

1308

EAST

LEVEL BOOK

No. 380 F

The index page 78 of page 84.

T-210,18000

ENGINEERING DEPARTMENT,
CITY OF SAN DIEGO,
CALIFORNIA.

MICROFILMED

DEC 2 1964

962
1622
173-23-20
173-23-20
173-23-20
173-23-20

087266
P234907
985
0908057

45
47-32-45

1077-10
9280
1167-10

2+5
31
3176

360-10
43-10
154-23-20
150-23-20
155-36-40
212-48-20

0847C
500
428000

17-26-20

1308

ENGINEERING DEPARTMENT
CITY OF SAN DIEGO,
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- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
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ENGINEERING and DRAFTING SUPPLIES
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Alinement Pershing Drive from 18 th	1
X. sec. Pershing Drive cont. Book 1306	26
" " Myrtle Ave. Florida to Alabama	42
" " " " " " Georgia	47
" " Landis 42 nd Fairmount	56
X-Section M ^o Clinch & El. Cajon to Monroe	65-71
Curbs on Mission Ave North of Madison	72-78
E & W Road Balboa Park Int. with Pershing Dr	79
" " " " " " " Park Blvd	79

72-78 18th Ave 78 6/21/23 M.H.

Pershing Drive

911517 FC

$\Delta = 29^{\circ} 41'$

$R = 500$

$T = 13757$

$L = 75918$

$D = 11^{\circ} 29'$

911517 FC

615599 PC

610 P.O.T

410 P.O.T

216064 FC

$\Delta = 71^{\circ} 40'$

$R = 200$

$T = 15254$

$L = 26064$

$D = 28^{\circ} 57'$

070 PCRT

1-7-29
Surrey
Kananis
Rupling

01

615599 PC

South Line of Belton Park

216064 FC

21931 FC

FC
18" ST

714
18" ST

Mon

UX

7

27+3648 FC

$A = 8^{\circ}38'$

$R = 500'$

$T = 37.74$

$L = 75.34$

$D = 11^{\circ}29'$

26+6114 P.C.P.

23+2121 FC

$A = 39^{\circ}50'$

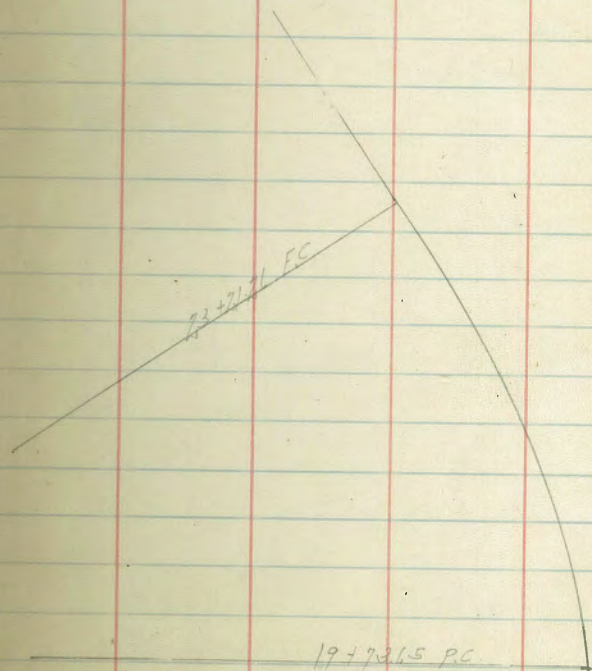
$R = 500'$

$T = 181.16$

$L = 347.61$

$D = 11^{\circ}29'$

19+7265 P.C.L.



Pershing Drive
#line

1-10-29

3

12+31.96 EC

$A = 5^{\circ} 05'$
 $R = 500'$
 $T = 22.19$
 $L = 44.36$

Changed

11+87.60 PC

6+42.06 EC ✓

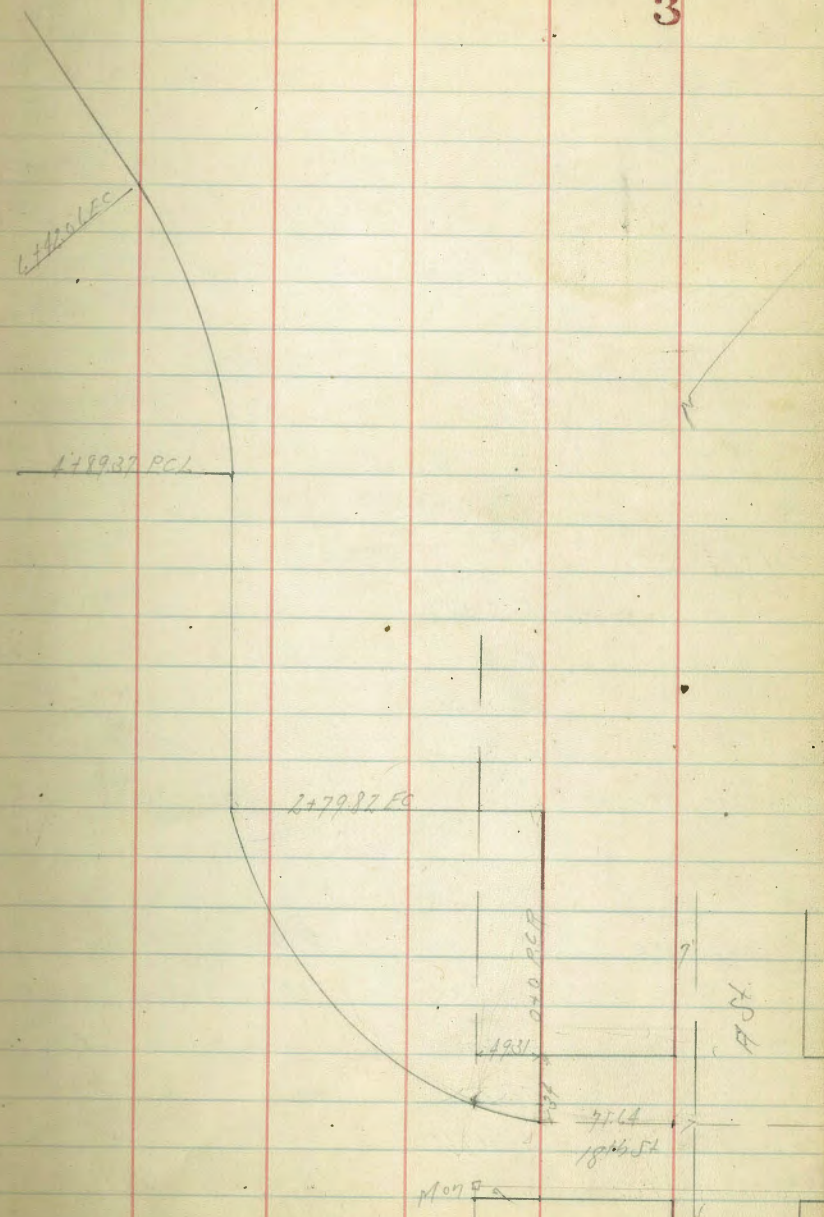
$A = 39^{\circ} 46'$
 $R = 220'$
 $T = 79.57$
 $L = 158.69$

4+89.37 PCL 4+117.61

2+79.82 EC ✓

$A = 88^{\circ} 50'$
 $R = 180.48$
 $T = 176.84$
 $L = 279.85$

0+0 PCP



Line on Pershing Drive From
6+42²⁶ E.C. (Sisson's Line)

Jan 18-28

Loudon

Isbell

Morgan

Pierce

4

24+24⁹² E.C.

Cont in Book 1306 P 20

23+85⁸⁵

23+47³¹

23+08⁷⁷

22+70²³

22+31⁶⁷

21+93¹⁵

21+54⁶¹

21+16⁰⁷

20+77⁵³

L = 385.43

T = 202.86

R = 500

$\Delta = 44^{\circ}10'$

20+38⁹⁹ B.C. C.V. L

27+65²⁴ E.C.

A = 8³⁸

R = 500

T = 37.74

L = 75.34

26+89⁹⁰ P.C.P.

11+67⁹⁰ E.C.

L = 90.80

T = 45.44

R = 1000

$\Delta = 5^{\circ}12'10''$

22+60⁴² E.C.

A = 38⁴⁰

R = 250

T = 88.12

L = 119.44

10+77¹⁰ B.C. C.V. L

20+90⁹⁸ P.C.L.

6+42⁰⁶ E.C.

(P 3)

34+82³³ E.C.

L = 397.89

T = 177.90

R = 1660

D = 13°44'

30+84⁴⁴ BC CV L

28+62²⁰ E.C.

L = 272.71

T = 136.74

R = 1500

D = 10°25'

25+89²² B.C

23+92²⁴ E.C.

L = 353.72

T = 184.62

R = 500

D = 40°32'

20+38⁰⁹ BC. CV. L

Change from 20+38⁰⁹ B.C.

Def'l. R 12°41'45"

27+25⁰⁰ L.

E.C.

L = 425.13

T = 251.19

R = 320

D = 76°15'45"

BC CV R

Alignment of Left Branch of Pershing
Drive from B.C. of Curve on top of Hill.

Feb 7-29
London.

0+00 B.C. cv Rt.

$\Delta = 38^{\circ}07'52''$
 $R = 330$
 $T = 114.05$
 $L = 219.62$

2+19⁶² P.C.C. cv Rt.

$\Delta = 38^{\circ}10'45''$
 $R = 471.16$
 $T = 163.05$
 $L = 313.96$

5+33⁵⁸ E.C.

6+33⁵⁸ B.C. cv Lt.

$\Delta = 11^{\circ}21'33''$ $T = 150.54$
 $R = 1500$ $L = 300.00$

9+33⁵⁸ P.C.C. cv Lt.

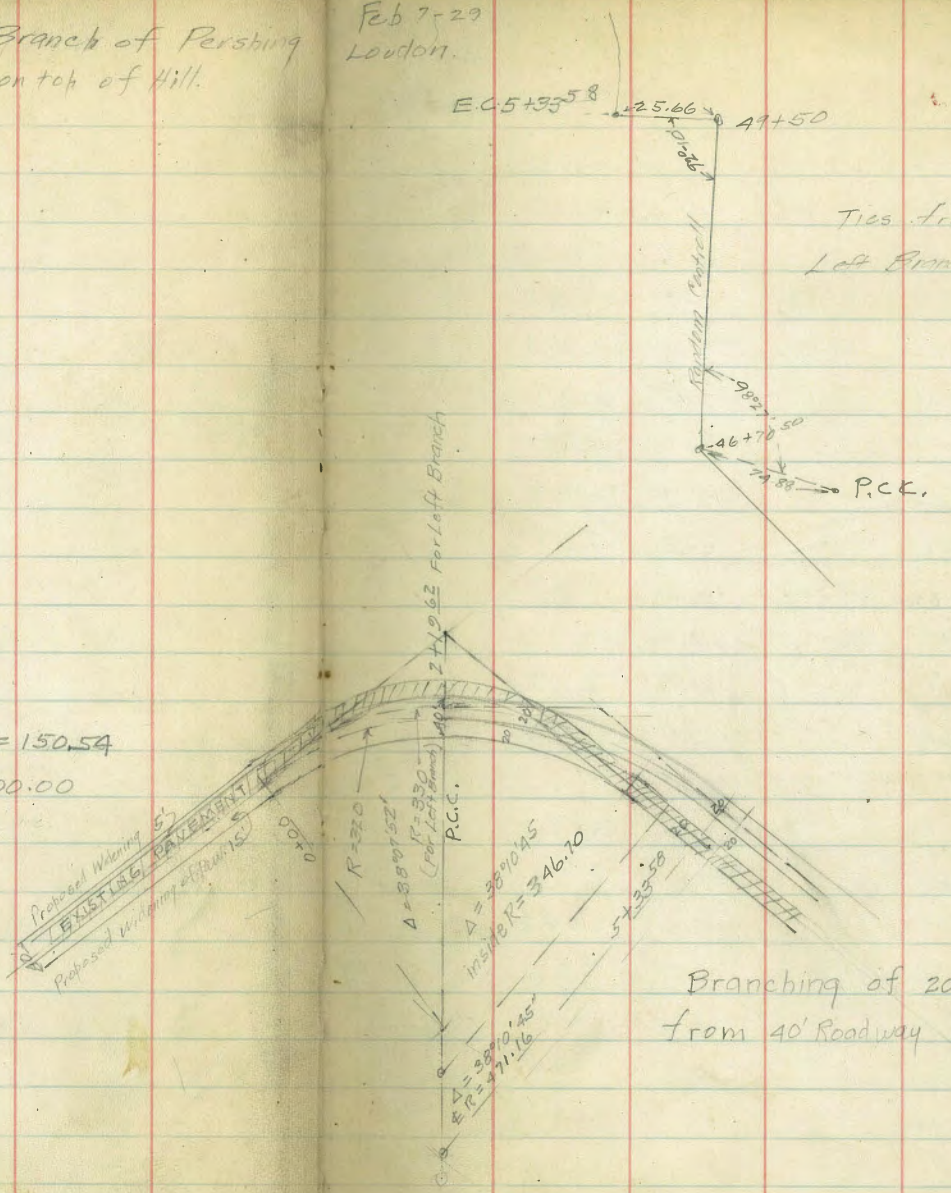
$\Delta = 20^{\circ}47'54''$
 $R = 1000$
 $T = 183.52$
 $L = 363.00$

12+96⁵⁸ E.C.

14+90⁵⁷ B.C. cv Lt.

$\Delta = 15^{\circ}53'30''$
 $R = 1500$
 $T = 209.35$
 $L = 416.04$

19+06⁶¹ E.C.



Ties from top of
Left Branch to Random

Branching of 20' Roadways
from 40' Roadway on Pershing Drive.

X Sec. Left Branch Pershing Drive
From Sta 2+19⁶² to (see P.6)

Hub. 46+70⁶⁰
on Randon

B.M. 12.13 239.47 227.34

2+19⁶² P.C.C. 15L R Pav 15.40 224.1

2L 15.6 223.9

± 12.4 227.1

10R 12.4 227.1

20R 12.4 227.1

2+51⁰²

20R 12.5 227.0

10R 12.5 227.0

1R 12.4 227.1

± 14.4 225.1

10L 14.4 225.1

11²L L Pav 14.40 225.1

2+82⁹²

20L Pav 12.36 227.1

6L R Pav 13.24 226.23

± 13.3 226.2

2R 13.8 225.7

5R 12.6 226.9

10R 12.6 226.9

20R 12.5 227.0

Feb 8-29
London.

239.47

3+13⁸²

20R 11.9 227.6

12R 12.0 227.5

10R 12.7 226.8

2⁵R R Pav 17.78 227.49

± ✓ 11.88 227.6

20L L Pav 11.08 228.4

3+45²²

20L 10.2 229.2

10L 9.9 229.6

8L L Pav 7.92 229.55

± ✓ 10.01 229.5

10R Pav 10.35 229.12

14R R Pav 10.52 229.0

20R 11.1 228.4

3+96⁶²

20R Pav 8.72 230.7

10R ✓ 8.63 230.8

4⁵R R Pav 8.68 230.79

± 8.9 230.6

10L 9.3 230.2

20L 9.9 229.6

7

A+0802 239.47

20L	7.7	231.8
10L	7.2	232.3
4	7.0	232.5
3R	6.9	232.6
6R	8.0	231.5
10R	7.7	231.8
15R L Pav.	7.31	232.2
20R	7.14	232.33

4+3942

20R	6.0	233.5
16R	6.4	233.1
10R	5.2	234.3
4	5.3	234.2
10L	5.4	234.1
20L	5.8	233.7

A+7082

20L	4.2	235.3
10L	3.9	235.6
4	3.6	235.9
10R	3.4	236.1
20R	3.3	236.2
T.P.	12.51	250.48
	1.50	237.97

5+0222 250.48

20R	13.2	237.3
10R	13.3	237.2
4	13.2	237.1
10L	13.3	237.2
20L	13.5	237.0

5+3358 E.C.

20L	12.2	238.3
10L	12.1	238.4
4	12.0	238.5
10R	11.9	238.6
20R	11.8	238.7

5+60

20R	11.1	239.4
10R	10.9	239.6
4	10.9	239.6
10L	10.9	239.6
20L	10.9	239.6

6+00

20L	9.7	240.8
10L	9.7	240.8
4	9.6	240.9
10R	9.4	241.1
20R	9.6	240.9

250.48
6+3358 B.C.

20R	8.5	242.0
10R	8.5	242.0
⊕	8.4	242.1
10L	8.4	242.1
20L	8.7	241.8

6+8358

20L	8.4	242.1
10L	8.3	242.2
⊕	7.5	243.0
10R	7.3	243.2
20R	7.2	243.3

7+04

20R	6.6	243.9
10R	7.4	243.1
⊕	7.7	242.8
10L	7.7	242.8
20L	7.9	242.6

7+3358

40L	13.8	236.7
26L	8.9	
20L	8.1	242.4
10L	7.0	243.5
⊕	7.0	243.5
10R	6.7	243.8
20R	6.3	244.2

7+8358 250.48

20R	3.1	247.4
10R	3.4	247.1
1R	3.8	246.7
⊕	4.5	246.0
10L	4.8	245.7
20L	4.6	245.9

T.P. 6.41 255.83 1.06 249.42

8+3358

20L	7.5	248.3
15L	6.7	249.1
10L	6.6	249.2
⊕	6.5	249.3
10R	6.5	249.3
20R	6.4	249.4

8+8358

20R	5.0	250.8
10R	5.0	250.8
⊕	5.0	250.8
10L	5.1	250.7
20L	5.2	250.6

255.83
 9+3358 P.C.C.
 20L 4.6 251.2
 10L 4.9 250.9
 † 5.1 250.7
 10R 5.2 250.6
 20R 5.3 250.5

9+8358
 20R 7.1 248.7
 10R 6.9 248.9
 † 6.8 249.0
 10L 6.7 249.1
 20L 6.8 249.0

10+3358
 20L 7.9 247.9
 10L 8.0 247.8
 † 7.9 247.9
 10R 7.7 247.9
 20R 8.2 247.6

10+8358
 20R 9.5 246.3
 10R 9.2 246.6
 † 9.6 246.2
 7L 9.4 246.4
 10L 10.0 245.8
 20L 10.1 245.7

11+3358 255.83 10
 20L 12.4 243.4
 15L 11.7 244.1
 10L 10.6 245.2
 † 10.9 244.9
 10R 10.0 245.8
 20R 9.6 246.2

11+8358
 20R 9.4 246.4
 10R 9.9 245.9
 † 10.4 245.4
 2L 10.7 245.1
 5L 11.4 244.4
 10L 11.6 244.2
 20L 12.1 243.7

12+3358
 20L 12.4 243.4
 10L 12.3 243.5
 8L 11.5 244.3
 † 11.3 244.5
 10R 11.1 244.7
 20R 11.0 244.8
 T.P. 4.17 247.12 12.88 242.95

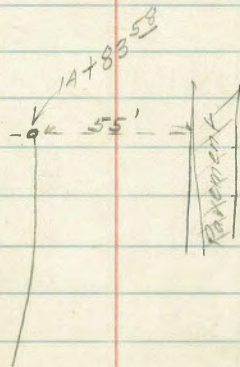
12+8358		247.12	
2.0R	4.7	242.4	
10R	4.7	242.4	
±	4.8	242.3	
10L	5.0	242.1	
12L	5.3	241.8	
20L	5.4	241.7	

13+3358			
20L	6.8	240.3	
10L	7.3	239.8	
±	6.9	240.2	
10R	6.9	240.2	
20R	7.0	240.1	

13+8358			
20R	9.7	237.4	
10R	9.2	237.9	
±	8.9	238.2	
10L	8.8	238.3	
15L	7.8	239.3	
20L	7.6	239.5	

14+3358		247.12	
20L	9.8	237.3	
10L	10.0	237.1	
±	10.3	236.8	
10R	10.3	236.8	
20R	11.1	236.0	

14+8358			
20R	11.1	236.0	
10R	10.9	236.2	
±	10.8	236.3	
10L	10.9	236.2	
20L	10.9	236.2	
BM. Hub	Random. 62+8662	3.32	243.80 (243.84)



X Sec. Left Branch Pershing
Drive from sta. 12+96⁵⁸ E.C.

T.P.	2.41	243.91	241.50
12+96 ⁵⁸ E.C.			
20L	2.4	241.5	
10L	2.1	241.8	
±	2.2	241.7	
10R	2.2	241.7	
20R	2.3	241.6	
Pav off	4.10	239.8	
13+50			
Pav off R	6.14	37.8	
20R	4.8	39.1	
10R	4.6	39.3	
±	4.5	39.4	
10L	4.5	39.4	
20L	4.0	39.9	
14+00			
20L	5.3	38.6	
14L	6.1	37.8	
10L	6.4	37.5	
±	6.2	37.7	
10R	6.8	37.1	
20R	7.2	36.7	
Pav off R	7.75	36.1	

Feb 12-29
London

14+50

Pav R off	8.47	35.4
20R	8.4	35.5
10R	7.8	36.1
±	7.3	36.6
10L	7.2	36.7
20L	7.2	36.7

14+90⁵⁷ B.C.

20L	7.6	36.3
10L	7.6	36.3
±	7.9	36.0
10R	8.0	35.9
20R	8.3	35.6
Pav off R	8.58	35.3
15+32 ¹²		
Pav off R	7.88	36.0
20R	7.8	36.1
10R	8.2	35.7
±	8.2	35.7
10L	8.3	35.6
20L	8.5	35.4
30L	8.8	35.1

12

15+73²²

35L	13.5	30.4
20L	11.6	32.3
10L	10.9	33.0
♀	9.9	34.0
10R	9.0	34.9
18R	8.5	33.4
19R	9.7	34.2
20R	9.3	34.6
Par off R	6.96	30.9
16+15 ³²		
Par off R	6.11	37.8
20R	8.1	35.8
10R	9.0	34.9
♀	10.0	33.9
10L	10.9	33.0
20L	12.2	31.7
45L	15.0	28.9
16+59 ⁹²		
25L	8.7	35.2
20L	8.4	35.4
10L	8.1	35.8
♀	7.5	36.4
10R	6.8	37.1
20R	6.4	37.5
Par off R	4.88	39.0

16+98⁵⁷

243.91

13

Par off R	3.46	40.4
20R	4.9	39.0
10R	4.9	39.0
♀	5.4	38.5
10L	5.9	38.0
20L	6.0	37.9
17+40 ¹⁷		
20L	4.2	39.7
10L	4.0	39.9
♀	3.6	40.3
10R	3.6	40.3
20R	3.3	40.6
par off R	2.25	41.6
TP 7.85	250.94	0.82 243.09
B.M.	(cor.) 250.86	7.02 243.92 243.84

17+81²²

Par off R	8.30	242.6
20R	8.7	42.2
10R	9.3	41.6
♀	9.7	41.2
10L	9.8	41.1
20L	9.9	41.0

18+23³⁷

250.86

20L	8.4	42.5
10L	8.2	42.7
⊕	8.1	42.8
10R	7.9	43.0
20R	7.3	43.6
Par opp R	7.30	43.6
18+46 ²¹		
Par opp R	6.30	44.6
20R	6.3	44.6
10R	6.5	44.4
⊕	6.6	44.3
10L	6.9	44.0
20L	7.1	43.8
19+06 ⁶¹ EC.		
20L	5.9	45.0
10L	5.6	45.3
⊕	5.5	45.4
10R	5.3	45.6
20R	4.8	46.1
Par opp R	5.53	45.3

19+50

3.7

250.86

14

Par opp R	4.99	45.8
20R	3.5	47.4
10R	3.6	47.3
⊕	3.6	47.3
10L	3.8	47.1
20L	4.0	46.9
20+00		
20L	2.8	48.1
10L	2.8	48.1
⊕	3.2	47.7
10R	2.9	48.0
20R	3.3	47.6
Par opp R	4.46	46.4
20+50		
Par opp R	3.87	47.0
20R	3.6	47.3
10R	3.0	47.9
⊕	2.9	48.0
10L	2.7	48.2
20L	2.5	48.4

21 + 00	250.86		
20L		2.4	48.5
10L		2.4	48.5
±		2.4	48.5
10R		2.3	48.6
15R		2.3	48.6
20R		3.1	47.8
Par app R		3.00	47.9
21 + 50 (?)			
20R on Paw		2.16	48.7
12R		2.4	48.5
10R		1.8	49.1
±		1.3	49.6
10L		1.9	49.0
20L		2.1	48.8

Pershing Drive
Proposed New Alignment
As to Cl post

11+67.79 = EC

$\Delta = 5^\circ 13' 10''$

$R = 1000.0$

$T = 45.44$ ✓

$L = 90.80$ ✓

10+76.99 = PCL

1076.99 ✓

641.95 ✓

435.04 ✓

6+41.95 = EC ✓

$\Delta = 39^\circ 46'$

$R = 2200$ ✓

$T = 79.57$ ✓

$L = 152.69$ ✓

4+89.26 PCL = 4+89.27 old Sta

489.26 ✓

279.82 ✓

209.44 ✓

2+79.82 EC

$\Delta = 88^\circ 50'$

$R = 180.48$ ✓

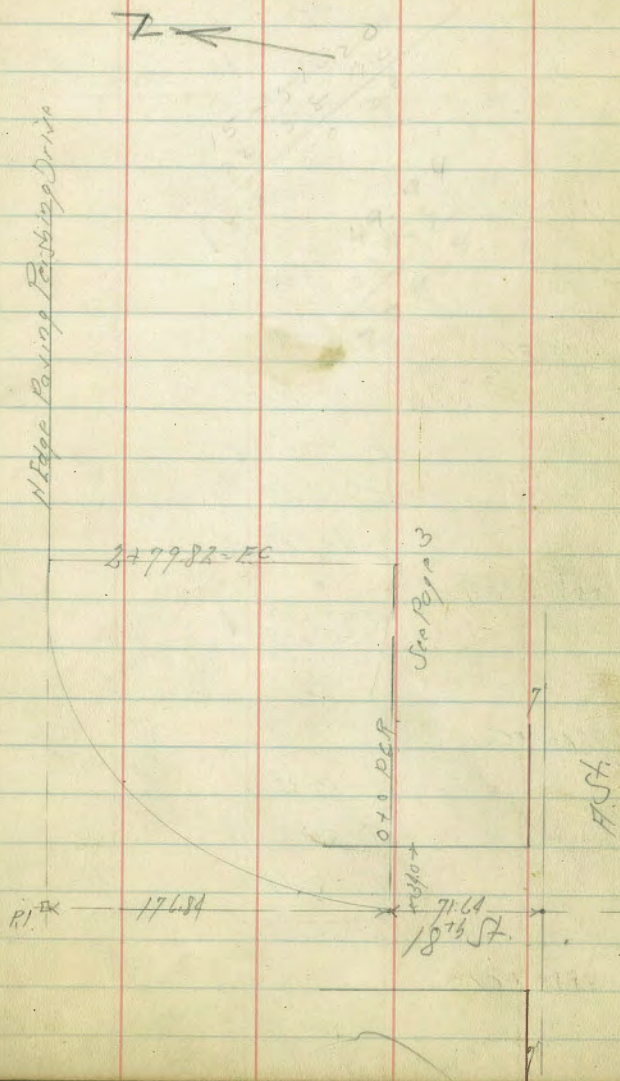
$T = 176.84$

$L = 379.82$

0+0 PCL

Additional ties
Book 1397-32-37

16
May 18-30
S. B. B. J.
Pershing
056017



Parking Drive
Proposed New Alignment.

34+46.88 F.C.

$\Delta = 12^{\circ} 20'$
 $R = 1000.0$ ✓
 $T = 108.05$ ✓
 $L = 215.26$ ✓

32+31.62 P.C.L.

3231.62
2843.27 ✓
388.33

28+43.29 F.C.

$\Delta = 9^{\circ} 04' 15''$
 $R = 1500.0$ ✓
 $T = 118.99$ 118.61
 $L = 237.47$ ✓

16+05.82 P.C.R.

2605.82
2392.60 ✓
213.22

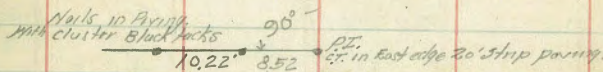
23+92.60 F.C.

$\Delta = 40^{\circ} 32'$
 $R = 500.0$ ✓
 $T = 184.62$ ✓
 $L = 353.72$ ✓

20+38.88 P.C.L.

2038.88 ✓
1167.79
871.09

F.C. • CT 117 Paving. is 50' start of East edge
Exit 20' paving.



B.C. • CT 117 Paving

F.C. • CT 117 Paving

P.I. • CT 117 Paving
11.7' End of East edge 20' Paving

Gone

Passing Drive
Proposed New Alignment

5-14-30
18

67+33.02 FC.

A = 26° 57' 30"

R = 1500.0 ✓

1.1459

T = 359.57 ✓

L = 705.77 ✓

60+37.25 P.C.L.

60 27.25

5751.25 ✓

276.00 ✓

57+51.25 FC.

A = 31° 49'

R = 1000.0 ✓

1.7188

T = 283.60 ✓

L = 562.69 ✓

51+98.56 P.C.L.

51 98.56

4822.46 ✓

376.10 ✓

48+22.46 FC.

A = 73° 14' 20"

R = 365.0 ✓

2.7092

T = 271.26 ✓

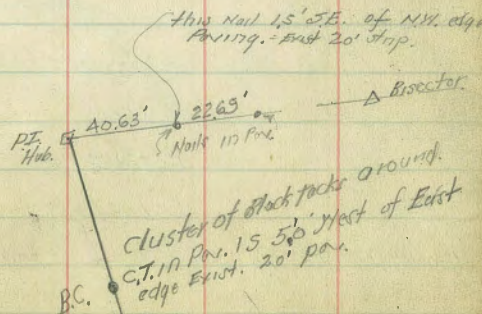
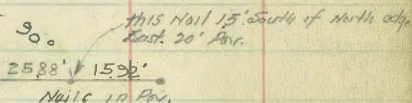
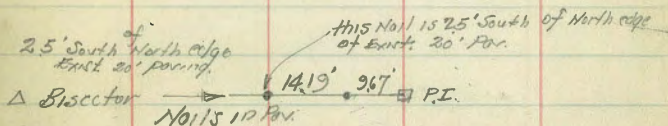
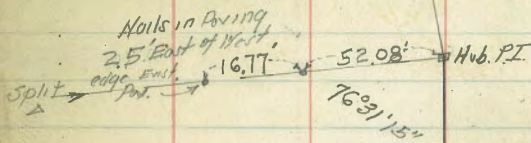
L = 466.56 ✓

43+55.90 P.C.P.

43 55.90

3446.88 ✓

909.02 ✓



Pershing Drive
Proposed New Alignment

HATCH
10-20-71

S.R. 71 GALAPAGA • F.D. P.V.

SEE BUELINE FOR
PERSHING DR. AND
SACARAUDA DR. TIES.

86+34.19 F.C.

$\Delta = 11^{\circ} 18'$
 $R = 391.87$
 $T = 159.52 \checkmark$
 $L = 303.0 \checkmark$

83+31.19 P.C.L.

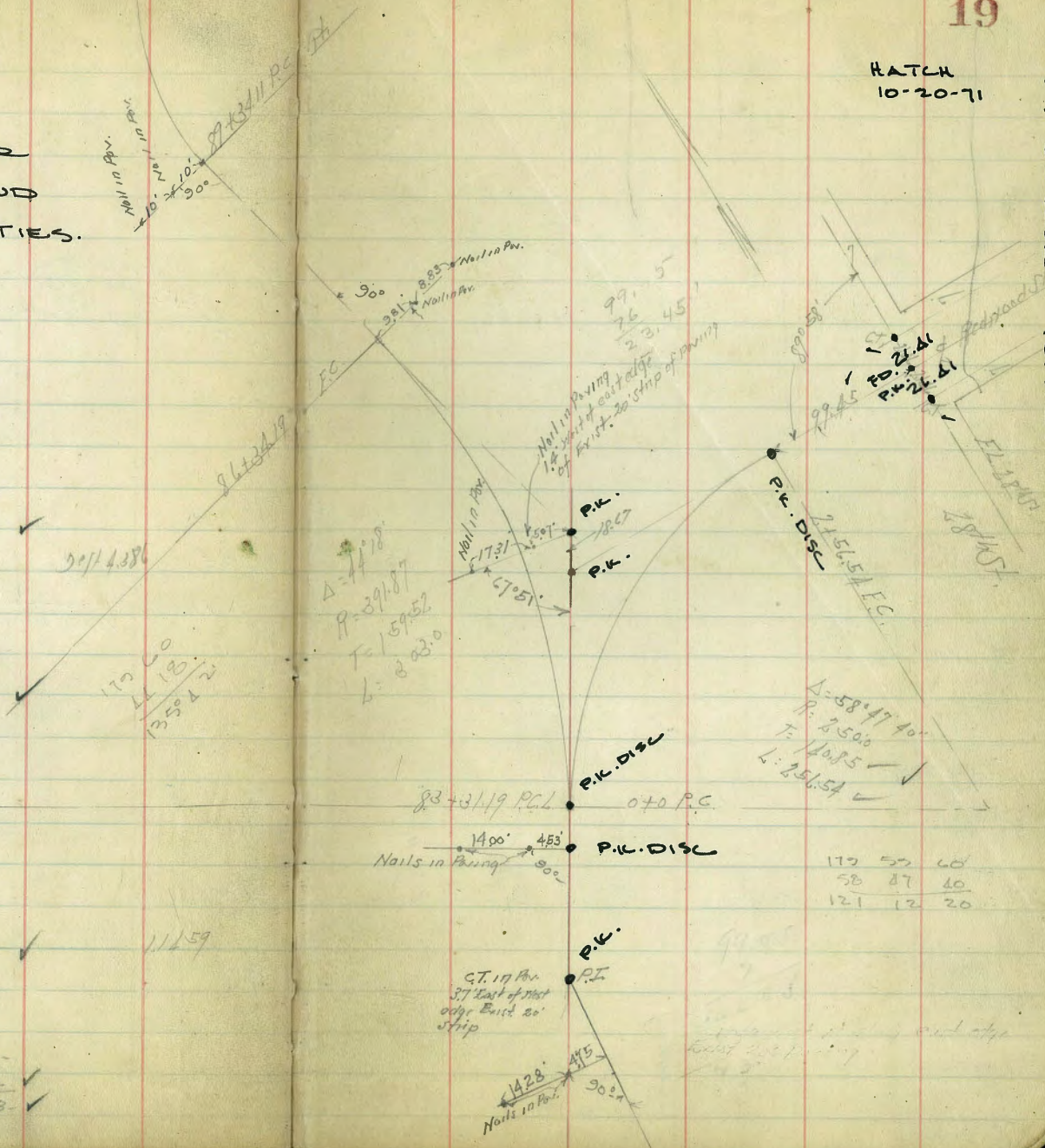
8331.19
7535.05
796.14

75+35.05 F.C.

$\Delta = 16^{\circ} 57' 26''$
 $R = 1500.0$
 $T = 223.58 \checkmark$
 $L = 443.90 \checkmark$

70+91.15 P.C.P.

7091.15
6733.02
358.13



Pershing Drive
Proposed New Alignment

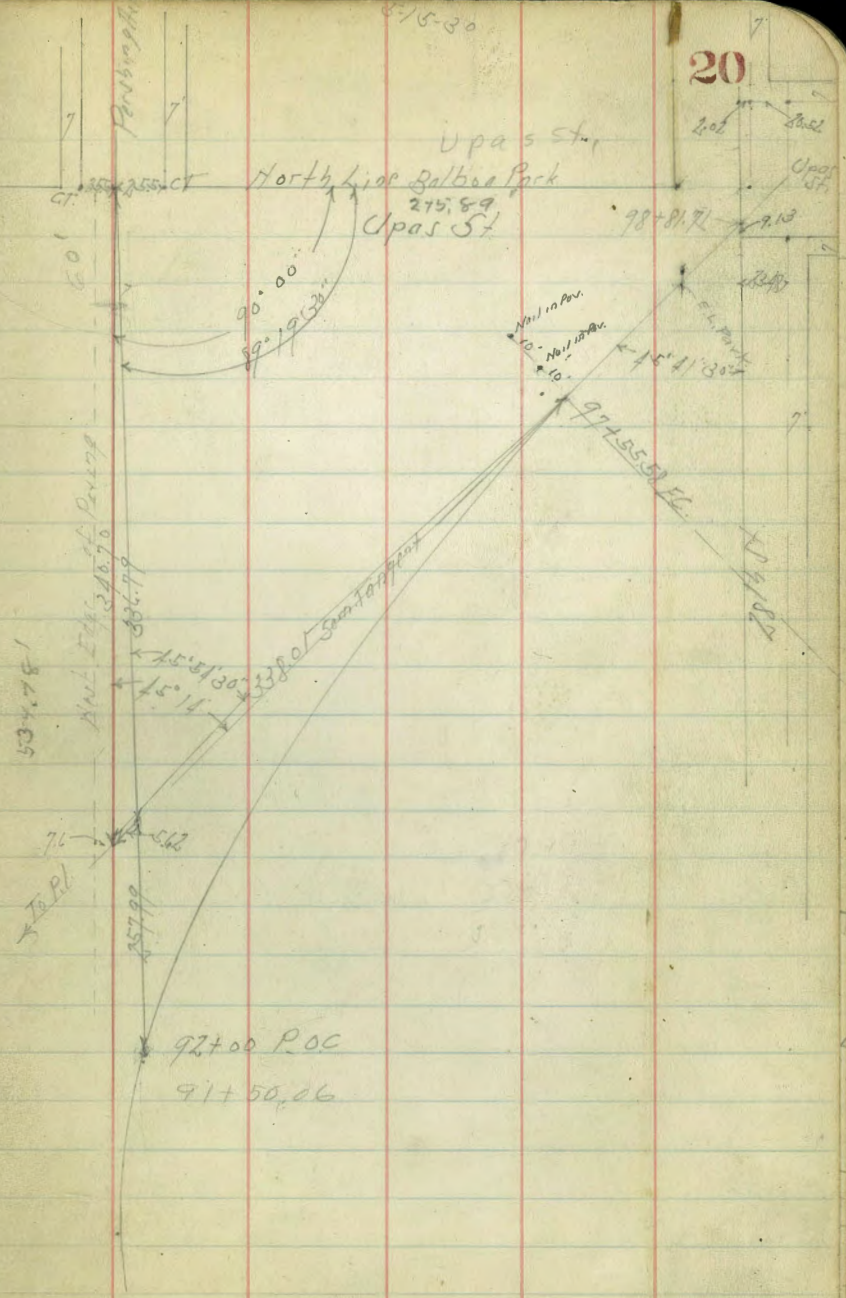
9881.71
9755.58
126.13

9715558 EG

$\Delta = 58^{\circ} 50'$
R = 800.0
T = 156.08 ✓
L = 821.47 ✓

1891311 P.C.P.

8934.11
8634.19 ✓
299.92



92700 P.O.C
91+50.06

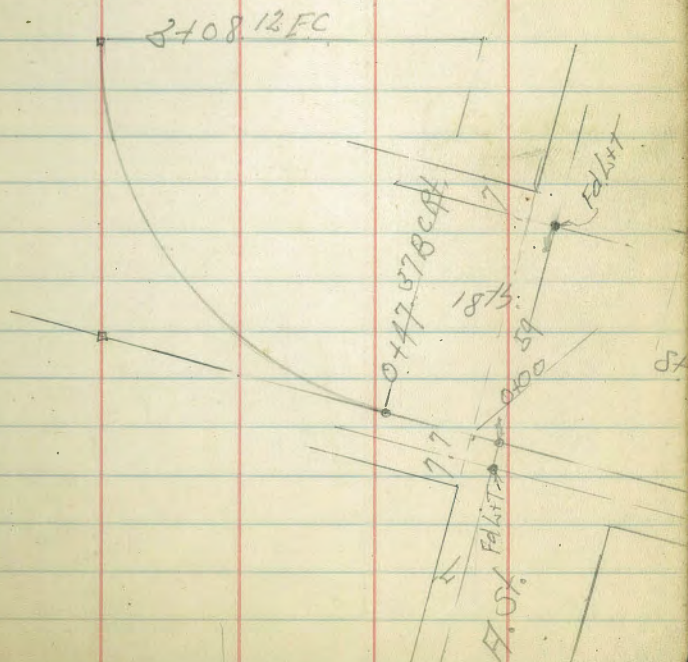
Parshing Drive Proposed Alignment
18th + H St North East.

3+08.12 FC	37° 21'	
3+0	36° 11.20	
+50	29° 01.48'	A 74° 42' R 20.0 T 152.63
2+0	21° 51.76'	L 260.75 D. 8.5944
+50	14° 42.04'	
1+0	7° 32.32'	
0+47.37 B.C.R.T.	0° 00'	

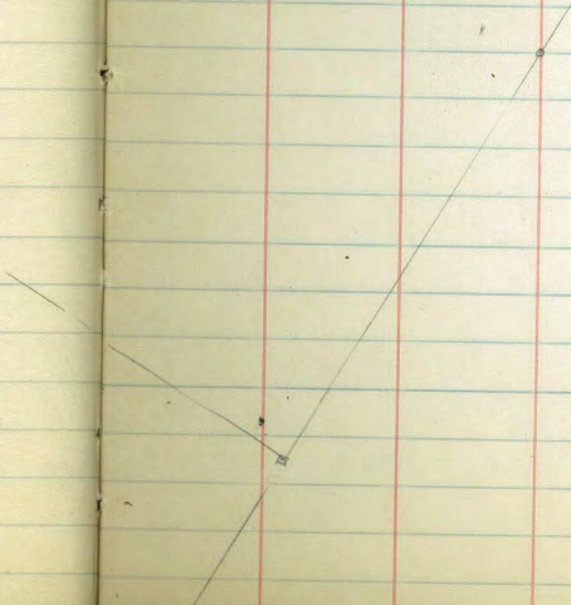
Jan. 12-50
F. Sisson
D. Smith
R. C. Chavez
H.O. 20006

21

N^o 5000 Sec 1832-23



BC Lt.



BPNE
1812B

XSec Pershing Drive

26

	BM	12.67	80.76		68.07
1	TP	12.42	93.10	0.08	80.68
	0+00 BC. L R				
	20R	topcb		4.40	88.70
	20R	gut		4.99	88.11
	±			4.46	88.62
	32L	gut.		5.20	87.90
	32L	topcb		4.57	88.53
	0+33 ² = End of cb on R & L				
	32L	topcb		2.59	90.51
	32L	gut		3.20	89.90
	16 ^E L	L Pav		2.82	90.28
	±			2.70	90.20
	16 ^R R	gut		3.54	89.56
	16 ^E R	topcb		2.95	90.15
	0+46 ⁶⁹ ①				
	20R	drive		2.82	90.28
	5 ^E R	R Pav		2.70	90.40
	4 ^E L	± Pav		2.50	90.60
	14 ^E L	L Pav		2.39	90.71
	15L			2.5	90.6
	17L			2.2	90.9
	18L			2.2	90.9
	25L			2.6	90.5
	30L			0.8	92.3
	TP	6.85	99.86	0.09	93.01

0+93²⁷ ② 99.86

40L		6.4	93.5
15L		7.4	92.5
13 ^{SL}	L Pav	7.77	92.09
3 ^{SL}	± Pav	8.02	91.84
8 ^R	R Pav	8.27	91.59
14R		8.4	91.5
18R		8.1	91.8
22R		8.4	91.5
30R		9.8	90.1
40R		11.2	88.7

1+39^{2L} ③

40R		10.3	89.6
32R		9.0	90.9
25R		7.1	92.8
20R		7.2	92.7
12R	R Pav	7.35	92.51
±		6.88	92.98
10 ^{SL}	L Pav	6.54	93.32
12L		6.4	93.5
19L		6.1	93.8
22L		5.4	94.5
40L		4.4	95.5

99.86

1+86⁵⁴ ④

40L		4.5	95.4
25L		4.8	95.1
7 ^L	L Pav	6.00	93.86
±		6.25	93.61
3R	± Pav	6.32	93.54
15 ^{SR}	R Pav	6.7	93.2
17R		6.6	93.3
23R		7.0	92.9
30R		10.3	89.6
40R		11.4	88.5

2+33^{L2} ⑤

40R		10.0	89.9
32R		9.0	90.9
27R		7.2	92.7
18 ^{SR}	R Pav	6.84	93.02
8 ^{SR}	± R	6.41	93.45
±		6.15	93.71
3 ^{SL}	L Pav	6.07	93.79
4L		6.1	93.8
13L		5.3	94.6
20L		5.3	94.6
40L		5.2	94.7

27

247982 E.C. ^{99.86}

40L		8.2	91.7
12L		5.7	94.2
6L		6.2	93.7
£	L Pav	6.01	93.86
10R	£ Pav	6.16	93.70
20 ⁵ R	R Pav	6.44	93.42
25R		7.1	92.8
28R		6.4	93.5
32R		6.7	93.2
40R		8.7	91.2
3+00			
40R		8.8	91.1
27R		6.0	93.9
20R	R Pav	6.17	93.69
10R	£ Pav	5.91	93.95
£	R Pav	5.79	94.07
3L		5.7	94.2
5L		5.8	94.1
8L		5.5	94.4
10L		5.7	94.2
14L		6.6	93.3
40L		6.1	93.8

28

3+25 99.86

40L		3.5	96.4
20L		5.4	94.5
5L		5.3	94.6
£	L Pav	5.48	94.38
10R	£ Pav	5.54	94.32
20R	R Pav	5.68	94.18
27R		5.8	94.1
32R		7.1	92.8
40R		7.8	92.1
3+50			
40R		6.8	93.1
31R		6.3	93.6
27R		5.5	94.4
20 ² R	R Pav	5.25	94.61
10R	£ Pav	5.22	94.64
£	L Pav	5.24	94.62
4L		5.3	94.6
6L		5.5	94.4
11L		4.8	95.1
13L		3.7	96.2
25L		1.1	98.8
T.P.	5.86	101.05	4.67 95.19
40L			0.9 100.2

A+00		101.05	
40L		+0.6	101.7
25L		1.3	99.8
12L		3.7	97.4
10L		5.2	95.9
8L		5.3	95.8
6L		5.9	95.2
♀	L Paw	5.78	95.27
10R	♀ Paw	5.75	95.30
20R	R Paw	5.95	95.38
11R		5.7	95.4
32R		6.1	95.0
35R		5.7	95.4
40R		5.6	95.5
	4+50 - ?		
40R		4.6	96.5
30R		4.4	96.7
25R		4.8	96.3
20R	R Paw	4.87	96.18
10R	♀ Paw	5.02	96.03
♀	L Paw	5.27	95.78
3L		5.2	95.9
5L		5.5	95.6
15L		1.5	99.6
19L		0.4	100.7
40L		+0.3	101.4

A+89 ³² BC		101.05		
40L		+1.0	102.1	
20L		0.1	101.0	
15L		1.4	100.7	
10L		5.1	96.0	
7L		5.0	96.1	
6L		5.5	95.6	
3L		5.1	96.0	
♀	L Paw	5.06	95.99	
10R	♀ Paw	4.63	96.42	
20 ⁹ R	R Paw	4.20	96.85	
30R		4.7	96.4	
40R		6.0	95.1	
T.P.	4.05	100.35	4.95	96.30
	5+199L	⊙		
40R		5.0	95.4	
30R		4.3	96.1	
20R	R Paw	3.58	96.77	
10R	♀ Paw	3.99	96.36	
♀	L Paw	4.41	95.94	
4L		4.5	95.9	
7L		5.0	95.4	
8L		4.5	95.9	
10L		4.5	95.9	
15L		1.0	99.4	
20L		+1.0	101.4	
40L		+1.6	102.0	

5+50⁹⁵

100.35

40L		+3.5	103.9
14L		0.0	100.4
10L		4.4	96.0
8L		5.3	95.1
±	L Pav	4.92	95.43
10R	± Pav	4.40	95.95
20R	R Pav	4.14	96.21
21R		4.10	96.4
28R		3.9	96.5
32R		4.4	96.0
40R		4.7	95.9

5+80⁹⁹

40R		5.9	94.5
30R		4.8	95.6
20R	R Pav	4.59	95.76
10R	± Pav	4.92	95.43
±	L Pav	5.43	94.92
7L		5.3	95.1
9L		5.0	95.4
15L		1.6	98.8
35L		0.5	99.9
40L		0.0	100.4

6+11⁵³

100.35

40L		0.1	100.3
15L		2.0	98.4
9L		5.6	94.8
7L		5.9	94.5
±	L Pav	5.94	94.41
10R	± Pav	5.43	94.92
20R	R Pav	5.11	95.24
22R		5.4	95.0
38R		5.7	94.7
40R		7.5	92.9

6+42⁰⁶ E.L.

40R		6.6	93.8
30R		5.6	94.8
20R	R Pav	5.46	94.89
10R	± Pav	5.82	94.53
±	L Pav	6.33	94.02
1L		6.2	94.2
7L		6.5	93.9
13L		5.6	94.8
15L		2.6	99.8
35L		1.0	99.4
40L		0.4	100.0

30

7+00		100.35		
40L		+1.0	99.4	
15L		3.6	96.8	
11L		6.3	94.1	
5L		6.4	94.0	
4L		6.9	93.5	
⊕	L Pav	6.54	93.81	
10R	⊕ Pav	6.42	93.93	
20R		6.24	94.11	
30R		6.5	93.9	
40R		7.3	93.1	
7+50				
40R		7.5	92.9	
30R		7.0	93.4	
20R	R Pav	6.72	93.63	
10R	⊕ Pav	6.77	93.58	
⊕	L Pav	6.85	93.50	
5L		7.0	93.4	
6L		6.3	94.1	
10L		6.0	94.4	
18L		1.1	99.3	
40L		+1.0	101.4	
T.P.	10.56	103.68	7.23	93.12

8+00		103.68		
40L		2.0	101.7	
20L		4.2	99.5	
10L		10.0	93.7	
7L		10.3	93.4	
5L		10.8	92.9	
⊕	L Pav	10.54	93.14	
10R	⊕ Pav	10.48	93.20	
20R	R Pav	10.50	93.18	
27R		10.5	93.2	
40R		11.4	92.3	
8+50				
40R		15.8	88.9	
29R		10.7	93.0	
20R	R Pav	10.99	92.69	
10R	⊕ Pav	10.98	92.70	
⊕	L Pav	11.04	92.64	
6L		11.3	92.4	
7L		10.8	92.9	
11L		10.4	93.3	
16L		8.0	95.7	
18L		5.1	98.6	
40L		1.0	102.7	

		103.68	
9+00			
40L		0.3	103.4
19L		5.6	98.1
13L		10.4	93.3
7L		11.1	92.6
6L		11.7	92.0
⊕	L Pav	11.54	92.14
10R	⊕ Pav	11.40	92.28
20R	R Pav	11.46	92.22
25R		11.5	92.2
26R		11.0	92.7
27R		10.9	92.8
40R		18.3	85.4
9+50			
40R		20.4	83.3
27R		12.1	91.6
25R		12.3	91.4
20R	R Pav	12.10	91.58
10R	⊕ Pav	11.98	91.70
⊕	L Pav	11.99	91.69
5L		12.1	91.6
7L		11.7	92.0
12L		10.8	92.9
16L		8.3	95.4
40L		10.6	104.3

		103.68	
10+00			
40L		1.1	102.6
18L		7.1	96.6
17L		9.7	94.0
11L		11.6	92.1
7L		12.8	90.9
5L		12.5	91.2
⊕	L Pav	12.52	91.16
10R	⊕ Pav	12.46	91.22
20R	R Pav	12.59	91.09
26R		12.4	91.3
40R		21.9	81.8
10+50			
40R		22.6	81.1
26R		13.0	90.7
20R	R Pav	13.07	90.61
10R	⊕ Pav	12.98	90.70
⊕	L Pav	13.08	90.60
4L		13.1	90.6
6L		13.5	90.2
8L		13.0	90.7
16L		12.3	91.4
13L		6.8	96.9
40L		0.4	103.3

		103.68	
10	+77 ¹⁰ B.C.		
40L		0.3	103.4
20L		6.4	97.3
18L		12.3	91.4
7L		13.9	90.8
5L		13.5	90.2
T.P.	9.72 91.47	12.93	90.75
±	L Paw	1.29	90.18
10R	± Paw	1.21	90.26
20R	R Paw	1.33	90.14
27R		1.3	90.2
40R	← 11+22 ⁵⁰	105	81.0
11	+17 ⁵⁰ C.O.f.C.V.		
40R		9.8	81.7
30R		2.0	89.5
21 ^A R	R Paw	2.07	89.48
11 ^A R	± Paw	2.10	89.37
1 ^A R	± Paw	2.23	89.24
±		2.1	89.4
4L		2.1	89.4
5L		2.5	89.0
7L		2.8	88.7
15L		0.9	90.6
20L		76.3	97.8
40L		+13.0	104.5

		91.47	
11	+67 ⁹⁰ EC		
40L		+14.0	105.5
28L		+10.0	101.5
28L		+2.3	93.8
16L		1.3	90.2
5L		3.4	88.1
±		3.0	88.5
4R	L Paw	3.13	88.34
14R	± Paw	2.87	88.60
24R	R Paw	2.75	88.72
34R		2.7	88.8
40R		6.3	85.2
12	+00		
40R		6.7	84.8
36R		3.6	87.9
27R	R Paw	3.15	88.32
17R	± Paw	3.37	88.19
7R	L Paw	3.73	88.74
6R		3.6	87.9
±		4.0	87.5
14L		1.6	89.9
20L		+12.6	104.1
40L		+19.0	110.5

12+50		91.47	
40L		+19.3	110.8
18L		+12.8	104.3
10L		2.6	88.9
⊕		4.5	87.0
4R		4.7	86.8
8R		4.4	87.1
9 ^E R	L Pav	4.58	86.89
19 ^E R	⊕ Pav	4.11	87.36
29 ^E R	R Pav	3.92	87.55
36R		4.1	87.4
40R		5.7	85.8
13+00			
40R		9.4	82.1
35R		5.0	86.5
27 ² R	R Pav	4.75	86.72
17 ² R	⊕ Pav	4.95	86.52
7 ³ R	L Pav	5.32	86.15
⊕		5.5	86.0
10L		3.7	87.8
15L		+6.5	98.0
40L		+12.8	104.3

13+50		91.47		34
40L		+3.0	94.5	
25L		0.4	91.1	
8L		6.0	85.5	
⊕		5.8	85.7	
2.5R	L Pav	5.88	85.59	
12 ^E R	⊕ Pav	5.68	85.79	
22 ^E R	R Pav	5.60	85.87	
28R		5.5	86.0	
32R		6.5	85.0	
40R		11.8	79.7	
14+00				
40R		12.7	78.8	
35R		11.2	80.3	
30R		7.5	84.0	
26R		6.5	85.0	
18R	R Pav	6.24	85.23	
8R	⊕ Pav	6.17	85.30	
⊕		6.30	85.17	
2L	L Pav	6.32	85.15	
5L		6.1	85.4	
13L		6.6	84.9	
24L		0.0	91.5	
40L		+6.6	98.1	

91.47

14 + 50			
40L		+10.4	101.9
23L		+1.5	93.0
17L		5.6	85.9
12L		6.6	84.9
10L		6.2	85.3
7L	L Pav	6.45	85.02
±		6.36	85.11
3R	± Pav	6.34	85.13
13R	R Pav	6.37	85.10
24R		7.1	84.4
38R		13.7	77.7
40R		14.3	77.2

15 + 00

40R		11.2	80.3
25R		8.0	83.5
15R		6.5	85.0
8 ² R	R Pav	6.48	84.99
±		6.30	85.17
1 ² L	± Pav	6.30	85.17
11 ² L	L Pav	6.42	85.05
13L		6.2	85.3
20L		6.7	85.4
24L		6.1	85.4
30L		+3.4	94.9
40L		+13.0	104.5

8.4
4.8
3.89.5
6.0
5.9

35

15 + 50 91.47

40L		+8.5	100.0	
33L		+3.0	94.5	
26L		6.4	85.1	
16 ² L	L Pav	6.36	85.11	
6 ² L	± Pav	6.27	85.28	
±		6.35	85.12	
4 ² R	R Pav	6.41	85.06	
10R		6.6	84.9	
TP	5.90	90.94	6.45	85.02
21R		7.7	83.2	
36R		9.0	81.9	
40R		11.7	79.2	

16 + 00

40R		12.1	78.8
28R		11.9	79.0
20R		10.3	80.6
10R		6.4	84.5
±		5.7	85.2
1L	R Pav	5.74	85.18
11L	± Pav	5.63	85.29
21L	L Pav	5.55	85.37
28L		6.4	84.5
40L		+3.8	94.7

16+50

90.92

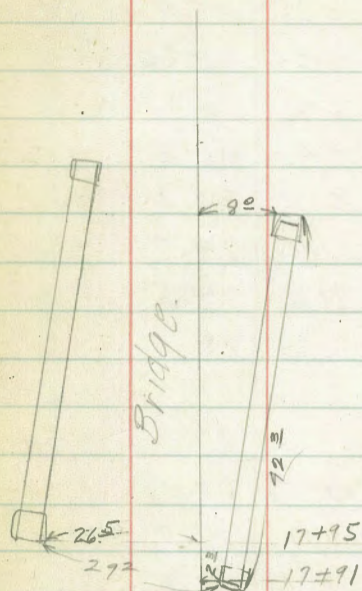
40L		7.8	83.1
35L		7.5	83.4
32L		5.9	85.0
25 ⁵ L	L Pav	5.28	85.64
15 ⁵ L	± Pav	5.44	85.48
5 ⁵ L	R Pav	5.66	85.26
±		5.7	85.2
6R		5.6	85.3
15R		9.9	81.0
25R		12.2	78.7
35R		10.8	80.1
40R		10.8	80.1
17+00			
40R		13.2	77.7
38R		12.8	78.1
25R		11.9	79.0
14R		9.8	81.1
3R		5.6	85.3
±		5.7	85.2
8L	R Pav	5.64	85.28
18L	± Pav	5.39	85.53
28L	L Pav	5.04	85.88
35L		5.8	85.1
40L		8.7	82.2

17+50

90.92

40L		6.6	84.3
35L		5.3	85.6
26 ⁶ L	L Pav	4.98	85.94
16 ⁶ L	± Pav	5.26	85.66
6 ⁹ L	R Pav	5.61	85.31
±		5.4	85.5
5R		5.3	85.6
14R		11.0	79.9
32R		11.4	79.5
40R		12.0	78.9
18+00			
40R		13.6	77.3
20R		12.5	78.4
6R		14.1	76.8
6R		4.6	86.3
±		5.1	85.8
1L	R Pav	5.22	85.70
11L	± Pav	5.00	85.92
21L	L Pav	4.92	86.00
26L		4.8	86.1
28L		6.8	84.1
40L		8.3	81.6

36



18+50	90.92			
40L		9.1	81.8	
35L		8.1	82.8	
24L		4.6	86.3	
14L	L Pav.	4.57	86.35	
4L	± Pav	4.48	86.44	
±		4.54	86.38	
6R	R Pav	4.57	86.35	
15R		4.2	86.7	
24R		8.6	82.3	
37R		8.6	82.3	
40R		9.3	81.6	
19+00				
40R		8.5	82.4	
34R		8.2	82.7	
26R		4.3	86.6	
12 ² R	R Pav	4.48	86.44	
2 ² R	± Pav	4.42	86.50	
±		4.44	86.48	
7 ³ L	L Pav	4.49	86.43	
9L		4.3	86.6	
20L		4.5	86.4	
T.P.	3.70	93.57	1.05	89.87
26L		10.5	83.1	
40L		11.0	82.6	

19750		8.57	
40L		10.2	83.4
20L		10.2	83.4
13L		6.6	87.0
2L		6.6	87.0
02L	L Paw	6.89	86.68
4		6.89	86.68
9 ⁸ R	R Paw	6.79	86.78
19 ² R	R Paw	6.80	86.77
34R		6.5	87.1
40R		10.2	83.4
20+00			
40R		6.1	87.5
26 ⁸ R	R Paw	5.65	87.92
16 ⁸ R	R Paw	5.81	87.76
6 ⁸ R	R Paw	6.13	87.44
4		6.1	87.5
6L		6.3	87.3
10L		7.8	85.8
40L		8.4	85.2

20+38⁹⁹ B.C. 93.57

40L		7.3	86.3
10L		6.7	86.9
4		5.1	88.5
11R	L Paw	5.55	88.02
21R		5.03	88.54
32R	R Paw	4.72	88.85
40R		5.2	88.4
20+77 ⁵³ ①			
40R		3.5	90.1
37 ⁰ R	R Paw	3.55	90.02
25 ⁴ R	R Paw	3.97	89.70
14R	L Paw	4.53	89.04
6R		4.4	89.2
1R		4.1	89.5
4		4.7	88.9
4L		7.0	86.6
33L		7.1	86.5
40L		6.9	86.7

21+16²² ② 93.57

40L	6.5	87.1
5L	5.9	87.7
±	3.4	90.2
3R	2.9	90.7
15 ⁸ R L Pav	2.93	90.64
27 ⁸ ± Pav	2.38	91.19
40 ⁵ R Pav	1.86	91.71

21+54^{6L} ③

T.P.	12.87	105.94	0.50	93.07
40R			11.5	94.4
39 ⁵ R R Pav			11.53	94.41
26 ⁵ R ± Pav			12.02	93.92
13 ⁵ R L Pav			12.67	93.27
4R			12.9	93.0
±			15.3	90.6
25L			17.7	88.2
40L			16.6	87.3

21+93¹⁵ ④ 105.94

40L	17.2	88.7
25L	15.8	90.1
8L	13.3	92.6
1L	10.0	95.9
±	10.1	95.8
9 ² R L Pav	9.82	96.12
22 ² R ± Pav	9.06	96.88
35 ² R R Pav	8.47	97.47
39R	8.1	97.8

22+31^{6I} ⑤

40R	6.0	99.9
27R R Pav	5.84	100.10
15R ± Pav	6.31	99.63
3R L Pav	6.89	99.05
±	6.8	99.1
7L	7.2	98.7
20L	12.5	93.4
40L	14.6	91.3

22 + 70²³ ④

40L	13.2	92.7
25L	10.3	95.6
15L	4.4	101.5
5 ² L L Paw	4.13	101.81
♀	3.94	102.00
5R ♀ Paw	3.65	102.29
16R R Paw	3.44	102.50
32R	3.4	102.5
35R	5.2	100.7
40R	2.5	103.4

23 + 08²⁷ ⑦

40R	11.5	107.4
26R	0.2	105.7
23R	3.2	102.7
18R	1.2	104.7
13R	0.9	105.0
8R R Paw	1.07	104.87
♀	1.11	104.83
2L ♀ Paw	1.11	104.83
12L L Paw	1.39	104.55
22L	2.0	103.9
40L	10.5	95.4

23 + 47³¹ ⑥

105.94

40L	5.1	100.8
T.R	12.59	118.13
29L	11.6	106.5
18 ² L L Paw	11.07	107.06
8 ² L ♀ Paw	11.05	107.08
♀	11.13	107.00
2 ³ R	11.17	106.96
6R	11.1	107.0
12R	11.4	106.7
15R	12.6	105.5
19R	9.2	108.9
27R	8.5	109.6
40R	8.2	109.9

23 + 65⁶⁵ ⑨

40R	4.4	113.7
17R	5.4	112.7
15R	8.3	109.8
♀ R Paw	8.80	109.33
10L ♀ Paw	8.67	109.46
20L L Paw	8.63	109.50
33L	9.1	109.0
36L	8.5	109.6
40L	8.4	109.7

24+24⁴² EC. 118.13

40L		6.0	112.1
38L		6.5	111.6
35L		6.3	111.8
28L		6.4	111.7
27L		6.8	111.3
25L		6.4	111.7
19 ² L	L Pav	6.09	112.04
9 ² L	± Pav	6.08	112.05
±		6.18	111.95
0 ³ R	R Pav	6.18	111.95
3R		6.1	112.0
8R		7.2	110.9
15R		7.1	111.0
19R		0.9	117.2
30R		1.0	117.1
40R		0.6	117.5
BM. Hub	10'E of Pav.	5.21	112.92

Cont in Book 1306 P21

X sec Myrtle Ave from web line
 Florida to Alabama. 60'± 10' cbs 40' Rdway.
 B.M. 12.97 210.98 198.01 ^{sw Myrtle} Florida.

Jan. 28-29
 Lorton
 1 shell
 Morgan.

210.98

42

Web Florida

60'S top cb	13.49	197.49
10'S old line of Myrtle	12.98	198.00
S.L.	13.3	197.7
cb	13.1	
1/4	12.9	
±	12.8	198.2
1/4	12.7	
cb	12.5	
N.L.	12.4	198.6
10N top cb old line Myrtle	11.94	199.04
50N top cb	10.69	199.29
(cbs 10' Radius in ^{For} 40' Rdway on Florida & 52' Rdway on Myrtle when Myrtle 80' wide)		
w 1/4 Florida		
N.L.	12.4	197.6
cb	12.5	
1/4	12.7	
±	12.8	197.2
1/4	13.0	
cb	13.2	
S.L.	13.3	196.7

Florida

S.L.	13.3	197.7
cb	13.1	197.9
1/4	12.9	198.1
± MH. top	12.48	198.50
FL.	15.63	195.35
1/4	12.4	198.6
cb	12.3	198.7
N.L.	12.2	198.8
E 1/4 Florida		
N.L.	11.9	199.1
cb	12.1	198.9
1/4	12.3	198.7
±	12.5	198.5
1/4	12.7	198.3
cb	12.9	198.1
S.L.	13.0	198.0
Ecb Florida		
60'S top cb	13.50	197.48
10'S old line top cb	13.01	197.97
S.L.	12.7	198.3'
cb	12.6	198.4
1/4	12.6	198.4
±	12.4	198.6'
1/4	12.3	198.7
cb	12.3	198.7

210,98

Feb Florida

N.L.		12.2	198.8 ✓
10 N	top cb old line	11.95	199.03
25 EN	end cb top cb	11.51	199.47
68 N	begin. of cb. top cb	10.31	200.61
E.L.	Florida = 3 + 87 ⁸⁹		
N.L.		11.8	199.2 ¹
+4	top	12.14	
+4		12.0	199.0
cb		12.2	198.8
1/4		12.2	198.8
+		12.3	198.7 ¹
1/4		12.2	189.8
cb		11.8	199.2
+6		11.7	199.3
SL		12.0	199.0 ¹
3 + 84			
SL		10.0	201.0 ¹
+3		9.8	201.2
+3 ⁵		11.4	199.6
+7		11.6	199.4
+8		11.0	200.0
cb		11.0	200.0
1/4		11.6	199.4
+3		11.7	199.3
+4		9.6	201.4

210,98

43

3 + 84

+		9.5	201.5 ¹
1/4		9.3	201.7
cb		9.1	201.9
N.L.		8.5	201.5 ¹
3 + 75			
N.L.		8.1	202.9 ¹
cb		9.0	202.0
1/4		9.3	201.7
+		9.3	201.7 ¹
1/4		9.7	201.3
cb		9.7	201.3
+4		11.3	199.7
+6 ⁵		11.1	199.9
+7		9.8	201.2
SL		9.6	201.4 ¹
3 + 50			
10's		8.6	202.4
SL		8.7	202.3 ¹
+5		8.4	202.6
+7		9.4	201.6
cb		8.6	202.4
1/4		8.7	202.3
+		8.2	202.8 ¹
1/4		7.7	203.3
cb		7.5	203.5
N.L.		7.2	203.8 ¹

3+25	210.98		
10'N		5.5	205.5
N.L.		5.9	205.1 ✓
cb		5.8	205.2
1/4		5.9	205.1
+		5.9	205.1 ✓
1/4		6.6	204.4
cb		7.3	203.7
S.L.		7.4	203.6 ✓
6'S		7.5	203.5
10'S		7.9	203.1
15'S		7.0	204.0

3+100			
15'S		4.1	206.9
S.L.		3.1	207.9 ✓
cb		2.5	208.5
1/4		3.0	208.0
+		2.8	208.2 ✓
1/4		2.6	208.4
cb		2.6	208.4 ✓
N.L.		2.8	208.2 ✓
T.P.	11.26	221.68 ✓	0.56 210.42

2+75	221.68		44
N.L.		8.3	213.4 ✓
cb		9.8	213.9
1/4		8.0	213.7
+		8.5	213.2 ✓
1/4		9.1	212.6
cb		9.2	212.5
S.L.		9.8	211.9 ✓
20'S		11.4	210.3

2+50			
20'S		9.3	212.4
S.L.		6.7	215.0 ✓
cb		6.0	215.7
1/4		4.6	217.1
+		3.8	217.9 ✓
1/4		3.7	218.0
cb		3.6	218.1
N.L.		3.3	218.4 ✓

2+37 ⁸⁸	= w.L. Alley		
N.L.		0.3	221.4 ✓
cb		0.7	221.0
1/4		0.8	220.9
+		2.0	219.7 ✓
1/4		3.2	218.5
cb		4.6	217.1
S.L.		5.8	215.9 ✓
20'S		8.9	212.8

22168
 2+17⁸⁸ = E.L. Alley.

25'S	10.4	211.3
16'S	10.3	211.4
S.L.	6.3	215.4 ✓
cb	4.1	217.6
1/4	1.4	220.3
TP	12.22	233.64
+	0.26	221.42
1/4	11.1	222.5 ✓
1/4	9.7	223.9
cb	8.6	225.0
N.L.	7.4	226.2 ✓
2+00		
N.L.	2.3	231.3 ✓
+4	2.2	231.4
cb	4.0	229.6
1/4	6.7	226.9
+	9.3	224.3 ✓
1/4	12.4	221.2
cb	15.9	217.7
S.L.	18.6	215.0 ✓
7'S	20.3	213.3
16'S	20.0	213.6
25'S	21.3	212.3

45
 1+75 233.64

30'S	20.4	213.2
13'S	19.0	214.6
S.L.	15.6	218.0 ✓
cb	12.3	221.3
1/4	9.1	222.5
+	6.3	227.3 ✓
1/4	2.3	231.3
TP	12.37	245.52
cb	0.49	233.15
cb	10.0	235.5
N.L.	18.2	237.3 ✓
1+50		
N.L.	5.1	240.4 ✓
cb	7.5	238.0
1/4	10.7	234.8
+	14.9	230.6 ✓
1/4	17.9	227.6
cb	20.7	224.8
S.L.	22.9	222.6 ✓
23'S	28.9	216.6
25'S	31.2	214.3
36'S	30.4	215.1
40'S	29.2	216.3

1+25	245.52		
40's	27.3	217.9	
28's	27.8	217.7	
24's	29.2	216.3	
17's	26.3	219.2	
8's	22.2	223.3	
3L	17.9	225.6 [✓]	
cb	17.9	228.6	
1/4	15.1	230.4	
1/4	11.8	233.7 [✓]	
1/4	8.2	237.3	
cb	4.7	240.8	
N.L.	2.2	243.3 [✓]	
1+00			
N.L.	0.7	244.8 [✓]	
cb	3.0	242.5	
+8	4.7	240.8	
1/4	5.6	239.9	
1/4	9.4	236.1 [✓]	
1/4	13.5	232.0	
cb	15.6	229.9	
3L	17.8	227.7 [✓]	
13's	21.1	224.4	
28's	26.6	218.9	
30's	28.1	217.4	
32's	26.6	218.9	
40's	26.1	219.4	

0+75	245.52		
40's	24.4	221.1	
38's	26.1	219.4	
25's	25.0	220.5	
21's	21.7	223.8	
3L	14.7	230.8	
cb	12.7	232.8	
1/4	10.0	235.5	
1/4	5.9	239.6	
1/4	2.8	242.7	
cb	+0.2	245.7	
N.L.	+1.9	247.4	
0+50			
N.L.	+5.7	251.2	
+5	+6.0	251.5	
cb	+3.6	249.1	
1/4	+3.9	249.4	
1/4	+0.4	245.9	
1/4	4.7	240.8	
cb	7.4	238.1	
3L	11.2	234.3	
27's	22.2	223.3	
34's	20.4	225.1	
40's	21.2	224.3	
FL Culvert at 0+98 vert Albania w. end	21.40	224.12 ^{30" conc.}	

0+25	245.52		
40's	12.9	232.6	
13's	11.1	234.4	
SL	5.2	240.3	
cb	0.8	244.7	
T.P. 10 89	255.73	0.68	244.84
1/4	4.4	251.3	
+5	3.6	252.1	
±	5.3	250.4	
1/4	5.2	250.5	
cb	4.1	251.6	
NL	3.8	251.9	
0+00 = W.L. Alabama			
NL back walk	4.11	251.62	
cb tot cb	4.25	251.48	
get Pav	4.84	250.89	
1/4 ✓	4.71	251.02	
± ✓	4.74	250.99	
1/4 ✓	4.83	250.90	
get ✓	5.07	250.64	
cb tot cb	4.60	251.13	
SL back walk	4.40	251.33	
40's	7.1	248.6	OK
B.M. Myrtle = Ala. NW 7' back	4.16	251.57	251.50
TP 6.40	259.43	2.70	253.03
NW Ala = Cypress. B.M.	14.60	244.83	(244.98) OK

Jan 29-29
London
Isbell
Morgan

B.M.	12.74	264.31	251.57	47
* T.P.			0.85	263.46
X sec Myrtle Ave from W.L.				
Florida to W.L. Georgia OK				
B.M.	12.27	210.28	198.01	sw Florida & Myrtle.
0+00 = W.L. Florida.				
SL			11.8	198.5
cb			12.0	198.3
1/4			11.6	198.7
+7			11.8	198.5
±			11.5	198.8
+5			11.1	199.2
1/4			11.3	199.0
cb			11.4	198.9
NL			11.1	199.2
0+06				
NL			10.4	199.9
+7			11.0	199.3
cb			10.9	199.4
1/4			10.8	199.5
+5			10.5	199.8
±			10.8	199.5
+4			11.0	199.3
1/4			10.4	199.9
cb			10.2	200.1
SL			10.0	200.3

Gorge at 0+15 6' south 0+25	9.6	200.7
SL	9.3	201.0
cb	9.2	201.1
1/4	8.9	201.4
+	9.0	201.3
+5	8.8	201.5
1/4	9.2	201.1
+8	8.6	201.7
cb	8.3	202.0
NL	8.0	202.3
10N	7.6	202.7
0+50		
10N	5.8	204.5
NL	6.2	204.1
+3	6.2	204.1
+6	6.8	203.5
cb	6.6	203.7
+4	7.0	203.3
1/4	6.7	203.6
+8	6.5	203.8
+	6.8	203.5
+3	6.6	203.7
1/4	6.9	203.4
cb	6.8	203.5
SL	6.8	203.5

0+50	210.28	
10's	5.7	204.4
0+75		
10's	+5.0	215.3
SL	+4.3	214.6
cb	+0.9	211.2
+3	0.4	209.9
1/4	1.1	209.2
+2	1.0	209.3
+8	2.3	208.0
+	3.6	206.7
+2	2.6	207.7
1/4	3.0	207.3
cb	3.4	206.9
NL	3.3	207.0
10N	3.7	206.6
T.P. 12.02	222.24	0.06 210.22
0+95		
10N	10.6	211.6
3N	10.2	212.0
2N	11.3	210.9
1N	10.2	212.0
NL	10.1	212.1
cb	9.3	212.9
1/4	7.7	214.5
+	5.9	216.3

0 + 95	222.24		
5'A		4.0	218.2
cb		2.0	220.2
S.L.		1.9	220.3
10'S		1.8	220.4
1 + 10			
10'S		+1.4	223.6
S.L.		+1.6	223.8
cb		+1.3	223.5
1/4		+1.2	223.4
±		+0.6	222.8
1/4		1.6	220.6
cb		2.7	219.5
+5		3.1	219.1
N.L.		4.0	218.2
1N		4.0	218.2
2N		5.4	216.8
3N		5.0	217.2
4N		4.2	218.0
7N		4.2	218.0
9N		7.0	215.2
11N		7.1	215.1
13N		4.6	217.6
T.P.	12.82	0.40	221.84

1 + 31	234.66		
11N		6.4	228.3
9N		8.0	226.7
7N		6.6	228.1
N.L.		6.7	228.0
+1		7.3	227.4
+4		6.7	228.0
+5		5.7	229.0
cb		4.9	229.8
+4		3.5	231.2
1/4		4.2	230.5
+4		4.6	230.1
±		4.3	230.4
1/4		5.1	229.6
cb		5.1	229.6
S.L.		5.6	229.1
10'S		5.7	228.8
1 + 40 = E.L. Wilshire Terrace			
10'S		3.6	231.1
S.L.		3.0	231.7
cb		2.9	231.8
1/4		2.2	232.5
±		2.1	232.6
1/4		2.3	232.4
cb		0.5	234.2
+3		+0.1	234.8
+5		0.2	234.5

247.19

50

1 + 40	234.66		
+6	2.6	232.1	
N.L.	1.8	232.9	
0.2N backwalks	+0.98	235.64	
Willshire Terrace	40' st. 5' cb	30' rdway	
Ecb Willshire Terrace			
X T.R. 12.89	247.19	0.36	234.30
0.2N top cb	11.54	235.65	
0.2N put	12.02	235.17	
N.L. ord.	12.6	234.6	
+2	11.5	235.7	
+7	11.6	235.6	
cb	12.1	235.1	
1/4	13.5	233.7	
+	13.0	234.2	
1/4	13.0	234.2	
+5	13.9	233.3	
cb	14.4	232.8	
SL	14.9	232.3	
10'S	15.0	232.2	

E'a Willshire Terrace		
10's	13.5	233.7
SL	12.8	234.4
cb	12.7	234.5
+8	11.9	235.3
1/4	12.2	235.0
+	11.7	235.5
+2	11.0	236.2
1/4	11.4	235.8
+3	11.8	235.4
cb	11.3	235.9
N.L.	11.7	235.5
0.2N Pav	11.45	235.74
+	Willshire	
0.2N Pav	11.12	236.07
N.L.	11.1	236.1
cb	11.1	236.1
1/4	10.6	236.6
+	11.2	236.0
+11 ⁵ M.H. top	10.77	236.42 ✓
FL	16.15	231.04 ✓
1/4	9.8	237.4
cb	10.7	236.5
SL	11.2	236.0
10'S	12.0	235.2

247.19

w.l. Wiltshire

105	9.7	237.5
SL	9.2	238.0
eb	8.9	238.3
+8	7.6	239.6
1/4	7.8	239.4
4	8.7	238.5
1/4	9.4	237.8
eb	10.0	237.2
+4	10.2	237.0
NL Pav	11.05	236.14

Web Wiltshire

NL top eb	10.51	236.68
NL g.f.	11.18	236.01
+4	9.8	237.4
eb	9.7	237.5
1/4	8.8	238.4
4	7.8	239.4
+5	7.0	240.2
1/4	6.7	240.5
eb	6.0	241.2
S.L.	7.5	239.7

247.19

w.l. Wiltshire = 0+00

SL	6.0	241.2
+7	5.0	242.2
eb	5.1	242.1
+5	5.4	241.8
1/4	6.1	241.1
4	7.5	239.7
1/4	8.1	239.1
+5	7.9	239.3
eb	9.0	238.2
+8	9.0	238.2
NL	10.0	237.2

0+05

NL	3.5	243.7
eb	3.2	244.0
+5	3.0	244.2
1/4	3.4	243.8
4	4.2	243.0
1/4	4.6	242.6
+5	4.5	242.7
eb	4.2	243.0
+6	3.9	243.3
S.L.	4.6	242.6
T.P.	12.65	259.66
	0.18	247.01

51

O + 30	259.66		
S.L.	11.3	248.4	
+6	10.2	249.5	
cb	10.6	249.1	
1/4	9.8	249.9	
+6	9.2	250.5	
+	10.5	249.2	
1/4	10.8	248.9	
cb	10.5	249.2	
N.L.	9.9	249.8	

O + 50			
N.L.	3.9	255.8	
+8	3.8	255.9	
cb	3.1	256.6	
+7	1.8	257.9	
1/4	2.4	257.3	
+	3.7	255.8	
1/4	5.6	254.1	
cb	6.1	253.6	
S.L.	6.4	253.3	

O + 65	259.66		
S.L.	1.9	257.8	
cb	1.7	258.0	
1/4	0.7	259.0	
+	0.7	259.0	
T.P.	12.88	272.45	0.09 259.57
1/4			12.0 260.5
cb			10.6 261.9
N.L.			9.1 263.4
* T.P.			9.04 263.41 (263.46)

O + 83			
N.L.	6.5	266.0	
cb	7.4	265.1	
1/4	8.4	264.1	
+	8.7	263.8	
1/4	8.7	263.8	
cb	8.7	263.8	
SL	8.4	264.1	

O + 89			
S.L.	8.1	264.4	
cb	7.7	264.8	
1/4	6.7	265.8	
+	6.2	266.3	
1/4	5.5	267.0	
cb	4.8	267.7	
N.L.	4.4	268.1	

1+00	272.45		
NL		1.7	270.8
cb		1.9	270.6
1/4		2.4	270.1
±		3.0	269.5
1/4		3.5	269.0
cb		3.7	268.8
SL		4.7	267.8
TP 12.61	285.05	0.01	272.44
1+16			
S.L		12.3	272.7
+2		12.1	273.0
+5		12.9	272.2
cb		12.9	272.2
1/4		11.8	273.3
±		11.7	273.3
1/4		11.3	273.8
cb		11.2	273.9
NL		11.5	273.5

53

1+22	285.05		
NL		7.4	277.6
cb		8.2	276.9
1/4		9.3	275.8
+4		9.4	275.7
+6		10.1	275.0
±		10.2	274.8
1/4		10.7	274.4
cb		11.8	273.3
+5		11.9	273.2
+8		10.9	274.2
SL		11.1	273.9
10S		12.0	273.1
1+40 = E.L. Georgia			
25S		10.8	274.3
SL		8.4	276.6
cb		7.4	277.7
1/4		6.0	279.1
±		5.0	280.0
1/4		4.5	281.6
cb		2.9	282.2
NL		0.3	284.7
TP 6.21	291.08	0.18	284.87

Ecb Georgia 291.08		
1 st N top cb	2.03	289.05
1 st N put	2.59	288.49
N.L.	2.8	288.3
cb	5.2	285.9
+4	5.0	286.1
1/4	6.5	284.6
+6	8.1	283.0
#	8.5	282.6
1/4	10.1	281.0
cb	11.5	279.6
S.L.	13.0	278.1
25's	15.6	275.5

E 1/4 Georgia		
20's	13.0	278.1
7's	12.4	278.7
5's	10.8	280.3
S.L.	11.5	279.6
cb	10.0	281.1
1/4	8.3	282.8
#	6.7	284.4
1/4	3.8	287.3
+3	3.0	288.1
cb	2.7	288.4
N.L.	2.1	289.0
1 st N Pav	1.89	289.19

E Georgia 291.08			54
0 th N Pav	1.51	289.57	
N.L.	1.5	289.6	
cb	2.2	288.9	
1/4	2.3	288.8	
#	3.6	287.5	
1/4	4.5	286.6	
cb	7.7	283.4	
+5	7.2	283.9	
S.L.	9.5	281.6	
3's	9.1	282.0	
11's	12.4	278.7	
20's	13.3	277.8	

W 1/4 Georgia		
15's	11.9	279.2
S.L.	9.3	281.8
+7	7.9	283.2
cb	6.9	284.2
1/4	4.0	287.1
+7	2.2	288.9
#	2.1	289.0
+6	1.4	289.7
1/4	1.4	289.7
cb	1.7	289.4
N.L.	1.5	289.6
0 th N Pav	1.38	289.70

291.08

Wcb Georgia

0 ² N	gut	1.54	289.54
0 ² N	topcb	0.78	290.30
N.L.		1.4	289.7
cb		0.9	290.2
1/4		0.9	290.2
+4		1.1	290.0
+		2.4	288.7
1/4		4.7	286.4
cb		6.9	284.2
SL		9.0	282.1
15's		11.6	279.5

W.L. Georgia

15's		10.9	280.2
SL		8.0	283.1
cb		6.0	285.1
1/4		3.8	287.3
+		1.3	289.8
+5		0.0	291.1
1/4		+0.3	291.11
cb		+0.8	291.16
N.L.		0.3	290.8

T.P.	2.09	290.96	2.21	288.87	
T.P.	1.19	285.70	6.45	284.51	
T.P.	0.13	272.78	13.05	272.65	
BM	SW Cypress 2 Willshire Terrace		11.13	261.65	261.53

SW Cypress
2 Willshire Terrace

Not in BM Book 55

BM	0.39	261.92	✓	261.53
T.P.	0.71	252.60	12.03	251.89
BM			7.72	244.88 (244.98)

Curb levels on Landis St
from 42nd to Fairmont

Jan 30-23
Louden
Jobell
Morgan.

Not in BMB Book

B.P. NW
42nd & Landis.

B.M.	6.51	348.81	342.30
0+00 = E.L.	42 nd		
Ncb	6.06	342.75	
Scb	6.53	342.28	
0+25			
Scb	6.39	342.42	
Ncb	6.00	342.81	
0+50			
Ncb	5.72	343.09	
Scb	6.17	342.64	
0+75			
Scb	6.00	342.81	
Ncb	5.60	343.21	
1+00			
Ncb	5.38	343.43	
Scb	5.88	342.93	
1+25			
Scb	5.75	343.06	
Ncb	5.21	343.60	
1+40 = W.L. Alley			
N.L. End Alley cb	4.88	343.93	
Ncb	5.08	343.73	
Scb	5.66	343.15	
S.L. End Alley cb	5.37	342.44	

Plotted Feb. 5-1929. CBH

348.81

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1+60 = E.L. Alley

S.L. End of Alley cb	5.16	343.65
Scb	5.37	343.44
Ncb	5.01	343.80
N.L. end Alley cb	4.83	343.98
1+75		
Ncb	4.89	343.92
Scb	5.33	343.48
2+00		
Scb	5.16	343.65
Ncb	4.68	344.13
2+25		
Ncb	4.49	344.32
Scb	5.00	343.81
2+50		
Scb	4.88	343.93
Ncb	4.46	344.35
2+75		
Ncb	4.24	344.57
Scb	4.70	344.11
3+00 = W.L. Van Dyke		
Scb	4.41	344.40
Ncb	3.96	344.85

348.81

Web Van Dyke			
N.L. top cb	3.92	344.89	
N.L. gnt	4.52	344.29	
S.L. top cb	4.42	344.39	
S.L. gnt	5.09	343.72	
W ^{1/4} Van Dyke			
T.P. 7.06	351.90	3.97	344.84
S.L. Pav	7.78	344.12	
N.L. ✓	6.91	344.99	
E Van Dyke			
N.L. Pav	6.65	345.25	
S.L. ✓	7.56	344.34	
E ^{1/4} Van Dyke			
S.L. Pav	7.55	344.35	
N.L. ✓	6.76	345.14	
Ecb Van Dyke			
N.L. gnt	7.17	344.73	
N.L. top cb	6.55	345.35	
S.L. gnt	7.78	344.12	
S.L. top cb	7.05	344.85	
FL Van Dyke = 0+00			
Sdb	7.00	344.90	
Ncb	6.61	345.29	
0+25			
Ncb	6.42	345.48	
Sdb	6.86	345.04	

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0+50	351.90		
Sdb	6.54	345.36	
Ncb	6.17	345.73	
0+75			
Ncb	6.05	345.85	
Sdb	6.43	345.47	
1+00			
Sdb	6.31	345.59	
Ncb	5.81	346.09	
1+25			
Ncb	5.54	346.36	
Sdb	6.11	345.79	
1+40 = W.L. Alley			
Sdb	6.12	345.78	
sdb Alley Pav.	6.50	345.40	
Ncb	5.44	346.46	
Ncb Alley Pav.	6.09	345.81	
1+60 = F.L. Alley			
Ncb Alley Pav.	5.94	345.96	
Ncb	5.34	346.56	
Sdb	5.74	346.16	
Sdb Alley Pav.	6.35	345.55	
1+75			
Sdb	5.68	346.22	
Ncb	5.27	346.63	

2+00 • 351.90

Neb.	5.06	346.84
Seb	5.46	346.44
2+25		
Seb	5.38	346.52
Neb	4.97	346.93
2+50		
Neb	4.70	347.20
Seb	5.06	346.84
2+75		
Seb	4.95	346.95
Neb	4.47	347.43
2+99.6 = N.L. 43rd St.		
Neb	4.32	347.50
Seb	4.65	347.25
Web. 43rd		
S.L. top eb	4.67	347.23
S.L. put	5.34	346.56
N.L. top eb	4.24	347.66
N.L. put	4.88	347.02
B.M.		
	4.24	

351.90

58

W's 43rd

N.L. Pav	4.24	347.66
S.L. ✓	4.93	346.97
+ 43rd		
S.L. Pav	4.66	347.24
N.L. ✓	3.96	347.94
E's 43rd		
N.L. Pav	3.99	347.91
S.L. ✓	4.72	347.18
Ecb 43rd		
S.L. put	5.01	346.89
S.L. top eb	4.27	347.63
N.L. put FL ^(ground ref) _{collected}	4.83	347.07
N.L. top eb	3.79	348.11
E.L. 43rd = 0+0.0		
Neb	3.77	348.13
Seb	4.14	347.76
0+25		
Seb	4.13	347.77
Neb	3.73	348.17
0+50		
Neb	3.68	348.22
Seb	4.15	347.75
0+75		
Seb	4.09	347.81
Neb	3.52	348.38

	1+00	351.90	
Neb.		3.49	348.41
Seb		4.05	347.85
	1+25 = W.L. Alley		
S.L. end Alley eb.		3.80	348.10
Seb		3.98	347.92
Neb		3.34	348.56
N.L. end Alley eb.		3.16	348.74
	1+45 = E.L. Alley.		
N.L. end Alley eb.		3.13	348.77
Neb		3.19	348.71
Seb		3.93	347.97
S.L. end Alley eb.		3.82	348.08
	1+75		
Seb		3.97	347.93
Neb		3.24	348.66
	2+00		
Neb		3.18	348.72
Seb		3.92	347.98
	2+25		
Seb		3.84	348.06
Neb		3.08	348.82
	2+50		
Neb		2.95	348.95
Seb		3.84	348.06

			351.90	
	2+70 ⁵	= W.L. Fairmont Ave.		59
Seb			3.68	348.22
gut	Par		3.97	347.93
1/4	✓		3.64	348.26
+	✓		3.28	348.62
1/4	✓		3.22	348.68
gut	✓		3.08	348.82
Neb			2.72	349.18
SP NW	Fairmont & Landis			
B.M.			2.79	349.11
				Note in B.M. Book

Cross Section ^{52'} Roadway LANDIS ST.
from N.W. 42nd to N.W. Fairmount St.

349.26

60

434	349.26		344.92	N.W. B.P. Landis + Van Dyke
	N.W. 42nd	13' 25"		
S. Gut.		7.8	341.5	
" 1/4		7.4	341.9	
2		7.2	342.1	
N 1/2		7.3	342.0	
" Gut.		7.4	341.9	
	N ch			
N on Pav.		7.44	341.82	
" Gut. = ch line		7.5	341.8	
" 1/4		7.4	341.9	
1		7.7	341.6	
S 1/4		7.7	341.6	
" Gut.		7.9	341.4	
S. on Paving		7.94	341.32	
	N 1/4			
S. on Paving		7.53	341.73	
S. Gut.		7.3	342.0	
" 1/4		7.2	342.1	
1		7.2	342.1	
N 1/2		7.0	342.3	
" Gut.		7.0	342.3	
N. on Pav.		6.82	342.44	
	2 42nd			
N " "		6.67	342.59	

N. Gut.	6.5	342.8
" 1/2	6.6	342.7
1	6.7	342.6
S 1/4	6.9	342.4
" Gut.	7.1	342.2
" on Pav.	7.12	341.84
	E 1/4	
S " "	7.48	341.78
S. Gut.	7.3	342.0
" 1/4	7.2	342.1
1	7.1	342.1
N 1/2	7.0	342.3
" Gut.	7.0	342.3
"	6.77	342.49
	E cb	
N. on Ground	7.1	342.2
cb.	7.4	341.9
1	7.4	341.9
1	7.5	341.8
1	7.5	341.8
cb.	7.7	341.6
S. on Pav.	7.73	341.53
	E. to 42nd = 0+00	
S. Gut.	7.6	341.7
" 1/4	7.2	342.1
1	7.1	342.2

N $\frac{1}{2}$	7.0	342.3
" Gut.	7.2	342.1
0+50		
N "	6.7	342.6
" $\frac{1}{2}$	6.3	343.0
$\frac{1}{2}$	6.4	342.9
S $\frac{1}{2}$	6.6	342.7
" Gut.	7.2	342.1
1+00		
" "	6.9	342.4
" $\frac{1}{2}$	6.4	342.9
$\frac{1}{2}$	5.9	343.4
N $\frac{1}{2}$	6.1	343.2
" Gut.	6.4	342.9
1+50		
" "	6.3	343.0
" $\frac{1}{2}$	5.8	343.5
$\frac{1}{2}$	5.7	343.6
S $\frac{1}{2}$	6.0	343.3
" Gut.	6.5	342.8
2+00		
S Gut.	6.2	343.1
" $\frac{1}{2}$	5.7	343.6
$\frac{1}{2}$	5.2	344.1
N $\frac{1}{2}$	5.7	343.6
" Gut.	5.9	343.4

0+50		
N. Gut.	1.6	344.7
" $\frac{1}{2}$	5.2	344.1
$\frac{1}{2}$	5.1	344.2
S $\frac{1}{2}$	5.5	343.8
" Gut.	5.9	343.4
3+00 = M.L. Van Dyke		
S Gut.	5.2	344.1
" $\frac{1}{2}$	5.0	344.3
$\frac{1}{2}$	4.5	344.8
N $\frac{1}{2}$	4.8	344.5
" Gut.	5.0	344.3
M. Cb.		
N on Porc.	4.97	344.28
cb.	4.9	344.4
$\frac{1}{2}$	4.7	344.6
$\frac{1}{2}$	4.4	344.9
$\frac{1}{2}$	4.8	344.5
cb.	5.3	344.0
S. on Porc.	5.48	343.78
M $\frac{1}{2}$		
S " "	5.13	344.13
cb.	4.7	344.6
$\frac{1}{2}$	4.5	344.8
$\frac{1}{2}$	4.3	345.0
$\frac{1}{2}$	4.3	345.0

cb.	4.4	344.9
N on Parking	4.30	344.96
	E Van Dyke	
N " "	4.01	345.25
cb.	4.4	344.9
$\frac{1}{2}$	4.2	345.1
$\frac{1}{2}$	4.1	345.2
$\frac{1}{2}$	4.3	345.0
cb.	4.5	344.8
S on Pav.	4.89	344.37
	E $\frac{1}{2}$	
" " "	4.86	344.40
cb.	4.6	344.7
$\frac{1}{2}$	4.6	344.7
$\frac{1}{2}$	4.4	344.9
$\frac{1}{2}$	4.4	344.9
cb.	4.3	345.0
N on Pav.	4.09	345.17
	E cb	
N " "	4.5	344.8
cb.	4.5	344.8
$\frac{1}{2}$	4.6	344.7
$\frac{1}{2}$	4.7	344.6
$\frac{1}{2}$	4.7	344.6
cb.	4.7	344.6
S on Pav.	5.15	344.11

E.L. VAN DYKE			
S Gut.	4.8	344.5	
" $\frac{1}{2}$	4.4	344.9	
$\frac{1}{2}$	4.2	345.1	
N $\frac{1}{2}$	4.1	345.2	
" Gut.	4.5	344.8	Van Dyke - handly
T.P.	7.85	352.77	on 81%
	0+50		
N Gut.	7.8	345.0	
" $\frac{1}{2}$	7.5	345.3	
$\frac{1}{2}$	7.2	345.6	
$\frac{1}{2}$	7.5	345.3	
S Gut.	8.2	344.6	
	1+00		
S "	7.8	345.0	
" $\frac{1}{2}$	7.1	345.7	
$\frac{1}{2}$	6.8	346.0	
N $\frac{1}{2}$	7.0	345.8	
N Gut	7.4	345.4	
	1+50		
N Gut on Parking - Alley at cb. line &	6.92	345.85	
" $\frac{1}{2}$	6.3	346.5	
$\frac{1}{2}$	6.1	346.7	
S $\frac{1}{2}$	6.5	346.3	
S Gut on Pav. - Alley at cb. line &	7.29	345.48	
	2+00		

S Gut.	6.9	345.9
" $\frac{1}{2}$	6.5	346.3
$\frac{1}{2}$	6.1	346.7
N $\frac{1}{2}$	6.4	346.4
" Gut.	6.5	346.3
5450		
N Gut.	6.3	346.5
" $\frac{1}{2}$	5.9	346.9
$\frac{1}{2}$	5.6	347.2
$\frac{1}{2}$	6.1	346.7
S Gut.	6.5	346.3
3400 = 11/2 439 ^{14' cb} _{13' 25}		
S Gut.	6.0	346.8
" $\frac{1}{2}$	5.5	347.3
$\frac{1}{2}$	5.1	347.7
N $\frac{1}{2}$	5.5	347.3
N Gut.	5.6	347.2
11 cb.		
N on Pav.	5.74	347.03
cb.	5.8	347.0
$\frac{1}{2}$	5.1	347.7
$\frac{1}{2}$	5.0	347.8
$\frac{1}{2}$	5.3	347.5
cb.	5.9	346.9
S on Pav.	6.22	346.55
11 $\frac{1}{2}$		

S on Pav.	5.81	346.96
cb.	5.4	347.4
$\frac{1}{2}$	5.1	347.7
$\frac{1}{2}$	4.8	348.0
$\frac{1}{2}$	4.9	347.9
cb.	5.0	347.8
N on Pav.	5.14	347.63
E 4.814		
N " "	4.89	347.88
cb.	4.6	348.2
$\frac{1}{2}$	4.7	348.1
$\frac{1}{2}$	4.6	348.2
$\frac{1}{2}$	4.8	348.0
cb.	5.0	347.8
S on Parking	5.53	347.24
E 1		
S " "	5.59	347.18
cb.	5.1	347.7
$\frac{1}{2}$	4.9	347.9
$\frac{1}{2}$	4.7	348.1
$\frac{1}{2}$	4.7	348.1
cb.	4.7	348.1
N on Pav.	4.86	347.91
E cb.		
N " "	5.71	347.06
cb.	4.7	348.1

$\frac{1}{2}$	47	348.1
$\frac{1}{6}$	47	348.1
$\frac{1}{4}$	50	347.8
cb.	54	347.4
S. on Pav.	589	346.88
E.L. 43rd = 0+00		
S. Gut.	57	347.1
" $\frac{1}{4}$	50	347.8
$\frac{1}{2}$	48	348.0
$\frac{1}{4}$	48	348.0
N. Gut.	51	347.7
0+50		
N. Gut.	53	347.5
$\frac{1}{4}$	48	348.0
$\frac{1}{2}$	46	348.2
$\frac{1}{4}$	50	347.8
S. Gut.	56	347.2
1+00		
S. Gut.	54	347.4
S. $\frac{1}{4}$	49	347.9
$\frac{1}{6}$	45	348.3
N. $\frac{1}{2}$	47	348.1
N. Gut.	50	347.8
1+50		
N. Gut.	49	347.9
N. $\frac{1}{2}$	46	348.2

$\frac{1}{2}$	44	348.4
$\frac{1}{4}$	48	348.0
S. Gut.	53	347.5
2+00		
S. Gut.	53	347.6
" $\frac{1}{4}$	47	348.1
$\frac{1}{6}$	44	348.4
N. $\frac{1}{4}$	45	348.3
" Gut.	48	348.0
2+50		
N. Gut.	47	348.1
" $\frac{1}{4}$	45	348.3
$\frac{1}{2}$	42	348.6
S. $\frac{1}{4}$	45	348.3
" Gut.	51	347.7
3+00 = 1/2 Fairmount		
S. Gut. on Pav.	484	347.93
" $\frac{1}{4}$ " "	456	348.21
$\frac{1}{6}$ " "	419	348.58
N. $\frac{1}{4}$ " "	415	348.62
" Gut. " "	403	348.74
cbk. N. of B.M. Page 59	366	349.11
349.11 - Landis 0.00 = Error.		



Bill Bliss
4/12/49

X Section Me Clintock Street. El Cajon

to Monroe
+ H.I. - Elev 60' St
12' 6" 8"
3' 8" 8"
El Cajon 372

BM 5.57 379.07 373.50

TP 5.53 378.37 623 372.84

comparing 0' 00' See sketch Page 65

E Top cb 5.56 372.81

G 6.08 372.29

1/4 5.80 372.57

ϕ 5.50 372.87

1/4 5.57 372.80

G 5.78 372.59

W Top cb 5.27 373.10

01.05

W 5.23 373.14

G 5.7 372.7

+5 5.5 372.9

1/4 5.6 372.8

ϕ 5.5 372.9

1/4 5.7 372.7

G 6.0 372.4

E Top cb 5.61 372.76

01.50

E Top cb 5.96 372.91

G 5.9 372.5

1/4 5.6 372.8

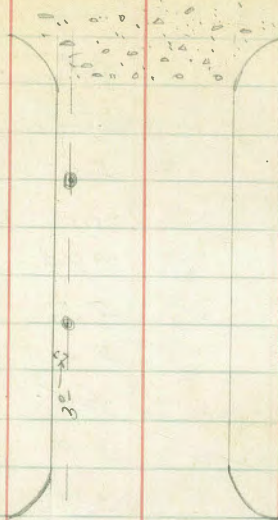
ϕ 5.3 373.1

+5 5.3 373.1

Used These Notes for yardage CB. Hou94

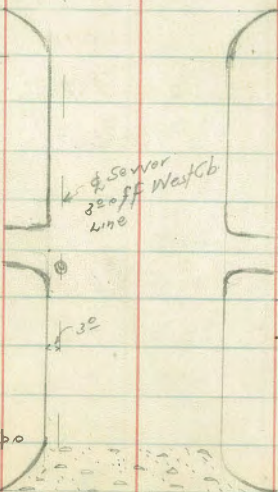
Monroe

Street 65



Meade

Street



El Cajon

Blvd

#	H.I.	-	Elev
	378.37		
14		5.4	373.0
15		5.6	372.8
G		5.6	372.8
W Top cb		5.07	373.30
		1400	
W Top cb		4.84	373.53
G		5.5	372.9
14		5.0	373.4
Q		4.9	373.5
14		5.4	373.0
G		5.7	372.7
E Top cb		5.05	373.32
		1440 S. Line Alley	
E on Top cb		4.61	373.76
E on Ground		4.6	373.8
E Top cb		4.72	373.65
G		5.2	373.2
14		5.0	373.4
15		4.7	373.7
Q		4.6	373.8
14		4.8	373.6
G		5.0	373.4
W Top cb		4.59	373.78
W on Top cb		4.26	374.11
W on Ground		4.3	374.1

H.I.		
378.37		
	1444 Mn. Hole	
	Mn. Hole on Rim ^{30° off} West of cb	4.82
		373.55
	1475 E. of Alley	
	N	4.2
		374.2
	cb	5.0
		373.4
	14	4.7
		373.7
	Q	4.6
		373.8
	14	4.9
		373.5
	G	5.3
		373.1
	E	5.0
		373.4
	1455 N. Line of Alley	
	E on Top cb	4.56
		373.81
	E	4.7
		373.7
	E Top cb	4.81
		373.56
	G	5.3
		373.1
	14	5.0
		373.4
	Q	4.5
		373.9
	14	4.7
		373.7
	G	5.0
		373.4
	W Top cb	4.31
		374.06
	W on Top cb	4.08
		374.29
	W on Ground	4.1
		374.3
	2100	
	W Top cb	4.11
		374.26
	G	4.8
		373.6
	15	4.7
		373.7

	H.I.	Elev
	378.37	
1/4	4.4	374.0
+6	4.2	374.2
⊕	4.3	374.1
1/4	4.7	373.7
⊖	5.2	373.2
E Topcb	4.55	373.82
	2+5.0	
E Topcb	4.23	374.14
G	4.8	373.6
1/4	4.4	374.0
+5	4.1	374.3
⊕	4.0	374.4
1/6	4.0	374.4
1/4	4.2	374.2
⊖	4.6	373.8
W Topcb	3.91	374.46
	3+0.0	
W Topcb	3.51	374.86
G	4.3	374.1
1/4	3.8	374.6
+4	3.5	374.9
⊕	3.5	374.9
+5	3.7	374.7
1/4	4.0	374.4
G	4.4	374.0
E Topcb	3.88	374.49

	H.I.	Elev
	378.37	
	3+5.0	
E Topcb	3.58	374.79
G	4.2	374.2
1/4	3.6	374.8
⊕	3.2	375.2
+6	3.2	375.2
1/4	3.3	375.1
+5	3.5	374.9
G	3.7	374.7
W Topcb	3.09	374.5
	4+0.0	
W Topcb	2.91	375.46
G	3.5	374.9
+5	3.4	375.0
1/4	3.1	375.3
+4	2.9	375.5
⊕	3.0	375.4
+3	3.1	375.3
1/4	3.5	374.9
J.P.	6.40	381.88
G	2.89	375.98
E Topcb	7.4	374.5
	6.86	375.02
	9+5.0	
E Topcb	6.52	375.36
G	7.2	374.7
1/4	6.7	375.2

67

H.I.
381.88

Elev

17	6.1	375.8
2	6.1	375.8
1/4	6.1	375.8
+4	6.6	375.3
G	6.6	375.3
N. Topcb	6.06	375.82
	5400	
N. Topcb	5.62	376.26
G	6.3	375.6
+4	6.0	375.9
1/4	5.8	376.1
2	5.8	376.1
+2	5.9	376.0
1/4	6.3	375.6
G	6.9	375.0
E. Topcb	6.2	375.66
	5450	
E. Topcb	5.89	375.99
G	6.5	375.4
1/4	6.0	375.9
+3	5.7	376.2
2	5.4	376.5
+5	5.3	376.6
1/4	5.5	376.4
+4	5.8	376.1
G	6.0	375.9

H.I.
381.88

Elev

68

W. Topcb	5.31	376.57
	64.05	Line of Meade
W. Topcb	5.03	376.85
G	5.8	376.1
+5	5.4	376.5
1/4	5.0	376.9
2	5.0	376.9
1/4	5.4	376.5
G	5.9	376.0
E. Topcb	5.57	376.31
	N. Line of Meade = 00	
E. Topcb	5.36	376.52
G	5.7	376.2
1/4	5.3	376.6
2	4.8	377.1
1/4	4.7	377.2
+5	4.8	377.1
G	4.8	377.1
N. Topcb	4.51	377.37
	01.25	
W. Topcb	4.56	377.32
G	5.1	376.8
+5	4.9	377.0
1/4	4.9	377.0
2	5.0	376.9
1/4	5.4	376.5

+

#I.
38188

-

Elev

G	5.7	376.2
E Topcb	5.21	376.67
	OK50	
E Topcb	5.09	376.84
G	5.6	376.3
+5	5.5	376.4
1/4	5.2	376.7
B	4.7	377.2
1/4	4.6	377.3
G	4.9	377.0
N Topcb	4.39	377.49
	1100	
N Topcb	4.06	377.88
G	4.6	377.3
1/4	4.7	377.2
+5	4.6	377.3
d	4.6	377.3
1/4	5.1	376.8
G	5.5	376.4
E Topcb	4.74	377.14
	1A50	
E Topcb	4.46	377.42
G	5.2	376.7
1/4	4.8	377.1
B	4.3	377.6
+7	4.3	377.6

+

#I.
38188

-

Elev

69

1/4	4.3	377.6
G	4.5	377.4
N Topcb	3.94	377.94
	2700	
N Topcb	3.66	378.22
G	4.2	377.7
1/4	4.0	377.9
d	4.1	377.8
1/4	4.5	377.4
G	4.9	377.0
E Topcb	4.23	377.65
J.P.	6.08	383.78
	2750	
E Topcb	5.83	377.95
G	6.5	377.3
1/4	6.0	377.8
B	5.6	378.2
1/4	5.4	378.4
+6	5.5	378.3
G	5.8	378.0
N Topcb	5.33	378.45
	3700	
N Topcb	5.21	378.57
G	5.5	378.3
1/4	5.3	378.5

+

H.I.
383.78

-

Elev

£	5.4	378.4
+4	5.6	378.2
1/4	5.8	378.0
G	6.2	377.7
E Topcb	5.57	378.21
	3750	
E Topcb	5.25	378.53
G	6.1	377.7
+3	6.0	377.8
1/4	5.6	378.2
+4	5.4	378.4
£	5.2	378.6
1/4	5.2	378.6
+3	5.3	378.5
G	5.4	378.4
N Topcb In Driveway	5.34	378.44
	4700	
N Topcb	4.65	379.13
G	5.1	378.7
1/4	4.9	378.9
£	5.0	378.8
+4	5.0	378.8
1/4	5.3	378.5
+6	5.6	378.2
G	5.6	378.2
E Topcb	5.03	378.75

+

H.I.
383.78

-

Elev

70

	4750	
E Topcb	4.69	379.09
G	5.3	378.5
+3	5.4	378.4
1/4	5.2	378.6
+5	4.8	379.0
£	4.7	379.1
1/4	4.8	379.0
G	5.0	378.8
N Topcb	4.49	379.29
	4760 Mn Hole ^{2.5 off} West Cb	
Rim	4.76	379.02 ✓
	5700	
N Topcb	4.23	379.55
G	4.7	379.1
1/4	4.4	379.4
£	4.5	379.3
+4	4.6	379.2
1/4	4.9	378.9
G	5.3	378.5
E Topcb	4.53	379.25
	5750	
E Topcb	4.27	379.51
G	4.8	379.0
+4	4.8	379.0
1/4	4.5	379.3

	H.L. 383.78	-	Elev
t3		4.2	379.6
2		4.1	379.7
17		4.0	379.8
1/4		4.2	379.6
G		4.5	379.3
N Top cb		4.17	379.61
		5.185	
N Top cb		3.89	379.94
G		4.3	379.5
t5		4.3	379.5
1/4		4.1	379.7
t4		3.9	379.9
2		4.1	379.7
1/4		4.4	379.4
G		4.8	379.0
E Top cb		4.14	379.64
		6.101 ²⁰	Line of Monroe
E Top cb	on paving	3.99	379.79
G		4.51	379.27
1/4		4.30	379.48
2		4.14	379.64
1/4		4.03	379.75
G		4.29	379.54
N Top cb		3.67	380.11
check BM		9.12	374.66
			374.50
			0.16 error

SWBP
37²⁰ + Monroe

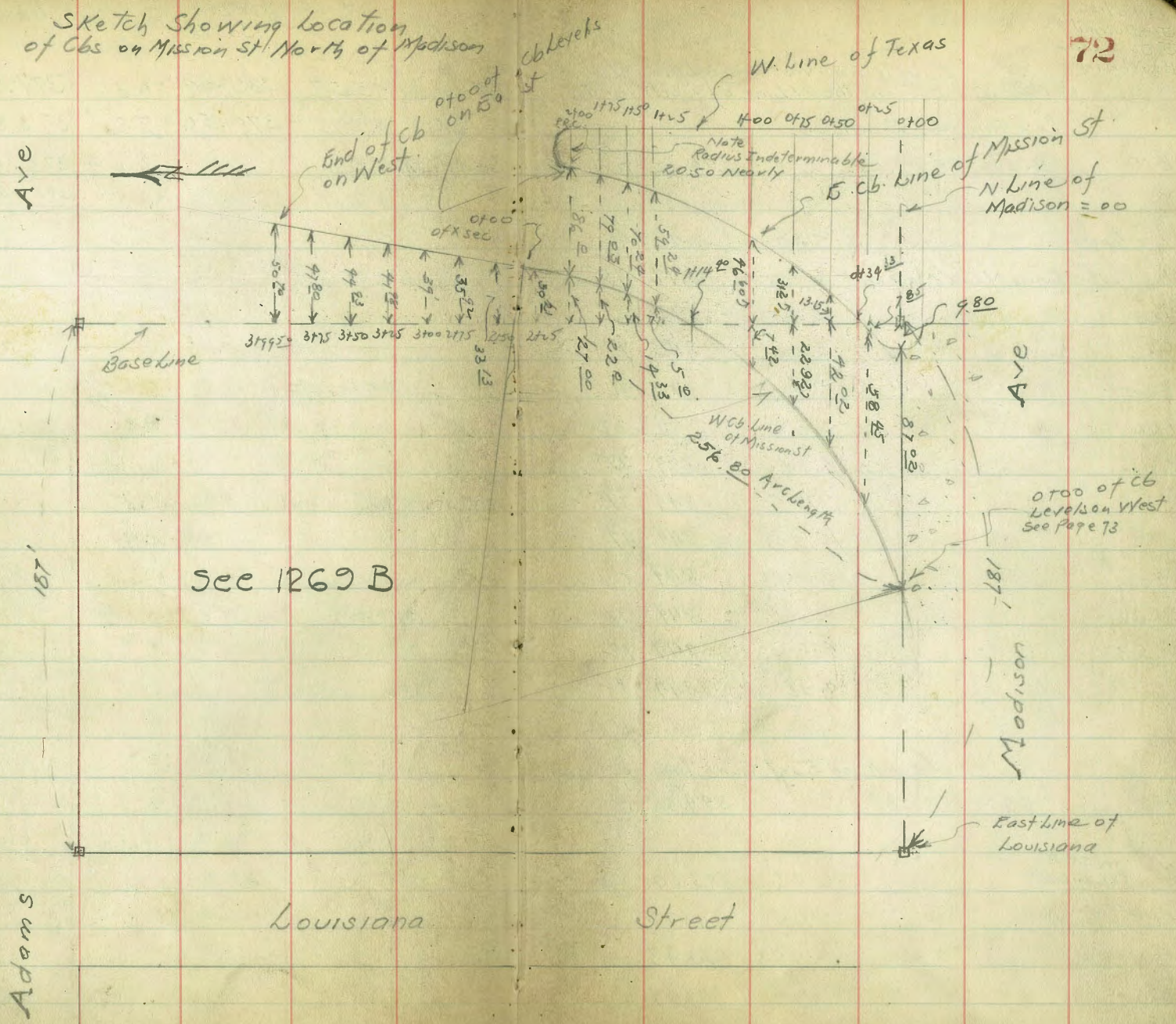
	H.L. 383.78	-	Elev
TP		3.57	381.04
TP		5.75	379.56
		6.31	377.47
		7.23	373.81
		6.04	373.52
			373.50
			0.02 error

check starting BM.

71
SWBP
E/Capn 37⁷⁵

Bill Bliss
4/7/28

Sketch Showing Location of Obs on Mission St North of Madison



Bill Bliss
 Joe Duermit
 J. Jacobszon
 P. Kiernan

Levels on West Curb line of
 Mission St. from the N. Line of Madison to
 P. of Tan. W. of Madison.

BM	3.02	349.05	346.03	S. E. B. P. Texas - Madison
0100 Topcb	5.60	343.45		1771
0100 Corneraving N. Line Madison	6.10	342.95		1111
0125	5.93	343.62		100. Pub. Driveway
0155	5.28	343.77		2728 ² Paragon Madison
0185	5.09	343.96		
1100	5.03	344.02		
1125	4.90	344.15		
1150	4.74	344.31		
1180	4.58	344.47		
2100	4.48	344.57		
2125	4.31	344.74		
2153	4.23	344.82		
2156 ⁶⁰ P. of Tan	4.21	344.84		

Levels on East Curb line of Mission

BM	552	350.37	344.85
0100 ^{See sketch} PRC on East	6.77	343.60	
0125	6.65	343.72	
0150	6.44	343.93	
0175	6.28	344.09	
1100	6.10	344.27	

Long Chord 257⁸⁰ / 2 4 24^{21.00}
 from P.C. to P.C. 125

1125	5.90	344.47
1150	5.70	344.67
1171	5.64	344.73
1111	6.13	344.24
100. Pub. Driveway	6.17	344.26
2728 ² Paragon Madison	6.05	344.32

Levels Around Return Texas Mission

0100	6.77	343.60
0110 ²⁰	6.84	343.53
0120 ⁴⁰	6.85	343.52
0130 ⁶⁰	6.82	343.55
0140 ⁸⁰	6.84	343.53
0151 Paragon on Texas	7.46	342.91
0151 Topcb	6.80	343.57

X Sections of Mission Street
from P. of Ton North of Madison North.

				SE BP Texas & Madison
BM	3.02	344.05	346.03	
IP.	3.70	348.55	4.20	344.85 Taken at Right Angles to C6
				of 00 See sketch
N Topcb		4.21	344.34	
G		4.4	344.2	
+5		4.9	343.7	
+10		5.0	343.6	
+20		4.7	343.9	
+30		5.2	343.4	
+40		5.4	343.2	
		0+25		
-90		5.8	342.8	
-30		5.5	343.1	
-20		5.3	343.3	
-16		5.4	343.2	
-11		5.4	343.2	
-6		4.8	343.8	
G		4.4	344.2	
N Topcb		3.55	345.00	
		0+50		
N Topcb		3.46	345.09	
G		4.1	344.5	
+7		4.3	344.3	
+15		4.8	343.8	
+20		5.3	343.3	

HZ
348.35

74

+24	5.8	342.8
+27	6.6	342.0
+30	6.7	341.9
+32	6.4	342.2
+40	6.6	342.0
	0+59	
-40	7.2	341.4
-32	5.4	343.2
-25	5.1	343.5
-20	4.7	343.9
-10	4.2	344.4
G	4.1	344.5
N Topcb	3.41	345.14
	0+65	
N Topcb	3.39	345.16
G	4.0	344.6
+10	4.2	344.4
+20	4.6	344.0
+25	5.0	343.6
+35	5.4	343.2
+40	5.5	343.1
	0+95	
-40	5.3	343.3
-37	4.8	343.8
-30	4.8	343.8
-20	4.8	343.8

HZ
34855

-10	49	343.7
G	45	344.1
W Topcb	3.74	344.81
	1400	
W Topcb	3.78	344.77
G	46	344.0
+10	49	343.7
+20	48	343.8
+30	46	344.0
+35	43	344.3
+37	3.7	344.9
+40	3.6	345.0
	1413	
-40	3.8	344.8
-35	3.5	345.1
-31	3.7	344.9
-27	4.7	343.9
-20	49	343.7
-10	49	343.7
G	47	343.9
W Topcb	3.87	344.68
	1425	
W Topcb	3.96	344.59
G	4.8	343.8
+10	50	343.6
+20	50	343.6

HZ
34855

4.06

75

+30	5.1	343.5
+35	4.4	344.2
+40	4.8	343.8
	1446	
-40	5.3	343.3
-30	5.4	343.2
-25	5.3	343.3
-20	5.2	343.4
-10	5.2	343.4
G	4.9	343.7
W Topcb	4.09	344.46
	1450	
W Topcb	4.16	344.39
G	5.0	343.6
+10	5.2	343.4
+20	5.2	343.4
+30	5.4	343.2
+34	5.6	343.0
+37	6.3	342.3
+40	8.4	340.2
+45	12.0	336.6
+50 Tooslope	14.9	333.7
	1475	
-50 " "	17.6	331.0
-40	13.0	335.6
-38	10.9	337.7

H.I
398.55

-34	8.9	339.7
-30	6.1	342.5
-26	5.4	343.2
-20	5.4	343.2
-10	5.3	343.3
-5	5.2	343.4
G	5.1	343.5
N Tapcb	4.41	344.14
TP	362 347.61	4.56 343.99
	1785 = End of cb on N	
W.Cb-20	2.3	345.3
-10	3.3	344.3
N Tapcb	3.62	343.99
G	3.9	343.71
+5	4.1	343.5
+10	4.5	343.1
+20	4.3	343.3
+27	4.3	343.3
+30	4.8	342.8
+35	6.8	340.8
+40	11.6	336.0
150 Toe	16.7	330.9
	2+00	
-50	17.5	330.1
-45	14.8	332.8
-40	12.4	335.2

H.I
397.4

76

-32	5.4	342.2
-28	4.6	343.0
-20	4.4	343.2
-10	4.4	343.2
-4	4.3	343.3
-2	3.9	343.7
06	3.8	343.8
+5	4.0	343.6
+10	3.3	344.3
+15	2.9	344.7
+20	2.5	345.1
	2+25	
-20	2.9	344.7
-15	3.2	344.4
-10	3.8	343.8
06	4.4	343.2
+7	4.8	342.8
+10	4.9	342.7
+20	4.9	342.7
+22	5.1	342.5
+30	6.0	341.6
+31	7.7	339.9
+40	9.4	338.2
+41	14.5	333.1
+50	17.4	330.2

H.I.
34761

2738

-50	16.0	331.6
-40	13.7	333.9
-38	9.4	338.2
-35	8.6	339.0
-28	6.1	341.5
-25	5.7	342.2
-20	5.4	342.2
-10	5.1	342.5
06	4.7	342.9
+5	4.2	343.4
+10	3.8	343.8
+15	3.4	343.2
+20	3.0	344.6
	2750	
-20	3.1	344.5
-10	3.3	344.3
06	4.4	343.2
+5	4.9	342.7
+10	5.1	342.5
+15	5.6	342.0
+20	6.1	341.5
+22	6.3	341.3
+30	8.6	339.0
+37	10.9	336.7
+40	11.9	335.7

+

H.I.
34761

77

+43	12.5	335.1
+44	14.8	332.8
+50	17.4	330.2
	2765	
-50	16.1	331.5
-42	13.7	333.9
-40	12.0	335.6
-34	10.4	337.2
-30	9.4	338.2
-23	7.9	339.7
-20	7.5	340.1
-13	5.9	341.7
-10	5.6	342.0
06	4.0	342.6
+10	2.9	345.2
+20	2.6	345.0
	2780	
-20	4.1	343.5
-10	5.1	342.5
-5	5.5	342.1
06	6.5	341.1
+5	7.2	340.4
+10	7.8	339.8
+15	8.9	338.7
+17	10.3	337.3
+20	11.1	336.5

	H.I.	-	Elev.
	347.61		
+25		12.9	334.7
+30		14.6	333.0
+35		17.8	329.8
+38 Top vertical Bank		19.~	328.6
		31.00	
-30 Top "	"	20.1	327.5
-26		17.3	330.3
-20		14.8	332.8
-16		12.5	335.1
-10		9.7	337.9
-5		8.1	339.5
26		6.8	340.8
+5		5.5	342.1
+10		5.2	342.4
+14 ⁸⁵ W Profile		5.0	342.6
+20		4.8	342.8
T.P.	6.02	350.32	3.31 344.30
checkout		4.30	346.02 ✓

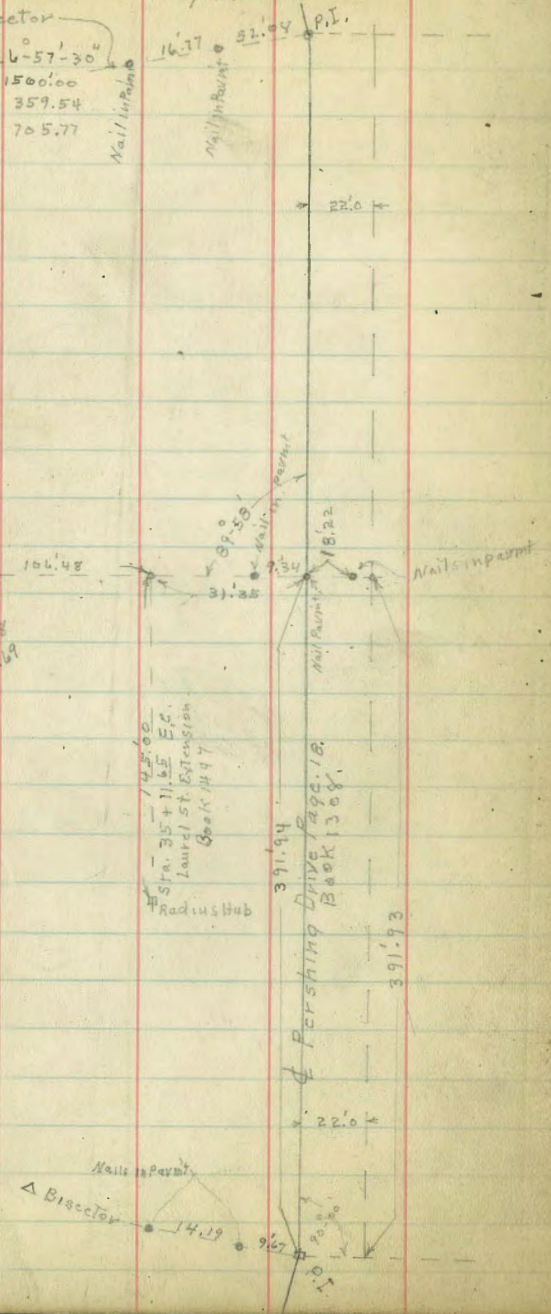
10-12-32
Mills
Walker
Bliss

Intersection Laurel St Extension
With Pershing Drive.

Δ Bisector
Δ = 26° 57' 30"
R = 1500.00
T = 359.54
L = 705.77

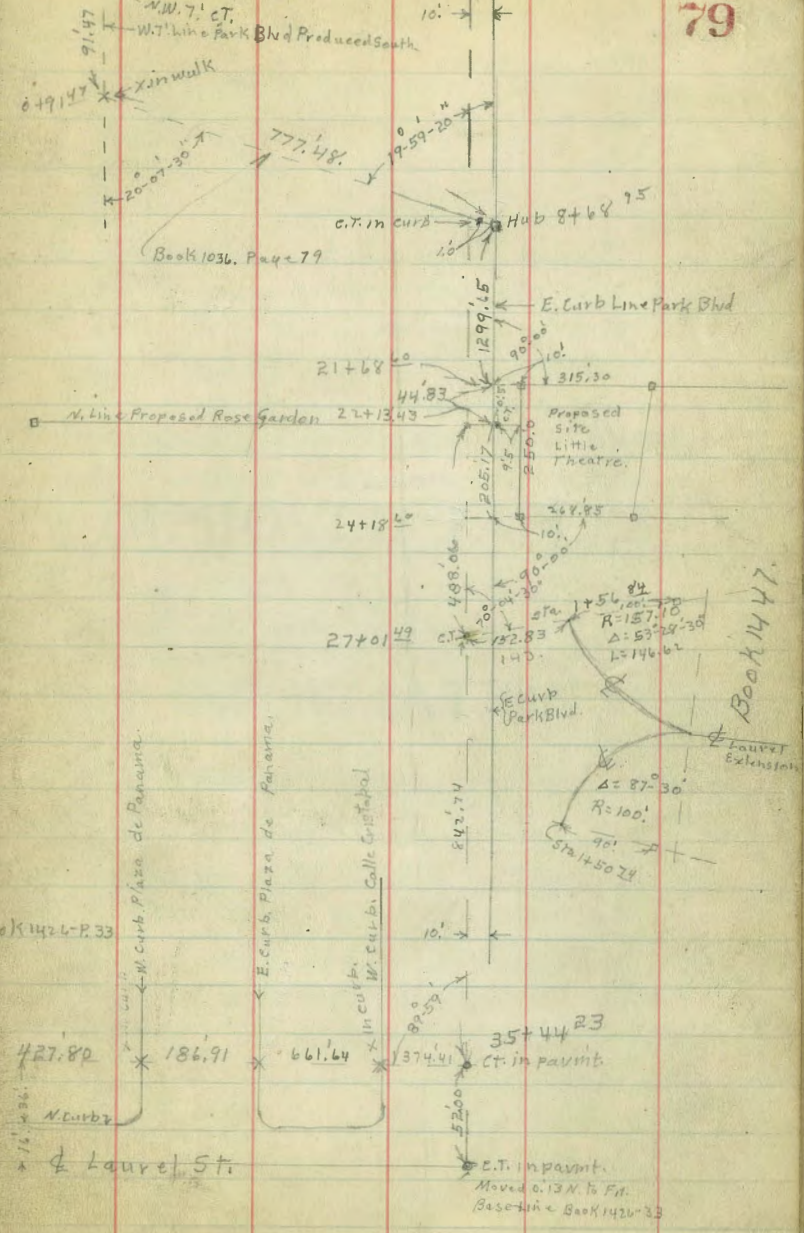
Δ = 72° 35' 30"
R = 145.00
T = 106.48
L = 193.69

Δ = 31° 40'
R = 1000.00
T = 283.60
L = 552.69



Intersection Laurel St Extension
With Park Blvd.

79



DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body

of table in same row and column gives distance from side stake to slope stake. If ground is not

level, the distance from side stake to slope stake is the same as that given in table, but the slope stake and slope stake lower table by this amount if cut, elevate if fill. Add this amount

to cut or fill and find distance in table. Set up rod at this point and line of sight should cut target.

target. necessary.

necessary.

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given T may be found by dividing tangent (or external), opposite T by given tangent (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

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DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

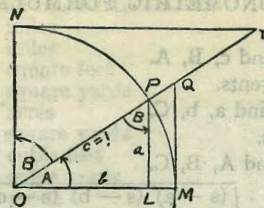


TABLE II
TRIGONOMETRIC FORMULÆ.

$$\angle A = \angle MOP \quad \angle B = \angle PON = \angle OPL$$

$$R = OB = c = 1$$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

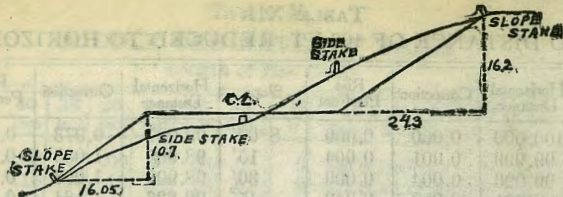
$$\sin \frac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \quad \cos \frac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \quad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Sines} \quad \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{C}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$$



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/4 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

182 B NE 68.07

2 C NE 56.87

Alabama Cypress N.W 244.98

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 CITY OF CALIFORNIA
 SAN DIEGO

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