

1301



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	Page
X Sec. La Jolla Blvd. ^{Salmor to} sea lane	1-40
Main + 32 nd Inter 5.	42
Alley N Univ. Hts	63
Playa Del Norte as Pers sketch (p-3)	40
Alley Blk 97 S.D.L. & T. Co.	43
Campo.	46
Metropolitan Center	47
Walk N.L. El Cajon Blvd. for	53
Poplar St. Lexington Park	58
X Sec. Alley Blk "N" Univ. Hts. Idaho & Oregon Copley & Collier	63
" " Franklin 29 th to 30 th	66
" " 29 th Ocean View Blvd. to Lincoln	72
" " Alley Blk 76 Park Villas Myrtle to Upper Arnold to Williams	75

Walker
Rippling
Leaky
No Wood
11-28-28

Cross Section LAJOLLA
Bet. Palomar and San Lane st.

Blvd.
100' wide
20' cbs.
15' 7.5

J.S. DP
Rosemont
Electric

0.66 84.46 83.80

Section A

F	6.1	78.1
cb.	7.0	77.5
7	7.0	77.5
+1 on E edge Pav.	7.05	77.9
2 " Pav.	6.94	77.52
+6 Hedge Spring	7.05	77.4
7	7.7	76.8
4 cb. on Ground	8.6	75.9
" " Pav.	9.08	75.4

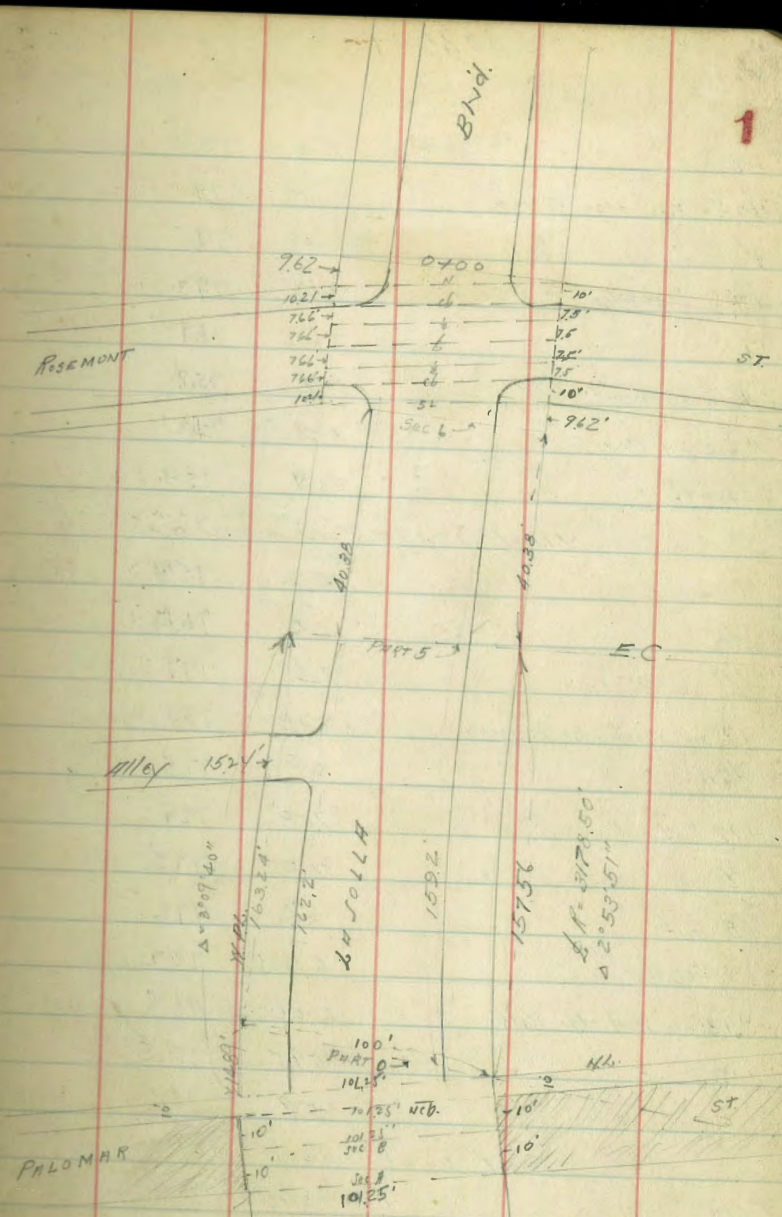
Section B - S. Roadway Palomar

4 " "	9.28	75.2
cb.	8.7	75.8
7	7.7	76.8
+7.2 on West edge Pav.	7.14	77.3
2 " Pav.	7.00	77.5
+12.5 = East edge Pav.	7.03	77.4
7	7.0	77.5
cb.	6.8	77.7
E. on Pav.	7.36	77.1

Ncb Line Palomar

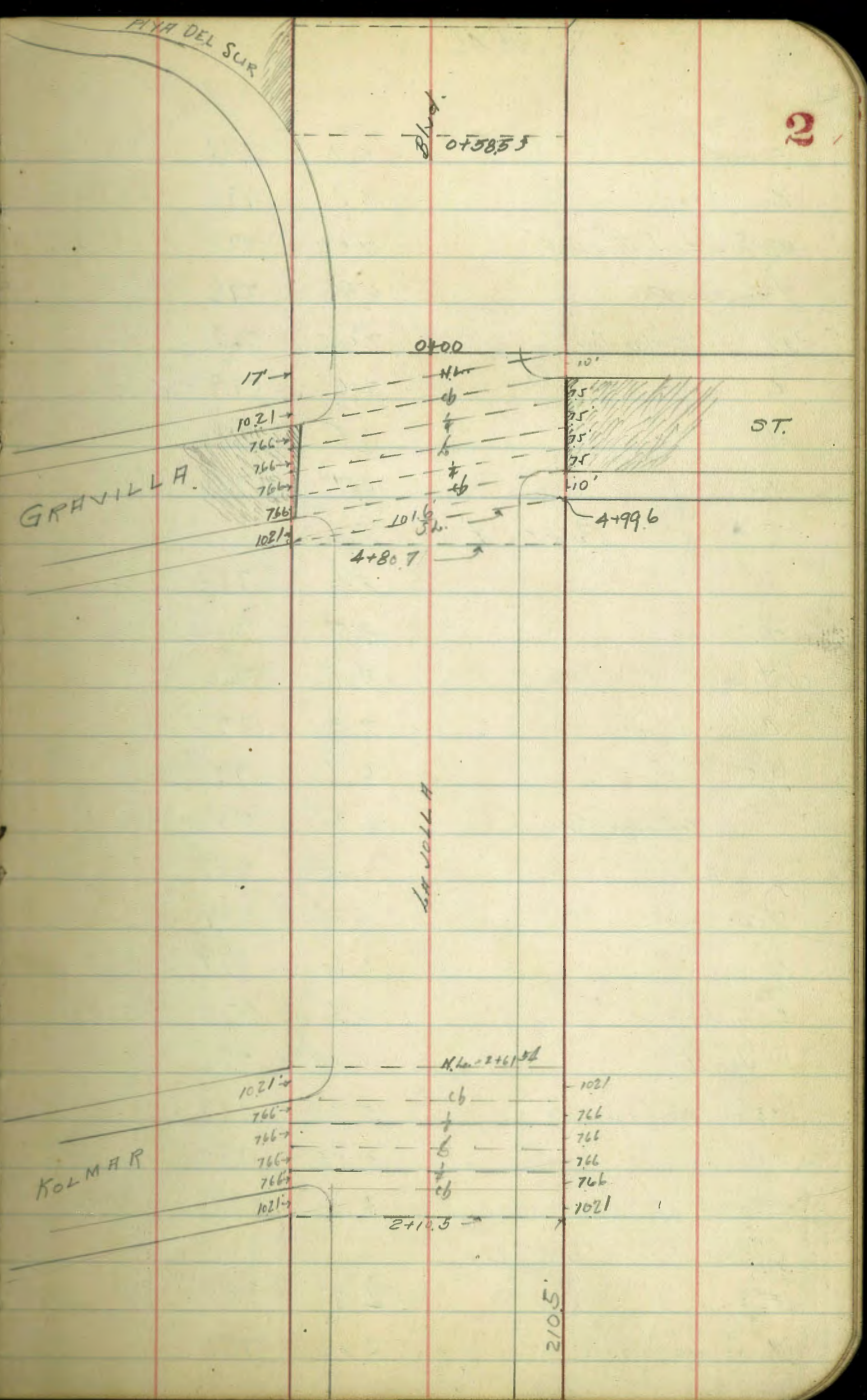
E Lap cb.	5.95	78.51
" Gut. on Spring	6.63	77.8
cb. on Ground	6.6	77.9

Garbage 12-17-28
T.G.H.



1/2	70	77.5
+2.5 = East edge Paring	70.5	77.9
1/2 on "	6.98	77.5
+7.5 " W edge "	7.11	77.3
1/2	7.6	76.9
W cb. on Ground	8.7	75.8
W Gut. on Pav.	9.70	74.8
" top cb.	9.09	75.4
N.L. PALOMAR		
W	8.7	75.8
cb.	8.5	76.0
1/2	7.4	77.1
-7.7 on West edge Paring	7.03	77.7
1/2 " " "	6.91	77.5
+12 " E " "	7.03	77.4
1/2	7.0	77.5
E Gut	6.9	77.6
" top cb.	6.25	78.2
+13 on West edge Walk	6.00	78.5
+18 " E " "	5.95	78.5
E	5.9	78.6
PART 0 of Curve { 5 equal parts }		
E	5.9	78.6
" +1 " on Walk	5.95	78.5
-6 " " "	6.00	78.5
E top cb.	6.25	78.2

Note: No Levels on curb on West Bldg. N.L. Palomar + Hilley N. No. "



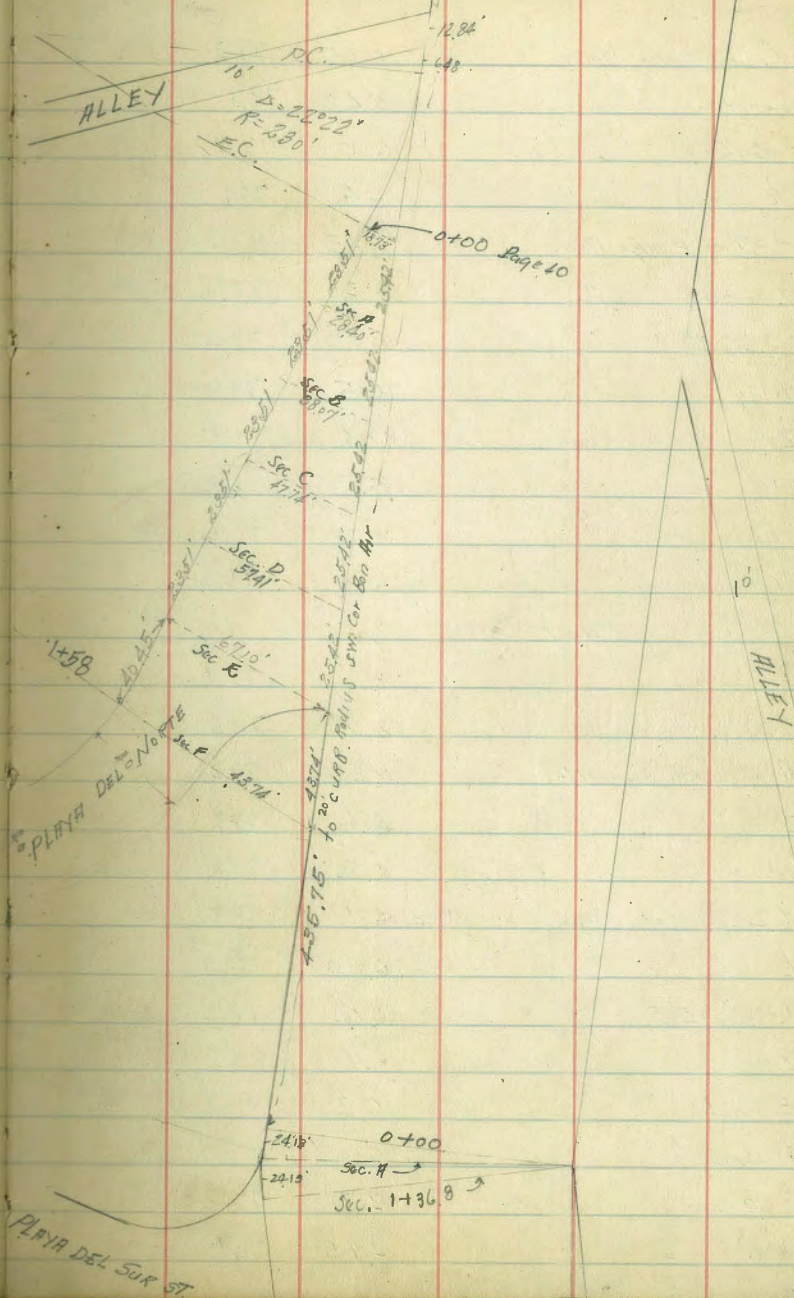
E Gut	6.9	77.6
$\frac{1}{2}$	6.9	77.6
+2.5 = East edge Pav.	7.00	77.5
$\frac{1}{2}$ = on Pav	6.90	77.6
+7.2 " West edge Pav.	7.00	77.5
$\frac{1}{2}$	7.6	76.9
cb.	8.5	75.0
M	8.7	75.8

PART 1

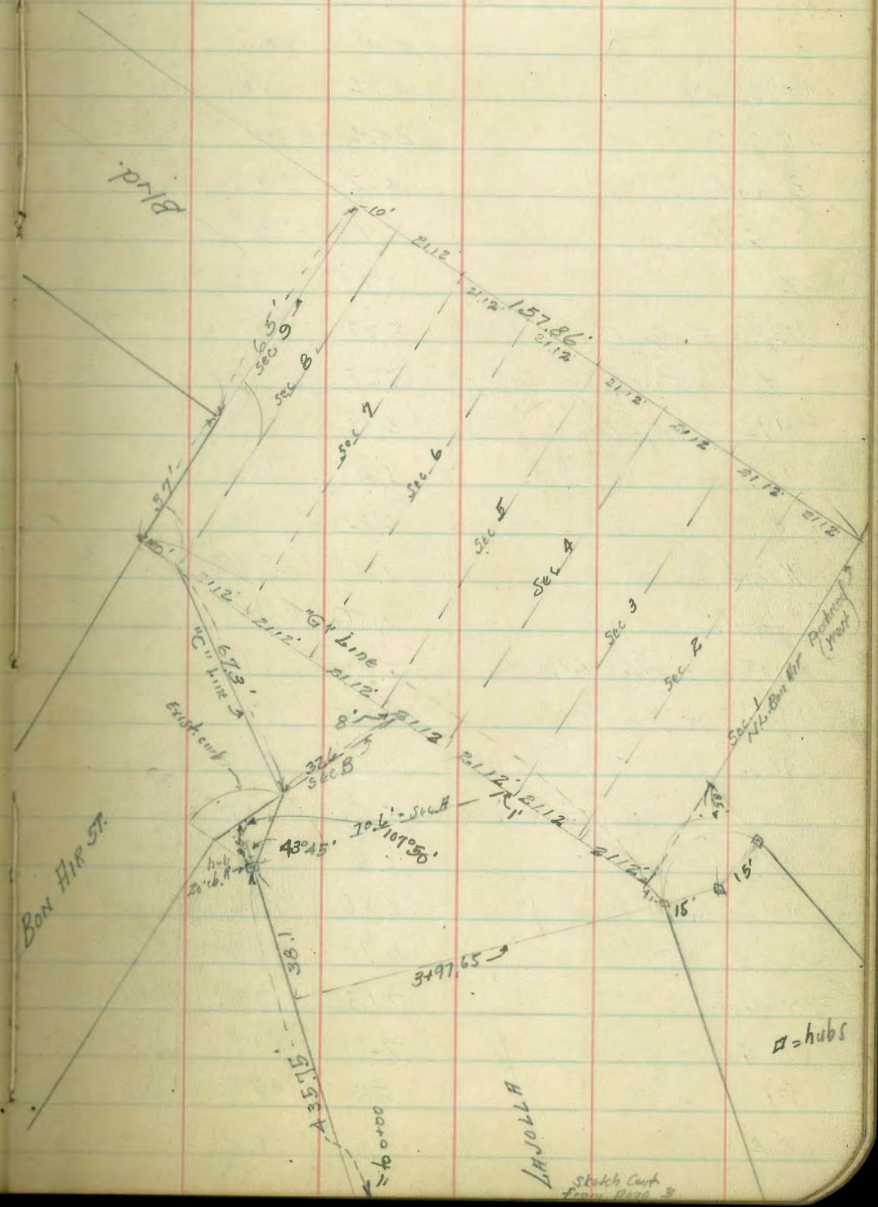
M	8.6	75.9
cb.	8.5	76.0
cb + G	8.5	76.0
$\frac{1}{2}$	7.3	77.2
+5	6.7	77.8
+7 = West edge Parking	6.75	77.7
$\frac{1}{2}$ on "	6.64	77.8
+12 " E " "	6.74	77.7
$\frac{1}{2}$	6.6	77.9
E Gut	6.7	77.8
" top cb.	5.84	78.6
+18" on West edge Walk	5.60	78.9
+18" E " "	5.58	78.9
E	5.1	79.4

PART 2

E	4.5	80.0
E+1 = top walk.	5.08	79.4



+6.012 W edge Walk	5.15	79.3
E top cb.	5.43	79.1
E Gut	6.5	78.0
$\frac{1}{2}$	6.4	78.1
+37" E edge Pav.	6.43	78.0
$\frac{1}{2}$ on " "	6.30	78.2
+82" W " "	6.42	78.0
+11	6.5	78.0
$\frac{1}{2}$	7.1	77.4
+13	8.3	76.2
cb.	8.3	76.2
W	8.0	76.5
PART 3		
W	8.6	75.9
cb	7.9	76.6
59" = on Riv. Sewer MH	7.23	77.2
$\frac{1}{2}$	6.6	77.9
+4	6.2	78.3
+6.2 on Wedge Pav.	6.11	78.4
$\frac{1}{2}$ " " "	6.00	78.5
+11.2 " E " "	6.12	78.3
$\frac{1}{2}$	6.0	78.5
E Gut.	6.2	78.3
• Top cb.	5.03	79.4
+13" on W edge Walk	4.79	79.7
+18.8" E " "	4.15	79.7



F	41	807
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PART 4

F	40	805
+1 ^m on walk	426	802
+6 ^d " "	436	801
F top ch.	462	798
" Gut.	57	789
$\frac{1}{2}$	57	788
+12' = E edge Pav.	579	787
$\frac{1}{2}$ on Pav.	567	788
-192 " W edge Pav.	579	787
+11	58	787
$\frac{1}{2}$	62	793
W Gut.	77	768
" top ch.	756	769
+135 on E edge Walk	728	772
+18.7 " " "	715	773
W	73	772

PART 5 = E.C.

W	68	777
+13 = top walk	686	776
+6.5 = " "	698	775
W top ch.	718	773
" Gut.	74	771
$\frac{1}{2}$	58	787
+4	55	790

+5.4 on W edge Par.ing	5.42	790
$\frac{1}{2}$ "	5.29	792
+10.3 " E " "	5.42	790
$\frac{1}{2}$	5.3	792
E Gut.	5.3	792
" top cb.	4.20	803
+13.6 = W edge walk	4.00	805
+18.8	3.87	806
E	3.4	811

section 6

E	3.6	809
" top walk	3.87	806
+6.2 "	3.95	805
E top cb.	4.18	803
" Gut.	5.3	792
$\frac{1}{2}$	5.0	795
+5 on E edge Par.	5.09	794
$\frac{1}{2}$ " "	4.97	795
+10 W " "	5.06	794
$\frac{1}{2}$	5.5	790
+10	6.8	777
W Gut.	7.0	775
" top cb.	6.69	778
+13.2 = E edge walk	6.56	779
+18.4 = W " "	6.00	780
W	6.6	779

S.L. Basement see sketch Page 1

W	6.0	78.5
W top cb.	6.65	77.8
" Gut.	7.0	77.5
+5	6.7	77.8
$\frac{1}{2}$	5.5	79.0
+5.1 = West edge Par.	5.05	79.4
$\frac{1}{2}$ on "	4.9	79.50
+10.1 " E " "	5.05	79.4
$\frac{1}{2}$	4.9	79.6
E Gut.	5.2	79.3
" top cb.	4.15	80.3
E	3.9	80.6

S cb. Basement - 1002

E top cb. at E.C.	4.05	80.4
" Gut. on Par.	4.68	79.8
cb.	5.1	79.4
$\frac{1}{2}$	5.0	79.5
+6.8 = E edge Par.	5.12	79.3
$\frac{1}{2}$ on "	4.96	79.5
+9 " W " "	5.07	79.4
W	5.1	79.4
$\frac{1}{2}$	5.4	79.1
W cb.	6.8	77.7
W Gut. on Par.	7.37	77.1
" top cb. at Prop.	6.76	77.7

S $\frac{1}{2}$ Basement = 100.3

X top Paring	706	774
cb	65	780
$\frac{1}{2}$	54	791
+4	51	794
+5.2 = West edge Par.	513	79.3
$\frac{1}{2}$ on " "	505	794
+10.2 = E " "	512	79.3
$\frac{1}{2}$	50	79.5
E cb.	51	79.4
+10	50	79.5
E top Paring	440	80.1
S Basement = 100.3		
E " "	429	80.2
" cb.	48	79.7
$\frac{1}{2}$	50	79.5
$\frac{1}{4}$ + 4.8 = East edge Paring	526	79.2
$\frac{1}{2}$ on " "	512	79.3
+9.8 = W " "	520	79.3
+11	52	79.3
$\frac{1}{2}$	54	79.1
cb.	63	78.2
W top Par	6.83	77.6
N $\frac{1}{2}$ Basement 100.35		
" "	705	77.4
cb.	64	78.1

$\frac{1}{2}$	56	78.9
+4	53	79.2
+5.2 on W edge Par.	530	79.2
$\frac{1}{2}$ " "	527	79.2
+10.2 = E " "	536	79.1
$\frac{1}{2}$	51	79.4
cb.	48	79.7
E top Par.	439	80.1
N cb. Basement = 100.3		
E " "	465	79.8
" top cb. at E.P.L.	411	80.4
" cb.	51	79.4
$\frac{1}{2}$	52	79.3
+4.8 = W Par.	512	79.0
$\frac{1}{2}$ on " "	529	79.2
+9.8 " "	539	79.1
+11	55	79.0
$\frac{1}{2}$	57	78.8
cb.	68	77.7
W top Par.	7.35	77.1
" " cb. at W.H.	670	77.8
N.L. Basement = 100.3		
W	64	78.1
+1 on Walk	642	78.0
W top cb.	671	77.8
" Gut.	7.0	77.5

$\frac{1}{2}$	5.8	787
+4	5.5	79.0
+5 ² on Pav.	5.50	79.0
$\frac{1}{2}$ " "	5.38	79.1
+10.2 " "	5.53	79.9
$\frac{1}{2}$	5.4	79.1
cb. on Gut	5.0	79.5
E top cb.	4.24	80.2
" " Walk	3.71	80.8
0+00		
E " "	3.71	80.8
" top cb.	4.25	80.2
" Gut	5.1	79.9
$\frac{1}{2}$	5.5	79.0
+5 on Pav.	5.59	78.9
$\frac{1}{2}$ " "	5.45	79.0
+10 " "	5.58	78.9
$\frac{1}{2}$	5.9	79.6
W Gut	7.3	77.2
" top cb.	6.80	77.7
W cb + 13.6 = E edge Walk	6.64	77.6
+18.8 = W " "	6.58	77.9
W	6.6	77.9
0+50		
W	7.4	77.1
+1 ² on Walk	7.18	77.3

+6.4 = Walk	7.26	77.2
W top cb.	7.43	77.0
" Gut	8.0	76.5
$\frac{1}{2}$	6.3	78.2
+5 = Pav.	6.27	78.2
$\frac{1}{2}$ = " "	6.16	78.3
+10 on Pav.	6.30	78.2
$\frac{1}{2}$	6.3	78.2
E	5.8	78.7
" top cb.	4.83	79.6
cb + 13.6 = Walk	4.63	79.8
E	4.5	80.0
1+00		
E	5.1	79.9
E top Walk	5.14	79.3
TP 3.61 21.09	6.98	77.48
E top cb.	2.13	79.0
" Gut	3.1	78.0
$\frac{1}{2}$	3.5	77.6
+5 on Pav.	3.56	77.65
$\frac{1}{2}$ " "	3.45	77.6
+10 " "	3.58	77.5
$\frac{1}{2}$	3.5	77.6
W cb. on Ground (in Pav.)	4.8	76.3
W	5.3	75.8
1+50		

8109

W	52	759
" top cb.	5.88	757
" Gut.	5.9	75.2
$\frac{1}{2}$	4.4	76.7
+5 on Pav.	4.18	76.9
$\frac{1}{2}$ " "	4.10	77.0
+10 " "	4.28	76.8
$\frac{1}{2}$	3.9	77.2
E Gut.	3.6	77.5
" top cb.	2.83	78.3
E cb + 13.6 = Walt	2.58	78.5
+18.8 = "	2.50	78.6
E	2.4	78.7
	Z+100	
F	31	780
+1.2 = Walt	3.14	78.0
E top cb.	3.45	77.6
" Gut.	4.4	76.7
$\frac{1}{2}$	4.9	76.2
+5 = Pav.	4.91	76.2
$\frac{1}{2}$ on "	4.74	76.4
+10 " "	4.82	76.3
$\frac{1}{2}$	5.0	76.1
W Gut.	6.6	74.5
" top cb.	6.06	75.0
W cb + 13.6 = Walt	5.84	75.3

8109

W	58	75.8
		Sketch Page 2
Z+10	5 = Pt. A to Lapolla Blvd. at SW. Kolimar St.	
W	5.9	75.2
+6.4 = top walk	5.96	75.1
W top cb.	6.15	74.9
" Gut.	6.6	74.5
$\frac{1}{2}$	5.2	75.9
+5 = W edge Pav.	5.01	76.1
$\frac{1}{2}$ on "	4.90	76.2
+10 " E " "	5.07	76.0
$\frac{1}{2}$	5.0	76.1
E Gut.	4.6	76.5
E top cb.	3.64	77.5
E	3.2	77.9
	S cb.	
E	3.4	77.7
" top cb.	3.76	77.3
" Gut.	4.8	76.3
$\frac{1}{2}$	5.1	76.0
+5 = E edge Pav.	5.24	75.9
$\frac{1}{2}$ = on "	5.08	76.0
+10 = W " "	5.18	75.9
$\frac{1}{2}$	5.3	75.8
cb.	6.6	74.5
W top cb.	6.20	74.9
" Gut. on Pav.	6.84	74.3

9

T.P.	318	78.10	617	74.90	74.92
	S $\frac{1}{4}$ Kolmar			SW. BR. Kolmar Lupilla. 84. 0.02 = Error	
N on top Paring			3.80	74.3	
cb.			3.3	74.8	
$\frac{1}{2}$			2.5	75.6	
+ 5 on N edge Par.			2.28	75.8	
L " "			2.17	75.9	
+10 " E " "			2.37	75.7	
$\frac{1}{2}$			2.3	75.8	
E Gut.			1.9	76.2	
" top cb.			0.88	77.2	
E			0.6	77.5	
	L Kolmar				
E			0.7	77.4	
" top cb.			0.93	77.2	
" Gut.			2.2	75.9	
$\frac{1}{2}$			2.5	75.6	
+ 5 = E edge Paring			2.42	75.7	
L = on " "			2.33	75.8	
+10 = N " "			2.39	75.7	
$\frac{1}{2}$			2.6	75.5	
cb.			3.2	74.9	
N on Paring			3.74	74.4	
	N $\frac{1}{4}$ Kolmar				
" " "			4.00	74.1	

cb.		3.4	74.7
$\frac{1}{2}$		2.7	75.4
+ 5 = N edge Par.		2.52	75.6
L on " "		2.40	75.7
+10 " E " "		2.53	75.6
$\frac{1}{2}$		2.5	75.6
E Gut.		2.1	76.0
" top cb.		1.04	77.1
E		1.0	77.1
	N cb.		
E		0.8	77.3
" top cb.		1.15	76.9
" Gut.		2.1	76.0
$\frac{1}{2}$		2.5	75.6
+10 = E edge Par.		2.64	75.5
L on " "		2.50	75.6
+10 " N " "		2.61	75.5
$\frac{1}{2}$		2.8	75.3
N cb.		3.8	74.3
N on Paring		4.45	73.7
N " top cb.		3.80	74.3
	2+61.54 = N.L. Kolmar		
N		3.6	74.5
" top cb.		3.70	74.4
" Gut		4.1	74.0
$\frac{1}{2}$		2.9	75.2

$\frac{7}{2} + 5 = \text{N edge Pav.}$	2.77	75.3
$\frac{1}{2}$ on "	2.65	75.4
+10 "E" "	2.79	75.3
$\frac{1}{4}$	2.6	75.5
E Gut.	2.3	75.8
" top ch.	1.39	76.7
E	1.1	77.0
3+00		
E	1.9	76.2
E Gut in Drive Way on Co.	2.92	75.2
$\frac{1}{2}$	3.5	74.6
+5 = E edge Pav.	3.57	74.5
$\frac{1}{2}$ on "	3.42	74.7
+10 "N" "	3.52	74.6
$\frac{1}{2}$	3.8	74.3
N Gut.	4.8	73.3
" top ch.	4.36	73.7
N	4.3	73.8
3+50		
N	5.0	73.1
" top ch.	5.17	72.9
" Gut	5.9	72.2
" $\frac{1}{2}$	4.8	73.3
+5 = N edge Pav.	4.56	73.5
$\frac{1}{2}$ on "	4.45	73.6
+10 = E " "	4.61	73.5

$\frac{1}{2}$	4.3	73.8
E Gut	4.2	73.9
" top ch.	4.40	73.7
E	3.7	74.9
4+00		
E	4.0	74.1
" top ch.	4.50	73.6
" Gut.	5.1	73.0
$\frac{1}{4}$	5.8	72.3
+5 = E edge Pav.	5.68	72.4
$\frac{1}{2}$ on "	5.57	72.5
+10 "N" "	5.71	72.4
$\frac{1}{2}$	5.9	72.2
N Gut.	7.0	71.1
" top ch.	6.41	71.7
"	6.2	71.9
4+50		
N	7.8	70.3
" top ch.	7.94	70.2
" Gut.	8.2	69.9
$\frac{1}{4}$	7.0	71.1
+5 = N edge Paving	6.92	71.2
$\frac{1}{2}$ on "	6.75	71.3
+10 = E " "	6.88	71.2
$\frac{1}{2}$	6.8	71.3
E Gut.	6.4	71.7

E top cb.	5.59	72.5
E	5.1	73.0
4+80.70 = Pt. A to Laptha Blvd of SW. Cor. Granville St		
E	6.0	72.1
" top cb.	6.31	71.8
" Gut.	7.2	70.9
$\frac{1}{2}$	7.4	70.7
+5 = E edge Pav.	7.62	70.5
L on "	7.54	70.6
+10 " " "	7.65	70.4
$\frac{1}{2}$	7.7	70.4
W Gut.	9.0	69.1
" top cb.	9.00	69.1
W	8.8	69.3
S. to Granville St. = 101.6 see sketch Page 2		
W	8.8	69.3
" top cb.	9.12	69.0
$\frac{1}{2}$	7.8	70.3
+5.2 = Pav. ^{W edge}	7.84	70.3
L on "	7.95	70.3
+10.2 = E edge Pav.	7.90	70.2
$\frac{1}{2}$	7.6	70.5
E Gut.	7.5	70.6
" top cb.	6.60	71.5
E	6.5	71.6
S. to Granville = 101.3		

E top cb.	6.65	71.4
E Gut. on Pav.	7.25	70.8
E "	7.6	70.5
$\frac{1}{2}$	7.9	70.2
+5.2 = E edge Pav.	8.01	70.1
L on "	7.96	70.1
+10.2 " " "	8.04	70.1
$\frac{1}{2}$	8.0	70.1
cb.	8.9	69.2
W Gut. on Pav.	7.88	68.2
" top cb.	7.14	69.0
S to Granville St. = 100.7		
W Gut. on Pav.	7.48	68.6
cb.	8.6	69.5
$\frac{1}{2}$	8.2	69.9
+5.1 = Pav.	8.11	70.0
L on "	8.07	70.0
+10.1 " "	8.12	70.0
$\frac{1}{2}$	8.0	70.1
cb.	7.8	70.3
E top Pav.	7.02	71.1
S. to Granville = 100.10		
E "	6.88	71.2
cb.	7.7	70.4
$\frac{1}{2}$	8.1	70.6
+5 = Pav.	8.38	69.7

7810

L on Pav.	8.25	69.8
+10 " N edge	8.32	69.8
$\frac{1}{4}$	8.3	69.8
cb	8.9	69.2
N on Pav.	9.27	68.8
N $\frac{1}{4}$ Gwalla = 99.9'		
N on Pav.	9.43	68.7
cb	9.2	68.9
$\frac{1}{4}$	8.4	69.7
+5 on Pav.	8.44	69.7
L " "	8.38	69.7
+10 " "	8.50	69.6
$\frac{1}{4}$	8.4	69.7
cb	7.8	70.3
E top Pav.	7.02	71.1
N cb. = 99.2'		
E top cb.	6.62	71.5
E Gut. on Pav.	7.30	70.8
cb	8.1	70.0
$\frac{1}{4}$	8.6	69.5
+6.0 E edge Paring	8.65	69.4
L on "	8.52	69.6
+11.3 " " "	8.60	69.5
$\frac{1}{4}$	8.6	69.5
cb	9.4	68.7
N Gut.	9.85	68.2

7810

13

N top cb.	9.25	68.8
N. L. = 101.4'		
N	9.1	69.0
" top cb.	9.23	68.9
" Gut.	9.7	68.4
$\frac{1}{4}$	8.9	69.2
+5.2 = Pav.	8.80	69.3
L = on "	8.78	69.3
10.2 = " E edge Pav.	8.96	69.1
$\frac{1}{4}$	9.0	69.1
+10	8.8	69.3
E Gut.	7.7	70.4
E top cb.	6.74	71.4
E	6.4	71.7
0 + 00		
E	6.4	71.7
" top cb.	6.78	71.3
" Gut.	7.7	71.4
+5	8.9	69.2
$\frac{1}{4}$	9.3	68.8
+5 on Pav.	9.18	68.9
L " "	9.08	69.0
+10 " "	9.07	69.0
$\frac{1}{4}$	9.2	68.9
N Gut.	10.1	68.0
" top cb.	9.71	68.4

X		9.7	68.1
chk. on N.W. B.P. La Salle rd + Gravelle		9.23	68.87
T.P.	138	68.65	10.83
	0+20		
X		1.0	67.7
+18 = Gut. in Drive Way		1.5	67.2
cb.		1.5	67.2
$\frac{1}{2}$		0.3	68.4
+5 = on Pav.		0.19	68.5
$\frac{1}{2}$ " "		0.32	68.3
+10 " "		0.50	68.2
$\frac{1}{2}$		0.6	68.1
+8		0.6	68.1
cb.		+1.1	69.8
E		+1.0	69.7
+5		+1.0	69.7
	0+40		
E		+0.4	69.1
+16		0.0	68.7
cb.		0.4	68.3
+5		1.0	67.7
+6		1.6	67.1
$\frac{1}{2}$		1.4	67.3
+5 = Pav.		1.30	67.4
$\frac{1}{2}$ " "		1.00	67.7
+10 = "		0.78	67.9

$\frac{1}{2}$		0.9	68.8
cb.		2.0	66.7
+7 on Gut of cb.		2.0	66.7
+7 " top cb.		1.64	67.0
X		1.6	67.1
	0+58.5		
X		2.9	65.8
+3' on top cb.		2.57	66.1
+3' " Gut. on Pav.		3.53	65.1
cb.		2.6	66.1
$\frac{1}{2}$		1.3	67.4
+5 on Pav.		1.80	67.4
$\frac{1}{2}$ " "		1.60	67.1
+10 " "		2.00	66.7
$\frac{1}{2}$		2.3	66.4
+10		2.3	66.4
+11		1.5	67.2
cb.		0.8	67.9
+13		0.0	68.7
E		0.0	68.7
	0+75		
E		0.2	68.5
+6		0.8	67.9
+10		1.5	67.2
cb.		1.6	67.1
+2		1.9	66.8

+0	3.0	65.7
$\frac{1}{2}$	3.0	65.7
+15 = on Pav. (East edge)	2.78	65.9
$\frac{1}{2}$ " "	2.30	66.4
+10 " "	1.88	66.8
$\frac{1}{2}$	1.8	66.9
cb.	3.0	65.7
+16 = on Paving Along Del sur of	4.03	64.6
X - " " " " "	4.15	64.5
1+00		
X on Pav.	5.06	63.6
+55 "	4.92	63.7
cb.	3.7	65.0
$\frac{1}{2}$	2.5	66.2
+6 on X edge Pav.	2.62	66.0
$\frac{1}{2}$ " " "	3.06	65.6
+11 " E " "	3.64	65.0
$\frac{1}{2}$	3.7	65.0
+13	3.8	64.9
cb.	3.0	65.7
+15	2.0	66.7
E	1.2	67.5
1+36.8 = Δ on E		
E 0	3.8	64.9
+8 on Walk	4.0	64.7
+9	4.4	64.3

cb.	5.0	63.7
+135 = East edge Pav.	4.81	63.9
$\frac{1}{2}$ on " "	4.72	64.0
$\frac{1}{2}$ " " "	3.92	64.7
+4 " X " "	3.76	64.9
$\frac{1}{2}$	4.1	64.6
cb.	5.7	63.0
+12 on Pav.	6.17	62.5
X	6.67	62.0
T.P. 001 68.45	0.21	68.44
Section A = on Director of Angle sketch Page 3		
X	6.0	62.5
+182 = top cb.	5.71	62.8
cb.	6.1	62.4
$\frac{1}{2}$	4.6	63.9
$\frac{1}{2}$ = West edge Paving	3.92	64.5
$\frac{1}{2}$ on " "	4.64	63.8
+15 " E " "	4.90	63.6
cb.	5.0	63.5
+14 = Exist cb. on Gut	4.3	64.2
+14 = " " " top	3.88	64.6
E on Walk	3.72	64.7
0+00		
E	3.72	64.7
+9 = Exist cb.	3.96	64.5
+9 on Gut	4.4	64.1

17 White Post

E cb.	50	63.5
+138 = E edge Par.	512	63.3
$\frac{1}{2}$ on "	508	63.4
$\frac{1}{2}$ " "	4.45	64.00
+4 = W edge "	4.33	64.1
$\frac{1}{2}$	4.7	63.8
cb.	5.6	62.9
W	5.6	62.9
+10	10.7	57.8

0+225

-20	21.0	47.5
-10	18.9	49.6
W	12.5	56.0
+15	5.4	63.1
cb.	5.0	63.5
$\frac{1}{2}$	4.8	63.7
+7.4 = W edge Paring	4.83	63.6
$\frac{1}{2}$ on "	512	63.3
+12.5 "E " "	5.68	62.8
$\frac{1}{2}$	5.5	63.0
cb.	5.4	63.1
+5	5.2	63.3
E	3.6	64.9

0+42

E	3.2	65.3
cb.	5.2	63.3

+2	5.7	62.8
$\frac{1}{2}$	5.8	62.7
+5 on Paring	5.94	62.5
$\frac{1}{2}$ " "	5.46	63.0
+10 " "	5.08	62.4
$\frac{1}{2}$	4.9	63.6
+2	5.4	63.1
+5	6.7	61.8
cb	10.4	58.1
+2	11.1	57.4
+5	13.8	54.7
W	17.5	51.0
+15	22.0	46.5
+25	21.5	47.0

0+62

-15	18.2	50.3
-5	22.0	46.5
W	21.7	41.8
cb.	13.0	55.5
+10	6.1	62.4
$\frac{1}{2}$	4.8	63.7
+5 on W edge Paring	5.04	63.4
$\frac{1}{2}$ " "	5.50	63.0
+10 "E " "	5.72	62
$\frac{1}{2}$	5.6	62.9
+9	6.2	62.3

cb.	4.8	63.7
E	3.6	64.9
	0+90	
-5	8.7	59.8
E	8.1	65.4
cb.	6.6	62.9
+5	6.6	61.9
+7	5.1	63.4
$\frac{1}{4}$	5.2	63.3
+5 on Pav.	5.53	62.9
$\frac{1}{2}$ " "	5.19	63.3
+10 " "	4.81	63.6
$\frac{1}{4}$	4.7	63.8
+2	6.4	62.1
+8	11.4	57.1
cb.	12.7	56.8
+10	22.0	46.5
H	21.3	47.2
+5	16.6	51.9
	1+08	
-H	14.4	54.1
+4	15.5	53.0
+7	12.0	49.5
cb.	16.1	52.4
+10	6.3	62.2
$\frac{1}{4}$	4.8	63.7

+5 on Pav	4.72	63.7
$\frac{1}{2}$ " "	5.02	63.4
+10 " "	5.48	63.0
$\frac{1}{4}$	5.8	63.2
+7	5.4	63.1
cb.	11.0	57.5
+4	14.7	53.8
E	15.1	53.4
+15	13.3	55.2
	1+28	
- 15	12.5	55.0
E	13.5	55.0
+7	10.0	58.5
cb.	8.7	59.8
+11	4.8	63.7
$\frac{1}{2}$	5.0	63.5
+5 on Pav	5.15	63.3
$\frac{1}{2}$ " "	4.93	63.5
+10 " "	4.57	63.9
$\frac{1}{4}$	4.5	64.0
+2	5.9	62.6
+13	14.8	53.7
cb.	14.8	53.7
+11	15.6	52.9
+13	12.9	55.6
H	10.8	57.9

1+50

X		54	63.1	
+6		6.0	62.5	
cb.		10.8	57.7	
+8		68	61.7	
+13		44	64.1	
$\frac{1}{2}$		44	64.1	
+5 = Pav.		4.29	64.2	
$\frac{1}{2}$ on Pav.		4.45	64.6	
+10 " "		4.68	63.8	
$\frac{1}{2}$		4.6	63.9	
+12		4.6	63.9	
cb.		7.8	61.2	
+7		8.7	59.8	
+17		12.9	55.6	
E		13.0	55.5	
+15		12.5	56.0	
T.P.	1.17	69.61	0.01	68.44
	1+65			
-15		13.1	56.5	
E		13.6	56.0	
+10		13.6	56.0	
+18		7.6	62.0	
cb.		7.1	62.5	
+10		5.6	64.0	
$\frac{1}{2}$		5.6	64.0	

+5 = E edge Pav.		5.37	64.0
$\frac{1}{2}$ on " "		5.27	64.3
+10 " " "		5.28	64.3
$\frac{1}{2}$		5.1	64.5
+5		6.0	63.6
+7		9.5	60.1
cb.		6.2	63.4
X		6.0	63.6
	1+77		
X		6.0	63.6
cb.		5.5	64.1
$\frac{1}{2}$		5.1	64.5
+5 = Pav.		5.18	64.4
$\frac{1}{2}$ = on " "		5.08	64.5
+10 " "		5.33	64.3
$\frac{1}{2}$		5.4	64.2
cb.		6.3	63.3
+13		13.6	56.0
E		13.8	55.8
+15		11.8	57.8
+27 = top 6" Sewer in Alley		7.27	60.3
+27 = on Ground at above Sewer		11.9	57.7
	1+94		
-18 on top Above 6" Sewer		9.02	60.6
-18 " Ground at Sewer		11.6	58.0
-6		12.4	57.2

on Trestle

E	9.9	59.7
+12	4.9	64.7
cb.	4.7	64.9
$\frac{1}{2}$	5.1	64.5
+5 = Parking	4.88	64.7
$\frac{1}{2}$ = "	4.80	64.8
+10 = "	4.85	64.7
$\frac{1}{2}$	5.0	64.6
cb.	5.3	64.3
X	5.5	64.1

2+00

X	5.2	64.4
cb.	5.1	64.5
$\frac{1}{2}$	4.9	64.7
+5 = Pav.	4.84	64.8
$\frac{1}{2}$ = "	4.70	64.9
+10 = "	4.77	64.8
$\frac{1}{2}$	5.0	64.6
cb.	4.7	64.9
+8	4.8	65.3
E	7.4	62.2
+14 = top Sewer ^{Pipe} in Alley	8.90	60.7
+14 = Ground at Sewer ^{top Pipe}	10.5	59.1
2+05 = Approx. end Sewer Trestle	8.80	60.8

2+15

-20	9.8	59.8
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Ground
Same Elev.

-8	6.1	63.5
E	4.0	65.6
cb.	4.8	64.8
$\frac{1}{2}$	4.8	65.1
+5 = Pav.	4.36	65.2
$\frac{1}{2}$ = "	4.80	65.3
+10 = Pav.	4.43	65.2
$\frac{1}{2}$	4.6	65.0
cb.	4.9	64.7
X	5.2	64.4

2+30

X	5.1	64.5
cb.	4.7	64.9
$\frac{1}{2}$	4.2	65.4
+5 = Pav.	4.04	65.6
$\frac{1}{2}$ = "	3.88	65.7
+10 = "	3.96	65.6
$\frac{1}{2}$	4.2	65.4
cb.	4.5	65.1
+13	3.9	65.7
E	5.2	64.4
+10	9.3	60.3

2+41.8 = Intersection N.P.L. La Salle Blvd. and X curb. Line Plaza Del Nor St.
top cb. = 4.36

2+50

-15	9.7	59.9
E	10.1	59.5

+10	4.3	65.3
cb.	3.8	65.8
$\frac{1}{2}$	3.7	65.9
+5 = Pav.	3.53	66.1
$\frac{1}{2}$ on "	3.41	66.2
+10 " "	3.54	66.1
$\frac{1}{2}$	3.7	65.9
cb.	4.4	65.2
+16.5 Gut of curb.	4.6	65.0
+16.5 = top cb.	4.05	65.5
$\frac{1}{2}$ on Walk.	4.05	65.5
2+65		
$\frac{1}{2}$	3.5	66.1
+10.3 = top cb.	3.51	66.1
+10.3 on Gut.	4.0	65.6
cb.	4.1	65.5
$\frac{1}{2}$	3.5	66.1
+5 = Pav.	3.14	66.5
$\frac{1}{2}$ = "	3.06	66.5
+10 = "	3.15	66.4
$\frac{1}{2}$	3.4	66.2
+7	3.5	66.1
+11	2.1	67.5
cb.	4.3	65.3
+5	8.0	61.6
+10	9.3	60.3

E	9.3	60.3
+15	8.0	61.6
2+82		
-10	6.7	62.9
E	6.8	62.8
+15	8.0	61.6
cb.	5.2	64.4
+7	3.2	66.4
$\frac{1}{2}$	3.0	66.6
+5 = Pav.	2.69	66.9
$\frac{1}{2}$ = "	2.58	67.0
+10 = "	2.72	66.9
$\frac{1}{2}$	3.0	66.6
cb.	3.4	66.2
+4.6 = Gut	3.4	66.2
+4.6 = top cb.	2.94	66.7
$\frac{1}{2}$	3.0	66.6
3+00		
$\frac{1}{2}$	1.9	67.7
+5	2.8	66.8
+19 = top cb.	2.24	67.4
+19 = Gut.	2.7	66.9
cb.	2.7	66.9
+5	3.3	66.3
$\frac{1}{2}$	2.5	67.1
+5 = Pav.	2.24	67.4

6961

$\frac{1}{2}$ = Pav		2.13	67.5
+10 = "		2.23	67.4
$\frac{1}{2}$		2.6	67.0
+6		2.7	66.9
+10		2.0	67.6
cb.		2.1	66.5
+8		4.2	65.4
E		4.3	65.3
+4		5.4	64.2
+8		5.1	64.5
+13		1.7	67.9
T.P.	6.85 74.40	2.06	17.55
	3+15		
-10		6.5	67.9
-8		2.0	65.4
E		9.0	65.4
+3		6.3	68.1
+15		5.8	68.6
cb		6.2	68.2
+7		4.8	67.6
$\frac{1}{2}$		7.0	67.4
+5 = Pav		6.62	67.8
$\frac{1}{2}$ on "		6.56	67.8
+10 " "		6.64	67.8
$\frac{1}{2}$		6.7	67.7
+11		7.8	66.6

7440

21

cb.		7.1	67.3
+0.2 = top cb.		6.52	67.9
+1.3		7.2	67.2
W		6.1	68.3
3+20.4 = End of Exist Curve on W		6.34	68.1
	3+50		
W		5.6	68.8
+4		6.2	68.2
cb.		6.0	68.4
+2		5.8	68.6
+5		7.2	67.2
+8		6.8	67.6
+9		6.2	68.2
$\frac{1}{2}$		5.8	68.6
+5 = Pav		5.71	68.7
$\frac{1}{2}$ = "		5.58	68.8
+10 = "		5.64	68.8
$\frac{1}{2}$		5.8	68.6
+6		5.7	68.7
+11		5.0	69.4
cb.		5.1	69.3
+8		5.7	68.7
+15		3.8	70.6
E		4.0	70.7
+5		4.3	70.1

Please Del Nor. St.

3+97.65 See sketch Page 4

-5	2.6	71.8
E	2.6	71.8
+9	3.3	71.1
cb	3.7	70.7
+5	4.3	70.1
$\frac{1}{2}$	4.5	69.9
+5 = Par.	4.36	70.0
L	4.21	70.2
+10 = "	4.43	70.0
$\frac{1}{2}$	4.5	69.9
+8	4.7	69.7
+10	5.8	68.6
cb	5.4	69.0
+2	4.4	70.0
M	4.1	70.3
TP	6.64	78.64
	2.40	72.00
	6.8	71.8
+20 = cb	7.2	71.4
cb + 3	9.3	69.3
+9	9.1	69.5
+12	7.9	70.7
$\frac{1}{2}$	7.7	70.9
+5 = M edge Paring	7.83	70.8
L on "	7.43	71.2
+10 = E "	7.34	71.3

Section H = 70.6' see sketch Page 4

$\frac{1}{2}$	7.4	71.2
+5.6 = "G" Line	7.7	70.9
	Sec B = 37.6'	
"G" Line on Par.	6.85	71.8
+10.3 " "	7.33	71.3
+20	7.50	71.1
+30	7.61	71.0
+37.6 = gutter on Par. at cb.	7.59	71.0
+37.6 " top cb.	7.05	71.6
	Section I = 102'	
"G" Line	7.1	71.5
+10.2	7.1	71.5
+20.4	6.9	71.7
+30.6	6.3	72.3
+40.8	5.5	73.1
+51 = d	5.0	73.6
+61.2	4.2	74.4
+71.4	3.8	74.8
+77.4 = West edge Paring	4.3	74.3
+81.6	4.5	74.1
+91.8	4.6	74.0
+97.6 = E Gut.	4.3	74.3
+97.6 = E Top cb.	3.85	74.8
+102	3.1	74.8
	Sec. E	
E	3.7	74.9

+3.2 = top E.ck.	3.81	748
+3.2 = Gut.	4.3	743
+10.2	13	743
+20.4	44	742
+24.2 = N edge Pav.	44	742
+30.6	48	738
+40.8	45	741
+51	56	730
+61.2	58	728
+71.4	70	716
+81.6	77	709
+91.8	78	70.8
1+0.2 = "6" Line	83	703

Section 3

"6" Line	7.8	708
+10.2	7.8	708
+20.4	6.8	71.8
+30.6	7.7	70.9
+40.8	6.1	72.5
+51	4.9	73.7
+61.2	51	73.5
+71.4	4.7	73.9
+77.4 = Pav.	44	74.2
+81.6	4.2	74.4
+91.8	4.2	74.4
+97.6 = Gut.		

+97.6 = E Gut.	4.3	74.3
+97.6 = E top ck.	3.77	74.8
1+0.2 = E	3.7	74.9
Section 4		
E	3.6	75.0
+3.2 = E top ck.	3.70	74.9
+3 Gut.	4.2	74.4
E+10.2	4.2	74.4
+20.4	4.1	74.5
+24.6 = N edge Pav.	4.4	74.2
+30.6	5.0	73.6
+40.8	5.1	73.5
+51	5.4	73.2
+61.2	5.7	73.4
+71.4	6.1	72.5
+81.6	6.2	72.4
+91.8	6.7	71.9
+97.6 = E edge Pav.	6.78	71.8
1+0.2 = "6" on Pav.	6.86	71.8

Section 5

1-21 = Edge Paving Intersection	7.50	71.1
"6" on Pav.	7.20	71.4
"8"	6.87	71.8
+10.2	6.39	72.2
+20.2 = E edge Paving	5.83	72.8
+30.6	5.8	72.8

+408	52	737
+51	51	735
+612	45	741
+714	43	743
+816	38	748
+918	39	747
+976 = E Gut.	40	746
+976 = "top ch	352	731
+102	35	731

Section 6

E	31	755
+32 = E top ch	32	754
+32 = " Gut.	37	749
+102	37	749
+204	37	749
+306	37	749
+408	41	745
+51	43	743
+612	46	740
+657 = E edge ^(Highway) Parking	489	737
+714 on "	530	733
+816 "	597	726
+918 "	659	721
+102 = "G"	691	717
"G" + 5 "	699	716
"G" + 25.5 = "C" line on Pav.	693	717

Section 7

"G" - 128 = C line on Pav.	601	726
"G" line on Pav.	605	726
+102 " "	607	726
+204 " "	619	724
+306 " "	584	728
+408 " "	504	736
+51 " "	430	743
+56 = E edge Highway Pav.	425	744
+612	42	744
+714	38	748
+816	36	750
+918	36	750
+976 = E Gut.	36	750
+976 = "top ch	310	755
+102 = E	30	756

Section 8 = N Ch. line Bon. Riv. on West.

E	27	749
+32 = E top ch. IN DRIVE way	34	752
+32 = " Gut.	34	752
+102	34	752
+204	35	751
+306	37	749
+372 = E edge Highway Parking	391	747
+408	408	746
+51	494	737

+61.2 on Pav.	553	731
+61.2 on top ch. paving	569	739
+71.4 on Pav	545	732
+81.6 " "	568	730
+91.8 " "	583	728
1+02 = Gut on Pav. at C Line = 6" hump	605	726
1+02 = top ch. at C line	551	
Section 2 = 0+00	{ 10' ch. } { 11.25' ch. }	From 0+00 to Belvedere
-37	50	736
-20	46	740
X on Walk	416	745
X top ch.	460	740
"Gut"	53	733
$\frac{1}{2}$	448	741
+10.5 = Edge Highway Paving	379	749
$\frac{1}{2}$	38	748
$\frac{1}{2}$	35	751
ch	33	753
+6.5 = gutter at exist ch.	33	753
+6.5 = top " "	279	758
E " Walk	265	760
	0+50	
E	23	763
+3.5 = top exist ch	235	763
+3.5 = Gut. at " "	27	759
ch	28	758

$\frac{1}{2}$	30	756
+1.2 = Edge Paving	296	757
$\frac{1}{2}$ on " "	376	749
+10 = X " "	454	741
$\frac{1}{2}$	46	740
+2	46	740
+7	40	746
ch	38	748
X	36	750
	0+70 = N.L. Hilley on E	
X	33	753
ch	36	750
$\frac{1}{2}$	41	745
+12.5 = Edge Paving	411	745
$\frac{1}{2}$ on " "	345	752
+10 = E " "	290	757
$\frac{1}{2}$	29	757
E Gut	26	760
E top ch.	222	764
E " " at line	200	766
	1+00	
E	19	767
E top ch.	215	765
" Gut.	26	760
$\frac{1}{2}$	27	759
+11.25 = Paving	271	759

78.64

$\frac{1}{2}$ on Pav.	3.19	75.4
+ 10" W edge Pav.	3.60	75.0
$\frac{1}{2}$	3.5	75.1
cb.	3.2	75.4
+ 5	2.8	75.8
W	2.8	75.8
1+25		
W	2.6	76.0
cb.	2.7	75.9
$\frac{1}{2}$	3.3	75.3
+ 1.7 - Pav.	3.24	75.4
$\frac{1}{2}$ on "	2.87	75.8
+ 10" "	2.55	76.1
$\frac{1}{4}$	2.5	76.1
E Gut	2.5	76.1
" top cb.	1.87	76.8
E	1.7	76.9
TR	6.59	83.30
1+27		
E	6.3	77.1
" top cb.	6.50	76.8
E Gut.	6.9	76.4
$\frac{1}{4}$	7.1	76.2
+ 12.5 - Pav.	7.19	76.1
L on "	7.50	75.8
+ 10 "	7.89	75.5

83.30

26

$\frac{1}{2}$	7.9	75.4
+ 6	7.8	75.5
+ 9	6.2	77.1
cb.	5.7	77.6
W	6.4	76.9
1+75		
W	6.1	77.2
cb.	5.6	77.7
+ 3	5.4	77.9
+ 6	7.6	75.7
$\frac{1}{2}$	7.3	76.0
+ 1.2 = Pav.	7.05	76.2
L on "	6.83	76.5
+ 10 " "	6.83	76.5
$\frac{1}{2}$	6.8	76.5
Gut	6.6	76.7
E top cb.	6.16	77.1
E	6.0	77.3
2+05		
E	5.8	77.5
E top cb.	6.03	77.3
" Gut.	6.7	77.1
$\frac{1}{2}$	6.6	76.7
+ 1.9 = Pav.	6.53	76.8
L on "	6.61	76.7
+ 10 "	6.75	76.5

z	6.8	76.5
+7	6.8	76.5
+9	5.0	76.3
cb.	5.1	76.2
Y	5.9	77.4
	2+2.5	
Y	6.2	77.1
cb.	6.3	77.0
$\frac{1}{2}$	6.5	76.8
+1.2 = Par.	6.5	76.8
E on "	6.38	76.9
+10 " "	6.37	76.9
z	6.4	76.9
Gut.	6.3	77.0
E top cb	5.90	77.4
E	5.7	77.6
	2+4.5 = Beginning Fresh ch and walk on Y	
E	5.6	77.7
" top cb	5.73	77.6
" Gut.	6.3	77.0
z	6.2	77.1
+1.2 = Par.	6.26	77.0
6 on "	6.14	77.2
+10 " "	6.27	77.0
$\frac{1}{2}$	6.3	77.0
Y top cb	6.19	77.1

Y on top walk		6.04	77.3	
		{ 12' CBS on E } 10' CBS on Y		
		{ 9' 25 " " } 10' 25 " Y		
2+7.5 = S.L. Nautilus st.				
Y on walk		6.01	77.3	
" top cb		5.90	77.4	
" Gut. on Par.		6.40	76.9	
$\frac{1}{2}$ " "		5.92	77.4	
$\frac{1}{2}$ " "		5.81	77.5	
$\frac{1}{4}$ " "		5.79	77.5	
E Gut. on "		6.13	77.2	
" top cb		5.52	77.8	
E " Walk.		5.34	77.0	
TP	3.57	83.76	3.11	80.19
				Mail in file on Y Bot. Nautilus and Yesthorne st.
				N.L. NAUTILUS st. = 0+00
E		5.3	78.5	
E top cb		5.48	78.3	
" Gut. on Par.		6.04	77.7	
$\frac{1}{2}$ " "		5.89	77.9	
$\frac{1}{2}$ " "		5.76	78.0	
$\frac{1}{4}$ " "		5.85	77.9	
Y Gut " "		6.35	77.4	
" top cb		5.85	77.9	
Y		5.9	77.9	
				0+50
Y		5.4	78.4	
cb.		5.4	78.4	
$\frac{1}{2}$		5.8	78.0	

+1.15 = W. adp. Pav.	5.66	781
L on Pav.	5.56	782
+ " "	5.65	781
$\frac{1}{2}$	5.6	782
E Gut. (in Drive)	5.5	783
E	5.1	787
1+00		
E	4.8	790
cb.	5.17	786
Gut.	5.1	784
$\frac{1}{2}$	5.4	784
+1.15 = Pav.	5.43	783
L on "	5.34	784
+10 " "	5.45	783
$\frac{1}{2}$	5.4	784
cb.	5.2	786
W	5.1	787
1+50		
W	5.1	787
cb.	5.2	786
$\frac{1}{2}$	5.2	786
+1.15 = Pav.	5.30	785
L on "	5.17	786
+10 " "	5.33	784
$\frac{1}{2}$	5.2	786
E Gut.	4.8	79.0

E top cb.	4.90	789
E	4.6	79.2
2+00		
E	4.6	79.2
cb.	4.74	79.0
Gut.	4.9	78.9
$\frac{1}{2}$	5.0	78.8
+1.15 = Pav.	5.04	78.7
L on "	4.96	78.8
+10 " "	5.06	78.7
$\frac{1}{2}$	4.9	78.9
cb.	4.9	78.9
W	5.0	78.8
2+50		
W	5.0	78.8
cb.	5.0	78.8
$\frac{1}{2}$	4.7	79.1
+1.15 Pav.	4.87	78.9
L on "	4.76	79.0
+10 " "	4.99	78.8
$\frac{1}{2}$	5.0	78.8
Gut.	5.0	78.8
E top cb.	4.57	79.2
E	4.3	79.5
2+69.5 = Sh. Harbourne sh on West.		
E	4.3	79.5

E topcb	4.53	79.2
" Gut.	4.9	78.9
$\frac{1}{2}$	5.0	78.8
+1.15 = Pav.	4.90	78.9
$\frac{1}{2}$ on "	4.75	79.0
+10 " "	4.82	79.0
$\frac{1}{2}$	4.7	79.1
cb.	4.6	79.2
W	4.9	78.9
2+81.5 = $\frac{1}{2}$ Fire Hydr. on W 1.3' Back of line to pole end		
3+09.5 = $\frac{1}{2}$ Westbourne on W		
W	5.1	78.7
cb	4.8	79.0
$\frac{1}{2}$	4.9	78.9
+1.15 = Pav.	5.08	78.7
$\frac{1}{2}$ on "	4.95	78.8
+10 " "	5.00	78.8
$\frac{1}{2}$	4.9	78.9
Gut.	5.0	78.8
E cb.	4.74	79.0
E	4.4	79.4
3+46.9 = S.W. Westbourne on E		
E	4.5	79.3
" topcb	4.93	78.8
" Gut. on Pav.	5.44	78.3
$\frac{1}{2}$ " "	5.24	78.5

$\frac{1}{2}$ on Pav.	5.19	78.6
+10 " "	5.33	78.4
$\frac{1}{2}$	5.3	78.5
cb.	5.4	78.4
W	5.4	78.4
$\frac{1}{2}$ Westbourne on E		
W	5.5	78.3
" topcb	5.85	77.9
Gut	6.2	77.6
$\frac{1}{2}$	5.7	78.1
+1 = Pav.	5.76	78.0
$\frac{1}{2}$ on "	5.61	78.2
+10 " "	5.61	78.2
$\frac{1}{2}$ " "	5.61	78.2
Gut. " "	5.84	77.9
E " "	5.39	78.4
N.L. Westbourne on E = 0+00		
E	5.4	78.4
" topcb	5.65	78.1
" Gut.	6.24	77.5
$\frac{1}{2}$ on Pav.	6.21	77.6
+1 " "	6.16	77.6
$\frac{1}{2}$ " "	6.05	77.7
+10 " "	6.22	77.5
$\frac{1}{2}$	6.3	77.5
Gut.	7.1	76.7

Y top cb.	6.25	77.5
Y	6.0	77.8
chk. on SE. B.P. Lapilla + Westberre	4.75	79.01 ✓
T.P. 2.41	79.74	6.43
	0 + 0.3	77.33
Y	2.0	72.7
cb.	2.28	77.6
Gut.	3.1	76.6
$\frac{1}{2}$	2.3	77.4
+1 = Y edge Pav.	2.26	77.5
L on "	2.12	77.6
+10 " E " "	2.21	77.5
$\frac{1}{2}$	2.2	77.5
+6	2.2	77.5
+7	+0.3	79.4
cb.	+0.3	79.4
E	+0.5	79.2
	0 + 50	
E	0.2	79.5
cb.	0.3	79.4
+6	1.1	78.6
+7	2.9	76.8
$\frac{1}{2}$	3.1	76.6
+1 = Pav.	2.94	76.8
L on "	2.88	76.9
+10 " "	3.04	76.7

$\frac{1}{2}$	3.1	76.6
Gut.	4.1	75.6
cb.	3.01	76.7
Y	2.8	76.9
	1 + 0.0	
Y	3.8	75.9
cb.	3.82	75.9
Gut.	4.5	75.2
$\frac{1}{2}$	4.0	75.7
+1 = Pav.	3.81	75.9
L on "	3.66	76.1
+10 " "	3.75	76.0
$\frac{1}{2}$	3.8	75.9
+5	3.9	75.8
+6	2.3	77.4
cb.	1.3	79.4
E	0.9	78.8
	1 + 50	
E	2.0	77.7
cb.	2.1	77.6
+5	2.6	77.1
+6	5.8	74.4
$\frac{1}{2}$	4.4	75.3
+1 = Pav.	4.41	75.3
L on "	4.46	75.3
+10 " "	4.62	75.1

$\frac{1}{2}$	4.6	75.1
Gut	5.1	74.6
cb.	4.55	75.2
\mathcal{N}	4.4	75.3
1+63 = S.L. Belvedere st.		
\mathcal{N}	4.5	75.2
cb.	4.70	75.0
Gut. on Paring	5.25	75.5
$\frac{1}{2}$ " "	4.81	74.9
$\frac{1}{2}$ " "	4.66	75.1
+10 " "	4.80	74.9
$\frac{1}{2}$	4.7	75.0
+6	5.5	74.2
+8	2.4	77.3
cb.	2.0	77.7
E.	1.8	77.9
1+93 = S. Belvedere st.		
E	2.7	77.0
cb.	3.8	75.9
+3	3.9	75.8
+5	6.2	73.5
$\frac{1}{2}$	5.3	74.4
+1 = Par.	5.35	74.4
$\frac{1}{2}$ on "	5.20	74.5
$\frac{1}{2}$ " "	5.27	74.5
cb. " "	5.25	74.5

\mathcal{N}	5.42	74.3	Note: All obs and st are taken as per Sheet 2/53 from Belvedere to Sea Lane
2+23 = N.L. Belvedere st			
\mathcal{N}	5.6	74.1	
" top cb.	5.68	74.1	
" Gut. on Par.	6.23	73.5	
$\frac{1}{2}$ " "	5.82	73.9	
$\frac{1}{2}$ " "	5.72	74.0	
+10 " "	5.81	73.9	
$\frac{1}{2}$	5.9	73.8	
+7	6.7	73.0	
+8	4.7	75.0	
cb.	4.3	75.4	
E.	3.6	76.1	
2+50			
E.	4.5	75.2	
cb.	4.9	74.8	
+2	5.9	73.8	
+3	7.2	72.5	
$\frac{1}{2}$	6.6	73.1	
+1 = Par.	6.44	73.3	
$\frac{1}{2}$ on "	6.31	73.4	
+10 " "	6.44	73.3	
$\frac{1}{2}$	6.4	73.3	
Gut.	7.2	73.5	
top cb.	6.31	73.4	
\mathcal{N}	6.3	73.4	

3+00

NY	7.7	72.0
cb.	7.62	72.1
Gut.	8.2	71.5
$\frac{1}{2}$	7.5	72.2
+1 = Pav.	7.56	72.2
L on "	7.48	72.3
+10 " "	7.63	72.1
$\frac{1}{2}$	7.8	71.9
+7	7.8	71.9
cb.	6.9	72.8
+3	6.0	73.7
E	5.4	74.3

3+33⁴ S.L. Fern Glen st. (60 wide?)

E	6.7	73.0
+7	7.8	71.9
cb.	8.3	71.4
$\frac{1}{4}$	8.2	71.5
+1 on Pav.	8.44	71.3
L " "	8.28	71.5
+10 " "	8.34	71.4
$\frac{1}{2}$	8.2	71.5
Gut.	8.5	71.2
NY	8.4	71.3
L Fern Glen st.		
NY	8.5	71.2

cb.	8.8	70.9
$\frac{1}{2}$	8.5	71.2
+1 = Pav.	8.55	71.2
L on "	8.46	71.3
+10 " "	8.52	71.2
$\frac{1}{2}$	8.5	71.2
cb.	8.6	71.1
E on Parking	8.62	71.1
N.L. Fern Glen = 0+00		
E	7.7	72.0
cb.	8.3	71.4
+1	9.1	70.8
$\frac{1}{4}$	8.7	71.0
+1 = Pav.	8.73	71.0
L on "	8.62	71.1
+10 " "	8.71	71.0
$\frac{1}{2}$	8.7	71.0
+5	8.7	71.0
cb.	8.3	71.4
NY	8.5	71.2
0+04		
-5	10.5	69.2
NY	10.5	69.2
cb.	8.7	71.5
+1	8.8	70.9
$\frac{1}{2}$	8.8	70.9

+1 on Pav.	8.75	710
L " "	8.66	711
+10 " "	8.73	710
$\frac{1}{2}$	8.7	710
710	9.0	702
cb.	8.6	711
+5	8.3	714
E	6.8	729
	0+10	
E	7.2	725
+5	8.4	713
cb.	8.9	728
+1	9.3	704
$\frac{1}{2}$	8.9	708
+1 on Pav.	8.81	709
L " "	8.74	710
+10 " "	8.84	709
$\frac{1}{2}$	8.9	708
+5	8.9	708
cb.	8.4	713
+5	9.5	702
N	12.3	674
+4	14.0	657
+10	13.7	660
	0+24	
-10	14.2	655

-4	14.0	657
N	11.1	686
+5	18.5	712
cb.	8.55	712
$\frac{1}{2}$	9.0	707
+1 = Pav.	8.97	708
L on "	8.86	709
+10 " "	8.88	709
$\frac{1}{2}$	9.0	707
cb.	9.1	706
E	7.4	723
T.P.	378 74.49	9.03 70.71
	0+32	
E	2.0	725
cb.	3.8	707
$\frac{1}{2}$	3.8	707
+1 = Pav.	3.67	708
L on "	3.60	709
+10 " "	3.76	70.7
$\frac{1}{2}$	3.8	707
cb.	3.4	711
N	4.0	705
+5	4.2	703
	0+50	
N	3.7	708
cb.	3.85	70.6

7449

Gut	4.1	704
$\frac{1}{2}$	3.8	707
+1 = Pav.	3.82	707
L on "	3.74	708
+10 " "	3.83	707
$\frac{1}{4}$	3.9	706
+10	4.2	703
cb.	3.8	707
E	1.7	728

1+00

E	1.6	729
cb.	3.0	715
+1	4.3	702
$\frac{1}{4}$	4.1	704
+1 = Pav.	4.09	704
L on "	4.10	704
+10 " "	4.20	703
$\frac{1}{4}$	4.2	703
Gut.	4.5	700
cb.	4.40	701
+8	4.1	704
W	2.8	717

1+50

W	2.4	721
+2	4.7	718
W top cb.	4.81	717

7449

Gut	5.1	694
$\frac{1}{2}$	4.6	69.9
+1 on boring	4.57	69.9
L " "	4.47	70.0
+10 " "	4.55	69.9
$\frac{1}{4}$	4.6	69.9
+8	4.7	69.8
cb.	2.8	71.7
E	1.5	73.0

1+642 = Sh. Rushville st. on E.

E on cb.	4.11	704
cb.	4.5	700
$\frac{1}{2}$	4.6	69.9
+1 = Pav.	4.69	69.8
L on "	4.59	69.9
+10 " "	4.69	69.8
$\frac{1}{4}$	4.8	69.7
Gut.	5.0	69.5
cb.	4.93	69.6
+8	4.8	69.7
W	2.6	71.9

1+90

W	3.3	712
+2	5.0	69.5
cb.	5.12	69.4
Gut.	5.4	69.1

34

$\frac{1}{2}$	5.0	69.5
+1 = Pav.	4.90	69.6
Loon "	4.76	69.7
+10" "	4.80	69.7
$\frac{1}{2}$	5.0	69.5
cb	5.0	69.5
E	5.0	69.5

1+93

E	2.5	72.0
cb.	3.6	70.9
+3	5.5	69.0
$\frac{1}{2}$	5.0	69.5
+1 = Pav.	4.79	69.7
Loon "	4.81	69.7
+10" "	4.93	69.7
$\frac{1}{2}$	5.1	69.4
Gut	5.5	69.0
X top cb	5.14	69.4
+8	5.0	69.5
X	3.1	71.4

2+23

X	5.3	69.2
cb.	5.40	69.1
Gut	6.0	68.5
$\frac{1}{2}$	5.3	69.2
+1 on Pav.	5.20	69.3

Loon Pav.	5.20	69.3
+10" "	5.17	69.3
$\frac{1}{2}$	5.3	69.2
+7	5.8	68.7
+8	4.0	70.5
cb.	3.8	70.7
E	2.5	72.0

2+50

E	3.0	71.5
cb.	4.6	69.9
+7	5.7	68.6
$\frac{1}{2}$	5.4	69.1
+1 = Pav.	5.35	69.1
Loon "	5.27	69.2
+10" "	5.37	69.1
$\frac{1}{2}$	5.4	69.1
Gut	6.5	68.0
cb	5.22	68.9
X	5.4	69.1

2+83

X	5.7	68.8
cb.	5.87	68.6
Gut.	6.6	67.9
$\frac{1}{2}$	5.7	68.8
+1 on Pav.	5.57	68.9
Loon "	5.46	69.0

+10 on Pav.	56/	68.9
$\frac{1}{2}$	56	68.9
+8	59	68.6
cb.	50	69.5
+5	45	70.0
+6	27	71.8
E	22	72.3
	3+00	
E	4.0	70.5
cb.	5/	69.7
+1	6.0	68.5
$\frac{1}{2}$	5.8	68.7
+1 = Pav.	5.76	68.7
E on "	5.66	68.8
+10 " "	5.77	68.7
$\frac{1}{2}$	5.8	68.7
Gut.	6.6	67.9
W top cb.	6.00	68.5
W	5.8	68.7
	3+49.8 = S. Area on E	
W	6.2	68.3
" top cb.	6.43	68.4
" Gut.	7.0	67.5
$\frac{1}{2}$	6.1	68.4
+1 = Pav.	6.16	68.3
E on "	6.02	68.5

+10 on Pav.	6.10	68.7
$\frac{1}{2}$	6.1	68.4
cb.	6.0	68.5
+1	5.7	69.3
E	4.3	69.2
	$\frac{1}{2}$ Areas on E	
E on Pav.	6.28	68.2
cb.	6.4	68.1
$\frac{1}{2}$	6.2	68.3
+1 = Pav.	6.34	68.2
E on "	6.40	68.1
+10 " "	6.49	68.0
$\frac{1}{2}$	6.5	68.0
Gut.	7.0	67.5
cb.	6.62	67.9
W	6.6	67.9
	All Areas S. on E = 0+00	
W on Pav.	7.74	66.8
cb. " "	7.54	67.0
$\frac{1}{2}$	7.1	67.4
+1 on "	6.94	67.6
E " "	6.55	67.9
+10 " "	6.38	68.1
$\frac{1}{2}$	6.4	68.1
cb.	6.3	68.2
E	5.7	68.8

0+02

E		4.9	69.6
+2		5.7	68.8
cb		6.1	68.4
$\frac{1}{2}$		6.4	68.1
+1 on Pav.		6.38	68.1
L " "		6.55	67.9
+10 " "		6.85	67.6
$\frac{1}{2}$		7.0	67.5
cb.		7.5	67.0
W on Pav.		7.70	66.8
T.P.	5.63 73.32	6.80	67.69

0+40 = Nbr. Areas on W

W		5.5	67.9
cb		5.64	67.7
Gut. on Pav.		5.95	67.4
$\frac{1}{2}$		5.5	67.8
+1 on " "		5.35	68.0
L " "		5.20	68.1
+10 " "		5.33	68.0
$\frac{1}{2}$		5.2	68.1
cb.		5.1	68.2
E		4.7	68.6

1+00

E		3.4	69.9
cb		4.3	69.0

+1		5.3	69.0
$\frac{1}{2}$		5.1	68.2
+1 on Pav.		5.14	68.2
L " "		5.02	68.3
+10 " "		5.13	68.2
$\frac{1}{2}$		5.2	69.1
Gut.		5.8	67.5
cb.		5.60	67.7
W		5.7	67.6

1+50

W		5.4	67.9
cb.		5.44	67.9
Gut.		5.8	67.5
$\frac{1}{2}$		5.1	68.2
+1 - Pav.		4.94	68.4
L on " "		4.81	68.5
+10 " "		4.96	68.4
$\frac{1}{2}$		4.9	68.4
+8		5.3	68.0
cb.		5.0	68.3
+2		4.2	69.1
E		3.8	69.5

2+05

E		3.0	70.3
cb.		4.0	69.3
+1		5.1	68.2

$\frac{1}{2}$	4.7	68.6
+1 = Pav.	4.75	68.6
$\frac{1}{2}$ on "	4.72	68.6
$\frac{1}{4}$ " "	4.75	68.7
Gut	5.6	67.7
W topcb.	5.18	68.1
W	5.0	68.3
2+50		
W	4.8	68.5
cb.	5.09	68.2
Gut.	5.5	67.8
$\frac{1}{2}$ on Pav.	4.79	68.5
$\frac{1}{2}$ " "	4.58	68.7
+10 " "	4.65	68.6
$\frac{1}{2}$	4.5	68.8
+8	5.0	68.3
cb.	3.9	69.4
E	3.5	69.8
2+95		
E	2.9	70.4
cb.	3.5	69.8
+1	4.7	68.6
$\frac{1}{2}$	4.5	68.8
+1 = Pav.	4.43	68.9
$\frac{1}{2}$ on "	4.41	68.9
$\frac{1}{2}$ " "	4.80	68.5

Gut.	5.5	67.8
cb.	4.96	68.4
W	4.9	68.4
3+00 = SL. Genter st. on E		
W	4.9	68.4
cb.	4.96	68.4
Gut. on Pav.	5.4	67.9
$\frac{1}{2}$ on Pav.	4.83	68.5
$\frac{1}{2}$ " "	4.39	68.9
$\frac{1}{2}$ " "	4.49	68.8
Gut " "	4.70	68.6
cb.	3.99	69.3
E	3.5	69.8
3+30 = $\frac{1}{2}$ Genter st		
E on Pav	4.03	69.3
cb " "	4.43	68.9
$\frac{1}{2}$ " "	4.21	69.1
$\frac{1}{2}$ " "	4.23	69.1
$\frac{1}{2}$ " "	4.63	68.7
Gut " " in Drive way =	5.38	67.9
W	4.6	68.7
N.L. Genter = 0+00		
W	4.5	68.8
" topcb.	4.65	68.7
" Gut. on Pav.	5.17	68.1
$\frac{1}{2}$ " "	4.48	68.8

E on Pav.	4.02	69.3
½ " "	4.01	69.3
Gut " "	4.16	69.2
cb.	3.60	69.7
E	3.7	70.1
0+50		
E	3.0	70.3
cb.	3.43	69.9
Gut. on Pav.	3.96	69.4
½ " "	3.85	69.5
L " "	3.80	69.5
½ " "	4.32	69.0
Gut " "	4.90	68.4
X cb.	4.40	68.9
X	4.3	69.0
1+00		
X	4.2	69.1
cb.	4.20	69.1
Gut. on Pav.	4.66	68.7
½ " "	4.09	69.2
L " "	3.63	69.7
½ " "	3.62	69.7
Gut. " "	3.76	69.6
E cb.	3.22	70.1
E	2.7	70.6

1+40 = S.L. Sea Lane of.

E	2.8	70.5
cb.	3.02	70.3
Gut. on Pav.	3.62	69.7
½ " "	3.50	69.8
L " "	3.50	69.8
½ " "	4.00	69.3
Gut. " "	4.58	68.7
cb.	4.02	69.3
X	3.9	69.4
1+70 = N.L. Sea Lane		
X	3.7	69.6
cb. on Walk	3.8	69.5
+3.75 = top X cb.	3.85	69.5
Gut. on Pav.	4.3	69.0
½ " "	4.00	69.3
L " "	3.38	69.9
½ " "	3.35	70.0
Gut. " "	3.45	69.9
E top cb.	2.95	70.4
E	2.7	70.6
chk. on N.E. B.P. in L.H.	1.56	71.76

Lafolla +
Sea Lane

Walker
Kempinger
Lusk
Ma Hoon
11-10-28

X. Section Playa Del Norte St.
As per sketch Page 3

- 0.44 68.00

68.44

T.P. in White
Post
Page 15

Section 0100

W 3.1 679
+10.4 = ch 3.32 677
+10.4 = Gut 4.2 639
+18.73 = E 3.6 644

Section A

E 3.8 642
+18.94 4.6 634
+18 = top ch. 4.07 629
+28 = West 3.6 644

Sec. B

W 4.5 635
+10.5 = ch 4.79 632
+10.5 = Gut 5.2 628
+15 5.0 630
+38.07 = E 4.4 636

Sec. C

E 6.3 617
+5 5.1 629
+18 5.2 628
+32 6.0 620
+34.2 = Gut 5.9 621
+34.2 = W ch. 5.56 624
+44.74 = W 5.6 624

68.00

R = 6.05

40

Sec. C + 18.5 = End Exist. Walk and curb on W

Sec. D

6.0 620
6.5 615
6.5 615
5.5 645
11.8 562

Sec. E

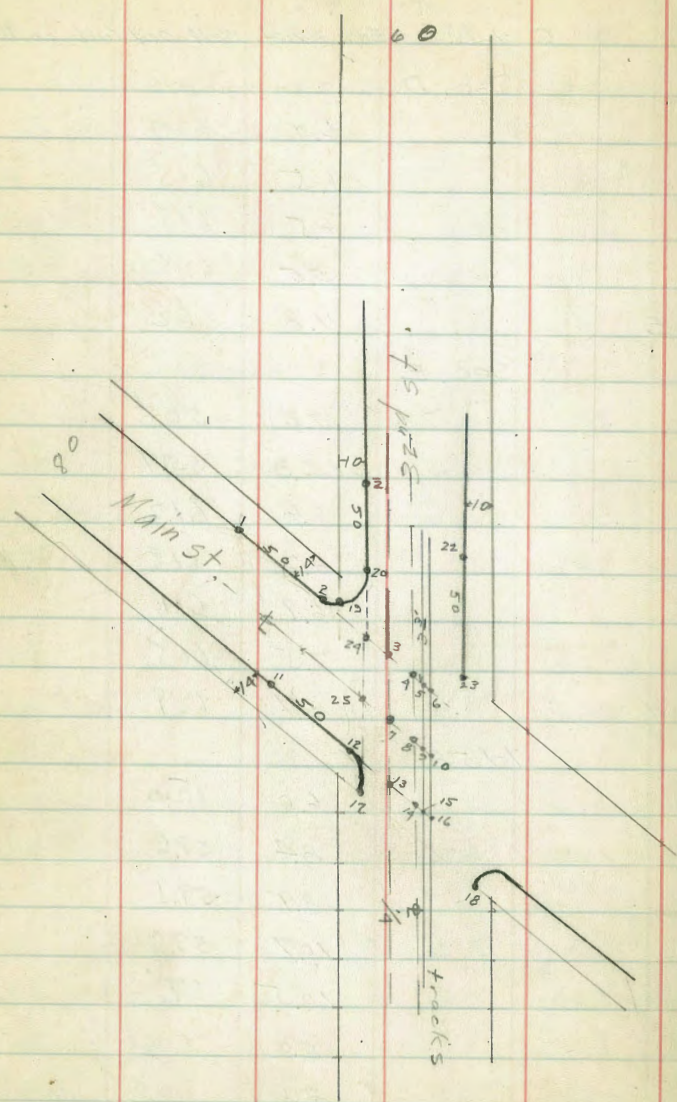
17.2 508
12.3 55.7
6.6 61.2
6.2 618
6.9 611
7.5 605
5.1 629

1758

W 710
+17
+42
+57.4 = E
E 714
+23
+34
+50
+64
+67.10 = W

W
+1
+5
+6
+8
+15
+25
+38
+40 = E
+55

6.0 620
8.4 59.6
8.9 59.1
10.7 57.3
10.5 57.5
8.0 60.0
8.0 60.0
8.3 59.7
9.7 58.3
13.7 54.3



Jan 10-20
Louden
Isbell
Marion.

Levels at Main & 32nd
Nos. correspond to those
Shown on sketch.

B.M		4.08	42.67	38.59
1	eb			39.97
1	gut			39.39
2	eb			39.22
2	gut			38.70
24				38.41
3				38.28
4				38.40
5				38.35
6				38.31
25				38.54
7				38.34
8				38.13
9				38.04
10				39.01
11	eb			39.04
11	gut			38.36
12	eb			38.43
12	gut			37.69
13				37.51
14				37.76
15				37.74
16				37.72
17	eb			38.22
17	gut			37.46

Along S.W.
Main & 32nd

42.67

18	eb	5.75	36.92
18	gvt.	6.16	36.51
19	eb	3.40	39.27
19	gvt	4.01	38.66
20	eb	3.40	39.27
20	gvt.	4.16	38.51
21	eb	3.12	39.55
21	gvt qrd.	4.1	38.57
22	eb	4.48	38.19
22	gvt qrd.	4.5	38.2
23	eb	4.85	37.82
23	gvt.	4.85	37.82

1/2 x 1/2
Moore

Cross section of alley (20')
Blk 97 San Diego L & T Co. Sub.

nwbp 9.1 39.13 29.99 Main Sampson

00 = W.L. Sampson = Beginning of Fence 1.0 is alley on North

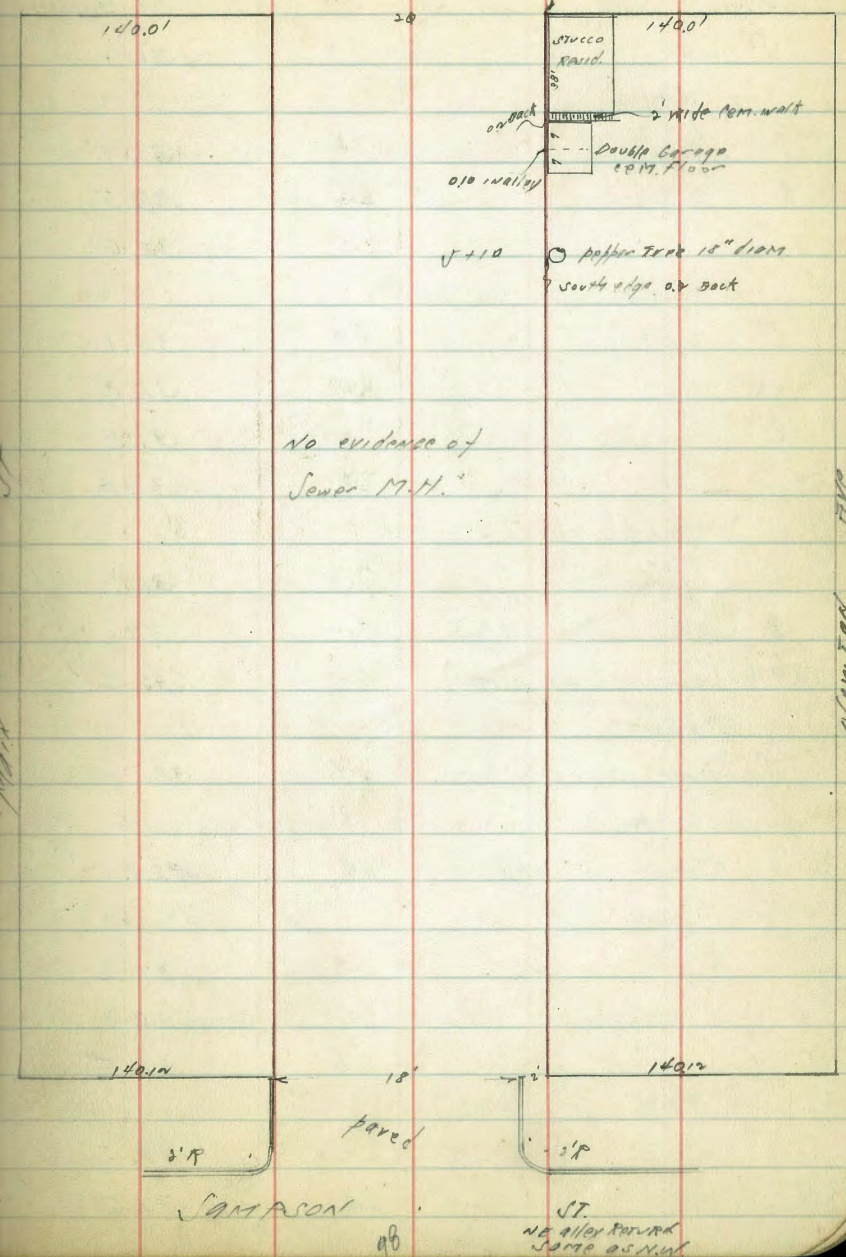
✓	Top com curb	5.80	33.33
✓	" paving	5.90	33.21
⊕	" "	6.00	33.13
+8	" "	5.58	33.55
+8	" com curb	5.39	33.74
	at 95		
✓		4.3	34.8
+1 = fence		4.3	34.8
C		4.5	33.6
✓		4.9	34.2
	at 10		
✓		5.2	33.7
⊕		5.1	34.0
+9.6 = end fence on North		4.9	34.2
	1400		
✓		5.9	33.2
⊕		5.9	33.2
✓		6.5	32.6
	1439		
✓		6.3	32.8
⊕		6.0	33.1
✓		6.4	32.7
	1437		
✓		6.4	32.7

Plotted Jan-26-29
C.B.H.

EVANS

36 55
graded only

57
03 back 43



No evidence of
Sener M.H.

ab

1737

3913

£	7.0	31.9
S	7.0	31.9
1450		
S	7.4	31.7
£	6.6	32.5
N	6.5	32.6
2400		
N	5.0	34.1
+V	6.8	32.3
£	7.0	31.9
S	7.3	31.8
2450		
S	7.0	32.1
£	7.0	32.1
+9.4 = line of sheds and garages beginning here	6.5	32.6
2477		
N S.W. Garage on alley	6.9	32.2 dirt floor
2492		
N E of Double Gar. on alley	6.9	32.2 " "
2400		
N	6.9	32.2
£	6.8	32.3
S	6.6	32.5
3438		
S	6.6	32.5
£	6.5	32.6

3913

44

N E of Six Gar. on back	6.4	32.7 dirt floor
3471		
N E S.W. Gar. on back	5.7	33.4 " "
£	6.1	33.0
S	6.3	32.8
4400		
S	5.6	33.5
£	5.4	33.7
N	5.4	33.7
T.P.	5.05	38.65
4450		
N	4.2	34.2
£	4.6	34.0
S	4.8	33.8
4490		
S	4.9	33.7
£	4.9	33.7
N E Six Gar. on back	4.5	34.2 dirt floor
5405		
N E " " 14 "	4.4	34.3 " " ✓
5410		
N at popper tree	4.1	34.6 ✓
5435		
N	4.4	34.3
£	4.5	34.2
S	4.9	33.8

5+59 E double Garage divide
0.1 in alley

✓ cam floor
level

N Top floor 0.67

34.98

5+68²

N Top cam work 2.61

35.04 ✓

+N 4.0

34.7

E 4.4

34.3

✓ 4.4

34.3

5+90

S 4.5

34.2

+S 5.0

33.7

E 4.9

33.7

+S 4.3

34.4

N 4.1

34.6

6+01 = E1 EVANS

✓ Top CURB 5.33

33.32

N gut 5.2

33.5

+S 5.6

33.1

C 5.7

33.0

+S 5.6

33.1

S gut 5.4

33.2

✓ Top curb 6.05

32.60

check to NUMB Mark EVANS 7.53

11.07

27.55

0.05 error

11.4

8.67

29.98

29.99

0.01 error

x-section, Campo Drive - Cajon to Alley
 " Rolando Blvd. " "
 " Pearson Drive - " "
 " Alley - Entire Length
 " Cajon Ave - along N. Side Metrop. Center

JAEGER }
 Bailey }
 Clare }
 Brooks } Jan. 5th 1929.

46

STA	+	H.I.	-	Elev.	B.M. Iron pipe	Check	Levels	-	Elev
B.M. N.W.B.P. El Cerito & El Cajon				457.43	T.P.	9.04		4.84	
T.P.	12.75	470.18			T.P.	7.61		4.42	
T.P.	8.75	478.47	0.26	469.72	T.P.	5.59		3.58	
T.P.	1.55	472.86	7.16	471.31	T.P.	4.99		5.80	
T.P.	5.58	471.78	6.66	466.20	T.P.	4.53		3.73	
T.P.	2.93	468.70	6.05	465.77	T.P.	6.34		7.17	
T.P.	5.03	470.33	3.40	465.30	T.P.	6.46		0.33	
T.P.	3.02	469.16	4.19	466.14	T.P.	7.62		12.37	
T.P.	3.89	467.95	5.10	464.06	T.P.	1.81		10.35	
T.P.	4.84	465.12	7.67	460.28					
B.M. on iron pipe			9.04	456.08		53.99		52.59	
			Correction	- .02		- 52.59			
				456.06		1.40			
						456.08			
						457.48			

Alley Metropolitan Center from West Boundary to Pearson Dr.
20' wide

STA	+	H.I.	-	Elev.	STA	+	H.I.	-	Elev.
B.M. I.P. SW. Cor. Metropolitan Center				456.060	N.L.			9.7	439.1
	0.54	456.60			+5'			8.9	439.9
fd. B.P. on SW Cor					0+60 ⁷⁶			9.1	
Set B.P. Curb HW. Rolando Blvd. & El Cajon Blvd.	4.07	452.53		452.53 ⁴⁶	W.L. Campo Dr.			9.1	439.7
T.P.			12.89	443.71	S.L.			10.1	438.7
	5.14	448.85			⊥			9.7	439.1
+ 10' West of Westl Boundary of Subdivision					N.L.			9.7	439.1
S.L.			3.6	445.2	+5'			9.7	439.1
⊥			2.0	446.8	0+70 ⁷⁶				
N.L.			1.6	447.2	+5'			11.0	437.8
0+00 Westl Boundary of Subdivision					N.L.			10.8	438.0
+5'			4.3	444.5	⊥			9.8	439.0
S.L.			4.0	444.8	S.L.			9.0	439.8
⊥			4.1	444.7	0+78 ⁷⁶				
N.L.			3.5	445.3	S.L.			8.7	440.1
+5'			3.2	445.6	⊥			10.1	438.7
0+28					N.L.			10.7	438.1
+5'			6.6	442.2	+5'			11.2	437.6
N.L.			5.9	442.9	0+85 ⁷⁶				
⊥			6.9	441.9	+5'			11.4	437.4
S.L.			7.4	441.4	N.L.			10.9	437.9
+5'			7.2	441.6	⊥			9.7	439.1
0+52					S.L.			8.5	440.3
+5'			8.9	439.9	0+93 ⁷⁶				
S.L.			9.4	439.4	S.L.			8.3	440.5
⊥			9.0	439.8	⊥			9.2	439.6

Plotted 4-3-29 GCH

STA	+	H.I.	-	Elev.	STA	+	H.I.	-	Elev.
N.L.			10.4	438.4	+5'			3.0	450.1
+5'			11.0	437.8	2+10				
1+00 ⁷⁶					+5'			1.6	451.5
+5'			10.0	438.8	N.L.			1.6	451.5
N.L.			9.6	439.2	ϕ			1.6	451.5
ϕ			8.4	440.4	S.L.			1.6	451.5
S.L.			7.8	441.0	+5'			1.5	451.6
1+10 ⁷⁶	E.L.	Campo Dr.			2+35				
S.L.			6.4	442.6	+5'			2.6	450.5
ϕ			6.8	442.0	S.L.			2.7	450.4
N.L.			7.3	441.5	ϕ			2.9	450.2
+5'			7.2	441.5	N.L.			3.1	450.0
1+35					+5'			3.3	449.8
+5'			4.4	444.4	2+60				
N.L.			4.1	444.7	+5'			7.0	446.1
ϕ			3.5	445.3	N.L.			6.7	446.4
S.L.			3.0	445.8	ϕ			5.8	447.3
+5'			2.8	446.0	S.L.			5.3	447.8
T.P.			1.60	447.25	+5'			5.2	447.9
	5.90	453.15	✓		2+90				
1+85					+5'			8.5	444.6
+5'			2.1	451.0	S.L.			9.1	444.0
S.L.			2.3	450.8	ϕ			9.3	443.8
ϕ			2.5	450.6	N.L.			9.9	443.2
N.L.			2.9	450.2	+5'			10.1	443.0

STA	+	H.I.	-	Elev.	STA	+	H.I.	-	Elev.
3+10					N.L.			3.0	450.1
+5'			8.0	445.1	ϕ			2.6	450.5
N.L.			7.6	445.5	S.L.			2.0	451.1
ϕ			7.1	446.0	4+15 ⁷⁶				
S.L.			6.6	446.5	S.W.			2.7	450.4
+5'			6.2	446.9	ϕ			3.3	449.8
3+35					N.L.			3.9	449.7
+5'			3.5	449.6	+5'			4.1	449.0
S.L.			3.5	449.6	4+25 ⁷⁶	ϕ	Rolando Blvd.		
ϕ			3.9	449.7	+5'			5.5	447.6
N.L.			4.1	449.0	N.L.			4.9	448.2
+5'			4.2	448.9	ϕ			3.7	449.4
3+60					S.L.			3.5	449.6
+5'			2.8	450.3	4+35 ⁷⁶	1/4			
N.L.			2.7	450.4	S.L.			5.3	447.8
ϕ			2.4	450.7	ϕ			6.3	446.8
S.L.			2.1	451.0	N.L.			7.6	445.5
+5'			2.0	451.1	+5'			7.9	445.2
3+85 ⁷⁶	W.L.	Rolando Blvd.			4+45 ⁷⁶	S.W.			
S.L.			1.7	451.4	+5'			9.2	443.9
ϕ			1.9	451.2	N.L.			8.8	444.3
N.L.			2.0	451.1	ϕ			7.8	445.3
+5'			2.0	451.1	S.L.			6.6	446.5
4+05 ⁷⁶					4+65 ⁷⁶	E.L.	Rolando Blvd.		
+5'			3.3	449.8	S.L.			7.9	445.2

STA	+	H.I.	-	Elev.	STA	+	H.I.	-	Elev.
ϕ			8.5	444.6	S.L.			4.4	449.8
N.L.			9.5	443.6	+5'			2.2	452.0
+5'			9.8	443.3	ϕ			1.6	452.6
4+90					N.L.			1.9	452.3
+5'			4.8	448.3	+5'			2.7	451.5
N.L.			4.8	448.3	5+84				
ϕ			4.8	448.3	+5'			2.4	451.8
S.L.			4.9	448.2	N.L.			5.0	449.2
+5'			4.9	448.2	ϕ			7.1	447.1
5+49					S.L.			6.7	447.5
+5'			2.0	451.1	+5'			6.3	447.9
S.L.			2.2	450.9	6+60				
ϕ			2.1	451.0	+5'			7.9	446.3
N.L.			2.3	450.8	S.L.			8.6	445.6
+5'			2.3	450.8	ϕ			8.1	446.1
T.P.			1.42	451.73	N.L.			8.6	445.6
	2.52	454.25 ✓			+5'			7.7	446.5
5+60					T.P.			12.26	441.99
+5'			3.0	451.2		2.72	444.71 ✓		
N.L.			3.0	451.2	6+84				
ϕ			2.9	451.3	+5'			5.3	439.4
S.L.			2.0	452.2	N.L.			4.7	440.0
+5'			1.5	452.7	ϕ			3.1	441.6
5+73					S.L.			2.4	442.3
+5'			6.1	448.1	+5'			2.0	442.7

STA		+	H.I.	-	Elev.	STA		+	H.I.	-	Elev.
7+08						0+20	S.L. Alley				
+5'				7.8	436.9	+5'				2.4	431.4
S.L.				8.0	436.7	W.L.				3.3	430.5
♀				8.7	436.0	+10'				5.3	428.5
N.L.				9.2	435.5	+20'				6.5	427.3
+5'				9.5	435.2	+30'				8.7	425.1
	T.P.			12.59	432.12	+40' E.L.				11.5	422.3
X-Section Pearson Dr. from N.L. Alley to Cajon Pl.						+5'				12.4	421.4
		1.66	433.78	✓		0+45					
0+00	N.L. Alley					+5'				11.0	422.8
+5'				4.0	429.8	E.L.				9.8	424.0
W.L.				4.8	429.0	+10'				7.6	426.2
+10'				7.0	426.8	+20'				5.8	428.0
+20'				9.1	424.7	+30'				3.3	430.5
+30'				11.3	422.5	+40' W.L.				1.0	432.8
+40' E.L.				13.7	420.1	+5'				0.0	433.8
0+10	♀ Alley						T.P.			1.62	432.16
+5'				13.6	420.2			6.73	438.89		
E.L.				12.7	421.1	0+74.85					
+10'				10.0	423.8	W.L.				3.2	435.7
+20'				7.7	424.1	+10'				5.6	433.3
+30'				6.0	427.8	+20'				7.9	431.0
+40' W.L.				3.6	430.2	+30'				10.0	428.9
+5'				2.3	431.5	+40' E.L.				12.3	426.6
						+5'				13.0	425.9

Plotted 4/3-29 GPH

NOTE
↓

X- Section Rolando Blvd. from S.L. Alley
20' SW. 10' Quarters

X- Section Dr. from S.L. Alley
10' SW. 7.5' Quarters

52

STA	+	H.I.	-	Elev.
B.M. B.P.				452.53
	4.28	456.81 ✓		
0+00	S.L. Alley X-Sections taken			
0+25				
+5'			5.0	451.8
W.L.			5.0 ✓	451.8
+20'			5.2 ✓	451.6
W 1/4			5.5 ✓	451.3
☐			6.1 ✓	450.7
E 1/4			6.6 ✓	450.2
+10'			7.6	449.2
E.L.			9.2	447.6
+5'			9.2	447.6
0+55				
+5'			7.3	449.5
E.L.			7.3	449.5
+20'			6.8	450.0
E 1/4			6.0	450.8
☐			5.2	451.6
W 1/4			5.0	451.8
+10'			4.8	452.0
W.L.			4.7	452.1
+5'			4.7	452.1
T.P.			9.79	447.02
	1.34	448.36 ✓		

STA	+	H.I.	-	Elev.
				448.36 ✓
0+00	S.L. Alley X-Sections taken			
0+25				
+5'			3.6	444.8
E.L.			4.2	444.2
+10'			5.2	443.2
E 1/4			6.0	442.4
☐			6.7	441.7
W 1/4			7.0	441.4
+7.5'			7.7	440.7
W.L.			8.0	440.4
+5'			7.9	440.5
0+55				
+5'			5.7	442.7
W.L.			5.6	442.8
+10'			5.7	442.7
W 1/4			5.5	442.9
☐			5.0	443.4
E 1/4			3.8	444.6
+7.5'			3.3	445.1
E.L.			2.3	446.1
+5'			2.0	446.4

X-Section 20' Side Walk on North of Cajon Blvd.
 Entire Length of Metropolitan Center.

STA	+	H.I.	-	Elev.	STA	+	H.I.	-	Elev.
B.M. B.P.	Eden Swly Cor.			452.53	Curb Bott.			4.41	452.41
	4.29	456.82 ✓			1+18	♀	Storm Drain		
SWL Cor. of SubDivision			0.73	456.09	1+10			12.6	444.2
+2' Curb Top			1.39	455.43	N.L.			11.8	445.0
✓ Bott.			2.08	454.74	+12'			11.2	445.6
0+00	S.W. Cor. Lot 33				+18			4.3	452.5
+10'			5.3	451.5	+22' Curb Top	↙		3.99	452.83
N.L.			5.2	451.6	✓ Bott.			5.01	451.81
+6'			4.7	452.1	Bottom Storm Drain			10.88	445.94
+13'			2.2	454.6	1+47 ⁰⁶		PC.		
+22' Curb Top			2.08	454.74	+10'			12.0	444.8
✓ Bott.			2.68	454.14	N.L.			11.0	445.8
0+38					+9'			10.3	446.5
+10'			8.5	448.3	+18			4.2	452.6
N.L.			8.2	448.6	+22' Curb Top	↙		4.18	452.64
+9'			7.5	449.3	✓ Bott.			4.76	452.06
+18			2.7	454.1	1+72 ⁰⁶		W.L. Campo Dr.		
+22' Curb Top			2.76	454.06	+10'			12.9	443.9
✓ Bott.			3.32	453.50	N.L.			12.0	444.8
0+89					+10'			10.5	446.3
+10'			12.5	444.3	+19'			4.3	452.5
N.L.			11.9	444.9	+22' Curb Top			4.16	452.66
+6'			11.6	445.2	✓ Bott.			4.79	452.03
+17'			4.1	452.7					
+22' Curb Top			3.76	453.06					

Plotted 4/10/29
A.L.

STA	+	H.I.	-	Elev.	STA	+	H.I.	-	Elev.
1+97 ⁰⁶	♀	Campo Dr.						4.15	452.67
+10'			12.2	444.6	3+22 ⁰⁶				
N.L.			11.2	445.6	+10'			4.5	452.3
+9'			10.4	446.4	N.L.			4.4	452.4
+18'			4.2	452.6	+22'	Curb Top		4.6	452.2
+22'	Curb Top	✓	4.26	452.56	✓	Both.		5.2	451.6
	✓	Both.	4.90	451.92	B.M. P. P.				452.53
2+22 ⁰⁶	E.L.	Campo Dr.					3.90	456.43	✓
+10'			9.8	447.0	3+72 ⁰⁶				
N.L.			8.9	447.9	+10'			7.3	449.1
+9'			8.2	448.6	N.L.			7.0	449.4
+19'			4.6	452.2	+12'			6.9	449.5
+22'	Curb Top	✓	4.41	452.41	+18'			4.3	452.1
	✓	Both.	5.02	451.80	+22'	Curb Top		4.34	452.09
2+47 ⁰⁶	-P.C.				✓	Both.		4.98	454.45
+10'			7.9	448.9	4+22 ⁰⁶				
N.L.			7.0	449.8	+10'			7.3	449.1
+8'			6.8	450.0	N.L.			6.9	449.5
+12'			5.0	451.8	+9'			6.3	450.1
+22'	Curb Top		4.42	452.40	+13'			5.0	451.4
	✓	Both.	5.09	451.73	+22'	Curb Top		4.54	451.89
2+97 ⁰⁶					✓	Both.		5.19	451.24
+10'			4.5	452.3	4+72 ⁰⁶				
N.L.			4.4	452.4	+10'			4.5	451.9
+22'	Curb Top		4.56	452.26	N.L.			4.2	452.2

STA	+	H.L.	-	Elev.	STA	+	H.L.	-	Elev.
+22'	Curb Top		4.68	451.75	6+52 ⁰⁶				
	✓ Bottom		5.25	451.18	+10'			4.6	451.8
4+97 ⁰⁶	W.L. Rolando Blvd.				N.L.			4.3	452.1
+10'			4.3	452.1	+10'			4.4	452.0
N.L.			4.1	452.3	+22'	Curb Top		5.82	450.61
+22'	Curb Top		4.77	451.66	✓ Bottom			6.48	449.95
	✓ Bottom		5.37	451.06	6+68				
5+39 ⁰⁶	♀ Rolando Blvd.				+10'			3.22	453.2
+10'			4.6	451.8	N.L.			5.9	450.5
N.L.			4.4	452.0	+10'			7.03	449.40
+18'			3.8	457.6	+22'	Curb Top		6.19	450.24
+19'			5.4	451.0	✓ Bottom			6.86	449.57
+22'	Pavement		5.63	450.80	6+77 ⁰⁶				
5+77 ⁰⁶	E.L. Rolando Blvd.				+10'			6.9	449.5
+10'			7.0	449.4	N.L.			6.9	449.5
N.L.			6.5	449.9	+10'			7.1	449.3
+15'			4.9	451.5	+22'	Curb Top		6.48	449.95
+22'	Curb Top		5.28	451.15	✓ Bottom			7.09	449.34
	✓ Bottom		5.91	450.52	T.P.			8.26	448.17
6+02 ⁰⁶		ps.					1.75	449.92	
+10'			6.3	450.1	7+77 ⁰⁶				
N.L.			5.9	450.5	+10'			4.1	445.8
+22'	Curb Top		5.34	451.09	N.L.			3.8	446.1
	✓ Bottom		5.99	450.44	+22'	Curb Top		4.65	445.87
					✓ Bottom			4.72	445.20

STA	+	H.I.	-	Elev.
8+77 ⁰⁶				
+10'			7.2	442.7
N.L.			7.4	442.5
+12'	Curb Top		6.56	443.36
	✓ Bott.		7.16	442.76
8+45				
+10'			11.0	438.9
N.L.			8.9	441.0
+10'			7.7	442.2
+12'	Curb Top		7.53	442.39
	✓ Bott.		8.13	441.79
8+52 ⁰⁶	W.L. Pearson			
+10'			13.1	436.8
N.L.			11.4	438.5
+9'			10.7	439.2
+16'			7.9	442.0
+12'	Curb Top		7.99	441.98
	✓ Bott.		8.54	441.38
	T.P.		13.08	436.84
		4.23	441.07 ✓	
8+77 ⁰⁶	☉ Pearson			
+10'			10.6	430.5
N.L.			10.0	431.1
+7'			9.4	431.7
+18'			0.9	440.2

STA	+	H.I.	-	Elev.
+22'	Curb Top		0.57	440.50
	✓ Bott.		1.20	439.87
9+02 ⁰⁶	E.L. Pearson			
+10'			13.3	427.8
N.L.			12.8	428.3
+18'			1.2	439.9
+12'	Curb Top		1.22	439.85
	✓ Bott.		1.85	439.22
9+10				
+10'			18.6	422.5
N.L.			13.8	427.3
+16'			2.7	438.4
+12'	Curb Top		2.72	438.35
	✓ Bott.		3.31	437.76
	T.P.		13.0	428.07
	Hand Lev	0.0	428.07	
9+55				
+15'			14.0	414.1
N.L.			0.5	427.6
		Instr.	441.07 ✓	
+14'			4.5	436.6
+12'	Curb Top		4.36	436.71
	✓ Bott.		5.00	436.07

	+	H.I.	-	Elev.
Sta 89+95 ⁶⁷		441.07		
Curb Bot.			6.2	434.9
✓ Top			5.57	435.50
+8'			6.1	435.0
T.P.			13.0	428.07
Hand Level	0.0	428.07		
+22' M.L.			0.9	427.2
+10'			6.0	422.1
+25'			16.8	411.3

	+	HZ 29212	-	5/6
t10			6.0	286.1
cb			6.9	285.7
1/4			6.4	285.7
2			6.1	286.0
+4			6.0	286.1
+6			6.3	285.8
1/4			6.5	285.6
-6			6.8	285.3
+7			6.7	285.4
S			9.6	282.5
+5			11.3	280.8
+15			12.8	279.3
			0750	
-15			13.4	278.7
-5			12.6	279.5
S			10.6	281.5
+10			6.8	285.3
cb			7.0	285.1
1/4			6.7	285.4
2			6.7	285.4
1/4			6.6	285.5
cb			6.7	285.4
+3			6.4	285.7
N			6.2	285.9
			0775	
N			6.3	285.8

+89 = 2'5
Flow line 11.53 = 15" diam

t10	6.3	285.8
cb	6.9	285.2
1/4	6.7	285.4
2	6.5	285.6
1/4	6.7	285.4
cb	6.8	285.3
+4	6.9	285.2
S	11.2	280.9
+15	12.9	279.2
	1100	5.6 line Holly
-15	9.2	282.9
-7	9.4	282.7
S	8.2	283.9
+3	6.8	285.3
+11	6.5	285.6
cb	6.9	285.2
1/4	6.6	285.5
2	6.6	285.5
1/4	6.8	285.3
+10	6.8	285.3
cb	7.2	284.9
+3	6.7	285.7
N	6.3	285.8
	1115	
N	6.1	286.0
cb	6.5	285.6

	H.I.		5/6 ✓
	292.12		
+5	6.5		285.6
+6	6.7		285.4
1/4	6.6		285.5
6	6.3		285.8
1/4	6.4		285.7
cb	6.7		285.4
tv	6.7		285.4
+3	6.3		285.8
S.	6.5		285.6
	1150		
S	5.9		286.7
+10	5.7		286.4
+12	6.2		285.9
cb	6.3		285.8
1/4	5.9		286.2
6	5.8		286.3
1/4	6.1		286.0
cb	6.2		285.9
+3	5.8		286.3
N	5.5		286.6
	2100		
N	4.5		287.6
+10	4.8		287.3
cb	5.4		286.7
+4	5.2		286.9
1/4	5.0		287.1

	H.I.		5/6 ✓
	292.12		
	4.9		287.2
	5.0		287.1
	5.2		286.9
	4.5		287.6
	4.1		288.0
	2122	Walkway N concrete	
	online	3.81	288.31
	2142	Auto Driveway	
	concrete online	3.35	288.77
	2146	Auto driveway	
	concrete online	3.36	288.76
	2150		
	2.8		289.3
	3.1		289.0
	3.5		288.6
	3.3		288.8
	3.9		288.7
	4.1		288.0
	3.5		288.6
	3.5		288.6
	3.4		288.7
	3.7		288.4
	4.3		287.8
	3.9		288.2
	3.6		288.5

	+	H.I. 292.12	-	Elev
			3+00	
N			1.6	290.5
+12			17	290.4
cb			2.7	289.4
+6			2.5	289.6
1/4			2.4	289.7
2			2.4	289.7
1/4			2.4	289.7
cb			2.9	289.2
+2			2.9	289.2
+4			2.4	289.7
S			20	290.1
			3+25	
S			1.6	290.5
+10			1.6	290.5
+12			2.9	289.7
cb			2.3	289.8
1/4			1.8	290.3
2			1.8	290.3
1/4			1.8	290.3
cb			2.1	290.0
+2			1.1	291.0
N			1.2	290.9
			3+50 ²⁹	
			Wline Dab/1a = 00	
N			0.3	291.8
+12			0.5	291.6
cb			1.5	290.6

	+	H.I. 292.12	-	Elev
+6			1.3	290.8
1/4			1.3	290.8
2			1.2	290.9
1/4			1.3	290.8
cb			1.9	290.2
+2			1.8	290.3
+4			1.1	291.0
S			1.1	291.0
			10' East of Wline	
S			0.9	291.2
+10			0.9	291.2
+12			1.7	290.4
cb			1.6	290.5
1/4			1.2	290.9
2			1.0	291.1
1/4			1.1	291.0
cb			1.4	290.7
+2			1.4	290.7
+3			0.3	291.8
N			0.1	292.0
TP	4.03	295.45	0.70	291.42
			13' East	
N			4.2	291.2
cb			4.6	290.8
1/4			4.4	291.0

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	HZ 295.95	-	Elev
ϕ		9.3	291.1
1/4		4.5	290.9
cb		9.9	290.5
t2		4.8	290.6
t3		4.0	291.4
S		9.0	291.4
		25' East	
S		3.8	291.6
t10		3.9	291.5
t12		4.5	290.9
cb		4.7	290.7
1/4		4.4	291.0
ϕ		4.3	291.1
1/4		4.4	291.0
cb		4.5	290.9
N		4.0	291.4
		37' East	
N		3.8	291.6
t5		3.8	291.6
cb		4.4	291.0
1/4		4.2	291.2
t4		4.1	291.3
ϕ		4.1	291.3
1/4		4.3	291.1
cb		4.5	290.9
t2		4.5	290.9

	HZ 295.95	-	Elev
t4		3.7	291.7
S		3.7	291.7
		90' East	
S		3.7	291.7
t10		3.6	291.8
t12		4.4	291.0
cb		4.5	290.9
1/4		4.3	291.1
ϕ		4.1	291.3
t8		4.0	291.4
1/4		4.2	291.2
cb		4.4	291.0
t2		4.1	291.3
t4		3.1	292.3
N		2.9	292.5
		50' East. E. line Pch/ia	
N		2.8	292.6
t12		2.9	292.5
cb		4.3	291.1
1/4		4.1	291.3
ϕ		3.9	291.5
1/4		4.1	291.3
cb		4.4	291.0
t2		4.4	291.0
t9		3.6	291.8
S		3.5	291.9
check out on starting BM		1.97	287.98

62

NW 1" pipe Oak + Paper

J.M. Bliss
March 11, 1927

X Sections Alley Block "N"
University Hts. Between Idaho & Oregon
Copley & Collier

	+	H.I.	-	Elev
BM SE BP				
Idaho Adams	6.73	391.64		389.91 ✓
T.P.	6.47	395.41	2.70	388.94 ✓
Set BM 3 & Top N. Copley & Idaho	3.94	398.41	0.99	394.47 ✓
		"on paring" 0100 Skine Copley		
E Top cb		6.98		391.43
G		7.37		391.04
Φ		7.49		390.92
G		7.39		391.02
N Top cb		7.12		391.29
		0110		
N		6.5		391.9
Φ		6.5		391.9
15		6.0		392.4
E		5.7		392.7
		0120 Main Hole		
E	Φ River	5.64		392.77
		0130		
E		4.3		394.1
+ 4		4.5		393.9
Φ		5.2		393.2
N		5.3		393.1
		0150		
N		5.2		393.2

Plotted 3/25/29
T.A.

	+	H.I.	-	Elev
		398.91		
			4.7	393.7
			4.8	393.6
			4.2	394.2
		0158 N End 2 Car Garage on W		
		4° Back N End Concrete lip	5.04	393.37
		0174 S End 2 Car Garage on W		
		4° Back S End Concrete lip	5.04	393.37
		0175		
			4.3	394.1
			4.7	393.7
			4.9	393.5
		1100		
			4.9	393.5
			4.7	393.7
			4.8	393.6
		1112		
			4.8	393.6
			4.9	393.5
			4.9	393.5
		1125 N End Single on East		
			5.8	392.6
			5.5	392.9
			5.2	393.2
			4.6	393.8
		N End lip 2° Back	4.59	393.82

	+	HI	-	Elev
		398.41		
				1131 N End 2 Car Garage on West
	3 ³ Back lip	5.93		392.48
				1137 S End Single Garage on East
	Edge concrete lip v ² back	4.64		393.77
				1147 S End Dbl Garage on West
	3.3 Back lip	5.83		392.58
		1150		
E		5.7		392.7
⊘		5.8		392.6
N		6.0		392.4
		1170		
N		6.1		392.3
⊘		6.1		392.3
E		6.1		392.3
		1180		
E		6.2		392.2
⊘		6.4		392.0
N		6.7		391.7
				1189 Single Garage on East
	5 ² Back concrete floor	6.33		392.08
		2100		
N		6.6		391.8
⊘		6.3		392.1
E		6.5		391.9
				2105 N End Dbl Garage on W
	3 ³ Back concrete lip	6.87		391.54

	+	HI	-	Elev
		398.41		
				2113
				6.9 392.0
				6.5 391.9
				6.9 391.5
				2122 S End Dbl Garage on West
				391.46
	3 ³ Back concrete lip	6.95		391.99
	T.P. >	9.08		396.07
				2126 Single Garage on East
	12 ² Back concrete floor	4.17		391.90
				4.2 391.9
				4.2 391.9
				4.2 391.9
				2150
				4.4 391.7
				4.6 391.5
				4.6 391.5
				2153 Walk on East
	online concrete	4.57		391.50
				2175
				5.2 390.9
				5.4 390.7
				5.4 390.7
				2185
				5.6 390.5
				5.6 390.5
				5.6 390.5

5-10-29 X-section Franklin St. 30th to
 C. Bliss
 Dyer +
 Rooney
 29th - 80' wide 20' cbs - 10' 9th 45

B.M. N.E.B.P. Franklin & 30 th	82.17	cb
+ 11.96	94.13	N
	N.L.	
	N.L. 30 th = 0+00. (on paving)	
N-Top concrete wall	9.33	85.80
N-Base wall on sidewalk	7.81	84.92
Tpcb	10.01	84.10
G	10.65	83.50
14	10.13	84.00
⊥	9.85	84.28
14	10.12	84.01
G	10.66	83.47
Tpcb	10.02	84.11
S-Base wall on sidewalk	9.77	84.36
S-Top concrete wall	8.32	85.81
	0+5.5	
Small tree 2.5' Back N cb line	10.0	84.1
	0+18	
⊥ 3' lower step in wall	8.45	85.68
	0+20	
S	8.9	85.2
cb	10.0	84.1
14	9.8	84.3
⊥	9.5	84.6
14	9.8	84.3

Plotted 5/11/29

1/2

94.13

66

	9.8	84.3
	9.1	85.0
0+45		
	7.9	86.2
	8.5	85.6
	9.4	84.7
	9.1	85.0
	8.7	85.4
	8.7	85.4
	9.3	84.8
	8.0	86.1
	7.5	86.6
0+55		
Top West end Concrete Wall on S.L.	5.56	88.57
	0+58.5	
Top West end concrete Wall on N.L.	6.41	87.72
	0+64	
6' Concrete drive 3' Back N.L.	6.19	87.94
	0+70	
	6.2	87.9
	6.5	87.6
	7.1	87.0
	8.0	86.1
	7.5	86.5
	7.4	86.7

94.13

14	80	86.1
+6	8.2	85.5
cb	80	86.1
+17	7.2	86.9
N	5.7	88.4
	0+95	
N	6.3	87.8
cb	7.2	86.9
+5	7.5	86.6
14	7.1	87.0
¢	6.4	87.7
14	6.2	87.9
+8	6.6	87.5
cb	5.6	88.5
5	4.8	89.3
	1+20	
5	3.2	90.9
+5	4.0	90.1
+18	4.3	89.8
cb	5.1	89.0
+2	5.6	88.5
14	5.3	88.8
¢	5.7	88.4
14	6.6	87.5
+8	7.1	87.0

94.13

67

cb	6.6	87.5
+16	5.9	88.2
N	4.7	89.4
	1+45	
N	4.2	89.9
+5	6.1	88.0
cb	6.4	87.7
+5	6.8	87.3
14	6.3	87.8
¢	5.3	88.8
14	4.8	89.3
cb	5.0	89.1
+2	4.0	90.1
5	3.2	90.9
	1+48	
	45' Set Concrete steps - Lower step	2.73 91.40
	1+70	
5	3.3	90.8
cb	4.1	90.0
+1	4.9	89.2
14	4.6	89.5
¢	5.1	89.0
14	6.2	87.9
cb	6.5	87.6
+17	6.0	88.1

94.13

N	5.3	88.8
	1495	
N	5.4	88.7
+3	6.1	88.0
cb	6.5	87.6
1/4	6.4	87.7
⊕	5.5	88.6
1/4	4.9	89.2
+9	4.8	89.3
cb	4.1	90.0
S	3.5	90.6
	2+20	
S	3.5	90.6
cb	4.1	90.0
+2	5.0	89.1
1/4	5.0	89.1
⊕	5.5	88.6
1/4	6.4	87.7
cb	6.7	87.4
N	6.3	87.8
	2+45	
N	6.7	87.4
cb	7.0	87.1
1/4	6.5	87.6
⊕	5.7	88.4

94.13

68

1/4	5.2	88.9
+9	5.1	89.0
cb	4.1	90.0
S	3.4	90.7
	So Concrete Steps at 5.4. - lower step 2.83	91.30
	2+59	
	Concrete Drive at 5.41	3.39 90.74
	2+70	
S	3.7	90.4
cb	4.3	89.8
+1	5.3	88.8
1/4	5.3	88.8
⊕	5.8	88.3
1/4	6.7	87.4
cb	7.1	87.0
N	6.6	87.5
	2+95	
N	6.8	87.3
cb	7.2	86.9
1/4	6.8	87.3
⊕	5.9	88.2
1/4	5.5	88.6
+8	5.2	88.9
cb	4.5	89.6
S	3.7	90.4

94.13

2+98.5

#1 of row of trees on North side 4' Back cb

Line. Shot at base of tree 7.0 87.1

3+13

#2 7.3 86.8

3+25

#3 7.3 86.8

3+38

#4 7.5 86.6

3+54

#5 7.5 86.6

3+69

#6 + last 7.6 86.5

3+20

#1 of row of trees on South side 4' Back of

cb line - Shot at base of tree #1 4.8 89.3

3+45

#2 4.9 89.2

3+70

#3 5.0 89.1

3+95

#4 5.1 89.0

4+20

#5 4.8 89.3

4+25

#6 + last 5.0 89.1

9413

69

T.P

-561 88.52

+2.44 90.96

#3 Concrete Walk 0.5' Back N.L.

4.01

86.95

5

12

89.8

cb

16

89.4

42

23

88.7

14

2.5

88.5

4

3.0

88.0

14

3.8

87.2

cb

4.2

86.8

N

4.2

86.8

3+45

N

4.1

86.9

cb

4.4

86.6

14

4.0

87.0

4

3.0

88.0

14

2.6

88.4

49

2.5

88.5

cb

1.8

89.2

5

1.3

89.7

3+50

#3 Concrete Walk at N.L.

4.15

86.81

90.96

3+70

J	1.5	89.5
cb	2.0	89.0
+1	3.7	87.3
1/4	3.7	87.3
£	3.2	87.8
1/4	4.2	86.8
cb	4.6	86.4
N	4.4	86.6

3+95

N	4.8	86.2
cb	4.6	86.4
1/4	4.3	86.7
£	3.4	87.4
1/4	2.8	88.2
+9	2.9	88.1
cb	1.9	89.1
S	1.5	89.5

4+20

J	1.4	89.6
cb	2.0	89.0
+2	2.8	88.2
1/4	3.0	88.0
£	3.5	87.5
1/4	4.5	86.5
cb	4.9	86.1

90.96

70

N	4.7	86.3
4+45		
N	4.7	86.3
cb	5.0	86.0
1/4	4.5	86.5
£	3.5	87.5
1/4	3.0	88.0
+8	2.9	88.1
cb	2.1	88.9
S	1.6	89.4

4+70

S	1.7	89.3
cb	2.3	88.7
+1	2.9	88.1
1/4	3.2	87.8
£	3.8	87.2
1/4	4.6	86.4
cb	4.9	86.1
N	4.9	86.1

4+89

£ 3 Concrete Mark 3.58 Back N.L. ~ 4.44 86.52

4+95

N	5.1	85.9
cb	5.1	85.9
1/4	4.7	86.3

90.96

¢	3.9	87.1
1/4	3.2	87.8
+ 9	3.0	88.0
cb	2.3	88.7
5	1.8	89.2
5+20		
5	1.8	89.2
cb	2.6	88.4
+ 1	3.3	87.7
1/4	3.2	87.8
¢	3.8	87.2
1/4	4.7	86.3
cb	5.1	85.9
N	5.1	85.9
5+45		
N	4.8	86.2
cb	5.1	85.9
1/4	4.8	86.2
¢	3.9	87.1
1/4	3.4	87.6
+ 9	3.7	87.3
cb	3.0	88.0
5	2.0	89.0

90.96

71

5+70

5	1.4	89.6
cb	2.5	88.5
+ 2	3.9	87.1
1/4	3.6	87.4
¢	4.0	87.0
1/4	4.7	86.3
cb	5.5	85.5
N	4.9	86.1
5+95		
N	4.3	86.7
+ 5	5.5	85.5
cb	5.6	85.4
1/4	4.9	86.1
¢	4.2	86.8
1/4	4.1	86.9
cb	3.8	87.2
+ 5	2.7	88.3
5	2.4	88.6
5+80 to 6+08		
String of 3 Garages 5' Back S.L. - Dirt Floors		
Shot at ¢	2.3	88.7
6+10		
25' Concrete Steps in Wall 0.5' in street from S.L.		
Shot on lower step	1.73	89.23

90.96

6700

7' Concrete steps on New Bldg N.E. Corner -

10' Back N.L. - On lower step 286 88.10

6 #20 = B.L. 29th

S- Top concrete Wall 40.9 91.9

S- Base " " 2.6 88.4

+15 2.8 88.2

0.6 4.0 87.0

1/4 4.3 86.7

1/4 4.5 86.5

1/4 5.2 85.8

0.6 5.6 85.4

N 5.5 85.5

T.P. Bolt in Flange Fire Hydrant S.W. Corner - 1.09

89.87

5-10-29

J.C. Bliss

Drebert

Pawley

X-section 29th St. Ocean

View to Lincoln - 60' wide

10' c 65 - 10' 145

72

B.M. N.W. B.P. Ocean View 29th

98.05

+235 100.40

H1

N.L. Ocean View = 0+00 (Paved)

N.T.P. cb 2.32 98.08

G 3.00 97.40

1/4 2.86 97.54

1/4 2.75 97.65

1/4 2.88 97.52

G 3.13 97.27

E.T.P. cb 2.83 97.57

0+25

E 2.6 97.8

0.6 3.3 97.1

1/4 3.2 97.2

1/4 3.0 97.4

1/4 3.1 97.3

+8 3.4 97.0

0.6 2.7 97.7

W 2.2 98.2

0+50

W 2.3 98.1

0.6 2.9 97.5

+2 3.3 98.9

1/4 3.1 97.3

Plotted to 5/11/29

100.40

♀	3.2	97.2
1/4	3.4	97.0
+8	3.8	96.6
cb	3.3	97.1
E	3.5	96.9

0+75

E	2.8	97.6
cb	3.5	96.9
+2	4.0	96.4
1/4	3.6	96.8
♀	3.2	97.2
1/4	3.3	97.1
+8	3.8	96.6
cb	3.0	97.4
W	2.2	98.2

1+00

W	2.4	98.0
cb	3.2	97.2
+2	4.1	96.3
1/4	3.6	96.8
♀	3.4	97.0
1/4	3.7	96.7
+8	4.2	96.2
cb	3.5	96.9
E	2.9	97.5

100.90

73

1+25

E	2.9	97.5
cb	3.7	96.7
+2	4.6	95.8
1/4	4.1	96.3
♀	3.8	96.6
1/4	3.9	96.5
♀	4.2	96.2
cb	3.8	96.6
+2	3.3	97.1
W	2.4	98.0

1+50

W	3.2	97.2
cb	4.2	96.2
1/4	4.3	96.1
♀	4.4	96.0
1/4	4.7	95.7
cb	5.3	95.1
E	3.9	96.5

1+60 - Start of Concrete Walls on both sides

E-Top concrete wall	0.88	99.52
" Base "	4.1	96.3
W Top concrete Wall	10.55	100.95
" Base "	3.8	96.6

100.40

1775

E	4.8	95.6
cb	5.8	94.6
H	6.3	94.1
1/4	5.7	94.7
⊕	5.3	95.1
1/4	5.4	95.0
+8	6.1	94.3
cb	4.6	95.8
W	4.4	96.0

1789

⊕ 4' Concrete steps in Wall at EL. Lower step 4.59 95.81

2400

W	5.2	95.2
cb	5.8	94.6
+2	7.1	93.3
1/4	6.4	94.0
⊕	6.3	94.1
1/4	6.7	93.7
+9	7.2	93.2
cb	6.6	93.8
E	6.0	94.4

2425

E	7.1	93.3
cb	8.2	92.2
H	9.2	91.2

100.40

74

1/4	8.2	92.2
⊕	7.7	92.7
1/4	7.6	92.8
+8	7.9	92.5
cb	6.7	93.7
W	6.4	94.0

2435

⊕ 5' Concrete steps in Wall at W.L. Lower step 6.20 94.20

2440

⊕ 4' Concrete steps in Wall at W.L. Lower step 7.50 93.90

2450

W	7.6	92.8
cb	8.0	92.4
+3	9.5	90.9
1/4	9.0	91.4
⊕	9.3	91.1
1/4	9.8	90.6
+8	10.5	89.9
cb	9.9	90.5
E	8.9	91.5

2475

E	10.1	90.3
cb	11.2	89.2
+	12.1	88.3
1/4	11.2	89.2

100.90

Q	10.7	89.7
1/4	10.5	89.9
+7	10.9	89.5
cb	9.6	90.8
w	9.0	91.4

3+00 = S.L. Franklin

W-Top concrete wall	5.74	94.66
w-Base " "	10.1	90.30
cb	10.5	89.9
+3	11.1	89.3
+5	11.8	88.6
1/4	11.8	88.6
Q	11.9	88.5
1/4	12.4	88.0
cd	12.9	87.5
+2	12.5	87.9
E-Base Concrete Wall	12.0	88.4
E-Top " "	8.53	91.87

B.M. Bolt in Flange Fire Hydrant S.W

29th + Franklin - 10.53 89.87

8-13-29 X-section Alley Block 76 - Park Villas - Myrtle to Upas - Between Arnold + Villa Terrace - 15' wide

75

B.M. N.W. B.P. Myrtle + Villa Terrace		300.01
+0.54	300.55	
T.P.		-1325 287.30
+0.59	28	
	± 287.89	

S.L. Myrtle = 0+00

E Top existing return	3.26	284.63
G	4.0	283.9
Q	4.4	283.5
G	4.3	283.6
W Top existing return	3.81	284.08

0+09

North edge Concrete Garage Apron S. Side E.L. 4.35 283.54 ✓

0+41

South edge above apron 5.37 282.52 ✓

0+25

W	5.4	282.5
Q	5.6	282.3
E	5.3	282.6
	0+50	

Plotted 8-17-29

E	7.6	280.3
Q	7.5	280.4
W	7.2	280.7

287.89

0475

W	8.8	279.1
☿	9.2	278.7
E	8.9	279.0

0494

28' Concrete drive 3' Back W.L. 10.72 277.17 ✓

1400

E	9.4	278.5
☿	10.1	277.8
W	10.1	277.8

1425

W	11.2	276.7
☿	11.1	276.8
E	10.3	277.6

1450

E	11.9	276.0
☿	12.9	275.0
W	13.4	274.5

T.P.

1405

278.79

1475

W	5.6	273.3
☿	5.1	273.7
E	4.2	274.6

278.79

76

2400

E	5.9	273.0
☿	6.6	272.3
W	6.9	272.0

2425

W	8.1	270.7
☿	7.5	271.4
E	6.8	272.1

2450

E	8.0	270.8
☿	9.1	269.7
W	9.1	269.7

2475

W	10.2	268.6
☿	9.9	269.0
E	8.8	270.0

3400

E	10.2	268.6
☿	10.6	268.2
W	10.9	267.9

3425

W	11.4	267.4
☿	11.4	267.4
E	10.4	268.4

278.79

3751.70 = N.L. Upas

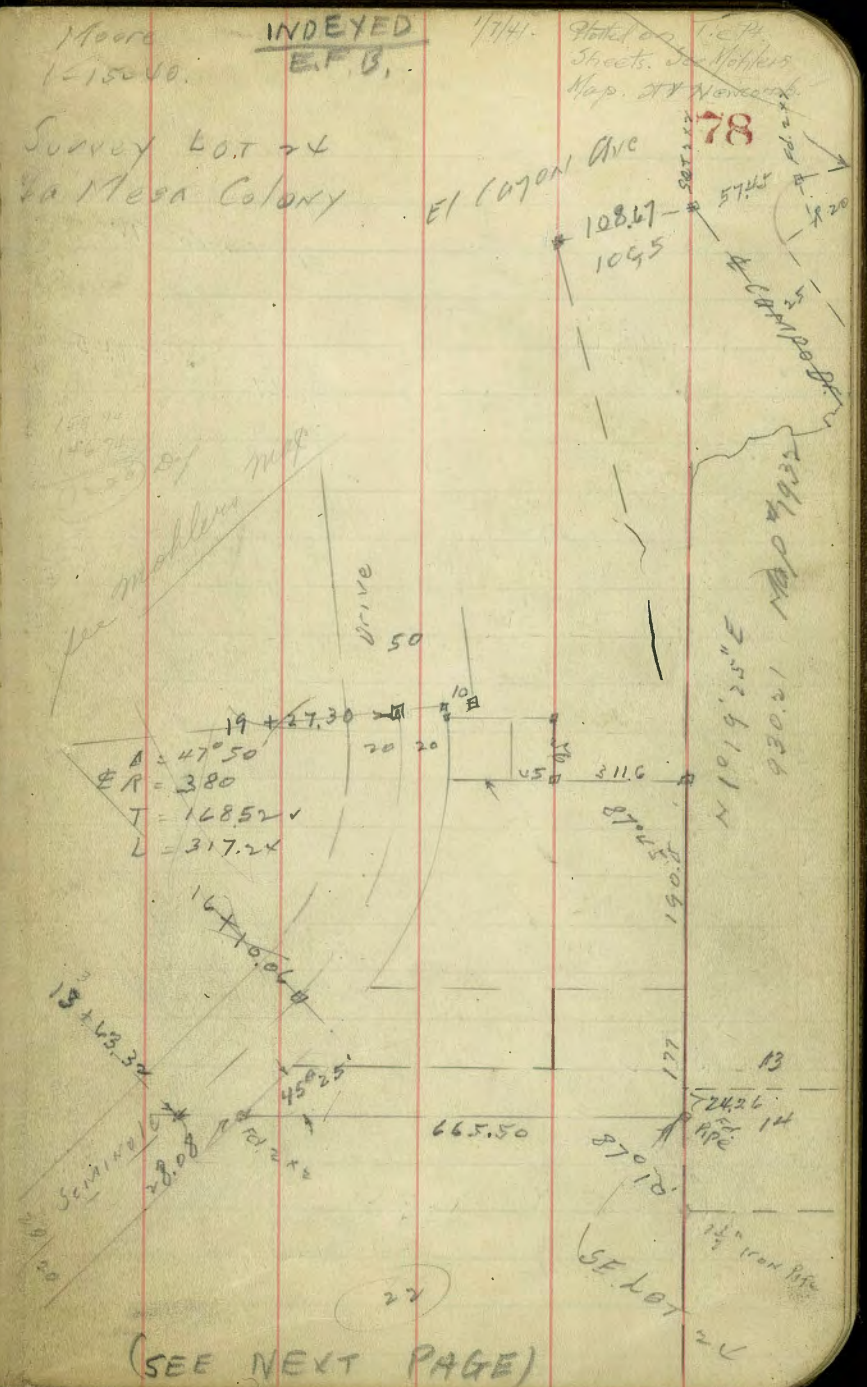
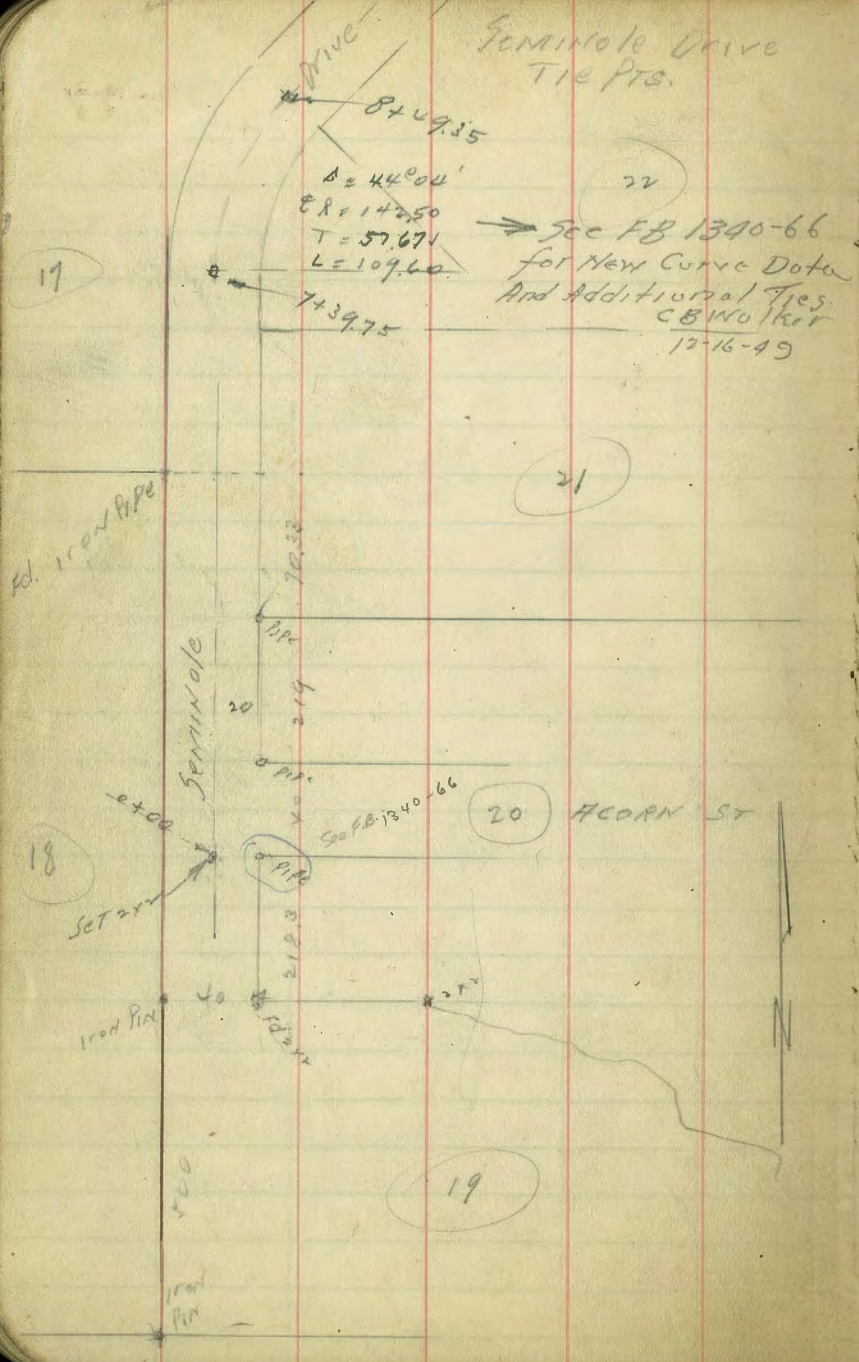
E	11.7	267.4
⊕	12.0	266.8
W	12.1	266.7
T.P.	-143	277.36

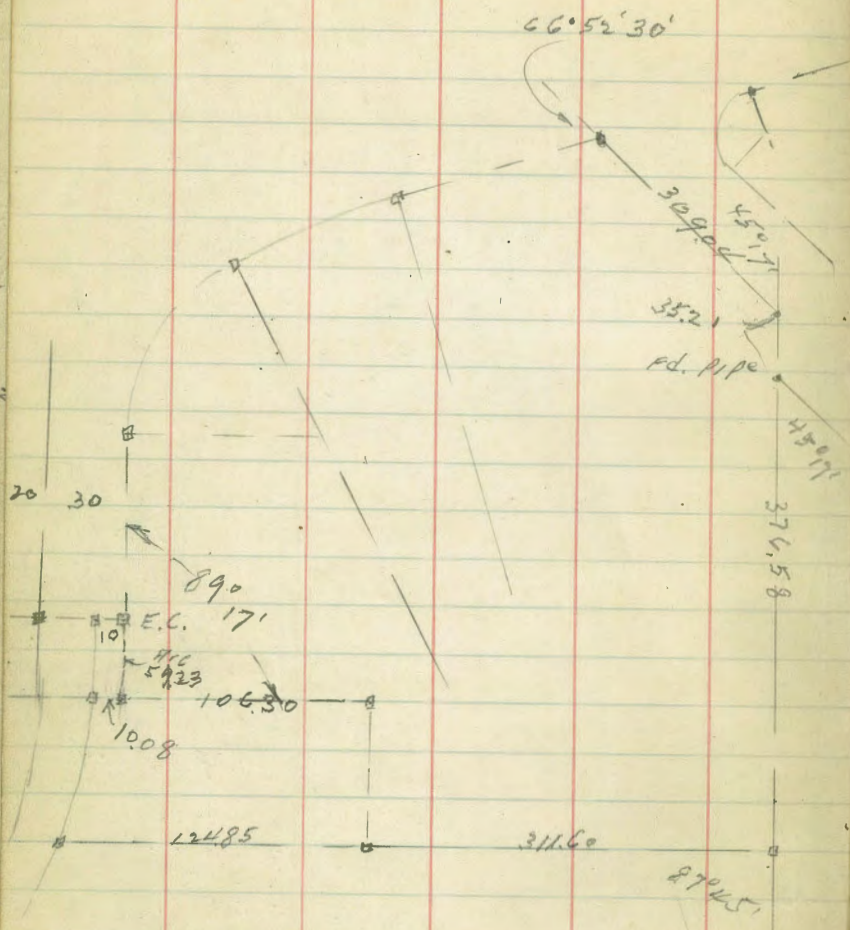
+221 279.57

B.M. S.E. of Myrtle & Arizona - -611 273.46

Correct 273.38

77





DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body

from side stake to slope stake. If ground is not level, the side stake and slope stake, lower target by the amount it cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point and line of sight should cut target.

IMPROVED TABLES AND INFORMATION

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given I may be found by dividing tangent (or external), opposite I by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=10°	I	T	E	I=20°	I	T	E	I=30°
1°	50.00	.218	+	11°	551.70	26.500	+	21°	1061.9	97.577	+
10'	58.34	.297	5° C.	10'	560.11	27.313	5° C.	10'	1070.6	99.155	5° C.
20'	66.67	.388	T	20'	568.53	28.137	T	20'	1079.2	100.75	T
30'	75.01	.491	.03	30'	576.95	28.974	.06	30'	1087.8	102.35	.10
40'	83.34	.606	.001	40'	585.36	29.824	.006	40'	1096.4	103.97	.013
50'	91.68	.733		50'	593.79	30.686		50'	1105.1	105.60	
2°	100.01	.873		12°	602.21	31.561	.006	22°	1113.7	107.24	.013
10'	108.35	1.024		10'	610.64	32.447		10'	1122.4	108.90	
20'	116.68	1.188		20'	619.07	33.347		20'	1131.0	110.57	
30'	125.02	1.364		30'	627.50	34.259		30'	1139.7	112.25	
40'	133.36	1.552		40'	635.93	35.183		40'	1148.4	113.95	
50'	141.70	1.752		50'	644.37	36.120		50'	1157.0	115.66	
3°	150.04	1.964	10° C.	13°	652.81	37.070	10° C.	23°	1165.7	117.38	10° C.
10'	158.38	2.188	T	10'	661.25	38.031	T	10'	1174.4	119.12	T
20'	166.72	2.425	.06	20'	669.70	39.006	.13	20'	1183.1	120.87	.19
30'	175.06	2.674	.003	30'	678.15	39.993	.011	30'	1191.8	122.63	.025
40'	183.40	2.934		40'	686.60	40.992		40'	1200.5	124.41	
50'	191.74	3.207		50'	695.06	42.004		50'	1209.2	126.20	
4°	200.08	3.492		14°	703.51	43.029		24°	1217.9	128.00	
10'	208.43	3.790		10'	711.97	44.066		10'	1226.6	129.82	
20'	216.77	4.099		20'	720.44	45.116		20'	1235.3	131.65	
30'	225.12	4.421		30'	728.90	46.178		30'	1244.0	133.50	
40'	233.47	4.755		40'	737.37	47.253		40'	1252.8	135.35	
50'	241.81	5.100	15° C.	50'	745.85	48.341	15° C.	50'	1261.5	137.23	15° C.
5°	250.16	5.459		15°	754.32	49.441		25°	1270.2	139.11	
10'	258.51	5.829	.09	10'	762.80	50.554	.19	10'	1279.0	141.01	.29
20'	266.86	6.211	E	20'	771.29	51.679	E	20'	1287.7	142.93	E
30'	275.21	6.606	.004	30'	779.77	52.818	.017	30'	1296.5	144.85	.038
40'	283.57	7.013		40'	788.26	53.969		40'	1305.3	146.79	
50'	291.92	7.432		50'	796.75	55.132		50'	1314.0	148.75	
6°	300.28	7.863		16°	805.25	56.309		26°	1322.8	150.71	
10'	308.64	8.307		10'	813.75	57.498		10'	1331.6	152.69	
20'	316.99	8.762		20'	822.25	58.699		20'	1340.4	154.69	
30'	325.35	9.230		30'	830.76	59.914		30'	1349.2	156.70	
40'	333.71	9.710	20° C.	40'	839.27	61.141	20° C.	40'	1358.0	158.72	20° C.
50'	342.08	10.202	T	50'	847.78	62.381	T	50'	1366.8	160.76	T
7°	350.44	10.707		17°	856.30	63.634		27°	1375.6	162.81	
10'	358.81	11.224	E	10'	864.82	64.900	E	10'	1384.4	164.86	E
20'	367.17	11.753	.006	20'	873.35	66.178	.022	20'	1393.2	166.95	.051
30'	375.54	12.294		30'	881.88	67.470		30'	1402.0	169.04	
40'	383.91	12.847		40'	890.41	68.774		40'	1410.9	171.15	
50'	392.28	13.413		50'	898.95	70.091		50'	1419.7	173.27	
8°	400.66	13.991		18°	907.49	71.421		28°	1428.6	175.41	
10'	409.03	14.582	25° C.	10'	916.03	72.764	25° C.	10'	1437.4	177.55	25° C.
20'	417.41	15.184	T	20'	924.58	74.119	T	20'	1446.3	179.72	T
30'	425.79	15.799	.16	30'	933.13	75.488	.32	30'	1455.1	181.89	.49
40'	434.17	16.426	E	40'	941.69	76.869	E	40'	1464.0	184.08	E
50'	442.55	17.065		50'	950.25	78.264		50'	1472.9	186.29	
9°	450.93	17.717	.007	19°	958.81	79.671	.028	29°	1481.8	188.51	.065
10'	459.32	18.381		10'	967.38	81.092		10'	1490.7	190.74	
20'	467.71	19.058		20'	975.96	82.525		20'	1499.6	192.99	
30'	476.10	19.746		30'	984.53	83.972		30'	1508.5	195.25	
40'	484.49	20.447		40'	993.12	85.431		40'	1517.4	197.53	
50'	492.88	21.161		50'	1001.7	86.904		50'	1526.3	199.82	
10°	501.28	21.887	30° C.	20°	1010.3	88.389	30° C.	30°	1535.3	202.12	30° C.
10'	509.68	22.624	T	10'	1018.9	89.888	T	10'	1544.2	204.44	T
20'	518.08	23.375	.19	20'	1027.5	91.399	.39	20'	1553.1	206.77	.59
30'	526.48	24.138	E	30'	1036.1	92.924	E	30'	1562.1	209.12	E
40'	534.89	24.913	.008	40'	1044.7	94.462	.034	40'	1571.0	211.48	.078
50'	543.29	25.700		50'	1053.3	96.013		50'	1580.0	213.86	

T = R tan 1/2 I

E = R exsec 1/2 I

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=40°	I	T	E	I=50°	I	T	E	I=60°
31°	1589.0	216.3	+	41°	2142.2	387.4	+	51°	2732.9	618.4	+
10'	1598.0	218.7	5° C.	10'	2151.7	390.7	5° C.	10'	2743.1	622.8	5° C.
20'	1606.9	221.1	T	20'	2161.2	394.1	T	20'	2753.4	627.2	T
30'	1615.9	223.5	.13	30'	2170.8	397.4	.17	30'	2763.7	631.7	.21
40'	1624.9	226.0	.023	40'	2180.3	400.8	.037	40'	2773.9	636.2	.056
50'	1633.9	228.4		50'	2189.9	404.2		50'	2784.2	640.7	
32°	1643.0	230.9		42°	2199.4	407.6		52°	2794.0	645.2	
10'	1652.0	233.4		10'	2209.0	411.1		10'	2804.9	649.7	
20'	1661.0	235.9		20'	2218.6	414.5		20'	2815.2	654.3	
30'	1670.0	238.4		30'	2228.1	418.0		30'	2825.6	658.8	
40'	1679.1	241.0		40'	2237.7	421.4		40'	2835.9	663.4	
50'	1688.1	243.5		50'	2247.3	425.0		50'	2846.3	668.0	
33°	1697.2	246.1	10° C.	43°	2257.0	428.5	10° C.	53°	2856.7	672.7	10° C.
10'	1706.3	248.7	T	10'	2266.6	432.0	T	10'	2867.1	677.3	T
20'	1715.3	251.3	.26	20'	2276.2	435.6	.34	20'	2877.5	682.0	.42
30'	1724.4	253.9	.046	30'	2285.9	439.2	.075	30'	2888.0	686.7	.112
40'	1733.5	256.5		40'	2295.6	442.8		40'	2898.4	691.4	
50'	1742.6	259.1		50'	2305.2	446.4		50'	2908.9	696.1	
34°	1751.7	261.8		44°	2314.9	450.0		54°	2919.4	700.9	
10'	1760.8	264.5		10'	2324.6	453.6		10'	2929.9	705.7	
20'	1770.0	267.2		20'	2334.3	457.3		20'	2940.4	710.5	
30'	1779.1	269.9		30'	2344.1	461.0		30'	2951.0	715.3	
40'	1788.2	272.6		40'	2353.8	464.6		40'	2961.5	720.1	
50'	1797.4	275.3	15° C.	50'	2363.5	468.4	15° C.	50'	2972.1	725.0	15° C.
35°	1806.6	278.1	T	45°	2373.3	472.1	T	55°	2982.7	729.9	T
10'	1815.7	280.8	.40	10'	2383.1	475.8	.51	10'	2993.3	734.8	.63
20'	1824.9	283.6	E	20'	2392.8	479.6	E	20'	3003.9	739.7	E
30'	1834.1	286.4	.070	30'	2402.6	483.4	.116	30'	3014.5	744.6	.168
40'	1843.3	289.2		40'	2412.4	487.2		40'	3025.2	749.6	
50'	1852.5	292.0		50'	2422.3	491.0		50'	3035.8	754.6	
36°	1861.7	294.9		46°	2432.1	494.8		56°	3046.5	759.6	
10'	1870.9	297.7		10'	2441.9	498.7		10'	3057.2	764.6	
20'	1880.1	300.6		20'	2451.8	502.5		20'	3067.9	769.7	
30'	1889.4	303.5	20° C.	30'	2461.7	506.4	20° C.	30'	3078.7	774.7	20° C.
40'	1898.6	306.4	T	40'	2471.5	510.3	T	40'	3089.4	779.8	T
50'	1907.9	309.3	.53	50'	2481.4	514.3	.68	50'	3100.2	784.9	.84
37°	1917.1	312.2	E	47°	2491.3	518.2	E	57°	3110.9	790.1	E
10'	1926.4	315.2	.093	10'	2501.2	522.2	.151	10'	3121.7	795.2	.225
20'	1935.7	318.1		20'	2511.2	526.1		20'	3132.6	800.4	
30'	1945.0	321.1		30'	2521.1	530.1		30'	3143.4	805.6	
40'	1954.3	324.1		40'	2531.1	534.2		40'	3154.2	810.9	
50'	1963.6	327.1		50'	2541.0	538.2		50'	3165.1	816.1	
38°	1972.9	330.2		48°	2551.0	542.2		58°	3176.0	821.4	
10'	1982.2	333.2	25° C.	10'	2561.0	546.3	25° C.	10'	3186.9	826.7	25° C.
20'	1991.5	336.3	T	20'	2571.0	550.4	T	20'	3197.8	832.0	T
30'	2000.9	339.3	.87	30'	2581.0	554.5	.85	30'	3208.8	837.3	.105
40'	2010.2	342.4	E	40'	2591.0	558.6	E	40'	3219.7	842.7	E
50'	2019.6	345.5		50'	2601.1	562.8		50'	3230.7	848.1	
39°	2029.0	348.6	.117	49°	2611.2	566.9	.189	59°	3		

TABLE X.
MIDDLE ORDINATES OF RAILS
Length of Rail (feet)

C	R	30	28	26	24	22	20	C	R	30	28	26	24	22	20
o /	Feet	Inch	Inch	Inch	Inch	Inch	Inch	o	Feet	Inch	Inch	Inch	Inch	Inch	Inch
0-20	17189	.08	.07	.06	.05	.04	.03	8	716.8	1.88	1.64	1.42	1.20	1.01	.84
0-40	8594	.16	.14	.12	.10	.08	.07	9	637.3	2.12	1.84	1.60	1.35	1.14	.94
1-0	5730	.24	.20	.18	.15	.13	.10	10	573.7	2.36	2.05	1.78	1.50	1.27	1.04
1-20	4297	.31	.27	.23	.20	.17	.13	11	521.7	2.59	2.26	1.95	1.65	1.39	1.15
1-40	3438	.39	.34	.29	.25	.21	.17	12	478.3	3.83	2.47	2.15	1.81	1.54	1.26
2-0	2865	.47	.41	.35	.30	.25	.20	13	441.7	3.05	2.66	2.30	1.96	1.66	1.36
2-20	2456	.55	.48	.41	.35	.29	.23	14	410.3	3.30	2.87	2.48	2.10	1.78	1.46
2-40	2149	.63	.55	.47	.40	.33	.27	15	383.1	3.54	3.08	2.68	2.26	1.91	1.57
3-0	1910	.71	.62	.53	.45	.38	.31	16	359.3	3.76	3.28	2.83	2.40	2.04	1.67
3-20	1719	.78	.68	.59	.50	.42	.35	17	338.3	4.00	3.48	3.02	2.57	2.16	1.78
3-40	1563	.86	.75	.65	.55	.46	.38	18	319.6	4.21	3.67	3.18	2.70	2.28	1.87
4-0	1433	.94	.82	.71	.60	.50	.42	19	302.9	4.45	3.89	3.36	2.86	2.41	1.98
4-20	1323	1.02	.89	.77	.65	.55	.45	20	287.9	4.70	4.09	3.55	3.00	2.54	2.09
4-40	1228	1.10	.96	.83	.70	.59	.48	22	262.0	5.16	4.44	3.84	3.30	2.80	2.29
5	1146	1.18	1.03	.89	.75	.63	.52	24	240.5	5.64	4.92	4.20	3.59	3.04	2.50
6	955.3	1.41	1.23	1.06	.90	.76	.62	26	222.3	6.07	5.29	4.58	3.88	3.29	2.70
7	819.0	1.65	1.44	1.24	1.05	.89	.73								

TABLE XI.
SHORT RADIUS CURVES

Radius Feet	Chord Feet	Central Angle	Deflection Angle	Deflection for 1 Foot
35	10	16-26	8-13	49.3
45	10	12-46	6-23	38.3
50	15	17-16	8-38	34.5
60	15	14-22	7-11	28.8
75	15	11-30	5-45	23.0
100	20	11-30	5-45	17.3
120	20	9-34	4-47	14.3
150	20	7-39	3-49	11.5
190	25	7-32	3-46	9.15
200	25	7-10	3-35	8.6
225	25	6-25	3-12	7.7
240	25	5-58	2-59	7.2
250	25	5-44	2-52	6.9
275	25	5-12	2-36	6.2
288	50	9-58	4-59	6.0
300	50	9-32	4-46	5.7
350	50	8-12	4-06	4.9
376	50	7-40	3-50	4.6
400	50	7-10	3-35	4.3
410	50	7-00	3-30	4.2

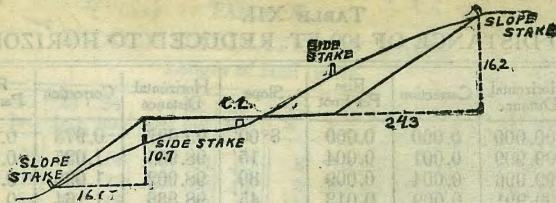
To find length of curve divide angle from P. C. to P. T. by central angle of chord, and multiply by length of chord.

TABLE XII.
INCLINED DISTANCE OF 100 FT. REDUCED TO HORIZONTAL

Slope	Horizontal Distance	Correction	Rise Per Foot	Slope	Horizontal Distance	Correction	Rise Per Foot
0°00'	100.000	0.000	0.000	8°00'	99.027	0.973	0.139
15'	99.999	0.001	0.004	15'	98.965	1.035	0.143
30'	99.996	0.004	0.009	30'	98.902	1.098	0.148
45'	99.991	0.009	0.013	45'	98.836	1.164	0.152
1 00	99.985	0.015	0.017	9 00	98.769	1.231	0.156
15	99.976	0.024	0.022	15	98.700	1.300	0.161
30	99.966	0.034	0.026	30	98.629	1.371	0.165
45	99.953	0.047	0.031	45	98.556	1.444	0.169
2 00	99.939	0.061	0.035	10 00	98.481	1.519	0.174
15	99.923	0.077	0.039	15	98.404	1.596	0.178
30	99.905	0.095	0.044	30	98.325	1.675	0.182
45	99.885	0.115	0.048	45	98.245	1.755	0.187
3 00	99.863	0.137	0.052	11 00	98.163	1.837	0.191
15	99.839	0.161	0.057	15	98.079	1.921	0.195
30	99.813	0.187	0.061	30	97.992	2.008	0.199
45	99.786	0.214	0.065	45	97.905	2.095	0.204
4 00	99.756	0.244	0.070	12 00	97.815	2.185	0.208
15	99.725	0.275	0.074	15	97.723	2.277	0.212
30	99.692	0.308	0.078	30	97.630	2.370	0.216
45	99.657	0.343	0.083	45	97.534	2.466	0.221
5 00	99.619	0.381	0.087	13 00	97.437	2.563	0.225
15	99.580	0.420	0.092	15	97.338	2.662	0.229
30	99.540	0.460	0.096	30	97.237	2.763	0.233
45	99.497	0.503	0.100	45	97.134	2.866	0.238
6 00	99.452	0.548	0.105	14 00	97.030	2.970	0.242
15	99.406	0.594	0.109	15	96.923	3.077	0.246
30	99.357	0.643	0.113	30	96.815	3.185	0.250
45	99.307	0.693	0.118	45	96.705	3.295	0.255
7 00	99.255	0.745	0.122	15 00	96.593	3.407	0.259
15	99.200	0.800	0.126	15	96.479	3.521	0.263
30	99.144	0.856	0.131	30	96.363	3.637	0.267
45	99.087	0.913	0.135	45	96.246	3.754	0.271

TABLE XIII.
MINUTES IN DECIMALS OF A DEGREE.

0 30"	.00833	10' 30"	.17500	20' 30"	.34167	30' 10"	.50833	40' 30"	.67500	50' 10"	.84167
1 00	.01667	11 00	.18333	21 00	.35000	31 00	.51667	41 00	.68333	51 00	.85000
30	.02500	30	.19167	30	.35833	30	.52500	30	.69167	30	.85833
2 00	.03333	12 00	.20000	22 00	.36667	32 00	.53333	42 00	.70000	52 00	.86667
30	.04167	30	.20833	30	.37500	30	.54167	30	.70833	30	.87500
3 00	.05000	13 00	.21667	23 00	.38333	33 00	.55000	43 00	.71667	53 00	.88333
30	.05833	30	.22500	30	.39167	30	.55833	30	.72500	30	.89167
4 00	.06667	14 00	.23333	24 00	.40000	34 00	.56667	44 00	.73333	54 00	.90000
30	.07500	30	.24167	30	.40833	30	.57500	30	.74167	30	.90833
5 00	.08333	15 00	.25000	25 00	.41667	35 00	.58333	45 00	.75000	55 00	.91667
30	.09167	30	.25833	30	.42500	30	.59167	30	.75833	30	.92500
6 00	.10000	16 00	.26667	26 00	.43333	36 00	.60000	46 00	.76667	56 00	.93333
30	.10833	30	.27500	30	.44167	30	.60833	30	.77500	30	.94167
7 00	.11667	17 00	.28333	27 00	.45000	37 00	.61667	47 00	.78333	57 00	.95000
30	.12500	30	.29167	30	.45833	30	.62500	30	.79167	30	.95833
8 00	.13333	18 00	.30000	28 00	.46667	38 00	.63333	48 00	.80000	58 00	.96667
30	.14167	30	.30833	30	.47500	30	.64167	30	.80833	30	.97500
9 00	.15000	19 00	.31667	29 00	.48333	39 00	.65000	49 00	.81667	59 00	.98333
30	.15833	30	.32500	30	.49167	30	.65833	30	.82500	30	.99167
10 00	.16667	20 00	.33333	30 00	.50000	40 00	.66667	50 00	.83333	60 00	1.00000



Distances from Side Stakes for Cross-Sectioning

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	73.00	73.15	73.30	73.45	73.60	73.75	73.90	74.05	74.20	74.35	50

Computed by L. Leland Locke.

20.26
15.2
35.76
50.66
65.86
81.06
101.38

101.3
101.3
20
260

885
15
165

15
1007
105
75
965

435
555
102

2105
5100
2615

890 = 200

100
29
706

1008
15
40
120

1984

3772
49.60
64.88
79.36
99.20

645
585
60
496
383
113

11w7w Willow d 9/corr

456.06	197.06	827.06
+ 0.54	25	93.13
<u>456.60</u>	<u>222.06</u>	<u>920.19</u>
- 4.07	441	
<u>452.53</u>	13	
	<u>428</u>	

456.60	45w.53	45w.53
- 1w.89	4.78	+ 4.29
<u>443.71</u>	<u>456.81</u>	<u>456.82</u>
+ 5.14	- 9.79	
<u>448.85</u>	<u>447.02</u>	<u>45w.53</u>
- 1.69	1.34	+ 3.90
<u>447.25</u>	<u>448.36</u>	<u>456.43</u> ✓
5.90		- 8.26
<u>453.15</u>		<u>448.17</u>
- 1.4w		+ 1.75
<u>451.73</u>		<u>449.92</u>
+ 2.5w		- 12.08
<u>454.25</u>		<u>436.84</u>
1w.76		+ 4.23
<u>441.99</u>		<u>441.07</u>
+ 2.7w		
<u>444.71</u>		
- 1w.59		
<u>432.12</u>		
1.66		
<u>433.78</u>		
- 1.6w		
<u>432.16</u>		

457.43	468.14	100)	160
+ 12.75	49.04	20320	20
<u>470.18</u>	<u>477.18</u>	1524	16
- 46	- 4.84		15
<u>469.72</u> ✓	<u>472.34</u>	3556	1680
+ 8.75	+ 7.6	50.80	240
<u>478.47</u> ✓	<u>479.93</u>	66.04	4070
- 7.16	- 4.42	81.28	3356
<u>471.31</u> ✓	<u>475.53</u>	101.60	516
+ 1.55	+ 5.59		61
<u>472.86</u> ✓	<u>481.12</u>	7500	61
- 6.66	- 3.58	16J	102
<u>466.20</u> ✓	<u>477.54</u>	18J	102
+ 5.58	+ 4.99		6
<u>471.78</u> ✓	<u>482.53</u>		1020
- 6.05	- 5.80		2180
<u>477.83</u>	<u>476.73</u>		102
+ 2.93	+ 4.53		6
<u>480.76</u>	<u>481.26</u>		1020
- 3.40	- 3.73		6
<u>477.36</u>	<u>477.53</u>		1020
+ 6.03	+ 6.34		6
<u>482.39</u>	<u>483.87</u>		1020
- 4.19	- 7.17		6
<u>478.20</u>	<u>476.70</u>		1020
+ 3.02	+ 6.46		6
<u>481.22</u>	<u>483.16</u>		1020
- 5.10	- 33		6
<u>476.12</u>	<u>482.83</u>		1020
+ 3.89	+ 7.62		6
<u>480.01</u>	<u>490.45</u>		1020
- 7.67	- 12.37		6
<u>472.34</u>	<u>478.08</u>		1020
+ 4.84	+ 1.87		6
<u>477.18</u>	<u>479.89</u>		1020
- 9.04	- 10.35		6
<u>468.14</u>	<u>469.54</u>		1020

ENGINEERING DEPARTMENT
 CITY OF
 SAN DIEGO,
 CALIFORNIA