

1309

PAINT

LETTER BOOK

No. 389 F

1309

ENGINEERING DEPARTMENT,
CITY OF SAN DIEGO,
CALIFORNIA.

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No. 1309 78 c/w/1309 H.H.

1309

Culvert levels	Lot 6 Blk 13	hablattermasa	2
X Sec.	KUFTZ	wright to Witherby	5
" "	JUNIPER	fulton to Gregory	15
" "	Gregory	Juniper to Ivy	20
" "	Robinson	Alabama to Florida	24
" "	Alley Blk 68	City Hts	33
" "	81	" "	35
" "	95	" "	38
" "	109	" "	41
" "	124	" "	44
" "	Mission Blvd	gequit Ct. to Pacific Ave	48
" "	Alexia Place	Mt View Blvd. to Copley	68

75' wide
12' ch
1278' 1/4

Kurtz St. X Sec
Wright to Wilherby

3 1/2 - 29
mills

sw.
Moore &
Wilherby

B.M.	2.84	30.57	27.73	
T.P.	1.37	20.09	11.85	18.72
T.P.		10.00	10.01	

Wright & Kurtz

S. line Wright St
80' wide
14' ch
13' 1/4

w

Page 5.

1

1-11-28
 J.C. Bliss
 Drebert
 Rouner

Culvert Levels along Line
 Parallel + 10' North of Northerly Line
 of Lot 6 - Block 13 of La Jolla Hermosa.

B.M. N.W. Top Lawn Sprinkler Camino de
 La Costa + La Jolla Blvd

+1.00

72.02

La Jolla Blvd.

H.I. 73.02

Sta

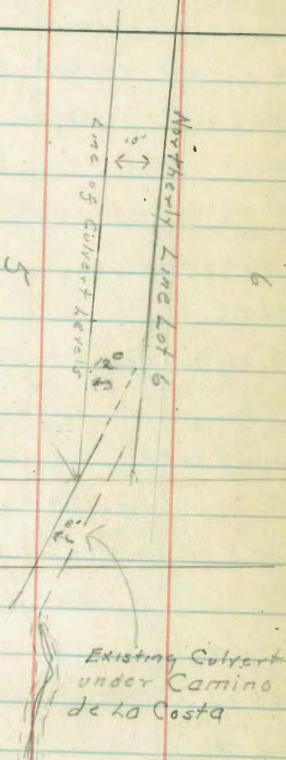
0+00 = West ab line La Jolla Blvd - Gutter	164	71.4	
	Tree	121	71.8
0+05 = Edge walk	111	71.9	
0+14 = Opposite mouth existing culvert under La Jolla Blvd	6.1	66.9	
Flowline existing culvert under La Jolla Blvd - 3' North of 0+14 stat	8.52	64.5	
0+18	7.2	65.8	
0+30 = W.L. La Jolla Blvd	9.3	63.7	
0+40	11.3	61.7	
0+50	10.7	62.3	
0+62	12.4	60.6	
0+72	12.8	60.2	
0+72	11.7	61.3	
1+00	10.9	62.1	
1+25	13.3	59.7	
T.P.	-12.60	60.42	
1+43	5.5	54.9	

+0.00

π 60.42

2

Camino de La Costa



Existing Culvert
under Camino
de La Costa

H. 1 60.42

3

1+52 = E. Camino de la Costa and angle Point

see sketch p. 2.

30 57.4

0+00

168 43.6

0+37 = Angle in drain

21.7 38.7

0+80

28.7 31.7

Culvert Levels along a line
parallel to 48' North of existing culvert
under Camino de la Costa

0+00 = 8' North of east end existing
culvert

58 54.6

East Flowline existing culvert

885 51.6

0+05

59 54.5

0+12.5 = Angle = 1+52 on other line

30 57.4

+15

23 58.1

0+26 = East c.b. Camino de la Costa

27.2 57.7

Gutter

306 57.3

0+55 = West c.b. Camino de la Costa

378 56.6

7p c.b.

340 57.0

0+67

39 56.5

0+75

87 51.7

0+80

97 50.7

West Flowline existing culvert

1530 45.1

Natural
Levels down drain as indicated

in sketch

Bottom of ditch under West Flowline of
existing culvert = 0+00

Kurtz 75' wide
12' ch
12.75 11.5

KURTZ ST X see
Wright to Witherby

3-12-29
Miller

Kurtz St

B.M.	2.84	30.57	27.73	
T.P.	1.37	20.09	11.85	18.82
T.P.	3.94	13.95	10.08	10.01
W			3.7	10.3
X 8			3.9	10.1
ch			4.8	9.2
1/4			3.8	10.2
c			3.3	10.7
1/4			2.7	11.3
ch			2.3	11.7
E			1.6	12.4
E			0.7	13.3
ch			1.6	12.4
1/4			2.7	11.3
c			2.8	11.2
1/4			3.7	10.3
ch			4.3	9.7
W			4.2	9.8
W			4.6	9.4
ch			4.0	10.0
1/4			3.3	10.7
c			2.0	12.0
1/4			1.3	12.7

Plotted 3-14-29

S. Line Wright { 80' wide
1.4 ch
13 1/4

T.L.

S. ch.

S. 1/4

S.W. Moore
& Witherby

Nail Pole S.W. Kurtz
& Wright

13.95

ch
E
E
ch
1/4
c
1/4
ch
W
W
ch
1/4
c
1/4
ch
E
E
ch
1/4
c
1/4
ch
W

Wright St.

N. 1/4

N. ch

0.9	13.2
0.6	13.4
0.7	13.3
1.6	12.4
1.3	12.7
1.5	12.5
3.0	11.0
3.7	10.3
4.1	9.9
5.3	8.7
4.6	9.4
3.5	10.5
2.0	12.0
2.1	11.9
1.6	12.4
1.3	12.7
2.3	11.7
2.7	11.3
2.7	11.3
2.5	11.5
3.9	10.1
4.8	9.2
5.1	8.9

5

13.95

00 = N. Line Wright St.

W	4.8	9.2
cl	4.5	9.5
"4	4.2	9.8
c	3.5	10.5
"4	3.5	10.5
cl	3.8	10.2
E	3.2	10.8

25' N

E	4.3	9.7
H0	4.7	9.3
cl	5.4	8.6
"4	5.1	8.9
c	4.7	9.3
"4	4.8	9.2
+5	5.1	8.9
cl	4.8	9.2
W.	5.3	8.7

65' N.

W	6.4	7.6
cl	6.2	7.8
"4	6.2	7.9
E	6.0	8.0
"4	6.2	7.8
+6	6.5	7.5
cl	6.0	8.0
c	5.6	8.4

Kurtz St.

13.95

100' N.

6

E.	6.7	7.3
cl	6.9	7.1
+6	7.2	6.8
"4	6.9	7.1
c	6.7	7.3
"4	7.3	6.7
cl	7.3	6.7
W	7.6	6.4

150' N.

W	8.5	5.5
cl	8.6	5.4
"4	8.7	5.3
c	9.2	4.8
"4	8.1	5.9
+6	8.8	5.2
cl	8.2	5.8
E	7.7	6.3

195' N = Door to Warehouse on W. line

W.	9.6	4.4	floor
E	9.5	4.5	
cl	9.7	4.3	
+4	9.3	4.7	
+6	9.9	4.1	
"4	9.5	4.5	
c	9.5	4.5	

200' N

13.95

200' N. (Coh)

1/4 10.0 4.0

ch 10.0 4.0

W 10.0 4.0

250' N

W 10.8 3.2

ch 11.0 3.0

+L 10.5 3.5

1/4 11.0 2.5

e 10.4 3.6

1/4 10.5 3.5

ch 10.1 3.9

E. 10.7 3.3

299.5' N. = S. line Bandini { 80' wide
1/4' obs

E 11.1 2.9

ch 10.9 3.1

1/4 11.1 2.9

e 11.0 3.0

1/4 11.6 2.4

+5 11.2 2.8

ch 11.9 2.1

W 12.0 2.0

T.P. 4.78 7.40 11.33 2.62

S. ch

W 5.5 1.9

ch 5.5 1.9

+L 4.7 2.7

7.40

Kurtz 51

1/4 5.0 2.4

e 4.5 2.9

1/4 4.6 2.8

ch 4.4 3.0

e 4.0 3.4

5.14

e 3.1 4.3

ch 3.8 3.6

1/4 4.5 2.9

e 4.3 3.1

1/4 5.1 2.3

ch 5.0 2.4

W 5.4 2.0

S. Bandini

W 5.1 2.3

ch 4.9 2.5

1/4 4.9 2.5

e 3.9 3.5

1/4 4.3 3.1

ch 3.5 3.9

e 2.6 4.8

N. 1/4

e 2.4 5.0

ch 3.2 4.2

1/4 4.5 2.9

e 4.2 3.2

on N.H.

7.40
N. 1/4 Bandini (con)

1/4	4.8	2.6
cl	5.3	2.1
W	5.7	1.7
N. cl		
W	5.8	1.6
cl	5.7	1.7
1/4	5.1	2.3
E	4.6	2.8
1/4	4.8	2.6
+5	4.8	2.6
cl	3.8	3.6
E	1.5	5.9

00 = N. Line Bandini St

E	1.4	6.0
+10	4.8	2.6
cl	5.2	2.2
1/4	4.7	2.7
E	4.9	2.5
1/4	5.3	2.1
cl	5.8	1.6
+1	5.2	2.2
W.	5.2	2.2

20' N. = S. Line emt Drive into Ware House

W.	5.10	2.30	on Drive
+8	5.13	2.27	" "
cl	5.59	1.81	" "

7.40

Kurtz St

+2 = E. End emt. drive	5.59	1.81	8 on drive
1/4	5.2	2.2	
E	5.0	2.4	
1/4	4.7	2.7	
cl	3.9	3.5	
+6	2.6	4.8	
E	1.8	5.6	

29' N. = N. edge above emt. drive

E	1.5	5.9	
+3	2.8	4.6	
+10	4.3	3.1	
cl	4.3	3.1	
1/4	4.9	2.5	
E	5.1	2.3	
1/4	5.2	2.2	

+10.5 = E. End emt. drive	5.60	1.80	on emt. drive
cl.	5.60	1.80	" " "
+4	5.21	2.19	" " "
W.	5.11	2.29	" " "

60' N

W	5.6	1.8	
cl.	5.9	1.5	
1/4	5.4	2.0	
E	5.2	2.2	
1/4	5.2	2.2	
cl	4.6	2.8	
E.	3.4	4.0	

7.40

100' N.

E	2.9	4.5
cl	4.3	3.1
"4	5.1	2.3
c	5.2	2.2
"4	5.5	1.9
cl	5.6	1.8
W	5.5	1.9

150' N.

W	5.6	1.8
cl	5.8	1.6
"4	5.6	1.8
c	5.1	2.3
"4	4.8	2.6
cl	4.8	2.6
E	3.5	3.9

200' N.

E	3.3	4.1
cl	4.5	2.9
cl	4.9	2.5
"4	5.2	2.2
c	5.2	2.2
"4	5.4	2.0
cl	5.6	1.8
W	5.6	1.8

7.40

250' N.

KURTZ ST.

W	5.5	1.9	9
cl	5.4	2.0	
"4	5.5	1.9	
c	5.0	2.4	
"4	5.0	2.2	
cl	4.7	2.7	
c	2.6	4.8	

300' N. = s. line Conts. St. { 80' wide
14' deep
13' deep

E	3.6	3.8
cl	4.3	3.1
"4	4.7	2.7
c	4.7	2.7
"4	5.4	2.0
cl	5.4	2.0
W	5.4	2.0

5. cl.

W	5.3	2.1
cl	5.4	2.0
"4	5.2	2.2
c	4.6	2.8
"4	4.7	2.7
cl	4.1	3.3
E	3.2	4.2

7.40

S. 1/4 Couts

E	3.4	4.0
cl	4.0	3.4
1/4	4.7	2.7
C	4.5	2.9
1/4	5.1	2.3
cl	5.3	2.1
W	5.3	2.1
	φ	
W	5.4	2.0
cl	5.0	2.4
1/4	5.0	2.4
E	4.5	2.9
1/4	4.6	2.8
cl	4.2	3.2
E	3.7	3.7
	N. 1/4	
E	4.1	3.3
cl	4.2	3.2
1/4	4.6	2.8
C	4.5	2.9
1/4	5.0	2.4
cl	5.1	2.3
W	5.4	2.0
	N. cl	
W	5.5	1.9
cl	5.3	2.1

Book 1288-78
MH = 3.35
M.H.

7.40

Kurtz St.

10

1/4	5.0	2.4	
E	4.6	2.8	
1/4	4.6	2.8	
cl	4.3	3.1	
	+ 8.65 = center of 4.5' culv X 2.75' grate	4.33	2.07
E	4.5	2.9	
	oo = N. line Couts St.		
E	3.9	3.5	
cl	4.2	3.2	
1/4	4.6	2.8	
C	4.7	2.7	
1/4	5.0	2.4	
cl	5.0	2.9	
W	5.3	2.1	
	50' N.		
W	5.0	2.4	
cl	5.1	2.3	
1/4	5.1	2.3	
E	4.9	2.5	
1/4	4.7	2.7	
cl	4.2	3.2	
E	3.9	3.5	

Book 1288-78
Grate = 361Intake into
Culvert

7.40
100' N

E	3.5	3.9
cl	4.0	3.4
"4	4.4	3.0
c	4.5	2.9
"4	5.0	2.4
cl	5.2	2.2
W.	4.9	2.5

150' N.

W.	4.9	2.5
cl	4.9	2.5
"4	4.9	2.5
c	4.2	3.2
"4	4.4	3.0
cl	3.2	4.2
E	3.1	4.3

200' N.

E	2.3	5.1
cl	3.1	4.3
+5	4.1	3.3
"4	4.2	3.2
c	4.2	3.2
"4	4.5	2.9
+6	5.0	2.4
cl	4.6	2.8
W	5.0	2.4

Knutz 2 st.

7.40
230' N

W	4.6	2.8
cl	4.7	2.7
+5	5.0	2.4
"4	4.6	2.8
c	4.3	3.1
"4	4.2	3.2
+4	4.1	3.3
cl	2.8	4.6
E	1.8	5.6

260' N.

E.	2.9	4.5
cl	3.8	3.6
+7	4.5	2.9
"4	4.5	2.9
c	4.5	2.9
"4	4.8	2.6
+7	4.9	2.5
cl	4.8	2.6
W	4.9	2.5

T.P. 4.15 8.02 3.53 3.87 Nail. Pole

290' N.

W	5.5	2.5
cl	5.2	2.8
"4	5.4	2.6
c	4.8	3.2

11

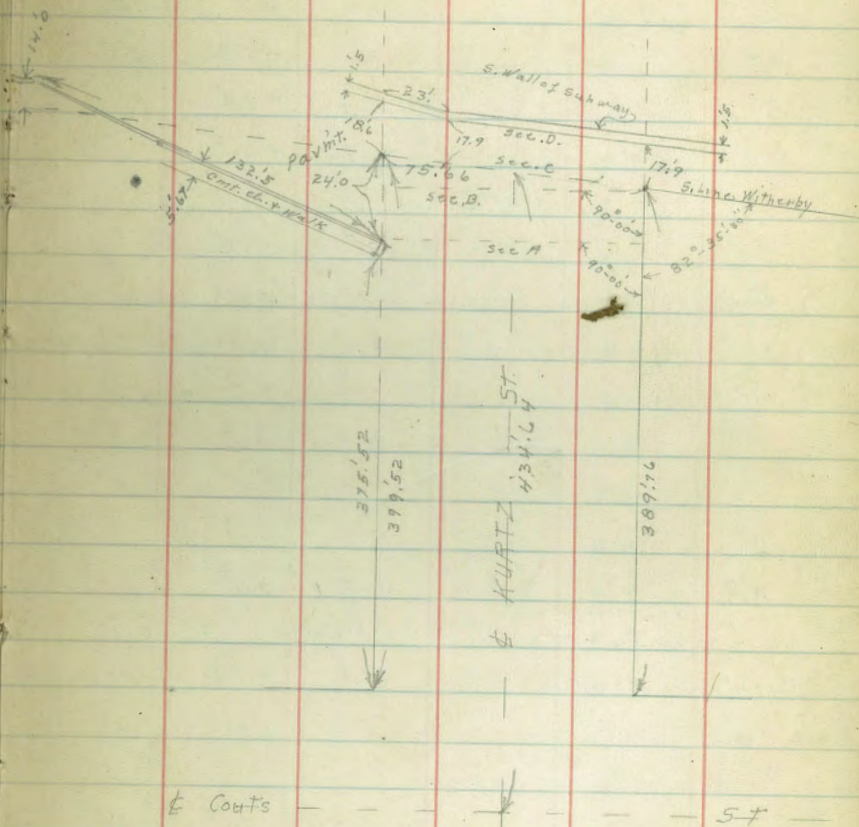
8.02

290' N. (con)

Kurtz St

12

14		4.7	3.3	
cl		3.4	3.6	
E		4.0	4.0	
+2		7.1	0.9	
+10		7.4	0.6	
	298' N. Inlet (N. End), Cmt. Box. Culvert opening			6' wide R. High
-10		7.0	1.0	
-3		7.0	1.0	
E		9.8	-1.8	ground
+0.7 = E. edge culvert		9.3	-1.3	Flow Line
" " " "		6.6	+1.4	Top cmt. Box
+6.7 = W. edge culvert		6.6	+1.4	Top cmt. Box
" " " "		9.3	-1.3	Flow Line
+7		9.4	-1.4	ground
cl.		3.5	+4.5	
+10		3.5	4.5	
14		4.7	3.3	
C		4.8	3.2	
14		5.3	2.7	
cl		5.2	2.8	
W		5.5	2.5	
	307' N.			
W.		5.5	2.5	
cl		5.2	2.8	
14		5.2	2.8	
C		4.7	3.3	



8.02 307' N. (con)			8.02 360' N			
E. 34	4.6	3.4	-10	5.2	2.8	
+3	3.5	4.5	E	4.9	3.1	
cl	4.0	4.0	cl	4.1	3.9	
+5	9.4	-1.4	"4	3.9	4.1	
E	9.4	-1.4	C	4.2	3.8	
+10	7.7	+0.3	"4	4.8	3.2	
316' N.			cl	5.1	2.9	
E	2.5	5.5	W	5.3	2.7	
cl	2.7	5.3	Sec A = 375.52 N = E. ent. ent. cl. on W. sec at 90° 00'			
+10	3.6	4.4	W on E. End ent. cl	5.23	2.79	
"4	4.4	3.6	gutter on E. Edge parmt.	5.96	2.06	
C	4.7	3.3	cl	5.0	3.0	
"4	5.2	2.8	"4	4.4	3.6	
cl	5.3	2.7	E	4.0	4.0	
W.	5.5	2.5	"4	3.9	4.1	
321.7 N on E. line } 316.5 N " W " } Old Vitrified Pipe Culvert 2'-6" diam.			cl	4.0	4.0	
6.5 W. of W. Line = W. End Pipe	9.6	-1.6	Flow Line	E	3.7	4.3
6.2 E " E " = E " "			" "	Sec B = 389.76 N. = S. Line Wetherby Stone. sec at 90° 00'		
350' N			E	2.7	5.3	
W	5.3	2.7	cl	3.0	5.0	
cl	5.4	2.6	"4	3.6	4.4	
"4	5.1	2.9	C	3.6	4.4	
C	4.5	3.5	"4	3.8	4.2	
"4	4.2	3.8	cl	4.6	3.4	
cl	2.9	5.1	W = E. Edge parmt.	5.60	2.42	
E	3.0	5.0				

8.02

Sec C. { 389.76 N. on E } = S. Line Wetherby St. 75.66
 { 399.52 N. on W }

W = E. Edge parmt

5.55 2.47

ch 4.6 3.4

1/4 3.8 4.2

E 3.7 4.3

1/4

ch

E

7. N. o

E

ch

1/4

E

1/4

ch

W = E. edge parmt

Sec. D = s.s.

W = E. edge par

W. Top Wall

ch " " "

1/4 " " "

E " " "

1/4 " " "

ch " " "

E " " "

chk on BM. Top Hwelt

3.71

4.31

Wetherby
W. Alliance

Kurtz St.

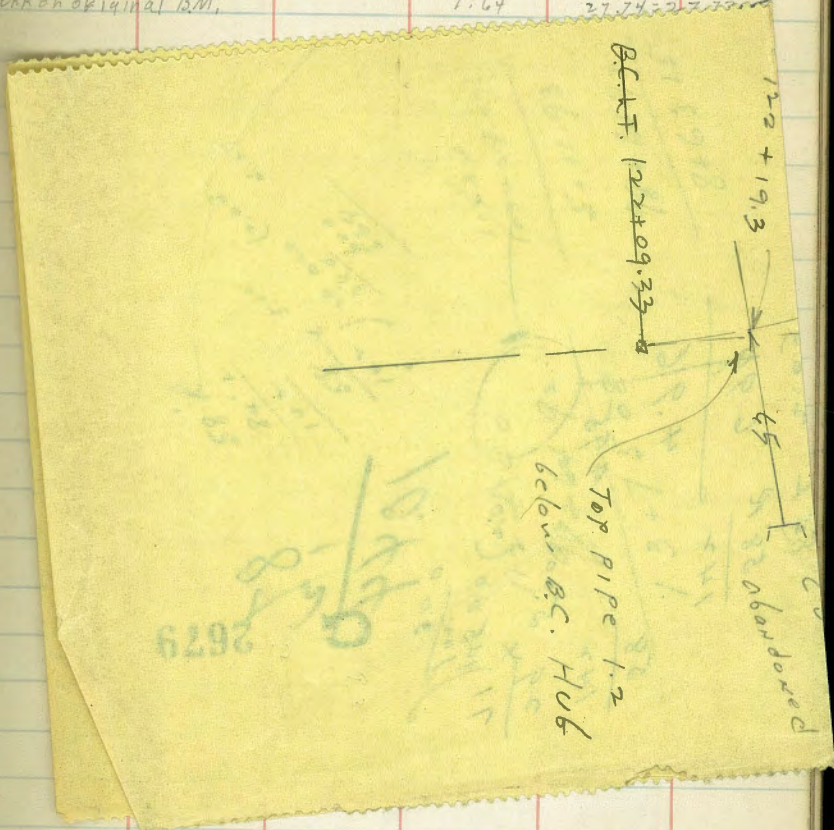
8.02

14

T.P. 11.73 16.65 3.10 4.92

T.P. 13.00 29.38 0.27 16.38

chk on original BM, 1.64 27.74 = 27.74



2679

U

$$\begin{array}{r} 58 \\ 848 \\ \hline 142 \\ 142 \\ \hline 284 \\ \times 500 \\ \hline 142000 \\ 284000 \\ \hline 426000 \end{array}$$

$$\begin{array}{r} 112 + 40 \\ \hline 152 \\ 98 + 64.92 \\ \hline 162.92 \\ 13 + 7508 \\ \hline 7638 \end{array}$$

$$\begin{array}{r} 112 + 28.07 \\ \hline 140.07 \\ 5 + 11.93 \\ \hline 16.93 \\ 98 + 64.92 \\ \hline 162.92 \\ 8 + 63.15 \\ \hline 71.15 \end{array}$$

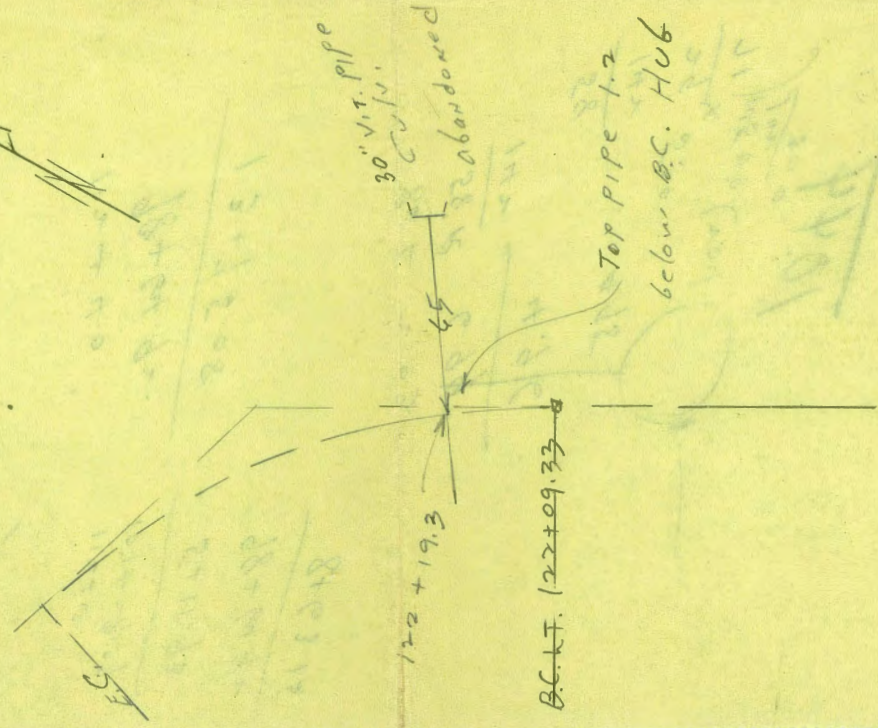
$$\begin{array}{r} 842 \quad 2.03 \\ 58R \quad 694 \\ \hline 142 \quad 4.96 \end{array}$$

$$\begin{array}{r} 58 \\ 142 \\ \hline 26 \\ 26 \\ \hline 52 \\ \times 11 \\ \hline 26 \\ 52 \\ \hline 284 \end{array}$$

$$\begin{array}{r} 10.44 \\ \hline 87 \end{array}$$

5029

G



30" V.I.T. PIPE
CULV.

abandoned

122 + 19.3

B.C.T.F. 122+09.33

Top pipe 1.2

below B.C. HUB

$\frac{1.2}{1.2} = 1.0$
 $\frac{1.2}{1.2} = 1.0$
 $\frac{1.2}{1.2} = 1.0$

8.02

Sec. C. { 389.76 N. on E } = S. Line Wetherby St. 75.66
 { 399.52 N. on W }

W = E. edge parmit

5.55 2.47

cl

4.6 3.4

1/4

3.8 4.2

E

3.7 4.3

1/4

3.5 4.5

cl

3.1 4.9

E

2.7 5.3

T.N. of S. Line Wetherby on diagonal

E

2.9 5.1

cl

3.3 4.7

1/4

3.6 4.4

E

3.8 4.2

1/4

4.1 3.9

cl

4.8 3.2

W = E. edge parmit

5.58 2.44

Sec. D = S. side Wall. of Under King

W = E. edge parmit

5.68 2.34

W. Top Wall

5.55 2.47

cl " " + dirt

5.50 2.52

1/4 " " " "

5.53 2.49

E " " " "

5.52 2.50

1/4 " " " "

5.53 2.49

cl " " " "

5.54 2.48

E " " " "

5.50 2.52

chk on BM. Top Hyd T

3.71 4.31

SW. Wetherby
+ W. Atlantic

Kurtz St.

14

T.P. 11.73 16.65 3.10 4.92

T.P. 13.00 29.38 0.27 16.38

chk on original BM, 1.64 27.74 = 27.73 ✓

255.61

46'E

33.6 N of S.L. = S. emb. ed.	12.17	243.44
" " " " gutter parvt.	12.82	242.79
29' " " " "	11.7	243.9
27' " " " "	5.5	250.1
20' " " " "	6.5	249.1
7.33 " " " " N. edge walk	6.70	248.90
S.L. etc. garage. emb. floor	6.35	249.26
74' E. = A an N. + 2i. edges of walk		
S.L.	8.8	246.8
+ 7.33 = N. edge walk	9.06	246.55
21' N. of S.L.	8.7	246.9
24' N	16.8	238.8
T.P. 0.33 244.68	11.26	244.35
29.7 N. of S.L. = S. emb. ed.	6.01	238.67
" " " " gutter parvt.	6.65	238.03
92' E. = E. End emb. wall: W. end 2' emb. walk		
26.1 N. of S.L. gutter parvt.	9.80	234.88
" " " " "	9.14	235.54
21' N. of S.L.	8.7	236.0
18' " " " "	0.0	244.7
7' " " " "	40.4	245.1
8' " " " " N. edge 2' emb. walk	0.00	244.7
S.L.	0.0	244.7

244.68

123.5

Juniper

16

14.5 of S.L.	0.0	244.7
10' " " " " dirt.	3.0	241.7
8' " " " " = N. edge 2' walk	3.31	241.37
S.L.	4.7	240.0
10' N. S.L.	4.2	240.5
12' " " " "	14.0	230.7
19.3 " " " " = N. emb. ed.	14.46	230.22
" " " " parvt.	15.21	229.47
140' E.		
16.8 N. of S.L. parvt.	18.30	226.38
" " " " S. emb. ed.	17.54	227.14
8' " " " "	16.6	228.1
8' " " " "	7.2	237.5
S.L.	5.3	239.4
7.5 of S.L.	6.7	238.0
13' " " " " = N. edge 2' walk	5.34	239.34
16' " " " "	5.1	239.6
19' " " " "	2.6	242.1
160' E.		
23.5 of S.L.	5.3	239.4
21' " " " "	7.4	237.3
17' " " " " = N. edge 2' walk	7.53	237.15
13' " " " "	9.0	235.7
5' " " " "	7.4	237.3
S.L.	11.0	233.4

244.68

160' E. (con)

3' N. of S.L.	14.2	230.5
5' " " " "	20.5	224.7
13' " " " " = s. cnt. ch	21.04	223.64
" " " " " " parnt.	21.55	223.13
180' E		
10.6 N. of S.L. = parnt.	25.34	219.34
" " " " " " = s. cnt. ch	24.56	220.12
S.L.	23.1	221.6
1' S. of S.L.	17.2	227.5
8' " " " "	9.6	235.1
16' " " " "	11.4	233.3
25.3 " " " " = N. edge 2' walk	9.85	234.83
28' " " " "	9.6	235.1
30' " " " "	7.2	237.5

200' E = W. Line Gregory St

34' S. of S.L. = Sec. A, Plat Page 15	12.2	232.5
31.2 S. of S.L. = N. edge 2' walk	12.21	232.47
30' " " " "	13.0	231.7
21' " " " "	13.5	231.2
16' " " " "	11.9	232.8
3' " " " "	15.5	229.2
T.P. 0.12 232.16	12.64	232.04
2' S. of S.L.	12.3	219.9
S.L.	13.6	218.6
4' N. of S.L.	15.2	217.0

232.16

Juniper St.

17

9' N. of S.L. = s. cnt. ch	15.53	216.63
" " " " gutter Parnt.	16.29	215.87
10' E. of W. Line		
8.4 N. of S.L. parnt.	17.92	214.24
" " " " " s. cnt. ch	17.17	214.99
S.L.	15.9	216.3
1' S. of S.L.	6.1	226.1
11' " " " "	0.7	231.5
16' " " " "	0.9	231.3
20' " " " "	2.8	229.4
22' " " " "	1.5	230.7
34' " " " " = Sec. A.	1.5	230.7
W. ch. Gregory		
34' S. of S.L. = Sec. A.	3.0	229.2
32' " " " "	1.7	230.5
24' " " " "	1.9	230.3
20' " " " "	4.6	227.6
16' " " " "	1.8	230.4
11' " " " "	2.4	229.8
3' " " " "	7.8	224.4
S.L.	17.8	214.4
8' N. of S.L. = s. cnt. ch	18.74	213.42
" " " " " parnt.	19.56	212.60

232.16
N. 1/4

7.7 N. of S.L. = S. gutter	21.03	211.13
" " " " = S. ent. ch.	20.40	211.76
S.L.	18.9	213.3
2.5. of S.L.	10.5	221.7
12. " " " "	4.2	228.0
17. " " " "	4.5	227.7
19. " " " "	2.1	226.1
23. " " " "	6.2	226.0
25. " " " "	3.3	228.9
34. " " " " = Sec. A.	2.3	229.9
E Gregory		
34.5. of S.L. = Sec. A.	5.8	226.4
22. " " " "	6.8	225.4
19. " " " "	9.4	222.8
15. " " " "	6.3	225.9
11. " " " "	6.5	225.7
1. " " " "	13.1	219.1
S.L.	18.6	213.6
2. N. of S.L.	20.8	211.4
7.7 " " " " = S. ent. ch.	21.65	210.51
" " " " " parvt.	22.35	209.81
E. by		
7.7 N. of S.L. = gutter parvt	23.61	208.55
" " " " " = S. ent. ch.	22.93	209.23
2. " " " "	22.3	209.9
S.L.	20.5	211.7

232.16

Juniper St

18

1. S. of S.L.	15.0	217.2	
10.5 " " "	9.0	223.2	
14. " " " "	9.1	223.1	
18. " " " "	12.7	219.5	
21. " " " "	9.6	222.6	
34. " " " " = Sec. A.	10.0	222.2	
T.P. 0.08	219.09	13.15	219.01
E. ch.			
34.5. of S.L. = Sec. A.	+1.5	220.6	
19. " " " "	+0.5	219.6	
17. " " " "	2.0	217.1	
15. " " " "	+0.2	219.3	
8. " " " "	+1.0	220.1	
1. " " " "	3.4	215.7	
S.L.	7.6	211.5	
2. N. of S.L.	8.4	210.7	
3. " " " "	10.5	208.6	
8.1 " " " " = S. ent. ch.	10.83	208.26	
" " " " " parvt	11.55	207.54	
10. E. of E. ch.			
8.5 N. of S.L. = gutter parvt.	17.39	206.70	
" " " " " S. ent. ch.	11.70	207.39	
4. " " " "	11.4	207.7	
2. " " " "	9.7	209.4	
S.L.	9.1	210.0	

219.09

10' E. of E. cl (con)

1' S. of S.L	8.5	210.6
2' " " " "	4.9	214.2
6' " " " "	3.1	216.0
12' " " " "	3.2	215.9
14' " " " "	4.1	215.0
16' " " " "	2.8	216.3
34' " " " " = sec. A.	10.1	219.0

E. Line Gregory

34' S. of S. L. = sec. A.	4.3	214.8
16' " " " "	5.5	213.6
3' " " " "	6.6	212.5
" " " " S.L.	10.9	208.2
3' N. of " " "	11.1	208.0
5' " " " "	12.2	206.9
9.1' " " " " = s. cnt. cl	12.45	206.64
" " " " " parmt.	13.08	206.01

25' E. of E. Line Gregory

11.5' N. of S.L. = parmt.	13.96	205.13
" " " " " = s. cnt. cl	13.26	205.83
" " " " " S.L.	12.3	206.8
13' S. of " " "	9.6	211.502 209.5
34' " " " " = Sec. A.	9.6	209.5

219.09

Juniper St.

50' E. of E. Line Gregory St.

19

34' S. of S.L. = sec. A	15.4	203.7
15' " " " "	14.8	204.3
" " " " S.L.	14.4	204.7
14.9' N. of S.L. = s. cnt. cl	13.62	205.47
" " " " " gutter parmt	14.46	204.63
T.P. 13.08 232.09	0.08	219.01

80' wide
20' elev
10' high

Gregory St. X Sec. Juniper to Ivy

3-18-24
miller

232.09 Page 19,
opp. S. line Juniper

232.09

20

34's. of S. line Juniper = Sec. H.

1							
2	E-50	28.4	203.7	+25			
6	E-25	22.6	209.5		45.5		
12	E. line	17.3	214.8	-25			
14	+10	13.1	219.0	E			
1	cb	11.5	220.6	+7			
3	"4	9.8	222.3	cb			
5	4	5.7	226.4	"4			
34	"4	2.2	229.9	E			
1	elc	2.9	229.2	+5			
3	+10	7.4	230.7	"4			
5	+12.4 = E. edge emb. walk	0.10	231.99	+1			
3	W. line	+0.4	232.5	+5			
5				+6			
9	W	0.0	232.1	cb			
1	+7.9 = S. edge emb. walk	0.36	231.73	+12.1 = E. edge emb. walk			
1	cb	2.0	230.1	W			
1	+2	4.2	227.9		50.5		
1	+5	4.4	227.7	W			
1	+7	2.2	229.9	+7.9 = E. edge walk			
1	"4	2.3	229.8	cb			
1	+3	2.3	229.8	+6			
1	C	4.6	227.5	+7			
1	"4	9.0	223.1	"4			
1	cb	11.0	221.1	+1			
1	+13	13.3	218.8	C			

Plotted

	E				16.6	215.5	
	+25				22.6	209.5	
	-25				23.0	209.1	
	E				16.0	216.1	
	+7				12.6	219.5	
	cb				11.0	221.1	
	"4				9.0	223.1	
	E				5.7	226.4	
	+5				3.3	228.8	
	"4				2.7	229.4	
	+1				5.2	226.9	
	+5				4.6	227.5	
	+6				2.4	229.7	
	cb				2.2	229.9	
	+12.1 = E. edge emb. walk				0.64	231.45	
	W				0.0	232.1	
	W				+0.2	232.3	
	+7.9 = E. edge walk				0.82	231.27	
	cb				2.6	229.5	
	+6				2.6	229.5	
	+7				5.6	226.5	
	"4				5.6	226.5	
	+1				2.9	229.2	
	C				5.8	226.3	

232.09

50's. (con)

E. 1/4	11.0	221.1
eb	12.8	219.3
E	18.0	214.1
+25.	23.8	208.3

54's. 1/2 S. line Juniper

-25	22.6	209.5
E	15.6	216.5
+7	12.6	219.5
eb	10.8	221.3
1/4	8.7	223.4
+5	9.3	222.8
E	8.1	224.0
+8	5.8	226.3
1/4	2.7	229.4
eb	2.6	229.5
+12.1 = E. edge walk	0.96	231.13
W	+0.3	232.4

58's.

W	+0.3	232.4
+7.9 = E. edge walk	1.14	230.95
eb	2.8	229.3
1/4	2.7	229.4
+3	2.9	229.2
E	5.4	226.7
1/4	8.5	223.6
eb	10.5	221.6

232.09

Gregory St

21

+13	12.3	219.8
E	15.6	216.5
+25	22.6	209.5

100's.

-25	28.1	204.0
E	17.3	213.8
+6	12.9	219.2
eb	10.7	221.4
1/4	8.4	223.7
E	5.7	226.4
+6	4.3	227.8
1/4	4.3	227.8
eb	4.5	227.6
+3	4.5	227.6
+5	3.5	228.6
+12.1 = E. edge walk	2.88	229.21
W	1.7	230.4

150's.

W	3.8	228.3
+7.9 = E. edge walk	5.20	226.90
+13	6.1	226.0
+17	7.1	225.0
eb	7.2	224.9
1/4	6.3	225.8
+4	6.3	225.8
E	8.6	223.5

232.09

150' S. Con

E. 14	11.1	221.0
el.	13.5	218.6
+12	15.3	216.8
E.	20.2	211.9
+25	32.5	199.6
	200' S. 31.2	
-26	31.2	200.9
E.	21.3	210.8
+8	17.1	215.0
el.	15.2	216.9
14	13.3	218.8
C	11.8	220.3
+8	8.9	223.2
14	8.9	223.2
el.	9.4	222.7
+4	9.6	222.5
+6	8.0	224.1
+12.1 = E. edge walk	7.55	224.54
N	6.6	225.5
	225' S.	
N	6.9	225.2
+3	8.5	223.6
+7.8 = E. edge walk	8.54	223.55
+14	9.1	223.0
+16	10.4	221.7
el.	10.6	221.5

232.09

Gregory St

22

14	10.1	222.0
+2	10.0	222.1
C	12.8	219.3
14	14.9	217.2
el.	16.9	215.2
+13	18.1	214.0
E.	21.4	210.7
+25	31.2	200.9
	225' S.	
-25	33.3	198.8
C	23.9	208.2
+8	18.8	213.3
el.	17.4	214.7
14	16.3	215.8
C	14.8	217.3
+8	11.2	220.9
14	11.2	220.9
el.	11.6	220.5
+4	11.6	220.5
+6	10.2	221.9
+12.2 = S. edge cont. walk	9.57	222.52
+17	9.5	222.6
N	8.5	223.6

300' S. = N Line = IVY ST.
232.09
What. Section

Gregory St.

23

W.			11.0	221.1
+7.8 = E. edge walk			11.53	220.56
+13			12.0	220.1
+15			13.3	218.8
cb			13.5	218.6
14			13.2	218.9
C			17.2	214.9
14			19.5	212.6
cb			20.4	211.7
+6			21.0	211.1
E			30.7	201.4
+15			38.0	194.1
T.P.	13.05	245.09	0.05	232.04
T.P.	11.49	255.84	0.74	244.25
chk on original B.M.			0.36	255.48

80' wide
14' elev
13' 1/4

Robinson Ave X sec
Alabama to Florida

4-26-29
Miller

261.76

24

BM.	3.75	261.76	258.01				
		00 = W. line Alabama		cl		4.4	257.2
				s		5.2	256.6
N. on emt. walk Return	3.47		258.29		25' W		
N. emf. cl	3.73		258.03	s		6.1	255.7
gutter part	4.34		257.38	cl		4.3	257.5
"y "	4.17		257.59	"y		3.7	258.1
c "	4.18		257.58	c		4.0	257.8
"y "	4.47		257.29	"y		4.3	257.5
gutter "	4.74		256.98	cl		4.4	257.4
S. emf. cl	4.25		257.51	N		4.2	257.6
S. on emt. Walk Return	4.06		257.70		40' W		
		2' W		N-S Wall House		7.3	252.5
s	3.3		258.5	N		7.1	252.7
+12	2.8		259.0	cl		6.4	255.4
cl	4.3		257.5	"y		5.4	256.4
"y	4.1		257.7	c		5.1	256.7
c	4.0		257.8	"y		4.6	257.2
"y	3.9		257.9	cl		5.6	256.2
cl	3.7		258.1	s		7.2	254.6
N	3.6		258.2		46' W		
		15' W		-5		9.2	252.6
N	3.8		258.0	s		9.2	252.6
cl	4.0		257.8	cl		8.8	253.0
"y	3.9		257.9	"y		9.0	252.8
c	3.8		258.0	c		7.1	254.7
"y	3.7		258.1	"y		7.5	254.3

Plotted 3-29-29 EAB

261.76
46' W. (coh)

14+8	7.0	254.8
cl	7.7	254.1
N	10.9	250.9
+5	11.0	250.8

56' N.

-10	12.8	249.0
N	12.7	249.1
cl	10.4	251.4
+5	9.7	252.1
14	11.9	249.9
+4	12.5	249.3
c	9.3	252.5
+9	12.1	249.7
14	12.0	249.8
+3	13.0	248.8
cl	13.0	248.8
s	13.1	248.7
+10	12.6	249.2

T.P. 0.68 250.14 12.30 249.46

75' N.

-10	5.0	245.1
s	5.7	244.4
cl	6.1	244.0
14	6.4	243.7
+5	6.3	243.8
c	3.8	246.3

250.14

Robinson Ave

25

14	4.4	245.7
cl	4.9	245.2
N	6.2	243.9
+10	6.2	243.9

79.5 N.

-10	6.5	243.6
N	7.0	243.1
cl	6.7	243.4
14	7.5	242.6
+2 = g. W. End. outlet 48" emb. Culvert.	8.2	241.9 ^{Flowline}
+8	4.8	245.3
c	6.0	244.1
+10	7.5	242.6
14	7.4	242.7
cl	6.8	243.3
s	6.4	243.7
+10	6.4	243.7

100' N.

-15	12.1	238.0
s	12.7	237.4
cl	12.8	237.3
14	13.0	237.1
c	12.7	237.4
14	12.0	238.1
cl	12.0	238.1
N	11.7	238.4
+15	10.5	239.6

250.14

Robinson Ave

240.61

26

T.P. 3.02 240.61 12.55 237.59

110' W

-15 3.7 236.9

N 4.0 236.6

E 4.3 236.3

14 4.3 236.3

E 4.1 236.5

14 4.6 236.0

E 4.9 235.7

S 5.3 235.3

+15 5.3 235.3

122' W

-15 6.6 234.0

S 6.4 234.2

E 6.1 234.5

14 5.8 234.8

E 5.4 235.2

14 5.3 235.3

E 5.2 235.4

N 5.8 234.8

+20 8.7 231.9

130' W

-25 10.7 229.9 in wash

-15 10.8 229.8 " "

N 8.5 232.1

E 4.0 234.6

14

E

14

E

S

+15

-15

S

E

14

E

14

+9

E

+9

N

+14

+25

-25

-12

N

E

+7

+9

5.9 234.7

6.1 234.5

6.5 234.1

6.6 234.0

7.0 233.6

7.2 233.4

140' W

7.9 232.7

7.7 232.9

7.6 233.0

7.3 233.3

7.7 232.9

7.1 233.5

9.0 231.6

8.9 231.7

9.5 231.1

11.2 229.4 wash

10.9 229.7

8.3 232.3

153' W

7.5 233.1

7.9 232.7

10.7 229.9 wash

11.5 229.1 "

11.2 229.4 "

9.5 231.1

240.61

153' W. (cont)

N. 1/4	9.5	231.1
C	9.5	231.1
1/4	9.1	231.5
cb	8.7	231.9
S	9.2	231.4
+25	9.5	231.1

160' W.

-25	10.2	230.4
S	9.5	231.1
cb	9.0	231.6
1/4	9.5	231.1
C	9.7	230.9
+6	9.8	230.8
+8	11.8	228.8 Wash
1/4	11.8	228.8 "
cb	11.4	229.0 "
N.	8.0	232.6
+25	7.6	233.0

175' W.

-25	7.6	233.0
N	8.1	232.5
cb	8.3	232.3
+7	8.4	232.2
1/4	9.3	231.3
+11	11.3	229.3
+12	12.6	228.0 Wash

240.61

Robinson Ave

27

C	12.7	227.9 Wash
+10	12.5	228.1 "
1/4	11.0	229.6
cb	9.9	230.7
S	9.5	231.1
+25	10.3	230.3

187' W.

-25	10.6	230.0
S	9.9	230.7
+8	11.2	229.4
+10	13.1	227.5 Wash
cb	13.3	227.3 "
+12	13.0	227.6 "
1/4	11.0	229.6
C	9.0	231.6
1/4	8.4	232.2
cb	8.4	232.2
N	8.2	232.4
+25	7.5	233.1

192' W.

-25	6.9	233.7
N	8.2	232.4
cb	8.3	232.3
1/4	8.5	232.1
C	9.0	231.6
+8	8.9	231.7

240.61		192' W. (E. W.)	
1.4		10.2	230.4
+8		11.2	229.4
+10		13.2	227.4 wash
el		13.2	227.4 "
S		13.3	227.3 "
+1		11.7	228.9
+12		9.8	230.8
+25		10.6	230.0
	200' W.		
-25		11.1	229.5
-16		11.7	228.9
-14		13.2	227.4 wash
S		13.4	227.2 "
+5		11.3	229.3
el		9.2	231.4
"4		9.0	231.6
C		8.8	231.8
"4		8.5	232.1
el		8.4	232.2
N		8.1	232.5
+25		6.7	233.9
	206' W.		
-25		6.4	234.2
N		7.7	232.9
el		8.3	232.3
"4		8.6	232.0

240.61

Robinson Ave

28

8.6	232. Dnded cat.
8.8	231.8
9.1	231.5
9.6	231.0
13.7	226.9 wash
13.7	226.9 "
	215' W.
10.3	230.3
9.0	231.6
8.8	231.8
8.3	232.3
8.4	232.2
8.1	232.5
8.0	232.6
6.7	233.9
5.2	235.4
2.5	238.1
	225' W.
0.7	239.9
3.8	236.8
5.8	234.8
7.3	233.3
8.3	232.3
8.0	232.6
8.1	232.5
8.4	232.2
9.5	231.1

+25

See Page 77 for 2483

240.61
235.18

253.18

Robinson Ave

29

S-25 See Page 77 5.7 234.9
 S. for Sec 2737= 7.7 232.9
 cl. El. Alley 6.7 233.9
 1/4 6.9 233.7
 c 6.8 233.8
 +5 6.8 233.8
 1/4 7.3 236.3
 cl. 2.0 238.6

S 17.0 236.2
 cl 17.7 235.5
 1/4 16.6 236.6
 c 13.0 240.2
 1/4 3.4 249.8
 cl 2.9 250.3
 N 1.1 252.1
 +5 1.0 252.2

T.P. 12.98 253.18 0.41 240.20

260.18

N. 11.6 241.6
 +15 6.7 246.5

-5 +0.4 253.6
 N +0.3 253.5

247.18

-5 2.0 251.2
 N 2.2 251.0
 +8 6.1 247.1
 cl 7.7 247.5
 1/4 10.2 243.0
 c 14.7 238.5
 1/4 17.6 235.6

cl 0.0 253.2
 1/4 1.2 252.0
 +7 2.1 251.1
 c 5.8 247.4
 1/4 10.3 242.9
 cl 11.3 241.9
 +6 11.5 241.7

+6 Top M.H. No yardage

cl. 16.6 236.6
 S 18.4 234.8
 S 18.4 234.8
 +13 18.5 234.7
 +25 14.5 238.7

+7 14.8 238.4
 +11 14.8 238.4
 S 12.4 240.8
 +5 13.7 239.5
 +8 9.8 243.4

252.18

+20

-25 11.4 241.8
 -6 18.0 235.2

6.4 246.8

266.03

285' W. (cont)

N. 14	4.4	261.6
c	5.1	260.9
14	6.6	259.4
+4	7.4	258.6
T10	11.1	254.9
+11	9.7	256.3
cb	10.1	255.9
S	10.6	255.4
+5	10.9	255.1
295' W.		
-5	9.6	256.4
S	9.7	256.3
cb	8.7	257.3
+2	8.4	257.6
+3	9.3	256.7
+5	9.1	256.9
+10	5.7	260.3
14	5.2	260.8
c	5.0	261.0
14	4.3	261.7
cb	4.0	262.0
+11.6 ground	3.7	262.3
+12.1 Top cmt. wall	3.40	262.63
+12.2 cmt. porch	4.90	261.13
N " "	4.21	261.12
+2.2 " " Front. of house	4.47	261.16

266.03

296' W

Robinson Ave

31

N-22 Front. of house	3.4	262.6
N.	3.4	262.6
N. cb	4.0	262.0
305' W		
-2.2 Front House	2.2	263.8
N	2.3	263.7
cb	3.1	262.9
14	3.1	262.9
c	3.1	262.9
+10	5.4	260.6
+11	6.5	259.5
14	5.7	260.3
cb	6.2	259.8
S	7.3	258.7
+5	8.1	257.9
315' W		
S. on cmt. porch	4.1	261.9
^{False Reading} Below for yardage		
+1.5 ground.	5.0	261.0
cb	4.0	262.0
14	2.3	263.7
+3	1.0	265.0
c	1.0	265.0
14	1.1	264.9
cb	1.0	265.0
N	0.2	265.8
T.P.	12.27	278.05
	0.25	265.78

278.05

335' W.

N.	9.3	268.8
ch	9.6	268.5
"4	10.4	267.7
c	10.5	267.6
"4	10.8	267.3
ch	12.2	265.9
S	13.0	265.1

350' W.

S	11.3	266.8
ch	10.3	267.8
"4	9.4	268.7
c	9.1	269.0
"4	8.2	269.9
ch	7.6	270.5
N	7.3	270.8

365' N

N.	5.2	272.9
ch	5.9	272.2
"4	6.5	271.6
c	7.3	270.8
"4	7.8	270.3
ch	8.5	269.6
S	9.5	268.6

385' W

S	7.3	270.8
ch	6.4	271.7

278.05

Robinson Ave

32

"4	5.6	272.5
c	5.1	273.0
"4	4.3	273.8
ch	3.8	274.3
N	3.3	274.8

400' W.

N	2.3	275.8
ch	2.9	275.2
"4	3.3	274.8
c	4.0	274.1
"4	4.5	273.6
+4	5.6	272.5
ch	5.7	272.4
S	6.2	271.9
+5	6.8	271.3

407' W = E. line Florida

S	5.4	272.7
emb. ch	5.09	272.96
+1	5.5	272.6
"4	5.1	273.0
c	4.2	273.9
"4	3.8	274.3
+12	3.5	274.6
N. emb. ch	3.05	275.00
N.	2.7	275.4

chk on BM. N.W. Robinson & Florida

2.06 275.99 = 275.96

5-8-29

X-section Alleys in City Hts
from Nighthman to Redwood
between Central & 40th - 20' wide
Bk 68 City Hts

J. C. Bliss
Dorchester
Pavner

H.I. 347.46

33

B.M. N.W. B.P. Nighthman & 40th (Section) 343.09

+437

H.I. 347.06⁴⁶

S.L. Nighthman = 0.00

W Tp existing return 4.83 342.63

G 4.9

Φ 5.0 342.5

+5 4.9

G 4.8

E Tp existing return 4.61 342.85

+20

Sencey M.H. & as alley - Floodline 10.62 336.84 ✓

+25

E 6.3 341.2

+5 6.3

Φ 6.3 341.2

W 6.0 341.5

+50

W 7.5 340.0

Φ 7.9 339.6

+5 7.9

E 7.9 339.6

+75

E 8.8 338.7

+5 8.8

Φ 8.9 338.6

W 7.1 338.4

+90

Φ 16' Double Garage - 13' Back E.L. Dirt Floor 8.9 338.6 ↓

1400

9.5 338.0

Φ 9.4 338.1

+5 9.2

E 9.1 338.4

1425

E 10.7 336.8

+5 10.4

Φ 10.1 337.4

W 9.9 337.6

1450

W 9.5 338.0

+5 10.2

Φ 10.5 337.3

E 10.8 336.7

1475

E 10.6 336.9

+5 10.3

Φ 9.8 337.7

W 9.0 338.5

2400

W 8.7 338.8

Φ 9.4 338.1

+5 9.9

E 10.1 337.4

2425

E 9.4 338.1

+5 9.1

Φ 8.7 338.6

W 8.2 339.3

2450

Φ 13' & 18' Double Garage - Dirt Floor 8.3 339.2

Plotted 5-10-29
C.B.H.

H 1.342.00⁴⁶

W	8.6	338.9
♀	8.8	338.7
+5	9.0	
F	9.3	338.2
2+75		
E	8.5	339.0
+5	8.6	
♀	8.8	338.7
W	8.1	339.4
T.P		-884 33862

+0.27

H.I. 338.89

3+00

W	0.4	338.5
♀	0.5	338.4
+5	0.8	
E	1.4	337.5
3+25		
E	1.7	337.2
+5	1.2	337.7
♀	0.9	338.0
W	1.3	337.6

3+35

8' Garage 6' Back W.L. Concrete Floor 0.50 338.39

3+50

W	1.3	337.6
♀	1.9	337.0

H.I. 33889

34

15	1.9	
E	1.9	337.0
3+75		
E	2.9	336.0
+5	2.8	
♀	2.8	336.1
W	2.3	336.6

3+69

♀ 8' Garage 6' Back W.L. Concrete Floor 1.30

337.59 ✓

4+00

W	3.2	335.7
♀	3.8	335.1
+5	4.5	334.4
E	5.0	333.9

4+25

E	5.5	333.4
+5	5.2	333.7
♀	4.9	334.0
W	3.9	335.0

4+33

♀ North 8' Garage of Double Garage

W.L. 3' Back - Dirt Floor 4.3

334.6 ✓

4+42

♀ South 8' Garage of Double Garage

3' Back W.L. Concrete Floor 3.48

335.41 ✓

H.1. 338.89

4+50

W	5.0	333.9
♀	6.4	332.5
+5	6.7	
E	7.4	331.5
	4+75	
E	9.0	329.9
+5	8.5	
♀	8.3	330.6
W	7.7	331.2
	5A00	
W	9.8	329.1
♀	10.3	328.6
+5	11.0	
E	11.0	327.9
	5+75	
Back 1' 12' Garage Dirt Floor	12.7	326.2
E	12.7	326.2
+5	12.6	326.3
♀	12.4	326.5
W	11.6	327.3
	5+50	
W	12.9	326.0
♀	13.1	325.8
+5	13.6	325.3
E	14.1	324.8

H.1. 338.89

T.P.

	4+39	
	H.1 330.52	
	5+75	
E	5.7	324.8
+5	5.5	325.0
♀	4.9	325.6
W	4.9	325.6
	6+00 = N.L. Landis	
W	4.9	325.6
♀	4.6	325.9
+5	4.5	325.9
E	4.6	325.9
	Shot on East end of N.E. Return Landis	
	4404	005
		330.47 ✓
	Shot on West end of N.W. Return at Landis + Central	
		3.91
		326.61 ✓
	S.L. Landis = 0+00	
E	5.6	324.9
+5	5.4	325.1
♀	5.1	325.4
W	5.0	325.5
	0+25	
W	21.5	309.0
♀	22.7	307.8
+5	20.5	310.0

BIRTI City Hts

35

-12.76 326.13

H.I. 330.52

E		20.3	310.2
	0+45		
E		27.3	303.2
+5		28.8	301.7
E		30.1	300.4
W		30.9	299.6
	0+75		
W		24.0	306.5
E		16.4	314.1
+5		10.0	320.5
E		9.1	321.4
	1+00		
E		2.4	328.1
+5		2.6	327.9
E		3.1	327.4
+2		3.5	
+3		13.1	
W		17.1	313.4
	1+25		
Out 3		12.7	
Out 2		2.4	
W		1.8	328.7
E		0.9	329.6
+5		0.4	330.1
E		0.4	330.1

H.I. 330.52

36

T.P.

-0.73 329.79

		+7.68	
			H.I. 337.47
			1+30
		M.A. & Alley - Flowline	12.52 324.95
			1+50
E		6.5	331.0
+5		6.9	330.6
E		7.3	330.2
W		7.2	330.3
			1+75
W		6.9	330.6
E		6.5	331.0
+5		6.3	331.2
E		6.2	331.3
			1+95
			5.30
		Garage 0.4' in Alley from E.L. Concrete Floor	332.17 ↓
			2+00
E		5.9	331.6
+5		6.2	331.3
E		6.1	331.4
W		6.4	331.1
			2+25
W		6.2	331.3
E		6.0	331.5
+5		6.1	331.4

#1. 337.47

E	6.1	331.4
	2+33	
⊕ 8' Garage 0.4' in Alley from E.L. Dirt Floor 56		331.9 ↓
	2+41	
⊕ 8' Garage 5' Back W.L. Dirt Floor 58		331.7 ↓
	2+50	
E	5.7	331.8
+5	5.7	331.8
⊕	5.8	331.7
W	5.6	331.9
	2+75	
W	6.0	331.5
⊕	5.8	331.7
+5	5.8	331.7
E	5.7	331.8
	3+00	
E	5.1	332.4
+5	5.5	332.0
⊕	5.5	332.0
W	5.8	331.7
	3+25	
W	5.4	332.1
⊕	5.4	332.1
+5	5.2	332.3
E	5.2	332.3

#1. 337.47

37

	3+50	
E	5.5	332.0
+5	5.4	332.1
⊕	5.4	332.1
W	5.6	331.9
	3+75	
W	5.3	332.2
⊕	5.2	332.3
+5	5.3	332.2
E	5.3	332.2
	3+95	
⊕ 11' Garage 4' Back W.L. Dirt Floor	5.6	331.9 ↓
	4+00	
E	5.1	332.4
+5	4.7	332.8
⊕	4.8	332.7
W	4.9	332.6
	4+25	
W	4.7	332.8
⊕	4.9	332.6
+5	5.1	332.4
E	5.3	332.2
	4+50	
E	5.8	331.7
+5	5.3	332.2
⊕	5.2	332.3

H.I. 337.47

W	5.4	332.1
	+4.95	
W	5.5	332.0
⊕	5.3	332.2
+5	5.4	332.1
E	5.5	332.0
	+4.91	
⊕ 8' Garage 5' Back W.L. Div + Floor	5.6	331.9
	+5.00	
E	5.2	332.3
+5	5.4	332.1
⊕	5.6	331.9
W	5.6	331.9
	+5.25	
W	5.5	332.0
⊕	5.7	331.8
+5	5.6	331.9
E	5.4	332.1
	+5.31	
⊕ 8' Garage 5' Back W.L. Div + Floor	5.7	331.8
	+5.50	
E	5.9	331.6
⊕ 5	5.8	331.7
⊕	5.9	331.6
W	5.7	331.8

H.I. 337.47

BIR 95 City Agt

38

5+7.5

W	5.9	331.6
⊕	5.9	331.6
+5	5.9	
E	5.9	331.6
	+6.00 = N.H. Dwight	
E Tp existing return	8.23	329.24
	8.2	
+5	7.5	330.0
⊕	7.8	329.7
G	8.5	
W Tp existing return	8.44	329.03
T.R		-6.44 331.03
	+3.10	H.I. 334.13
	J.L. Dwight = 0.100	
W Tp existing return	5.45	328.68
G	5.5	
⊕	4.4	329.7
+5	4.8	329.3
G	5.1	
E Tp existing return	5.07	329.06
	+0.04	
E	3.0	331.1
+5	3.1	331.0
⊕	3.0	331.1
W	3.1	331.0
	+0.25	
W	2.8	331.3

H. 1. 334. 13

♀	2.6	331.5
+5	2.3	331.8
E	2.4	331.7
0+50		
E	2.6	331.5
+5	2.7	331.4
♀	2.6	331.5
W	2.9	331.2
0+60		
♀ 8' Garage 3.5' Back W.L. Dirt Floor	3.0	331.1 ✓
0+75		
W	3.3	330.8
♀	2.9	331.2
+5	3.0	331.1
E	3.0	331.1
1+00		
E	3.4	330.7
+5	3.4	330.7
♀	3.4	330.7
W	3.7	330.4
1+18		
♀ 8' Garage 7' Back E.L. Concrete Floor	3.48	330.65 ✓
1+25		
W	3.8	330.3
♀	3.7	330.4

H. 1. 334. 13

39

+5	3.7	330.4
E	3.8	330.3
1+30		
♀ 8' Garage 7' Back E.L. Concrete Floor	3.66	330.47 ✓
1+42		
♀ 10' Garage 8' Back W.L. Concrete Floor	4.30	329.83 ✓
1+50		
E	4.2	329.9
+5	4.3	329.8
♀	4.3	329.8
W	4.4	329.7
1+75		
W	4.8	329.3
♀	4.8	329.3
+5	4.8	329.3
E	4.8	329.3
2+00		
E	5.2	328.9
+5	5.1	329.0
♀	5.2	328.9
W	5.3	328.8
2+05		
♀ 8' Garage 1.5' Back E.L. Concrete Floor	5.01	329.12 ✓
2+25		
W	5.9	328.2

H.I. 334.13

¢	58	328.3
+5	56	328.5
E	55	328.6
	2+33	
¢ 8' Garage 1.5' Back W.L. Concrete Floor	564	328.49 ✓
	2+50	
E	61	328.0
+5	63	327.8
¢	62	327.9
W	66	327.5
	2+75	
W	69	327.2
¢	69	327.2
+5	69	327.2
E	66	327.5
	3+00	
E	74	326.7
+5	75	326.6
¢	74	326.7
W	74	326.7
	3+13	
¢ 8' Garage 1.5' Back W.L. Concrete Floor	739	326.74 ✓
	3+25	
W	77	326.4
¢	78	326.3

H.I. 334.13

40

	78	326.3
E	79	326.2
	3+50	
E	84	325.7
+5	82	325.9
¢	81	326.0
W	83	325.8
	3+75	
W	89	325.2
¢	88	325.3
+5	89	325.2
E	86	325.5
	3+90	
¢ 8' Garage 1.0' Back E.L. Concrete Floor	855	325.58 ✓
	4+00	
E	92	324.9
+5	92	324.9
¢	92	324.9
W	91	325.0
	4+25	
W	98	324.3
¢	97	324.4
+5	97	324.4
E	97	324.4

41.334.13

4450

E	10.3	323.8
+5	10.3	323.8
♀	10.2	323.9
W	10.3	323.8

4475

W	10.0	323.1
♀	10.9	323.2
+5	10.8	323.3
E	10.6	323.5

5400

E	10.9	323.2
+5	11.4	322.7
♀	11.5	322.6
W	11.2	322.9
T.P.	-10.90	323.23

+1.56

41.324.79

5425

W	2.3	322.5
♀	2.5	322.3
+5	2.4	322.4
E	2.4	322.4

5440

♀ 8' Garage 1.5 Back EL. Dist Flow	2.6	322.2
------------------------------------	-----	-------

BIR109 City Hqs

41.324.79

41

5450 P

E	2.7	322.1
+5	2.7	322.1
♀	2.7	322.1
W	2.7	322.1

5475

W	3.7	321.1
♀	3.6	321.2
+5	3.3	321.5
E	3.3	321.5

5490

E	3.6	321.2
+5	3.8	321.0
♀	4.2	320.6
W	3.7	321.1

5499 = N.L. Myrtle

N Tp existing return	5.35	319.44
G	5.4	319.4
♀	5.4	319.4
+5	5.4	319.4
G	5.0	
ETp existing return	4.98	319.81
B.M. N.W.B.P. Myrtle + 40%	-6.62	318.17

5.L Myrtle 5000

ETp existing return	5.58	319.21
G	5.6	

H.I. 324.79

+5	57	319.1
£	58	319.0
G	58	
W.Tp. existing return	57.0	319.09
	0725	
W	6.0	318.8
£	57	319.1
+5	56	319.2
E	5.8	319.0
	0750	
E	6.2	318.6
+5	6.2	318.6
£	6.3	318.5
W	6.6	318.2
	0775	
W	7.0	317.8
£	6.9	317.9
+5	6.9	317.9
E	6.8	318.0
	1400	
E	7.7	317.6
+5	7.5	317.3
£	7.6	317.2
W	7.5	317.3

H.I. 324.79

42

	1400	
£ 2' Concrete Walk / in Alley from W.L.	7.34	317.45 ✓
	1425	
W	8.0	316.8
£	7.9	316.9
+5	8.0	316.8
E	7.9	316.9
	1440	
£ 12' Garage 2' Back W.L. Concrete Floor	8.04	316.75 ✓
	1450	
E	8.6	316.2
+5	8.6	316.2
£	8.5	316.3
W	8.6	316.2
	1475	
Out 1' & 2' Concrete Walk	9.15	315.64 ✓
W	9.2	315.6
£	9.3	315.5
+5	9.1	315.7
E	9.3	315.5
	2400	
E	9.6	315.2
+5	9.6	315.2
£	9.6	315.2
W	9.8	315.0

H.I. 324.79

2+08

♀ 8' Garage 2' Back W.L. Dix + Floor 10.2

314.6 ✓

2+25

W 10.5

314.3

♀ 10.4

314.4

+5 10.2

314.6

E 10.1

314.7

2+50

E 11.0

313.8

+5 10.5

314.3

♀ 10.7

314.1

W 11.0

313.8

2+75

W 11.4

313.4

♀ 11.2

313.6

+5 11.0

313.8

E 11.2

313.6

2+82

♀ 8' Garage 2' Back W.L. Concrete Floor 11.03

313.76 ✓

3+00

E 12.0

312.8

+5 11.6

313.2

♀ 11.7

313.1

W 11.7

313.1

T.P.

-11.67 313.14

+0.50 313.62

H.I. 313.62

43

3+25

-W 1.5

312.1

♀ 1.4

312.2

+5 1.1

312.5

E 1.2

312.4

3+50

E 2.1

311.5

+5 1.9

311.7

♀ 2.3

311.3

W 2.4

311.2

3+75

W 3.0

310.6

♀ 2.8

310.8

+5 2.8

310.8

E 2.8

310.8

4+00

E 3.3

310.3

+5 3.3

310.3

♀ 3.1

310.5

W 3.4

310.2

4+25

W 3.9

309.7

♀ 3.4

310.2

+5 3.6

310.0

E 3.9

309.7

41.31362

4+50

E	45	309.1
+5	46	309.0
☿	47	308.9
W	49	308.7

4+55

☿ 8' Garage - 8' Back EL. Concrete Floor 395 309.67 ✓

4+75

W	50	308.6
☿	50	308.6
+5	50	308.6
E	50	308.6

5+00

E	59	307.7
+5	55	308.1
☿	55	308.1
W	60	307.6

5+25

W	68	306.8
☿	66	307.0
+5	62	307.4
E	62	307.4

5+31

☿ 8' Garage 0.5' Back EL. Dirt Floor 64 307.2 ✓

5+50

E	66	307.0
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BIR 124. City Hqs

41.31362

44

+5	66	307.0
☿	67	306.9
W	72	306.4

5+75

W	74	306.2
☿	78	305.8
+5	72	306.4 ⁶
E	73	307.3

5+95

E	75	306.1
+5	93	304.3
☿	10.0	303.6
+7	9.1	
W	7.8	305.8

5+99.5 = N.L. Thorn

W-Tp existing return 10.88 302.74

☿ 11.0

☿ 10.7 302.9

+5 10.7 302.9

G. 10.4

E-Tp existing return 10.57 303.25

S.L. Thorn = 0+00

E-Tp existing return 11.12 302.50

G 11.4

+5 11.4 302.2

H.I. 3136 v

Q	11.6	302.0
E	11.5	302.1
W-Tp existing return	11.47	302.15
	0+05	
W	11.0	302.6
Q	11.4	302.2
+5	11.1	302.5
+8	10.0	
E	10.2	303.4
	0+25	
E	11.0	302.6
+5	11.2	302.4
Q	11.4	302.2
W	10.9	302.7
	0+50	
W	11.4	302.2
Q	11.6	302.0
+5	11.7	301.9
E	11.9	301.7
T.P		-11.52 302.11
	+4.83	H.I. 306.93
	0+75	
E	5.0	301.9
+5	5.3	301.6
Q	5.2	301.3

H.I. 306.93

45

W	5.0	301.9
	+00	
W	5.4	301.5
Q	5.5	301.4
+5	5.6	301.3
E	5.7	301.2
	1+25	
E	6.2	300.7
+5	6.2	300.7
Q	6.0	300.9
W	5.7	301.2
	1+50	
W	6.7	300.2
Q	6.7	300.2
+5	6.7	300.2
E	6.7	300.2
	1+75	
E	7.5	299.4
+5	7.5	299.4
Q	7.5	299.4
W	7.4	299.5
	2+00	
W	8.0	298.9
Q	8.2	298.7
+5	8.3	298.6

H.I. 306.93

E	8.2	298.7
	2+05	
8' Garage 17' Back E.L. Concrete Floor	8.4	298.51 ✓
	2+25	
E	8.5	298.4
+5	8.2	298.7
♀	8.0	298.9
W	7.2	299.7
	2+50	
W	7.8	299.1
♀	7.6	299.3
+5	8.0	298.9
E	8.2	298.7
	2+25	
E	7.7	299.2
+5	7.4	299.5
♀	7.2	299.7
W	7.1	299.8
	3+00	
W	5.5	301.4
♀	5.7	301.2
+5	6.1	300.8
E	6.9	300.0

H.I. 306.93

46

	3+25	
E	5.0	301.9
+5	4.4	302.5
♀	4.2	302.7
W	4.3	302.6
	3+50	
W	2.2	304.7
♀	2.8	304.1
+5	3.0	303.9
E	3.6	303.3
	3+75	
E	2.6	304.3
+5	2.0	304.9
♀	1.8	305.1
W	2.4	304.5
	4+00	
W	1.6	305.3
♀	1.7	305.2
+5	2.0	304.9
E	2.4	304.5
	4+05	
♀ 8' Garage at E.L. Concrete Floor	2.19	304.74 ✓
	4+20	
8' Garage at E.L. Dirt Floor	6.4	300.5 ✓

H. 1. 306.93

4+25

E	1.8	305.1
+5	1.6	305.3
♀	1.3	305.6
W	1.0	305.9

4+50

W	0.6	306.3
♀	0.9	306.0
+5	1.0	305.9
E	1.2	305.7

4+75

E	0.8	306.1
+5	0.4	306.5
♀	0.2	306.7
W	0.4	306.5

T.P.

-0.07 306.86

+3.49

H. 1. 310.35

5+00

W	3.8	306.6
♀	3.3	307.1
+5	3.4	307.0
E	3.5	306.9

5+15

♀ 8' Garage 2.5' in alley from W.H. Dist floor 4.1 306.3 ✓

H. 1. 310.35

47

5+25

E	4.2	306.2
+5	4.0	306.4
♀	4.0	306.4
W	4.2	306.2

5+33

♀ 8' Garage 7' Back W.H. Concrete Floor 3.70 306.65 ✓

5+50

W	4.1	306.3
♀	4.1	306.3
+5	4.3	306.1
E	4.3	306.1

5+56

♀ 8' Garage 2.5' Back W.H. Concrete Floor 3.90 306.45 ✓

5+75

E	4.4	306.0
+5	4.2	306.2
♀	4.3	306.1
W	4.4	306.0

6+00 = N.H. Redwood - Curb in on Redwood to W.H. Alley

W - Sp existing return	4.99	305.36 ✓
G	5.0	"
♀	4.8	305.6
+5	4.8	305.6
E	4.8	305.6

B.M. N.W. B.P. 40th + Redwood-728 303.07
Correct 302.97

Ycb. +24' E edge E. Rail N Track	4.55	+0.78
" +35.9' N " W " E "	4.24	+1.09
" +41.1' E " E " " "	4.50	+0.83
cb. B.	5.24	+0.09
Gut. B.	5.65	-0.32
L.E. Pav.	5.71	-0.38
E. Gut.	5.94	-0.61
" cb.	5.55	-0.22
52.3' N of & Toulon ch. on W.		
52.6' " " " " " E		
Ecb.	5.52	-0.21
" Gut.	6.02	-0.62
L.E. Pav.	5.85	-0.52
Gut. B.	5.71	-0.38
cb. B.	5.29	+0.10
" A	5.19	+0.14
Gut. A	5.48	-0.15
L.W. Pav.	5.52	-0.19
N. Gut.	5.79	-0.46
" top cb.	5.13	+0.20
S.W. top cb.	4.88	+0.45
" " Pav.	5.01	+0.32
C " "	4.98	+0.35
W. N. Alley		
Y.G. on Grading Tole. #1	5.83	-0.50
N.W. top Pav.	4.99	+0.34
" " " cb.	5.04	+0.29

3' N.W. Alley, B19 and B20

60' Red. cbs.

Ycb.	5.16	+0.17
" Gut.	5.83	-0.50
L.W. Pav.	5.54	-0.21
Gut. A	5.45	-0.12
cb. A	5.20	+0.13
" B.	5.22	+0.11
Gut. B	5.69	-0.36
L.E. Pav.	5.74	-0.41
E. Gut.	6.00	-0.67
" top cb.	5.61	-0.28
N.E. top cb.	5.41	-0.08
" " Pav.	6.07	-0.74
C " "	5.97	-0.64
E.G. " "	6.00	-0.67
S.E. top cb.	5.27	+0.06
" " Pav.	6.00	-0.67
53.4' N.W. Alley B20		
53.4' " " " B19		
Ecb.	5.62	-0.22
" Gut.	5.95	-0.62
L.E. Pav.	5.79	-0.40
Gut. B.	5.68	-0.35
cb. B.	5.23	+0.10
Expt. 1885 E edge E. Rail E Track	4.53	+0.80
" + 24.0' W " W " " "	4.19	+1.14
" + 36.0' E " E " W "	4.58	+0.75
" + 41.5' W " W " " "	4.24	+1.09

3' N.W. Alley B20 } = VANITIE COURT. 60' Red. cbs.

Tole. #2
 -074
 -Grading
 (219)

Tole. #3
 -075
 -Grading
 (52)

cb. A	522	+0.11
Gut. A	546	-0.13
L. H. Pav.	548	-0.15
" Gut.	566	-0.33
N. cb.	507	+0.26
5235 N. of Van Aie (Ch. on W.) 5726 " " " " " E } 3' S. N. Alley 223 + 224		
N. cb.	506	+0.27
" Gut.	574	-0.41
L. H. Pav.	552	-0.19
Gut. A	546	-0.13
cb. A	516	+0.17
" B.	524	+0.09
Gut. B.	563	-0.30
L. H. Pav.	574	-0.41
E. Gut.	600	-0.67
" cb.	557	-0.24
S. E. top cb.	547	-0.14
" " " Pav.	610	-0.77
" " "	602	-0.69
E. G. " " } Alley 224	595	-0.62
N. E. top cb.	561	-0.28
" " " Pav.	607	-0.74
3' N. N. Alley's. 223 + 224		
E. cb.	554	-0.21
" Gut.	601	-0.68
L. E. Pav.	575	-0.42

Gut. B.	565	-0.32
cb. B.	523	+0.10
" A	517	+0.14
Gut. A	549	-0.16
L. H. Pav.	554	-0.21
N. Gut.	577	-0.44
" top cb.	511	+0.22
N. H. top cb.	494	+0.39
" " " Pav.	494	+0.39
C " "	501	+0.32
2758 Alley } Alley 223 N. E. Gut. top cb.	581	-0.48
S. H. top cb.	484	+0.49
" " " Pav.	492	+0.41
502 N. N. Alley 223 501 " " " " 224 } S. Line SAN RAFAEL Pl. 60.3' Bot. chs. Section from East		
S. E. top cb.	541	-0.08
" " " Pav.	553	-0.20
E. cb. on Pav.	592	-0.59
L. E. Pav.	573	-0.40
E. cb. + 12' = Loc. Cross over.	568	-0.35
" + 18' = E. edge E. Pav. E. Trch.	450	+0.83
" + 24' = N. " " " " "	419	+1.14
" + 36' = E. " " " " "	459	+0.74
" + 41' = N. " " " " "	428	+1.05
" + 47' = Loc. Cross over.	538	-0.05
L. H. Pav.	541	-0.08
N. cb. on Pav.	562	-0.29

C top Pav.	5.31	-0.58	
E. A. "	5.39	-0.66	
NE. " "	5.34	-0.61	
" " " cb.	5.00	-0.27	
	3' N. N. W. Alley's 227 + 228		61.4' Bet. chs
E cb.	5.04	-0.31	
" Gut.	5.41	-0.68	
S. E. Pav.	5.21	-0.48	
Gut. B.	5.11	-0.38	
cb. B.	4.60	+0.13	
cb. A	4.54	+0.19	
Gut. A	4.84	-0.11	
S. W. Pav.	4.89	-0.16	
W. Gut.	5.15	-0.42	
" cb.	4.50	+0.23	
N. W. top cb.	4.36	+0.37	
" " " Pav.	4.45	+0.28	
C " " = From M.H.	4.48	+0.25	
1' S. Alley			} Alley 228
M.G. on Gutting Sump	5.19	-0.36	
S.W. top Pav.	4.97	+0.26	
" " " cb.	4.87	+0.36	
56.00 N. N. W. Alley 227			} -2' VENICE COURT
56.07 " " " 228			
			61.7' Bet. chs
W. cb.	4.73	0.00	
" Gut.	5.19	-0.36	
S. W. Pav.	5.01	-0.28	
Gut. A	4.94	-0.21	

cb. A	4.61	+0.12	
W. cb. + 19.6' = N. Alley W. Pav. W. Tract.	3.87	+0.86	
" " + 24.3' = E " E " " "	4.13	+0.60	
" " + 37.05' = W " W " E "	3.74	+0.99	
" " + 42.3' = E " E " " "	4.09	+0.64	
cb. B.	4.65	+0.08	
Gut. B.	5.22	-0.49	
S. E. Pav.	5.29	-0.56	
E. Gut.	5.56	-0.83	
E. cb.	5.09	-0.36	
53.7' N. of S. Venice Ct. on E			} 3' S. S. W. Alley's 231 + 232.
53.43' " " " " " " W }			
			62.10' Bet. chs
E. cb.	5.31	-0.58	
" Gut.	5.76	-1.03	
S. E. Pav.	5.48	-0.75	
Gut. B.	5.28	-0.55	
cb. B.	4.74	-0.01	
" A	4.66	+0.07	
Gut. A	4.94	-0.21	
S. W. Pav.	5.00	-0.27	
W. Gut.	5.25	-0.52	
" cb.	4.82	-0.09	
N. W. top cb.	4.59	+0.14	
" " " Pav.	4.66	+0.07	
C " "	4.67	+0.06	
23' South S. Alley			} Alley 231
M.G. on Gutting Sump	5.37	-0.59	
S. W. top cb.	4.74	-0.01	
" " " Pav.	4.67	+0.06	

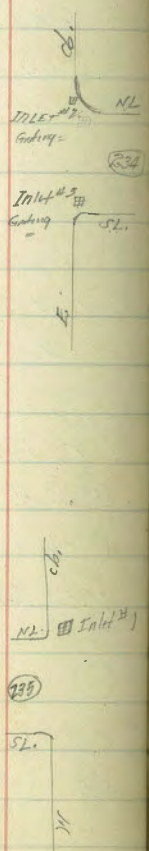
Notes for Section 3' N.W. Alleys 231 + 232 Sec P-55

Notes	Y/cb.	
57' N.W. Alley 231	} -2 VERONA COURT.	
5733 " " " 232		
This section from West.		
Y/cb.	4.98	-0.25
" Gut.	5.40	-0.67
L.W. Pav.	5.14	-0.41
Gut. A	5.35	-0.32
cb. A.	4.70	+0.03
Y/cb. + 20.3' = Y edge Y Riv W Trch.	3.97	+0.76
" " + 25.4' = E " E " " "	4.24	+0.19
" " + 37.7' = Y " Y " E "	3.93	+0.80
" " 43.8' = E " E " E "	4.18	+0.55
cb. B.	4.73	0.00
Gut. B.	5.32	-0.59
L.E. Pav.	5.41	-0.68
E. Gut.	5.64	-0.91
" cb.	5.27	-0.54
545' N. of 1 Verona Court W }	} -3 S.S.L. Alleys 234 + 235	
5463 " " " " " E }		
E cb.	5.40	-0.67
" Gut.	5.79	-1.06
L.E. Pav.	5.47	-0.74
Gut. B.	5.22	-0.49
cb. B.	4.72	+0.01
" H	4.66	+0.07
Gut. A	5.10	-0.37
L.S.P. Pav.	5.19	-0.46
Y. Gut.	5.46	-0.73

Y/cb.	5.08	-0.35
SE top cb	4.98	-0.25
" " Pav	4.98	-0.25
C " "	4.93	-0.20
Y.G. " "	5.50	-0.77
NE top cb	4.75	-0.02
" " Pav	4.83	-0.10
3' N.W. Alleys 231 + 232		
Y/cb.	4.81	-0.08
" Gut.	5.28	-0.55
L.W. Pav.	5.02	-0.29
Gut. A	4.95	-0.22
cb. A	4.65	+0.08
" B.	4.69	+0.04
Gut. B.	5.29	-0.56
L.E. Pav.	5.46	-0.73
E Gut.	5.81	-1.08
" cb.	5.27	-0.19
NE top cb	5.10	-0.37
" " Pav	5.90	-1.17
C " "	5.72	-0.99
E.G. " "	5.74	-1.01
SE " "	5.85	-1.12
" " cb.	5.19	-0.46

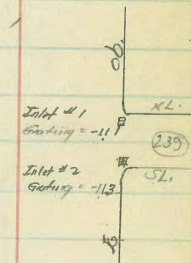
3' N.N.W. Alleys 234 + 235

N top cb.	5.04	-0.31
" Gut.	5.55	-0.82
S.W. Pav.	5.27	-0.54
Gut. A	5.12	-0.39
cb. A	4.68	+0.05
" B.	4.70	+0.03
Gut. B.	5.21	+0.48
E.E. Pav.	5.45	-0.72
E Gut.	5.81	-1.08
Ecb, PC = 113' N.N.W. Alley	5.42	-0.70
N.E. top cb.	5.24	-0.51
" " " Pav.	5.90	-1.17
C " "	5.86	-1.13
E.G. " "	5.73	-1.00
S.E. " "	5.87	-1.14
" " " cb.	5.18	-0.45
Inlet #1 on Graffiti opp PC Alley 235	5.52	-0.79
" #2 = S.A. N.N.W. Alley	5.88	-1.15
" #3 = 1' N.S.E. " } = 2' WHITING COURT. 57.68' N.N.W. Alley 234 } 58.17' " " " 235 }	5.87	-1.14
E cb.	5.32	-0.59
" Gut.	5.62	-0.89
E.E. Pav.	5.36	-0.63
Gut. B.	5.20	-0.47
cb. B.	4.73	0.00



E cb. + 20' = E edge E Pav / E Tact	4.28	+0.45	
" " 125.9' - Y " Y " " "	4.22	+0.51	
" " 138.45' = E " E " Y "	4.29	+0.44	
" " 144.0' = Y " Y " " "	4.14	+0.59	
cb. A	4.68	+0.05	
Gut. A	5.18	-0.45	
S.W. Pav.	5.30	-0.57	
Y Gut.	5.64	-0.91	
" cb.	5.17	-0.44	
T.P. 186	3.55	3.04	1.69
N top cb.	4.16	-0.61	
" Gut.	4.56	-1.01	
S.W. Pav.	4.23	-0.68	
Gut. A	4.07	-0.52	
cb. A	3.56	-0.01	
" B.	3.60	-0.05	
Gut. B.	4.05	-0.50	
S.E. Pav.	4.24	-0.69	
E Gut.	4.62	-1.07	
" cb.	4.20	-0.65	
S.E. top cb. Finest " " " " " " " " " " " "	—	—	
" " " Pav.	4.72	-1.17	
C " " } Alley 239	4.59	-1.04	
E.G. " "	4.57	-1.02	
N.E. top cb.	3.38	-0.33	

56.03' N. of 2' Whiting Ct. on Y.
55.75' " " " " " E } = 3' S.W. Pav. Alley #38 # of 239
64.6' E.H. chs.
#114 298 SW
at Fire Hydr.



N.E. top Pav.	4.64	-1.09	63.8' Bot. obs.
			3' N.H.L. Alley's. 238
E. cb.	4.21	-0.66	4th/239
" Gut.	4.60	-1.05	
E. E. Pav.	4.28	-0.73	
Gut. B.	4.06	-0.51	
cb. B.	3.65	-0.10	
" H	3.56	-0.01	
Gut. H	4.12	-0.57	
E. W. Pav.	4.24	-0.69	
W. Gut.	4.60	-1.05	
" cb.	4.00	-0.45	
N.W. top cb.	3.88	-0.33	
" " " Pav.	3.98	-0.43	
C " "	4.02	-0.47	
M.G. " Inlet.	4.61	-1.06	Alley 238
S.W. top cb.	3.98	-0.43	
" " " Pav.	3.90	-0.35	65.45' N.H.L. Alley 238
			66.41
W. cb.	3.94	-0.39	62.9' Bot. obs.
" Gut.	4.50	-0.95	W. Windmere court,
E. W. Pav.	4.22	-0.67	
Gut. H	4.08	-0.53	
cb. H	3.59	-0.04	
W. cb. + 17.85	3.06	+0.49	- W. edge W. Rail. V. Track.
" " + 15.3	2.94	+0.61	" " " " " " " "

W. cb. + 37.6	3.08	+0.47	- W. edge W. Rail. V. Track.
" " + 43.3	2.91	+0.64	" " " " " " " "
cb. B.	3.65	-0.07	
Gut. B.	4.08	-0.53	
E. E. Pav.	4.23	-0.68	
E. Gut.	4.50	-0.95	
" cb.	4.17	-0.62	56.55' N. of E. Windmere ct. on W.
			57.02 " " " " " " " "
			61.9' Bot. obs.
			3' S.H.L. Alley's. 240 + 241
E. cb.	4.24	-0.69	
" Gut.	4.65	-1.10	
E. E. Pav.	4.32	-0.77	
Gut. E.	4.12	-0.57	
cb. B.	3.67	-0.12	
" H	3.64	-0.09	
Gut. H	4.02	-0.47	
E. W. Pav.	4.10	-0.55	
W. Gut.	4.37	-0.82	
" cb.	3.92	-0.37	
S.W. top cb.	3.77	-0.22	
" " " Pav.	3.81	-0.26	
C " "	3.86	-0.31	
W. G. " Gating Sump	4.35	-0.80	16.55' Alley 241
W. " Pav.	3.80	-0.25	
" top cb.	3.80	-0.25	
			61.7' Bot. obs.
			3' N.H.L. Alley's. 241 + 240
W. cb.	3.78	-0.23	

S.W. top cb.	3.68	-0.13
" " " Pav.	3.77	-0.22
N.W. top cb.	3.66	-0.11
" " " Pav.	3.75	-0.20
C " "	3.76	-0.21
16' S of Alley		
Y.G. Gateway Swamp	4.34	-0.79
58.57' N.W. Alley 44 on W.		
59.4' " " " Produced on E. } = 2 York Court. 60.15' Bet. chs.		
Y. cb.	3.78	-0.23
" Gut.	4.38	-0.83
S.W. Pav.	4.11	-0.56
Gut. A	4.08	-0.53
cb. A	3.72	-0.17
Y. cb. + 18.95' = Y. cb. W. Pav. W. Tract.	3.31	+0.24
" " + 24.10' = E " E " " " "	2.88	+0.67
" " + 36.0' = W " W " E " "	3.28	+0.27
" " + 41.2' = E " E " " " "	2.86	+0.69
cb. B.	3.72	-0.17
Gut. B.	4.17	-0.62
S.E. Pav.	4.24	-0.69
E Gut.	4.44	-0.89
" cb.	4.15	-0.60
54.83' N. of 2 York ct. on W.		
57.1' " " " " Produced on E. } = 3.25' 2.45		
E. cb.	4.30	-0.75
" Gut.	4.60	-1.05
S.E. Pav.	4.38	-0.83
Gut. B.	4.28	-0.73
cb. B.	3.83	-0.28
" A	3.82	-0.27

Gut. A	4.15	-0.60	
S.W. Pav.	4.23	-0.68	
Y. Gut.	4.44	-0.89	
" cb.	3.90	-0.35	
S.W. top cb.	3.77	-0.22	
" " " Pav.	3.85	-0.30	
C " "	3.92	-0.37	
16' S of Alley			
Y.G. Gateway Swamp	4.44	-0.89	
N.W. top cb.	3.94	-0.39	
" " " Pav.	4.03	-0.48	
3' N. N.L. Alleys 2.45	60.1' Bet. chs.		
Y. cb.	3.94	-0.39	
" Gut.	4.48	-0.93	
S.W. Pav.	4.28	-0.73	
Gut. A	4.27	-0.72	
cb. A	3.85	-0.30	
" B.	3.87	-0.32	
Gut. B.	4.32	-0.77	
S.E. Pav.	4.40	-0.85	
E. Gut.	4.63	-1.08	
" cb.	4.36	-0.81	
T.P. 4.20	3.99	3.76	-0.21
57.57' N. N.L. Alley 2.45 on W.			
59.78' " " " " 2.45' Produced on E. } = ZANZIBAR COURT. 60.15' Bet. chs.			
E. cb.	4.93	-0.94	
" Gut.	5.21	-1.22	
S.E. Pav.	5.15	-1.06	

Gut. B	4.97	-0.98
cb. B.	4.51	-0.52
E. cb. + 19.05 = E. edge E. Parl. E. Tract.	3.65	+0.34
" " + 24.15 = " " " " " "	3.88	+0.11
" " + 36.10 = E " E " " "	3.64	+0.35
" " + 41.2 = " " " " " "	3.90	+0.09
cb. A	4.51	-0.52
Gut. A	4.81	-0.82
E. M. Pav.	4.89	-0.90
M. Gut.	5.09	-1.10
" cb.	4.60	-0.61
<small>37.51' N. of 1/2 cor. 1st & 2nd on W. = South line of North 1/2 by Santa Rita Rd</small>		
SW top cb Broken up.	4.88	
" " Pav.	4.88	-0.89
M. cb. on Pav.	5.24	-1.25
E. M. Pav.	5.11	-1.12
M. cb. + 13.0 = toe grass over.	5.08	-1.09
" " + 19.05 = E edge M. Parl. M. Tract.	4.08	-0.09
" " + 24.2 = E " E " " "	4.02	-0.03
" " + 36.05 = " " " E "	4.00	-0.01
" " + 41.2 = E " E " " "	3.88	+0.11
" " + 47.2 = toe grass over.	5.29	-1.30
E. Pav.	5.30	-1.31
E. Gut.	5.44	-1.45
" top cb.	5.08	-1.09
S.E. " "	5.23	-1.24

S.E. top Pav.	5.60	-1.61
C " "	5.46	-1.47
E.G. " "	5.45	-1.46
N.E. top cb.	5.17	-1.18
" " Top Pav.	5.50	-1.51
<small>North line Santa Rita Rd. Mission Ranch.</small>		
E. cb. on Pav.	5.56	-1.57
E. Pav.	5.37	-1.38
E. cb. + 13.0 = toe grass over.	5.40	-1.41
" " + 19.05 = E edge E. Parl. E. Tract.	4.10	-0.11
" " + 24.2 = " " " " " "	4.17	-0.18
" " + 36.05 = E " E " " "	4.19	-0.20
" " + 41.2 = " " " " " "	4.19	-0.20
" " + 47.4 = toe grass over.	5.28	-1.29
E. M. Pav.	5.06	-1.37
M. cb. on Pav.	5.53	-1.54
" " + 10 = H. on Pav.	5.21	-1.22
" " + 20 on Pav.	5.53	-1.54
" " + 20 " cb.	5.05	-1.06
" " + 30 " "	4.90	-0.91
C. on Pav. on N. line = 2 1/2' lag	5.06	-1.07
M.G. " "	5.35	-1.36
PC ¹ top cb. } 3' 58" L.	4.79	-0.80
PC ¹ " Pav.	5.21	-1.22
PC ² " " }	5.05	-1.06
PC ² " cb. } d1 = 13.2'	4.78	-0.79

E. Gut.	5.09	-1.67
E. cb.	4.73	-1.31
Section B = 80.15' Bet. obs.		
E. cb.	4.74	-1.32
" Gut.	5.12	-1.70
L. E. Par.	4.96	-1.54
Gut. B.	4.94	-1.52
cb. B.	4.60	-1.18
" A	4.55	-1.13
Gut. H	4.86	-1.44
L. W. Par.	5.00	-1.58
W. cb. on Par.	5.20	-1.78
+ 10' " "	5.32	-1.90
+ 20' " "	5.31	-1.89
+ 20' " cb.	4.76	-1.34
N.Y. top "	4.39	-0.97
" " Par.	4.47	-1.05
C " "	4.86	-1.44
W.G. " "	5.28	-1.86
S.Y. " cb.	4.54	-1.12
" " Par.	4.62	-1.20
Section C = 80.25' Bet. obs.		
W. cb. - 20' on top cb.	4.92	-1.50
" " - 20' Gut. Par.	5.48	-2.06
" " - 10' " Par.	5.42	-2.00
W. cb. on "	5.26	-1.84

L. W. Par.	5.04	-1.62
Gut. A	4.96	-1.54
cb. A	4.72	-1.30
" B.	4.70	-1.28
Gut. B	5.08	-1.66
L. E. Par.	5.04	-1.62
E. Gut.	5.18	-1.76
E. cb.	4.75	-1.33
Section D 80.10' Bet. obs.		
E. cb.	4.82	-1.40
" Gut.	5.26	-1.84
L. E. Par.	5.10	-1.68
Gut. B.	5.10	-1.68
cb. B.	4.74	-1.32
E. cb. + 18.9' = E. edge B. Par. to Trch.	4.03	-0.61
" " + 24.5' = " " " " " "	4.06	-0.64
" " + 35.85' = E. " E. " " " "	4.12	-0.70
" " + 41.0' = " " " " " "	4.07	-0.65
cb. A	4.81	-1.39
Gut. A	5.01	-1.59
L. W. Par.	5.12	-1.70
W. cb. on Par.	5.34	-1.92
" " + 10' "	5.50	-2.08
" " + 20' on Gut.	5.57	-2.15
" " + 20' top cb.	4.99	-1.57
N.Y. " "	4.75	-1.33

N.Y. top Pav	475	-1.33
C " "	496	-1.54
M.G. " "	553	-2.11
S.Y. " "	463	-1.21
" " " cb.	459	-1.17

Section E = 80.2' Bet. chs

Mcb. - 20' on cb.	518	-1.76
" " - 20' " Gut. Pav.	570	-2.28
" " - 10' " Pav.	562	-2.20
Mcb. " "	541	-1.99
L.Y. Pav.	517	-1.75
Gut. A	510	-1.68
cb. A	497	-1.55
cb. B	489	-1.47
Gut. B.	521	-1.79
L.E. Pav.	524	-1.82
L. Gut.	540	-1.98
" cb.	491	-1.49

Section F = 80.20' Bet. chs.

E cb.	492	-1.50
" Gut.	543	-2.01
L.E. Pav.	530	-1.88
Gut. B.	525	-1.83
cb. B.	498	-1.56
" A	502	-1.60
Gut. A	516	-1.74

L.Y. Pav.	520	-1.78
Mcb. on Pav.	544	-2.02
" " + 10' on Pav.	566	-2.24
" " + 20' " "	574	-2.32
" " + 20' " cb.	521	-1.79
N.Y. top cb.	494	-1.52
" " " Pav.	508	-1.66
C " "	535	-1.93
M.G. " "	575	-2.33
S.Y. top cb.	498	-1.56
" " " Pav.	508	-1.66

Section G = 80.05' Bet. chs

Mcb. - 20' on top cb.	519	-1.77
" " - 20' " " Pav.	571	-2.29
" " - 10' " " "	564	-2.22
Mcb. " "	543	-2.01
" " + 7.5' "	523	-1.81
cb. Gut. A.	525	-1.83
" A	512	-1.70
" B.	512	-1.70
Gut. B. on Pav.	537	-1.95
" " + 7.5' on Pav.	541	-1.99
E Gut.	555	-2.13
" cb.	510	-1.68

Section H = 80' Bet. chs

E cb.	518	-1.76
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Section J

Note: Sections from J. to P. Int. curve = 80' st. ^{10' chs} 15' 25'

E.L. + 2 1/2' top cb.	526	-1.84
" " + 2 1/2' " Pav.	568	-1.26
E.cb. 00 Pav	525	-1.83
E. 1/2 " "	439	-0.97
+ 1 " "	438	-0.96
+ 9 3/4 " "	444	-1.02
1/2 " "	433	-0.91
+ 11 1/2 " "	436	-0.94
1/2 1/2 " "	435	-0.93
+ 10 7/8 " "	491	-1.49
1/2 cb. " "	483	-1.41
1/2 L. " "	483	-1.41
+ 20' " " 1/2 edge	495	-1.53

Section K

1/2 - 20' " "	450	-1.08
1/2 L. " "	444	-1.02
1/2 cb. " "	410	-0.98
" 1/2 00 "	438	-0.96
1/2 " "	438	-0.96
+ 11' " "	449	-1.07
1/2 " "	442	-1.00
E.cb. " Pav.	482	-1.40
E.L. " "	511	-1.69
" " + 10' " Pav.	590	-2.48
" " + 10' " cb.	505	-1.63

Section L

E.L. - 10' top Pav.	542	-2.00
E.L. " "	502	-1.60
" cb. " "	481	-1.39
E 1/2 " "	453	-1.11
1/2 " "	440	-0.98
+ 5' " "	435	-0.93
1/2 1/2 " "	435	0.93
1/2 cb. " "	430	-0.88
1/2 L. " "	435	-0.93
+ 20' " "	442	-1.00

Section M. - Pacific Ave.

1/2 L. - 20' top Pav.	438	-0.96
1/2 L. " "	438	0.96
" cb. " "	432	-0.90
" 1/2 " "	432	-0.90
1/2 " "	439	-0.97
1/2 " "	456	-1.14
E.cb. " "	484	-1.42
E.L. " "	500	-1.58
+ 40' " "	521	-1.79

Section N

E.L. - 10' top Pav.	516	-1.74
E.L. " "	516	-1.74
E.cb. " "	502	-1.60
E 1/2 " "	456	-1.14

E 2 + 8' on Pav.	454	-1.12
L " "	438	-0.96
1/2 " "	435	-0.93
Ncb. " "	453	-1.11
Y/b. " "	462	-1.20
+20 " "	444	-1.02

Section O = Ncb. Line Pacific Ave.

Y/b. -20' on top cb.	3.93	-0.51
" " -20' " Pav.	4.57	-1.15
Y/b. " "	5.09	-1.67
" " " cb.	4.27	-0.85
B. on inlet	5.16	-1.74
Y/cb. on Pav.	4.94	-1.52
" 1/2 " "	4.37	-0.95
L " "	4.37	-0.95
+135 " "	4.50	-1.08
1/2 " "	4.59	-1.17
E.cb. " "	4.53	-1.11
C " inlet	5.88	-2.46
E.L. " cb.	5.10	-1.68
" " Pav.	5.68	-2.26
E.L. + 40' on cb.	4.96	-1.54
" " + 40 " Pav.	5.60	-2.18

Section P = Ncb. PACIFIC

E.cb. on cb.	5.08	-1.66
" " " Pav.	5.92	-2.50

E 1/2 on Pav.	4.61	-1.19
" " + 15' on Pav.	4.51	-1.09
E line + 28' = Edge E. Rail E. Track	4.47	-1.05
" " + 340' = Y. Y " " "	4.45	-1.03
" " + 458' = E " E " Y " "	4.32	-0.90
" " + 509' = Y " Y " " "	4.31	-0.89
L on Pav.	4.32	-0.90
" + 135 on Pav.	4.35	-0.93
1/2 on Pav.	4.41	-0.99
Y.cb. " "	5.17	-1.75
" " on cb.	4.32	-0.90

100' N. N.L. Pacific Ave

Y.cb. on cb.	3.88	-0.46
" " " Pav.	4.47	-1.05
Y 1/2 " "	4.18	-0.76
Y/cb. + 19.5 = Y edge N. Rail N. Track	4.18	-0.72
" " + 127' = E " E " " "	4.16	-0.74
" " + 137' = Y " Y " E "	4.15	-0.73
" " 408' = E " E " " "	4.17	-0.75
L top Pav.	4.11	-0.69
" + 135 on Pav.	4.17	-0.75
E 1/2 " "	4.24	-0.82
E. Gut	5.16	-1.74
" cb.	4.58	-1.16
Chk. on N.P. B.P.	5.055	1.635

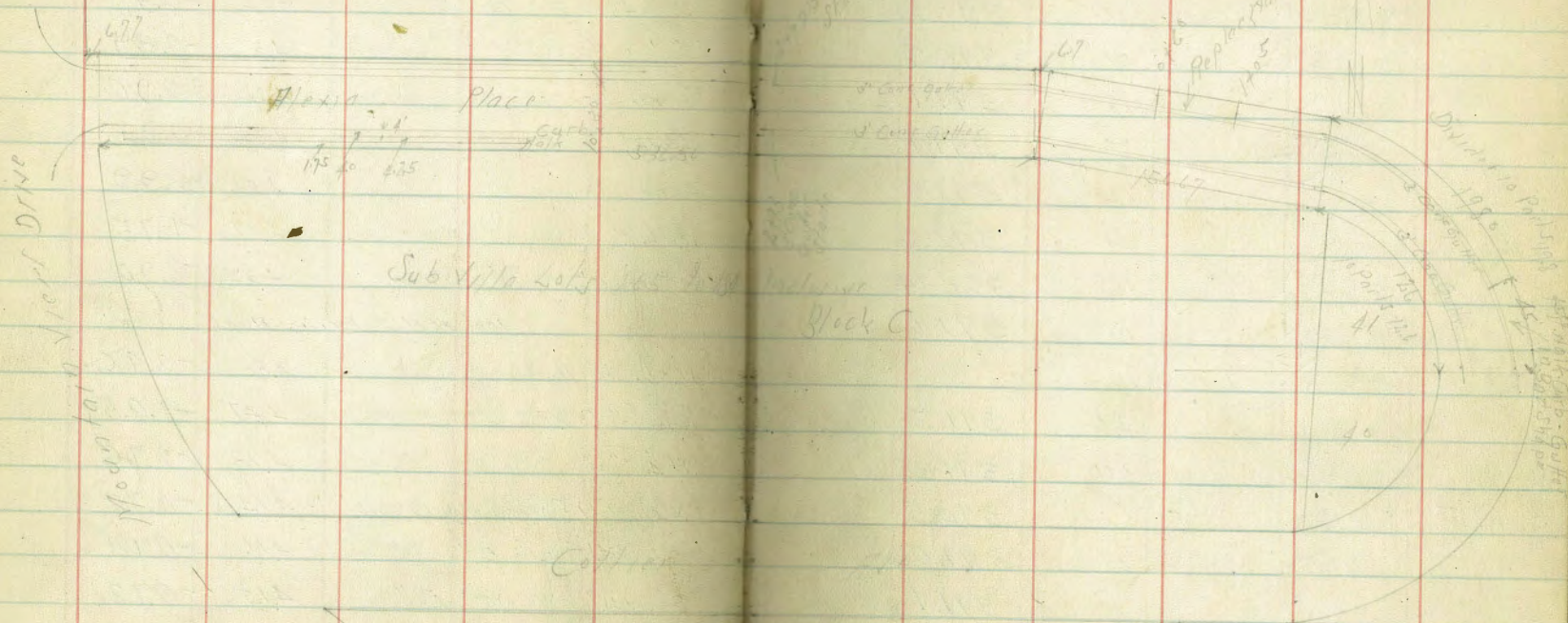
1637 = 511 Book 1344
 0.007 = 1.101 page 12

Alexia Place
Cross Section

50' wide
10' chs
75' Qtr

67

Walk + Car in
Except where noted



Flexia Place
Cross Section

BM	455	395.92	391.37
		Face Line Measurements	50.3274
S		42	391.6
cb Top		44	391.31
Gutter		52	390.7
1/4		48	391.1
1/2		45	391.1
3/4		49	391.0
Gutter		53	390.6
cb Top		45.8	391.34
H		43	391.6
		Face Line Measurements	27.5471
H		41	391.5
cb Top		46	391.26
Gutter		51	390.5
1/4		49	391.0
1/2		48	391.1
3/4		50	390.9
Gutter		52	390.7
cb Top		46	391.31
S		43	391.6
		20' E of F.L.M. View on S	
S		48	391.1
cb		51	390.81
Gutter		55	390.1

Plotted 8-7-29 C.H.V.S.

ok
SMBP
Call 101-22-10

395.78

42		51	390.5
44		52	390.7
46		54	390.5
Gutter		59	390.0
cb Top		51.5	390.77
H		47	391.2
		50' E of F.L.M. View on S	
H		54	390.5
TP	268	422.97	390.39
cb		273	390.24
Gutter		332	389.7
1/4		26	390.4
1/2		26	390.4
3/4		28	390.1
Gutter		24	389.6
cb Top		210	390.37
S		23	390.7
		25	
S		28	391.2
cb Top		301	389.96
Gutter		26	389.4
1/4		32	389.7
1/2		31	389.9
3/4		32	389.7
Gutter		27	389.3
cb Top		225	389.72

68

7-31-29
S. Moran
Rup. Jones
Portland
Oregon

392.97

H	30	390.0
	100 F	
H	35	389.5
cb Top	380	389.17
Gutter	45	388.51
1/4	40	389.01
5	37	389.31
1/4	39	389.1
Gutter in drive	41	388.91
cb top	38	
5	34	389.6
	125 F	
5	28	389.2
cb	409	388.88
Gutter	48	388.2
1/4	46	388.6
2	43	388.7
1/4	46	388.4
Gutter	52	387.7
cb Top	439	388.60
H	43	388.7
	150 F	
H	47	388.3
cb Top	490	388.07
Gutter	57	387.3
1/4	51	387.9

392.97

69

2	47	388.3
1/4	48	388.2
Gutter	50	388.0
cb Top	451	388.41
5	45	388.5
	175 F	
5	49	388.1
cb	509	387.88
Gutter	57	387.3
1/4	54	387.6
2	51	387.9
1/4	57	387.3
Gutter	62	386.7
cb Top	541	387.53
H	52	387.8
	200 F	
1/4	58	387.2
cb Top	603	386.94
Gutter	67	386.3
1/4	64	386.9
2	68	387.2
1/4	59	387.1
Gutter	63	386.7
cb	546	387.45
5	63	387.7
	225 F	

S	57	387.3
cb Top	65	386.92
Gutter	69	386.1
"	63	386.7
S	64	386.6
"	66	386.4
Gutter	71	385.9
cb Top	155	386.42
"	14	386.6
250 F		
"	19	386.1
cb Top	705	385.92
Gutter	78	385.2
"	73	385.7
S	70	386.0
"	70	386.0
Gutter	77	385.3
cb Top	158	386.39
S	64	386.6
275 F		
S	70	386.0
cb Top	712	385.85
Gutter	81	384.9 ³
"	76	385.4
S	75	385.5
"	78	385.2

Gutter	81	384.6
cb Top	763	385.34
"	75	385.5
300 F		
"	81	384.9
cb	822	384.70
Gutter	907	383.90
Edge Gutter	875	384.27
"	85	384.5
S	82	384.8
"	83	384.7
Edge Gutter	817	384.80
Gutter	853	384.49
cb Top	773	385.24
S	75	385.4
325 F		
S	83	384.7
cb Top	851	384.46
Gutter	724	383.73
Edge Gutter	891	384.06
"	89	384.1
S	89	384.1
"	93	383.7
Edge Gutter	953	383.44
Gutter	957	383.10
cb Top	907	383.90

N		90	384.0
	350 F		
H		97	383.3
Gutter in Drive		1070	382.27
Edge Gutter		1031	382.63
"		101	382.9
"		96	383.4
"		96	383.4
Edge Gutter		983	383.15
Gutter in Drive		1010	382.87
S		96	383.8
	375 F		
S		101	382.9
cb Top		1029	382.68
Gutter		1101	381.91
Edge "		1081	382.16
"		106	382.4
"		105	382.5
"		109	382.1
Edge Gutter		1120	381.77
Gutter		1105	381.42
cb Top		1079	382.18
H		105	382.5
	400 F		
H		117	381.6
cb Top		110	381.87 81.37

Gutter		1138	380.57
Edge		1206	379.9 / 380.91
"		117	381.3
"		112	381.6
"		115	381.5
Edge Gutter		1174	381.23
Gutter in Drive		1205	380.92
S		114	381.9
	115 F		
P	117	382.30	1184 381.13
S		114	380.9
cb Top		1158	380.72
Gutter		213	379.87
Edge "		202	380.22
"		17	380.6
"		16	380.6
"		19	380.4
Edge Gutter		225	380.05
Gutter		210	379.70
cb Top		193	380.47
"		11	380.7
	150 F		
"		25	379.8
cb Top		26	379.64
Gutter		214	378.86
Edge "		215	379.17

Alexia Place

382.3'

41	27	379.6
2	25	379.8
41	26	379.7
Edge Gutter	202	379.27
Gutter	223	378.91
Cb Top	256	379.74
N	213	380.0

175'

N	212	379.0
Cb Top	245	378.85
Gutter	223	378.07
Edge	290	378.40
41	26	378.7
2	24	378.90
41	27	378.6
Edge Gutter	296	378.37
Gutter	289	378.01
Cb Top	351	378.76
N	32	379.1

500'

N	41	378.2
Gutter in Drive	521	377.06
Edge Gutter	490	377.40
41	26	377.70
2	23	378.00
41	16	377.70

382.3'

Edge Gutter	111	377.46
Gutter	517	377.13
Cb Top	438	377.92
N	42	378.1
531.561 - 6.993'		
N	51	376.7
Cb Top	580	376.50
Gutter	660	375.70
Edge	630	376.00
41	62	376.1
2	59	376.40
41	61	376.2
Edge Gutter	615	376.15
Gutter	642	375.88
Cb Top	561	376.69
N	54	376.9
4 Point on S 69' of N Point on N		
N	57	376.6
Cb Top	586	376.44
Gutter	666	375.64
Edge	635	375.95
41	62	376.10
2	61	376.2
41	62	376.0
Edge Gutter	637	375.93
Gutter	661	375.66

cb Top	544	376.47
S	56	376.7
	55 F of A	
S	70	375.3
cb Top	725	375.05
Gutter	810	374.20
Edge	791	374.39
1/2	79	374.4
2	71	374.7
1/4	78	374.5
Edge Gutter	803	374.27
Gutter	831	373.99
cb Top	750	374.80
H	73	375.0
	50 F of A	
H	94	372.9
cb Top	910	372.70
Gutter	1040	371.90
Edge	1003	372.7
1/4	95	372.5
2	94	372.9
1/4	96	372.7
Edge Gutter	994	372.36
Gutter	1014	372.16
cb Top	937	372.93
S	91	373.2

	75 F	
S	109	371.4
cb Top	1108	371.12
Gutter	1198	370.32
Edge	1168	370.62
1/2	115	370.8
2	112	371.0
1/4	116	370.7
Edge Gutter	1182	370.48
Gutter	1216	370.14
cb Top	1141	370.89
H	115	370.8
H	108	370.34
	100 F	
H	16	368.7
cb Top	115	369.19
Gutter	125	368.39
Edge	160	368.74
1/2	122	369.05
2	0.9	369.4
1/4	122	369.04
Edge Gutter	1258	368.76
Gutter	1283	368.54
cb	1223	369.31
S	0.7	369.6
	125 F	
S	2.5	367.4

1405 Walk
OK on H

370.34

Cb Top	271	367.63
Gutter	251	366.83
Edge "	285	367.09
"	29	367.4
"	21	367.7
"	29	367.4
Edge Gutter	285	367.09
Gutter	255	366.79
Cb Top	271	367.56
"	27	367.64
	151.67 F-PC	0
"	42	365.91
Cb Top	157	365.77
Gutter	531	365.03
Edge "	502	365.32
"	46	365.74
"	13	366.0
"	41	365.7
Edge Gutter	195	365.39
Gutter	518	365.06
Cb Top	449	365.85
"	42	366.14
	Part 1	
"	17	365.6
Cb Top	502	365.31
Gutter	522	364.51

370.34

74

Edge Gutter	553	364.81
"	53	365.0
"	50	365.3
"	52	364.9
Edge Gutter	575	364.59
Gutter	607	364.28
Cb	521	365.08
"	50	365.3
	Part 2	
"	55	364.8
Cb Top	58	364.5
Gutter	659	363.75
Edge "	630	364.04
"	59	364.4
"	51	364.7
"	58	364.5
Edge Gutter	667	364.28
Gutter	640	363.94
Cb	512	364.72
"	53	365.0
	Part 3	
"	59	364.4
Cb Top	610	364.24
Gutter	687	363.47
Edge "	661	365.70
"	63	364.0

37034

2	60	364.3
1/4	63	364.0
Edge Gutter	66.5	363.69
Gutter	69.5	363.39
Cb Top	61.5	364.19
H	59	364.4
Part 4		
H	63	364.0
Cb Top	64.9	363.85
Gutter	73.0	363.04
Edge	62.8	363.36
1/4	67	363.64
2	65	363.8
1/4	68	363.5
Edge Gutter	70.2	363.32
Gutter	72.1	363.10
Cb Top	64.9	363.85
S	63	364.0
Part 5		
S	65	363.8
Cb Top	68.7	363.47
Gutter	76.6	362.72
Edg. Gutter	73.4	363.00
1/4	72	363.14
2	69	363.4
1/4	71	363.2

37034

75

Edge Gutter	73.5	362.99
Gutter	76.0	362.74
Cb Top	68.5	363.91
H	66	363.7
Part 6		
H	68	363.5
Gutter in Drive	79.7	362.37
Edge Gutter	78.1	362.53
1/4	74	362.94
2	73	363.0
1/4	76	362.7
Edge Gutter	77.0	362.64
Gutter	80.0	362.34
Cb Top	71.9	363.15
S	70	363.3
Part 7		
S	73	363.0
Cb Top	75.8	362.76
Gutter	83.3	362.01
Edg	80.6	362.28
1/4	79	362.4
2	76	362.7
1/4	78	362.5
Edge Gutter	81.2	362.22
Gutter	84.2	361.92
Cb	76.1	362.73

H	75	362.8	
	Part 8		
H	82	362.3	5.7 inch P1118
Cb Top	831	362.03	Subst. Malt Spd
Gutter	904	361.30	2.5 inch
Edge	811	361.73	
H	83	362.14	
S	80	362.3	
H	84	361.9	
Edge Gutter	849	361.85	
Gutter	879	361.55	
Cb Top	861	362.33	
S	77	362.64	
	Part 9		
S	82	362.1	
Cb Top	841	361.86	
Gutter	923	361.11	
Edge Gutter	892	361.42	
H	87	361.6	
S	84	361.9	
H	88	361.5	
Edge Gutter	911	361.10	
Gutter	986	360.98	
Cb	908	361.26	
H	81	361.74	

Part 10

H			8.8	361.5
Cb Top			9.51	360.8
Gutter			10.38	359.96
Edge			9.86	360.48
H			9.1	361.2
S			8.7	361.6
H			9.1	361.2
Edge Gutter			9.40	360.94
Gutter			9.70	360.69
Cb Top			9.88	361.46
S			8.60	361.74
S	12.43	382.44	0.33	370.01
TP	10.13	391.50	0.07	382.27
TP	5.22	396.30	1.53	390.97
S			4.82	391.32

SNOP
GUTTER & MALT
37137

OK

Robinson Ave.
Alabama to Florida

Other Notes on Page 28

12-30-29

BM	102	275.92		273.96	SJKBP. Robinson + Florida
TP	0.96	214.96	11.92	264.00	
TP	0.52	252.48	12.00	251.91	

233 H of HL Alabama

H.L. Robinson		122		240.3
12 H of HL		85		241.0
85 H		1.1		248.1

237 H - F.L. Alley

25 H of H.L.		3.5		249.0
20 H		3.6		248.9
10 H		7.0		245.5
H.L. Robinson		101		242.4

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DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 1/2 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body

of table in same row and column gives distance from side stake to slope stake. If ground is not

level, the side stake and slope stake, lower tangent by the amount of cut, elevation of fill. Add this amount to cut or fill and find distance in table. Set up rod at this point and line of sight should cut tangent.

**IMPROVED TABLES
AND
INFORMATION**

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given L may be found by dividing tangent (or external), opposite L by given tangent (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

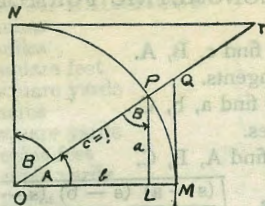


TABLE II
TRIGONOMETRIC FORMULÆ.

$$\angle A = \angle MOP \quad \angle B = \angle PON = \angle OPL$$

$$R = OB = c = 1$$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

$$\sin \frac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \quad \cos \frac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \quad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Sines} \quad \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{C}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$$

TABLE VI (continued)
SINES, COSINES, TANGENTS, COTANGENTS (continued)

deg.	sin 0'	tan 0'	sin 10'	tan 10'	sin 20'	tan 20'	sin 30'	tan 30'	sin 40'	tan 40'	sin 50'	tan 50'	deg.
46	7193	1.0355	7214	1.0416	7234	1.0477	7254	1.0533	7274	1.0599	7294	1.0661	43
47	314	.0724	333	.0786	353	.0850	373	.0913	392	.0977	412	.1041	42
48	431	.1106	451	.1171	470	.1237	490	.1303	509	.1369	528	.1436	41
49	547	.1504	566	.1571	585	.1640	604	.1708	623	.1778	642	.1847	40
50	660	.1918	7679	1.1988	7698	1.2059	7716	1.2131	7735	1.2203	7753	1.2276	39
51	771	.2349	790	.2423	808	.2497	826	.2572	844	.2647	862	.2723	38
52	880	.2799	898	.2876	916	.2954	934	.3032	951	.3111	969	.3190	37
53	986	.3270	8004	.3351	8021	.3432	8039	.3514	8056	.3597	8073	.3680	36
54	8090	.3764	107	.3848	124	.3934	141	.4019	158	.4106	175	.4193	35
55	192	.4281	208	.4370	225	.4460	241	.4550	258	.4641	274	.4733	34
56	290	.4826	307	.4919	323	.5013	339	.5108	355	.5204	371	.5301	33
57	387	.5399	403	.5497	418	.5597	434	.5697	450	.5798	465	.5900	32
58	480	.6003	496	.6107	511	.6212	526	.6319	542	.6426	557	.6534	31
59	572	.6643	587	.6753	601	.6864	615	.6977	631	.7090	646	.7205	30
60	660	1.7321	8675	1.7437	8689	1.7556	8704	1.7675	8718	1.7797	8732	1.7917	29
61	746	.8040	760	.8165	774	.8291	788	.8418	802	.8546	816	.8676	28
62	829	.8807	843	.8940	857	.9074	870	.9210	884	.9347	897	.9486	27
63	910	.9626	923	.9768	936	.9912	949	2.0057	962	2.0204	975	2.0353	26
64	988	2.0503	9001	2.0655	9013	2.0809	9026	.0965	9038	.1123	9051	.1283	25
65	9063	.1445	075	.1609	088	.1775	100	.1943	112	.2113	124	.2286	24
66	135	.2460	147	.2637	159	.2817	171	.2998	182	.3183	194	.3369	23
67	205	.3559	216	.3750	228	.3945	239	.4142	250	.4342	261	.4545	22
68	272	.4751	283	.4960	293	.5172	304	.5386	315	.5605	325	.5826	21
69	336	.6051	346	.6279	356	.6511	367	.6746	377	.6985	387	.7228	20
70	397	2.7475	9407	2.7725	9417	2.7980	9426	2.8239	9436	2.8502	9446	2.8770	19
71	455	.9042	465	.9319	474	.9600	483	.9887	492	3.0178	502	3.0475	18
72	511	3.0777	520	3.1084	528	3.1397	537	3.1716	546	.2041	555	.2371	17
73	563	.2709	572	.3052	580	.3402	588	.3759	596	.4124	605	.4495	16
74	613	.4874	621	.5261	628	.5656	636	.6059	644	.6470	652	.6891	15
75	659	.7321	667	.7760	674	.8208	681	.8657	689	.9136	696	.9617	14
76	703	4.0108	710	4.0611	717	4.1126	724	4.1653	730	4.2193	737	4.2747	13
77	744	.3315	750	.3897	757	.4494	763	.5107	769	.5736	775	.6382	12
78	781	.7046	787	.7729	793	.8430	799	.9152	805	.9894	811	5.0658	11
79	816	.1446	822	5.2257	827	5.3093	833	5.3955	838	5.4845	843	.5764	10
80	9848	5.6713	9853	5.7694	9858	5.8708	9863	5.9758	9868	6.0844	9872	6.1970	9
81	877	6.3138	881	6.4348	886	6.5606	890	6.6912	894	.8269	899	.9632	8
82	903	7.1154	907	7.2687	911	7.4287	914	7.5958	918	7.7704	922	7.9530	7
83	925	8.1443	929	8.3450	932	8.5555	936	8.7769	939	9.0098	942	9.2553	6
84	945	9.5144	948	9.7882	951	10.0778	954	10.3855	957	10.7111	959	11.059	5
85	962	11.430	964	11.826	967	12.250	969	12.706	971	13.197	974	13.727	4
86	976	14.300	978	14.924	980	15.605	981	16.350	983	17.169	985	18.075	3
87	986	19.081	988	20.206	989	21.470	990	22.903	992	24.542	993	26.432	2
88	994	28.636	995	31.242	996	34.368	997	38.189	997	42.964	998	49.104	1
89	9998	57.290	9999	63.750	9999	85.940	9999	114.58	1.000	171.88	1.000	343.77	0
deg.	60'	60'	50'	50'	40'	40'	30'	30'	20'	30'	10'	10'	deg.
cos	cot	cos	cot	cos	cot	cos	cot	cos	cot	cos	cot	cos	cot

533
607
074

TABLE VII
RODS IN FEET AND INCHES

Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches
1	16-6	21	346-6	41	676-6	61	1006-6	81	1336-6
2	33-0	22	363-0	42	693-0	62	1023-0	82	1353-0
3	49-6	23	379-6	43	709-6	63	1039-6	83	1369-6
4	66-0	24	396-0	44	726-0	64	1056-0	84	1386-0
5	82-6	25	412-6	45	742-6	65	1072-6	85	1402-6
6	99-0	26	429-0	46	759-0	66	1089-0	86	1419-0
7	115-6	27	445-6	47	775-6	67	1105-6	87	1435-6
8	132-0	28	462-0	48	792-0	68	1122-0	88	1452-0
9	148-6	29	478-6	49	808-6	69	1138-6	89	1468-6
10	165-0	30	495-0	50	825-0	70	1155-0	90	1485-0
11	181-6	31	511-6	51	841-6	71	1171-6	91	1501-6
12	198-0	32	528-0	52	858-0	72	1188-0	92	1518-0
13	214-6	33	544-6	53	874-6	73	1204-6	93	1534-6
14	231-0	34	561-0	54	891-0	74	1221-0	94	1551-0
15	247-6	35	577-6	55	907-6	75	1237-6	95	1567-6
16	264-0	36	594-0	56	924-0	76	1254-0	96	1584-0
17	280-6	37	610-6	57	940-6	77	1270-6	97	1600-6
18	297-0	38	627-0	58	957-0	78	1287-0	98	1617-0
19	313-6	39	643-6	59	973-6	79	1303-6	99	1633-6
20	330-0	40	660-0	60	990-0	80	1320-0	100	1650-0

TABLE VIII
LINKS IN FEET AND INCHES

Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches
1	0-7.92	18	11-10.56	35	23-1.20	52	34-3.84	69	45-6.48	86	56-9.12
2	1-3.84	19	12-6.48	36	23-9.12	53	34-11.76	70	46-2.40	87	57-5.04
3	1-11.76	20	13-2.40	37	24-5.04	54	35-7.68	71	46-10.32	88	58-0.96
4	2-7.68	21	13-10.32	38	25-0.96	55	36-3.60	72	47-6.24	89	58-8.88
5	3-3.60	22	14-6.24	39	25-8.88	56	36-11.52	73	48-2.16	90	59-4.80
6	3-11.52	23	15-2.16	40	26-4.80	57	37-7.44	74	48-10.08	91	60-0.72
7	4-7.44	24	15-10.08	41	27-0.72	58	38-3.36	75	49-6.00	92	60-8.64
8	5-3.36	25	16-6.00	42	27-8.64	59	38-11.28	76	50-1.92	93	61-4.56
9	5-11.28	26	17-1.92	43	28-4.56	60	39-7.20	77	50-9.84	94	62-0.48
10	6-7.20	27	17-9.84	44	29-0.48	61	40-3.12	78	51-5.76	95	62-8.40
11	7-3.12	28	18-5.76	45	29-8.40	62	40-11.04	79	52-1.68	96	63-4.32
12	7-11.04	29	19-1.68	46	30-4.32	63	41-6.96	80	52-9.60	97	64-0.24
13	8-6.96	30	19-9.60	47	31-0.24	64	42-2.88	81	53-5.52	98	64-8.16
14	9-2.88	31	20-5.52	48	31-8.16	65	42-10.80	82	54-1.44	99	65-4.08
15	9-10.80	32	21-1.44	49	32-4.08	66	43-6.72	83	54-9.36	100	66-0.00
16	10-6.72	33	21-9.36	50	33-0.00	67	44-2.64	84	55-5.28	101	66-7.92
17	11-2.64	34	22-5.28	51	33-7.92	68	44-10.56	85	56-1.20	102	67-3.84

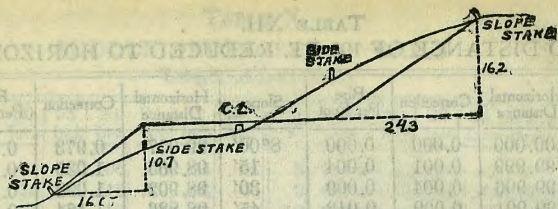
TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=10°	I	T	E	I=20°	I	T	E	I=30°
1°	50.00	.218	+	11°	551.70	26.500	+	21°	1061.9	97.577	+
10'	58.34	.297	5° C.	10'	560.11	27.313	5° C.	10'	1070.6	99.155	5° C.
20'	66.67	.388	T	20'	568.53	28.137	T	20'	1079.2	100.75	T
30'	75.01	.491	E	30'	576.95	28.974	E	30'	1087.8	102.35	E
40'	83.34	.606	.03	40'	585.36	29.824	.06	40'	1096.4	103.97	.10
50'	91.68	.733	E	50'	593.79	30.686	E	50'	1105.1	105.60	E
2°	100.01	.873	.001	12°	602.21	31.561	.006	22°	1113.7	107.24	.013
10'	108.35	1.024	10° C.	10'	610.64	32.447	10° C.	10'	1122.4	108.90	10° C.
20'	116.68	1.188	T	20'	619.07	33.347	T	20'	1131.0	110.57	T
30'	125.02	1.364	E	30'	627.50	34.259	E	30'	1139.7	112.25	E
40'	133.36	1.552	.03	40'	635.93	35.183	.06	40'	1148.4	113.95	.10
50'	141.70	1.752	E	50'	644.37	36.120	E	50'	1157.0	115.66	E
3°	150.04	1.964	10° C.	13°	652.81	37.070	10° C.	23°	1165.7	117.38	10° C.
10'	158.38	2.188	T	10'	661.25	38.031	T	10'	1174.4	119.12	T
20'	166.72	2.425	E	20'	669.70	39.006	E	20'	1183.1	120.87	E
30'	175.06	2.674	.06	30'	678.15	39.993	.13	30'	1191.8	122.63	.19
40'	183.40	2.934	T	40'	686.60	40.992	T	40'	1200.5	124.41	T
50'	191.74	3.207	.003	50'	695.06	42.004	.011	50'	1209.2	126.20	.025
4°	200.08	3.492	15° C.	14°	703.51	43.029	15° C.	24°	1217.9	128.00	15° C.
10'	208.43	3.790	T	10'	711.97	44.066	T	10'	1226.6	129.82	T
20'	216.77	4.099	E	20'	720.44	45.116	E	20'	1235.3	131.65	E
30'	225.12	4.421	.03	30'	728.90	46.178	.06	30'	1244.0	133.50	.10
40'	233.47	4.755	T	40'	737.37	47.253	T	40'	1252.8	135.35	T
50'	241.81	5.100	E	50'	745.85	48.341	E	50'	1261.5	137.23	E
5°	250.16	5.459	20° C.	15°	754.32	49.441	20° C.	25°	1270.2	139.11	20° C.
10'	258.51	5.829	T	10'	762.80	50.554	T	10'	1279.0	141.01	T
20'	266.86	6.211	E	20'	771.29	51.679	E	20'	1287.7	142.93	E
30'	275.21	6.606	.04	30'	779.77	52.818	.07	30'	1296.5	144.85	.10
40'	283.57	7.013	T	40'	788.26	53.969	T	40'	1305.3	146.79	T
50'	291.92	7.432	E	50'	796.75	55.132	E	50'	1314.0	148.75	E
6°	300.28	7.863	25° C.	16°	805.25	56.309	25° C.	26°	1322.8	150.71	25° C.
10'	308.64	8.307	T	10'	813.75	57.498	T	10'	1331.6	152.69	T
20'	316.99	8.762	E	20'	822.25	58.699	E	20'	1340.4	154.69	E
30'	325.35	9.230	.06	30'	830.76	59.914	.09	30'	1349.2	156.70	.13
40'	333.71	9.710	T	40'	839.27	61.141	T	40'	1358.0	158.72	T
50'	342.08	10.202	E	50'	847.78	62.381	E	50'	1366.8	160.76	E
7°	350.44	10.707	30° C.	17°	856.30	63.634	30° C.	27°	1375.6	162.81	30° C.
10'	358.81	11.224	T	10'	864.82	64.900	T	10'	1384.4	164.86	T
20'	367.17	11.753	E	20'	873.35	66.178	E	20'	1393.2	166.95	E
30'	375.54	12.294	.08	30'	881.88	67.470	.11	30'	1402.0	169.04	.15
40'	383.91	12.847	T	40'	890.41	68.774	T	40'	1410.9	171.15	T
50'	392.28	13.413	E	50'	898.95	70.091	E	50'	1419.7	173.27	E
8°	400.66	13.991	35° C.	18°	907.49	71.421	35° C.	28°	1428.6	175.41	35° C.
10'	409.03	14.582	T	10'	916.03	72.764	T	10'	1437.4	177.55	T
20'	417.41	15.184	E	20'	924.58	74.119	E	20'	1446.3	179.72	E
30'	425.79	15.799	.10	30'	933.13	75.488	.13	30'	1455.1	181.89	.17
40'	434.17	16.426	T	40'	941.69	76.869	T	40'	1464.0	184.08	T
50'	442.55	17.065	E	50'	950.25	78.264	E	50'	1472.9	186.29	E
9°	450.93	17.717	40° C.	19°	958.81	79.671	40° C.	29°	1481.8	188.51	40° C.
10'	459.32	18.381	T	10'	967.38	81.092	T	10'	1490.7	190.74	T
20'	467.71	19.058	E	20'	975.96	82.525	E	20'	1499.6	192.99	E
30'	476.10	19.746	.12	30'	984.53	83.972	.15	30'	1508.5	195.25	.19
40'	484.49	20.447	T	40'	993.12	85.431	T	40'	1517.4	197.53	T
50'	492.88	21.161	E	50'	1001.7	86.904	E	50'	1526.3	199.82	E
10°	501.28	21.887	45° C.	20°	1010.3	88.389	45° C.	30°	1535.3	202.12	45° C.
10'	509.68	22.624	T	10'	1018.9	89.888	T	10'	1544.2	204.44	T
20'	518.08	23.375	E	20'	1027.5	91.399	E	20'	1553.1	206.77	E
30'	526.48	24.138	.14	30'	1036.1	92.924	.17	30'	1562.1	209.12	.21
40'	534.89	24.913	T	40'	1044.7	94.462	T	40'	1571.0	211.48	T
50'	543.29	25.700	E	50'	1053.3	96.013	E	50'	1580.0	213.86	E

T = R tan 1/2 I E = R exsec 1/2 I

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=40°	I	T	E	I=50°	I	T	E	I=60°
31°	1589.0	216.3	+	41°	2142.2	387.4	+	51°	2732.9	618.4	+
10'	1598.0	218.7	5° C.	10'	2151.7	390.7	5° C.	10'	2743.1	622.8	5° C.
20'	1606.9	221.1	T	20'	2161.2	394.1	T	20'	2753.4	627.2	T
30'	1615.9	223.5	E	30'	2170.8	397.4	E	30'	2763.7	631.7	E
40'	1624.9	226.0	.13	40'	2180.3	400.8	.17	40'	2773.9	636.2	.21
50'	1633.9	228.4	E	50'	2189.9	404.2	E	50'	2784.2	640.7	E
32°	1643.0	230.9	.023	42°	2199.4	407.6	.037	52°	2794.0	645.2	.056
10'	1652.0	233.4	10° C.	10'	2209.0	411.1	10° C.	10'	2804.9	649.7	10° C.
20'	1661.0	235.9	T	20'	2218.6	414.5	T	20'	2815.2	654.3	T
30'	1670.0	238.4	E	30'	2228.1	418.0	E	30'	2825.6	658.8	E
40'	1679.1	241.0	.03	40'	2237.7	421.4	.04	40'	2835.9	663.4	.04
50'	1688.1	243.5	E	50'	2247.3	425.0	E	50'	2846.3	668.0	E
33°	1697.2	246.1	10° C.	43°	2257.0	428.5	10° C.	53°	2856.7	672.7	10° C.
10'	1706.3	248.7	T	10'	2266.6	432.0	T	10'	2867.1	677.3	T
20'	1715.3	251.3	E	20'	2276.2	435.6	E	20'	2877.5	682.0	E
30'	1724.4	253.9	.26	30'	2285.9	439.2	.34	30'	2888.0	686.7	.42
40'	1733.5	256.5	T	40'	2295.6	442.8	T	40'	2898.4	691.4	T
50'	1742.6	259.1	E	50'	2305.2	446.4	E	50'	2908.9	696.1	E
34°	1751.7	261.8	.046	44°	2314.9	450.0	.075	54°	2919.4	700.9	.112
10'	1760.8	264.5	15° C.	10'	2324.6	453.6	15° C.	10'	2929.9	705.7	15° C.
20'	1770.0	267.2	T	20'	2334.3	457.3	T	20'	2940.4	710.5	T
30'	1779.1	269.9	E	30'	2344.1	461.0	E	30'	2951.0	715.3	E
40'	1788.2	272.6	.03	40'	2353.8	464.6	.03	40'	2961.5	720.1	.03
50'	1797.4	275.3	E	50'	2363.5	468.4	E	50'	2972.1	725.0	E
35°	1806.6	278.1	20° C.	45°	2373.3	472.1	20° C.	55°	2982.7	729.9	20° C.
10'	1815.7	280.8	T	10'	2383.1	475.8	T	10'	2993.3	734.8	T
20'	1824.9	283.6	E	20'	2392.8	479.6	E	20'	3003.9	739.7	E
30'	1834.1	286.4	.07	30'	2402.6	483.4	.08	30'	3014.5	744.6	.08
40'	1843.3	289.2	T	40'	2412.4	487.2	T	40'	3025.2	749.6	T
50'	1852.5	292.0	E	50'	2422.3	491.0	E	50'	3035.8	754.6	E
36°	1861.7	294.9	.070	46°	2432.1	494.8	.116	56°	3046.5	759.6	.168
10'	1870.9	297.7	25° C.	10'	2441.9	498.7	25° C.	10'	3057.2	764.6	25° C.
20'	1880.1	300.6	T	20'	2451.8	502.5	T	20'	3067.9	769.7	T
30'	1889.4	303.5	E	30'	2461.7	506.4	E	30'	3078.7	774.7	E
40'	1898.6	306.4	.20	40'	2471.5	510.3	.20	40'	3089.4	779.8	.20
50'	1907.9	309.3	T	50'	2481.4	514.3	T	50'	3100.2	784.9	T
37°	1917.1	312.2	.39	47°	2491.3	518.2	.39	57°	3110.9	790.1	.39
10'	1926.4	315.2	E	10'	2501.2	522.2	E	10'	3121.7	795.2	E
20'	1935.7	318.1	.093	20'	2511.2	526.1	.151	20'	3132.6	800.4	.225
30'	1945.0	321.1	T	30'	2521.1	530.1	T	30'	3143.4	805.6	T
40'	1954.3	324.1	E	40'	2531.1	534.2	E	40'	3154.2	810.9	E
50'	1963.6	327.1	.53	50'	2541.0	538.2	.53	50'	3165.1	816.1	.53
38°	1972.9	330.2	.093	48°	2551.0	542.2	.093	58°	3176.0	821.4	.283
10'	1982.2	333.2	30° C.	10'	2561.0	546.3	30° C.	10'	3186.9	826.7	30° C.
20'	1991.5	336.3	T	20'	2571.0	550.4	T	20'	319		



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/4 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 05	1 20	1 35	1 50	1 65	1 80	1 95	2 10	2 25	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
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47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

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ENGINEERING DEPARTMENT
 CITY OF CALIFORNIA
 SAN DIEGO

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68 - handis to Wightman 4th to Central
 81 - " " Dwight
 95 Myrtle "
 109 " Thorn
 124 Redwood "

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 Verona Ct
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 Whittier Ct
 533
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221 + 229
 241 + 240
 YARMOUTH Ct
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 Yark Ct
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 ZANZIBAR Ct
 North 11/16