

1302

FIELD

NOTE BOOK

No. 389 F

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CITY OF
SAN DIEGO
CALIFORNIA.

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No. 1000 77 6/30/20 A.H.

$$\begin{array}{r} 53.2 \\ 41.8 \\ \hline 11.4 \end{array}$$

$$\begin{array}{r} 1.55 \\ 8 \overline{) 12.5} \end{array}$$

$$\begin{array}{r} 68.3 \\ 67.5 \\ \hline 5.8 \end{array}$$

$$\begin{array}{r} 76.2 \\ 62.5 \\ \hline 13.7 \end{array}$$

$$\begin{array}{r} 1.55 \\ 21.70 \\ 20.1 \\ 41.8 \end{array}$$

$$\begin{array}{r} 82.6 \\ 20.1 \\ \hline 102.7 \\ 104.4 \\ \hline 1.7 \end{array}$$

$$\begin{array}{r} 5.59 \\ 5.25 \\ \hline .34 \\ A 95d \\ \hline 5.294 \end{array}$$

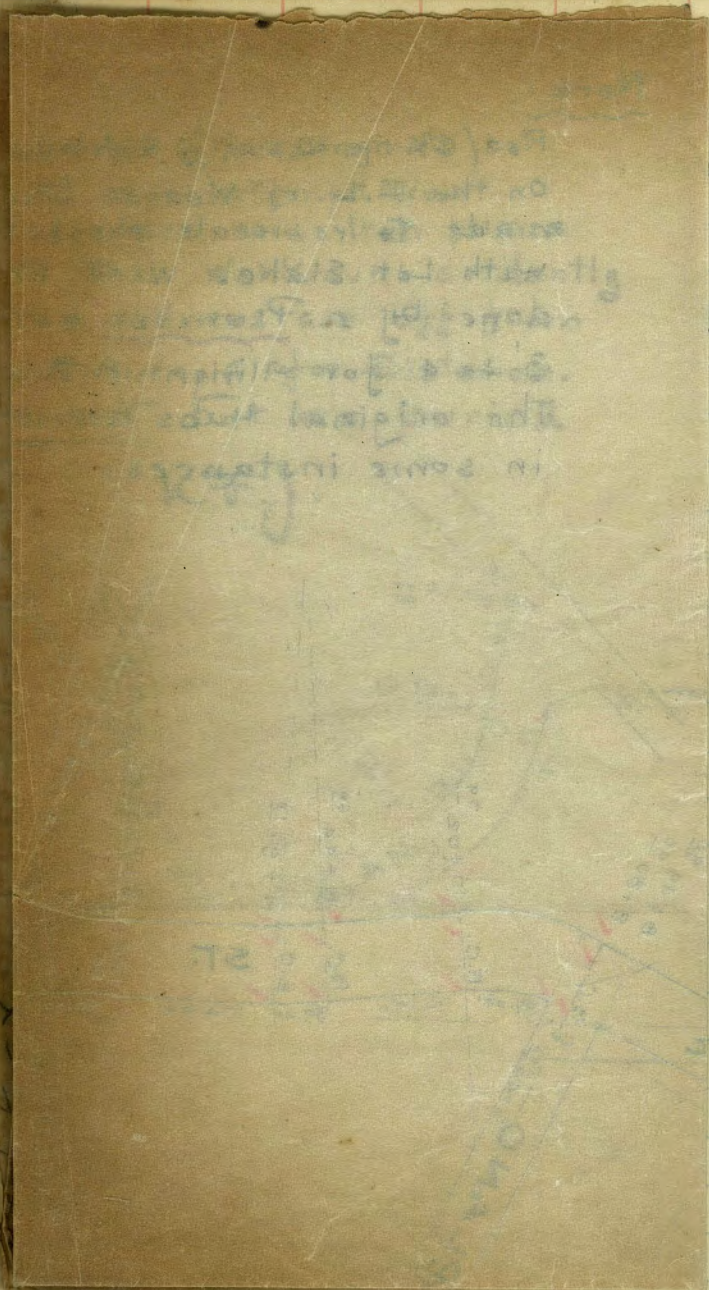
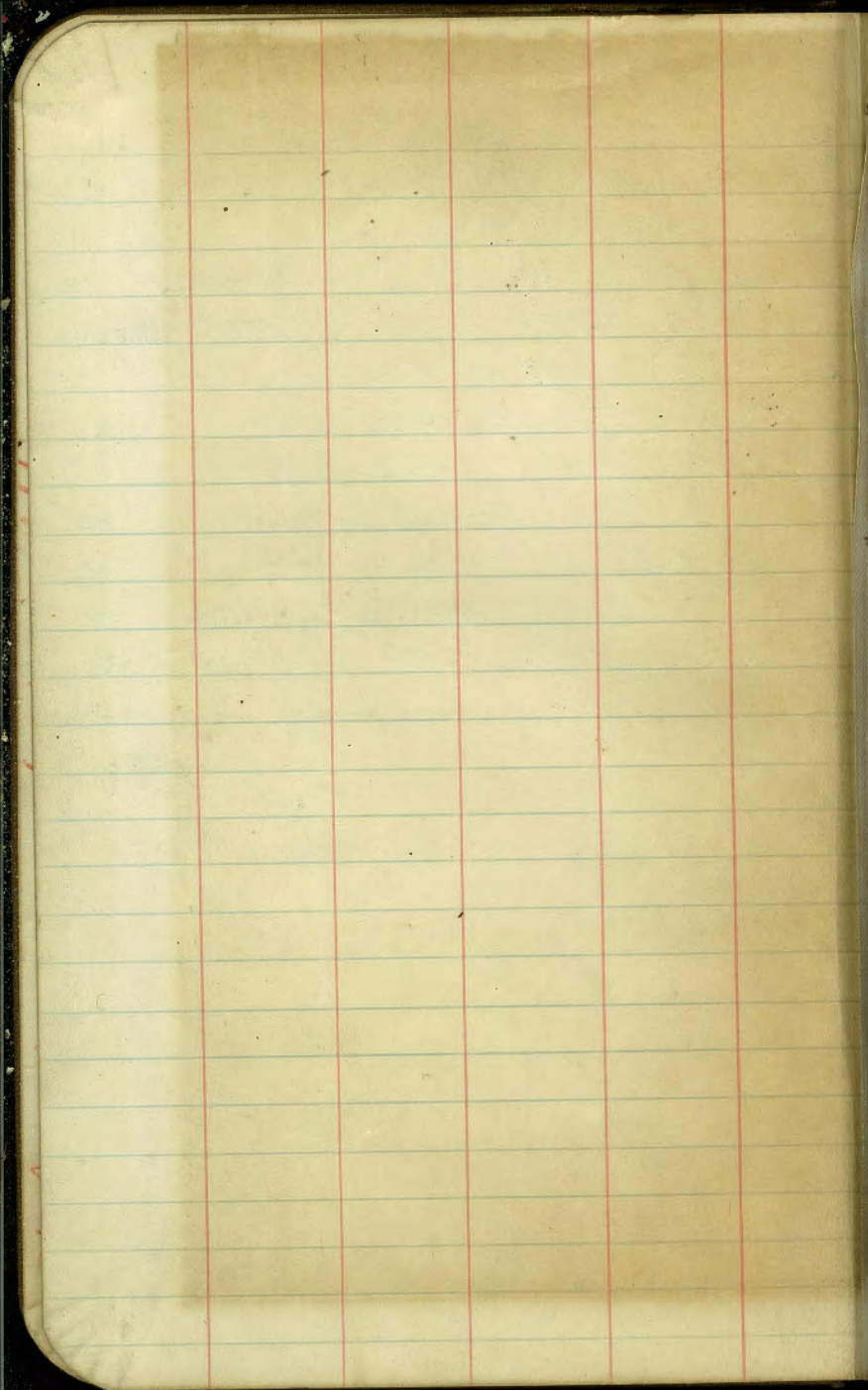
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No. June App 77 6/30/20 A.H.

Note This book was No 194

X. Sec.	WEAVER	Tooley to Burian	1
" "	REPUBLIC	Weaver	11
" "	BURIAN	" Radio Dr	12
" "	DIPPER	" 60 th City Limits	16
" "	ALLISON ST	Turquoise to Archer	20
" "	AGATE ST	Allison to Cass	26
" "	AGATE ST	Allison to Wend.	33
" "	13 th St.	National to Newton	36 ^v
" "	Newton	13 th " 26 th	42
" "	16 th	National to Newton	71
" "	Commercial	13 th " National	73



Dr.

ge

Faint, illegible handwriting on the brown paper, possibly including the words "Dr." and "ge".

BM. Hub NE. Cor. Winnett & Radio Dr.
300.64

" " NE. " Winnet & Orange
330.56

x-section Weaver from S.L. Tooley to Burian.

Republic from E.L. Weaver to Sta. 19 +32.06

2

STA	+	H.I.	-	Elev.
B.M. Hub NE. Cor. Winnet & Radio Dr.				300.64
T.P.	11.08	311.72		
T.P.			0.47	311.25
T.P.	13.00	324.25		
T.P.			0.57	323.68
T.P.	13.12	336.80		
T.P.			0.66	336.14
T.P.	12.70	348.84		
T.P.			0.82	348.02
T.P.	13.15	361.17		
T.P.			0.05	361.12
T.P.	12.56	373.68		
T.P.			0.06	373.62
T.P.	12.31	385.93		
T.P.			0.02	385.91
T.P.	12.26	398.17		
T.P.			0.05	398.12
T.P.	12.18	410.30		
T.P.			0.94	409.36
T.P.	11.95	421.31		
T.P.			1.25	420.06
T.P.	12.76	432.82		
T.P.			0.61	432.31
T.P.	12.20	444.41		
T.P.			0.67	443.74

STA	+	H.I.	-	Elev.
T.P.	11.38	453.12		
T.P.			5.59	447.53
T.P.	4.83	454.36		
T.P. B.M. Bolt in Conc. Base of Flag Pole } inside P.L. Lot 168, Empire Add. } to Encanto Hts. }			3.00	451.36
T.P.	1.24	452.60		
T.P.			12.07	440.53
T.P.	0.56	441.09		
T.P.			13.07	428.02
T.P.	0.81	428.83		
T.P.			12.67	416.16
T.P.	0.63	416.79		
T.P.			13.05	403.74
T.P.	0.94	404.68		
T.P.			12.88	391.80
T.P.	0.64	392.44		
0+00 S.L. Tooley				
+10'			15.9	
W.L.			15.0	377.4
+43'			11.4	381.0
E.L.			5.2	387.2
+10'			4.6	
T.P.			12.75	379.69

Plotted
12-6-28
C.B.H.

STA	+	H.I.	-	Elev.	STA	+	H.I.	-	Elev.
	0.10	379.79 ✓			2+99 ⁴⁵		344.19		3
0+00					E.C.				
					+10'			4.3	
+10'			3.9		E.L.			4.5	339.7
F.L.			3.9	375.9	+30'			5.3	338.9
+30'			3.4	376.4	W.L.			8.4	335.8
W.L.			2.5	377.3	+10'			9.4	
+10'			1.7		3+32				
0+70 ⁵⁰					+10'			11.8	
T.P.			13.05	366.74	W.L.			10.6	333.6
	0.25	366.99 ✓			+30'			7.2	337.0
+10'			2.9		E.L.			6.7	337.5
E.L.			2.9	364.1	+10'			5.8	
+30'			2.1	364.9	3+49 ³⁵				
W.L.			1.6	366.0	N.L. Dipper				
+10'			1.0		+10'			0.7	
1+85					E.L.			2.8	341.4
T.P.			13.05	353.94	+17'			6.6	
	1.34	355.28 ✓			+30'			6.8	336.4
+10'			8.4		W.L.			10.2	334.0
W.L.			7.9	347.4	B.M. Dipper & Weaver			8.29	335.90
+30'			7.0	348.3	T.P.			0.94	343.25
E.L.			5.5	349.8	12.34	355.59 ✓			
+10'			5.5		4+09 ³⁵				
T.P.			13.05	343.17	S.L. Dipper			0.9	
	1.02	344.19 ✓			+10'			3.1	352.5
					E.L.			4.4	
					+8'				

355.59

STA	+	H.I.	-	Elev.
+16			8.2	
+20			7.8	
+30			9.3	346.3
+50			14.5	
W.L.			16.2	339.4
4+50				
+10'			10.5	
W.L.			8.8	346.8
+25			5.8	
+30'			4.3	351.3
+36			1.7	
+46'			0.9	
+48			1.3	
+52' T.P.			0.0	355.59
Hand Level	11.50	367.09		
+56'			9.2	
E.L.			8.0	359.1
+10'			6.0	
T.P.	Instr.	355.59 ✓	0.96	354.63
		12.96		367.59 ✓
5+00				
+10'			3.7	
+3'			4.9	
E.L.			6.5	361.1
+17'			8.9	

367.59

4

STA	+	H.I.	-	Elev.
+30'			11.6	356.0
W.L.			16.8	350.8
+10'			19.2	
5+50				
+10'			19.3	
W.L.			17.0	3506
+35			8.9	57.0 358.7
+40			8.4	
+50			7.6	
+54			6.2	
+68			3.7	361.7
+73			4.6	
E.L. +80			2.6	
+10'			1.1	366.5
6+00			0.0	
+10'			0.0	
E.L.			1.7	365.9
+6'			4.3	
+15'			5.7	
+25'			2.3	361.3
+40'			6.9	
+52'			10.8	
+60'			11.6	356.0
W.L. +80			11.8	
			14.2	
			18.4	349.2
T.P.			13.0	354.59

STA	+	H.I.	-	Elev.	STA	+	H.I.	-	Elev.
	Hand Level	0.0	354.59		7+50		374.98		5 Elev.
+10'			7.8		+10'			7.2	
	T.P.	Instr.	367.59	1.04	366.55	E.L.		9.8	365.2
		8.43	374.98	✓		T.P.		13.0	361.98
6+50					Hand Level	0.00	361.98		360.8
+10'			7.8		20'			4.5	357.5
E.L.			11.3	363.7	+35'			6.6	
	T.P.		13.0	361.98	+40'			7.3	
	Hand Level	0.00	361.98		+45'			9.0	
+35'	20'			359.7	+56'	50'		9.7	352.5
			5.2	356.8	+65'			13.2	
+40'			8.0	353.0				15.6	346.4
+55'	50'		9.5	352.5	W.L. +80			19.0	
+66'			13.0		+10'				
W.L. +80'			15.2	346.8	8+00				
+10'			17.8		+10'			16.8	
7+00					W.L.			14.2	347.8
+10'			19.7		+15'			12.2	
W.L.			16.7	345.3	+27'	30'		8.2	354.0
+17'			13.3		+38'			7.5	
+22'			11.2	352.0	+40'			6.7	
+40'	30'		8.5		+48'	60'		2.6	359.4
+45'			6.0	353.0				361.0	
+70'	+60'			352.0	E.L. +80	Instr.	374.98	10.5	364.5
¢ Pipe	Instr.	374.98	✓	13.1	361.9			6.1	
E.L. +80'			10.6	364.4	+10'				
+10'			7.0						

STA		374.98	H.I.	-	Elev.
8+44 ⁹⁵	N.L. Upland				
+10'				5.0	
E.L.				9.6	365.4
+10'	C. Pipe			12.7	362.0
+20'	20'			13.2	
	T.P.			13.0	361.98
	HandLevel	0.00	361.98		
+40'				4.8	
+43'	50'			5.8	355.8
+55'				6.6	
+62'				8.9	
W.L. +80'				14.8	349.2
+10'				15.0	
8+80 ⁹⁰	B.C.				
+10'				14.6	
W.L.				14.8	349.2
+20'				7.5	356.0
+33'	30'			5.7	
+40'				2.4	
+45'				0.6	361.4 363.6
+75'	60'	Instr.	374.98 ✓	9.8	365.2
E.L. +80'				6.9	368.1
+10'				3.2	
9+05 ⁹⁵	S.L. Upland				
+10'				4.3	

STA		374.98	H.I.	-	Elev. ⁶
E.L.				7.5	367.5
+5'				10.1	
	T.P.			13.0	361.98
	HandLevel	0.00	361.98		
+33'	20'			1.0	361.0
+40'				4.6	
+45'	50'			6.3	355.4
+58'				7.0	
+70'				11.2	
W.L. +80'				12.8	349.2
+10'				14.8	
9+50					
+10'				16.4	
W.L.				14.2	347.8
+15'				10.9	
+23'				7.5	355.0
+37'	30'			6.6	
+40'				5.0	
+45'	60'			2.9	359.1
		Instr.	374.98 ✓		362.2
E.L. +80'				8.6	366.4
+10'				4.7	
10+02 ⁷⁹	E.C.				
+10'				3.6	
E.L.				6.9	368.1

STA	+	H.I.	-	Elev.
+10	ϕ Pipe		10.3	
	T.P.		13.0	361.98
	Hand Level	0.00		360.2
+32			1.3	360.7
+40			5.0	
+50			7.8	354.2
+58			8.2	
+65			10.8	
+75			12.6	
	T.P.		13.0	348.98
		0.00		348.98
W.L. +80			2.2	346.8
+10			5.0	
	Instr.	374.98		
	T.P.		6.14	368.84
		12.46		381.30
10+50				
+10			8.8	
E.L.			13.1	368.2
	T.P.		13.0	368.30
	Hand Level	0.00		363.4
+28			6.0	362.3
+40			11.2	
+45			13.3	355.0
				357.3
	T.P.		13.0	355.30

STA	+	H.I.	-	Elev.
				17
				Elev.
+56			1.5	353.8
+63			4.8	
+80 W.L.			9.0	346.3
+10			11.7	
11+00				
+10			8.3	
W.L.			5.6	349.7
+16			2.2	
	T.P.		0.0	355.30
		13.0		368.30
+23			12.3	357.1
+35			10.2	
+40			8.8	
+45			6.1	
+50			3.9	364.4
+80 E.L.			10.5	367.0
	Instr.	381.30		357.8
+10			6.3	
11+44				
+10			5.9	
E.L.			9.7	374.6
+10	ϕ Pipe		13.7	
	T.P.		13.0	368.30
	Hand Level	0.00		367.6
+30			1.5	366.8

STA	+	H.I.	-	Elev.
		368.30		
+40'			5.9	
+47'	rod		8.0	369.1
+58'			9.3	
+65'			11.9	
	T.P.		13.0	355.30
		0.00	355.30	
+80' W.L.			3.3	352.0
+10'			5.7	
11+70				
+10'			4.5	
W.L.			2.2	353.1
	T.P.		0.0	355.3
		13.0	368.30	
+20'			11.6	
+25'	rod		<u>9.2</u>	→ 359.6
+38'			8.2	
+40'			7.0	
+52'	60' Instr.		<u>2.5</u>	365.8
		381.30 ✓		→ 364.3
+70' φ Pipe			12.6	368.7
+80' E.L.			10.0	371.3
+10'			5.8	
			7.14	374.16 ✓
11+97 ¹⁸	E.C.	5.56	379.72 ✓	
+10'			2.0	

STA	+	H.I.	-	Elev.
		379.72		8
E.L.			7.9	371.8
T.P.			13.0	366.72
HandLevel	0.00	366.72		→ 366.3
+31'			0.6	366.1
+46'	rod		<u>6.7</u>	→ 359.7
+57'			7.4	
+70'			11.9	
	T.P.		13.0	353.72
		0.00	353.72	
W.L.			2.3	351.4
+10'			4.8	
12+50				
+10'			4.0	
W.L.			1.8	351.9
	T.P.		0.0	353.72
		13.0	366.72	
+14'			11.3	
+23'	rod		<u>7.4</u>	→ 359.7
+35'			6.7	
+50'	60'		0.0	366.7
			<u>8.8</u>	→ 367.5
+80' E.L.	Instr.	379.72 ✓		370.9
+10'			4.3	
13+00				
+10'			2.9	
E.L.			7.0	372.7

STA		+	379.72	-	Elev.
+3'				8.5	371.2
+30'	20'			11.4	369.0
	T.P.			13.0	366.72
	Hand Level	0.0	366.72		
+50'	4			5.4	361.3
+59'				6.0	
+67'				10.0	
+80' W.L.				13.0	353.7
+10'				15.2	
13+36					
+10'				14.1	
W.L.				11.9	354.8
+15'				8.4	
+23'				5.4	361.7
+35'	304			4.2	
+48'	60'	Instr.	379.72	12.8	366.9
+80' E.L.				7.6	372.1
+10'				3.0	
13+72 ⁰⁸	B.C.				
+10'				2.0	
E.L.				6.3	373.4
+5'				8.4	369.6
+30'	20'			10.3	
	T.P.			13.0	366.72
	Hand Level	0.00	366.72		

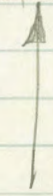
STA		+	366.72	-	Elev.
+48'	50'			5.0	361.6
+60'				5.6	
+70'				8.7	
+80' W.L.				12.0	354.7
+10'				14.6	
14+00	on W.L. of Road				
+10'				14.6	
W.L.				12.3	354.4
+15'				8.7	
+22'				6.0	361.0
+34'	30'			5.6	
		Instr.	379.72		
+55'				9.2	370.7
+70'	60'			8.9	
+75'				9.3	
E.L. 14+00	on E.L. Road			6.2	373.5
+10'				1.9	
	T.P.			6.97	372.75
		7.55	380.30		
14+30	on E.L. of Road				
+10'				1.0	
E.L.				5.1	375.2
+10'				9.5	
+20'	✓			8.6	372.7
+30'				8.9	

STA		+	H.I.	-	Elev.
+40'	T.P.			13.0	367.30
	HandLevel	6.00	367.30	=	362.8
+55'	W			7.0	360.3
+70'				7.8	
+80'				11.0	356.3
14+30	on W.L. Road			14.2	
+10'				16.3	
14+54 ⁴³	E.C. E.L. Road				
+10'	Instr.	380.30	✓	1.4	
E.L.				4.7	375.6
+10'				9.6	
+20'	✓			7.6	372.7
+30'				8.4	
+40'	T.P.			13.0	367.30
	HandLevel	0.0	367.30	=	362.3
+67'	50'			8.0	359.3
+70'				8.4	
+82'				9.5	357.8
+87'				11.4	
14+62 ¹⁸	E.C. on W.L. Road			16.0	351.3
+10'				18.0	
15+00	on E.L. Road				
+10'	Instr.	380.30	✓	1.9	
E.L.				5.7	374.6
+10'				10.3	

STA		+	H.I.	-	Elev.
			380.30		
+20'	✓			7.5	372.8
+30'				8.3	
+40'				10.6	
+45'	T.P.			13.0	367.30
	HandLevel	0.00	367.30		
+60'				3.6	363.7
+80'	754			<u>8.7</u>	359.3
+92'				11.9	
+105'	T.P.			13.0	354.30
		0.00	354.30		
15+00	on W.L. Road			6.0	348.3
+10'				8.0	
15+52 ⁸⁸	NW. Cor. Burian & Weaver				
+10'				11.0	
	W.L.			9.1	345.2
+16'				6.9	
+22'				4.8	350.0
+36'	304			<u>4.0</u>	
+40'				2.7	
	T.P.			0.0	354.30
		13.0	367.30		
+60'	0+00 NW. Cor. Lot 53			11.0	356.3
+80'				9.1	
+100'				5.6	
+120'				2.2	

Sta		H.I.	-	Elev.
+140'			0.0	
+145'	Instr.	380.30 ✓	11.8	
+160'			11.7	
15+81 ⁹³	on N.L. Republic		10.3	
+10'			7.1	
N.L.			10.3	370.0
+9'			12.7	
+20'			13.4	367.1
	T.P.		13.0	367.30
	HandLevel	0.00		367.30
+30'			3.0	
+40'	S.L.		4.4	362.9
+10'			7.4	
16+31 ⁵²				
+10'			5.0	
S.L.			3.8	363.5
+20'	Instr.	380.30 ✓	10.8	369.5
+30'			10.6	
+31'			8.7	
+40' N.L.			6.4	373.9
+10'			4.4	
	T.P.		2.47	377.83
		5.40		383.23 ✓
16+81 ⁶¹				
+10'			3.0	

Plotted 12-6-28
C.B.H.



Sta		H.I.	-	Elev.
		383.23		
N.L.			5.3	377.9
+10'			8.3	
+11'			10.2	
+23'			10.3	373.0
+26'			12.3	
+40' S.L.			15.8	367.4
+10'			18.0	
17+31 ⁷⁰				
+10'			13.6	
S.L.			10.8	372.4
+14'			7.3	
+18'			5.2	378.0
+30'			5.4	
+31'			3.2	
+40' N.L.	T.P.		1.1	382.13
	HandLevel	10.00		392.13
+10'			7.3	
17+81 ⁷⁹				
+10'			3.7	
N.L.			6.5	385.6
+9'			8.8	
+10'			10.7	
+21'	Instr.	383.23	1.40	381.8
+25'			3.2	
+40' S.L.			7.7	375.5

STA	+	383.23 H.I.	-	Elev.
+10'			10.6	
18+31 ⁸⁸				
+10'			7.2	
S.L.			4.0	3792
T.P.			0.81	382.42
	12.21	394.63 ✓		
+13'			11.2	
+17'	not		8.8	385.6
+28'			9.2	
+29'			6.4	
+40' N.L.			4.1	390.5
+10'			1.6	
18+81 ⁹⁷				
+10'			0.0	
N.L.			2.9	391.7
+12'			6.0	
+13'			8.2	
+24'	not		7.8	386.6
+30'			10.6	
+40' S.L.			13.6	381.0
+10'			16.2	
T.P.			3.15	390.88
	8.16	399.04 ✓		
19+32 ⁰⁶				
+10'			20.4	

STA	+	399.04 H.I.	-	12 Elev.
S.L.			17.0	382.0
+10'			12.9	
+14'			10.5	388.0
+24'			11.0	
+25'			8.7	
+40' N.L.			5.1	393.9
+10'			2.3	
Weaver contd. from STA. 15+52 ⁸⁷ = 0+00				
To 1+67 ²⁰				
T.P. See Pg. 8				
	6.00	380.16		374.16
T.P.			12.15	368.01
	1.27	369.28		
T.P.			12.45	356.83
	0.47	357.30 ✓		
0+00 For x-Sect. see Page 10				
0+41 P.C.				
+10'			3.8	353.5
E.L.			5.6	351.7
+10'			8.0	
+30'			10.3	347.0
W.L.			13.5	343.8
+10'			15.2	
0+60				
+10'			15.2	

Plotted 12-6-28
C.B.H.

357.30

STA		+	H.I.	-	Elev.
W.L.				13.7	143.6
+30'				11.4	145.9
+36'				11.3	
+40'				10.0	
E.L.				6.9	150.4
+10'				6.5	
1+04	T.P.			12.70	344.60
		0.11	344.71 ✓		
+10'				0.0	
E.L.				0.2	344.5
+23'				1.6	
+40'				2.1	
+60'				2.3	
+80'				1.3	
+100'				1.0	
1+67 ²⁰	B.C. Beginning of Burian				
+10'				11.8	
W.L.				12.4	332.3
+20'				12.5	332.1
+40'	30E			12.8	
+45'				10.3	
+60' E.L.				8.4	336.3
+10'				6.8	
	T.P.			11.96	332.75
		1.04	333.79 ✓		

333.79

13

STA		+	H.I.	-	Elev.
2+00					
+10'				0.5	
E.L.				2.1	331.8
+15'				4.5	
+20'				6.9	
+40'	30E			7.2	326.6
				7.4	
+60' W.L.				8.1	325.7
+10'				5.3	
2+56					
+10'				11.0	
W.L.				12.7	321.1
+9'				15.8	
+15'				15.9	
+23'				13.6	
+40'	30E			14.4	319.8
+45'				11.6	
+60' E.L.				8.8	325.0
+10'				6.8	
	T.P.			12.25	321.54
		3.40	324.94 ✓		
3+00					
+10'				1.5	
E.L.				4.0	320.9
+17'				8.4	
+19'				12.0	

324.94

STA	+	H.I.	-	Elev.
			11.7	313.1
+36'	304		13.7	
+40'			13.7	
+48'			8.7	316.2
+60' W.L.			6.2	
+10'			15.6	
3+50			18.3	306.6
+10'			19.0	
W.L.			14.5	309.3
+17'			16.8	
+22'			13.3	
+38'	302		8.9	316.0
+43'			6.9	
+60' E.L.			12.95	311.99
+10'			1.05	313.04 ✓
T.P.				
3+99 ²⁰	B.C.		0.0	
+10'			3.0	310.0
E.L.			6.7	
+16'			9.2	303.8
+19'	304		9.2	
+35'			11.3	
+40'			14.2	
+53'			16.4	
+57'				

313.04

14

STA	+	H.I.	-	Elev.
+60' W.L.			16.9	296.1
+10'			14.9	
4+61 ³⁹			5.9	
+10'			8.6	304.4
E.L.			11.7	
+12'			13.0	300.04
T.P.			0.00	300.04
Hand Level			1.9	
+14'			1.5	298.5
+30'	4		3.5	
+35'			8.7	291.3
+60' W.L. (82)			9.8	
+10'				313.04 ✓
T.P.			13.20	299.84
			2.20	302.04 ✓
5+25 ⁴⁹	E.C.		2.0	
+10'			4.1	297.9
E.L.			7.2	
+16'			10.1	
+18'			9.6	292.5
+33'	304		12.5	
+45'			15.5	286.5
+60' W.L.			17.5	
+10'				

302.04

STA	+	H.I.	-	Elev.
S+50.				
+10'			17.4	
W.L.			15.3	286.7
+15'			13.3	
+25'			10.9	
+41'	302		<u>11.2</u>	→ 290.9
+42'			9.4	
+60' E.L.			5.7	296.3
+10'			3.7	
G+00	T.P.		12.12	289.92
		4.74	294.66	✓
+10'			1.6	
E.L.			3.2	291.4
+15'			6.0	
+17'			8.6	
+40'	302		<u>8.6</u>	→ 286.1
+60'			11.4	
+80'			14.8	
+100'			16.5	
G+54.09	N.L.	Radio Rd.		
+10'			11.0	
E.L.			11.1	283.6
+17'			11.6	
T.P.			11.11	283.55 ✓
		3.36	286.91	✓

286.91

STA	+	H.I.	-	Elev.
+22'			6.0	
+40'	302		<u>5.8</u>	→ 280.9
+50'			6.3	
+58'			6.0	
+62'			5.3	
+80'			6.1	
+100'			8.0	
+126'			9.5	
G+69.09	15' South of N.L.	Radio Rd.		
E.L.			7.3	279.6
+20'			7.6	
+40'			8.2	
+60'			9.2	
+80'			10.7	
+100'			14.0	
+130'			13.8	273.1
				283.55 ✓
		8.15	291.70	
T.P.			1.70	290.00
		6.80	296.80	
T.P.			0.43	296.37
		9.12	305.49	
P.M. Hub NE. Cor. Winnet & Radio		<u>300.64</u>	4.94	300.55

X- Section Dipper From Weaver to City Limits.

STA	+	H.I.	-	Elev.	STA	+	H.I.	-	Elev.
BM.	Sec pg. 3			335.90	1+50				
	6.78	342.68 ✓			+10'			6.7	
0+00	W.L. Weaver				S.L.			6.8	3233
+10'			9.1		+30'			7.6	322.5
N.L.			8.8	333.9	+60' N.L.			7.0	323.1
+23'			7.2		+10'			7.0	
+27'			5.7	→ 337.1	2+00				
+45'			5.2		+10'			11.0	
+60' S.L.			3.3	339.4	N.L.			10.9	3192
+10'			1.6		+30'			11.4	319.7
0+50					+60' S.L.			11.6	318.5
+10'			8.0		+10'			11.6	
S.L.			8.5	333.2	T.P.			11.84	318.26
+30'			9.8	332.9		1.20	319.46 ✓		
+60' N.L.			11.4	331.3	2+50				
+10'			11.9		+10'			5.1	
T.P.			13.26	329.42	S.L.			5.0	314.5
	0.68	330.10 ✓			+30'			4.4	315.1
1+00					+60' N.L.			4.6	314.9
+10'			3.1		+10'			4.9	
N.L.			3.2	326.9	2+90				
+30'			3.1	327.0	+10'			8.2	
+60' S.L.			1.5	328.6	N.L.			8.5	311.0
+10'			1.3		+30'			8.5	311.0
					+60' S.L.			9.5	310.0

Plotted 12-7-28 - C.B.H.

330.10

16

319.46

STA	+	H.I.	-	Elev.
			9.6	
3+00				
			11.1	
S.L.			11.4	308.1
			9.3	310.2
+60' N.L.			7.7	311.8
			6.6	
3+15				
			4.0	
N.L.			5.3	314.2
			8.4	311.1
+60' S.L.			10.7	308.9
			11.2	
3+21 ²⁰	Subdivision Line (Sta. on Nit. Dipper)			
			5.4	
S.L.			5.3	314.2
+33.5'			3.6	315.9
+67' N.L.			3.0	316.5
			2.6	
	T.P.		0.87	318.59
		12.13		330.72 ✓
3+61 ²⁰	City Limits			
			8.30	
N.L.			8.5	322.2
+33.5'			8.8	321.9

330.72

STA	+	H.I.	-	Elev.
			8.9	321.8
+67' S.L.				
			8.9	

17
Elev.

GRADES ON 40th
E TO F ST

	W/66	E66
1. L.E. = 00	181.0	181.0
2. 1+60 = PVC	178.0	178.3
+80	177.45	177.75
N	176.75	177.05
+20	175.75	176.05
3. 1+40 = EVC	174.50	174.80
4. 1+60 = ALF ST	149.0	150.0

3) (13.33)

4) (53.33)

Permit # 44111 12/11/21 Cont. R. Leo
Lot 7-8-9 BIK 3 Sun Harbor
Eastside 40th betw. E & F STS

1845/7

	PVC				
1+50	1+60	1+80	2+00	2+20	2+25
178.47	178.30	177.75	177.05	176.05	175.75
6.04	6.21	6.76	7.46	8.26	8.76

12/12/21 Moore

12-20-28 X-section Allison Street
 J.C. Bliss
 Drebert Turquoise to Archer
 Roney 60' wide 10' cbs 10' 145

B.M. S.E. Top Hydrant Turquoise + Allison 107.58

+ 707

X 114.65

N.L. Turquoise = 0+00

Plotted 12/28/28

W	10.7	104.0
cb	10.5	04.2
1/4	10.3	04.4
¢	10.3	04.4
1/4	10.3	04.4
cb	10.5	04.2
+3-Gutter	10.72	03.93
Top cb over catch Basin	9.77	04.88
E	9.6	05.1
	0+00	
E	9.5	105.2
+ 8-10 cb over Catch Basin	9.75	04.90
Gutter	10.71	03.94
cb	10.4	04.3
1/4	10.1	04.6
¢	10.1	04.6
1/4	10.3	04.4
cb	9.6	05.1
+2	7.7	07.0
W	8.0	06.7

T 114.65

20

0+25

W	7.7	107.0
cb	8.0	06.7
+2	8.7	06.0
1/4	9.0	05.7
¢	8.5	06.2
1/4	8.6	06.1
cb	8.2	06.5
+6	7.5	07.2
E	4.8	09.9
	0+50	
E	5.1	109.6
cb	6.6	08.1
+5	7.5	07.2
1/4	7.3	07.4
¢	7.2	07.5
1/4	7.5	07.2
+5	7.6	07.1
cb	7.2	07.5
W	7.2	07.5
	0+75	
W	6.9	107.8
cb	6.6	08.1
1/4	6.4	08.3
¢	6.2	08.5
1/4	6.2	08.5

T 114.65

+5	6.1	108.6
+6	5.1	9.6
cb	5.0	9.7
E	4.7	110.0
1400		
E	4.6	110.1
cb	4.5	110.2
1/4	5.4	109.3
¢	5.3	109.4
1/4	5.8	108.9
cb	5.8	108.9
W	6.2	108.5
1425		
W	5.3	109.4
cb	5.0	109.7
+3	5.5	109.2
1/4	5.2	109.5
¢	4.6	110.1
1/4	4.6	110.1
+6	3.6	111.1
cb	3.7	111.0
E	3.5	111.2
1450		
E	3.0	111.7
cb	3.2	111.5

T 114.65

21

+4	3.2	111.5
+5	4.0	110.7
1/4	3.9	110.8
¢	3.9	110.8
1/4	4.5	110.2
+6	4.9	109.8
cb	4.6	110.1
W	4.9	109.8
1475		
W	4.2	110.5
cb	3.8	110.9
+3	4.3	110.4
1/4	3.8	110.9
¢	3.3	111.4
1/4	3.4	111.3
+6	3.3	111.4
+7	2.6	112.1
cb	2.6	112.1
E	2.3	112.4
2400		
E	1.6	113.1
cb	2.0	112.7
+4	2.1	112.6
+5	2.7	112.0
1/4	2.8	111.9

T 114.65

♀	2.8	111.9
1/4	3.3	111.4
+6	3.6	111.1
+7	3.0	111.7
cb	3.2	111.5
w	3.5	111.2

2+25

w	3.2	111.5
cb	2.9	111.8
+3	3.3	111.4
1/4	2.9	111.8
♀	2.4	112.3
1/4	2.4	112.3
cb	1.5	113.2
E	1.2	113.5

2+50

E	0.9	113.9
2b	1.4	113.3
1/4	2.0	112.7
♀	1.8	112.8
1/4	2.4	112.3
+7	2.7	112.0
cb	2.3	112.4
w	2.7	112.0

T 114.65

22

2+75

w	2.2	112.5
cb	1.6	113.1
+1	2.2	112.5
1/4	1.9	112.8
♀	1.5	113.2
1/4	1.4	113.3
cb	0.9	113.8
E	0.5	114.2

3+0570 = S.L. Agate

80' wide
4.05
13.1/45

E	0.2	114.5
cb	0.3	114.4
1/4	0.7	114.0
♀	0.9	113.8
1/4	1.4	113.3
cb	2.1	112.6
w	2.0	112.7

T. P. - S.W. Paring Stake Allison + Agate

-0.10 114.55

+10.20

T 124.75

5 cb. Agate

w	12.1	112.7
cb	11.6	113.2
1/4	11.0	113.8
♀	10.6	114.2
1/4	10.6	114.2

124.75

cb	10.0	114.8
E	9.8	115.0
S 1/4 Agate		
E	9.5	115.3
cb	9.6	115.2
1/4	10.1	114.7
£	10.3	114.5
1/4	10.4	114.4
cb	11.0	114.8
W	11.5	114.3
£ Agate		
W	11.0	114.8
cb	10.5	114.3
1/4	10.2	114.6
£	10.0	114.8
1/4	9.8	115.0
cb	9.5	115.3
B	9.0	115.8
N 1/4 Agate		
E	8.7	116.1
cb	8.9	115.9
1/4	9.0	115.8
£	9.3	115.5
1/4	9.7	115.1
cb	10.4	114.4

124.75

W	10.7	114.1
N cb Agate		
W	9.8	115.0
cb	9.3	115.5
1/4	9.0	115.8
£	9.0	115.8
1/4	8.7	116.1
cb	8.5	116.3
E	8.3	116.5
N. L. Agate = 0+00		
E	7.9	116.8
cb	8.1	116.7
1/4	8.3	116.5
£	8.5	116.3
1/4	8.7	116.1
cb	9.0	115.8
W	9.3	115.5
0+25		
W	9.0	115.8
cb	8.7	116.1
1/4	8.4	116.4
£	8.0	116.8
1/4	7.7	117.1
cb	7.6	117.2
E	7.3	117.5

124.75

0+50

E	66	118.2
cb	69	117.9
1/4	72	117.6
♀	76	117.2
1/4	79	116.9
cb	83	116.5
w	86	116.2

1+00

w	75	117.3
cb	71	117.7
1/4	68	118.0
♀	65	118.3
1/4	61	118.7
cb	57	119.1
E	55	119.3

1+50

E	41	120.7
cb	45	120.3
1/4	48	120.0
♀	51	119.7
1/4	54	119.4
cb	56	119.2
w	58	119.0

124.75

1+80

w	46	120.2
cb	45	120.3
1/4	41	120.7
♀	38	121.0
1/4	35	121.3
cb	32	121.6
E	27	122.1

1+88

E	25	122.3
cb	29	121.9
1/4	34	121.4
+5	62	118.6
♀	70	117.8
1/4	100	114.8
cb	104	114.4
w	110	113.8

1+95

w	41	120.7
cb	78	117.0
1/4	78	117.0
+9	76	117.2
♀	92	115.6
+9	83	116.5
1/4	68	118.0
+8	67	118.1

24

124.75

cb	8.8	116.0
+8	7.7	117.1
E	2.6	122.2

2+00

E	8.4	116.4
+4	8.2	116.6
+5	6.7	118.1
cb	6.6	118.2
1/4	7.1	117.7
£	6.8	118.0
1/4	6.7	118.1
cb	5.3	119.5
+4	3.9	120.9
W	3.9	120.9

2+19

W	3.4	121.4
cb	3.4	121.4
1/4	3.1	121.7
£	2.7	122.1
1/4	2.4	122.4
cb	1.9	122.9
E	1.8	123.0

2+50

E	0.7	124.1
cb	1.1	123.7

124.75

25

1/4	1.4	123.4
£	1.6	123.2
1/4	1.9	122.9
cb	2.1	122.7
W	2.3	122.5

2+65 = S.L. Archer

W	1.6	123.2
cb	1.5	123.3
1/4	1.2	123.6
£	0.9	123.9
1/4	0.5	124.3
cb	0.3	124.5
E	0.1	124.7

Levels for culvert in ditch on a line that crosses Allison at 2+07 on E.L. and 1488 on W.L.

0+00	7.9	116.9
0+07	7.7	117.1
0+10 = E.L. Allison	6.3	118.5
0+12	4.5	120.3
0+30	7.7	117.6
0+64	8.4	116.4
0+66	10.2	114.6
0+71 = W.L. Allison	11.0	113.8
0+90	11.6	113.2

12-20-28

J.C. Bliss

Drebert

Ranner

X-section Agate Ave - Allison
to Cass - 80' Wide 14' cbs - 13' 1/4s

T 127.29

26

B.M.S. E. Top paving Stake Allison & Agate 114.55

+12.74

T 127.29 ✓

E.L. Allison = 0+00

S	12.7	114.6
cb	12.3	115.0
1/4	11.9	115.4
♀	11.6	115.7
1/4	11.2	116.1
cb	10.9	116.4
N	10.5	116.8

12/28/28 7/1

0+50

N	9.2	118.1
cb	7.8	117.5
1/4	10.1	117.2
♀	10.7	116.6
1/4	10.9	116.4
cb	11.2	116.1
S	11.5	115.8

Plotted

1+00

S	9.8	117.5
cb	9.7	117.6
1/4	9.4	117.9
♀	9.1	118.2
1/4	8.9	118.4

cb	8.5	118.8
N	8.0	119.3

+50

N	6.5	120.8
cb	7.1	120.2
1/4	7.3	120.0
♀	7.4	119.9
1/4	7.6	119.7
cb	8.2	119.1
S	8.2	119.1

2+00

S	6.0	121.3
cb	5.9	121.4
1/4	5.5	121.8
♀	5.2	122.1
1/4	5.1	122.2
cb	5.1	122.2
N	4.9	122.4

2+50

N	2.6	124.7
cb	3.0	124.3
1/4	3.2	124.1
♀	3.4	123.9
1/4	3.5	123.8
cb	3.7	123.6

π 127.29

S	4.3	123.0	
3+00			
S	2.3	125.00	
cb	1.9	125.4	
1/4	1.4	125.9	
♀	1.3	126.0	
1/4	1.0	126.3	
cb	0.9	126.4	
N	0.6	126.7	
T.P.		-0.37	126.92

668

π 133.60

3+50

N	5.1	128.5	
cb	5.3	128.3	
1/4	5.7	127.9	
♀	6.0	127.6	
1/4	6.3	127.3	
cb	6.4	127.2	
S	6.9	126.7	

4+00

S	5.1	129.5	
cb	4.9	129.1	
1/4	4.2	129.4	
♀	4.2	129.4	

π 133.60

27

1/4	4.1	129.5	
cb	3.6	120.0	
N	3.4	130.2	
4+25			
N	2.7	130.9	
cb	2.9	130.7	
1/4	3.5	130.1	
♀	3.6	130.0	
1/4	3.4	130.2	
cb	4.1	130.5	
S	7.5	126.1	
Out 1.5	13.7	119.9	

4+50

Out 1.0	13.2	120.4	
S	9.6	124.0	
cb	3.7	129.9	
1/4	2.6	131.0	
1/3	3.9	129.7	
♀	3.9	129.7	
1/4	3.2	130.4	
cb	1.7	131.9	
N	1.8	131.8	

4+75

N	0.9	132.7	
cb	0.9	132.7	

π 13360

+10	1.5	132.1
1/4	3.9	129.7
+3	4.8	128.8
¢	4.8	128.8
+11	4.6	129.0
1/4	3.7	129.9
cb	7.1	126.5
S	11.5	122.1
Out 20	12.0	121.6
5+40		
Out 20	11.3	122.3
S	11.3	122.3
+10	11.0	122.6
cb	9.2	124.2
1/4	5.6	128.0
¢	6.0	127.6
1/4	5.7	127.9
tr	4.5	129.1
cb	3.7	129.9
N	0.8	132.8
5+15		
N	4.6	129.0
cb	6.6	127.0
1/4	6.4	127.2
¢	5.9	127.7

π 13360

28

+5	5.7	127.9
1/4	8.1	125.5
cb	9.0	124.6
S	11.0	122.6
Out 20	10.9	122.7
5+50		
Out 20	13.3	120.3
Out 10	13.5	120.1
Out 8	11.0	122.6
S	9.5	124.1
cb	8.4	125.2
1/4	7.2	126.4
¢	6.5	127.1
1/4	6.7	126.9
cb	6.4	127.2
N	6.4	127.2
Out 5	6.1	127.5
Out 15	1.0	132.6
5+70		
Out 15	7.1	126.5
N	8.4	125.2
cb	8.7	124.9
1/4	8.7	124.9
¢	9.9	123.7
+10	11.3	122.3

T 13360

14	8.0	125.6
cb	12.0	121.6
S	12.6	121.0
Out 15	2.7	130.9
	6+00	
S	0.0	133.6
+10	0.2	133.4
cb	1.3	132.3
14	4.4	129.2
+3	5.0	128.6
+5	9.8	123.8
¢	9.7	123.7
14	9.2	124.4
cb	7.4	126.2
+7	5.6	128.0
N	5.5	128.1
Out 12	4.7	128.9
Out 14	7.2	126.4
Out 20	7.2	126.4
	6+10	
Out 15	4.1	129.5
N	4.7	128.9
cb	4.8	128.8
+6	4.7	128.9
14	9.0	124.6

T 13360

29

+7	8.6	125.0
¢	3.9	129.7
14	0.5	133.1
+5	+0.2	133.8
cb	0.0	133.6
S	0.2	133.4
	6+13	
S	0.2	133.4
cb	0.1	133.5
+8	0.4	133.2
14	2.1	131.5
¢	3.9	129.7
14	4.3	129.3
cb	4.4	129.2
N	4.9	128.7
Out 15	4.7	128.9
	6+25	
Out 15	3.0	130.6
N	3.6	130.0
cb	3.8	129.8
14	3.5	130.3
¢	2.4	131.2
14	+0.2	133.8
cb	0.0	133.0

π 133.60

S	0.5	133.1
T.P		-0.38
		133.22

+13.04

 π 146.26

S	12.8	133.5
cb	12.3	134.0
1/4	12.0	134.3
♀	12.8	133.5
1/4	13.9	132.4
+4	14.6	131.7
cb	14.2	132.1
N	13.4	132.9
Out 15	12.8	133.5

6+75

N	9.2	137.1
+10	9.5	136.8
cb	11.2	135.1
1/4	12.2	134.1
+3	11.7	134.6
♀	11.4	134.9
1/4	11.4	134.9
cb	11.8	134.5
S	12.5	133.8

7+00

S	10.5	135.8
cb	10.4	135.9

 π 146.26

30

1/4	10.3	136.0
♀	9.9	136.4
1/4	9.9	136.4
cb	8.9	137.4
N	8.9	137.4
1/4	7.9	138.4
cb	7.9	138.4
1/4	8.6	137.7
♀	7.9	138.4
1/4	8.0	138.3
cb	7.9	138.4
S	8.4	137.9

7+50

S	7.0	139.3
cb	6.7	139.6
1/4	6.5	139.8
♀	6.6	139.7
1/4	6.6	139.7
cb	5.9	140.4
N	6.2	140.1

7+75

N	4.5	141.8
cb	4.5	141.8
1/4	5.2	141.1

$\pi 146.26$

¢	5.2	141.1	
1/4	5.2	141.1	
cb	5.5	140.8	
S	5.9	140.4	
8+00			
S	4.7	141.6	
cb	4.4	141.9	
1/4	3.7	142.4	
¢	3.9	142.4	
1/4	4.0	142.3	
cb	3.3	143.0	
N	3.5	142.8	
8+50			
N	1.5	144.8	
cb	1.6	144.7	
1/4	1.9	144.4	
¢	1.8	144.5	
1/4	1.8	144.5	
T.P.		-149	144.77

+10.87

 $\pi 155.64$

cb	11.7	143.9	
S	12.3	143.3	

 $\pi 155.64$

31

9+00

S	10.4	145.2	
cb	10.0	145.6	
1/4	9.3	146.3	
¢	9.5	146.1	
1/4	9.7	145.9	
cb	9.1	146.5	
N	9.1	146.5	

9+50

N	6.6	149.0	
cb	6.7	148.9	
1/4	7.7	147.9	
¢	7.3	148.3	
1/4	7.2	148.4	
cb	7.9	147.7	
S	8.4	147.2	

10+00

S	7.0	148.6	
cb	6.5	149.1	
1/4	5.7	149.9	
¢	5.7	149.9	
1/4	5.4	150.2	
N	4.4	151.2	

10+38

3' Sidewalk at N.L. 2.99 152.65

15564

10+50

N	2.9	152.7
cb	3.6	152.0
1/4	4.6	151.0
¢	5.0	150.6
1/4	4.8	150.8
cb	5.4	150.2
S	6.0	149.6

10+63

6' Concrete Drive at N.L. 2.40 153.24

1	11+00	
S	5.1	150.5
cb	4.1	151.5
1/4	4.0	151.6
¢	3.6	152.0
1/4	3.5	152.1
cb	2.5	153.1
N	2.1	153.5

11+18.7 = W.L. Cass

N	1.4	154.2
cb	1.8	153.8
1/4	2.6	153.0
¢	3.2	152.4
1/4	3.8	151.8
cb	4.5	151.1
S	4.7	150.9

15564

32

T.P.		-8.10	147.54
+1.00	148.54		
B.M. N.W. Nails	Cass + Turquoise	-8.92	139.62
T.P.		-12.69	135.85
+0.38	136.23		
		-10.00	126.23
+0.32	126.55		
		12.87	115.68
+1.10	116.78		
B.M. SE Top Hydrant		-9.17	107.57
			107.58

12-21-28
J.C. Bliss
Drebert
Raney

X-section Gate Ave Allison
to West end. 80' wide
14' obs
13' 1/2

π 115.43

33

B.M. S. E. Paring Stake Gate + Allison

114.55

+0.88

π 115.43

W.L. Allison = 0+00

S	29	112.5
cb	27	112.7
1+	27	113.2
£	14	114.0
14	14	114.0
+8	0.9	114.5
cb	0.6	114.8
N	2.1	115.3
	0+50	
N	2.0	113.4
cb	24	113.0
+10	34	112.0
1+	33	112.1
£	33	112.1
14	41	111.3
+3	3.5	111.9
cb	41	111.3
S	42	111.2
	1+00	
S	6.0	109.4
cb	54	110.0

Plotted 12/29/28
T.S.

+7

14

£

12

+5

cb

N

N

cb

+7

+8

1+

£

1+

+7

cb

S

S

cb

14

£

14

+3

5.0

110.4

5.6

109.8

5.0

110.4

5.2

110.2

4.4

111.0

4.2

111.2

3.6

111.8

1+50

5.1

110.3

5.6

109.8

5.9

109.5

6.8

109.6

6.7

108.7

6.5

108.9

6.9

108.5

6.4

109.0

7.1

108.3

7.3

108.1

2+00

9.1

106.3

8.5

106.9

8.5

106.9

8.1

107.3

8.5

106.9

8.6

106.8

\bar{A} 115.43

+5	7.7	107.7
cb	7.1	108.3
N	6.8	108.6
2+50		
N	8.7	106.7
cb	9.4	106.0
+3	9.1	106.3
1/4	10.2	105.2
¢	9.4	106.0
1/4	10.0	105.4
+5	10.3	105.1
cb	10.0	105.4
J	10.7	104.7
3+00		
S	12.0	103.4
cb	11.5	103.9
+7	11.7	103.7
1/4	11.5	103.9
¢	10.8	104.6
1/4	11.4	104.0
+2	11.7	103.7
+4	10.3	105.1
cb	9.9	105.5
N	9.6	105.8

 \bar{A} 115.43

34

3+50

N	10.8	104.6
cb	11.2	104.2
+7	12.0	103.4
+8	12.9	102.5
1/4	12.9	102.5
¢	12.4	103.0
1/4	12.9	102.5
cb	13.1	102.3
S	13.3	102.1
T.P.		-13.2
		102.31
+4.95		
\bar{A} 107.26		
4+00		
S	6.9	100.4
cb	6.1	101.2
1/4	6.2	101.1
¢	5.5	101.8
1/4	5.9	101.4
+2	5.9	101.4
+3	5.1	102.2
cb	4.7	102.6
N	4.3	103.0
4+40		
N	5.2	102.1
cb	5.7	101.6

T 10726

35

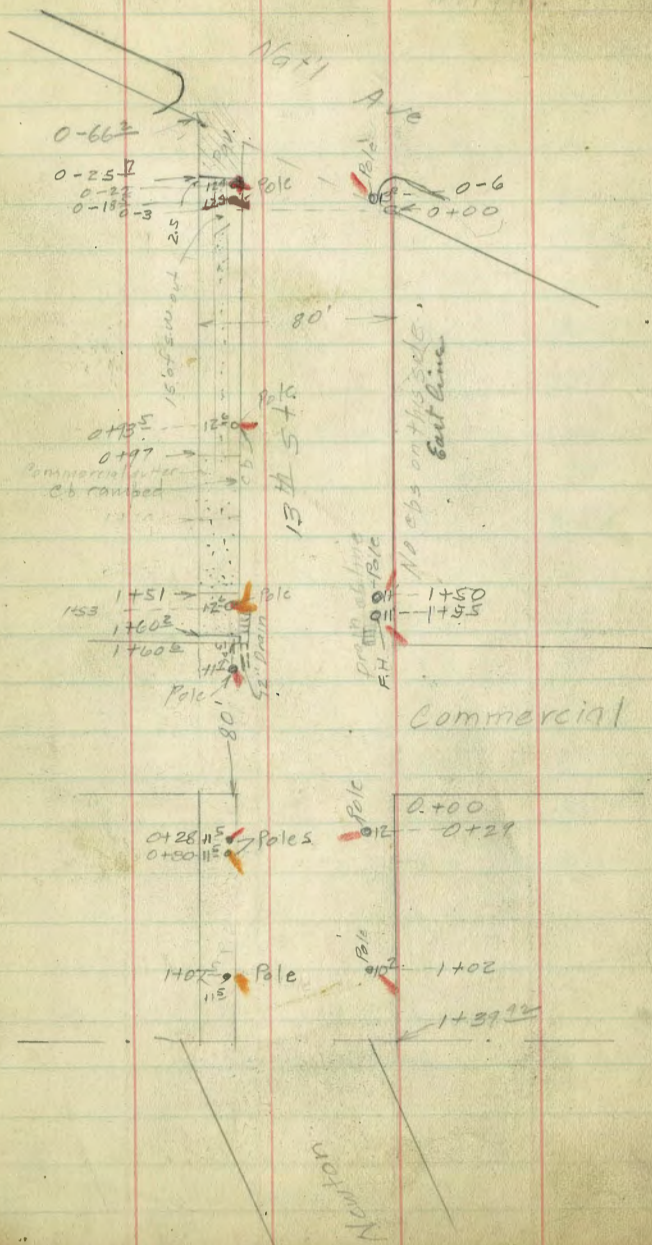
+9	6.3	101.0
+10	7.3	100.0
14	7.2	100.1
6	6.8	100.5
14	7.5	99.8
+5	7.3	100.0
cb	7.6	99.7
5	8.2	99.1

4+80 = West end Agate

5	9.2	98.1
cb	8.5	98.8
+5	8.2	99.1
14	8.6	98.7
6	7.8	99.5
14	8.1	99.2
+3	8.2	99.1
+5	7.4	99.9
cb	7.1	100.2
11	6.4	100.9
T.P.	-1.91	105.35

+1074 116.09

B.M. SE. Paving Stake Allison + Agate - 1.51 114.58
 → 114.55



Plotted 1-18-29 GRB

13
X Sec 19th St. from Nat'l to
Newton. 30'± 14 cbs 52' R/Way.

BM	1.11	7.95	6.89
TR	3.96	8.05	3.86
Elev Sec 0-46 ² on W = 0+00 on E.			
wL	Par	5.46	2.59
cb	✓	6.04	2.01
'A	✓	5.59	2.46
±	✓	5.44	2.61
'Z	✓	5.65	2.40
qt	✓	6.09	1.96
cb	tab cb	5.47	2.58
+13 ²	back walk	5.13	2.92
EL		4.6	3.5
0-23 ²			
E 1/4	Par = Int. with Nat'l	5.65	2.40
±		5.2	2.9
'A		5.3	2.8
+6		5.3	2.8
qt		6.1	1.95
wcb		5.46	2.59
wL	14 cbs	5.06	2.99
0+00			
wL		5.4	2.8
wcb		5.38	2.67
qt		6.1	1.95
+12		5.6	2.4
'A		5.2	2.8
±		5.1	3.0
'A		5.2	2.8

35
BP NE
4th Imp.
673 Rec. changed to
conform more closely to BMS
on Nat'l & Newton.
See P 7 B

Station	8.05	
0+00		
E/A +7	5.5	2.5
eb	5.4	2.6
+5	4.1	3.9
E.L.	4.6	3.5
0+29		
E.L.	5.0	3.1
cb	5.2	2.9
+3	6.2	1.9
+6	5.6	2.5
1/4	5.5	2.6
+	5.2	2.9
1/4	5.2	2.9
+3	5.2	2.9
gut	6.1	1.95
wcb	5.41	2.64
0+50		
w.l.	5.1	2.8
wcb	5.51	2.54
gut	6.1	1.95
+2	5.8	2.3
+7	5.3	2.8
1/4	5.2	2.9
+	5.2	2.9
1/4	5.5	2.6
+6	5.7	2.4
+10	6.4	1.7
eb	5.2	2.9

Station	9.05	37
0+50		
+2	4.9	3.2
+10	5.3	2.8
E.L.	4.9	3.3
0+96 ⁵		
wcb begin of ramp	5.58	2.47
1+00		
E.L.	4.8	3.25
+5	5.3	2.8
eb	5.3	2.8
+1	5.5	2.6
+1	6.4	1.7
+3	6.4	1.7
+6	5.7	2.4
1/4	5.3	2.8
+	5.0	3.1
1/4	5.2	2.9
+12	5.5	2.6
gut	6.0	2.05
wcb	5.88	2.17
w.l.	5.3	2.7
1+09 ⁵		
wcb end ramp	5.95	2.10
1+11		
wcb	5.70	2.35

1+30		8.05		
w.l.		4.9	3.1	
wcb		5.69	2.36	
9vt		6.3	1.75	
+3		5.4	2.7	
1/4		5.1	3.0	
±		5.0	3.05	
1/4		5.3	2.8	
+6		5.5	2.6	
+7		5.9	2.2	
+10		6.4	1.7	
cb		5.2	2.9	
+2		4.9	3.2	
+5		5.2	2.9	
+10		4.9	3.2	
EL		4.2	3.9	
1+39 ^b				
wcb		5.70	2.35	
1+50 ^I				
w.l.		4.90	3.1	
wcb		4.95	3.10	
T.P.	4.70	8.59	4.16	3.89
1+55				
EL		4.8	3.8	
+8		4.8	3.8	
cb		6.0	2.6	
+1		6.9	1.7	
+3		6.8	1.8	

1+55		8.59		38
+6		5.4	3.2	
1/4		5.2	3.4	
±		5.2	3.4	
1/4		5.2	3.4	
+8		5.5	3.1	
+10		5.7	2.9	
+12		6.8	1.8	
9vt		6.8	1.8	
wcb		5.50	3.09	
w.l.		5.48	3.2	
1+60 ^b				
wcb		5.53	3.06	
EL Drain SW.		7.84	0.75	
1+60 ^b = N.E. Commercial				
w.l.		5.5	3.1	
cb		5.8	2.8	
+5		5.2	3.4	
1/4		5.2	3.4	
±		5.1	3.5	
1/4		5.0	3.6	
+7		5.2	3.4	
cb		6.7	1.9	
Job grating Drain NE		7.2	1.4	
EL		5.8	2.8	
rail line + 3 ² E = line + 2 ¹ W.				
EL		5.17	3.42	
±		5.24	3.35	

rail		859	
w.L.		5.61	2.98
rail line + 7° W = line + 8° E.			
w.L.		5.57	3.02
±		5.27	3.32
E.L.		5.31	3.28
N cb Commercial			
E.L.		5.4	3.2
cb		5.4	3.2
1/4		5.1	3.5
±		5.1	3.5
1/4		5.1	3.5
+8		5.1	3.5
cb		5.2	3.4
w.L.		5.3	3.3
N 1/4 Commercial			
w.L.		5.3	3.3
cb		5.3	3.3
+3		5.4	3.2
+6		4.9	3.7
1/4		5.0	3.6
±		5.1	3.5
1/4		4.7	3.7
+11		5.0	3.6
cb		5.2	3.4
E.L.		5.3	3.3

rail		1/4 + 2° E = 1/4 + 2° W.	
E.L.		4.99	3.00
±		5.07	3.52
w.L.		5.08	3.51
rail 1/4 + 7° W = 1/4 + 7° E.			
w.L.		5.20	3.39
±		5.13	3.46
E.L.		4.97	3.62
± Commercial			
E.L.		5.4	3.2
+11		5.4	3.2
cb		5.2	3.4
1/4		5.2	3.4
±		5.2	3.4
1/4		5.1	3.5
cb		5.1	3.5
w.L. MH top		5.36	3.23
rail ± + 5° W = ± + 5° E			
w.L.		5.40	3.19
±		5.23	3.36
E.L.		5.36	3.23
rail ± + 9° E = ± + 9° W			
E.L.		5.37	3.22
±		5.26	3.33
w.L.		5.45	3.14

8.59

S¹⁴ Commercial

w.L.	5.4	3.2
cb	5.2	3.4
+5	5.1	3.5
1/4	5.2	3.4
±	5.1	3.5
1/4	5.1	3.5
cb	5.2	3.4
+8	5.5	3.1
EL	5.5	3.1

S^{cb} Commercial

EL	5.7	2.9
cb	5.6	3.0
+8	5.2	3.4
1/4	5.2	3.4
±	5.4	3.2
1/4	5.2	3.4
cb	5.4	3.2
+10	5.5	3.1
w.L.	5.2	3.3

8.59

S.L. Commercial = 0+00

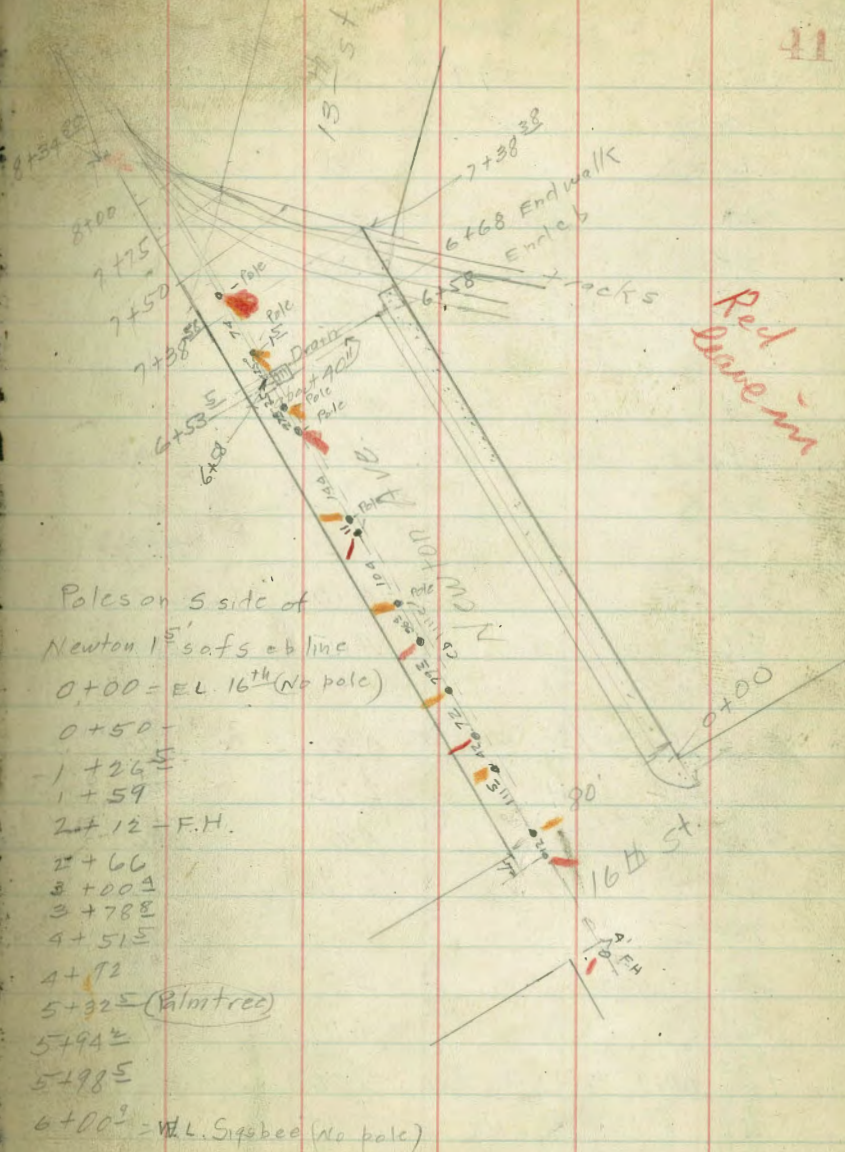
40

w.L.	5.7	2.9
+11	5.9	2.7
cb	6.2	2.4
+4	5.4	3.2
1/4	5.3	3.3
±	5.5	3.1
1/4	5.6	3.0
+5	5.5	3.1
+8	6.7	1.9
cb	6.1	2.5
EL	5.9	2.7

D+50

EL	6.2	2.4
cb	6.4	2.2
+3	6.8	1.8
1/4	6.4	2.2
+7	5.9	2.7
±	5.9	2.7
1/4	6.0	2.6
+10	6.4	2.2
cb	6.7	1.9
w.L.	6.2	2.4

Station	8.59		
WL	6.1	2.5	
cb	6.4	2.2	
+8	6.5	2.1	
1/4	6.2	2.4	
1/2	5.8	2.8	
3/4	6.1	2.5	
cb	6.5	2.1	
EL	6.2	2.4	
1+37 ⁴² = End 13 th			
EL	6.2	2.4	
cb	6.0	2.6	
1/4	5.6	3.0	
1/2	5.5	3.1	
3/4	5.8	2.8	
cb	5.7	2.9	
WL	5.7	2.9	
B.M. Hub NE 13 th & Newton	6.40	2.19	
B.M. Top F.H. NE Commercial & 13 th	2.61	5.98	



Poles on S side of
 Newton 15' safe's e.b. line
 0+00 = EL 16th (No pole)
 0+50 -
 1+26.5
 1+59
 2+12 - F.H.
 2+66
 3+00.9
 3+78.8
 4+51.5
 4+72
 5+32.5 (Palm tree)
 5+94.5
 5+98.5
 6+00.9 = WL Sigsbee (No pole)

X sec Newton Ave. from End
of 13th to 26th

BM. 500	7.19	2.79	Hub NE Kendall 13
End sec. 8+34 ² on South = 7+38 ³² on North			
S.L.	4.0	3.2	
cb	4.1	3.1	
+3 ² top rail	3.66	3.53	
+10 ² on diag. top rail			
+17 ² ✓ top rail	3.75	3.44	
1/4	4.2	3.0	
+14 ⁴ on diag. top rail	3.75	3.44	
⊕	4.2	3.0	
1/4	4.3	2.9	
cb	4.0	3.2	
EL	4.5	2.7	
8+00			
5 cb + 11 Inf.	4.2	3.0	
5 cb + 6 ⁶ top rail	3.75	3.44	
5 cb	4.0	3.2	
S.L.	3.8	3.4	
7+75			
S.L.	3.7	3.5	
1/4	4.1	3.1	
+2 ² top rail	3.76	3.43	
+7 ⁴ ✓ ✓	3.85	3.34	
+9 ² ✓ ✓	3.76	3.43	
⊕	4.2	3.0	
+1 ² top rail	3.81	3.38	
+3 Int.	4.2	3.0	

Plotted Jan 19-29 CBH.

Jan 10-28
London.

7.19

42

7+50		
N ⁴ +10 ² Int.	4.1	3.09
N ⁴ +5 ³ top rail	4.20	2.99
N ⁴ rail & grd.	4.05	3.14
+7 ⁴ rail & grd.	3.90	3.29
+12 ² rail & grd.	3.87	3.32
⊕	3.8	3.4
1/4	3.8	3.4
cb	3.5	3.7
S.L.	3.7	3.5
7+38 ³⁸		
S.L.	3.6	3.6
cb	3.2	4.0
1/4	3.6	3.6
⊕	3.8	3.4
+8 ² top rail & grd.	3.90	3.29
1/4	3.9	3.3
+1 rail & grd.	3.90	3.29
cb	4.1	3.1
+1 ² rail	4.10	3.09
+7 ⁶ rail	4.21	2.98
N.L.	4.5	2.7

7.19

7+305

N.L. rail	4.23	2.96
7+22 ² rail		
N.L. rail	4.20	2.99
7+00		
N.L.	4.3	2.9
cb	4.1	3.1
+10	4.8	2.4
1/4	4.7	2.5
1/4	4.2	3.0
1/4	3.9	3.3
cb	3.8	3.4
S.L.	3.6	3.6
6+97		
N.L. rail	4.26	2.93
6+88 ⁷		
N.L. rail	4.22	2.97
6+58 = End cb on North.		✓
S.L.	3.7	3.5
+8	3.6	3.6
cb	4.7	2.5
+10	4.2	3.0
1/4	4.1	3.1
1/4	4.5	2.7
1/4	4.8	2.4
Neb	5.19	2.00
+12	4.9	2.3

7.19

43

6+58

N.L.	4.5	2.7
at 6+53 ^E		
FL. Drain on Seb line	12.20	- 5.01
top box	5.55	1.64
6+00		
Neb	4.63	2.56
gut	5.4	1.79
1/4	4.9	2.3
1/4	4.6	2.6
1/4	4.1	3.1
cb	3.7	3.5
S.L.	3.7	3.5
5+50		
S.L.	3.8	3.4
cb	3.9	3.3
1/4	4.2	3.0
1/4	4.4	2.8
1/4	4.6	2.6
gut	4.9	2.29
Neb	4.37	2.82

7.19

5+00

Ncb	4.10	3.09
gut	4.8	2.4
1/4	4.4	2.8
+	4.0	3.2
1/4	4.0	3.2
cb	3.6	3.6
S.L.	3.5	3.7

4+50

S.L.	3.5	3.7
cb	3.6	3.6
+6	4.3	2.9
1/4	4.1	3.1
+	3.7	3.5
1/4	4.4	2.8
gut	4.6	2.6
Ncb	3.88	3.31

4+00

Ncb	3.53	3.66
gut	4.5	2.7
+6	4.7	2.5
1/4	4.3	2.9
+	3.6	3.6
1/4	4.0	3.2
+8	4.3	2.9
cb	4.1	3.1
S.L.	3.4	3.8

44

7.19

T.P.	2.41	7.26	2.42	4.77
3+50				
S.L.			3.6	3.7
+5			3.7	3.6
cb			4.4	2.9
+4			4.8	2.5
1/4			4.1	3.2
+			3.7	3.6
1/4			4.9	3.0
gut			4.7	2.6
Ncb			3.77	3.49
3+00				
Ncb			4.05	3.21
gut			5.1	2.2
1/4			4.6	2.7
+			4.0	3.3
1/4			4.2	3.1
+9			4.9	2.4
cb			4.8	2.5
+9			3.8	3.5
S.L.			3.7	3.6

7.26

15

2+50

7.26

S.L.	3.6	3.7
+5	3.9	3.4
cb	5.1	2.2
+3	5.2	2.1
1/4	4.4	2.9
±	4.2	3.1
1/4	4.8	2.5
+9	5.2	2.1
gut	5.0	2.3
Ncb	4.24	3.02
2+100		
Ncb	4.55	2.71
gut	5.1	2.2
+4	5.4	1.9
1/4	5.0	2.3
±	4.5	2.8
1/4	4.7	2.6
+10	5.3	2.0
cb	5.2	2.1
S.L.	4.1	3.2

1+70

S.L.	4.4	2.9
+9	4.8	2.5
cb	5.4	1.9
+3	5.5	1.8
1/4	4.8	2.5
+8	4.5	2.8
±	4.6	2.7
1/4	5.1	2.2
gut	5.2	1.9
Ncb	4.75	2.51
1+35		
Ncb	4.85	2.41
gut	5.5	1.8
1/4	5.3	2.0
±	4.4	2.9
1/4	4.6	2.7
+7	5.5	1.8
+11	5.6	1.7
cb	5.3	2.0
+6	4.7	2.6
S.L.	4.5	2.8

7.26

1+00

S.L.	4.3	3.0
cb	5.0	2.3
+4	5.7	1.6
1/4	4.9	2.4
+9	4.1	3.2
±	4.3	3.0
1/4	5.2	2.1
gut	5.3	2.0
Ncb	5.01	2.25
0+50		
Ncb	5.26	2.00
gut	5.7	1.6
1/4	5.2	2.1
±	4.5	2.8
1/4	5.2	2.1
cb	5.4	1.9
S.L.	5.1	2.2
0+10		
S.L.	4.2	3.1
cb	5.4	1.9
1/4	5.1	2.2
±	4.6	2.7
1/4	5.0	2.3
+6	5.3	2.0
gut	5.8	1.5
Ncb	5.47	1.79

7.26

0+00 = W.L. 16th st.

46

Ncb	5.44	1.82
gut	5.8	1.5
1/4	5.0	2.3
±	4.7	2.6
1/4	4.8	2.5
cb	4.4	2.9
S.L.	4.4	2.9
16 th 60' st 10' cbs 40' Rdway.		
Wcb 16 th		
S.L.	5.3	2.0
cb	4.5	2.8
+3	5.2	2.1
+5	4.6	2.7
1/4	5.1	2.2
±	5.0	2.3
1/4	5.2	2.1
cb	5.5	1.8
NL gut	5.6	1.7
NL to bcb	5.42	2.84

7.26

W 1/4 16th

N.L.	5.2	2.1
cb	5.5	1.8
+11	5.0	2.3
1/4	5.1	2.2
±	5.7	1.6
1/4	5.6	1.7
cb	5.4	1.9
+8	5.1	2.2
+12	5.7	1.6
S.L.	4.8	2.5
± 16 th		
S.L.	4.7	2.6
cb	5.2	2.1
1/4	5.0	2.3
±	4.8	2.5
1/4	4.7	2.6
cb	5.2	2.1
N.L.	4.7	2.6
E 1/4 16 th		
N.L.	4.9	2.4
cb	5.1	2.2
1/4	4.8	2.5
±	4.6	2.7
1/4	4.7	2.6
cb	5.0	2.3
+7	4.3	3.0

7.26

47

E 1/4 16th

+10	4.9	2.4
S.L.	4.2	3.1
E cb 16 th		
S.L.	4.1	3.2
cb	4.9	2.4
1/4	4.7	2.6
±	4.6	2.7
1/4	4.8	2.5
cb	5.1	2.2
N.L. gut	5.0	2.3
N.L. top cb	5.37	1.89
0+00 = E.L. 16 th		
Ncb	5.42	1.84
gut	5.0	2.3
1/4	4.7	2.6
±	4.4	2.9
1/4	4.9	2.4
cb	4.8	2.5
S.L.	3.9	3.4
0+25		
S.L.	3.8	3.5
cb	4.0	3.3
+7	4.8	3.5
1/4	4.7	2.6
±	4.5	2.8

7.26

0+25

1/4	4.5	28
gut	4.4	29
Ncb.	4.96	230

0+50

Ncb	4.35	291
gut	3.9	34
1/4	4.3	30
+	4.3	3.0
1/4	4.5	28
+6	4.6	27
cb	4.2	31
+6	3.4	39
+10	3.4	39
S.L.	3.8	35

0+82⁵

S.L.	3.6	37
cb	3.6	37
1/4	3.9	34
+	3.9	34
1/4	3.9	34
gut	3.3	4.0
Ncb	3.82	3.44

7.26

rail 0+88⁸N = 0+88⁵S

Ncb line	3.71	3.54
+	3.84	3.42
S.L.	3.58	3.68

rail 0+93²S = 0+93²N

S.L.	3.52	3.74
+	3.72	3.54
Ncb line	3.63	3.63

1+00

Ncb	3.21	4.05
gut	3.4	3.9
1/4	3.5	3.8
+	3.5	3.8
1/4	3.4	3.9
cb	3.4	3.9
S.L.	3.4	3.9

1+26³

Seb	3.02	4.24
gut	3.4	3.9
1/4	3.1	4.2
+	3.0	4.3
1/4	2.9	4.4
+4	2.9	4.4
gut	3.0	4.3
Ncb	2.64	4.62

48

2+50 16.6P
 +11 9.6 7.0
 gut 9.6 7.0
 Neb 8.91 7.70

3+00
 Neb 7.75 8.86
 gut 8.4 8.2
 1/4 8.0 8.6
 + 8.1 8.5
 1/4 8.3 8.3
 gut 9.3 7.3
 Seb 8.49 8.12

3+50
 Seb 7.33 9.28
 gut 7.9 8.7
 1/4 7.0 9.6
 + 6.9 9.7
 1/4 7.0 9.6
 +8 6.7 9.9
 gut 7.4 9.2
 Neb 6.60 10.01

4+00 16.6P
 Neb 5.43 11.18
 gut 6.1 10.5
 1/4 6.0 10.6
 + 5.7 10.9
 +8 6.0 10.6
 1/4 6.0 10.6
 gut 6.8 9.8
 Seb 6.13 10.48

4+50
 Seb 5.16 11.45
 gut 5.6 11.0
 1/4 4.9 11.7
 +8 4.5 12.1
 + 4.5 12.1
 1/4 5.0 11.6
 +8 5.3 11.3
 gut 5.0 11.6
 Neb 4.20 12.41

5+00
 Neb 3.23 13.38
 gut 4.0 12.6
 1/4 4.0 12.6
 + 3.4 13.2
 1/4 3.6 13.0
 +4 3.8 12.8

5+00	16.80		
gut	4.6	12.0	
Scb	3.98	12.63	
5+50			
Scb	2.85	13.76	
gut	3.5	13.1	
+10	2.4	14.2	
1/4	2.3	14.3	
±	2.2	14.4	
1/4	2.3	14.3	
gut	2.7	13.9	
Ncb	1.98	14.63	
5+92			
Ncb	0.99	15.62	
gut	1.5	15.1	
1/4	1.5	15.1	
±	1.5	15.1	
1/4	1.6	15.0	
gut	2.4	14.8	
Scb	1.99	14.62	

51

6+00 ^g = W.L. Sigsbee	16.80		
Scb	1.69	14.92	
gut. Pav	2.30	14.31	
1/4 ✓	1.94	14.67	
± ✓	1.56	15.05	
1/4 ✓	1.46	15.15	
gut ✓	1.40	15.20	
Ncb	0.75	15.86	
sw Newton. 2 Sigsbee			
B.M. 13.07	28.02	1.66	14.95 (14.91)
0+00 = E.L. Sigsbee.			
Ncb	11.14	16.08	
gut Pav	11.81	16.21	
1/4 ✓	11.87	16.15	
± ✓	11.79	16.03	
1/4 ✓	12.31	15.71	
gut ✓	12.67	15.35	
Scb	12.16	15.86	
0+39			
Scb	11.50	16.52	
gut	12.0	16.02	
1/4	10.7	17.3	
+3	10.5	17.5	
±	10.6	17.4	
1/4	10.8	17.2	
+9	10.7	17.3	
gut	11.0	17.0	
Ncb	10.44	17.58	

1+00		28.02	
Ncb	9.30	18.72	
gut	10.0	18.0	
1/4	10.0	18.0	
+	9.8	18.2	
1/4	9.7	18.3	
+6	10.1	17.9	
gut	11.0	17.0	
Scb	10.35	17.67	
1450			
Scb	9.40	18.62	
gut	10.1	17.9	
1/4	8.9	19.1	
+9	8.8	19.2	
+	8.9	19.1	
1/4	9.2	18.8	
+8	9.1	18.9	
gut	9.3	18.7	
Ncb	8.43	19.59	
2+00			
Ncb	7.54	20.48	
gut	8.6	19.4	
1/4	8.2	19.8	
+10	8.3	19.7	
+	8.0	20.0	
+8	7.9	20.1	
1/4	8.1	19.9	

2+00		28.02	
gut	9.3	18.7	
Scb	8.47	19.55	
2+50			
Scb	7.58	20.44	
gut	8.2	19.8	
1/4	7.1	20.9	
+9	7.0	21.0	
+	7.0	21.0	
1/4	7.4	20.6	
+9	7.2	20.8	
gut	7.4	20.6	
Ncb	6.57	21.45	
3+00			
Ncb	5.70	22.32	
gut	6.4	21.6	
1/4	6.3	21.7	
+10	6.3	21.7	
+	6.2	21.8	
+7	6.0	22.0	
1/4	6.2	21.8	
gut	7.4	20.6	
Scb	6.64	21.38	

28.02

3+50		
Scb	5.74	22.28
gut	6.4	21.6
1/4	5.2	22.8
±	5.1	22.9
1/4	5.3	22.7
+7	5.0	23.0
gut	5.2	22.8
Ncb	4.70	23.32
4+00		
Ncb	3.69	24.33
gut	4.6	23.4
1/4	4.3	23.7
±	4.1	23.9
1/4	4.3	23.7
+4	4.5	23.5
gut	5.4	22.6
Scb	4.82	23.20
4+50		
Scb	3.86	24.16
gut	4.4	23.6
1/4	3.4	24.6
+9	3.2	24.8
±	3.3	24.7
1/4	3.4	24.6
gut	3.3	24.7
Ncb	2.85	25.17

28.02

53

5+00		
Ncb	1.90	26.12
gut	2.3	25.7
1/4	2.4	25.6
±	2.4	25.6
+9	2.4	25.6
1/4	2.5	25.5
gut	3.6	24.4
Scb	2.93	25.09
5+50		
Scb	1.98	26.04
gut	2.7	25.3
1/4	1.6	26.4
+9	1.4	26.6
±	1.5	26.5
1/4	1.7	26.3
+7	1.6	26.4
gut	1.7	26.3
Ncb	1.00	27.02
5+94		
Ncb	0.21	27.81
gut	0.7	27.1
1/4	0.9	27.1
±	0.8	27.2
1/4	0.8	27.2
gut	1.8	26.2
Scb	1.20	26.82

2802

6+01⁶ = W.L. Beardsley

Scb		1.08	26.94	
gut	Par.	1.59	26.43	
1/4	✓	1.27	26.75	
+	✓	1.10	26.92	
1/4	✓	0.87	27.15	
gut	✓	0.83	27.19	
Ncb		0.05	27.97	
BM	5.72	33.68	0.06	27.96

0+00 = E.L. Beardsley

Ncb		5.66	28.02
gut	Par.	6.40	27.28
1/4	✓	6.42	27.26
+	✓	6.52	27.16
1/4	✓	6.80	26.88
gut.	✓	7.06	26.62
Scb		6.65	27.03
0+10			
Scb		6.68	27.00
gut	33.1	7.1	26.6
1/4		6.4	27.3
+6		6.0	27.7
+		5.8	27.7
+5		5.7	28.0
1/4		5.7	28.0
+8		5.8	27.9
gut		6.2	27.5

0+10 33.68

Ncb		5.68	28.00
0+50			
Ncb		5.51	28.17
gut		6.2	27.5
1/4		5.7	28.0
+		5.6	28.1
1/4		6.0	27.7
+7		6.3	27.4
gut		7.0	26.7
Scb		6.52	27.16
1+00			
Scb		6.38	27.30
gut		7.0	26.7
+7		6.3	27.4
1/4		5.9	27.8
+		5.6	28.1
1/4		5.5	28.2
gut		5.7	28.0
Ncb		5.28	28.40
1+50			
Ncb		5.24	28.44
gut		5.6	28.1
1/4		5.5	28.2
+		5.5	28.2
+8		5.6	28.1
1/4		5.8	27.9

54

33.68

1+50		
+8	6.2	27.5
qut	6.8	26.8
Seb	6.21	27.47
2+00		
Seb	6.06	27.62
qut	6.5	27.2
1/4	5.6	28.1
+	5.3	28.4
1/4	5.4	28.3
qut	5.3	28.4
Neb	5.07	28.61
2+50		
Neb	4.69	28.99
qut	5.3	28.4
1/4	5.2	28.5
+	5.1	28.6
1/4	5.4	28.3
qut	6.3	27.4
Seb	5.89	27.79

33.68

55

3+00		
Seb	5.63	28.05
qut	6.1	27.6
1/4	5.2	28.5
+	4.9	28.8
1/4	5.1	28.6
qut	5.2	28.5
Neb	4.71	28.97
3+50		
Neb	4.56	29.12
qut	5.1	28.6
1/4	4.9	28.8
+	4.8	28.9
1/4	5.0	28.7
+3	5.1	28.6
qut	6.0	27.7
Seb	5.56	28.12
4+00		
Seb	5.38	28.30
qut	5.9	27.8
+10	4.8	28.9
1/4	4.8	28.9
+	4.6	29.1
1/4	4.7	29.0
qut	4.9	28.8
Neb	4.35	29.33

A+50		
Ncb	4.21	29.47
gut	4.8	28.9
1/4	4.5	28.2
+	4.4	29.3
1/4	4.7	29.0
+4	4.8	28.9
gut	5.8	27.9
Scb	5.16	28.52

5+00

Scb	5.08	28.60
gut	5.5	28.2
+10	4.3	29.4
1/4	4.2	29.6
+	4.2	29.5
1/4	4.3	29.4
gut	4.5	29.2
Ncb	3.95	29.73

5+50

Ncb	3.84	29.84
gut	4.4	29.3
1/4	4.0	29.7
+	4.0	29.7
1/4	4.3	29.4
gut	5.3	28.4
Scb	4.80	28.88

6+00^S = W.L. Crosby
3368

Scb	4.70	28.98
gut	5.2	28.5
1/4	4.4	29.3
+	3.9	29.8
1/4	3.7	29.8
gut	4.1	29.6
Ncb	3.63	30.05

Crosby 60' wide 10' cbs 40' Rdway

Wcb Crosby

NL topcb	3.60	30.08
NL gut	4.1	29.6
cb	3.9	29.8
1/4	3.8	29.9
+	3.9	29.8
1/4	4.3	29.4
cb	4.8	28.9
SL gut	5.5	28.2
SL topcb	4.66	29.08

W 1/4 Crosby

SL	4.9	28.8
cb	4.5	29.2
1/4	4.2	29.5
+	3.8	29.9
1/4	3.6	30.1
cb	3.6	30.1
NL	3.5	30.2

33.68

± Crosby

NL	3.4	30.3
cb	3.4	30.3
1/4	3.9	29.8
±	3.7	30.0
1/4	4.1	29.6
cb	4.4	29.3
SL	4.6	29.1
E 1/4 Crosby		
SL	4.7	29.0
cb	4.6	29.1
1/4	4.4	29.3
±	4.2	29.5
1/4	4.1	29.6
cb	3.8	29.9
NL	3.4	30.3
Ecb Crosby		
NL tob cb	3.61	30.07
NL gut	4.3	29.4
cb	4.5	29.2
1/4	4.5	29.2
±	4.8	28.9
1/4	4.9	28.8
cb	5.0	28.7
SL gut	5.1	28.6
SL topcb	4.65	29.03

33.88

sw Newton Crosby

B.M.	8.27	37.31	4.66	29.02	28.93
E.L. Crosby = 0+00					
Seb			8.30	29.01	
gut			8.6	28.7	
1/4			8.5	28.8	
±			8.2	29.1	
1/4			8.1	29.2	
gut			7.8	29.5	
Ncb			7.36	29.95	
0+16					
Ncb			7.26	30.05	
gut			8.1	29.2	
1/4			7.6	29.7	
±			7.6	29.7	
1/4			7.7	29.8	
1/4			7.7	29.4	
gut			8.6	28.7	
Seb			8.31	29.00	
0+50					
Seb			8.19	29.12	
gut			8.6	28.7	
1/4			7.5	29.8	
±			7.4	29.9	
1/4			7.4	29.9	
gut			7.9	29.4	
Ncb			7.20	30.11	

1+00		37.81	
Neb.	7.06	30.25	
put	7.6	29.7	
1/4	7.2	30.1	
±	7.3	30.0	
1/4	7.4	29.9	
put	8.2	29.1	
Seb	8.09	29.22	

1+50			
Seb	7.89	29.42	
put	8.1	29.2	
1/4	7.1	30.2	
±	7.1	30.2	
1/4	7.2	30.1	
put	7.3	30.0	
Neb	6.91	30.40	

2+02			
Neb	6.69	30.62	
put	7.3	30.0	
1/4	7.1	30.2	
±	6.9	30.4	
1/4	7.1	30.2	
put	8.0	29.3	
Seb	7.69	29.62	

2+50			
Seb	7.45	29.86	
put	7.7	29.4	
1/4	6.9	30.4	
±	6.8	30.5	
1/4	6.9	30.4	
put	7.1	30.2	
Neb	6.56	30.75	

3+00			
Neb	6.32	30.99	
put	7.0	30.3	
1/4	6.7	30.6	
±	6.5	30.8	
1/4	6.8	30.5	
put	7.8	29.5	
Seb	7.29	30.02	

3+50			
Seb	7.13	30.18	
put	7.6	29.7	
1/4	6.6	30.7	
±	6.4	30.9	
1/4	6.6	30.7	
put	6.8	30.5	
Neb	6.17	30.14	

3731

4+00		
Ncb	6.01	31.30
gut	6.7	30.6
1/4	6.4	30.9
+	6.3	31.0
1/4	6.4	30.9
gut	7.3	30.0
Seb	7.00	30.31

4+50		
Seb	6.50	30.81
gut	7.3	30.0
1/4	6.2	31.1
+	6.1	31.2
1/4	6.3	31.0
gut	6.4	30.9
Ncb	5.86	31.45

5+00		
Ncb	5.72	31.59
gut	6.3	31.0
1/4	6.1	31.2
+	6.0	31.3
+8	6.0	31.3
1/4	6.2	31.1
gut	7.1	30.2
Seb	6.66	30.65

5+50	3730	59
Seb	6.38	30.93
gut	6.8	30.5
1/4	6.0	31.3
+	5.8	31.5
1/4	5.7	31.6
gut	6.1	31.2
Ncb	5.52	31.79

6+01 ⁶ = W.L. Dewey		
Ncb	5.32	31.99
gut Paw	6.04	31.27
1/4 ✓	5.78	31.53
+	5.72	31.59
1/4 ✓	6.24	31.07
gut ✓	6.99	30.32
Seb	6.30	31.01
NW Newton's Dewey		
BN 8.66	40.67	5.30 32.01 31.95

0+00 = E.L. Dewey		
Seb	9.72	30.95
gut Paw	10.27	30.40
1/4 ✓	9.77	30.90
+	9.37	31.30
1/4 ✓	9.32	31.35
gut ✓	9.32	31.35
Ncb	8.64	32.03

40.67

0 + 10

Ncb		8.66	32 01
gut	40.7	9.2	31 5
1/4		8.7	32 0
+		8.9	31.8
1/4		9.2	31 5
gut		9.8	30 9
Scb		9.73	30.94
0 + 50			
Scb		9.30	31 37
gut		9.5	31 2
1/4		8.8	31 9
+		8.6	32.1
1/4		8.5	32 2
gut		8.7	32 4
Ncb		8.26	32 41
1 + 00			
Ncb		7.55	33 12
gut		8.3	32 4
1/4		8.1	32 6
+		8.0	32.7
1/4		8.2	32 5
gut		8.2	32 5
Scb		8.74	31.93

40.67

Ends at 2 + 44

60

1 + 50 = begin com gutter on south			
Scb		8.09	32 58
gut		8.7	32 0
1/4		7.7	33 0
+5		7.4	33 3
+		7.4	33 3
1/4		7.6	33 1
gut		7.8	32 9
Ncb		6.98	33 69
2 + 00			
Ncb		6.55	34 12
gut		7.3	33 4
1/4		7.1	33 6
+		6.9	33 8
1/1		7.1	33 6
1/4		7.2	33 5
gut		8.1	32 6
Scb		com gutter.	
2 + 50			
Scb	407	7.01	33.66
gut		7.7	33 0
1/4		6.6	34 1
+7		6.3	34 4
+		6.3	34.4
+9		6.3	34 4
1/4		6.7	34 0
gut		6.6	34 1

4067

2+50		
Neb	5.94	34.73
3+00		
Neb	5.46	35.21
gut	6.1	34.6
1/4	6.1	34.6
+	5.8	34.9
+6	5.8	34.9
1/4	6.2	34.5
gut	7.2	33.5
Seb	6.44	34.23
3+50		
Seb	5.94	34.73
gut	6.6	34.1
1/4	5.6	35.1
+7	5.3	35.4
+	5.3	35.4
1/4	5.5	35.2
gut	5.8	34.9
Neb	4.83	35.84

4067

61

4+00		
Neb	4.32	36.35
gut	5.1	35.6
1/4	5.0	35.7
+	4.7	36.0
1/4	4.9	35.8
gut	6.0	34.7
Seb	5.32	35.35
4+50		
Seb	4.79	35.88
gut	5.4	35.3
1/4	4.3	36.4
+	4.1	36.6
1/4	4.3	36.4
gut	4.6	36.1
Neb	3.78	36.89
5+00		
Neb	3.25	37.42
gut	4.0	36.7
1/4	3.7	37.0
+	3.6	37.1
1/4	3.8	36.9
+3	3.9	36.8
gut	5.0	35.7
Seb	4.24	36.43

40.67

5450

Scb	3.73	36.94
prt	4.4	36.3
1/4	3.3	37.4
+6	3.1	37.6
♀	3.1	37.6
1/4	3.2	37.5
prt	3.5	37.2
Ncb	2.70	37.97

6+00⁶ = WL EVANS

Ncb	2.21	38.46
prt	2.7	38.0
1/4	2.8	37.9
♀	2.6	38.1
1/4	2.9	37.8
prt	3.7	37.0
Scb	3.24	37.43

Web Evans

SL top cb	3.21	37.46
SL prt	4.4	36.3
cb	3.6	37.1
1/4	3.2	37.5
♀	2.8	37.9
1/4	2.6	38.1
cb	2.5	38.2
NL prt	2.4	38.3
NL top cb	2.20	38.47

40.67

62

W 1/4 EVANS

NL	1.9	38.8
cb	2.1	38.6
1/4	2.4	38.3
♀	2.7	38.0
1/4	3.0	37.7
cb	3.5	37.2
SL	4.0	36.7

♀ EVANS

SL	3.6	37.1
cb	3.3	37.4
1/4	2.8	37.9
♀	2.4	38.3
1/4	2.1	38.6
cb	2.0	38.7
NL	1.7	39.0

F 1/4 EVANS

NL	1.6	39.1
cb	2.1	38.6
1/4	2.4	38.3
♀	2.7	38.0
1/4	3.0	37.7
cb	3.2	37.5
SL	3.3	37.4

Ecb Evans		40.67	
S.L top cb	3.16	37.51	
gut	3.7	37.0	
cb	3.6	37.1	
1/4	3.4	37.3	
+	3.0	37.7	
1/4	2.7	38.0	
cb	2.5	38.2	
NL gut	2.5	38.2	
NL top cb	2.18	38.49	
EL EVANS = 0+00			
Ncb	2.14	38.53	
gut	2.5	38.2	
1/4	2.5	38.2	
+	2.4	38.3	
1/4	2.8	37.9	
gut	3.6	37.1	
Seb	3.17	37.50	
S.W. Newton & Evans			
B.M. 5.51	42.98	3.20	37.47 (37.40)
0+50			
Seb	5.49	37.49	
gut	5.9	37.1	
+10	4.9	38.1	
1/4	4.8	38.2	
+9	4.5	38.5	
+	4.6	38.4	

0+50		42.98	
1/4	4.6	38.4	
+8	4.6	38.4	
gut	5.0	38.0	
Ncb	4.52	38.46	
1+00			
Ncb	4.55	38.43	
gut	4.9	38.1	
1/4	4.8	38.2	
+	4.7	38.3	
+5	4.7	38.3	
1/4	5.1	37.9	
gut	5.8	37.2	
Seb	5.54	37.44	
1+50			
Seb	5.57	37.41	
gut	6.0	37.0	
1/4	5.2	37.8	
+	4.9	38.1	
1/4	5.0	38.0	
gut	5.0	38.0	
Ncb	4.54	38.44	

42.98

2+00

Ncb	4.66	38.32
gut	5.1	37.9
1/4	5.1	37.9
+	5.1	37.9
1/4	5.3	37.7
gut	6.0	37.0
Scb	5.66	37.32

2+50

Scb	5.64	37.34
gut	6.0	37.0
1/4	5.3	37.7
+	5.1	37.9
1/4	5.1	37.9
gut	5.1	37.9
Ncb	4.66	38.32

3+00

Ncb	4.67	38.31
gut	5.3	37.7
1/4	5.2	37.8
+	5.2	37.8
+9	5.3	37.7
1/4	5.5	37.5
gut	6.2	36.8
Scb	5.70	37.28

42.98

3+50

Scb	5.78	37.20
gut	6.3	36.7
1/4	5.6	37.4
+5	5.3	37.7
+	5.2	37.8
1/4	5.2	37.8
gut	5.2	37.8
Ncb	4.76	38.22

4+00

Ncb	4.80	38.18
gut	5.4	37.6
1/4	5.3	37.7
+	5.2	37.8
+9	5.4	37.6
1/4	5.5	37.5
gut	6.4	36.6
Scb	5.87	37.11

4+50

Scb	5.89	37.09
gut	6.4	36.6
1/4	5.5	37.5
+	5.5	37.5
1/4	5.3	37.7
gut	5.5	37.5
Ncb	4.82	38.16

64

5400	42.98		
Neb		4.95	38.03
gut		5.5	37.5
1/4		5.0	38.0
+7		5.1	37.9
+		5.3	37.7
1/4		5.7	37.3
gut		6.5	36.5
Seb		5.98	37.00
5450			
Seb		5.92	37.06
gut		6.6	36.4
1/4		5.6	37.4
+		5.1	37.9
+4		5.1	37.9
1/4		5.1	37.9
+9		5.2	37.8
gut		5.5	37.5
Sw. Newton & Samson			
B.M.	4.84	41.86	5.96 37.02 (36.97)
Neb		3.76	38.10

65

6401 = W.L. Samson	4186		
Neb		3.81	38.05
gut	Par	5.00	36.86
1/4	✓	4.53	37.33
+	✓	4.71	37.15
1/4	✓	5.04	36.82
gut	✓	5.43	36.43
Seb		4.84	37.02
0400 = F.L. Samson			
Seb		4.86	37.00
gut	Par	5.45	36.41
1/4	✓	5.06	36.80
+	✓	4.69	37.17
1/4	✓	4.56	37.30
gut	✓	4.44	37.42
Neb		3.84	38.02
0409			
Neb		3.84	38.02
gut		4.4	37.50
1/4		4.4	37.5
+		4.3	37.5
1/4		4.5	37.4
gut		5.2	36.7
Seb		4.93	36.93

0450 41.86

Scb	5.00	36.86
gut	5.6	36.3
1/4	4.6	37.3
+	4.5	37.4
1/4	4.6	37.3
gut	4.7	37.2
Ncb	4.05	37.81
1+00		
Ncb	4.23	37.63
gut	4.9	37.0
1/4	4.7	37.2
+	4.6	37.3
+9	4.6	37.3
1/4	4.8	37.1
gut	5.7	36.2
Scb	5.20	36.66
1+50		
Scb	5.35	36.51
gut	6.0	35.9
1/4	4.9	37.0
+	4.7	37.2
1/4	4.8	37.1
gut	4.9	37.0
Ncb	4.38	37.48

41.86 66

2+00

Ncb	4.49	37.37
gut	5.3	36.6
1/4	5.0	36.9
+	5.0	36.9
+8	5.0	36.9
1/4	5.3	36.6
gut	6.1	35.8
Scb	5.55	36.31
2+50		
Scb	5.69	36.17
gut	6.2	35.7
1/4	5.3	36.6
+5	5.2	36.7
+	5.2	36.7
1/4	5.4	36.5
gut	5.3	36.6
Ncb	4.65	37.21
3+00		
Ncb	4.85	37.01
gut	5.6	36.3
1/4	5.5	36.4
+	5.4	36.5
+9	5.4	36.5
1/4	5.6	36.3
gut	6.5	35.7
Scb	5.86	36.00

41.86

3+50

Seb	6.07	35.79
gut	6.6	35.3
1/4	5.7	36.2
+4	5.4	36.5
+	5.4	36.5
1/4	5.6	36.3
gut	5.7	36.2
Neb	5.05	36.81

4+00

Neb	5.18	36.68
gut	5.8	36.1
1/4	5.9	36.0
+	5.6	36.3
+6	5.5	36.4
1/4	5.9	36.0
gut	6.9	35.0
Seb	6.23	35.63

4+50

Seb	6.45	35.41
gut	7.0	34.9
1/4	6.0	35.9
+5	5.7	36.2
+	5.8	36.1
1/4	5.9	36.0
gut	5.7	36.0
Neb	5.45	36.41

41.86

5+00

Neb	5.58	36.28
gut	6.1	35.8
1/4	6.1	35.8
+	6.0	35.8
+9	6.1	35.8
1/4	6.4	35.5
gut	7.3	34.6
Seb	6.60	35.26

5+50

Seb	6.70	35.16
gut	7.5	34.4
1/4	6.4	35.5
+9	6.1	35.8
+	6.1	35.8
1/4	6.1	35.8
gut	6.4	35.5
Neb	5.77	36.09

6+00² = W.L. Sicard.

Neb	5.87	35.99
gut	6.2	35.7
1/4	6.4	35.5
+	6.6	35.2
1/4	6.8	35.1
gut	7.5	34.4
Seb	6.79	35.07

su. Newton. 41.85
 B.M. Sicard. 40.25 6.77 35.09
 5.16

Web Sicard

S.L. top cb 40.2 5.27 34.98
 S.L. gut 6.0 34.2
 cb cb 5.8 34.4
 1/4 5.5 34.7
 ♀ 5.4 34.8
 1/4 5.1 35.1
 cb 4.7 35.5
 N.L. gut 4.4 35.8
 N.L. top cb 4.25 36.00

W 1/4 Sicard

N.L. 3.9 36.3
 cb 4.2 36.0
 1/4 4.6 35.6
 ♀ 5.0 35.2
 1/4 5.1 35.1
 cb 5.4 34.8
 S.L. 5.7 34.5

♀ Sicard

S.L. 5.3 34.9
 cb 5.1 35.1
 1/4 4.9 35.3
 ♀ 4.8 35.4
 1/4 4.5 35.7
 cb 4.3 35.9

40.25

68

♀ Sicard

N.L. 4.0 36.2
 ♀ Sicard +25
 N.L. top rail 4.09 36.16
 ♀ +7.4
 N.L. top rail 4.16 36.09
 E 1/4 Sicard
 N.L. 4.2 36.0
 cb 4.4 35.8
 1/4 4.6 35.6
 +5 top rail 4.70 35.55
 ♀ 4.8 35.4
 +8 top rail 4.84 35.41
 1/4 4.8 35.4
 cb 5.0 35.2
 S.L. 5.4 34.8
 E cb Sicard
 S.L. top cb 5.34 34.91
 S.L. gut 5.5 34.7
 +12⁶ top rail 5.09 35.16
 cb 5.1 35.1
 +8 top rail 5.10 35.15
 1/4 5.0 35.2
 ♀ 5.0 35.2
 1/4 4.9 35.3
 cb 4.8 35.4

40.25

Eeb Sicard

N.L. put	4.7	35.5
N.L. top ch	4.24	36.01
EL Sicard = 0+00		
Neb	4.27	35.98
put	4.9	35.3
'A	4.8	35.4
+	4.7	35.5
'A	5.1	35.1
put	5.2	35.0
Seb	5.26	34.99
+6 ^E top rail	5.24	35.01
S.L. top rail	5.21	35.04
0+50		
Seb	5.45	34.80
put	5.8	34.4
'A	5.2	35.0
+	4.8	35.4
'A	4.9	35.3
+8	5.3	34.9
put	5.1	35.1
Neb	4.42	35.83

40.25

69

1+00

Neb	4.50	35.75
put	5.1	35.1
'A	4.8	35.4
+	4.7	35.5
+4	4.7	35.5
'A	5.4	34.8
put	6.1	34.1
Seb	5.55	34.70
1+50		
Seb	5.65	34.60
put	6.1	34.1
+8	6.0	34.2
'A	5.8	34.1
+	5.0	35.2
'A	5.2	35.0
put	5.1	35.1
Neb	4.66	35.59

Corb broken 1+55 to 1+70 on South

40.25

1+73 = End cb & sidewalk on North.

N.L.	4.2	360
Ncb	4.74	35.51
gut	5.2	350
1/4	5.3	349
±	5.2	350
1/4	5.9	343
gut	6.1	341
Seb	5.70	34.55
2+00		
Seb	5.71	34.54
gut	6.1	341
1/4	5.9	343
±	5.4	34.8
+6	5.3	349
1/4	5.4	348
cb	5.4	348
+1	5.4	348
+1	4.2	360
N.L.	4.3	360

40.25

70

2+45 = Begin of curb on North (No walk)

N.L.	3.9	363
+7	4.8	354
Ncb	4.84	35.41
gut	5.4	348
1/4	5.6	346
±	5.7	34.5
+8	5.8	344
1/4	6.0	342
gut	6.5	337
Seb	5.89	34.36

3+54⁶ = W.L. 26th on North

Seb	6.15	34.10
gut	6.7	335
1/4	6.3	339
±	5.9	343
1/4	5.7	345
gut	5.8	344
Ncb	5.18	35.07

End Sec on incl. 26th = 4+16⁶ on South

cb-2 nd Ncb on rat	5.20	35.05
gut Pav	5.91	34.34
cb Inc Pav	5.88	34.37
1/4 ✓	5.88	34.37
± ✓	6.00	34.25
1/4 ✓	6.28	33.97

40.25

End Sec.

gut.	Pav	6.80	33.45
Seb		6.26	33.99

X sec. 16th st. from S.L.
National to Newton.
csc = walks in 10' Rdway.

Jan 11-27
London

71

B.M.	4.23	8.03	3.80
------	------	------	------

B.P.N.W. 16th
Nat'l. 16th

0+00 = 54 Nat'l.

web		4.75	3.28
-----	--	------	------

gut	Pav	5.25	2.78
-----	-----	------	------

1/4	✓	4.78	3.25
-----	---	------	------

1/4	✓	4.44	3.59
-----	---	------	------

1/4	✓	4.46	3.57
-----	---	------	------

gut	✓	5.01	3.02
-----	---	------	------

Ecb		4.17	3.86
-----	--	------	------

0+50

Ecb		4.48	3.55
-----	--	------	------

gut	20	5.2	2.8
-----	----	-----	-----

1/4		4.9	3.1
-----	--	-----	-----

1/4		4.8	3.2
-----	--	-----	-----

1/4		5.1	2.9
-----	--	-----	-----

gut		5.6	2.4
-----	--	-----	-----

web		5.02	3.01
-----	--	------	------

1+00

web		5.27	2.76
-----	--	------	------

gut		5.8	2.2
-----	--	-----	-----

1/4		5.3	2.7
-----	--	-----	-----

1/4		5.0	3.0
-----	--	-----	-----

1/4		5.1	2.9
-----	--	-----	-----

gut		5.3	2.7
-----	--	-----	-----

Ecb		4.78	3.25
-----	--	------	------

Plotted Jan 19-29 CBH

1+40 = N.L. Alley on East.
803

E.L. top Alleyeb	4.83	3.20
Ecb Alley ret	5.04	2.99
gut	5.1	2.9
+3	5.5	2.5
1/4	5.2	2.8
+	5.0	3.0
1/4	5.4	2.6
gut	5.9	2.1
web	5.43	2.60

1+60 = S.L. Alley on East

web	5.51	2.52
gut	6.0	2.0
1/4	5.6	2.4
+	5.1	2.9
1/4	5.3	2.7
+6	5.7	2.3
gut	5.2	2.8
Ecb Alley ret	5.13	2.90
E.L. top Alleyeb	4.87	3.16

2+00 8.03

Ecb	5.57	2.46
gut	5.2	2.8
+4	5.7	2.3
1/4	5.4	2.6
+	5.4	2.6
1/4	5.6	2.4
gut	6.3	1.7
web	5.72	2.31

2+50

web	5.99	2.04
gut	6.6	1.4
1/4	5.7	2.3
+	5.3	2.7
1/4	5.5	2.5
+6	5.8	2.2
+7	5.3	2.7
gut	5.4	2.6
Ecb	5.92	2.11

3+00 = N.L. Newton.

Ecb	6.19	1.83
gut	5.9	2.1
1/4	5.7	2.3
+	5.3	2.7
1/4	6.0	2.0
gut	6.5	1.5
web	6.22	1.81

X sec Commercial from EL 13th
to W.L. Nat'l. 80' st. 10' chs 52' Rdway.

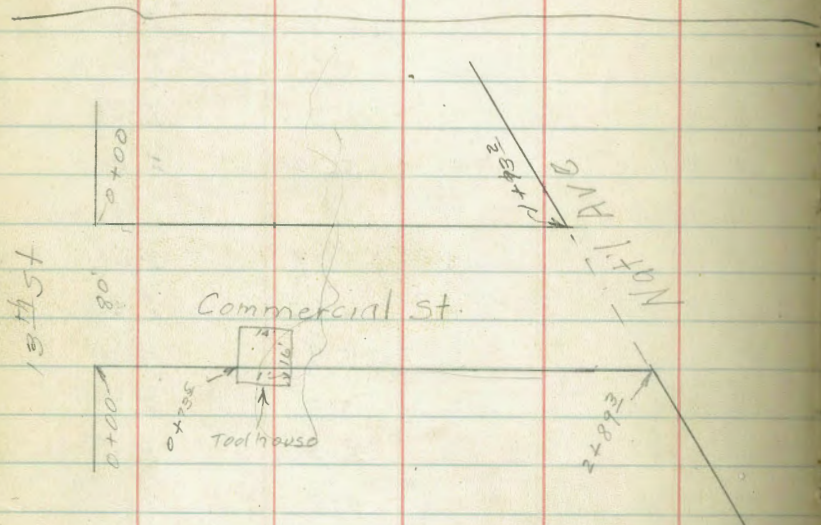
73
Tob F. H.
N.E. Commercial

BM	4.87	8.67	3.80	N.W. Nat'l. 216 th
T.P.	3.51	7.87	4.31	4.36
BP N.E. 14 th Imperial				
S.M.		1.03	6.8A	(6.93 Pa)
B.M. 430 F.H. N.E. Commercial 213 th		1.89	5.98	

BM	3.92	9.90	5.98
0+00 = EL	13 th		
N.L.	6.5	3.4	
+3 ² top rail	6.48	3.42	✓
+8 ¹ rail	6.62	3.28	
cb	6.7	3.2	
1/4	6.6	3.3	
+4 ² rail	6.31	3.59	
+7 ³ rail	6.29	3.61	
±	6.7	3.2	
+5 rail	6.68	3.22	
+9 ² rail	6.70	3.20	
1/4	6.8	3.1	
cb	7.0	2.9	
S.L.	7.0	2.9	
0+37			
S.L.	7.6	2.3	
cb	7.2	2.7	
1/4	6.9	3.0	
+2 rail	6.66	3.24	✓
+6 ³ rail	6.63	3.27	
±	6.8	3.1	✓
+5 ⁶ rail	6.30	3.60	
+10 ⁵ rail	6.38	3.52	
1/4	6.7	3.2	
cb	6.7	3.2	

Plotted Jan 18-22-CBH

Note: Do not use rail elevs in ground sections.



9.90

9.90

74

0+37

cb+2 ³ rail	6.56	3.34
+7 ² rail	6.41	3.49 ✓
+10	6.7	3.2
N.L.	6.7	3.0

0+50

N.L.	5.7	4.2
+4	6.8	3.1
+8 ⁶ rail	6.37	3.53 ✓
+13 ⁵ rail	6.54	3.36
cb	6.8	3.1
1/4	6.6	3.3
+2 ⁵ rail	6.36	3.54
+7 ⁴ rail	6.34	3.56
±	6.8	3.1 ✓
+5 ³ rail	6.63	3.27
+10 rail	6.66	3.24 ✓
1/4	6.9	3.0
+8	7.3	2.6
cb	7.2	2.7
S.L.	7.5	2.4

1+00

S.L.	7.1	2.8
+1	6.8	3.1
cb	6.7	3.2
1/4	6.7	3.2
+3 rail	6.66	3.24 ✓
+7 ⁸ rail	6.55	3.35
±	6.8	3.1 ✓
+5 ² rail	6.50	3.40
+10 ³ rail	6.52	3.38
1/4	6.9	3.0
+5 rail	6.61	3.29
+10 rail	6.45	3.45 ✓
cb	6.9	3.0
+4	7.0	2.9
+6	5.9	4.0
N.L.	5.7	4.2

1+50

N.L.	5.9	4.0
+4	5.6	4.3
+12	5.3	4.6
cb	5.8	4.1
+4	7.2	2.7
+11 ² rail	6.66	3.24 ✓
1/4	7.1	2.8
+3 rail	6.65	3.25
+3 ⁶ rail	6.65	3.25

990

1+50		
cb+8 ³ rail	6.73	3.17
±	7.1	2.8 ✓
+5 ² rail	6.64	3.26
+10 ⁵ rail	6.71	3.18 ✓
1/4	7.1	2.8
+7	7.1	2.8
cb	7.3	2.6
S.L.	7.4	2.5
1+93 ³ = wL Nat'l on North.		
S.L.	7.1	2.8
+3	7.4	2.5
cb	7.4	2.5
1/4	7.2	2.7
+2 ⁵ rail	6.90	3.00 ✓
+7 ³ rail	6.81	3.09
±	7.1	2.8 ✓
+4 ¹ rail	6.86	3.04
+5 rail	6.81	3.09
+9 ¹ rail	6.79	3.11
+9 ² rail	6.78	3.12 ✓
1/4	7.0	2.9
+8	7.2	2.7
+11	5.4	4.5
cb	5.5	4.7
N.L.	5.8	4.1

9.90

75

2+30		
N4+5 int Pav	6.89	3.01
+9 ¹ rail	6.97	2.93
±	7.1	2.8 ✓
+5 ⁸ rail	6.99	2.91
+10 ⁶ rail	6.96	2.94
1/4	6.9	3.0
cb	6.8	3.1
+7	6.7	3.2
S.L.	5.8	4.1
Ebd Sec 2+89 ³ on South = 1+93 ² on North.		
S.L.	6.6	3.3
+16 enddiag.	6.6	3
cb tabch	6.98	2.92 ✓
gvt Pav	7.79	2.11 ✓
1/4 ✓	7.13	2.77
+3 ⁸ enddiag rail	6.94	2.96
+11 ⁴ ✓ rail	6.97	2.93
± Pav	6.95	2.95 ✓
+5 ⁸ enddiag rail	6.97	2.93
+13 ² ✓ rail	6.95	2.95
1/4 Pav	7.07	2.83
cb+1 ² gvt enddiag.	7.58	2.32
cb+1 ² top cb enddiag.	7.09	2.81
N.L.	5.8	4.1

X Sec. Alleg BIK. C. Middle town
Columbia to State.
North of Bdw.

4-23-29
Miller.

27.16

76

B.M.	5.41	27.16	21.75	Use this B.M. SW State a Bdw.	T.P.	2.54	23.78	5.92	21.24	
		oo = W. line state					200 W = E. line Columbia.			
S		4.27	22.89	dirt + Pavmt.	S		4.17	19.61	dirt + pavmt.	
C		4.35	22.81	dirt + pavmt.	C		4.20	19.58	pavmt.	
N		4.06	23.10	dirt + Pavmt.	N		3.87	19.91	dirt + pavmt	
		67' W. = E. End Garage door on S			OK OR B.M.		3.63	20.15 = 20.10	N.G. N.W. E + Columbia	
N		5.3	21.86	dirt	T.P.	7.87	24.56	7.09	16.69	
C		5.5	21.66	dirt.	check original B.M.		2.81	21.75 = 21.75	Use this B.M.	
S		5.19	21.97	garage floor						
		86' W. = E. garage door on N								
S		5.18	21.28	garage floor						
C		5.2	21.96	dirt						
N		4.97	22.19	garage floor						
		97.5' W. = W. End garage door on S.								
N		5.3	21.86	dirt						
C		5.4	21.76	dirt						
S		5.88	21.28	garage floor						
S		6.0	21.16	dirt						
		102' W. = Approx E. End Pavmt. Not much good.								
S		5.74	21.42	pavmt.						
C		5.86	21.30	"						
N		5.77	21.69	"						
		149' W. = E. garage door on N								
N		6.26	20.90	garage floor						
C		6.75	20.41	pavmt.						
S		6.29	20.87	"						

Plotted
4.24.29
T.G.H.

Newton Ave

335.90

+ 6.78

342.68

- 13.26

329.42

+ 0.68

330.10

- 11.89

318.21

- 11.89

306.32

- 0.87

305.45

+ 14.13

319.58

+ 11.13

330.71

Evans SW 37.904

Crabby SW 28.874

Sambson 31.974

Seward 31.952

Sigsbee 14.912

N.W. 1.818

Natl Ave

Seward SW 48996

Beardsley SW 35914

16th NW 3.797

26th St

Natl NE 49.957

14th

N.W. NE 6.932

30 24 3 27 8.1

39

35.1
16.9
52.0
11.9
68.9
16.9
85.8

468
17

ENGINEERING DEPARTMENT
CITY OF SAN DIEGO
CALIFORNIA

299.84 ✓

+ 7.20

307.04 ✓

- 11.11

295.93 ✓

+ 4.74

300.67 ✓

- 11.11

289.56 ✓

+ 3.36

292.92 ✓

- 86.91

206.01 ✓

+ 8.15

214.16 ✓

+ 1.70

215.86 ✓

- 6.80

209.06 ✓

- 0.43

208.63 ✓

+ 9.12

217.75 ✓

- 4.94

212.81 ✓

300.55

353.94 ✓

+ 1.39

355.33 ✓

- 12.11

343.22 ✓

+ 1.02

344.24 ✓

- 8.29

335.95 ✓

+ 394.19

730.14 ✓

- 9.94

720.20 ✓

+ 343.45

1063.65 ✓

- 12.34

1051.31 ✓

+ 355.59

1406.90 ✓

- 0.96

1405.94 ✓

+ 354.63

1760.57 ✓

+ 12.96

1773.53 ✓

- 367.59

1405.94 ✓

- 1.04

1404.90 ✓

+ 366.55

1771.45 ✓

+ 8.43

1779.88 ✓

- 12.70

1767.18 ✓

+ 374.98

2142.16 ✓

+ 0.11

2142.27 ✓

- 344.71

1797.56 ✓

- 11.96

1785.60 ✓

+ 381.30

2166.90 ✓

- 7.14

2159.76 ✓

+ 374.16

2533.92 ✓

+ 5.56

2539.48 ✓

- 379.72

2159.76 ✓

+ 6.97

2166.73 ✓

+ 372.75

2539.48 ✓

+ 7.55

2547.03 ✓

- 380.30

2166.73 ✓

- 2.47

2164.26 ✓

+ 377.83

2542.09 ✓

+ 5.40

2547.49 ✓

- 383.23

2164.26 ✓

- 0.81

2163.45 ✓

+ 382.42

2545.87 ✓

+ 12.21

2558.08 ✓

- 394.63

2163.45 ✓

- 3.75

2167.20 ✓

+ 390.88

2558.08 ✓

+ 8.16

2566.24 ✓

- 399.04

2167.20 ✓

+ 374.16

2541.36 ✓

+ 6.00

2547.36 ✓

- 380.16

2167.20 ✓

- 12.15

2155.05 ✓

+ 368.01

2523.06 ✓

+ 1.27

2524.33 ✓

- 369.28

2155.05 ✓

- 12.45

2142.60 ✓

+ 356.83

2500.43 ✓

+ 0.47

2500.90 ✓

- 357.30

2142.60 ✓

- 12.70

2129.90 ✓

+ 344.60

2474.50 ✓

+ 0.11

2474.61 ✓

- 344.71

2129.90 ✓

- 11.96

2117.94 ✓

+ 332.75

2450.69 ✓

+ 1.04

2451.73 ✓

- 374.16

2077.57 ✓

- 12.25

2065.32 ✓

+ 321.54

2386.86 ✓

+ 3.40

2390.26 ✓

- 324.94

2065.32 ✓

- 12.95

2052.37 ✓

+ 311.99

2364.36 ✓

+ 1.05

2365.41 ✓

- 313.04

2052.37 ✓

- 13.20

2039.17 ✓

+ 299.84

2339.01 ✓

- 0.81

2338.20 ✓

+ 382.42

2720.62 ✓