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ENGINEERING DEPARTMENT  
CITY OF SAN DIEGO  
CALIFORNIA

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Balboa Park

N Bliss  
 Overmit  
 Jacobson  
 12/18/20

A Section's Neale Street from  
 the S Line of Pringle to the N Line  
 of Andrews

B.M. N.W. 8P  
 Pringle + Wash  
 Bl 1/4

2.74 267.81 265.07 50' St  
 12.06

T.P. 0.80 255.91 1270 255.11

S Line Pringle = 00

E Top cb 1.87 254.04

G 2.63 253.28

1/4 2.63 253.28

1/2 2.96 252.95

3/4 3.56 252.35

G 4.22 251.69

W Top cb 3.75 252.16

0125

N Top cb 6.03 249.80

G 6.6 249.3

1/4 6.1 249.8

1/2 5.4 250.5

3/4 5.0 250.9

G 5.0 250.9

E Top cb 4.23 251.68

0150

E Top cb in Auto Driveway 7.17 248.74

G 7.3 248.6

1/4 7.6 248.3

1/2 7.8 (148.1) 248.1

3/4 8.7 247.5

G 9.0 246.9

Plotted Jan 10 - 1922 CBH

	+	H.I.	-	Elev
		255.91		
N. Top cb		8.34		247.57
		0.75		
N. Top cb		10.66		245.25
G		11.0		244.9
1/4		10.6		245.3
1/4		10.1		245.8
1/4		9.7		246.2
G		9.6		246.3
E. Top cb		9.04		246.87
		11.00		
E. Top cb		11.90		244.51
G		11.8		244.1
1/4		11.7		244.2
1/4		12.2		243.7
1/4		12.8		243.1
G		13.0		242.9
W. Top cb	1.26	244.31	12.86	243.05
		1120 Brk in Grade on Cps		
W. Top cb		3.12		241.19
G		3.9		240.9
1/4		3.3		241.0
1/4		2.8		241.5
1/4		2.9		241.9
G		2.2		242.1
E. Top cb		1.56		242.75

	+	H.I.	-	Elev
		244.31		
		11.50		
E. Top cb		9.25		235.06
G		10.2		234.1
1/4		9.9		234.4
1/4		10.03		234.28
		Flow Line		
		15.23		229.08
1/4		10.6		233.7
G		10.9		233.4
W. Top cb		10.56		233.75
TP	0.34	232.42	12.23	232.08
		1175		
W. Top cb		5.03		227.39
G		5.4		227.0
1/4		4.9		227.5
1/4		4.7		224.7
1/4		4.2		228.2
G		4.5		227.9
E. Top cb		3.55		228.87
		2100 End of cb on West com 5'		
E		9.71		222.71
G		10.8		221.6
1/4		10.7		221.7
1/4		10.7		221.7
1/4		11.6		220.8
G		11.8		220.6
W. Top cb		11.22		221.20
W		11.0		221.4

HI  
232.92

T.P.	0.78	220.24	12.92	219.46
		2125		
W		6.4		213.8
cb		6.3		213.9
+2		6.9		213.3
1/4		6.5		213.7
ϕ		5.8		214.4
1/4		5.9		214.3
G		5.5		214.7
E Top cb		4.85		215.39
		2150		
E Top cb		12.22		208.02
c		13.1		207.1
1/4		13.0		207.2
ϕ		12.9		207.4
1/4		13.9		206.3
+4		14.6		205.6
cb		14.3		205.9
+2		13.9		206.3
W		14.0		206.2
T.P.	0.65	207.79	13.10	207.14
		2175		
W		9.6		198.2
+11		9.1		198.7
cb		9.8		198.0
+3		9.3		198.5

HI  
207.79

1/4		8.9		198.9
ϕ		8.1		199.7
1/4		7.9		199.9
G		7.9		199.9
E Top cb		7.23		200.56
TP	100	196.38	12.41	195.38
		2193		
E Top cb		1.17		195.21
G		2.0		194.4
1/4		1.6		194.8
ϕ		1.5		194.9
1/4		2.6		193.8
+4		2.8		193.6
cb		3.9		193.0
+1		2.8		193.6
W		2.8		193.6
		3400	N Line Keating	
W		4.5		191.9
cb		4.0		192.4
1/4		3.9		192.5
ϕ		3.9		193.0
1/4		3.1		193.3
G		3.2		193.2
E Top cb		3.20		193.18
		S. Line Keating	= 00	
		4.2		192.2

3

	H.I.	E/ey
	196.38	
cb	3.7	192.7
1/4	3.7	192.7
H	3.9	192.5
t2	5.1	191.3
ϕ	5.5	190.9
1/4	5.8	190.6
+1	5.9	190.5
t2	5.0	191.4
cb	5.4	191.0
+5	6.3	190.1
W	7.7	188.7
	0+0.6	
W-10	13.2	183.2
W	12.0	184.4
+7	10.7	185.7
cb	10.7	185.7
+3	10.0	186.4
1/4	10.0	186.4
ϕ	9.6	186.8
1/4	8.7	187.7
+3	7.9	188.5
+5	6.4	190.0
cb	5.8	190.6
+4	5.7	190.7
E	6.6	189.8
+10	7.7	188.7

	H.I.	E/ey
	196.38	
	0+15	
		4
		12.8
		183.6
		12.5
		183.9
		12.3
		184.1
		11.5
		184.9
		11.1
		185.3
		12.6
		183.8
		13.2
		183.2
	0.61	189.05
		12.94
		183.44
		1.4
		182.6
		1.7
		182.3
		3.8
		180.2
		5.4
		178.6
		0+30
		11.4
		172.6
		9.7
		174.3
		8.4
		175.6
		8.0
		176.0
		7.4
		176.6
		7.0
		177.0
		7.1
		176.9
		6.8
		177.2
		7.6
		176.4
		7.8
		176.2
		0+50
		14.6
		169.4
		14.2
		169.8



HI  
184.05

cb			13.5	170.5
t3			14.2	169.8
1/4			14.7	169.3
2			14.5	169.5
+4			13.2	170.8
T.P.	0.92	171.34	13.13	170.92
1/4			1.4	169.9
cb			1.7	169.6
W			4.1	167.2
+15			7.0	164.3
		0+65		
-15			14.2	157.1
W			9.8	161.5
cb			8.3	163.0
1/4			8.3	163.0
2			8.1	163.2
1/4			8.8	162.5
t3			8.2	163.1
cb			8.9	162.9
E			9.1	162.2
+15			9.8	161.5
T.P.	0.15	158.62	12.87	158.77
		0+80		
-15			5.7	152.9
E			5.0	153.6
cb			4.0	154.6

HI  
158.62

5

1/4				3.6	155.0
t2				9.3	154.3
2				3.9	155.2
1/4				4.8	153.8
cb				4.4	154.2
W				4.6	154.0
+15				7.6	151.0
T.P.	0.29	146.31	12.55	146.07	
		140.0			
-15				3.2	143.1
W				1.7	144.6
cb				0.7	145.6
1/4				1.0	145.3
2				0.4	145.9
1/4				1.8	144.5
cb				2.0	144.3
E				2.4	143.9
+15				3.0	143.3
				1425	
-30				10.8	135.5
-15				11.3	135.0
E				11.4	134.9
cb				11.7	134.6
1/4				11.9	134.4
2				12.0	134.3
1/4				11.8	134.5

H.I.  
146.31

cb			11.5	134.8
N			11.4	134.9
+15			12.2	134.1
+30			13.9	132.4
T.P.	9.34	137.83	12.82	133.49
			+33	
-30			7.4	130.4
-15			6.3	131.5
W			5.7	132.1
cb			5.7	132.1
1/4			5.7	132.1
E			5.8	132.0
1/4			6.5	131.3
cb			6.3	131.5
E			6.7	131.1
+15			5.7	132.1
+30			9.2	133.6
			+37	
-30			5.5	132.3
-15			6.4	131.4
-13			6.4	131.4
-5			9.9	127.9
E			10.5	127.3
cb			10.5	127.3
+2			10.6	127.2
+3			7.0	130.8

H.I.  
137.83

146. Muffole  
Feb 7.73

6

1/4			7.1	130.7
E			7.3	130.5
1/4			7.2	130.6
cb			6.9	130.9
W			7.2	130.6
+15			8.0	129.8
+30			8.7	129.1
			+44	
-30			10.0	
-15			9.1	128.7
W			8.8	129.0
cb			8.9	129.4
1/4			8.3	129.5
E			8.1	129.7
+E			7.9	130.4
1/4			11.2	126.6
cb			10.7	127.1
+2			9.8	128.0
E			8.7	129.1
+1			8.1	129.7
+14			9.9	127.9
+21			9.5	128.3
+25			8.0	129.8
+30			7.2	130.6
			+50	
-30			8.2	129.6

H.I.  
13783

-29	9.2	128.6
-29	9.9	127.9
-20	7.5	130.3
-16	6.9	130.9
E	7.5	130.3
cb	9.2	128.6
+3	9.1	128.7
+4	10.9	126.9
1/4	11.3	126.5
£	11.7	126.1
+1	9.1	128.7
1/4	9.6	128.2
cb	9.8	128.0
+5	9.8	128.0
W	9.7	128.1
+5	12.0	125.8
+10	13.2	124.6
+30	14.5	123.3
	14.58	
-30	10.0	127.8
-15	9.8	128.0
-6	9.6	128.2
-5	13.1	124.7
W	12.7	125.1
cb	12.5	125.3
1/4	12.6	125.2

H.I.  
13783

7

£	11.3	126.5
+5	8.5	129.3
1/4	7.7	130.1
cb	7.5	130.3
E	7.1	130.7
+15	6.3	131.5
+30	6.3	131.5
	14.65	
-30	4.3	133.5
-15	4.0	133.8
E	5.0	132.8
cb	5.6	132.2
1/4	5.9	131.9
£	5.6	132.2
1/4	5.6	132.2
cb	5.6	132.2
W	5.9	132.4
+15	6.3	131.5
+30	7.5	130.3
	14.71	
-30	6.6	131.2
-15	5.6	132.2
W	4.8	133.0
cb	4.7	133.1
1/4	4.1	133.7
£	3.7	134.1

HI.  
13783

1/4	3.3	134.5
cb	2.9	134.9
E	1.5	136.3
+15	1.2	136.6
+30	1.7	136.1
T.P.	10.79	147.99
	0.63	137.20
	1+76	
-30	8.9	139.1
-15	9.5	138.5
E	11.4	136.6
cb	12.6	135.4
1/4	13.1	134.9
ϕ	13.5	134.5
1/4	14.1	133.9
cb	14.5	133.5
+8	14.5	133.5
N	14.1	133.9
+10	14.2	133.8
+30	14.4	133.6
	148~	
-30	13.1	134.9
-15	11.3	136.7
N	11.5	136.5
cb	10.8	137.2
1/4	10.6	137.4
ϕ	10.1	137.9

+

HI.  
147.99

-

Elev

8

1/4	9.4	138.6
cb	10.6	137.4
E	10.3	137.7
+15	9.5	138.5
+30	8.8	139.2
	1190	
+20	9.9	143.1
E	5.6	142.4
cb	6.4	141.6
1/4	6.4	141.6
ϕ	7.1	140.9
1/4	7.6	140.4
cb	8.3	139.7
N	9.1	138.9
+15	8.7	139.3
+30	9.4	138.6
	2+00	
-30	5.5	142.5
-15	6.5	141.5
N	6.3	141.7
cb	4.5	143.5
1/4	3.5	144.5
ϕ	3.2	144.8
1/4	2.2	145.8
cb	1.5	146.5
T.P.	12.13	159.43
	0.69	147.30

+

H.I.  
159.43

-

E/10

E		11.8	147.6	
+20		10.5	148.9	
	1+15			
-15		3.8	155.6	
E		4.2	155.2	
cb		5.4	154.0	
1/4		6.2	153.2	
ϕ		6.8	152.6	
1/4		7.9	151.5	
cb		9.4	150.0	
+5		10.1	149.3	
W		11.4	148.0	
+15		12.9	146.5	
+30		11.7	147.7	
	1+25			
-30		6.6	152.8	
-15		9.5	149.9	
W		7.2	152.2	
+5		6.1	153.3	
cb		4.2	155.2	
1/4		3.0	156.4	
ϕ		2.9	156.5	
1/4		1.7	157.7	
T.P.	10.59	169.77	0.25	159.18
cb		11.2	158.6	
E		10.2	159.6	

H.I.  
169.77

9

+10		9.8	160.0	
	2+37			
-10		3.8	166.0	
E		3.8	166.0	
cb		4.2	165.6	
1/4		5.2	164.6	
ϕ		6.6	163.2	
1/4		7.6	162.2	
cb		8.7	161.1	
W		12.3	157.5	
+15		14.4	155.4	
+20		13.6	156.2	
	2+50			
-20		7.6	162.2	
-12		8.9	160.9	
W		5.5	164.3	
+5		3.9	165.9	
cb		2.7	167.1	
1/4		1.5	168.3	
ϕ		1.0	168.8	
TP	11.81	181.01	0.57	169.20
1/4		10.7	170.3	
cb		10.0	171.0	
E		9.1	171.9	
+10		8.5	172.5	
	2+62			

	H.I.	-	Elev
	181.01		
	2+62		
-10		3.4	177.6
E		3.4	177.6
cb		4.7	176.3
1/4		5.9	175.1
2		7.6	173.4
1/4		8.4	172.6
cb		9.9	171.1
W		12.8	168.2
+10		15.6	165.4
+20		15.9	165.1
+30		12.3	168.7
	2+75		
-20		10.5	170.5
-10		12.0	169.0
W		9.3	171.7
+5		7.0	174.0
cb		4.5	176.5
1/4		3.4	177.6
2		2.2	178.8
+3		1.0	180.0
1/4		0.3	180.7
T.P.	10.88	191.26	180.38
cb		9.7	181.6
+7		8.7	182.6
E		8.3	183.0
+10		8.0	183.3

	H.I.	-	Elev
	191.26		
	2+88		
-10		2.9	185.4
E		4.1	187.2
cb		6.1	185.2
1/4		7.2	184.1
+2		7.7	183.6
+4		8.7	182.6
2		9.5	181.8
1/4		10.8	180.5
cb		12.2	179.1
W		15.8	175.5
+10		17.0	174.3
+20		13.7	177.6
	3+00		
-20		8.9	182.4
-5		12.7	178.6
W		12.8	178.5
+8		11.8	179.5
1/4		10.8	180.5
1/4		9.2	182.1
2		7.5	183.8
1/4		6.0	185.3
cb		4.7	186.6
E		2.3	189.0
+10		0.2	191.1
	N.CB		
E		0.4	190.9

10

50st  
N Line of Andrew 5'0" cb  
7 1/2

HI  
191.26

cb		26	188.7	W	
1/4		4.0	187.3	+15	
ϕ		5.2	186.1		
1/4		6.7	184.6	-15	
cb		8.3	183.0	W	
W		9.5	181.8	cb	
+6		8.7	182.6	1/4	
+15		6.0	185.3	ϕ	
	N 1/4			+3	
-15		2.9	188.4	4	
-3		7.2	184.1	1/4	
W		7.5	183.8	cb	
cb		5.5	185.8	E	
1/4		3.7	187.6		
ϕ		2.4	188.9	E	
1/4		1.6	189.7	+9	
cb		0.5	190.8	cb	
J.P.	12.15	202.74	0.67	190.59	1/4
E			9.8	192.9	+~
		ϕ			+3
E		7.9	194.8	ϕ	
cb		9.5	193.2	1/4	
1/4		10.7	192.0	cb	
ϕ		11.9	190.8	+6	
1/4		13.3	189.4	W	
cb		14.8	187.9	+10	

HI  
202.79

11

		16.8	185.9
		11.4	191.3
	S 1/4		
		9.1	193.6
		13.8	188.9
		13.2	189.5
		11.4	191.3
		9.1	193.6
		8.3	194.4
		7.1	195.6
		7.0	195.7
		5.9	196.8
		5.3	197.4
	S cb		
		1.8	200.9
		1.7	201.0
		2.9	200.3
		4.1	198.6
		4.7	198.0
		6.0	196.7
		7.0	195.7
		8.0	194.7
		10.3	192.4
		11.0	191.7
		10.9	192.3
		7.1	195.6

H.I.  
202.74

S. Line of Andrews

12

-10		3.5	199.2	
W		6.9	195.8	
+8		7.5	195.2	
cb		6.4	196.3	
1/4		5.2	197.5	
¢		3.7	199.0	
T.P.	10.32	207.09	6.02	196.72
+9		6.4	200.6	
+5		5.3	201.7	
1/4		9.6	202.4	
cb		3.1	203.9	
E		1.1	205.9	
check out on BM. set on X Section of Torrance	10.32		196.72	
			196.61	
			0.11	



X Sections Columbia Street from  
the South Line of Pringle to the N Line  
of Andrews

N Bliss  
Dvermit  
Jacobson  
12/28/18  
13M SE 8P Top  
Pringle & Keitner

	10.03	109.25		99.22
T.P.	12.73	121.70	0.28	108.97
T.P.	13.17	134.13	0.74	120.96
T.P.	9.78	138.42	0.49	133.64
Set 0M SE Top Hy Columbia Pringle			0.73	137.69

0400 S Line Pringle 33 rd do  
on paving

E Topcb		4.83		133.59
G		5.53		132.89
1/4		5.83		132.59
1/4		6.19		132.23
1/4		6.89		131.53
G		8.00		130.42

W Topcb 7.50 130.92

0410 P.C. Return 50 57  
100 65  
75 74 1/2

W Topcb		7.30		131.12
G		7.7		130.7
1/4		7.2		131.2
1/4		6.3		132.1
1/4		5.9		132.5
G		5.8		132.6

E Topcb 5.33 133.09

0450

Auto  
E Topcb driveway 4.98 133.44 ✓

G		5.1		133.3
1/4		5.3		133.1
1/4		5.6		132.8

Plotted Jan 11-29 CBH

HI  
138.92

1/4	6.4	132.0
G	7.0	131.4
N Topcb	7.09	131.38
	1400	BK in CB Grade
N Topcb	5.49	132.93
G	6.1	132.3
1/4	5.5	132.9
⊘	4.7	133.7
1/4	4.4	134.0
G	4.2	134.2
E Topcb	3.95	134.97
	1450	
E Topcb	3.68	134.74
G	4.3	134.1
1/4	4.4	134.0
⊘	4.7	133.7
1/4	5.6	132.8
G	6.0	132.4
N Topcb	5.62	132.80
	2400	
N Topcb	5.11	137.62
G	5.5	132.1
1/4	5.2	132.4
⊘	4.3	134.1
1/4	4.0	133.6
G	3.9	133.7

HI  
137.62

14

E Topcb	3.09	134.53
	2450	
E Topcb	3.83	133.79
G	4.6	133.0
1/4	4.6	133.0
⊘	4.9	132.7
1/4	5.8	131.8
G	6.3	131.3
N Topcb	5.80	131.82
	3400	N Line Keating
N	6.4	131.2
Topcb	6.63	130.99
G	7.0	130.6
1/4	6.3	131.3
⊘	5.7	131.9
1/4	5.2	132.4
G	5.1	132.5
E Topcb	4.59	133.03
E	4.1	132.5
T.P.	5.52	139.16
	3.98	133.69
		N Line + 7
E	2.1	137.1
cb	3.8	135.4
TS	4.4	134.8
1/4	5.5	133.7
⊘	6.2	133.0

H.F  
13916

1/4	7.0	132.2
cb	8.1	131.1
W	8.8	130.4
	N cb	
W	8.9	130.3
cb	8.0	131.2
1/4	6.6	132.6
⊕	5.9	133.3
+5	5.4	133.8
1/4	4.9	134.3
cb	3.6	135.6
E	2.9	136.8
	N 1/4	
E	3.1	136.1
cb	4.5	134.7
1/4	5.5	133.7
⊕	6.2	133.0
1/4	7.0	132.2
cb	7.9	131.3
W	9.0	130.2
	⊕	
W	10.0	129.2
cb	8.6	130.6
1/4	7.7	131.5
⊕	6.7	132.5
+5	5.8	133.4

H.I  
13916

1/4	6.0	133.2
cb	5.5	133.7
E	3.9	135.3
	S 1/4	
E	4.2	135.0
cb	4.8	134.4
1/4	5.7	133.5
⊕	6.6	132.6
1/4	7.7	131.5
cb	8.9	130.3
W	10.2	129.0
	S 1/4 + 5.50	
W	10.1	129.1
cb	8.8	130.4
1/4	8.0	131.2
+3	7.7	131.5
+4	6.8	132.4
⊕	6.3	132.9
1/4	5.6	133.6
cb	4.9	134.3
E	4.0	135.2
	S cb	
E	5.9	133.8
cb	5.8	133.4
1/4	6.3	132.9
⊕	6.8	132.4

15

HZ  
13916

+1	8.2	131.0
1/4	8.6	130.6
cb	8.9	130.3
W	10.2	129.0
	S.Cb. +6	
W	10.6	128.6
cb	9.3	129.9
1/4	9.0	130.2
£	9.3	129.9
1/4	9.2	130.0
+4	8.9	130.3
cb	7.1	132.1
E	6.5	132.7
	S.Cb +8	
E	7.0	132.2
+3	7.2	132.0
+5	8.9	130.3
cb	9.2	130.0
1/4	9.4	129.8
£	9.3	129.9
1/4	9.1	130.1
+6	9.2	130.0
cb	9.7	129.5
W	10.7	128.5
	Slime of Keating	
W	10.8	128.4

HZ  
13916

16

cb		10.0	129.2	
1/4		8.8	130.4	
£		9.4	129.8	
1/4		9.4	129.8	
cb		9.4	129.8	
E		9.6	129.6	
T.P.	0.78	132.63	7.31	131.85
		0+01		
-01 House		0+08	3.9	128.7 ✓
W.			5.1	127.5
+04			5.1	127.5
cb			5.5	127.1
1/4			5.1	127.5
£			4.4	127.2 / 128.2
1/4			3.4	129.2
+05			2.7	129.9
cb			2.7	129.9
E. sidewalk			3.10	129.53
		0+11		
-9.5 House			2.9	129.7
-04			5.0	127.6
E. Topkall			4.8	127.8
cb			4.6	128.0
1/4			4.9	127.7
£			5.6	127.0
1/4			5.9	126.7

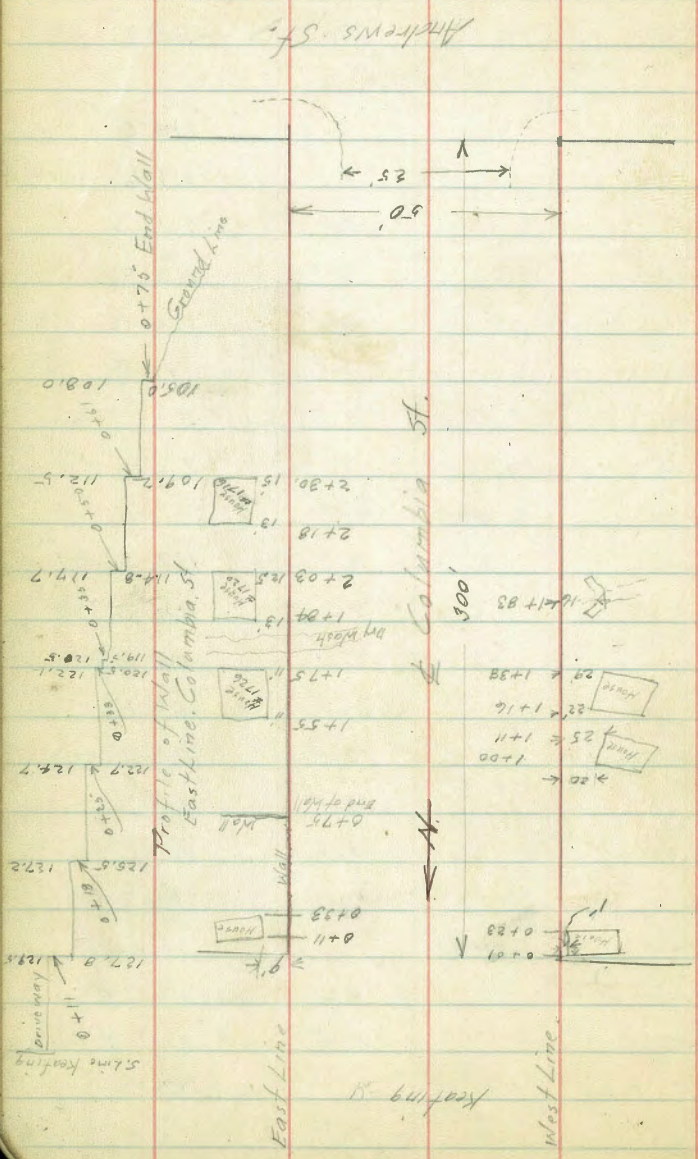
132.63

cb		6.6	126.0	
W.		6.7	125.9	
+01 House		6.7	125.9 ✓	
	0+18			
E. Line TopWall		5.9	127.2 ✓	
E. " "		7.1	125.5	
	0+23			
-01 S. End House		12.0	120.6 ✓	
	0+25			
W.		12.0	120.6	
cb		11.3	121.3	
1/4		11.0	121.6	
£		10.6	122.0	
1/4		10.1	122.5	
cb		9.8	122.8	
		7.9	124.7	
E. Line TopWall		9.9	122.7 ✓	
	0+33			
		10.5	122.1	
E. Line TopWall		12.1	120.5 ✓	
	0+35			
		12.1	120.5	
E. Line TopWall		13.1	119.5 ✓	
T.P.	0.53	120.67	120.14	
E. TopWall		1.2	119.6 ✓	
+02		1.9	118.8	
cb		2.9	117.8	
1/4		3.6	117.1	
£		4.5	116.3	

H.I.  
120.67

17

1/4		4.6	116.1	
cb		5.2	115.5	
W.		5.5	115.3	
	0+50			
W.		10.2	110.6	
cb		9.1	111.6	
1/4		8.4	112.3	
£		7.8	112.9	
1/4		6.7	114.0	
cb		5.9	114.8	
E. Top Wall		5.9	114.3	
E. Top Wall		3.00	117.7 ✓	
	0+60			
E.		8.2	112.5	8.2 17.0
cb		9.5	111.2	
1/4		10.4	110.3	
£		11.6	109.1	
1/4		12.8	107.9	
cb		13.4	107.3	
W.		15.2	105.6	
+10		15.8	104.9	
	0+61			
E. Line TopWall		8.2	112.5 ✓	
E. Line TopWall		11.5	109.2 ✓	
T.P.	2.60	110.37	12.90	107.77



H.I.  
110.37

18

	0+64	
-10	7.7	102.7
W.	7.9	102.5
cb	7.1	103.3
1/4	4.9	105.5
£	2.5	107.9
1/4	2.0	108.4
cb	1.1	109.3
E.	0.7	109.7
	0+70	
E. Top Wall	2.2	108.2
E. Bottom Wall	3.3	107.1
cb	4.1	106.3
1/4	4.5	105.9
£	5.7	104.7
1/4	7.3	103.1
cb	10.2	100.7
W.	11.1	99.3
+15	10.9	99.5
	0+75	
E. Top Wall	2.4	108.0
E. Bottom Wall	5.4	105.0
	0+80	
-15	16.0	94.4
W.	16.8	93.6
cb	14.6	95.8
1/4	13.3	97.1

110.37

£		11.0	99.7
¼		9.3	100.6
cb		8.4	102.0
E.		7.6	102.8
+10		6.8	103.6
	0+90		
-10		10.7	99.7
E		12.0	98.4
cb		13.4	97.0
T.P.	0.81	98.90	98.09
¼		2.8	96.1
£		4.4	94.5
¼		6.3	92.6
cb		7.9	91.0
W.		9.1	89.8
+20		9.3	89.6
	1+00		
-20	House	13.8	85.1
-15		12.1	86.8
-10		11.3	87.6
W.		10.6	88.3
cb		10.5	88.4
¼		9.4	89.5
£		8.4	90.5
¼		7.2	91.7
cb		6.0	92.9

H.1  
98.90

19

E.		4.0	94.9
+10		2.8	96.1
	1+15		
-10		8.1	90.8
E.		9.3	89.6
cb		11.3	87.6
¼		12.5	86.4
£		13.3	85.6
T.P.	0.82	86.85	12.87
¼		2.0	84.8
cb		3.4	83.4
W.		3.6	83.2
+10		3.7	83.1
+22	Cor. of. House	3.8	83.0
	0+25		
-25	House	5.7	81.1
-10		5.5	81.3
-05		7.4	79.4
W.		7.2	79.6
cb		6.4	80.4
¼		5.4	81.4
£		4.4	82.4
¼		3.3	83.5
cb		2.1	84.7
+07		0.5	86.3
E.		0.4	86.4

H.I.  
86.85

+05		0.0	
	1+35		
-10		2.1	84.7
E		3.4	89.4
cb		4.9	81.9
1/4		6.0	80.8
£		7.1	79.7
1/4		7.8	79.0
cb		8.4	78.4
W.		9.2	77.6
+05		8.8	78.0
+15		5.6	81.2
+20 House		6.4	80.4
+28 Sill of Cellar Door		8.43	78.42
	1+38		
-29 Cor. of House		6.4	80.4
	1+50		
-30		6.0	80.8
-18		6.1	80.7
-10		9.5	77.3
W.		9.3	77.5
cb		9.3	77.5
1/4		9.0	77.8
£		8.9	77.9
1/4		8.6	78.2
cb		7.8	79.0

86.85

20

E.		6.3	80.5
+20		3.7	83.1
	1+55		
-11 Foundation of House		6.00	80.85
	1+70		
-11 Floor of Porch		3.81	83.04
-11 Ground.		7.5	79.3
E.		8.0	78.8
cb.		8.8	78.0
1/4		9.0	77.8
£		9.0	77.8
1/4		9.2	77.6
cb		9.3	77.5
W.		8.8	78.0
+20		9.2	77.6
+25		6.1	80.7
+30		6.1	80.7
	1+75		
-30		5.9	80.9
-25		5.9	80.9
-20		9.2	77.6
W.		9.5	77.3
+05		9.7	77.1
+06		11.3	75.5
cb		11.9	75.4
1/4		10.6	76.2



H.I.  
86.85

£		9.4	77.4
+02		9.2	77.6
¼		10.4	76.4
cb		10.0	76.8
E.		9.7	77.1
+12	Car. House Foundation	7.39	79.46 ✓
+12	Ground	9.4	77.4
	1+80		
-15		8.9	77.9
E.		8.8	78.0
cb		9.0	77.8
¼		9.5	77.3
+01		10.3	76.5
£		10.8	76.0
¼		11.3	75.5
+03		9.8	77.0
cb		10.3	76.5
+05		11.3	75.5
W.		11.7	75.1
+16	Flow Line 20' Concrete Culvert	13.11	73.74
+16	Top Hd. Wall	9.56	77.29
+25		5.7	81.1
+30		5.8	81.0
	2+00		
-30		5.7	81.7
-20		5.1	81.7

H.I.  
86.85

21

-02		6.3	80.5
W.		8.4	78.4
+02		9.6	77.2
cb		9.4	77.4
¼		9.3	77.5
£		9.6	77.2
¼		9.7	77.1
cb		9.3	77.5
E.		9.2	77.6
	1+84		
E.-13	North Cor. Foundation House	8.3	78.5
E.-13	Floor Line House	3.1	83.7
	2+03		
E.-12.5	South Cor. House Floor Line	2.9	84.0
E.-12.5	" Foundation	8.7	78.1
	2+13		
E.-13	North Cor. House Foundation	8.0	78.8
	" Floor Line	3.09	83.81
	2+25		
-09	Steps of House	6.7	80.1
E.		8.0	78.8
cb		8.2	78.6
¼		8.1	78.7
£		8.1	78.7
¼		7.7	79.1
cb		7.4	79.4

H.I.  
86.85

W.	7.4	79.4
+10	6.8	80.0
+16	4.7	82.1
+20	4.4	82.4
2+28		
-20	4.0	82.8
-16	4.5	82.3
-05	6.3	80.5
W.	5.9	80.9
cb	6.2	80.6
1/4	6.1	80.7
1/4	6.1	80.7
1/4	5.7	81.1
cb	6.0	80.8
E.	6.1	80.7
+09	Steps of House.	5.7 81.1
2+30		
-15	Ground Line. South. Cor. House.	2.7 84.1
2+36		
-10	2.7	84.1
E.	2.9	83.9
cb	3.4	83.4
1/4	3.3	83.5
1/4	3.7	83.1
1/4	3.6	83.2
cb	3.8	83.0

H.I.  
86.85

22

W.	3.7	83.1
+20	3.0	83.8
2+41		
-20	2.7	84.1
-10	2.2	84.6
W.	2.7	84.1
cb	2.3	84.5
1/4	1.8	85.0
1/4	1.3	85.5
1/4	0.8	86.0
T.P.	12.40	98.65 0.68 86.17
cb	10.9	87.7
E.	11.7	87.0
+10	13.3	85.3
2+51		
-10	12.0	85.8
E.	11.3	87.3
cb	10.8	87.8
1/4	10.1	88.5
1/4	9.4	89.2
1/4	8.9	89.7
+02	10.6	88.0
cb	10.9	87.7
W.	10.8	87.8
+15	12.4	86.2

H.1  
98.65

2+53

-15	12.8	85.8
W.	10.6	88.0
cb	9.6	89.0
1/4	8.8	89.8
E	9.3	89.3
1/4	9.9	88.7
+06	10.9	88.2
cb	8.3	90.3
E.	7.8	90.8
+10	8.1	90.5

2+60

-10	6.6	92.0
E.	6.4	92.2
cb	7.0	91.6
+05	6.9	91.7
+06	8.2	90.4
1/4	8.3	90.3
E	8.4	90.2
1/4	8.3	90.3
+02	8.3	90.3
cb	9.5	89.1
W.	9.7	89.0
+10	11.0	87.6

2+70

-10	9.7	88.9
W	8.6	90.0

H.1  
98.65

23

cb	8.2	90.4
1/4	7.4	91.2
E	6.9	92.7
1/4	5.8	92.8
cb	5.1	93.5
E	4.2	94.4
+10	3.3	95.3

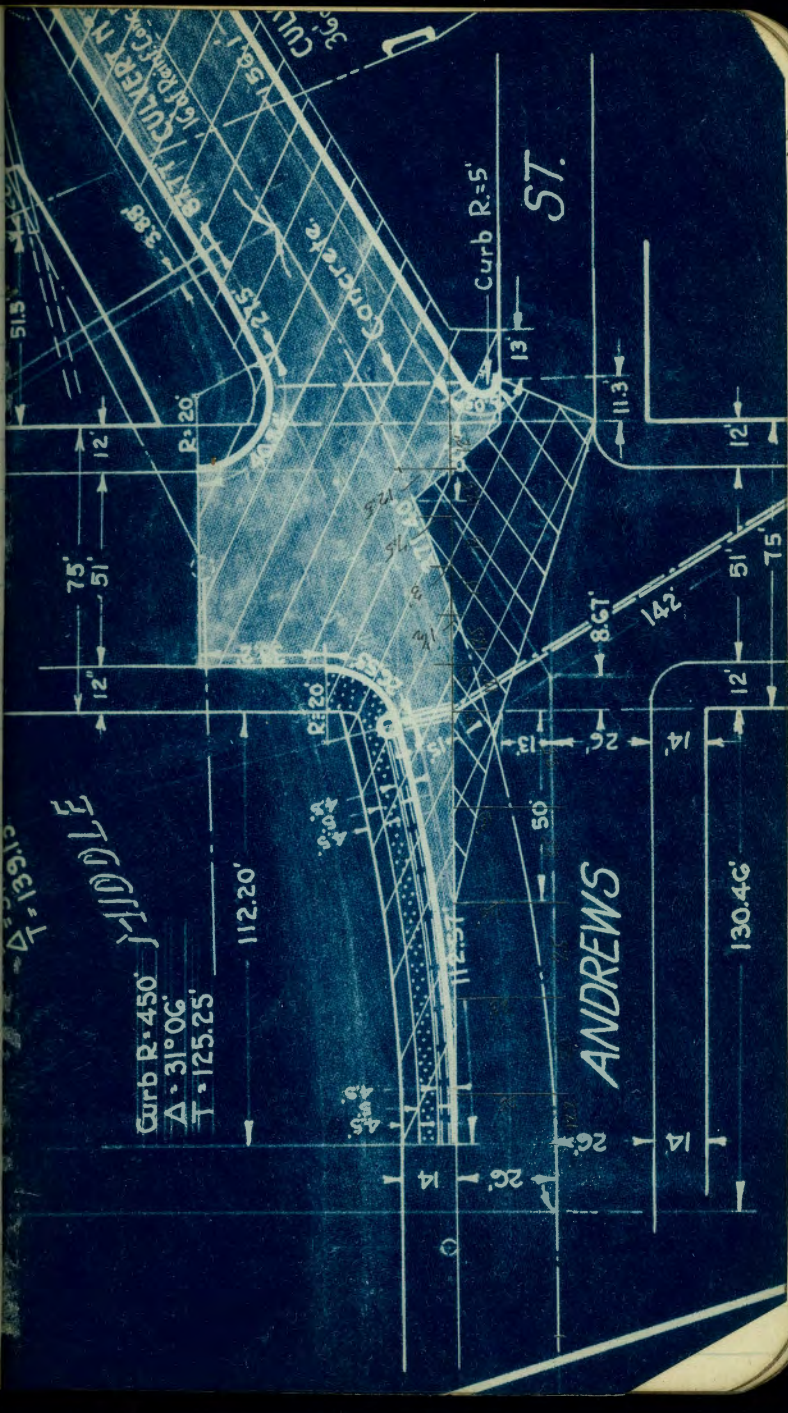
2+80

-10	2.2	96.4
E.	2.8	95.8
cb	3.8	94.8
1/4	4.3	94.3
E	5.0	93.6
+05	4.9	93.7
1/4	4.5	94.1
cb	5.9	92.7
W.	7.5	91.1
+10	8.8	89.8

2+90

-10	7.7	90.9
W.	6.0	92.6
+05	4.8	93.8
cb	3.5	95.1
1/4	4.5	94.1
E	4.3	94.3
1/4	3.3	95.3

-15	cb			2.2	96.4
W.	E.			1.2	97.4
cb	+10			0.4	98.2
$\frac{1}{4}$		3+00	N. Line		Andrews St
$\frac{1}{4}$	E.			0.0	98.6
$\frac{1}{4}$	+06			0.0	98.6
+06	+07			1.6	97.0
cb	cb	Note: Existing		2.00	96.65
E.	+02.5	Curb is		2.11	96.54
+10	G	25 ft. West of Cb. Line			
	$\frac{1}{4}$			2.4	96.2
	$\frac{1}{4}$			2.6	96.0
-10	$\frac{1}{4}$			3.1	95.5
E.	$\frac{1}{4}$			3.4	95.2
cb	G			3.4	95.2
+05	cb	Note: Existing Curb is		3.07	95.68
+06	cb	25 East of Cb Line		3.02	95.63
$\frac{1}{4}$	W.			3.8	94.8
$\frac{1}{4}$	T.P.	1.36	87.33	12.68	85.97
$\frac{1}{4}$	T.P.			9.35	77.98
+02					<u>78.00</u>
cb					
W.					
+10					
-10					
W					



278  
LL

0.11

1.08

5'88

278  
LL

0.11  
5.5  
5.116  
7.8  
1.08  
7.5  
7.76  
6.8  
29.86

Levels Along  $\phi$  of Unix Ave Ext. West.

BM. - NW.B.P. India + Andrews El 77.97

	20'N	$\phi$	20'S	+ HI	- Elev
	78.6	79.02	79.4	8.5083.47	7797
Ecb India	4.9	4.45	4.1		
E 1/4	79.4	79.12	79.42		
	4.1	4.35	4.05		
$\phi$	79.1	78.6	78.9		
	4.4	4.9	4.6		
W 1/4	78.2	78.1	78.8		
	5.3	5.4	4.7		
Wcb	78.2	77.8	78.4		
	5.3 on Wcb	5.2	5.1		
W.L. India	77.3	77.52	77.7		
	6.2	5.95	5.8		
25'W	76.0 Gutter 25.6	76.4 7.1	76.4 7.1		
50'W	74.6 8.9 Gut	75.1 5.0	75.0 5.05	74.6 +5.50	80.07 8.9   74.57
75'W	73.2 6.9 Gut	73.3 6.8	73.5 6.6		
100'W	71.5 8.6 Gut	72.0 5.0	71.7 5.9 Gut	71.6 +5.50	76.97 8.6   71.47
112.2	70.8 6.26	71.2 5.8	70.55 6.45		
137.2	69.1 7.98	69.5 7.5	69.1 7.9		
	N.G. Andrews	$\phi$	SG Andrews	8.20	86.17   7797
EL India St	80.02 6.15 G	80.42 5.75	80.47 6.00		
25'E	83.0 3.20 G	83.22 2.45	83.47 2.70		
12'W EL India		79.9 6.3	79.9 6.30		
25'W		79.32 6.75	79.4 6.80		

Jan. 3, 1929  
 Duermit  
 Jacobzoon  
 Kiernan

X-Sections, India St. from North Line  
 Andrews St. to South Line McKee St.  
 India St. 75' Prop. to Prop. line  
 51' Curb to Curb.  
 H.L.

18  
 5190  
 E  
 1/4

87.35

25

9.35 87.35

78.00 B.M.  
 77.97

N-Line Andrews 0+00

W.	9.1	78.3
cb	9.30	78.05
G	9.61	77.74
1/4	8.82	78.53
E	8.25	79.10
1/4	8.04	79.31
G	8.05	79.30
cb	7.26	80.09
E.	7.0	80.4

cb  
 E.

0+65

E	7.1	80.2
cb	7.2	80.2
1/4	7.6	79.8
E	8.4	79.0
1/4	8.7	78.7
cb	9.1	78.3
W. Store Bldg	8.6	78.8

Plotted Jan. 11-29 C.B.A.

0+99 1/2 End Pav. on India.

0+75

E	6.2	81.1
cb	6.39	81.01
G	7.20	80.15
1/4	7.13	80.22
E	7.28	80.07
1/4	7.95	79.50
G	8.70	78.65
W. Store Bldg	8.17	79.18

W. Store Bldg

W. Store Bldg	8.6	78.8
77	9.0	78.4
79	9.5	77.9
cb	7.6	77.8
1/4	7.3	78.1
E	8.9	78.5
1/4	8.5	78.9
cb	8.1	79.3
E.	7.8	79.6

0+58

0+88

W. Store Bldg	8.5	78.9
cb	8.5	78.9
1/4	7.8	79.5

E	7.9	79.5
cb	8.3	79.1
1/4	8.7	78.7

87.35

£	9.1	78.3
¼	9.4	78.0
cb	9.6	77.8
+03	9.6	77.8
+05	9.1	78.3
W. End Store Bldg	8.8	78.6
-10	0+99 9.9	77.5
W.	9.9	77.5
cb	9.8	77.6
¼	9.4	78.0
£	9.1	78.3
¼	8.6	78.8
cb	8.2	79.2
E.	7.9	79.5
+10	7.7	79.7
-15	1+00 7.4	80.0
E.	7.8	79.6
cb	8.3	79.1
¼	8.6	78.8
£	9.1	78.3
¼	9.4	78.0
cb	9.6	77.8
W.	10.1	77.3
+20	11.1	76.3

H.1  
87.35  
1+15

26

-10	8.0	79.4
W	8.7	78.7
cb	8.9	78.5
¼	9.0	78.4
£	8.9	78.5
¼	8.2	79.2
cb	8.1	79.3
E.	8.0	79.4
+10	7.9	79.5
-10	1+27 8.0	79.4
E.	8.0	79.4
cb	7.8	79.6
¼	7.6	79.8
£	8.2	79.2
+07	8.4	79.0
¼	7.6	79.8
cb	5.9	81.5
+02	5.8	81.6
+03	6.3	81.1
+10	6.3	81.1
+11	5.1	82.3
W.	4.9	82.5
+10	4.0	83.4
-10	1+35 3 1.2	86.2

H. 1.  
87.35

W.	2.3	85.1
+02	2.7	84.7
+03	4.3	83.1
+06	4.4	83.0
+07	3.0	84.4
cb	3.2	84.2
1/4	5.0	82.4
+05	5.8	81.6
£	7.1	80.3
1/4	6.7	80.7
cb	6.7	80.7
E.	7.4	80.0
+04 S.W. Cor. House #3779	7.7	79.7
	1+46	
E. Porch	5.7	81.7
Floor Level of House	3.37	83.98
cb	4.3	83.1
1/4	3.9	82.0
£	2.3	85.1
1/4	1.3	86.1
cb	0.0	87.4
T.P.	12.12	99.88
	0.59	86.76
+06	11.2	87.7
+07	12.3	86.0
+10	12.2	86.7
+11	10.5	88.4

H. 1  
98.88

27

W.	10.1	88.8
+10	70.4	88.5
	1+51	
-10	8.2	90.7
-7	8.8	90.1
W.	9.0	89.9
+07	9.2	89.7
cb	10.1	88.8
1/4	11.1	87.8
£	11.6	87.3
+05	12.4	86.5
+07	13.6	85.3
1/4	15.0	83.9
+03	16.2	82.7
cb	15.5	83.4
+04	15.3	83.6
+05	16.1	82.8
E. Porch	16.5	82.4
	1+60	
-04 N.W. Cor. House #3779	15.1	83.0
E.	15.5	83.4
+03	14.7	84.2
cb	14.9	84.0
+05	14.6	84.3
+07	11.5	87.4
+10	10.9	88.5



H.1  
98.88

1/4	9.8	89.1
+04	8.9	90.0
♀	8.2	90.7
1/4	7.3	91.6
cb	6.0	92.9
+03	5.5	93.4
W.	5.2	93.7
+10	3.2	95.7
1+67		
-10	0.8	98.1
W.	2.1	96.8
cb	3.3	95.6
+03	3.0	95.9
+04	3.5	95.4
1/4	4.3	94.6
♀	5.1	93.8
1/4	6.7	92.2
cb	9.0	89.9
+02	14.1	84.8
E.	14.1	84.8
+02 Garage.	14.1	84.8
1+65		
E.-02 S.W. Cor. Garage.	14.1	84.8
1+75		
-02 N.W. Cor. Garage.	11.4	87.5
-02 Ground Line.	6.8	92.1

H.1  
98.88

28

E.	7.0	91.9
+05	7.1	91.8
cb	5.5	93.4
+07	4.2	94.7
1/4	3.3	95.6
♀	1.8	97.1
1/4	1.4	97.5
+04	0.2	98.7
T.P. 12.14 110.92		
+09	13.1	97.8
cb	11.9	99.0
W.	11.0	99.9
+10	10.5	100.4
1+85		
-10	8.3	102.6
W.	8.2	102.7
cb	8.1	102.8
+07	8.8	102.1
1/4	9.8	101.1
+04	9.3	101.6
♀	10.2	100.7
1/4	11.4	99.5
cb	12.9	98.0
E.	13.4	95.5
+10	16.6	94.3
+25	21.3	89.6

H.1  
110.92  
2+00

-20	12.0	98.9
-15	9.7	101.2
E.	8.2	102.7
cb	7.0	103.9
1/4	5.4	105.5
♀	4.5	106.4
1/4	3.8	107.1
cb	3.5	107.4
W.	4.5	106.4
+10	5.3	105.6

2+15

-10	2.8	108.1
W.	1.6	109.3
cb	0.7	100.7 110.2
T.P.	11.63	122.30
	0.25	110.67

+05	11.7	110.6
+07	11.0	111.3
1/4	10.8	111.5
♀	11.2	111.1
1/4	11.4	110.9
cb	12.5	109.8
E.	13.6	108.7
+15	15.4	106.9
+25	16.7	105.6

2+25

-15	11.1	111.2
-----	------	-------

H.1  
122.30

29

E.	10.0	112.3
cb	8.7	113.6
1/4	8.4	113.9
♀	8.2	114.1
1/4	8.8	113.5
cb	10.0	112.3
W.	11.5	110.8
+10	12.5	109.8

2+31

-10	11.9	110.4
W.	10.4	111.9
cb	9.0	113.3
1/4	8.3	114.0
+05	7.3	115.0
♀	6.8	115.5
1/4	6.4	115.9
cb	6.7	115.6
E.	6.5	115.8
+15	7.6	114.7

2+39<sup>29</sup>

-15	2.8	119.5
E.	2.0	120.3
cb	4.5	117.8
+05	3.7	118.6
1/4	4.0	118.3
♀	4.7	117.6

H.1  
122.30

1/4		6.3	116.0
cb		7.6	114.7
W.		9.2	113.1
+ 15		11.2	111.1
	2+50		
-15		9.8	112.5
W.		7.6	114.7
cb		6.3	116.0
1/4		9.5	117.8
£		3.1	119.2
1/4		1.3	121.0
cb		0.8	121.5
+ 08	E. Line India	1.4	120.9
+ 02	Garage	1.4	120.9
	2+56		
Line - 02	House	1.2	121.1
- 05	E. Line India	1.0	121.3
cb		0.7	121.6
1/4		0.9	121.4
£		2.4	119.9
1/4		3.9	118.4
cb		5.5	116.8
W.		7.3	115.0
+ 15		9.4	112.9
	2+61		
- 15		9.1	113.2
W		6.9	115.4

H.1  
122.30

30

cb		5.3	117.0	
+ 05		4.1	118.2	
1/4		3.3	119.0	
£		1.7	120.6	
1/4		0.3	122.0	
T.P.	5.62	127.77	0.15	122.15
+ 05		5.8	122.0	
+ 06		4.8	123.0	
		3.4	124.4	
1/4 + 11	House. E. Line India	3.7	124.1	
	2+66			
E. Line	N.W. Cor House #3791	3.0	124.8	
	2+72± E. Line to 2+75 W. Line.			
1/4 - 11	E. Line India st.	3.0	124.8	
1/4		3.9	123.9	
£		5.7	122.1	
1/4		7.8	120.0	
cb		9.4	118.4	
W.		11.1	116.7	
+ 15		13.1	114.7	
	3+11± W. Line to 2+71± E. Line.			
W.		8.6	119.2	
cb		7.0	120.8	
1/4		6.0	121.8	
£		4.3	123.5	
1/4		3.4	124.4	

H.I.  
127.77.

E Line India 2.9 124.9

3+11 ± South Line McKee St.

±-08 2.1 125.7

± 2.7 125.1

1/4 5.5 122.3

cb 7.3 120.5

W. -8.4 119.4

TP 9.88 127.65 5.00 122.77  
B.M. ± Hnb. McKee St.  
3+91 ± McKee India

W 5.9 122.4

+7 4.8 122.8

cb 4.1 123.5

1/4 2.3 125.3

+9.56 E Line India 0.8 127.0

N Line McKee  
See 5K24  
Page 31

cb-10 E Line India 0.1 127.7

cb 1.7 125.9

W 2.8 125.0

C-St. Cross Section.  
Cont. From. P-74

18.10

S+100' on Pav.	5.92	12.18
Eh. Kettner +37.5 = S. Kettner.		
S-100' on Pav.	6.66	11.44
-75' " "	6.63	11.47
-50' " "	6.61	11.49
-25' " "	6.58	11.55
S " Pin Survey M.H.	6.51	11.59
cb. " Pav.	6.46	11.64
$\frac{1}{2}$ " "	6.47	11.63
$\frac{1}{2}$ " "	6.46	11.64
$\frac{1}{4}$ " "	6.40	11.70
cb. " "	6.42	11.68
N " "	6.38	11.72
N+25' " "	6.30	11.80
+50' " "	6.24	11.86
+75' " "	6.19	11.90
+100' " "	6.16	11.94
T.P. 6.24 21.43	2.91	15.19
cbk. on B.M. P 76	4.51	16.92

16.90 = B.M.  
0.02 = Error.

32

See 2015

31

12/27/49

W.E. Bliss  
 Duvernit  
 Jacobson  
 Neiman  
 1/4/29  
 B.M. N.E. & P.  
 Andrews California

X Sections McKee St from the E line  
 of California to W line of India

2.59      62.05      52.51      60.31

E. line of California = 00

S Topcb		488	57.17
G	on paving	5.49	56.56
1/4		4.70	57.35
1/2		4.35	57.70
3/4		4.27	57.78
G		4.68	57.37
N Topcb		9.07	57.98
TP	1190	7350 045	61.60
		0225	
N Topcb		12.51	60.99
G		13.3	60.2
+5		13.2	60.3
1/4		13.4	60.1
1/2		13.1	60.4
3/4		13.3	60.2
+8		13.8	59.7
G		13.8	59.7
S Topcb		13.23	60.27
		0750	Break in cb Gads
S Topcb		10.02	63.48
G		10.7	62.8
1/4		10.2	63.3
1/2		9.8	63.7
3/4		10.3	63.2

Plotted Jan-11-1929 CBH

H.I.  
73.50

Elev

G	10.2	63.3
N Topcb	9.98	64.02
	0715	
N Topcb	5.61	67.89
G	6.3	67.2
1/4	6.4	67.1
+5	6.3	67.2
⊕	6.0	67.5
+5	6.1	67.4
1/4	6.4	67.1
G	6.9	66.6
S Topcb	6.25	67.25
	1100	
S Topcb <sup>Auto</sup> Dummy	2.97	70.53
G	3.1	70.4
1/4	2.9	71.1
⊕	2.2	71.3
1/4	2.9	71.1
G	2.5	71.0
N Topcb	1.66	71.84
TP	12.54 8.542 0.62	72.88 ✓
	1125	
N Topcb	9.64	75.78
G	10.3	75.1
1/4	10.5	74.9
⊕	10.3	75.1

H.I.  
85.42

Elev

34

1/4	10.5	74.9
G	11.1	74.3
S Topcb	10.50	74.92
	1150	
S Topcb <sup>Auto</sup> Driveway	7.19	77.23 78.23
G	7.2	78.2
1/4	6.9	78.5
⊕	6.6	78.8
1/4	6.7	78.7
G	6.8	78.6
N Topcb	5.80	79.62
	1175	
N	1.84	83.58
G	2.8	82.6
1/4	2.6	82.8
⊕	2.6	82.8
1/4	2.8	82.6
G	3.2	82.2
S Topcb	2.84	82.58
TP	12.86 97.95 0.33	85.09 ✓
	2100	
S Topcb	11.56	86.39
G	12.0	85.95
+5	11.4	86.5
1/4	11.4	86.5
⊕	11.1	86.8

10.00  
9.90

514  
97.95

1/4	111	86.8
G	110	86.9
N Top cb	10.49	87.46
W line Kettner	2710	
N Top cb	9.04	88.91
G	9.74	88.21
1/4	9.60	88.35
ϕ	9.64	88.31
1/4	9.95	88.00
G	10.99	87.46
S Top cb	10.00	87.95
W line of Kettner	500	Page 33
S	8.9	89.0
S Top cb	8.94	89.01
G	9.52	88.43
1/4	8.1	89.8
ϕ	8.1	89.8
1/4	8.3	89.6
G	8.58	89.37
N Top cb	7.91	90.04
N	7.7	90.2
	0+0.50	
N	3.7	94.2
cb	4.0	93.9
+5	4.9	93.0
+7	6.9	91.0

97.95

35

1/4	80	89.9
ϕ	7.9	90.0
1/4	8.1	89.8
cb	8.1	89.8
+6	6.8	91.1
+7	3.8	94.1
S	3.9	94.0
S Top Wall	5.07	92.88
	0705	
S	4.1	93.8
+5	3.9	94.5
+9	7.1	90.8
cb	7.2	90.7
1/4	7.5	90.4
ϕ	7.2	90.7
1/4	7.2	90.7
+5	6.5	91.4
+8	1.6	96.3
cb	0.8	97.1
N	0.5	97.4
TP	9.50	107.16
	0.29	97.66 ✓
	0725	
N	5.9	101.3
cb	6.8	100.4
+5	11.1	96.1
1/4	12.5	94.7



	+	HZ	-	Elev
			107.16	
+5			13.0	94.2
6			13.5	93.7
+7			13.7	93.5
1/4			13.0	94.2
+7			13.1	94.1
cb			11.3	95.9
+3			10.1	97.1
S			10.9	96.3
		0+55		
S			6.9	100.3
cb			6.9	100.3
1/4			8.4	98.8
6			7.7	99.5
1/4			6.9	100.3
cb			5.8	101.4
+2			5.6	101.6
+6			2.1	105.1
N			1.9	106.3 105.3
		0+60		
N			1.3	105.9
+4			1.6	105.6
+8			4.6	102.6
cb			4.7	102.5
1/4			4.9	102.3
+1			5.1	102.1
+2			6.0	101.2

	+	HZ	-	Elev
			107.16	
				36
				6.8
				7.6
				6.0
				6.3
		0+75		100.9
				102.1
				102.9
				102.4
				102.7
				103.1
				103.7
				104.0
				105.0
				105.6
				106.5
	108.6	117.31	0.71	106.45
				107.1
				107.9
				107.8
				0+83
				Porch of residence on South
				12.5
				104.8
				0+90
				7.7
				109.6
				8.3
				109.0
				9.6
				107.7
				10.3
				107.0

117.31

1/4	10.5	106.8	-10
2	11.5	105.8	S
1/4	12.5	104.8	cb
cb	12.9	104.4	1/4
S	13.4	103.9	2
	14.00		+7
S	12.3	(115.0) 105.0	1/4
+7	11.7	105.6	cb
cb	11.5	105.8	N
1/4	11.1	106.2	T.P.
2	10.1	107.2	
1/4	9.4	107.9	N
+5	8.7	108.6	cb
+7	7.7	109.6	1/4
cb	8.0	109.3	2
N	7.1	110.2	1/4
	14.15		+2
N	9.0	113.3	cb
cb	6.2	111.1	S
1/4	7.3	110.0	+10
2	8.4	108.9	
1/4	8.9	108.4	-10
cb	9.1	108.2	S
S	10.1	107.2	cb
+10	10.8	106.5	1/4

14.25

+

H2

E/10x

117.31

37

	9.6	107.7	
	8.9	108.9	
	7.5	109.8	
	7.1	110.2	
	6.6	110.7	
	5.5	111.8	
	5.2	111.7	
	4.3	113.0	
	2.6	114.7	
11.72	127.65	1.38	115.93 ✓
	14.50		
	10.0	117.6	
	11.1	116.5	
	11.9	115.7	
	12.8	114.8	
	14.1	113.5	
	13.8	113.8	
	14.1	113.5	
	14.5	113.1	
	15.7	111.9	
	14.75		
	12.5	115.1	
	11.8	115.8	
	11.3	116.3	
	10.8	116.8	
	10.3	117.3	

127.65

t6	9.0	118.6
z	8.5	119.1
1/4	8.1	119.5
cb	7.5	120.1
N	6.7	120.9

2100

N	3.8	123.8
cb	4.7	122.9
1/4	5.1	122.5
z	6.1	121.5
1/4	7.4	120.2
cb	8.4	118.7
S	9.2	118.4
+10	10.0	117.6

2109.<sup>20</sup> White India

S	8.5	119.1
cb	8.0	119.6
t5	6.9	120.7
1/4	6.3	121.3
z	5.4	122.2
1/4	4.6	123.0
cb	3.5	124.1
N	2.8	124.8

check 35.00 PM  
5000 sec India

	4.88	122.77
TP	10.74	133.51
	4.88	122.77

E. Line India = 00. See sketch page 38

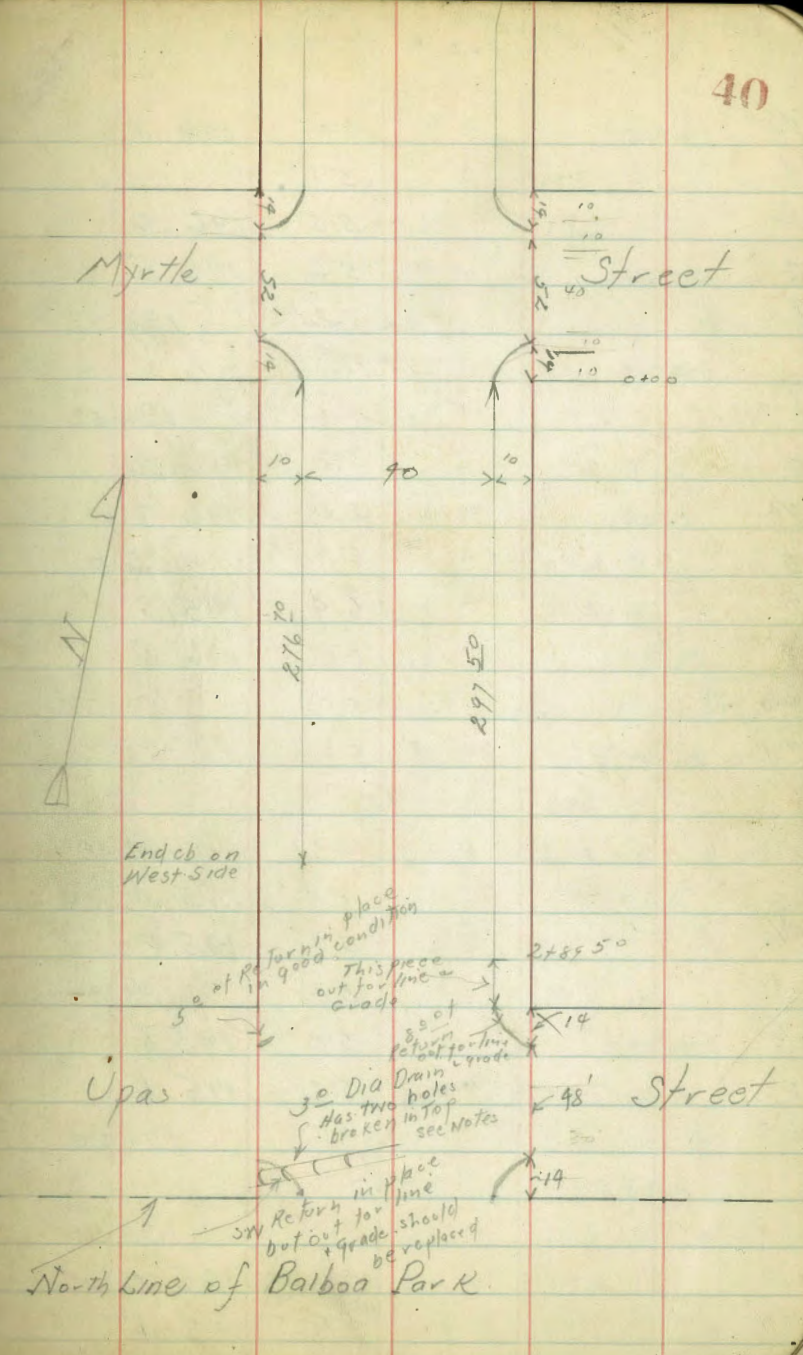
38



X Sections Florida Street from the  
S Line of Myrtle to the North Line of  
Balboa Park.

W Blss Duermit Jacobson Kiernan 1/9/29				
BM NW 87 Myrtle-Albana	4.44	255.94	251.50	
T.P.	0.58	249.00	12.52	243.42
T.P.	0.60	231.65	12.95	231.05
T.P.	0.35	219.08	12.92	218.73
T.P.	0.59	206.64	13.03	206.05
T.P. <sup>BM jet</sup> <sub>SW of</sub>	4.13	203.14	8.63	198.01
See page 24 for the X Section of the entire of Myrtle Florida		S Line of Myrtle = 00		Co St. 10065 10/95
W Top Cb	4.14	198.00		
G	4.6	197.5		
1/4	4.7	197.4		
E	4.5	197.6		
1/4	4.3	197.8		
G	4.3	197.8		
E Top Cb	4.17	197.97		
	0+50			
E Top Cb	4.68	197.48		
G	5.0	197.1		
1/4	4.9	197.2		
1/4	5.2	197.0		
1/4	5.3	196.8		
G	5.0	197.1		
W Top Cb	4.66	197.48		
	1+00			
	519	196.95		
	60	196.1		

Plotted Jan. 8-29-29 - CBH



42.  
20219

1/4		6.0	196.1	
£		5.8	196.4	
1/4		5.5	196.6	
G		5.6	196.5	
E Topcb		5.21	196.93	
	1A42			
E Topcb		5.61	196.53	
G		5.9	196.2	
1/4		5.8	196.3	
£		6.1	196.0	
1/4		6.4	195.7	
G		6.0	196.1	
N Topcb		5.55	196.59	
T.P.	436	200.80	5.70	196.44
		1475		
N Topcb		4.52	196.28	
G		5.4	195.4	
1/4		5.4	195.4	
£		5.0	195.8	
1/4		5.0	195.8	
G		5.2	195.6	
E Topcb		4.60	196.20	
	2400			
E Topcb		4.81	195.99	
G		5.8	195.0	
1/4		5.4	195.4	

42.  
200.80

41

£		5.4	195.4
1/4		5.5	195.3
G		5.7	195.1
N Topcb		4.78	196.02
	2450		
N Topcb		5.34	195.46
G		5.7	195.1
1/4		6.0	194.8
£		6.0	194.8
1/4		6.1	194.7
G		6.3	194.5
E Topcb		5.29	195.51
	2476	20	End 66 on West
E Topcb		5.62	195.18
G		6.8	194.0
1/4		6.6	194.2
£		6.2	194.6
1/4		5.8	195.8
G		6.0	194.8
N Topcb		5.60	195.20
N		5.9	195.4
	2497	50	N line Up 05
N		5.6	195.2
cb		6.2	194.6
1/4		6.2	194.6
£		6.3	194.5

500.5000  
2090.90

14.6.0001  
05. Roadway  
12.1.195  
14.6.0008

H.I.  
200.80

8°  
for Under Grade

5°  
cb on wall

1/4	6.8	194.0
5	7.2	193.6
Top cb	6.2/14°	194.59
N. cb		
Non Top cb	5.71	195.09
Non Ground	6.3	194.5
+5	6.2	194.6
+8	7.1	193.7
cb	7.2	193.6
1/4	6.8	194.0
5	6.4	194.4
1/4	6.4	194.4
cb	6.6	194.2
+5	7.5	193.3
+6	6.7	194.1
Non Ground	6.2	194.6
Non Top cb	5.75 12°	195.05
N 1/4		
W	6.5	194.3
+4	6.8	194.0
+5	8.1	192.7
+7	8.1	192.7
+8	7.2	193.6
cb	7.2	193.6
+2	6.8	194.0
1/4	6.8	194.0

H.I.  
200.80

42

6.6	194.2	
1/4	6.9	193.9
cb	7.0	193.6
+5	7.1	193.7
+7	6.5	194.3
E	6.2	194.6
6		
E	6.4	194.4
+5	7.2	193.6
cb	7.2	193.6
1/4	7.0	193.8
6	6.9	193.9
1/4	6.9	193.9
cb	7.4	193.4
+2	6.7	194.1
+6	8.7	192.1
N	9.2	191.6
+1	6.6	194.2
8 5/8		
Rim	7.03	193.77
Pipe in Bottom Pens of Thr.	12.29	188.51
No open flow line		
5/4		
N-4	6.9	193.9
-3	9.0	191.8
W	9.4	191.4
+8	7.1	193.7
cb	7.0	193.8

HI  
200.80  
12.43  
188.47

365.04 3 3/4  
65.04 5/16

HI  
200.80

1/4	7.1	193.7
2	7.0	193.8
1/4	7.1	193.7
cb	7.3	193.5
E	6.8	194.0
Scb		
+ E on Top cb	6.79	194.01
+ E on Ground	7.0	193.8
+ 5	6.7	194.1
cb	7.5	193.3
1/4	7.3	193.5
2	7.3	193.5
1/4	7.4	193.4
+ 7	7.6	193.2
cb	8.1	192.7
+ 2	9.0	191.8
N	9.7	191.1
+ 5	9.9	190.9
+ 7	8.4	192.4
S. cb + 6		
N-10	11.2	189.6
- 1 Bottom Floor 3" Dia Storm Drain 5.5 x 5.5 x 1	12.93	188.47
- 1 Top Hood Wall	6.80	194.00
N	6.80	193.95
N+1	8.9	191.9
+ 5	9.01	191.79

cb	9.1	191.7
cbt 2 Hope in Pipe	8.9	191.9
+ 4	8.9	191.9
+ 5	8.1	192.7
1/4	7.6	193.2
2	7.3	193.5
1/4	7.6	193.2
G	7.3	193.5
E Top of 2nd Return	6.85	193.95
S Line Up		
E Top cb	6.87	193.93
G	6.9	193.9
+ 5	7.4	193.4
1/4	7.7	193.1
2	7.5	193.3
1/4	7.5	193.3
+ 7	7.5	193.3
cb	7.1	193.7
+ 3	6.8	194.0
N	9.3	191.5
+ 10	10.7	190.1
T.P.	10.28	208.29
T.P.	10.03	217.99
T.P.	11.57	229.19
T.P.	11.50	240.13
TP	11.12	251.09
TP	12.03	262.94
TP	13.03	275.80
TP	4.00	279.56
check out		
6700 NW 1st Robinson		
Florida		
0.21	0.21	239.42
0.10	0.10	250.42
0.20	0.20	262.97
0.24	0.24	275.56
3.52	3.52	276.04



Bliss  
1/4/29

+ HI - E/64

X Section of the Intersection of  
Myrtle & Florida

BM SW 13P Myrtle & Florida	421	202.22	198.01
N. Line of Myrtle			
W Top cb		320	199.02
G		3.7	198.5
1/4		3.5	198.7
1/4		3.3	198.9
1/4		3.0	199.2
G		3.4	198.8
E Top cb		318	199.04
N. cb			
E on Top cb		338	198.84
E on Ground		3.4	198.8
cb		3.3	198.9
1/4		3.2	199.0
1/4		3.4	198.8
1/4		3.6	198.6
cb		3.8	198.4
+5		3.4	198.8
W on Ground		3.3	198.9
W on Top cb		329	198.98
N 1/4			
W		30	199.2
cb		3.9	198.3
1/4		3.9	198.3
1/4		3.7	198.5

H.I.  
202.22

44

1/4	3.5	198.7
cb	3.6	198.6
E	3.7	198.8
E		
E	3.9	198.8
cb	3.5	198.7
1/4	3.8	198.4
1/4	3.78	198.44
Top Ma Hole Rim		
Flow Line 12" Main	6.91	195.31
1/4	4.0	198.2
cb	4.1	198.1
W	3.5	198.7
5 1/4		
W	3.7	198.5
cb	4.3	197.9
1/4	4.3	197.9
1/4	4.2	198.0
1/4	4.0	198.2
cb	3.9	198.3
E	3.3	198.9
S. cb		
E on Top cb	4.25	197.97
on Ground	3.0	199.2
+8	3.3	198.9
cb	4.0	198.2
1/4	4.2	198.0

H.I.  
202.22

45

L	44	197.8
W	45	197.6
CB	45	197.7
W on Ground	41	198.1
W on Topck	4.21	198.01
For South Line of Myrtle See Page 90.		

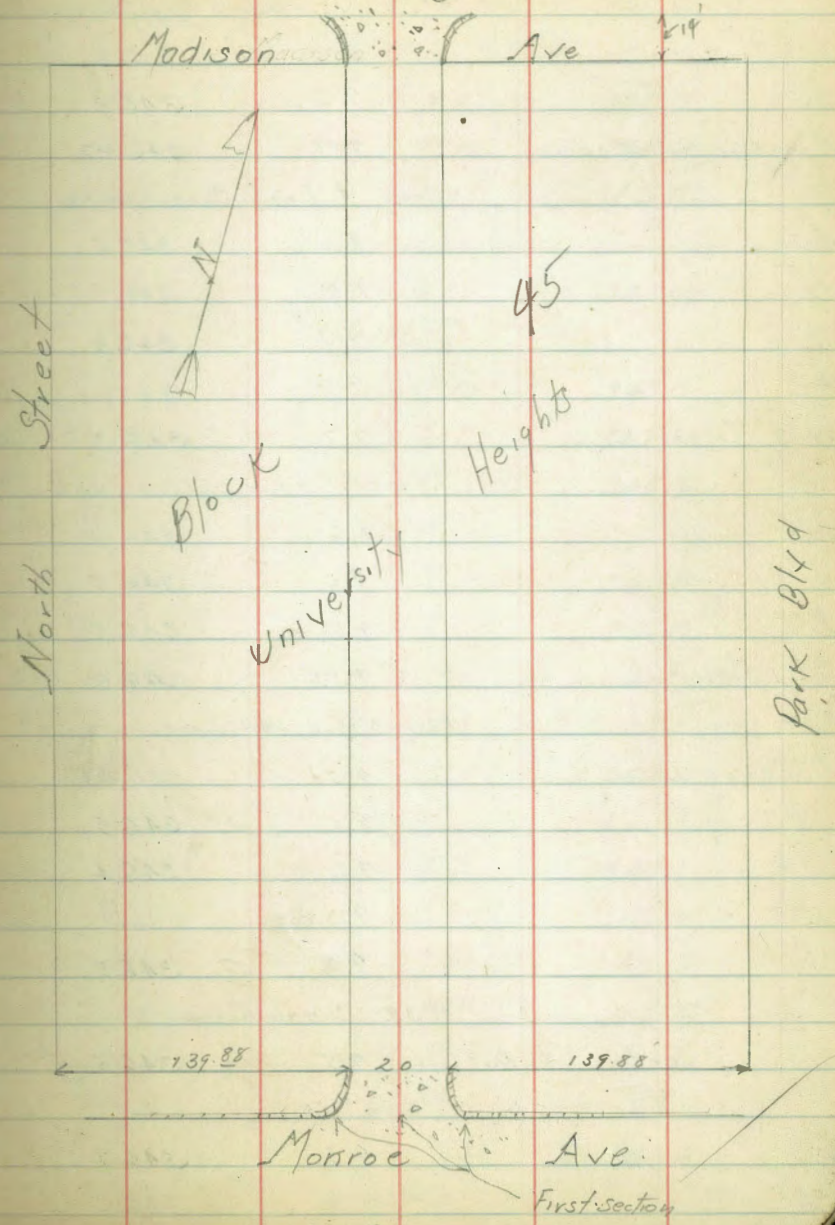
W.E. Bliss  
Duermit  
Jacobson  
Kiernan  
1/5/28

X Section Alley Block 45 Univ  
1/5. Monroe + Madison. Park Blvd + North

BM SE 87 Monroe  
+ Park Blvd

607	351.05	344.98
Section on obline of Monroe		
W Top Ch	5.21	345.84
Paving in Gutter	5.65	345.40
Φ	5.81	345.44
Paving in Gutter	5.60	345.45
E Top ch	5.11	345.71
on paving 0+00 N. Line of Monroe		
W Top ch	7.81	346.24
Gutter	5.01	346.04
E	5.14	345.91
E	4.92	346.13
E Top ch	4.84	346.21
0+05		
E	5.3	345.7
+ 4	5.1	345.9
Φ	9.9	346.1
N	4.8	346.2
0+25		
N	4.7	346.3
Φ	5.0	346.0
+ 7	5.0	346.0
E	4.9	346.1
0+56 S. End Apron Dbl Garage on East		
E on line concrete	4.61	346.44
Φ	4.9	346.1
W	4.5	346.5

Plotted Jan 8-29 CBH  
Yoge figured 1/6/29 TD  
BX 16-266



H.I.  
35/05

E/01

0174 N. End Concrete Apron Db/ Garage on East

W	4.4	346.6	E
E	4.8	346.2	E
E on Edge concrete apron	4.78	346.27	E

0195 E. Single Garage on West

E	4.6	346.4	W
+5	4.9	346.1	W
E	4.7	346.3	E
+5	4.9	346.1	W
W E Garage on line	4.7	346.3	E

1105 S. End Db/ Garage on East

W	4.6	346.4	E
E	4.5	346.5	E
E	4.5	346.5	E
3' Back concrete Floor	4.55	346.50	+5

1120 N. End Db/ Garage on East

3' Back concrete floor	4.51	346.54	W
E	4.5	346.5	W
E	4.6	346.4	W
+7	4.5	46.5	+3
W	4.8	346.2	+4

1139 Single Garage on East

online E. Dirt floor	4.5	346.5	+5
----------------------	-----	-------	----

1145

W	4.3	346.7	E
E	4.4	346.6	E

H.I.  
35/05

E/01

4.4 346.6

1152 S. Edge Concrete apron of Garage on West

4.3	346.7
4.0	347.0

4.13 346.92

1162 N. End concrete Apron of Single Garage on West

3.96 347.09

1168

4.0 347.0

3.9 347.1

4.3 346.7

1170

4.2 346.8

4.2 346.8

4.2 46.8

3.9 47.1

3.9 347.1

1180

3.9 347.1

3.8 47.2

4.5 46.5

4.4 346.6

4.4 46.6

4.0 47.0

4.2 346.8

1194

47

	H.I. 35/05	Elev	
	1199		
E	39	347.1	♀
+4	40	347.0	+3
+5	43	346.7	+6
♀	44	346.6	E
+2	40	347.0	TP
+7	42	46.8	
+8	38	47.2	E
W	40	347.0	+5
	2105 S End Concrete Apron Garage of West		+8
W on Edge concrete apron	378	347.27	♀
♀	39	347.1	Edge of Apron <sup>05</sup> in alley
+1	44	46.6	
+3	43	46.7	
+4	40	47.0	
E	39	347.1	W
	2115 N End Concrete Apron Garage of West		+7
on line.	365	347.40	♀
	2125	276 Beginning of concrete floor	+4
E	36	347.4	+5
+5	37	347.3	+7
♀	37	347.3	+8
W	32	347.8	E
	2132 S End Apron Db/Garage on West.		+5 Back. concrete floor.
W on concrete	327	347.78	
+1 Edge in Alley	330	347.7	Pod on ♀
+7	37	347.3	

	H.I. 35/05	Elev	
			48
	6.9/	359.4/	355
			347.50
			2150 N End Apron Db/Garage on West <sup>05</sup>
			6.7
			347.7
			7.0
			47.4
			7.0
			47.4
			6.8
			347.6
			6.53
			347.88
			2166 S End Single Garage on East
			6.60
			347.81
			2175
			6.4
			348.0
			6.5
			347.8
			6.4
			348.0
			6.6
			47.8
			6.9
			47.5
			6.8
			47.6
			6.6
			47.8
			6.6
			347.8
			6.60
			347.81
			2176 ♀ Concrete Drain on East Garage <sup>2" wide below</sup>
			6.57
			347.84

+

H.I.  
359.91

E/W

H.I.  
359.91

49

	2177	S. End Apron of 6 car Garage on East	W			
Floor 2 <sup>o</sup> Back	6.09	348.32				
East on Edge concrete apron	6.43	347.98				
£	6.4	348.0	N			
N	6.9	347.5	+4			
	2182	£ Drain on West <sup>This Drain Drain Back yard on West 1.5 Wide</sup>	£			
online £ of Drain	6.33	348.08	+5			
	2183	S. End of Dbl. Garage on West.	+6			
2 <sup>o</sup> Back	6.00	348.41	+8			
	2190	N. E. of Dbl. Garage on West Has Apron	E			
S. End of Apron online	6.07	348.34				
	2198	N. End of Dbl. Garage on West	E			
N. End Apron online	6.08	347.33	+2			
Floor 2 <sup>o</sup> Back	6.00	348.41	+5			
	3400		£			
W	6.1	348.3	W			
+5	6.3	348.1				
£	6.1	348.3				
+8	6.2	48.2				
+9	6.4	48.0				
E on Edge of Apron 6 car garage	6.26	348.15				
on floor 2 <sup>o</sup> Back	6.09	348.37				
	3125	N. End 6 Car Garage on East				
Floor 2 <sup>o</sup> Back	5.99	348.47				
Edge Apron online	6.18	348.23				
£	5.9	348.5	W			

	6.1	348.3				
	2132	S. End Dbl. Garage on West				
Floor 1.5 <sup>o</sup> Back concrete	5.60	348.01				
	5.8	348.6				
	6.0	48.4				
	5.7	348.7				
	5.8	48.6				
	6.0	48.4				
	5.7	48.7				
	5.8	348.6				
	3150	N. End Dbl. Garage on West				
	5.5	348.9				
	5.7	48.7				
	5.6	48.8				
	5.9	349.0				
	5.5	348.9				
Floor Garage 1.5 <sup>o</sup> Back <sup>concrete</sup>	5.97	348.94 ✓				
	3153	S. End Dbl. Garage on East				
Edge Concrete Apron 1.5 <sup>o</sup> Back	5.43	348.98				
Floor 3 <sup>o</sup> Back	5.13	349.28 ✓				
	3153	S. End Simple Garage on West				
concrete floor 1.2 <sup>o</sup> Back	5.36	349.05 ✓				
	3164	N. End Simple Garage on West				
concrete floor 1.2 <sup>o</sup> Back	5.36	349.05 ✓				
	3171	N				
	5.3	349.1				

H.I.  
354.41

3785 Pepper Tree  
3792 " "  
o.c. Back

♀	5.2	349.2
E	5.4	349.0
Apron 1.0 Back	5.35	349.06
Floor 3.00 Back	5.14	349.27 ✓
3776 S. End Db1 Garage on East		
floor 2.8 Back	5.19	349.22 ✓
3797 N. End Db1 Garage on East		
floor 2.4 Back	5.13	349.28 ✓
E	5.2	349.2
+5	5.2	49.2 ✓
♀	5.0	349.4
+8	4.9	49.5
N.	5.9	348.5
3794		
N	5.2	349.2
+2	5.0	49.4
♀	5.0	349.4
E	5.0	349.4
4725		
E	4.9	349.5
♀	4.8	349.8
N	4.8	349.6
4780 S. End Db1 Garage on East		
N	4.8	349.6
♀	4.6	349.8
E	4.6	349.8

H.I.  
354.91

933

50

Garage 5.8 Back concrete	4.95	349.96 ✓
9739 ♀ Simple Garage on West		
Wooden floor 2.5 Back	4.95	349.96 ✓
4796 N. End Db1 Garage on East		
floor 5.8 Back concrete	4.33	350.08 ✓
E	4.6	349.8
♀	4.4	350.0
N	4.4	350.0
4765		
N	4.2	350.2
♀	4.1	350.3
E	4.2	350.2
9775 S. End Db1 Garage on West		
E	4.1	350.3
♀	4.0	350.4
N	4.0	350.4
Apron 2.2 Back	3.65	350.76
floor 4.0 "	3.50	350.91 ✓
9798 N. End Db1 Garage on West		
floor 4.0 Back	3.44	350.97 ✓
Apron 2.2 Back	3.60	350.81 ✓
N	3.6	350.8
♀	3.7	350.7
E	4.0	350.4
5709 S. End Db1 Garage on West		
Apron 2.7 Back	3.49	350.92

H.I.  
354.41

floor	3-4 Back	3.93	350.98	↓	♀
					N
					5121 N. End Db/Garage on West
floor	3-4 Back	3.29	351.12	↓	
Apron	2.7	3.42	350.99	↓	N
N		3.4	351.0		♀
+7		3.1	351.3		+5
♀		3.3	351.1		E
E		3.7	350.7		7P

5123 S. End Db/Garage on West

floor	3-4 Back	3.26	351.15	↓	E - Paving a Top cb level
					♀ Top
					Bottom
					5132 S. End Db/Garage on East
					5141 N. End Db/Garage on West
E		3.9	351.0		N
♀		3.5	350.9		N Top cb
+2		3.2	351.2		♀ Bottom
N		3.5	350.9		Top
floor concrete	3-4 Back	3.24	351.17	↓	E

5150 N. End Db/Garage on East

	1.8 Back Dirt floor	3.4	351.0		E Top cb
					♀ Top
					Bottom
					5160
N		3.4	351.0		♀ Bottom
♀		3.1	351.3		N Top cb
E		3.0	351.4		
					5180
E		2.9	351.5		N Top cb
					N in Color

H.I.  
354.41

5185

51

		2.9	351.5		
		3.1	351.3		
					5195
		3.2	351.2		
		3.0	351.4		
		3.2	351.2		
		2.9	351.5		
		2.90	351.51		

6101 S. Line of Madison

		5.50	351.35		
		5.59	351.26		
		5.72	351.13		
		5.50	351.35		
					S. Line of Madison + 5
		5.56	351.29		
		5.92	350.93		
		5.85	351.00		
		5.59	351.26		

S. Line of Madison + 10

		5.85	351.00		
		6.11	350.74		
		6.19	350.69		
		5.87	351.01		
		5.72	351.13		

Section on Cb line of Madison + 41.04

		5.91	350.94		
		6.52	350.33		



H.I.  
356.85

¢			6.91	350.41
to in gutter			6.96	350.39
Topcb			5.81	351.04
T.P.	2.39	352.89	6.35	350.50
			6.96	346.73
T.P.	7.32	350.75	7.97	344.92
check on starting			5.83	344.92
Bar				344.92
				0.05 ✓

C-st. Cross Sections

Cont. from P. 79

20.24

T.P.	5.40	18.44	7.20	13.04
on track #1-75' N.N.L.			5.96	12.48
" " #2-75' N.N.L.			5.96	12.48
" " #1 at S.L.			5.50	12.94 ✓
" " #4 " N.N.L.			5.55	12.89 ✓
" " #4 " S.C-st.			5.42	13.02
" " #2 " " "			5.43	13.01
" " #3 " " "			5.42	13.02
" " #1 " " "			5.39	13.05
" " #1 " S.L.-C-st.			5.28	13.16
" " #2 " " "			5.37	13.07
" " #3 " " "			5.34	13.10
" " #4 " " "			5.31	13.13
" " #1 " 75' S.S.L.			5.09	13.35
" " #2 " " "			5.21	13.23

18.44

52

on track #3-75' S.S.L.-C-st.	5.21	13.23
" " #4- " " " "	5.19	13.25
" " #5- " " " "	6.01	12.43
" " #6- " " " "	6.02	12.42
" " #7- " " " "	6.25	12.19
" " #8- " " " "	6.26	12.18
" " #9- " " " "	6.87	11.57
" " #10- " " " "	6.89	11.55
" " #10 at S.L.-C-st.	6.75	11.69
" " #9 " " " "	6.74	11.70
" " #8 " " " "	6.00	12.44
" " #7 " " " "	6.00	12.44
" " #6 " " " "	5.77	12.67
" " #5 " " " "	5.77	12.67
" " #5 at S.L.-C-st.	5.66	12.78 ✓
" " #6 " " " "	5.65	12.79 ✓
" " #7 " " " "	5.89	12.55 ✓
" " #8 " " " "	5.88	12.56 ✓
" " #9 " " " "	6.74	11.70 ✓
" " #10 " " " "	6.74	11.70
" " #10 " N.L.-C-st.	6.73	11.71
" " #9 " " " C-st.	6.73	11.71
" " #8 " " " "	5.88	12.56
" " #7 " " " "	5.93	12.51
" " #6 " " " "	5.51	12.93
" " #5 " " " "	5.48	12.96

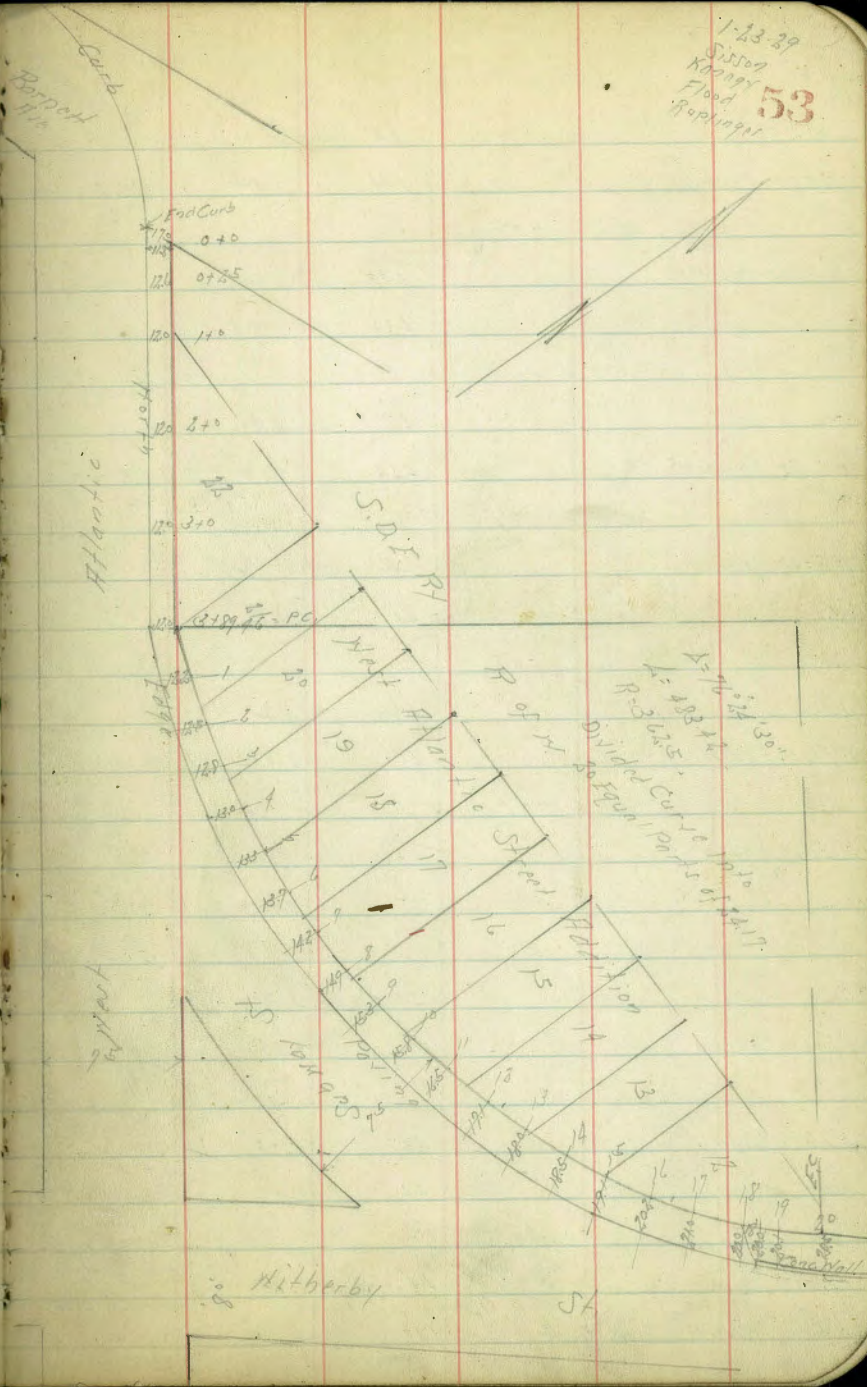
Cont. on P. 68

West Atlantic & Subway Street  
 Cross Section  
 Yardage B13 B 40  
 4-2-29  
 70.

1-23-39  
 D. J. ...  
 Flood  
 53

BM	1.52	5.90	4.38
TP	4.29	5.58	4.11 1.29
		040 = S.L. Barnett on Diagonal	
Top Cb		1.03	1.55
Gutter		4.66	0.92
H.L. of Atlantic		3.8	1.8
		040 Paving Squared off	
H.L. of Atlantic		3.8	1.8
+11.8 = N Edge Paving		4.56	1.02
		25' E of S.L. Barnett	13.6 del. to the
H. Edge Paving		4.41	1.17
H.L.		4.3	1.4
		50' E	
H.L.		5.2	0.4
N Edge Paving		4.40	1.18
		75' E	
H Edge Paving		4.41	1.17
H.L.		4.30	1.4
		100' E	13.0 del. to the
H.L.		4.2	1.4
H Edge Paving		4.43	1.15
		125' E	
H Edge Paving		4.41	1.14
H.L.		4.40	1.18
		150' E	

SE Top of  
 H. L. of Atlantic



558

H.L.	43	1.3
H. Edge Pairing	444	1.14
175 F		
H. Edge Pairing	442	1.16
H.L.	430	1.38
200 F		
H.L.	42	1.4
H. Edge Pairing	444	1.14
225 F		
H. Edge Pairing	446	1.12
H.L.	41	1.5
250 F		
H.L.	43	1.2
H. Edge Pairing	446	1.12
275 F		
H. Edge Pairing	448	1.10
H.L.	45	1.6
300 F		
H.L.	43	1.3
H. Edge Pairing	450	1.08
325 F		
H. Edge Pairing	447	1.11
H.L.	43	1.3
350 F		
H.L.	44	1.2
H. Edge Pairing	442	1.16

12.0 H.L. to Pair

12.0 H.L. to Pair

558

54

375 F

H. Edge Pairing	450	1.08
H.L.	47	1.2
389 H.F. = PC		
H.L.	45	1.1
H. Edge Pairing	450	1.08
Part 1		
H. Edge Pairing	466	0.92
H.L.	44	1.2
Part 2		
H.L.	45	1.1
H. Edge Pairing	479	0.79
Part 3		
H. Edge Pairing	470	0.88
H.L.	45	1.1
Part 4		
H.L.	46	1.0
H. Edge Pairing	470	0.88
Part 5		
H. Edge Pairing	461	0.97
H.L.	45	1.1
Part 6		
H.L.	47	0.8
H. Edge Pairing	460	0.98
Part 7		
H. Edge Pairing	471	0.87

12.0 H.L. to Pair

12.3 H.L. to Pair

12.5 H.L. to Pair

12.8 H.L. to Pair

13.0 H.L. to Pair

12.3 H.L. to Pair

12.7 H.L. to Pair

12.2 H.L. to Pair

N.L.	47	0.9
Part 8		
N.L.	44	1.1
N Edge Pavine	150	1.08
Part 9		
N Edge Pavine	476	0.82
N.L.	46	1.0
Part 10		
N.L.	44	1.2
N Edge Pavine	479	0.79
Part 11		
N Edge Pavine	453	1.05
N.L.	44	1.2
Part 12		
N.L.	40	1.6
N Edge Pavine	432	1.26
Part 13		
N Edge Pavine	417	1.41
N.L.	43	1.3
Part 14		
N.L.	46	1.0
N Edge Pavine	461	1.32
Part 15		
N Edge Pavine	422	1.34
N.L.	31	2.5
Part 16		

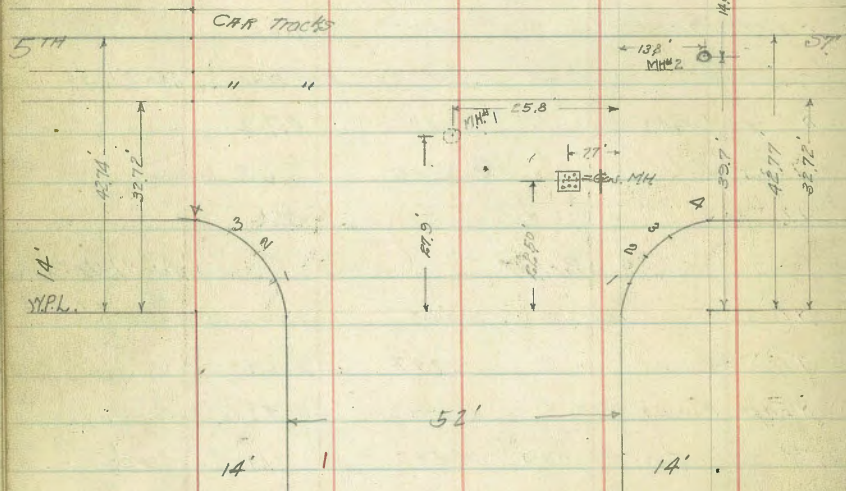
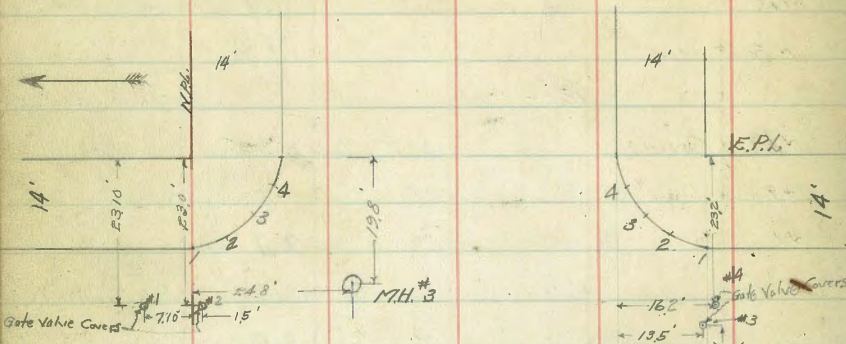
148 N.L. to Pav  
153 N.L. to Pav  
158 N.L. to Pav  
165 N.L. to Pav  
171 N.L. to Pav  
180 N.L. to Pav  
185 N.L. to Pav  
191 N.L. to Pav  
202 N.L. to Pav

N.L.	415	2.5	3.1	
N Edge Pavine	428	2.9	2.7	
Part 17				
N Edge Pavine	423	1.23	1.35	
TP	49	3.1	2.0	
N.L.	42	2.9	2.7	
Part 18				
N.L.	46	3.6	2.0	
N Edge Pavine	452	1.52	1.06	
Part 19				
N Edge Pavine	486	1.86	0.72	
Top Wall	495	2.95	2.63	
N.L.	40	3.0	2.6	
Part 19				
N.L.	46	3.0	2.6	
Top Wall	497	2.97	2.61	
N Edge Pavine	500	5.00	0.58	
TP	500	7.63	2.95	2.63
Part 20 - FC				
N Edge Pavine	807	8.07	-0.44	
Top Wall	504	5.04	+2.59	
N.L.	40	4.0	+3.6	
BM	324	3.24	4.39	

210 N.L. to Pav  
200 N.L. to Pav  
200 N.L. to Pav  
201 N.L. to Pav  
205 N.L. to Face of Edge Pav

CROSS SECTION "G" STREET  
From E.L. 4TH ST. to N.L. 6TH ST.

Walker  
145 High.  
Lee Roy  
Morton  
8.66-19



Station	526	31.48	26.22	St. BP 15" Rad 5'17"
E. line 4th St. = 0+00				
N-735			8.55	23.13
= N top cb.				
" Gut. on Pav.			9.41	22.07
cb + 5.2			9.26	22.22
+ 15.6			9.30	22.18
g			9.45	22.03
+ 10.4			9.64	21.84
+ 20.8			9.96	21.52
S Gut.			10.02	21.46
S-14'				
= top cb.			9.55	21.93
0+20				
S+14			8.99	22.49
= S top cb.				
" Gut. on Pav.			9.65	21.83
cb + 5.2			9.44	22.04
+ 15.6			9.08	22.40
g			8.92	22.56
+ 10.4			8.75	22.73
+ 20.8			8.76	22.72
N Gut. on "			8.74	22.74
N-14.15				
= N top cb.			8.10	23.38
0+40				
N-14.15			7.61	23.87
= N top cb.				
" Gut on Pav.			8.28	23.20
" cb + 5.2			8.17	23.31
+ 15.6			8.32	23.16

L on Pav.	8.39	23.09
+10.4 " "	8.54	22.94
+20.8 " "	8.94	22.54
S Gut. " "	9.20	22.28
" Top cb. 10 Drive Way	9.20	22.28
S + 14'	0+60	
= S top cb.	7.89	23.59
" Gut. on Pav.	8.60	22.88
s cb. + 5.2 on Pav.	8.38	23.10
+ 15.6 " "	8.04	23.44
L " "	7.84	23.64
+ 10.4 " "	7.72	23.76
+ 20.8 " "	7.66	23.82
N Gut. " "	7.70	23.78
N-14.15'		
= N top cb.	7.12	24.36
N-14.10'	0+80	
= N top cb.	6.61	24.82
N Gut. on Pav.	7.21	24.27
cb + 5.2	7.20	24.28
+ 15.6	7.28	24.20
L	7.25	24.23
+ 10.4	7.40	24.08
+ 20.8	7.84	23.64
S Gut.	8.12	23.36
S top cb.	7.33	24.15
	1+00	

S + 14.05'		
= S top cb.	6.84	24.64
S Gut. on Pav.	7.54	23.94
s cb + 5.2	7.32	24.16
+ 15.6	7.03	24.48
L	6.83	24.65
+ 10.4	6.75	24.73
+ 20.8	6.77	24.71
N-14.10'		
N Gut.	6.78	24.70
N top cb.	6.13	25.35
N-14.00'	1+20	
= N top cb.	5.72	25.76
N Gut.	6.50	24.98
cb + 5.2	6.31	25.15
+ 15.6	6.29	25.19
L	6.39	25.09
+ 10.4	6.61	24.82
+ 20.8	6.99	24.49
S Gut.	7.18	24.30
S-14.05'		
= S top cb.	6.43	24.99
S + 14.00'	1+40	
= S top cb.	6.15	25.33
S Gut.	6.86	24.62
+ 5.2	6.62	24.86
+ 15.6	6.29	25.19
L	6.11	25.37
+ 10.4	5.96	25.52

L + 20.8		5.90	25.58
N Gut.		6.14	25.34
<sup>N-12'</sup> = N top cb.		5.38	26.10
	1 + 60		
<sup>N+14'</sup> = N Top cb.		5.26	26.42
" Gut.		5.81	25.62
+ 5.2		5.58	25.90
+ 15.6		5.65	25.83
L		5.82	25.66
+ 10.4		5.95	25.53
+ 20.8		6.22	25.26
S Gut.		6.44	25.04
S top cb.		5.80	25.68
	{ 1 + 10 } Note 1 + 10		
S top cb.		6.55	24.93
" Gut.		7.36	24.12
+ 5.2		7.14	24.24
+ 15.6		6.84	24.64
L		6.59	24.89
+ 10.4		6.51	24.97
+ 20.8		6.44	25.04
N Gut.		6.61	24.89
N top cb.		5.87	25.61
	1 + 80		
<sup>N+14'</sup> = N top cb.		4.68	26.80
" Gut.		5.10	26.08

Gut. + 5.2'		5.25	26.23
+ 15.6		5.35	26.13
L		5.45	26.03
+ 10.4		5.61	25.87
+ 20.8		5.91	25.57
S Gut.		6.14	25.34
<sup>S-14.03'</sup> = S top cb.		5.45	25.03
	L + 00.3 = N. 5.14 <sup>14' cbs</sup> 13.75		
<sup>S+18.9'</sup> = S top cb.		5.06	26.42
S Gut.		5.75	25.73
+ 5.2		5.68	25.80
+ 15.6		5.52	25.96
L		5.30	26.18
+ 10.4		5.22	26.26
+ 20.8		4.94	26.54
N Gut.		4.94	26.54
<sup>N-13.96'</sup> = N top cb.		4.22	27.26
	N.M. Return in 4 equal Parts		
Part 1 on top cb.		4.35	27.13
" 1 " Gut.		4.89	26.59
" 2 " top cb.		4.28	27.20
" 2 " Gut.		4.16	26.62
" 3 " top cb.		4.32	27.16
" 3 " Gut.		4.85	26.63
" 4 " top cb.		4.25	27.13
" 4 " Gut.		4.80	26.68

T.P. 4.75 30.97 5.26 26.22

S.W. Return 4 = Parts

Part 1 on cb. 4.59 26.38  
 " 1 " Gut 5.25 25.72  
 " 2 " " 5.21 25.76  
 " 2 " cb. 4.60 26.32  
 " 3 " " 4.55 26.42  
 " 3 " Gut 5.25 25.72  
 " 4 " " 5.29 25.68  
 " 4 " top cb. 4.60 26.32

S.E. Return 4 Parts

Part 1 oil top cb. 4.78 26.19  
 " 1 " Gut. 5.50 25.47  
 " 2 " " 5.43 25.54  
 " 2 " top cb. 4.75 26.22  
 " 3 " " " 4.79 26.18  
 " 3 " Gut 5.38 25.59  
 " 4 " " 5.33 25.64  
 " 4 " cb. 4.79 26.18

N.E. Return 4 = Parts

Part 1 on cb. 3.76 27.21  
 " 1 " Gut 4.50 26.47  
 " 2 " " 4.50 26.47  
 " 2 " cb. 3.73 27.24  
 " 3 " " 3.71 27.26  
 " 3 " Gut 4.50 26.47

Part 4 on cb. 3.80 27.17

" 4 " Gut. 4.41 26.56

Shots on M.H. Etc.

Gas. M.H. 4.87 26.10  
 M.H. #1 4.60 26.37  
 M.H. #2 5.06 25.91  
 M.H. #3 4.47 26.50  
 Gate Valve Cover #1 3.89 27.08  
 " " " #2 4.09 26.89  
 " " " #3 5.02 25.95  
 " " " #4 5.10 25.87

Readings on <sup>West</sup> Rails = 32.77 E. of W.L.

S prop on Rail 4.95 26.02

" cb " " 4.77 26.20

2 5" st. " " 4.48 26.49

N cb " " 4.16 26.87

N " " 3.93 27.04

42.77 E. of W.L. - 1/2 Rail of E. track

N " " 3.96 27.01

" cb " " 4.15 26.82

2 5" st. " " 4.48 26.49

1 5" cb. " " 4.80 26.17

S " " 4.97 26.00

S-10' on Pav. West cb. Line 5 1/2 st. 5.47 25.50

S on Pav. 5.31 25.66

cb. 5.11 25.86



1/2 on Pav.	4.92	26.05
1/2 " "	4.66	26.31
1/2 " "	4.45	26.52
cb	4.28	26.69
N	4.28	26.69
+20	3.98	26.99
West of 5th st.		
-20 on Pav.	3.66	27.31
N " "	3.97	27.00
cb. " "	4.18	26.79
1/2 " "	4.37	26.60
1/2 " "	4.56	26.21
1/2 " "	4.69	26.28
5 cb. " "	4.82	26.15
S " "	5.03	25.94
+10 " "	5.18	25.79
2 5th st.		
-10' " "	5.10	25.87
S " "	5.00	25.97
cb " "	4.78	26.19
1/2 " "	4.65	26.32
1/2 " "	4.51	26.46
1 1/2 " "	4.33	26.64
cb. " "	4.16	26.81
N " "	3.95	27.02
+20 " "	3.63	27.34

			East of 5th		
			N-20' on Pav.	3.60	27.37
			N " "	4.00	26.97
			" d. " "	4.20	26.77
			" 1/2 " "	4.42	26.55
			1/2 " "	4.58	26.39
			S 1/2 " "	4.74	26.23
			" cb. " "	4.89	26.08
			S " "	5.03	25.94
			+10 " "	5.17	25.80
			East cb. 5th		
			-10' " "	5.65	25.32
			S " "	5.50	25.47
			d. " "	5.33	25.64
			S 1/2 " "	5.19	25.78
			1/2 " "	5.00	25.97
			N 1/2 " "	4.78	26.19
			" cb. " "	4.63	26.34
			N " "	4.50	26.47
			+20' " "	4.12	26.85
			East Line 5th st. = 0+00		
			N+1205 = N cb.	3.68	27.29
			" Sid.	4.31	26.66
			+5.2	4.44	26.53
			+15.6	4.58	26.39
			1/2	4.68	26.29

3097

2 + 104	4.96	26.01
+ 20.8	5.25	25.72
S Gut S-14.27 = S cb.	5.18	25.69
	4.76	26.21
S-14.24 = S cb.	4.34	26.63
S Gut on Pav.	5.02	25.95
+ 5.2	4.90	26.07
+ 15.6	4.19	26.48
2	4.17	26.80
+ 10.4	3.91	27.06
+ 20.8	3.90	27.07
N Gut N-12.10 = N top cb.	3.99	26.98
	3.23	27.74
N+12.1 = N top cb.	2.71	28.26
" Gut.	3.45	27.52
+ 5.2	3.26	27.51
+ 15.6	3.53	27.44
2	3.77	27.20
+ 10.4	4.00	26.97
+ 20.8	4.33	26.64
S Gut	4.46	26.51
S-14.23 = S top cb.	3.87	27.10
TP	8.73	37.07
0+60	2.69	28.34

3707

61

S+14.2 = S cb.	9.19	27.58
S Gut	10.07	27.00
+ 5.2	10.01	27.06
+ 15.6	9.64	27.43
2	9.35	27.62
+ 10.4	9.10	27.97
+ 20.8 N-12.09	9.06	28.01
= N Gut N-12.09 = N cb.	9.16	27.91
	8.38	28.69
N+12.09 = N cb.	7.94	29.13
" Gut.	8.69	28.38
+ 5.2	8.54	28.53
+ 15.6	8.66	28.41
2	8.97	28.10
+ 10.4	9.24	27.83
+ 20.8	9.52	27.55
S Gut S-14.23 = S top cb.	9.67	27.40
	9.13	27.94
S+14.32 = S cb.	8.70	28.37
" Gut.	9.22	27.85
+ 5.2	9.08	27.99
+ 15.6	8.79	28.28
2	8.52	28.55
+ 10.4	8.22	28.85

£ + 208		8.10	28.97
N Gut.		8.10	28.97
N-1408			
= N cb		7.48	29.59
N + 1408	1+20		
= N cb.		7.00	30.07
" Gut.		7.68	29.39
+ 52		7.72	29.35
+ 156		7.85	29.22
£		8.13	28.94
+ 104		8.35	28.72
+ 208		8.60	28.47
S Gut.		8.74	28.33
S-1404			
= S topcb		8.05	29.02
Note 1+00.05 on south topcb =		8.50	28.57
S + 1404	1+40		
= S cb		7.59	29.48
" Gut.		8.26	28.81
+ 52		8.09	28.98
+ 15.6		7.84	29.23
£		7.67	29.40
+ 104		7.36	29.71
+ 208		7.20	29.87
N Gut.		7.31	29.76
N-1409			
= N topcb.		6.52	30.55
N + 1407	1+60		
= N cb.		6.13	30.94

N Gut.		6.79	30.28
+ 52		6.73	30.34
+ 15.6		6.92	30.15
£		7.15	29.22
+ 104		7.29	29.78
+ 208		7.58	29.49
S Gut.		7.81	29.26
S-1405			
= S cb.		7.12	29.95
S + 1402	1+80		
= S cb.		6.61	30.46
S Gut.		7.23	29.84
+ 52		7.04	30.03
+ 15.6		6.83	30.24
£		6.50	30.57
+ 104		6.26	30.81
+ 208		6.11	30.96
N Gut.		6.28	30.79
N-1412			
= N cb.		5.65	31.42
N + 1410	£ + 00.3' = N.L. 6 1/2		
= N cb.		5.08	32.99
" Gut.		5.50	31.57
+ 52		5.65	31.42
+ 15.6		5.86	31.21
£		6.07	31.00
+ 104		6.28	30.79
+ 208		6.50	30.57

3707

S Gut	6.52	30.55
5-1398		
= S top cb	6.14	30.23
5.85' East W.A. 6th = Section on A		
S cb	6.15	
" Gut	6.60	
S cb + 5.2	6.53	
+ 15.6	6.27	
L	6.10	
+ 10.4	6.02	
+ 20.8	5.81	
N Gut	5.65	
N top cb	5.16	

N.Y. Return

Part 2 on cb.	5.20
" " " Gut	5.85
" 3 " "	5.90
" 3 " cb	5.26
" 4 " "	5.20
" 4 " Gut	5.81

S.Y. Return

Part 2	6.16
" " " Gut	6.73
" 3 " "	6.76
" 3 " cb	6.20
" 4 " "	6.19
" 4 " Gut	6.88

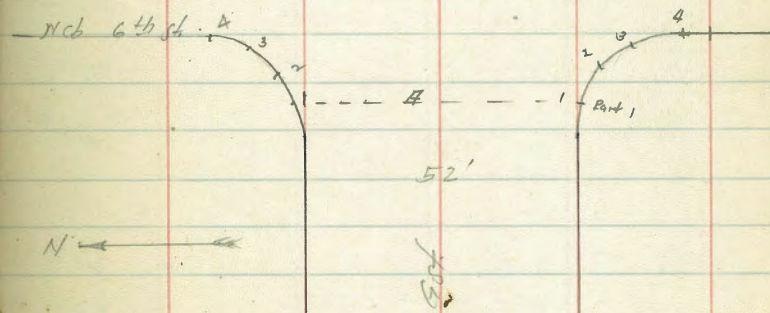
3707

N cb Line 6th

63

S cb.	6.81
+ 5.2	6.74
+ 15.6	6.33
L	6.26
+ 10.4	6.18
+ 20.8	5.97
N Gut	5.93
cb. N.E. BR 5th and 6.	10.86

26.71  
26.72 - B.M.  
0.01 - Error.



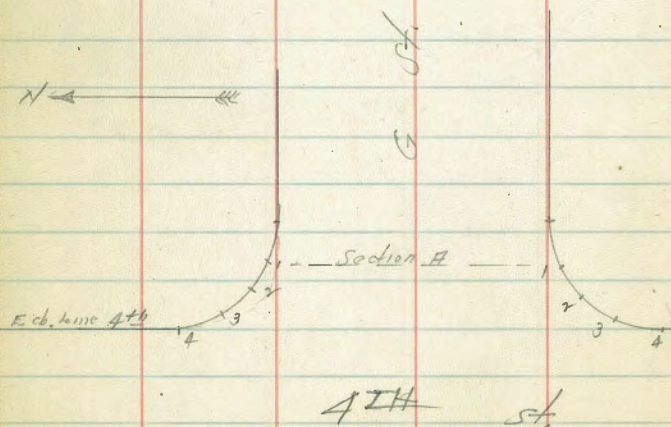
2.95

29.17

26.22

N.E. Return. 4 Parks 4th & G St.

Part 1 on cb.	6.30
" " " Gut.	6.96
" 2 " "	6.95
" 2 " cb.	6.29
" 3 " "	6.34
" 3 " Gut.	6.94
" 4 " "	6.92
" 4 " top cb.	6.31



S.E. Returns.

Part. 1 on cb.	7.18
" 1 " Gut.	7.83
" 2 " "	7.89
" 2 " cb.	7.19
" 3 " "	7.17
" 3 " Gut.	8.00
" 4 " "	8.09
" 4 " cb.	7.25

Section #

S Gut.	7.83
+5.2	7.66
+15.6	7.47
↓	7.26
+10.4	7.12
+20.8	7.03
N Gut.	6.96

E cb. line 4th

N Gut. = N cb. line	7.06
+5.2	7.14
+15.6	7.29
↓	7.45
+10.4	7.65
+20.8	7.79
S Gut.	7.89

5-22-29 Levels on Paving of Witherby  
 J.C. Bliss Street Underpass - below Santa Fe  
 Dierbert R.R. - 30' wide - Roadway - 7 1/2' / 4.5  
 Runway

B.M. B.P. Westab. line Witherby by Arc light Pole.			1/4	
about 550 East of Underpass	27.73		S	
+ 0.11	27.84			
T.P.		-12.92	14.92	S
+ 0.11	15.03			1/4
T.P.		-12.70	2.33	1/4
+ 0.28				1/4

H.I. 2.61

1450 - East

N	0.85	1.76	N	
1/4	0.85	1.76	1/4	
1/4	0.87	1.74	1/4	
1/4	0.95	1.66	1/4	
G	1.15	1.46	S	
S T.P. 66	0.70	1.91		

1425 - East

S	3.30	-0.69	1/4	
1/4	3.18	-0.57	1/4	
1/4	2.98	-0.37	1/4	
1/4	3.00	-0.39	N	
N	3.00	-0.39		

1400 - East

N	5.08	-2.47	1/4	
1/4	5.12	-2.51	1/4	
1/4	5.06	-2.45	1/4	

Reduced May 22, 29  
 Reynolds

H.I. 2.61

65

	5.15	-2.54	
	5.22	-2.61	✓
0+80 - East - Beginning of seepage			
	6.78	-4.17	✓ ✓
	6.77	-4.16	✓
	6.81	-4.20	✓ -
	6.82	-4.21	✓
	6.82	-4.21	✓ -

0+70

	7.60	-4.99	✓ -
	7.63	-5.02	✓
	7.60	-4.99	✓
	7.60	-4.99	
	7.61	-5.00	✓

0+60

	8.39	-5.78	✓
	8.38	-5.77	✓
	8.35	-5.74	✓
	8.36	-5.75	✓
	8.37	-5.71	✓ ✓

0+50

	9.15	-6.54	✓ ✓
	9.17	-6.56	✓
	9.19	-6.58	✓ -
	9.22	-6.61	

H.I. 261

S	9.22	-6.61 <sup>✓</sup>	S
	0+40		1/4
S	10.03	-7.42 <sup>✓</sup>	£
1/4	10.07	-7.46 <sup>✓</sup>	1/4
£	10.07	-7.46 <sup>✓✓</sup>	N
1/4	10.04	-7.43 <sup>✓</sup>	
N	9.94	-7.33 <sup>✓✓</sup>	Viaduct
	0+30		
N	10.64	-8.03 <sup>✓✓</sup>	N
1/4	10.76	-8.15 <sup>✓</sup>	1/4
£	10.78	-8.17 <sup>✓</sup>	£
1/4	10.80	-8.19 <sup>✓</sup>	1/4
S	10.76	-8.15 <sup>✓</sup>	S
	0+20		
S	11.30	-8.69 <sup>✓</sup>	S
1/4	11.34	-8.73 <sup>✓</sup>	1/4
£	11.35	-8.74 <sup>✓</sup>	£
1/4	11.38	-8.77 <sup>✓</sup>	1/4
N	11.40	-8.79 <sup>✓</sup>	N
	0+10		
N	11.76	-9.15 <sup>✓</sup>	N
1/4	11.78	-9.17 <sup>✓</sup>	1/4
£	11.74	-9.13 <sup>✓</sup>	£
1/4	11.75	-9.14 <sup>✓</sup>	1/4
S	11.70	-9.09 <sup>✓</sup>	S

H.I. 261

66

0+00 - £ 12" Grating - bottom Underpass

11.80	-9.19 <sup>✓</sup>	S
11.84	-9.23	1/4
11.84	-9.23 <sup>✓</sup>	£
11.83	-9.27 <sup>✓</sup>	1/4
11.80	-9.19 <sup>✓</sup>	N

Shot on bottom of deck of Santa Fe

+3.16 +5.77

0+10 - West

11.76	-9.15 <sup>✓✓</sup>	N
11.67	-9.06 <sup>✓✓</sup>	1/4
11.67	-9.06 <sup>✓✓</sup>	£
11.71	-9.10	1/4
11.68	-9.07 <sup>✓✓</sup>	S

0+20 - West

11.50	-8.89 <sup>✓✓</sup>	S
11.50	-8.89	1/4
11.52	-8.91 <sup>✓</sup>	£
11.47	-8.86 <sup>✓</sup>	1/4
11.60	-8.99 <sup>✓✓</sup>	N

0+30 - West

11.32	-8.71 <sup>✓✓</sup>	N
11.25	-8.64 <sup>✓</sup>	1/4
11.22	-8.61 <sup>✓</sup>	£
11.20	-8.59 <sup>✓</sup>	1/4
11.17	-8.56 <sup>✓</sup>	S

H.1.2.61

0+40-West

S	10.75	-8.14 ✓
1/4	10.70	-8.09
¢	10.71	-8.10 ✓
1/4	10.79	-8.19 ✓
N	10.85	-8.24 ✓

0+50-West

N	10.30	-7.69 ✓
1/4	10.27	-7.66 ✓
¢	10.24	-7.63 ✓
1/4	10.26	-7.65
S	10.23	-7.62 ✓

0+60

S	9.72	-7.11 ✓
1/4	9.72	-7.16
¢	9.77	-7.18 ✓
1/4	9.81	-7.20 ✓
N	9.83	-7.22 ✓

0+70

N	9.34	-6.73 ✓
1/4	9.30	-6.69 ✓
¢	9.25	-6.64 ✓
1/4	9.26	-6.65
S	9.25	-6.64 ✓

H.1.2.61

67

0+80

S	8.77	-6.16 ✓
1/4	8.77	-6.16
¢	8.75	-6.14 ✓
1/4	8.76	-6.15 ✓
N	8.81	-6.20 ✓✓

0+90

N	8.35	-5.74 ✓
1/4	8.28	-5.67 ✓
¢	8.23	-5.62 ✓
1/4	8.24	-5.63
S	8.20	-5.59 ✓

1+00

S	7.66	-5.05 ✓
1/4	7.70	-5.09 ✓
¢	7.67	-5.06 ✓
1/4	7.72	-5.11 ✓
N	7.72	-5.11 ✓✓

Note - Main seepage ends at 1+00 - there is slight seepage up to 1+20

1+25

N	6.44	-3.83 ✓
1/4	6.41	-3.80 ✓
¢	6.40	-3.79 ✓
1/4	6.40	-3.79 ✓
S	6.36	-3.75 ✓



H.I. 2.61

1+50-West

S	5.01	-2.40
1/4	5.20	-2.59
1/2	5.32	-2.71 <sup>rx</sup>
3/4	5.45	-2.84 <sup>v</sup>
N	5.47	-2.86
T.P.	-2.67	(-0.06)

+ 7.51 7.46

B.M. S.W. Top Hydrant Within by Atlantic

	-3.18	4.28
Correct		+38
Error		0.10

## C-St. Cross Sections

Cont. from P-52

18.44

Truss # 7-75' N.W. C-St	6.00	12.44
" " 8- " " " " "	5.96	12.48
" " 9- " " " " "	6.61	11.83
" " 10- " " " " "	6.61	11.83

Z+00 = E.L. Kettner Blvd.

N	6.2	12.1 ✓
cb	6.2	12.2 ✓
1/4	6.2	12.2
1/2	6.2	12.2
3/4	6.3	12.1
cb	6.3	12.1

18.44

68

S 6.2 12.2

E.L. Kettner +20.8 = Back edge curb line

S	6.7	11.7
cb	6.8	11.6 ✓
1/4	6.6	11.8
1/2	6.6	11.8
3/4	6.7	11.7
cb	6.7	11.7
N	6.8	11.6 ✓

E.L. Kettner +21.6 = curb line = curb face

N-100' on top cb	5.89	12.55
-75' " " "	5.95	12.49
-50' " " "	5.97	12.47
-25' " " "	6.03	12.41
N on " " "	6.06	12.38 ✓
cb " " "	6.07	12.37 ✓
1/4 " " "	6.07	12.37
1/2 " " "	6.07	12.37
3/4 " " "	6.04	12.40
cb " " "	6.06	12.38
S " " "	6.05	12.39
S+25' " " "	6.14	12.30
+50' " " "	6.20	12.24
+75' " " "	6.25	12.19
+100' " " "	6.29	12.15
T.P. 5.71 18.10	6.05	12.39

Cont. on P-74

5/25/29  
 Flood  
 Prev. by  
 Calverton  
 Osborn

Levels for Sewer Connection Health Dept.  
 3138 Main St.

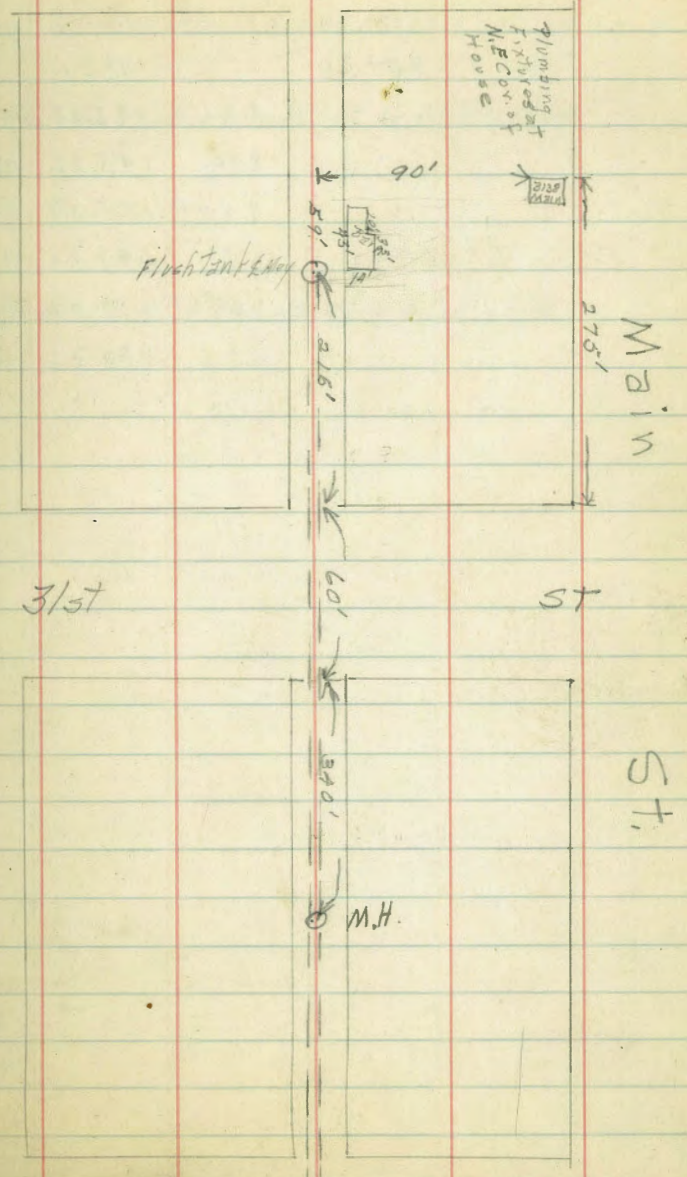
B.M. N.W. B.P. 31st & Main Sts.

	9.64	54.69	15.05	
Rim of M.H. 340' W. of W.L. 31st St.	2.67		52.02	
Flow Line " " " " " "	11.57		43.12	
& Alley W.L. 31st St.	6.86		47.83	
& Alley E.L. 31st St.	6.81		47.82	
Rim of Flush Tank 216' E of E.L. 31st St.	3.20		51.49	
Top of Flush Pipe in Flush Tank	6.12		48.57	
Water Level of Flush Pipe = Flowline Sewer	8.00		46.69	✓
Top of 6' sewer pipe 210' E of E.L. 31st	7.51		47.18	✓
Ground & Alley 259' E of E.L. 31st	6.8		47.8	= E Line of Alley
" " " 275' E of E.L. 31st	7.50		47.19	= E.L. House
T.P.	4.40	54.05	5.04	19.65
Ground at N.E. Cor House 90' S of & Alley		275' E of E.L. 31st	5.80	48.25
Top of pipe outlet from house 2' iron pipe	4.61		19.11	✓
Flow line of 1' iron pipe outlet from house	2.00		52.05	✓
Floor level of house		1.20	52.85	✓
T.P.	5.26	50.09	9.22	44.83
N.W. B.P. 31st & Main		5.09	45.05	✓

46.50  
 44.22

Boston Ave.

32nd ST 69



See Book 198-10  
 2/21/29

Elevations of Sewer in Florida St near Myrtle

Hayler  
McCarthy  
5-28-29.

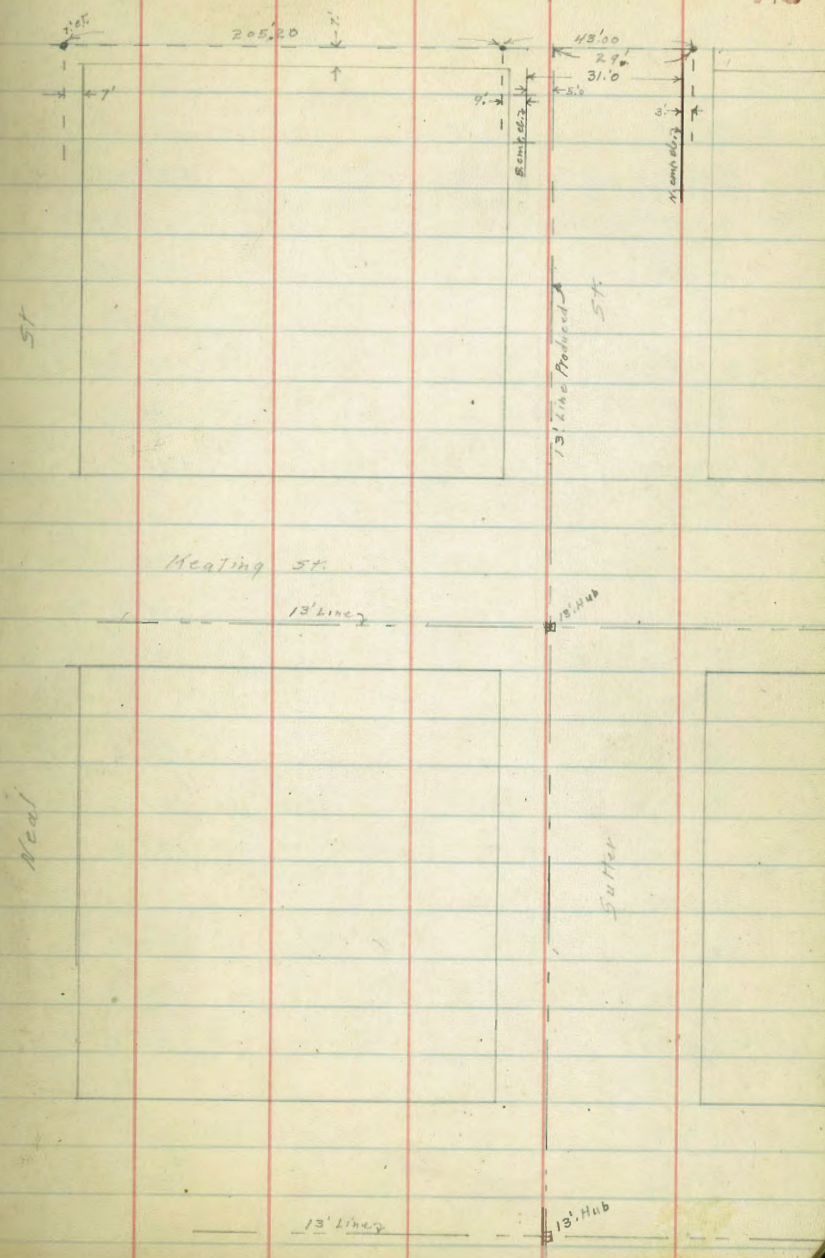
70

			B.M.	
6.29	204.30	198.01	vit.	Brass Plug SW Cor Florida and Myrtle clay
9.07	195.23			Top of 12" Pipe 85' S. of Manhole at $\frac{1}{2}$ of Myrtle
8.94	195.36			Top of Bell 12" Pipe
9.00	195.30			Flow Line of M.H. $\frac{1}{2}$ Myrtle
6.47	197.83			Top of 12" Pipe
6.28	198.02			Top of Bell 12" Pipe 85' N of Manhole at $\frac{1}{2}$ of Myrtle
5.85	198.45			On Rim of Manhole



Pringle St.

72



Alloy Block 3 Treasure Hill  
 Cross Section From CSH to Broadway  
 Between Edgmont + 32nd St

201.28

123.22  
 515.00  
 No. 111  
 No. 112  
 191.65

BM	169	201.28	19959	NE BP CIVIL ENGINEER	13.5E = N End Dr Garage Concrete Floor	9.13	191.65
		52.00			12.5E - S End Dr Garage	9.17	191.61
12.5E - End old Cb	4 1/2 ft from 1/2 in.	489	196.39		12.5E	9.9	191.4
7.5E - End New Cb		500	196.28		12.5E	9.5	191.8
Gutter on Pavement		556	195.78		12.5E	8.9	192.4
		7.15	195.13				
7.5E - Gutter		646	194.86		12.5E	10.4	190.9
Top Cb		637	194.91		8.11	11.0	190.3
12.5E		65	194.8			11.0	190.3
		20.5 ft of 5/2 CSH			12.5E - Floor	7.8	193.5
13.5E of 1		52	196.1		2.17	191.99	12.96
		47	196.6		2.03		188.36
12.5E of 2		42	197.1		12.5E - N End Dr Drive Concrete	4.69	187.30
	15.5					3.7	188.3
12.2E - Garage Dr + Floor		49	196.4		8.11	3.1	188.6
		56	195.7		12.5E	2.8	189.2
12.5E		63	195.0				
	9.5				12.5E	4.8	188.2
12.5E		86	192.7		8.11	4.1	187.6
		81	193.2			4.5	187.5
11.6E - Shed return		72	194.0		12.5E - S End Dr Drive	4.77	187.22
	10.9						
12.5E		84	192.9		12.5E - Top of 1/2" brick	5.88	186.11
		90	192.3		Ground	6.5	185.5
12.5E		94	191.9			6.3	185.7

Plotted Nov. 25-1929

191.99

8N	62	185.8
12.5N	65	186.5
27.5S		
12.5N	7.0	185.0
8N	72	184.8
8	73	184.8
12.5E - Mid Gypsum Hedge	75	184.2
30.8S - N.L. Broadway		
12.5E - Gypsum Hedge	81	183.4
8	83	183.7
8N	85	184.0
12.5N	78	184.2
34.2S - Broadway		
12.5E	98	182.2
8	101	181.9
12.5E - S End Gypsum Hedge	104	180.6

## C-57. Cross Sections.

Cont. From P-68

18.10

E. L. Kettner + 2146

S 7+4' on Pav.	6.34	11.76
8 " "	6.36	11.74
N 4 " "	6.32	11.78
N cb " "	6.30	11.80 ✓
N " "	6.27	11.83 ✓

18.10

74

N + 25' on Pav.	6.24	11.86
+ 50 " "	6.20	11.90
+ 75 " "	6.16	11.94
+ 100 " "	6.09	12.01
E. L. Kettner + 23.89		
N - 100' on Pav.	6.08	12.02
- 75 " "	6.16	11.94
- 50 " "	6.17	11.93
- 25 " "	6.27	11.83
N " "	6.26	11.84 ✓
cb " "	6.31	11.79 ✓
8 " "	6.32	11.78
8 " "	6.37	11.73
7 " "	6.36	11.74
7 " top cb.	5.70	12.40
S cb " " "	5.72	12.38
" " " Pav.	6.34	11.76
S " "	6.40	11.70
" " top cb.	5.73	12.37
S + 25' on top cb.	5.77	12.33
+ 25 " Pav.	6.41	11.69
+ 50 " "	6.43	11.67
+ 50 " cb.	5.83	12.27
+ 75 " "	5.88	12.22
+ 75 " Pav.	6.50	11.60
+ 100 " "	6.53	11.57

Cont. on P-32





Cross Section C-st.  
See sketch Page 75

20.96

75

BM.	4.06	20.96	16.30	WE. B.P. C-st. India st.
	0+00	63' = E curbline India st.		
N-100'	on Pav.	4.37	16.59	
N-80'	" "	4.41	16.55	
N-60'	" "	4.36	16.60	
N-20'	" "	4.47	16.49	
N	" "	4.47	16.49	✓
cb.	" "	4.58	16.38	✓
$\frac{1}{4}$	" "	4.43	16.53	
$\frac{1}{2}$	" "	4.20	16.66	✓
$\frac{3}{4}$	" "	4.32	16.64	
cb.	" "	4.39	16.57	✓
S	" "	4.64	16.32	✓
+20'	" "	4.86	16.10	
+40'	" "	5.04	15.92	
+60'	" "	5.32	15.64	
+80'	" "	5.48	15.48	
+100'	" "	5.73	15.23	
	0+00	50.25' = E of India		
S-100'	on Pav.	5.32	15.64	
-80'	" "	5.11	15.85	
-60'	" "	4.94	16.02	
-40'	" "	4.73	16.23	
-20'	" "	4.55	16.41	
S	" "	4.39	16.57	✓
S cb	" "	4.47	16.49	✓

S $\frac{1}{4}$	on Pav.	4.48	16.48	
$\frac{1}{2}$	" "	4.50	16.46	✓
N $\frac{1}{2}$	" "	4.65	16.31	
N cb.	" "	4.68	16.28	✓
N	" "	4.52	16.44	✓
N+20'	" "	4.18	16.78	
+40'	" "	4.17	16.79	
+60'	" "	4.21	16.75	
+80'	" "	4.16	16.80	
+100'	" "	4.09	16.87	
	0+00	37.5' = E India		
N-100'	on Pav.	4.18	16.78	
-80'	" "	4.22	16.74	
-60'	" "	4.26	16.70	
-40'	" "	4.19	16.77	
-20'	" "	4.31	16.65	
N	" "	4.65	16.31	✓
" cb.	" "	4.79	16.17	✓
$\frac{1}{4}$	" "	4.76	16.20	
$\frac{1}{2}$	" "	4.61	16.35	✓
S $\frac{1}{4}$	" "	4.64	16.32	
S cb.	" "	4.48	16.48	✓
S on Rim Sewer	M.H.	4.35	16.61	✓
S+20'	on Pav.	4.57	16.39	
+40'	" "	4.74	16.22	
+60'	" "	4.98	15.98	

S+80' on Pav.	5.21	15.75
+100' " "	5.38	15.58
0+00 - 24.75' = N 1/4 India st.		
S-100' on Pav.	5.74	15.22
-80' " "	5.55	15.41
-60' " "	5.38	15.58
-40' " "	5.13	15.83
-20' " "	4.97	15.99
S " "	4.80	16.16 ✓
S cb. " "	4.76	16.20
1/2 " "	4.80	16.16
1/2 " "	4.82	16.14 ✓
1/2 " "	4.91	16.05
N cb. " "	5.00	15.96 ✓
N " "	4.91	16.05 ✓
+20' " "	4.72	16.24
+40' " "	4.66	16.30
+60' " "	4.76	16.20
+80' " "	4.74	16.22
+100' " "	4.71	16.25
0+00 - 12' = N cb. India.		
N-100' on Pav.	5.33	15.63
-80' " "	5.46	15.50
-60' " "	5.33	15.47
-40' " "	5.40	15.56
-20' " "	5.40	15.56

N on Pav.	5.32	15.64 ✓
cb. " "	5.22	15.74 ✓
1/2 " "	5.03	15.93
1/2 " "	5.11	15.85 ✓
1/2 " "	5.01	15.95
cb. " "	5.11	15.85
S " "	5.31	15.65 ✓
+20' on Pav.	5.55	15.41
+40' " "	5.72	15.24
+60' " "	5.85	15.01
+80' " "	6.15	14.81
100'	6.28	14.68
0+00 - 12' = N cb. Line India st.		
-100' on curb	5.89	15.07
-40' " "	5.30	15.66
-21' " "	5.16	15.80
-20' in Drive Way	5.58	15.38
S 1/2 + 2' " " "	5.01	15.95
S 1/2 + 3' on curb	4.91	16.05
N 1/2 + 12' " "	4.81	16.15
N cb. in Drive Way	5.42	15.54 ✓
N " " "	5.32	15.64 ✓
+3' on curb	4.98	15.98
+20' " "	5.02	15.94
+22' in Drive Way	5.44	15.52
+40' " " "	5.34	15.62

2096

N+41' on curb	5.00	15.96	
+100' " "	4.92	16.04	
0+00 = 1/4 mi. INDIA ST			
N	4.5	16.5	✓
cb.	4.5	16.5	✓
1/4	4.6	16.4	
1/2	4.8	16.2	✓
3/4	4.6	16.4	
cb.	4.8	16.2	✓
S	5.0	16.0	✓
0+50			
-5-5'	6.4	14.6	
S	5.6	15.4	✓
+5 at Fence	4.8	16.2	
cb.	4.1	16.9	✓
1/4	4.2	16.8	
1/2	4.2	16.8	✓
3/4	4.3	16.7	✓
cb.	4.3	16.7	✓
N	4.3	16.7	✓
3.96	20.24	4.68	16.28
0+70			
N	3.5	16.7	✓
cb.	3.4	16.8	✓
1/4	3.4	16.8	
1/2	3.4	16.8	✓

2024

1/4	3.4	16.8	
cb.	2.5	16.7	✓
+9	3.6	16.6	
S	5.7	14.8	✓
+5	5.8	14.4	
0+75			
-5	5.7	14.5	
S	5.5	14.7	✓
cb.	5.0	15.2	✓
1/4	4.8	15.4	
1/2	5.1	15.1	✓
+2.7 on Gen. Slab.			
1/4 " " "	5.00	15.24	
cb. " " "	5.03	15.21	✓
N " " "	5.06	15.18	✓
1+00			
N " con. Slab.	5.10	15.14	✓
cb. " " "	5.06	15.18	✓
1/4 " " "	5.03	15.21	
+105 " " "			
1/2	5.07	15.17	
1/4	5.1	15.1	✓
1/2	5.3	14.9	
cb.	5.7	14.5	✓
S	6.1	14.1	✓
+5	6.2	14.0	
1+15			

-9

S-S		6.3	13.9
S		6.2	14.0 ✓
cb.		6.3	13.9
$\frac{1}{4}$		6.3	13.9
$\frac{1}{2}$		6.3	13.9 ✓
$\frac{3}{4}$		6.3	13.9
cb.		6.3	13.9 ✓
N		6.2	14.0 ✓
	1+25		
N		6.6	13.6 ✓
cb.		6.6	13.6 ✓
$\frac{1}{4}$		6.5	13.7
$\frac{1}{2}$		6.4	13.8 ✓
$\frac{3}{4}$		6.4	13.8
cb.		6.3	13.9
South		6.1	14.1
+5		6.3	13.9
	1+50		
S		7.1	13.1
cb.		7.1	13.1
$\frac{1}{4}$		7.2	13.0
$\frac{1}{2}$		7.2	13.0 ✓
$\frac{3}{4}$		7.0	13.0
cb.		7.0	13.0
N		7.0	13.0

Cont. on Page 52

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1% to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body

IMPROVED TABLES  
AND  
INFORMATION

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given L may be found by dividing tangent (or external) opposite L by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.



TABLE II—Continued  
TRIGONOMETRIC FORMULAE (continued)

In any triangle:

Given a, b, C; to find c, B, A.

Use Law of Tangents.

Given A, B, c; to find a, b, C.

Use Law of Sines.

Given a, b, c; to find A, B, C.

$$\text{Let } \frac{a+b+c}{2} = s, \sqrt{\frac{(s-a)(s-b)(s-c)}{s}} = r$$

$$\cos \frac{1}{2} A = \sqrt{\frac{s(s-a)}{bc}}$$

$$\tan \frac{1}{2} A = \frac{r}{s-a}$$

$$\tan \frac{1}{2} B = \frac{r}{s-b}$$

$$\tan \frac{1}{2} C = \frac{r}{s-c}$$

Area of a triangle:

$$\text{Area} = \frac{1}{2} ab \sin C$$

$$\text{Area} = \sqrt{s(s-a)(s-b)(s-c)}$$

PRISMOIDAL FORMULA.

$$\text{Vol.} = \frac{h}{6} (B+b+4M)$$

h = altitude; b, B = bases; M = midsection

TABLE III  
INCHES AND FRACTIONS OF AN INCH IN DECIMALS OF A FOOT

	0	1	2	3	4	5	6	7	8	9	10	11	
$\frac{1}{16}$	.0052	.0885	.1719	.2552	.3385	.4219	.5052	.5885	.6719	.7552	.8385	.9219	$\frac{1}{16}$
$\frac{1}{8}$	.0104	.0938	.1771	.2604	.3438	.4271	.5104	.5938	.6771	.7604	.8438	.9271	$\frac{1}{8}$
$\frac{3}{16}$	.0156	.0990	.1823	.2656	.3490	.4323	.5156	.5990	.6823	.7656	.8490	.9323	$\frac{3}{16}$
$\frac{1}{4}$	.0208	.1042	.1875	.2708	.3542	.4375	.5208	.6042	.6875	.7708	.8542	.9375	$\frac{1}{4}$
$\frac{5}{16}$	.0260	.1094	.1927	.2760	.3594	.4427	.5260	.6094	.6927	.7760	.8594	.9427	$\frac{5}{16}$
$\frac{3}{8}$	.0313	.1146	.1979	.2813	.3646	.4479	.5313	.6146	.6979	.7813	.8646	.9479	$\frac{3}{8}$
$\frac{7}{16}$	.0365	.1198	.2031	.2865	.3698	.4531	.5365	.6198	.7031	.7865	.8698	.9531	$\frac{7}{16}$
$\frac{1}{2}$	.0417	.1250	.2083	.2917	.3750	.4583	.5417	.6250	.7083	.7917	.8750	.9583	$\frac{1}{2}$
$\frac{9}{16}$	.0469	.1302	.2135	.2969	.3803	.4635	.5469	.6302	.7135	.7969	.8802	.9635	$\frac{9}{16}$
$\frac{5}{8}$	.0521	.1354	.2188	.3021	.3854	.4688	.5521	.6354	.7188	.8021	.8854	.9688	$\frac{5}{8}$
$\frac{11}{16}$	.0573	.1406	.2240	.3073	.3906	.4740	.5573	.6406	.7240	.8073	.8906	.9740	$\frac{11}{16}$
$\frac{3}{4}$	.0625	.1458	.2292	.3125	.3958	.4792	.5625	.6458	.7292	.8125	.8958	.9792	$\frac{3}{4}$
$\frac{13}{16}$	.0677	.1510	.2344	.3177	.4010	.4844	.5677	.6510	.7344	.8177	.9010	.9844	$\frac{13}{16}$
$\frac{7}{8}$	.0729	.1563	.2396	.3229	.4063	.4896	.5729	.6563	.7396	.8229	.9063	.9896	$\frac{7}{8}$
$\frac{15}{16}$	.0781	.1615	.2448	.3281	.4115	.4948	.5781	.6615	.7448	.8281	.9115	.9948	$\frac{15}{16}$
1	.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167	1.0000	1
	0	1	2	3	4	5	6	7	8	9	10	11	

TABLE IV  
USEFUL RELATIONS

Lineal feet	×.00019	= miles
Lineal yards	×.0006	= miles
Square inches	×.007	= square feet
Square feet	×.111	= square yards
Square yards	×.0002067	= acres
Acres	×4840	= square yards
Cubic inches	×.00058	= cubic feet
Cubic feet	×.03704	= cubic yards
Links	×.22	= yards
Links	×.66	= feet
Feet	×1.5	= links

360° = 21600' = 1296000"  
Radius = arc of 57.2957790°  
Arc of 1° (radius = 1) = .017453292  
Arc of 1' (radius = 1) = .000290888  
Arc of 1" (radius = 1) = .000004848

$\pi = 3.141592654$	$\sqrt{\frac{1}{4}} = 0.564190$
$\frac{\pi}{4} = 0.785398163$	$\sqrt{\frac{6}{\pi}} = 1.240700982$
$\frac{\pi}{6} = 0.523598776$	$\pi^2 = 9.869604401$
$\sqrt{\frac{4}{\pi}} = 1.128379167$	$\frac{1}{\pi^2} = 0.101321184$
$\frac{\pi}{6} = 0.523598776$	$\sqrt{\pi} = 1.772453851$
$\frac{4\pi}{3} = 4.188790205$	$\frac{1}{\pi} = 0.3183099$

Curvature of Earth's surface = about 0.7 feet in 1 mile  
Curvature in feet = 0.667 (Dist. in miles)<sup>2</sup>  
Difference between arc and chord length, 0.05 feet in 11½ miles

$$\text{Probable error of a single observation} = 0.6754 \sqrt{\frac{Mv^2}{n-1}}$$

Error in chaining of 0.01 feet in 100 feet:

Due to—

1. Length of tape error of 0.01 feet
2. Alignment. One end 1.4 feet out of line
3. Sag of tape at centre of 0.61 feet.
4. Temperature difference of 15°
5. Difference of pull of 15 lbs.

STADIA REDUCTION FORMULÆ.

$$\text{Horizontal Distance} = R - R \sin^2 a + C \cos a$$

$$\text{Vertical Distance} = R \frac{1}{2} \sin 2a + C \sin a$$

$$R = \text{Reading} \times \frac{\text{distance from Object glass to cross hairs}}{\text{distance between cross hairs}}$$

C = distance from Object glass to cross hairs + distance from Object glass to center of instrument.

a = angle of elevation for mid Reading

27.73

B.P. in cb by Archlight Pole  
East end of road  
Wilhoys

ENGINEERING DEPARTMENT,  
CITY OF SAN DIEGO,  
CALIFORNIA.

70  
3 | 270 12' 30  
255  
3750  
1225  
2475  
1275  
1200  
37  
2176  
16.04

18VU  
1810  
4

1810 1844  
487 485 567  
1323 1325 1243  
5.21 5.19 6.01

461  
775 +18

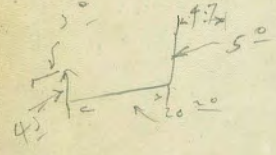
196.60

75

7.51

62  
63.00  
12.75  
50.25  
32.50  
22.75 = 14 1/4  
12

9.0 Sec  
70.25



225.5  
12.75  
12  
24.75  
12.75  
37.50  
12.75  
25.5  
12.5  
12.75  
57.00

122.77  
70.26  
52.51

63  
12  
2080  
238.0  
215.6  
232

6 + 0.05 = 850

514  
7.1

125  
125  
125  
37.5  
25

51  
75  
51  
24  
12.00  
12.75  
25

12.00  
24.75  
12.75  
37.50

39.31  
24.75  
64.06