N. 17th. Ave
VWBP				
	EL 97+200			
√ Top CON CURB		4.10		55.72
C		3.9		55.9
N		3.63		56.19
	0+10			
N		1.7		58.1
C		2.4		56.4
S		2.0		57.8
T.P.	12.06	71.28	0.60	59.22
	0+40			
√		10.7		60.6
C		10.7		60.6
N		10.0		61.9
	0+63			
N		8.5		62.8
C		8.8		62.5
S		8.6		62.7
	0+81			
S		8.2		62.9
C		8.2		63.1
N		7.8		63.5
+13.3	Six Gar. Com. floor	6.77		64.51
	1+00			
N		6.5		64.8
C		7.1		64.2



71.28

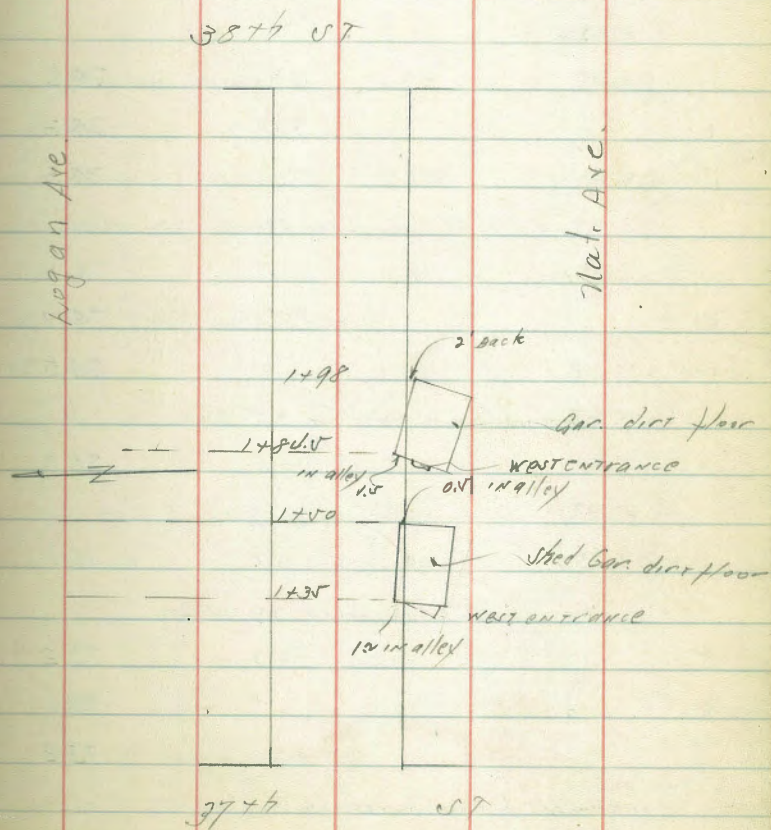
69

	7.6	63.7
beginning of fence 0.5 in alley		
1+14 = end fence 0.5 in alley		
1+35		
-3 ^{wood} Entrance Gar. dirt floor	5.7	65.6
√	5.6	65.7
+1.5 = NW Cor. Gar.	5.5	65.8 see sketch next page
C	5.3	66.0
N	4.6	66.7
	1+59	
-13 Six Gar. Com. floor	1.34	69.24
N	2.8	68.5
C	3.6	67.7
S	4.5	66.8
	1+84.5	
-4 ^{wood} Entrance Gar	3.6	67.7 dirt floor
S	3.2	68.1 see sketch
+1.5 = NW Cor	2.9	68.4
C	2.7	68.6
N	1.9	69.4
	2+00	
N	1.6	69.7
C	1.8	69.5
S	1.9	69.4
	2+46	
-5	4.7	66.6
S	3.9	67.4
C FL Sewer MH	7.25	64.03
" RIM MH	3.00	68.28

7/1/8

✓	4+46		5.4	69.1
✓	4+72		2.4	68.9
✓			3.1	68.2
✓			4.1	67.2
✓			4.1	67.2
	2+99			
-✓			2.0	69.3
✓			1.7	69.6
✓			1.8	69.5
✓			1.5	69.8
	3+00			
✓			1.4	69.9
✓			1.7	69.6
+	6.5 = 2" outhead		1.2	70.1
+	7		0.2	71.1
✓			0.2	71.1
T.P.	10.22	81.30	0.20	71.08
	3+13.2 = 2" in. Car den floor			Also has drive from Wash to garage
✓	South of SL		9.70	71.6
	3+35			
✓			8.5	72.8
+	1.4 = beginning of fence to shed		8.5	72.8
✓			8.9	72.4
✓			8.6	72.7

70



81.30

3765

N	7.5	73.8
E	7.7	73.6
+7 fence	7.4	73.9
S 3+80.5 = E of Single Garage on North	12.7 back dirt floor	
ON floor	6.4	74.9
4+00		
S+1 = fence	6.7	74.6
E	7.0	74.3
N	7.0	74.3
4+34 = end of combination fence	1.0 in Alley	
N	6.5	74.8
E ON North edge of Cement Walk 7' long	6.6	74.7
1' in Alley	6.77	74.53
4+41.5 = E single Garage dirt floor	3.5 Back	
ON floor	6.8	74.5
4+53.5 = E single Garage dirt floor	1' Back	
ON floor	6.2	75.1
4+61 = Beginning of Board fence	1.4 in Alley	
S	6.1	75.2
E	6.2	75.1
N	6.1	75.2
5+00 = end of Board fence	1.4 in Alley	
N	5.4	75.9
E	5.3	76.0
S	5.5	75.8

81.30

5+35

S	4.1	77.2
E	4.2	77.1
N	4.1	77.2
5+63		
N	3.4	77.9
E	3.3	78.0
S = E of Reem. Walk on line	2.82	78.48
5+78.5		
S = E of 2' Brick Walk on 2 Back	2.54	78.76
E	2.8	78.5
N	2.8	78.5
5+99.5 = W.L. of 38 th st		
N. top of Curb	1.20	80.10
cut.	1.6	79.7
E	2.0	79.3
cut.	2.0	79.3
S top of Curb	1.58	79.72

71

81.30

1.15

80.15

3.64

83.79

7.28

76.51 on S.E. BP Net + 38

76.58 = given elevation.

0.99

77.57

12.80

64.77

0.16

64.93

11.78

53.15

2.29

55.44

55.44 = H.I.

2.49

46.95 on SWBP Net + 37.

46.89 = given elevation

Benches .07 in Error.

80' wide
14' ebs
13' 1/4s

Polk St. Sec.
Hamilton to Oregon.

2-25
with

349.50

36.02 S.E. Oregon.

H.M. of E. line Hamilton

72

B.M. B.P.	6.88	336.83	O.K.	S.E. Polk & Arizona	N.			
			329.95				+0.6	350.1
T.P.	12.87	349.50	0.20	336.63	+8		+0.4	350.1
	10' W. of E. line Hamilton = End of Radius =		E. End. ent. walk Returns.		ent. cl		4.37	345.13
N. ent. walk		4.65	344.85		gutter pavmt.		5.13	344.37
ent. cl.		5.02	344.48		" "		5.06	344.44
gutter pavmt		5.71	343.79		" "		5.08	344.42
" "		5.72	343.78		" "		5.46	344.04
" "		5.72	343.78		gutter "		5.98	343.52
" "		6.06	343.44		ent. cl		5.27	344.23
gutter "		6.51	342.99		+4		1.7	347.8
ent. cl.		5.97	343.53		5		1.2	348.3
S. ent. walk		5.65	343.85					
	9' W. of E. line				5		0.6	348.9
5		1.9	347.1		+10		1.0	348.5
+10		4.3	345.2		+12		4.3	345.2
ent. cl.		5.84	343.66		ent. cl		4.85	344.65
gutter pavmt.		6.46	343.04		gutter pavmt		5.55	343.95
" "		6.00	343.50		" "		4.94	344.56
" "		5.60	343.90		" "		4.63	344.87
" "		5.61	343.89		" "		4.62	344.88
gutter "		5.62	343.88		gutter "		4.71	344.79
ent. cl.		4.89	344.61		ent. cl		4.02	345.48
+7		3.7	345.8		T.P.	12.08	360.96	0.62
N.		0.9	348.6		+5		10.5	350.5
					N		10.5	350.5

Plotted 8-26-39

T.H.

Ydgs. figured to Subgrade

2-26-39

T.H.

0.0 = E. Line Hamilton St = E. End. ent. cl. & pavmt.

360.96
R.C. of E. line Hamilton

N.	10.3	350.7
+12	10.5	350.5
cl	13.8	347.2
+6	15.3	345.7
1/4	15.6	345.4
c	15.9	345.1
1/4	16.3	344.7
cl	16.2	344.8
+2	11.7	349.3
S	11.8	349.2
5' E		
S	11.4	349.6
cl	11.2	349.8
+8	12.7	348.3
1/4	12.3	348.7
+9	10.9	350.1
c	11.1	349.9
1/4	10.5	350.5
cl	10.1	350.9
N	10.0	351.0
15' E		
N	9.0	352.0
cl	9.3	351.7
1/4	9.7	351.3
c	10.2	350.8
1/4	10.6	350.4

360.96

P.O.K

73

cl	10.5	350.5
S	10.6	350.4
47' E		
S. line	8.02	352.94
cl	8.2	352.8
1/4	8.1	352.9
c	7.0	354.0
1/4	6.7	354.3
cl	6.5	354.5
N	6.1	354.9
59' E		
N	5.3	355.7
cl	5.5	355.5
1/4	5.8	355.2
c	6.6	354.4
1/4	7.2	353.8
cl	7.5	353.5
S. line	7.77	353.19
+10.3	7.68	353.28
69' E		
S. line	7.15	353.81
cl	6.4	354.2
1/4	6.6	354.4
c	5.3	355.7
1/4	5.1	355.9
cl	4.7	356.3
N	4.6	356.4

on ent. walk to
House

on ent. drive
to garage

Front garage floor

ent. strips
to garage

360.96

82' E

N.		4.1	356.9
cb		4.3	356.7
1/4		4.4	356.6
c		4.7	356.3
1/4		5.8	355.2
cb		6.0	355.0
S		5.9	355.1
	100' E.		
S		4.5	356.5
cb		4.9	356.1
1/4		4.6	356.4
c		3.6	357.4
1/4		3.5	357.5
cb		3.1	357.9
N		3.0	358.0
	121' E		
N		2.0	359.0
cb		1.8	359.2
1/4		2.0	359.0
c		3.0	358.0
1/4		3.3	357.7
cb		3.7	357.3
S. Line		3.49	357.47
T.P.	9.02	367.54	2.44 358.52

on cent walk
To House

367.54

POLK

150' E

74

S		8.9	358.6
cb		9.2	358.3
1/4		9.0	358.5
c		8.70	358.84
1/4		13.50	354.04
cb		8.1	358.4
S		7.8	359.7
	100' E.		
N.		7.2	360.3
	200' E.		
N		5.8	361.7
cb		5.9	351.6
1/4		6.4	361.1
c		6.7	360.8
1/4		6.9	360.6
cb		7.4	360.1
S		7.2	360.3
	225' E		
4' S. of S. line		6.06	361.48
S		6.2	361.3
cb		6.7	360.8
1/4		6.0	361.5
c		5.5	362.0
1/4		5.1	362.4
cb		4.8	362.7
N		4.24	363.26

on E. edge
M.H. Cover

Flow Line

on E. cent strip
to garageon cent walk
To House

367.54
242'.8

N. line 4.01 363.53

on cnt. walk
to House

256'.8

N. line 3.16 364.38

cnt. Driveway

cl 3.6 363.9

" 4.0 363.5

e 4.2 363.3

" 5.0 362.5

cl 5.2 362.3

S 4.7 362.8

295'.8

S 3.6 363.9

cl 3.5 364.0

" 3.6 363.9

e 3.3 364.2

" 3.3 364.2

cl 2.5 365.0

N 2.0 365.5

300'.e. = W. line Oregon

N 2.03 365.51 on cnt. walk

cnt. cl 2.58 364.96

gutter paint 3.33 364.21

" 3.12 364.42

e " 3.21 364.33

" 3.48 364.06

gutter " 4.08 363.46

cnt. cl. 3.56 363.98

367.54

Folk.

75

S. on cnt. walk

3.18 364.56

RM. SE. Folk & Oregon B.P. gate

1.54

on cnt. at Hole for B.P.
O.K.
366.00 = 366.02

X Sec. Side Walks on Kettner Blvd. 3-23-29
Kalmia to Laurel mill

32.97 SE Kettner loop

35.11
35'N

76

B.M.	5.31	36.28	30.97	N.E. Juniper + Kettner	E. Line	3.0	32.1	
T.P.	3.61	35.11	4.78	31.50	E. ent. ch	3.56	31.55	
				N. ch Line Kalmia		46'N		
E. Line Kettner ch. to E		3.74	36.57		N. ent. ch	5.09	30.02	
" " "		ent. ch Ret.	4.21	30.90	W. Line	5.3	29.8	
" " "		parbit			+10.	8.3	26.8	
				8' S. of N. Line Kalmia		50'N. { N. End ent. walk on W. "		
W. ent. ch Kettner		5.08	30.03		E. Line	3.3	31.8	
3.5 W = E. edge ent. walk		5.06	30.05		+3.5 = E. edge ent. walk	3.26	31.85	
8.5 W = W " " "		4.93	30.18		+8.5 = W " " "	3.51	31.60	
W. Line		5.1	30.0		E. ent. ch.	2.46	31.65	
				3.5 S of N. Line Kalmia		W. ent. ch		
11.5 W. of W. ch Kettner		5.00	30.11		+3.5 = E. edge ent. walk	4.95	30.16	
8.5 " " " " "		5.36	29.75		W. edge ent. walk to top	4.83	30.28	
W. ch Line		5.56	29.55		W. Line	7.1	28.0	Top Bank
				00 = N. Line Kalmia		+4		Bottom "
W. ent. ch		5.49	29.62		+20	20.2	14.9	
E. ent. ch Ret		3.61	31.50		+40	22.1	13.0	
E. " " To N		3.73	31.38					
E. Line on ent. walk,		3.60	31.51					
				10'N.		70'N		
E. Line		2.9	32.2		W	17.0	18.1	Bottom Bank
E. ent. ch		3.66	31.45		+1	17.0	18.1	Bottom Bank
				20'N		+2		Top "
E. ent. ch.		3.67	31.44		+8	4.0	31.1	
E. Line		3.3	31.8		W. ent. ch	4.88	30.33	

Plotted 3/20/29 T.J.

35.11
100' N.

W. cont. el	4.69	30.42	
+ 3	4.4	30.7	
+ 8	4.6	30.5	
+ 11	5.8	29.3	Top Bank
W	19.5	15.6	Bottom "
+ 20	22.8	12.3	
+ 40	23.3	11.8	

115' N.

W-40	23.5	11.6	
- 20	22.6	12.5	
W	19.8	15.3	Bottom Bank
+ 2	5.3	29.8	Top "
+ 9	4.3	30.8	
W. cont. el	4.55	30.56	

140' N.

W. cont. el	4.38	30.73	
+ 4	4.1	31.0	
W.	5.7	29.4	Top Bank
+ 1	19.0	16.1	Bottom "
+ 13	21.8	13.3	
+ 20	23.0	12.1	
+ 40	23.4	12.0	

151' N.

- 40	19.4	15.7	
- 35	21.3	13.8	
- 20	19.1	16.0	

35.11

- 15	12.8	17.3	Bottom Bank
- 8	8.6	26.5	Top "
W	4.8	30.3	
+ 3	4.2	30.9	
W. cont. el	4.30	30.81	

160' N.

W. cont. el	4.20	30.91	
W	4.1	31.0	
+ 5	4.1	31.0	
+ 15	7.8	27.3	

175' N = S End cont. walk on W.

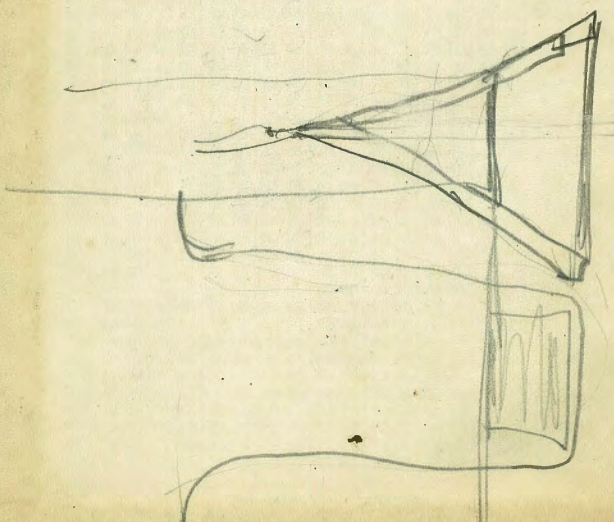
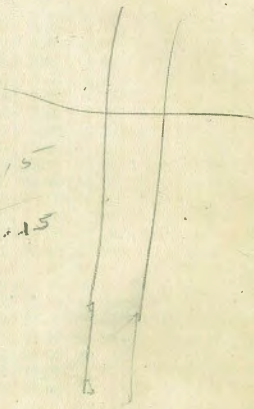
W. on S. End cont. walk	3.84	31.27	
W. cont. el	4.08	31.03	
chk. on B.M.	2.13	32.98	S.E. Hallway + Laurel 32.97

ENGINEERING DEPARTMENT
CITY OF SAN DIEGO, CALIFORNIA.

225.27
1097.81
1322.08
1322.08

1322.08
72.42
1394.50
1394.50

52.15
47
801.15
801.15



50.74
202.96
202.96

13.3
18
31.3
5779.65
5810.95
5810.95

11622
00262
23244
69732
23244
30447.64

1029
2
1027
26
69732
13244
302172
302172

8-55

180
55
535
13
1605
535
6955
3600
6335.5
559

2-55

1-55