

1312

1312

AST

LEVEL BOOK

No. 380 F

1312

16° 34' - Angle between Swift  
& Wabash

59805 - Myrtle to Dwight

Angle Between Wabash  
& Vancouver - 22° 40'

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- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
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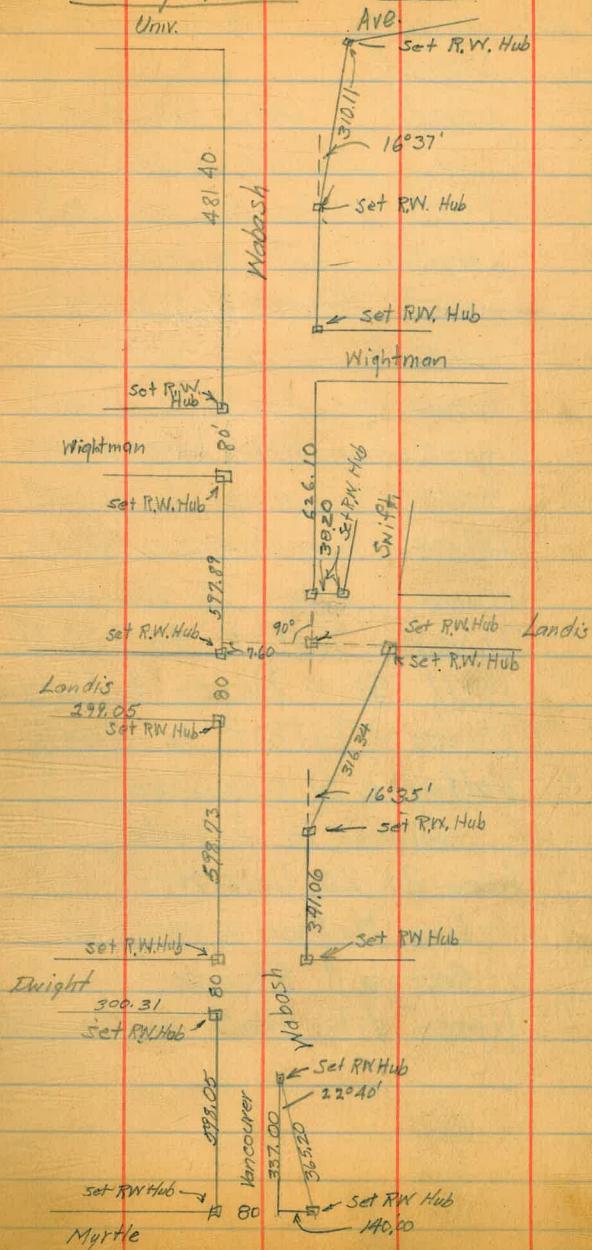
Notes copied  
By T.G. Hawley

1312

Surveyed By  
J.C. Bliss

Survey Wabash

Univ. Ave to Myrtle



X Sec.	Landis	Nile to Wabash	1
" "	Dwight	" " "	4
" "	Landis	Swift & Wabash Intersection	7
" "	"	EL Swift 75' East.	8 1/2
" "	Swift	N.L. Landis 100' North	9
" "	Landis	35th to Swift	10
" "	Landis	Triangle EL Wabash & EL Swift	12
" "	Wabash	Landis to Myrtle	15
" "	Vancouver	Myrtle to Dwight	22
" "	Creek Bed on	Wabash Dwight to Myrtle	29
" "	Grant & Garnet	intersection	34
" "	Upas	Villa Terrace to Arnold	44
" "	Plum	Alcott to Browning	49
" "	Dover	Talbot to 700' N.	55
" "	Hill St.	Dover to Concord	57
" "	Dover	Talbot to Inez	58
" "	Voltaire St.	sidewalks -	59
" "	Venice to Froude		
" "	Alley Bk. 23,	Univ. Hts.	71
" "	from Madison	to Adams bet.	
" "	Georgia & Florida		
" "	Upas, Villa Tract	to Arnold	75

2-4-29  
J.C. Bliss  
Drabert  
Raucy

X-section Landis Street  
Nile to Wabash - 80' wide  
14' c.b.s  
13' 1/2

1

B.M. N.E.B.P. Boundary & Landis

329.04

+ 2.18

H.I. 331.22

E.L. Mile = 0 + 100

N		9.1	322.1
Top existing return		9.20	322.02
Gutter		9.6	321.6
1/4		9.4	321.8
1/4		9.4	321.8
1/4		9.5	321.7
Gutter		9.7	321.5
Top existing end return		8.85	322.47
S		9.0	322.2
		0 + 25	
S		10.1	320.5
cb		10.6	320.6
1/4		10.6	320.6
1/4		10.5	320.7
1/4		10.3	320.9
cb		10.4	320.8
N		10.0	321.2
		0 + 50	
N		11.0	320.2
cb		10.9	320.3
1/4		11.3	319.9

B/25/29  
T.H.

Plotted

H. I. 331.22

H. I. 318.41

2

¢	11.3	319.9
1/4	11.5	319.7
cb	11.7	319.5
S	11.8	319.4

1475

S	12.6	318.6
cb	12.5	318.7
1/4	12.2	319.0
¢	11.9	319.3
1/4	11.9	319.3
cb	11.7	319.5
N	11.7	319.5

1400

N	12.3	318.9
cb	12.3	318.9
1/4	12.6	318.6
¢	12.9	318.3
1/4	13.0	318.2
cb	13.0	318.2
S	13.5	317.7

T. P. -13.03 318.19

+0.22

H. I. 318.41 ✓

1425

S	1.3	317.1
cb	1.0	317.4

1/4

¢

1/4

cb

1

N

cb

1/4

¢

1/4

cb

S

S

cb

1/4

¢

1/4

cb

N

0.8

0.7

0.4

0.3

0.1

0.6

0.5

0.7

1.0

1.3

1.7

1.9

2.7

2.3

2.2

1.8

1.7

1.6

1.5

317.6

317.7

318.0

318.1

318.3

317.8

317.9

317.7

317.4

317.1

316.7

316.5

315.7

314.1

316.2

316.6

316.7

316.8

316.9

1450

1475

1473. Walk at N.U.

1.11

317.30

H.I. 318.41

2+00

N	2.6	315.8
cb	2.8	315.6
114	3.0	315.4
♀	3.1	315.3
114	3.2	315.2
cb	3.3	315.1
S	3.8	314.6

2+25

S	5.3	313.1
cb	4.9	313.5
114	4.6	313.8
♀	4.5	313.9
114	4.3	314.1
cb	4.1	314.3
N	4.0	314.4

2+30

4' walk at N.L.	3.74	314.67
-----------------	------	--------

2+37

N	4.4	314.0
cb	4.8	313.6
114	5.0	313.4
♀	5.2	313.2
114	5.2	313.2
cb	5.5	312.9
S	6.6	311.8

H.I. 318.41

2+50

S	10.0	308.4
45	7.8	308.6
114	6.8	311.6
cb	6.6	311.8
114	6.2	312.2
♀	5.6	312.8
114	5.6	312.8
cb	5.7	312.7
N	5.6	312.8

2+65

N	6.3	312.1
cb	6.4	312.0
114	6.7	311.7
♀	7.1	311.3
114	8.2	310.2
cb	13.6	304.8
S	17.3	301.1

2+75

S	22.8	295.6
cb	21.3	297.1
114	15.1	303.3
♀	12.5	305.9
114	7.8	309.4
cb	7.2	311.2
N	7.5	310.9

3

H.I. 318.41

2 + 99.05 W.L. Wabash

N	15.0	303.4
cb	19.1	299.3
1/4	23.6	294.8
1/2	26.5	291.9
1/4	29.5	288.9
cb	33.5	284.9
S	35.5	282.9
T.P.		-0.22 318.19

1125 330.34

B.M. N.E.B.P. Boundary Landis -1.30 329.04  
 329.04

2-4-29 X-section Dwight Street  
 J.C. Bliss Nile to Wabash - 80' wide  
 Drebert 14' cbs  
 Roney 13' 1/2"

4

B.M. N.E.B.P. Dwight and Nile

317.15

	+3.00	
		H.I. 320.15
E.L. Nile =	0+00	
N		2.8
Top existing end return		3.04
Gutter		3.5
1/4		3.8
1/2		3.7
1/4		3.8
Gutter		4.1
Top existing end return		3.60
S		4.0
	0+25	
S		3.7
cb		3.8
1/4		3.6
1/2		3.2
1/4		3.1
cb		2.6
N		1.4
	0+50	
N		1.3
cb		2.3
1/4		2.9

H.I. 320.15

H.I. 320.15

5

1425

¢	3.0
1/4	2.8
cb	2.7
S	2.4

0435

2.5' Concrete walk at SL. 337

0457

2.0' Concrete walk at SL. 302

0475

S	3.2
cb	2.9
1/4	2.5
¢	2.5
1/4	2.4
cb	2.1
N	1.7

1400

N	1.6
cb	1.7
1/4	1.7
¢	2.0
1/4	2.3
cb	2.7
S	3.2

S

cb

1/4

¢

1/4

cb

N

N

cb

1/4

¢

1/4

cb

S

S

T.P

cb

1/4

¢

1/4

cb

N

3.5

2.9

2.7

2.5

2.4

2.3

2.2

4.0

4.9

5.0

5.0

5.7

4.8

4.7

10.9

- 12.73 307.42

10.21

H.I. 307.63

0.9

3.1

3.2

4.6

3.8

1.3



H.I. 307.63

H.I. 271.72

6

T.P.		-12.77	294.86
+1.24			
	H.I. 296.10		
	2100		
N	6.2		
cb	7.5		
1/4	8.0		
£	8.8		
1/4	7.9		
cb1	5.8		
S	1.6		
T.P.		-12.58	283.72
+0.50			
	H.I. 284.22		
	2125		
S	2.5		
cb	6.7		
1/4	9.6		
£	12.0		
1/4	11.2		
cb	11.0		
N	9.1		
T.P.		-13.20	271.02
+0.10			
	H.I. 271.72		
	2150		
1	9.5		262.2

cb	10.8	260.9
1/4	11.0	260.7
£	11.0	260.7
1/4	7.7	262.0
cb	6.4	265.3
S	2.8	268.9
T.P.		-13.00
		258.22
	+7.02	
	H.I. 265.74	
	2175	
S	7.4	258.3
cb	9.1	256.6
1/4	9.4	256.3
£	9.4	256.3
1/4	10.2	255.5
cb	10.0	255.7
N	10.0	255.7
	3100.31 = W.L. Wobash	
N	11.6	251.1
cb	12.0	153.7
1/4	12.3	153.4
£	12.7	153.0
1/4	12.8	152.9
cb	12.9	152.8
S	12.2	153.5

H.I. 265.74

B.M. N.E. Prop Hub Dwight Wobash - 14.5 251.18

2-9-29 X-section Landis-Swigt + Wobash  
J.C. Bliss Intersection - Landis 80' wide  
Drebert 11' cbs  
Kouner 18' 1/2  
Swigt 80' wide

7

B.M. S.E. Nails Landis + Swigt. 285.94

+1.80 H.I. 287.74

N.L. Landis - on Swigt St. Paving

E.T. ob	2.50	285.24
Gutter	3.15	284.59
1/4	3.08	284.66
1/4	3.28	284.46
Gutter	3.66	284.08
W.T. ob.	4.16	283.58
W.L. Swigt	3.55	284.19
+19 - Top fill	3.3	284.4
+22	4.4	283.3
+38.2 - E.L. Wobash	9.2	278.5
	16.1	271.6
	N c b Landis	
E.L. Wobash	12.0	275.7
+14 - Top fill	3.0	284.7
+34 - W.L. Swigt	3.6	284.1
cb	4.0	283.7
1/4	3.7	284.0
1/4	3.2	284.5
1/4	3.3	284.4
cb.	3.0	284.7
E.L. Swigt - Gutter	3.0	284.7
Top ob	2.48	285.26

Contours Plotted  
C.B.H. 2/22-29

H.I. 287.74

N 1/4 Landis

E.L. Swift	3.1	284.6
cb	3.4	284.3
1/4	3.5	284.4
♀	3.3	284.4
1/4	3.9	283.8
cb	4.5	283.2
W.L. Swift	4.2	283.5
+ 20 - Top Fill	3.7	284.0
+ 30.4 E.L. Wabash	9.8	277.9
	♀ Landis	
E.L. Wabash	10.0	277.7
+ 8 - Top Fill	4.5	283.2
4127.2 = W.L. Swift	4.0	283.7
cb	4.3	283.4
1/4	3.8	283.9
♀	3.5	284.2
1/4	3.6	284.1
cb	3.9	283.8
E.L. Swift	2.1	285.6
	S 1/4 Landis	
E.L. Swift	2.7	285.0
cb	4.1	283.6
1/4	3.9	283.8
♀	3.8	283.9
1/4	4.1	283.6

H.I. 287.74

8

cb	4.6	283.1
W.L. Swift	4.4	283.3
+ 13 - Top Fill	4.1	283.6
+ 24 = E.L. Wabash	9.1	278.6
	S cb Landis	
E.L. Wabash	6.8	280.9
+ 10	4.8	282.9
+ 19.4 = W.L. Swift	5.0	282.7
cb	5.0	282.7
1/4	4.5	283.2
♀	4.3	283.4
1/4	4.3	283.4
cb	4.3	283.4
E.L. Swift	4.8	284.9
	S L Landis	
E.L. Swift	3.5	284.2
cb	4.8	282.9
1/4	4.7	283.5
♀	4.1	283.6
1/4	5.0	282.7
cb	6.6	281.1
W.L. Swift	7.2	280.5
+ 14.46 = E.L. Wabash Top Fill	6.8	280.9

1-9-29 Levels on existing Improvements on  
 J.C. Bliss Landis from E.L. Swift to 75' East of  
 E.L. Swift

B.M. S.E. Nails Landis + Swift 285.94

+ 72.06

298.00

H.I. ~~288.0~~

E.L. Swift = 0+00

North Edge of sidewalk - South side Landis 13.65 289.35

N Top cb 12.73 285.27

0+25

N Edge Walk South side 9.67 288.33

North Top cb 8.97

0+50

N Edge Walk - South side 5.86

North Top cb 5.12

0+75

N Edge Walk - South side 1.86

North Top cb 1.27

Levels on existing Improvements on  
 Swift from N.L. Landis to 100' North  
 of N.L. Landis

B.M. S.E. Nails Landis + Swift 285.94

+ 11.03

H.I. 296.97

N.L. Landis = 0+00

E Top cb 11.72 285.25

W " " 12.78 284.19

0+25

E Top cb 9.59 287.38

W " " 10.60 286.37

0+50

E Top cb 7.44 289.53

W " " 8.50 288.47

0+75

E Top cb 5.30 291.67

W " " 6.32 290.45

1+00

E Top cb 3.09 293.88

W Top " 4.09 292.88

2-25-28 X-section lands ST 35<sup>th</sup> to  
 J.C. Bliss  
 Paaner  
 Brooks  
 Swist - 80' wide - 14' cbs - 13' 1/2"

H.I. 327.83

10

B.M. N.W.C.P 35<sup>th</sup> + Lands 326.34

+ 1.49

H.I. 327.83

W.L. 35<sup>th</sup> = 0+00

N Top existing cb. 1.64 326.19

Gutter Existing paving 2.40 325.43

1/4 " 327.83 2.12 325.71

♀ " " 2.09 325.74

1/4 " " 2.41 325.48

Gutter 3.12 324.71

S Top existing cb. 2.68 325.15

Plotted 3/7/89 - G.M.J.

0+25

S Top cb. 5.23 322.10

G 6.4 321.4

1/4 5.6 322.2

♀ 5.1 322.7

1/4 4.6 323.2

G 5.3 322.5

N Top cb. 4.66 323.17

0+50

X Top cb. 7.66 320.17

G 8.3 319.5

1/4 7.5 320.3

♀ 8.4 319.4

1/4 8.1 319.1

G

9.4

318.4

S Top cb

8.62

319.21

0+75

S Top cb

11.62

316.21

G

12.1

315.7

1/4

11.7

316.1

♀

11.5

316.3

1/4

11.0

316.8

G

11.3

316.5

N Top cb. Driveway

11.28

316.58

T.P.

-13.09

314.74

+0.84

H.I. 315.58

1+00

X Top cb

13.6

314.22

G

2.0

313.6

1/4

315.6

1.9

313.7

♀

2.2

313.4

1/4

2.6

313.0

G

2.9

312.7

S Top cb

2.33

313.25

140 = E.L. Alley

S Top cb

7.02

308.56

Concrete Gutter

7.70

307.88

1/4

6.9

308.7

H.I. 315.58

£	6.7	308 9
1/4	6.8	308 8
G	6.8	308 8
N Top cb	5.89	309.69

+60 = W.L. Alley

N Top cb	8.84	306.74
G	8.9	306 7
1/4	9.5	306 1
£	9.4	306 2
1/4	9.8	305 8
G	9.92	305 66
S Top cb - Alley return mark end of existing cb on Scott's. Sidewalk continues	9.37	306 21

Note

Alley is paved on South side from South Prop line  
to cb line

Section across <sup>Alley</sup> paving on S cb line

W Top cb	9.37	306 21
Gutter	9.92	305 66
£	8.75	306 83
Gutter	7.59	307 99
E Top cb	6.96	308 62
T.P.		-12.73 302.85

+0.92

H.I. 303.77

11

H.I. 303.77

2+00

S - inside edge of sidewalk - 7' South South cb line	5.84	299.93	
1/4	4.4		
cb	5.2	299.4	
1/4			
	303.8	3.9	299.9
£		3.0	300.8
1/4		3.2	300.6
G		4.1	299.7
N Top cb		3.19	300.58
	2+25		
N Top cb		7.11	296.66
G		8.0	295.8
1/4		7.0	296.8
£		6.9	296.9
1/4		7.7	296.1
cb		8.8	295.0
1/4		8.1	295.7
#7 sidewalk		7.68	296.09
	2+50		
Sidewalk		11.70	292.07
1/4		12.0	291.8
cb		12.8	291.8
1/4		11.5	292.3
£		10.8	293.0
1/4		10.9	292.9
G		11.7	292.1
N Top cb		10.95	292.82

H.I. 303.77

2.25.79 X-section of Triangle Bounded by  
J.R. Bliss  
Romer  
Brooks  
S.L. Landis - E.L. Wabash and E.L. Swift

12

T.P. -12.51 291.26 B.M. S.E. Nails Landis + Swift 285.94

+1.25

11.06

H.I. 292.51

H.F. 287.00

2+75

S.L. Landis = 0.00

N. Top cb 0 3.50 289.01 E.L. Swift 2.5 284.5

G 4 288.1 +12 5.4 281.6

H 3.5 289.0 +16 3.9 283.1

R 3.1 289.4 +20 3.7 283.3

H 3.8 288.7 +40 3.4 283.6

cb 5.2 287.3 +60 5.3 281.7

H 4.4 288.1 +80 6.4 280.6

Sidewalk 4.25 288.26 +85 5.8 281.2

3+00 = E.L. Swift

+94.46 E.L. Wabash 6.1 280.9

Sidewalk 8.00 284.5 0+10

H 7.6 284.9 E.L. Wabash 7.3 279.7

cb 8.1 284.4 40 8.2 278.8

H 7.5 285.0 +30 8.2 278.8

R 7.0 285.5 +50 10.9 276.1

H 6.9 285.6 +70 10.7 276.3

Gutter 7.6 284.9 +90 = E.L. Swift 9.4 277.6

N. Top cb 7.11 285.32 T.P. -12.52 274.48

B.M. S.E. Nails Landis + Swift - 6.59 285.97 + 40+

Correct 285.94

H.F. 278.52

E.L. Swift 5.7 272.8

+5 4.9 273.6

Contours Plotted  
3/18-29 GRH

H.I. 278.52

H.I. 278.52

13

+20	6.3	272.2
+40	6.1	272.1
+50	6.2	272.3
+55	3.2	275.3
+60	3.2	275.3
+80	2.5	276.0
+87 = E.L. Wabash	1.1	277.4

0+50

E.L. Wabash	7.6	270.9
+20	6.5	272.0
+25	7.4	271.1
+40	7.9	270.6
+60	8.2	270.3
+80 = E.L. Swift	8.9	269.6

0+75

E.L. Swift	9.3	269.2
+17	9.2	269.3
+20	8.5	270.0
+40	9.0	269.5
+59	8.7	269.8
+60	8.0	270.5
+88 = E.L.	8.0	270.5
+71.5 = E.L. Wabash	8.2	270.3

1400

E.L. Wabash	9.8	268.7
+5	10.2	268.3
+20	10.3	268.2
+25	9.5	269.0
+45	9.4	269.1
+65 = E.L. Swift	9.6	268.9

1+25

E.L. Swift	10.5	268.0
+70	11.0	267.5
+27	11.0	267.5
+35	11.6	266.9
+40	11.0	267.5
+57.8 = E.L. Wabash	10.2	268.8

1+50

E.L. Wabash	11.0	267.5
+10	11.5	267.0
+20	11.8	266.7
+25	13.0	265.5
+30	12.0	266.5
+50 = E.L. Swift	11.9	266.6

1+75

E.L. Swift	12.3	266.2
+10	12.5	266.0
+18	13.6	264.9
+20	13.4	265.1



H.I. 278.52

+23	12.8	265.7
+34	11.8	266.7
+42.5 = E.L. Wabash	11.8	266.7

2+00

E.L. Wabash	13.4	265.1
+5	12.9	265.6
+10	12.8	265.7
+15	13.0	265.5
+20	14.1	264.4
+25	12.7	264.8
+35 = E.L. Swift	12.1	266.4

2+25

E.L. Swift	12.4	266.1
+8	12.2	266.3
+9	13.5	265.0
+15	14.6	263.9
+20	14.2	264.3
+27 = E.L. Wabash	14.2	264.3

2+50

E.L. Wabash	14.3	264.2
+10	14.2	264.3
+17	12.6	265.9
+20 = E.L. Swift	14.3	264.2

H.I. 278.52

14

2+75

E.L. Swift	14.3	264.2
+5	14.9	263.6
+15 = E.L. Wabash	14.7	263.8

3+00

E.L. Wabash	15.0	263.5
+5 = E.L. Swift	15.0	263.5

3+16.4 = P.I.

15.3 263.2

B.M. N.W.B.R. Swift - Nightman

337.44

+1.46 338.88

-13.28 325.60

+0.79 326.39

-13.06 313.33

+0.13 313.46

-13.18 300.28

+0.75 301.03

-12.27 288.26

+4.07 292.33

B.M. S.E. Nails Landisv Swift

-6.39 285.94

2-26-29 X-section Woods Hole - Landis  
 J.C. Bliss  
 Rowner  
 Sommermeier  
 to Myrtle - 130' wide - 20' cbs - 20' 1/2

H.I. 281, 93

15

B.M. S.E. Keils Swift + Landis 285.94

+ 1.48 287.42

- 10.83 276.59

+ 5.34

H.I. 281, 93

N 1/4 Landis

E 1.3 280.0

+ 4 5.6 276.3

cb 10.3 271.6

+ 5 11.8 270.1

1/4 11.3 270.6

+ 4 9.5 272.4

+ 15 9.6 272.3

¢ 8.1 273.8

1/4 10.2 282.1

cb + 8.5 290.4

W + 12.4 299.8

N 1/4 Landis

W + 12.0 293.9

cb + 2.2 284.1

1/4 3.8 278.1

¢ 8.6 273.3

+ 15 9.9 272.0

1/4 11.7 270.5

cb 11.1 270.8

+ 10

E

E

+ 15

cb

1/4

+ 7

+ 10

¢

+ 15

1/4

+ 15

cb

W

W

+ 16

cb

+ 5

1/4

¢

+ 3

+ 4

1/4

5.2

5.3

7.4

10.6

10.6

12.0

12.3

10.3

9.6

8.5

6.8

2.6

1.1

+ 9.0

+ 6.0

2.0

2.4

3.4

7.4

10.3

10.5

13.0

12.1

276.7

276.6

274.5

271.3

271.3

269.9

269.6

271.6

272.3

273.4

275.1

279.3

280.8

290.9

287.9

279.9

279.5

278.5

274.5

271.6

271.4

268.9

269.8

¢ Landis

5 1/4 Landis

H.I. 28193

cb	11.5	270.4
#16	10.8	271.1
E	9.8	272.1
S cb Landis		
E	11.1	270.8
cb	10.7	271.2
1/4	11.8	270.1
¢	12.4	269.5
+5	12.9	269.0
+6	11.0	270.9
1/4	8.0	273.9
+10	8.0	273.9
cb	3.9	278.0
+10	2.0	279.9
W	+2.4	284.8

South Line Landis +100

W	0.0	281.9
+5	3.1	278.8
cb	6.4	275.5
+8	9.1	272.8
1/4	10.4	271.5
+9	10.8	271.1
+8	13.8	268.1
¢	12.5	269.7
1/4	12.0	269.9

H.I. 28193

16

cb	11.4	270.5
E	11.7	270.2
0+25		
E	12.9	269.0
cb	12.6	269.3
1/4	12.1	269.8
+10	13.4	268.5
¢	13.7	268.5
+14	13.2	268.7
1/4	14.9	267.0
+10	15.0	266.9
+11	9.6	272.3
cb	8.3	273.6
W	1.5	280.4
0+50		
W	2.7	279.2
+12	7.7	274.2
cb	9.1	272.8
+1	15.0	266.9
1/4	14.3	267.6
¢	14.6	267.3
+5	13.5	268.4
1/4	13.5	268.4
cb	13.7	268.7
E	13.3	268.6

H.I. 281.93

-13.23 268.70

T.P.

+3.14

H.I. 271.84

0475

E	4.0	267.8
cb	3.9	267.9
1/4	5.0	266.8
+4	5.4	266.4
+17	4.6	267.2
♀	6.0	265.8
1/4	4.5	267.3
+5	4.1	267.7
+15	5.8	266.0
cb	5.7	266.1
+5	4.7	267.1
+8	+2.0	273.8
W	+6.9	278.7
1400		
W	+6.0	277.8
cb	6.2	265.6
1/4	6.2	265.6
♀	6.5	265.3
+2	5.9	265.9
1/5	6.2	265.6
1/4	5.1	266.7

H.I. 271.84

17

Cb

5.5

266.3

F

4.7

267.1

1425

E

5.3

266.5

+3.

6.2

265.6

cb

6.2

265.6

1/4

5.5

266.3

+2

8.3

263.5

♀

7.1

264.7

1/4

6.3

265.5

+3

5.3

266.5

+12

4.5

267.3

cb

2.2

269.6

W

+6.0

277.8

1450

W

+6.4

278.2

cb.

3.1

268.7

+14

7.6

264.2

1/4

7.2

264.6

♀

7.4

264.4

1/4

8.4

263.4

+4

8.4

262.4

+6

5.9

265.9

cb

6.8

265.0

E

7.0

264.8

H.I. 271.84

1+75

E	7.7	264.1
cb	7.7	264.1
+7	6.9	264.9
+8	8.1	263.7
14	8.4	263.4
+10	9.3	262.5
♀	7.9	263.9
+5	7.0	264.8
14	7.4	264.4
+11	8.1	263.7
cb	3.6	265.2
W	17.4	279.2

2+00

W	+10.2	282.0
+10	0.00	271.8
cb	4.2	267.6
+10	9.0	262.8
14	9.2	262.6
+10	8.1	263.7
♀	8.3	263.5
+3	10.5	261.3
14	9.1	262.7
+10	7.9	263.9
cb	8.1	263.7
E	8.4	263.4

H.I. 271.84

18

T.P. - East side Sta 2+00 -256 264.28  
+2.18

H.I. 266.46

2+25

E	3.2	263.3
+10	3.8	262.7
cb	3.8	262.7
14	3.2	263.3
+5	4.4	262.1
♀	5.1	261.4
14	4.3	262.2
+10	0.0	266.5
cb	+2.4	268.9
W	+13.0	279.5

2+57.6-L Pt. EL. Swift + EL. Wabash

W	+12.2	283.7
+17	+6.0	272.5
cb	+0.3	266.8
+15	6.5	260.0
14	5.6	260.9
♀	5.7	260.8
+3	4.3	262.2
14	3.9	262.6
cb	4.6	261.9
+11	5.5	261.0

H.I. 266.46

+12	3.8	262.7
E	3.6	262.9
2+75		
E	4.7	261.8
+12	4.7	261.8
+13	5.9	260.6
cb	5.4	261.1
+10	4.3	262.2
14	4.1	262.4
φ	4.8	261.7
+10	4.8	261.7
+12	6.6	259.9
14	5.7	260.8
cb	7.1	259.4
W	+12.4	276.9
3400		
W	+9.0	275.5
+11	+3.0	269.5
cb	7.0	259.5
14	7.3	259.2
+2	6.2	260.3
φ	5.5	261.0
14	5.0	261.5
+10	5.1	261.4
+12	6.3	260.2

H.I. 266.46

19

cb	5.8	260.7
E	5.5	261.0
3+25		
E	4.8	261.7
+11	5.0	261.5
+12	7.0	259.5
cb	6.0	260.5
14	5.8	260.7
φ	6.2	260.3
+14	6.0	260.5
14	7.0	259.5
cb	8.3	258.2
14	1.0	265.5
W	+11.0	277.5
3+50		
W	+9.2	275.7
+12	0.7	265.8
cb	8.8	257.7
14	8.1	258.4
+2	7.1	259.4
φ	6.8	259.7
14	6.8	259.7
+18	7.5	259.0
cb	5.9	260.6
E	5.6	260.9

H. 1. 266. 4c

3+75

E	5.8	260.7	+10
cb	6.3	260.2	+14
+12	6.3	260.2	+
+14	8.1	258.4	14
14	8.1	258.4	cb
+	7.3	259.2	+5
14	9.7	256.8	w
+12	8.9	257.6	
cb	5.1	261.4	w
w	+5.0	271.5	+15
	4+00		cb
w	0.3	266.2	+10
+13	7.8	258.7	14
cb	8.0	258.5	+10
14	8.2	258.3	+12
+	10.4	256.1	+
+5	10.7	255.8	+12
+6	7.8	258.7	14
14	7.6	258.9	cb
cb	7.0	259.5	E
E	6.6	259.9	
	4+25		E
E	7.3	259.2	cb
cb	7.1	259.4	14
14	8.9	257.6	+13

H. 1. 266. 4c

20

	8.4	258.1	
	11.7	254.8	
	10.6	255.9	
	8.9	257.6	
	9.1	257.4	
	8.8	257.7	
	4.1	262.4	
	4+50		
	8.2	258.3	
	9.5	257.0	
	8.7	257.8	
	10.0	256.5	
	9.1	257.4	
	10.1	256.4	
	12.2	254.3	
	11.4	255.1	
	9.9	256.6	
	9.2	257.3	
	7.8	258.7	
	6.5	260.0	
	4+75		
	6.7	259.8	
	7.7	258.8	
	8.1	258.4	
	13.0	253.5	

H.I. 266.40

♀	10.7	255.8
14	10.1	256.4
+12	11.2	255.9
+14	9.6	256.9
cb	8.6	257.9
w	9.3	257.2
T.P.	+ 9.57	H.I. 262.88 5+00
w	6.0	-13.15 253.01
+11	5.6	256.9
+15	3.3	256.3
cb	3.1	259.6
+10	7.2	259.8
14	7.4	255.7
♀	7.2	255.5
+6	7.5	255.7
14	8.8	255.4
+5	7.8	254.1
+8	5.1	255.1
cb	4.4	257.8
E	2.9	258.5
	5+25	260.0
E	4.4	257.5
+18	6.2	256.7
cb	9.1	253.5
14	8.2	254.7
+10	8.9	254.0

H.I. 262.88

21

♀	7.8	255.1
14	7.2	255.7
cb	2.7	260.2
+11	6.4	256.5
w	6.4	256.5
	5+50	
w	6.6	256.3
cb	8.1	254.8
+15	8.6	259.3
14	7.8	255.1
♀	8.8	254.1
+19	8.6	254.3
14	9.2	253.7
cb	9.6	253.3
E	9.3	253.6
	5+75	
E	10.4	252.5
+13	10.2	252.7
cb	9.2	253.7
14	9.1	253.8
♀	8.6	254.3
+18	9.2	253.7
14	11.9	251.0
+5	9.6	253.3
cb	8.0	254.9



H.I. 262.88

W	7.3	255.6
5 + 9.8 <sup>73</sup>	N.L. Dwight	
W	8.7	254.2
cb	8.8	254.1
14	9.4	253.5
+10	10.6	252.3
+15	11.6	250.3
£	9.9	253.0
14	9.8	253.1
cb	10.3	252.6
+13	10.4	251.5
+15	11.8	251.1
E	11.6	251.3

B.M. N.E. Prop. Dwight & Wobash	-11.59	251.27
+12.94	264.23	
T.P.	-0.51	263.72
+864	272.36	
	-0.67	271.69
+12.20	283.89	
	-10.9	292.90
+5.40	298.20	

B.M. - S.E. Nails Landis & Swift	-2.24	285.96
		285.74

B-1-29 X-section Vancouver Ave - Myrtle  
 J.C. Blass to Dwight - 80' wide 14' cbs  
 Pomeroy  
 Osborn 13' 1/4"

22

B.M. - S.E. B.P. Myrtle & Nilesb - 314.56  
 + 4.86

	H.I. 319.42	
	N.L. Myrtle = 0+00	
W	5.2	314.2
cb	5.5	313.9
14	5.9	313.5
£	6.4	313.0
14	7.3	312.1
cb	7.7	311.7
+7	7.8	311.6
E	11.6	307.8
Out 15	18.9	300.6
	0+25	
Out 16	23.7	295.7
E	18.0	301.4
cb	10.5	308.9
14	9.9	312.5
£	6.8	312.6
14	5.4	314.0
cb	5.2	314.2
W	5.0	314.4
	0+50	
W	4.8	314.6
cb	5.0	314.4

Plotted J. Sam & C.B.H. 3/28-29

H.I. 319.42

1/4	6.8	312.6
+ 11	6.5	312.9
♀	7.8	311.6
1/4	12.0	307.4
cb	17.4	302.0
E	23.0	296.4
Out 15	29.5	289.9
	0775	
Out 15	32.9	286.5
E	27.2	292.2
cb	21.3	298.1
1/4	15.8	303.6
♀	11.1	308.3
1/4	7.9	311.5
+ 1	6.3	313.1
cb	6.4	313.0
W	5.1	314.3
	1700	
W	6.5	312.9
+ 11	6.7	312.7
cb	8.0	311.4
1/4	12.2	307.2
♀	16.7	302.7
1/4	21.4	298.0
cb	25.8	293.6

H.I. 319.42

23

E	32.1	287.3
Out 15	37.7	281.7
	1725	
Out 15	46.0	273.4
E	38.5	280.9
cb	31.3	288.1
1/4	27.8	291.6
♀	23.1	296.3
1/4	18.2	301.2
cb	13.6	305.8
W	8.5	310.9
T.P.		-12.63
	+1.36	306.79
	H.I. 308.15	
	1750	
W	2.7	305.5
cb	8.1	300.1
1/4	12.9	295.3
♀	18.1	290.1
1/4	22.2	286.0
cb	26.8	281.4
E	31.9	276.3
Out 15	38.4	269.8
	1775	
Out 15	45.3	262.8

H.I. 308.15

E	37.7	270.4
cb	30.7	277.4
1/4	26.0	282.1
♀	22.8	285.3
1/4	17.7	290.4
cb	12.3	295.8
W	6.1	302.1
2+00		
W	9.1	299.1
cb	16.0	292.2
1/4	22.0	286.2
♀	27.0	281.2
1/4	34.1	274.1
cb	41.4	266.8
E	47.6	260.6
out 15	58.5	249.7
2+25		
out 15	64.5	243.6
E	57.1	251.0
cb	51.5	256.6
1/4	44.9	263.2
♀	37.8	270.3
1/4	31.6	276.5
cb	25.0	283.1
W	18.8	289.3

H.I. 308.15

24

T.P.		-12.07	296.08
	+0.60	296.68	
T.P.		-13.27	283.41
	10.79		
		H.I. 284.20	
		2+50	
W		5.5	278.7
cb		13.0	271.2
1/4		19.0	265.2
♀		24.8	259.4
1/4		30.8	253.4
cb		35.1	249.1
E		38.2	246.0
out 15		41.8	242.4
		2+75	
out 15		42.0	242.2
E		39.0	245.2
cb		36.7	247.5
1/4		34.3	249.9
♀		31.3	252.9
1/4		25.6	258.6
cb		20.7	263.5
W		13.4	270.8
T.P.		-13.12	271.08
	+1.93	272.41	

H.I. 272.41

2+90

W	4.8	267.6
cb	10.5	261.9
1/4	15.6	256.8
♀	20.2	252.2
1/4	23.7	248.7
cb	25.4	247.0
E	27.8	244.6
Out 15	31.0	241.4

2+92

Out 15	31.1	241.3
E	30.8	241.6
cb	30.1	242.3
+2	26.0	246.4
1/4	23.8	248.6
♀	20.5	251.9
1/4	15.8	256.6
cb	10.7	261.7
W	5.0	267.4

3+00

W	5.6	266.8
cb	12.5	259.9
1/4	18.1	254.3
♀	22.0	250.4
1/4	24.0	248.4
+7	25.0	247.4

H.I. 272.41

25

+8	30.5	241.9
cb	30.7	241.7
E	30.1	242.3
Out 15	30.2	242.2

3+37 - P.J. - NL. Wabash + EL. Vancouver

Out 15	30.3	242.1
E	29.7	242.7
cb	29.0	243.4
1/4	28.6	243.8
♀	29.5	242.9
+4	30.3	242.1
+10	22.6	249.8
1/4	20.2	252.2
cb	15.0	257.4
W	7.4	265.0

T.P

-12.14 260.27

+280

H.I. 263.07

3+75

W	1.7	261.4
cb	8.2	254.9
+5	10.0	253.1
+7	18.6	244.5
1/4	18.7	244.4
♀	19.2	243.9
1/4	19.9	243.2

H.I. 263.07

+ 11	20.7	242.4
cb	19.0	244.1
E	19.3	243.8
4+00		
F	18.3	244.8
cb	17.8	245.3
1/4	17.4	245.7
♀	19.6	243.5
1/4	18.0	245.1
+9	10.6	252.5
cb	9.2	253.9
W	3.2	259.9
4+25		
W	4.8	258.3
cb	9.0	254.1
1/4	11.6	251.5
♀	18.6	244.5
1/4	19.2	243.9
+10	16.5	246.6
cb	16.6	246.5
E	16.8	246.3
4+50		
E	17.8	245.3
cb	18.2	244.9
+11	19.2	243.9

H.I. 263.07

26

1/4	17.3	245.8
♀	13.8	249.3
1/4	9.3	253.8
cb	6.9	256.2
W	5.8	257.3
4+75		
W	3.6	259.5
cb	7.1	256.0
1/4	10.0	253.1
♀	11.8	251.4
1/4	14.0	249.1
+6	14.8	248.3
+9	18.2	244.9
cb	18.5	244.6
E	16.5	246.6
T.P.	3' East of Sta 4+30 W.L.	- 5.80 257.27
+1311		
H.I. 270.38		
5+00		
E	24.8	245.6
+10	25.2	245.2
cb	24.0	246.4
+3	22.5	247.9
1/4	21.8	248.6
♀	20.7	249.7

H.I. 270.38

1/4	17.6	252.8
cb	10.3	260.1
w	4.1	265.7
	5+25	
w	2.7	267.7
cb	8.8	261.6
1/4	14.7	255.7
♀	19.4	251.0
+ 5	21.0	249.4
1/4	22.0	248.4
+ 8	22.7	247.7
+ 9	24.4	246.0
+ 12	24.4	246.0
cb	23.4	247.0
E	23.2	247.2
	5+50	
E	21.8	248.6
cb	22.6	247.8
+ 7	23.3	247.1
+ 8	21.2	249.2
1/4	21.3	249.1
♀	20.2	250.2
+ 12	16.7	253.7
1/4	14.9	255.5
cb	9.4	261.0

H.I. 270.38

27

w	2.9	267.5
	5+75	
w	10.9	259.5
T.P		-12.78 257.60
	+ 5.03	
	H.I. 262.63	
cb	8.1	254.5
+ 7	11.9	250.7
1/4	12.2	250.4
♀	12.7	249.9
1/4	12.5	250.1
cb	13.1	249.5
+ 2	15.6	247.0
+ 6	15.1	247.5
E	12.7	249.9
	5+98 <sup>05</sup> = S. L. Dwight -	80' wide 14' obs 12' 1/2
E	11.8	250.8
cb	13.1	249.5
1/4	12.6	250.0
♀	12.1	250.5
1/4	11.6	251.0
cb	11.5	251.1
w	9.0	253.6

262.63

S cb Dwight

W	9.8	252.8
cb	11.1	251.5
1/4	11.4	251.2
¢	11.4	251.2
1/4	11.4	251.2
cb	11.4	251.2
+5	12.5	250.1
E	11.4	251.2

¢ Dwight

E	10.6	252.0
+8	11.0	251.6
+9	12.2	250.4
cb	12.5	250.1
+1	11.1	251.5
1/4	10.6	252.0
¢	10.1	252.5
1/4	9.9	252.7
cb	10.6	252.0
W	9.8	252.8

N cb Dwight

W	9.0	253.6
cb	9.0	253.6
1/4	9.5	253.1
¢	9.4	253.2
1/4	10.0	252.6

262.63

28

+6	11.1	250.9
cb	10.3	252.3
E	9.9	252.7

N.L. Dwight - Page 22 This Book

B. M. N.E. Prop Hub - Dwight + Wabash

-11.45	251.18
Correct	251.29

3-4-29 X-section of Creek Bed on Wabash

J.C. Bliss from N.L. Dwight to N.L. Myrtle

Diabert Wabash to Myrtle

Paover

B.M. N.E. Prop. Hub Dwight + Wabash 25129

+210

H.I. 25339

N.L. Dwight

E.L. Vancouver 04 2530

+20 0.7 252.7

+34 West bank 1.0 252.4

+37 2.2 251.2

+40 1.9 251.5

+50 0.9 252.5

+60 0.7 252.7

+70 Base East Bank 1.6 251.8

& Dwight

E.L. Vancouver 1.3 252.1

+20 1.9 251.5

+25 West bank 2.6 250.8

+27 3.2 250.2

+40 2.8 250.6

+47 1.7 251.7

+60 2.4 251.0

+68 Base East bank 2.4 251.0

S.L. Dwight - 5+98.05 - From Myrtle

E.L. Vancouver 2.2 251.2

+15 Top West bank 2.9 250.5

+17 Base " " 4.2 249.2

+20 4.4 249.0

H.I. 25339

29

Page 22

+32 3.2 250.2

+40 3.8 249.6

+55 Base East bank 3.8 249.6

5+75 - Myrtle to Dwight Stationing on Vancouver

E.L. Vancouver 3.2 250.2

+10 Top West bank 3.5 249.9

+11 Base " " 4.4 249.0

+20 4.2 249.2

+33 Base East bank 4.8 248.6

5+50

E.L. Vancouver - W. Top bank 3.7 248.7

+3 " Base " 4.6 248.8

+20 4.8 248.6

+33 Base East bank 5.8 247.6

+35 Top " " 4.5 248.9

5+25

E.L. Vancouver 5.2 248.2

+4 Top West bank 5.0 248.4

+5 Base " " 6.3 247.1

+10 5.5 247.9

+20 5.5 247.9

+30 Base East bank 6.2 247.2

+33 Top " " 4.8 248.6

Note - Creek Enters Vancouver between Sta 5+00

5+25 - See X-section of Vancouver Arc - This book



H.I. 253.39

## Section Along E.L. Vancouver

between Sta 5+00 &amp; 5+25

5+00	7.2	246.2
5+06	7.8	245.6
5+12	6.5	246.9
5+25	5.2	248.2
T.P		-9.2 244.08
+0.25		

H.I. 244.33

## X-section of Creek in Wabash Are

From Intersection E.L. Vancouver & W.L. Wabash  
to N.L. Myrtle.

## Intersection E.L. Vancouver &amp; W.L. Wabash - Sta

3+37 - Myrtle to Dwight Stationing on Vancouver.

P.I. = 0+00

W.L. Wabash	0.7	243.6
+7	1.9	242.4
+14	2.6	241.7
+20 - Base East bank	2.3	242.0
+25 Top " "	0.7	243.6
	0+25	
W.L. Wabash	1.3	243.0
+20	1.8	242.5
+24	2.6	241.7
+31	2.8	241.5

H.I. 244.33

30

+40 - Base East bank	2.2	242.1
+43 Top " "	0.3	244.6
	0+50	
Out 5 = Top West bank	1.0	243.3
W.L. Wabash - Base West bank	2.6	241.7
+5	1.8	242.5
+20	2.3	242.0
+40	2.6	241.7
+49 - Base East bank	3.2	241.1
+50 Top " "	0.7	244.1
	0+75	
Out 6 = Top West bank	1.0	243.3
W.L. Wabash - Base " "	3.3	241.0
+20	2.4	241.9
+30	2.5	241.8
+40	3.1	241.2
+60 = Base East bank	3.9	240.4
63 = Top " "	0.8	243.5
	1+00	
Out 8 = Top West bank	1.5	242.8
W.L. Wabash - Base " "	3.4	240.9
+20	4.5	239.8
+35	3.1	241.2
+40	3.2	241.1
+60	3.8	240.5

H.I. 244.33

+70	44	2399
+80 = Base East bank	42	2401
+82 Top " "	18	2425
1+25		
Out 7 = Top West bank	33	2410
W.L. Wabash = Base " "	42	2401
+12	52	2391
+20	50	2393
+22	49	2394
+25	38	2405
+40	46	2397
+50	40	2403
+60	43	2400
+65	51	2392
+80	46	2397
+84 = Base East bank	52	2391
+85 = Top " "	23	2420
1+50		
Out 9 = Top West bank	34	2409
Out 7 = Base " "	44	2399
W.L. Wabash	47	2396
+3	52	2391
+7	61	2382
+14	54	2389
+20	55	2388

H.I. 244.33

31

+40	54	2389
+52	62	2381
+55	56	2387
+60	55	2388
+70 = Base East bank	58	2385
+72 = Top " "	39	2404
1+75		
Out 7 = Top West bank	11	2432
W.L. Wabash = Base " "	74	2369
+10	71	2372
+20 = Base East bank	62	2381
+32 = Top " "	50	2393
2+00		
Out 10 = Top West Bank	0.0	2443
Out 4 = Base " "	8.7	2356
W.L. Wabash	7.9	2364
+10	65	2378
+17 = Base East bank	59	2384
+19 = Top " "	54	2389
2+25		
Out 2 = Top West bank	47	2396
W.L. Wabash = Base " "	83	2360
+10	80	2363
+20 = Base East bank	72	2371
+25 = Top " "	58	2385

H.I. 244.33

2+50

W.L. Wabash	5.6	238.7
+5 = Top West bank	5.9	238.4
+9 = Base " "	8.0	236.3
+15	9.1	235.2
+20	8.4	235.9
+27 = Base East bank	8.2	236.1
+30 = Top " "	6.0	238.3

2+75

W.L. Wabash	6.4	237.9
+12 = Top West bank	5.9	238.4
+14 Base " "	8.4	235.9
+20	8.4	235.9
+30 = Base East bank	9.8	234.5
+32 = Top " "	7.0	237.3

3+00

W.L. Wabash	5.0	239.3
+5	6.6	237.7
+17 = West Top bank	7.1	237.2
+20 = " Base "	9.0	235.3
+38 = Base East bank	9.6	234.7
+40 = Top " "	8.1	236.2

W.L. Wabash	5.9	238.4
+9	7.8	236.5
+18 = Top West bank	8.0	236.3

H.I. 244.33

32

+25 = Base West bank	9.0	235.3
+40 = " East "	9.8	234.5
+50 = Top " "	7.7	236.6

3+64 = N.L. Myrtle

W.L. Wabash	7.6	236.7
+20 = Top West bank	8.8	235.5
+32 = Base " "	9.3	235.0
+33	9.8	234.5
+42	9.5	234.8
+50	11.2	233.1
+55 = Base East Bank	10.5	233.8
+56 = Top " "	7.4	236.9

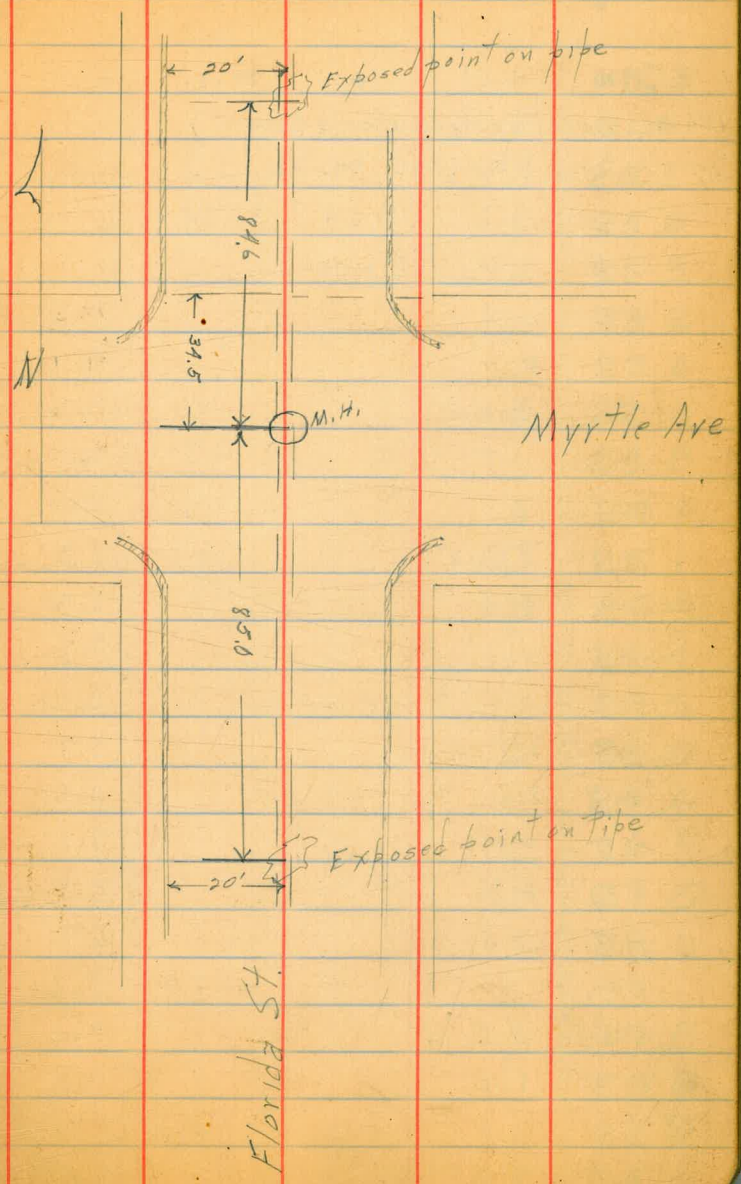
B.M. N.W. Prop Hub Myrtle &amp; Wabash -9.79 236.54

Landon's Elev. from South 236.20

5/28/29  
 Flood  
 Pierce  
 Colquhoun

Levels on Sewer  
 Myrtle and Florida.

	+	π	-	Elev.	
B.M. N.W. B.P.	5.42	250.19		244.77	Cypress & Alabama
T.P.	0.26	237.72	12.73	237.46	
T.P.	1.41	226.23	12.93	227.79	
T.P.	0.22	213.41	13.09	213.19	
T.P.	1.67	203.91	11.17	202.29	
Top of 1' pipe 24.6' N of M.H.			5.99	197.92	
Rim of M.H.			5.44	198.47	
Flow line of M.H.			8.57	195.34	
Top of 1' pipe 25' S of M.H.			8.63	195.28	
S.W. B.P. Myrtle & Florida			5.86	198.05	



X-Section Intersection Grant & Garnet from  
82.36 West of W.L. Quincy To about 200'  
beyond E.C. on Grand Ave.

Jaeger Clavert } June 5<sup>th</sup> 1929.  
Bailey Parrocks }

34

STA	+	H.I.	-	Elev.		+	31.39 H.I.	-	Elev.
					0+25				
								13.1	18.3
BM. SE. Spike Pole Pendleton & Grant } Set by Bliss F.B. 1246, Pg. 36 }				28.75	+5'			10.0	21.4
	2.64	31.39 ✓			S.L. Grant			6.3	25.1
	0+00				+8'			5.8	25.6
					+19'			6.1	25.3
+25'			14.5	18.9	S. Curb			8.2	23.2
+4'			9.1	22.3	+13'			9.4	22.0
S.L. Grant			7.6	23.8	S 1/4			8.8	22.6
+10'			6.1	25.3	+3'			7.6	23.8
+13'			7.7	23.7	+7'			7.3	24.1
+40' S Curb			8.3	23.1	+10'			6.3	25.1
+41 <sup>25</sup> ' S 1/4			8.2	23.2	±			6.0	25.4
+47 <sup>25</sup> '			7.7	23.7	N 1/4			5.0	26.4
+51 <sup>25</sup> '			6.2	25.2	+1'			7.0	24.4
+62 <sup>50</sup> ' ±			5.7	25.7	+6'			7.5	23.9
+78'			5.6	25.8	+10'			6.8	24.6
+81 <sup>25</sup> '			7.1	24.3	+11'			4.9	26.5
+83 <sup>25</sup> ' N 1/4			6.7	24.7	N. Curb			3.9	27.5
+87 <sup>50</sup> '			6.7	24.7	N.L.			3.4	28.0
+92 <sup>50</sup> '			5.1	26.3		0+50			
+105 <sup>00</sup> ' N. Curb			4.1	27.3	+25'			13.6	17.8
+125 <sup>00</sup> ' N.L.			2.8	28.6	+7'			10.8	20.6
					+5'			8.5	22.9
					S.L. Grant			6.8	24.6

STA	+	31.39 H.I.	-	Elev.
+8'			6.9	24.5
+19'			10.2	21.2
S. Curb			11.5	19.9
+4'			10.0	21.4
+4'			14.0	19.4
+7'			11.7	19.7
+11'			9.8	21.6
+15'			8.3	23.1
S/4			8.4	23.0
+2'			7.0	24.4
+12'			6.2	25.2
☐			6.5	24.9
N/4			5.2	26.2
+5'			7.2	24.2
+10'			7.9	24.0
N. Curb			5.1	26.3
N.L.			3.5	27.9
O+82 <sup>36</sup> W.L. Quincy				
X-sec. Right angle with S.L. Grant				
S.L.			8.9	22.5
+2'			8.0	23.4
+14'			9.5	21.9
+14'			12.7	18.7
S. Curb			13.5	17.9
+9'			12.5	18.9

STA	+	31.39 H.I.	-	Elev.
+18'			10.4	21.0
S/4			7.7	23.7
☐			7.0	24.4
N/4			6.1	25.3
N. Curb			4.9	26.5
N.L.			3.6	27.8
+2.5	S.L. Pavement		3.49	27.90
	T.P.		8.74	22.65
		6.44	29.09	
		O+82 <sup>36</sup>	W.L. Quincy	
X-sec. on Prolongation of W.L. Quincy				
+25'			11.7	17.4
+10'			9.8	19.3
+6'			6.9	22.2
S.L. Grant			6.6	22.5
+3'			5.8	23.3
+5'			7.6	21.5
+12'			8.3	20.8
+14'			11.2	17.9
+25'			11.0	18.1
+43'			10.3	18.8
+50'			8.2	20.9
+60'			6.3	22.8
+75'			5.1	24.0
+83 <sup>5</sup>			4.3	24.8

Sta		29.09 H.I.	-	Elev.
+ 113 <sup>51</sup>	S.L. Pavement		2.99	26.10
+ 123 <sup>51</sup>	☒ "		2.87	26.22
+ 133 <sup>51</sup>	N.L. "		2.90	26.19
+ 137'			3.3	25.8
+ 138'			3.9	25.2
+ 148'			3.6	25.5
+ 163 <sup>51</sup>	N.L. Garnet		1.1	28.0
	0+93 <sup>73</sup> W. Curb Quincy			
S.L. Grant			10.8	18.3
+5'			11.8	17.3
+10'			11.3	17.8
+30'			10.8	18.3
+40'			10.3	18.8
+55'			6.8	22.3
+64'			5.7	23.4
+85'			4.4	24.7
+ 108.4	S.L. Pavement		3.21	25.88
+ 118.4	☒ "		3.23	25.86
+ 128.4	N.L. "		3.38	25.71
+ 132'			3.4	25.7
+ 135'			4.4	24.7
+ 138'			3.7	25.4
+ 153'			4.0	27.1
	1+05 <sup>09</sup> W/4 Quincy			
S.L. Grant			11.6	17.5

Sta		29.09 H.I.	-	Elev.
+15'				11.0
+35'				10.4
+41'				8.0
+50'				8.5
+60'				6.7
+65'				5.8
+80'				4.9
+103'	S.L. Pavement			3.57
+113'	☒ "			3.65
+123'	N.L. "			3.84
+5'				4.0
+8'				4.7
+12'				3.7
+25'				4.0
+25'				2.7
	1+16 <sup>46</sup> ☒ Quincy			
	S.L. Grant			11.4
+15'				10.4
+30'				8.5
+50'				6.9
+65'				5.7
+85'				4.5
+98'	S.L. Pavement			3.81
+108'	☒ "			3.99
+118'	N.L. "			4.18
				25.52
				25.44
				25.25
				25.1
				24.4
				25.4
				25.1
				26.4
				17.7
				18.7
				20.6
				22.2
				23.4
				24.6
				25.28
				25.15
				24.91

Sta	+	29.09 H.I.	-	Elev.
+4			4.4	24.7
+8			5.0	24.1
+13			4.8	24.3
+13			3.4	25.7
	1+27 <sup>80</sup>	E. 1/4 Quincy		
S.L. Grant			10.9	18.2
+20			9.0	20.1
+50			6.6	22.5
+80			4.5	24.6
+93	S.L. Pavement		3.89	25.20
+103	¢	"	4.05	25.04
+113	N.L.	"	4.28	24.81
+4			4.4	24.7
+10			5.0	24.1
+13			3.5	25.6
	1+39 <sup>19</sup>	E. Curb Quincy		
S.L. Grant			10.7	18.4
+25			8.4	20.7
+50			6.4	22.7
+60			5.8	23.3
+75			4.8	24.3
+87	S.L. Pavement		4.18	24.91
+97	¢	"	4.36	24.73
+107	N.L.	"	4.53	24.56
+11			4.6	24.5

Sta	+	29.09 H.I.	-	37 Elev.
+7'			5.6	23.5
+15'			3.5	25.6
	1+50 <sup>55</sup>	E.L. Quincy		
	X- Sec. on Prolongation of	E.L. Quincy		
S.L. Grant			12.3	16.8
+20			10.3	18.8
+15			9.0	20.1
+40			7.3	21.8
+50			6.6	22.5
+60			6.3	22.8
+80			4.4	24.7
+80	S.L. Pavement		4.32	24.87
+90	¢	"	4.59	24.60
+100	N.L.	"	4.81	24.38
+2			4.8	24.3
+8'			6.0	23.1
+10'			4.7	24.4
+25			4.2	24.9
	1+75	Right & with S.L. Grant		
+15			15.2	13.9
S.L. Grant			12.2	16.9
+10'			10.8	18.3
+30			8.3	20.8
+35			7.0	22.1
+50			6.6	22.5



Sta	+	29.09 H.I.	-	Elev.
+57			5.7	23.4
	T.P.		8.60	20.49
	4.50	24.99 ✓		
	2+00			
+75			11.6	13.4
S.L. Grant			9.0	16.0
+5			8.4	16.6
+10			6.4	18.6
+18			4.5	20.5
+19			3.3	21.7
+30			3.6	21.4
+50			2.0	23.0
+61			0.8	24.2
+68	S.L. Pavement		0.39	24.61
	☒		0.58	24.42
	N.L.		0.64	24.36
	2+75			
+75			12.0	13.0
S.L. Grant			9.8	15.2
+10			7.5	17.5
+20			3.2	21.8
+30			2.6	22.4
+50			1.3	23.7
+54	S.L. Pavement		1.26	23.74
	☒		1.57	23.43

Sta	+	24.99 H.I.	-	38 Elev.
	N.L. Pavement		1.91	23.09
+8			3.0	22.0
+13			0.3	24.7
+20			1.9	23.1
+31			1.7	23.3
	2+50			
+75			12.5	12.5
S.L. Grant			9.8	15.2
+10			6.9	18.1
+20			2.7	22.3
+40			1.6	23.4
+47	S.L. Pavement		1.91	23.09
	☒		2.23	22.77
	N.L.		2.66	22.34
+8			3.5	21.5
+8			2.2	22.8
+17			1.1	23.9
+75			2.4	22.6
+35			1.7	23.3
+40			0.6	24.4
	2+75			
+5			10.6	14.4
S.L. Grant			10.0	15.0
+6			8.4	16.6
+10			5.7	19.3

Sta		24.99		Elev.
	+	H.I.	-	
+15			3.3	21.7
+30			2.7	22.3
+33	S.L. Parement		2.78	22.22
	☿	"	3.19	21.81
	N.L.	"	3.88	21.12
+8			4.5	20.5
+8			3.0	22.0
+20			2.6	22.4
+24			2.6	22.4
+28			3.9	21.1
+38			3.9	21.1
+40			3.8	21.2
	3+00			
+5			11.3	13.7
	S.L. Grant		9.8	15.2
+5			7.5	17.5
+10			4.7	20.3
+15			3.3	21.7
+25.5	S.L. Parement		3.50	21.50
	☿	"	3.94	21.08
	N.L.	"	4.50	20.50
+9			4.7	20.3
+9			3.8	21.2
+20			3.3	21.7
+28			3.1	21.9

Sta		24.99		Elev.
	+	H.I.	-	
+33			4.5	20.5
+40			4.4	20.6
	3+25			
+5			11.4	13.6
	S.L. Grant		10.0	15.0
+8			4.5	20.5
+10			4.2	20.8
+20.5	S.L. Parement		4.24	20.76
	☿	"	4.71	20.29
	N.L.	"	5.35	19.65
+10			5.3	19.7
+10			4.5	20.5
+20			3.9	21.1
+30			3.8	21.2
+32			4.7	20.3
+40			4.7	20.3
	3+50			
+5			11.4	13.6
	S.L. Grant		9.9	15.1
+16			4.4	20.6
+17.5	S.L. Parement		4.89	20.19
	☿	"	5.35	19.65
	N.L.	"	5.84	19.16
+11			6.2	18.8
+11			5.0	25.0

Sta		24.99		Elev.
	+	H.I.	-	
+20			4.7	20.3
+30			4.9	20.1
+40			5.2	19.8
	T.P.		5.9	19.09
		3.17	22.26	
		3+81 <sup>55</sup>	E.C.	
+10			9.2	13.1
S.L.	Grant		7.7	14.6
+7			2.7	19.6
+16			3.2	19.1
+15	S.L. Pavement		3.10	19.16
+25	¢ "		3.51	18.75
+35	N.L. "		4.11	18.15
+5			4.1	18.2
+12			4.6	17.7
+20			2.5	19.8
+25			2.6	19.7
+45	N.L. Grant		2.4	19.9
+5			2.5	19.8
		4+00		
+10			9.6	12.7
S.L.	Grant		7.7	14.6
+5			3.8	18.5
+10			4.1	18.2
+15	S.L. Pavement		3.78	18.48

Sta		22.26		Elev.
	+	H.I.	-	40
	¢ Pavement		4.11	18.15
	N.L. "		4.51	17.75
+5			4.6	17.7
+11			5.3	17.0
+20			2.8	19.5
+25			2.9	19.4
+45	N.L. Grant		3.1	19.2
+5			3.1	19.2
		4+25		
+10			9.7	12.6
	S.L. Grant		7.7	14.6
+5			5.2	17.1
+10			5.2	17.1
+15	S.L. Pavement		4.7	17.6
	¢ "		4.85	17.41
	N.L. "		5.10	17.16
+5			5.3	17.0
+10			6.2	16.1
+15			5.2	17.1
+20			3.3	19.0
+25			3.2	19.1
+45	N.L. Grant		3.7	18.6
+5			3.8	18.5
		4+50		
+10			10.0	12.3

22.26

Sta	+	H.I.	-	Elev.
S.L. Grant			7.5	14.8
+3'			6.0	16.3
+10'			6.0	16.3
+15'	S.L. Pavement		5.56	16.70
	¢	"	5.54	16.72
	N.L.	"	5.62	16.64
+5'			6.0	16.3
+10'			6.7	15.6
+15'			5.7	16.6
+20'			3.7	18.6
+25'			3.7	18.6
+35'			3.4	18.9
+38'			4.2	18.1
+45'	N.L. Grant		4.3	18.0
+5'			4.2	18.1
	A+75			
+10'			11.1	11.2
	S.L. Grant		8.7	13.6
+3'			6.8	15.5
+10'			6.7	15.6
+15'	S.L. Pavement		6.38	15.88
	¢	"	6.36	15.90
	N.L.	"	6.42	15.84
+5'			6.6	15.7
+10'			7.2	15.1

41

Sta	+	H.I.	-	Elev.
			7.0	15.3
			4.1	18.2
			4.0	18.3
			3.8	18.5
			4.7	17.6
			4.8	17.5
			4.8	17.5
	S+00			
			11.1	11.2
			9.2	13.1
			7.9	14.9
			7.9	14.9
			7.16	15.10
			7.06	15.20
			7.24	15.02
			7.5	14.8
			8.0	14.3
			6.5	15.8
			4.2	18.1
			4.0	18.3
			4.0	18.3
			4.1	18.2
			5.1	17.2
			5.2	17.1
			5.0	17.3

22.26

STA	+	H.I.	-	Elev
	5+25			
+10'			11.5	10.8
S.L. Grant			9.6	12.7
+3'			8.5	13.8
+10'			8.3	14.0
+15'	S.L. Pavement		9.85	14.41
¢	"		7.71	14.55
N.L.	"		7.83	14.43
+5'			8.0	14.3
+9'			8.6	13.7
+12'			7.8	14.5
+20'			4.4	17.9
+25'			4.4	17.9
+29'			4.3	18.0
+35'			5.8	16.5
+45'	N.L. Grant		5.5	16.8
+5'			5.4	16.9
	5+50			
+10'			11.7	10.6
S.L. Grant			10.2	12.1
+5'			9.0	13.3
+10'			9.0	13.3
+15'	S.L. Pavement		8.60	13.66
¢	"		8.50	13.76
N.L.	"		8.72	13.54

22.26

STA	+	H.I.	-	Elev
				<b>42</b>
+5'			8.8	13.5
+9'			9.2	13.1
+18'			4.8	17.5
+20'			4.5	17.8
+25'			4.6	17.7
+32'			4.9	17.4
+35'			6.0	16.3
+45'	N.L. Grant		6.2	16.1
+5'			5.5	16.8
	5+75			
+10'			11.3	11.0
S.L. Grant			9.7	12.6
+10'			9.6	12.7
+15'	S.L. Pavement		9.32	12.94
¢	"		9.22	13.04
N.L.	"		9.30	12.96
+5'			9.6	12.7
+10'			9.6	12.7
+18'			5.0	17.3
+20'			4.9	17.4
+25'			4.8	17.5
+34'			5.1	17.2
+35'			6.0	16.3
+45'	N.L. Grant		7.1	15.2
+5'			5.8	16.5

22.26

Sta	+ H.I.	-	Elev.
	6+00		
+10'		12.1	10.2
S.L. Grant		9.6	12.7
+10'		10.2	12.1
+15'	S.L. Pavement	9.92	12.44
	φ "	9.81	12.55
	N.L. "	9.95	12.30
+5'		10.2	12.1
+8'		10.8	11.5
+13'		8.0	14.3
+15'		6.3	16.0
+20'		5.0	17.3
+25'		5.0	17.3
+30'		5.1	17.2
+35'		7.7	14.6
+40'		9.3	13.0
+45'	N.L. Grant	9.9	14.4
+5'		5.7	16.6
	T.P.	2.58	19.68
	12.21 31.89		
	T.P. B.M. 28.75	3.15	28.74

43

Sta	+ H.I.	-	Elev.
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Const. BM on Villa Terrace

X Sec. Upas from w.L. Villa Terrace to w.L. Arnold. 60'5" + 20' ebs 20' Rd quad.

8/5/27 Loudon.

B.M.	0.08	297.57	297.49
0+100 = w.L. Villa Terrace.			
N.L.		6.8	290.8
+17		8.1	289.5
eb		6.4	291.2
1/4		6.6	291.0
+		10.2	287.4
1/4		13.4	284.2
eb		16.7	280.9
+8		20.6	277.0
S.L.		23.0	274.6
10 S		25.0	272.6
0+40			
10 S		29.1	268.5
S.L.		25.1	272.5
+15		15.6	282.0
eb		13.2	284.4
1/4		13.3	284.3
+		12.6	285.0
1/4		12.3	285.3
eb		12.0	285.6
+14		11.1	286.5
N.L.		10.6	287.0
10 N		13.3	284.3
T.P.	0.45	285.70	12.32 285.25

Plotted & Figured New yardage. Aug 8 - 29. C.B.H.V. Gd.

0+55	285.70		
25 N		11.6	274.1
10 N		11.4	274.3
N.L.		5.2	280.5
+7		0.8	284.9
eb		1.6	284.1
1/4		1.8	283.9
+		1.9	283.8
1/4		2.3	283.4
eb		2.3	283.4
+5		2.3	283.4
S.L.		13.5	272.2
10 S		18.8	266.9
0+72			
10 S		19.5	266.2
S.L.		16.0	269.7
eb		2.3	283.4
1/4		2.7	283.0
+		1.8	283.9
1/4		2.3	283.4
eb		2.9	282.8
+5		2.6	283.1
N.L.		10.6	275.1
T.P.	0.90	273.61	12.99 272.71
8 N		2.7	270.9
10 N		2.5	271.1
20 N		2.2	271.4

0+88 273.61

20N	3.1	270.5
10N	3.9	269.7
NL	4.7	268.9
eb	0.0	273.6
1/4	0.3	273.3
+	0.1	273.5
1/4	0.8	272.8
eb	1.5	272.1
S.L.	7.6	267.0
10S	8.9	264.7

1+00

10S	9.6	264.0
S.L.	9.2	264.4
eb	8.3	265.3
1/4	8.2	265.4
+	7.9	265.7
1/4	7.9	265.7
eb	7.4	266.2
NL	5.4	268.2
15N	4.3	269.3

1+31<sup>83</sup> = E.L. Alley 273.61

15N	6.1	267.3
NL	6.5	267.1
eb	7.8	265.8
1/4	8.1	265.5
+	8.6	265.0
1/4	8.8	264.8
eb	9.1	264.5
S.L.	10.0	263.8
10S	11.2	262.4

1+46<sup>83</sup> = W.L. Alley

10S	11.1	262.5
4S	10.4	263.2
S.L.	8.6	265.0
+7	8.0	265.6
+14	9.6	264.0
eb	9.1	264.5
1/4	9.0	264.6
+	8.4	265.2
1/4	8.1	265.5
eb	7.8	265.8
+13	7.3	266.3
NL	7.1	266.5
10N	7.1	266.5

45



1+57	273.61		
10N	7.4	266.2	
NL	7.7	265.9	
+7	7.5	266.1	
eb	8.4	265.2	
+3	8.5	265.1	
1/4	7.8	265.0	
<del>1/4</del>	6.4	267.2	
1/4	5.7	267.9	
eb	6.3	267.3	
+18	8.0	265.6	
S.L.	9.2	264.2	
3S	11.0	262.6	
10S	11.3	262.3	

1+75			
10S	11.8	261.8	
3S	11.3	262.3	
S.L.	9.3	264.3	
+10	7.1	266.5	
eb	8.1	265.5	
1/4	7.6	266.0	
<del>1/4</del>	8.0	265.6	
1/4	9.0	264.6	
eb	9.1	264.5	
+13	8.6	265.0	
NL	8.5	265.1	
10N	8.3	265.3	

2+00	273.61		
10N	10.1	263.5	
NL	10.4	263.2	
+8	9.8	263.8	
eb	9.5	264.1	
1/4	9.2	264.4	
<del>1/4</del>	9.4	264.2	
1/4	8.5	265.1	
eb	8.5	265.1	
+15	9.5	266.1	
S.L.	9.3	264.3	
10S	10.5	263.1	
20S	13.3	260.3	
2+25			
10S	14.4	259.2	
S.L.	12.7	260.9	
+10	8.8	264.8	
eb	9.0	264.6	
1/4	9.1	264.5	
<del>1/4</del>	9.6	264.0	
1/4	9.8	263.8	
cb	10.3	263.3	
+9	10.3	263.3	
NL	10.5	263.1	
10N	10.5	263.5	
T.P.	468	267.99	10.50 263.11

Upas

.79

2+50

267.99

10N	5.1	262.7
NL	5.2	262.6
+11	5.0	262.8
eb	5.3	262.5
1/4	4.9	262.9
1/4	4.7	263.1
1/4	4.3	263.5
eb	4.2	263.6
+5	3.1	264.7
SL	9.6	258.2
10S	10.0	257.8

2+60

10S	10.0	257.8
SL	9.9	257.9
+6	8.8	259.0
+14	4.8	263.0
eb	4.3	263.5
1/4	3.7	264.1
1/4	4.3	263.5
1/4	4.8	263.0
eb	5.0	262.8
NL	5.3	262.5
10N	5.1	262.7

Upas

267.79

2+7

= E.L. Arnold.

47

NL	5.3	262.5
+15	6.9	260.9
eb	7.8	260.0
1/4	7.5	260.3
1/4	7.4	260.4
1/4	6.9	260.9
eb	6.6	261.2
+5	6.6	261.2
+10	9.0	258.8
SL	9.9	257.9
10.S	10.5	257.3

E. cb Arnold (65' wide 10' cbs 45' Rdway)

10S	10.1	257.7
SL	10.0	257.8
+10	8.9	258.9
eb	5.9	261.9
1/4	5.0	262.8
1/4	5.6	262.2
1/4	6.2	261.6
eb	6.0	261.8
NL	6.23	261.56
NL	5.80	261.99

267.79

E/A Arnold

NL Pav.	5.42	262.37
+7	5.2	262.6
eb	5.4	262.4
1/4	5.7	262.1
1/4	6.0	261.8
1/4	6.1	261.7
eb	7.1	260.7
+10	9.0	258.8
S.L.	9.6	258.2
105	9.9	257.9

E Arnold

105	9.2	258.4
S.L.	9.0	258.8
+15	7.8	260.0
eb	6.1	261.7
1/4	5.8	262.0
1/4	5.5	262.3
1/4	5.6	262.2
cb	5.5	262.3
NL Pav	5.02	262.77

267.79

W/A Arnold.

NL Pav	5.01	262.78
eb	5.5	262.3
1/4	5.5	262.3
1/4	5.7	262.1
1/4	5.8	262.0
eb	6.6	261.2
S.L.	6.4	259.4
105	8.6	259.2

Web Arnold

105	8.5	259.3
S.L.	7.7	260.1
+5	6.2	261.6
+9	6.1	261.7
+13	7.1	260.7
eb	6.3	261.5
1/4	5.7	261.1
1/4	5.6	262.2
1/4	5.6	262.2
cb	5.6	262.2
+9	5.5	262.3
+10 topeb	4.82	262.97
NL Pav	5.38	262.41
NL topeb	4.74	263.05

48

Upper

W.L. Arnold	267.79		
Neb top	4.84	262.95	
gutter	5.4	262.4	
1/4	5.4	262.4	
1/2	5.6	262.2	
3/4	5.3	262.5	
cb	5.2	262.6	
+5	4.2	263.6	
+10	4.2	263.6	
+17	7.5	260.3	
S.L.	7.9	259.9	
105	8.5	259.3	
T.P.	12.74	280.48	0.05 267.74
B.M.	NE BP	Myrtle & Arnold.	1.50 278.98 (279.00)

X sec Plum st. from S.L. Alcott  
 S.L. Browning 70' wide 18' bbs 34' Rdway

B.M.	12.70	125.49	112.79	49
T.P.	11.84	136.59	0.74	124.75
T.P.	12.60	148.16	1.03	135.56
S.L. Alcott				
B.M.			10.22	137.94 ✓
W.L.			10.1	138.1
cb			10.8	137.4
1/4			11.0	137.2
1/2			11.4	136.8
3/4			11.8	136.4
cb			12.1	136.1
EL			13.2	135.0
S cb Alcott				
EL			11.5	136.7
cb			10.0	138.2
1/4			9.7	138.5
1/2			9.6	138.6
3/4			9.1	139.1
cb			9.1	139.1
W.L.			8.4	139.8

Reduced Aug 8 - 60 ft.  
Plotted

BM. Book (113.26)  
THIS E.I. IS APPROXIMATELY MEASURED.

H1 14816

S  $\frac{1}{4}$  Alcott

w.L.	7.7	140.5
cb	8.5	139.7
$\frac{1}{4}$	8.7	139.5
$\frac{1}{2}$	8.8	139.4
$\frac{1}{4}$	9.1	139.1
cb	9.4	138.8
E.L.	11.1	137.0

$\frac{1}{2}$  Alcott

EL	10.3	137.9
+7	9.3	138.9
cb	8.8	
$\frac{1}{2}$	8.5	

MH  $\frac{1}{2}$  Plum Alcott (F.L.)

	18.93	
+op	9.33	
$\frac{1}{2}$	8.5	139.7
$\frac{1}{4}$	7.9	
cb	7.7	
w.L.	7.2	141.0

14816

960

50

N  $\frac{1}{4}$  Alcott

w.L.	7.2	141.0
+7	7.3	
cb	7.7	
$\frac{1}{4}$	8.2	
$\frac{1}{2}$	8.4	139.8
$\frac{1}{4}$	8.8	
cb	9.1	
EL	10.1	138.1

Ncb Alcott

EL	9.7	138.5
cb	9.0	
$\frac{1}{4}$	8.6	
$\frac{1}{2}$	8.1	140.1
$\frac{1}{4}$	7.8	
cb	7.5	
w.L.	6.7	141.5

NL Alcott = 0+00

w.L.	5.8	142.4
cb	6.7	141.5
$\frac{1}{4}$	6.9	141.3
$\frac{1}{2}$	7.2	141.0
$\frac{1}{4}$	7.7	140.6
cb	8.0	140.2
+5	8.3	139.9
EL	9.8	138.4

148.16

Plum  
148.16

51

0+75

11'E at 0+6 <sup>2</sup> School Bldg. Floor level	9.90	138.26
0+25		
5 E	10.6	137.6
EL.	9.8	138.4
+7	7.5	140.7
cb	7.0	141.2
1/4	6.4	141.8
1/2	5.9	142.3
1/2	5.5	142.7
cb	5.0	143.2
wL	4.3	143.9
door way at 0+36 7.5' wide 6.4'E	10.11	
0+50		
wL	2.9	145.3
+12	4.2	144.0
cb	4.4	143.8
1/2	4.7	143.5
1/2	4.9	143.3
1/4	5.4	142.8
cb	5.7	142.5
+14	6.3	141.9
EL	9.5	138.7
2 E	10.1	138.1
11 E (Bldg)	10.5	137.7

11 E (Bldg)

EL.

+9

cb

+4

1/4

1/2

1/4

cb

+8

wL

1+00

wL

+10

cb

1/4

1/2

1/4

cb

+6

EL

11 E (Bldg)

11 E at 1+10 Floor level  
cor at 5<sup>th</sup> Court.

35° E at 1+10 Floor level  
back of Court

10.2

9.3

6.4

5.4

5.1

5.0

4.6

3.8

3.2

2.5

1.9

1.4

1.6

2.2

2.9

3.6

4.5

5.2

5.4

9.1

10.1

9.94

10.00

138.9

141.8

142.8

143.1

143.2

143.6

144.4

145.0

145.7

146.3

146.8

146.6

146.0

145.3

144.6

143.7

143.0

142.8

139.1

138.1

138.22

1+25		
35'E (Bldg)	9.6	138.6
10E	10.0	138.2
EL.	9.3	138.9
+8	7.0	141.2
cb	6.3	141.9
+5	5.3	142.9
1/4	5.3	142.9
±	4.3	143.9
1/4	3.9	144.3
cb	3.4	144.8
W.L.	2.5	145.7

1+50

W.L.	4.1	144.1
cb	4.2	144.0
1/4	4.7	143.5
±	5.5	142.7
1/4	6.0	142.2
+6	6.1	142.1
cb	6.7	141.5
EL.	7.2	139.0
7E	9.7	138.3
35E	9.4	138.8
at 1+68 1/4 E Floor level	9.87	138.29
at 1+68 35'E 1st. NE cor. court.	9.1	

1+75	148.16	
11E (Bldg)	9.9	
6E	10.4	
EL.	9.0	139.2
+3	8.3	139.9
cb	7.2	141.0
1/4	7.2	141.0
±	6.7	141.3
T.P.	4.46	145.18
1/4	3.6	141.6
cb	3.5	141.7
W.L.	2.2	143.0

1+94

W.L.	3.3	141.9
cb	4.1	141.1
1/4	4.4	140.8
±	4.9	140.3
1/4	5.3	139.9
cb	6.3	138.9
+3	6.1	139.1
+5	5.8	139.4
EL.	6.3	138.9
8E	7.6	
11E (Bldg)	7.2	

145.18

2 + 0 0 =	S.L. Browning		
E.L.		7.5	137.7
+ 9 <sup>5</sup>	top eb ret.	7.73	137.45
+ 9 <sup>5</sup>	gutter	8.21	137.97
cb	Paw	7.81	
1/4	"	7.44	
±	"	7.09	138.09
1/4	"	6.91	
cb	"	6.76	
+ 8	gutter	6.61	138.57
+ 8	top eb ret.	6.10	139.08
W.L.		5.3	139.9

## Job Browning

W.L. Paw		6.47	138.71
cb	"	7.10	138.08
1/4	"	7.34	
±	"	7.58	137.60
1/4	"	7.88	
cb	"	8.08	137.10
E.L.	"	8.54	
±	Browning		
E.L. Paw		8.64	136.54
cb	"	8.19	
1/4	"	7.98	
±		7.72	137.46
1/4		7.51	
cb		7.28	137.90

145.18

## ± Browning

W.L. Paw		6.69	
(Browning = Plum)			
Returns in equal Parts from S.L. Browning			
around to P.C.'s on Browning. 49' Rad.			
S.W. return.			
①	top eb	5.87	139.31
①	gut	6.40	.24
②	top eb	5.63	139.55
②	gut	6.15	.23
③	top eb	5.40	139.78
③	gut	5.95	.31
④	top eb P.C. on Browning	5.09	140.09
④	gut	5.65	
S.E. return.			
①	top eb	7.91	137.27
①	gut.	8.44	136.74
②	top eb	8.15	137.09
②	gut	8.71	.22
③	top eb	8.37	136.81
③	gut.	8.94	.27
④	P.C. on Browning. top eb	8.64	136.54
④	gut.	9.14	
T.P.	3.40	136.84	117.4
B.M.	B.P. SW Willow = Browning	6.93	129.91
B.M. Book (129.91)			
T.P.	0.77	124.60	13.01
B.P. SW Willow = Alcott			
B.M.			11.81
			112.79

53



124.60

T.P.	12.95	137.41	0.14	124.46	
T.P.	6.55	142.59	1.37	136.04	
B.P. SW. 2nd Willow					
B.M.			4.37	138.22	(B.M. Book 138.21)

4.3 PC  
Prow

54 PC  
Prowning  
S East

S.W.  
9.35  
Sel.

4.5  
4.75  
4.9  
5.1

.1  
.25  
.15  
.2  
P.L.

.35  
.20  
.25  
.21

4.85  
4.60  
4.35 PL

X Sec. Dover St.  
from - Talbot to 700' N.

Party  
Reading  
Leach

10/25/29

Sta. +  $\pi$  - E.L.

217.78 - assumed H.

55

B.M. #5 - Int. of Dover & Talbot Sts.

7.29 225.07

0+00

E.L. 5.8 219.3

$\pm$  7.3 217.8

W.L. 8.3 216.8

0+30 = N Line Talbot St.

W.L. 8.6 216.5

$\pm$  7.2 217.9

E.L. 5.8 219.3

0+80

E.L. 6.2 218.9

$\pm$  7.9 217.2

W.L. 9.0 216.1

1+30

W.L. 6.2 218.9

$\pm$  4.7 220.4

E.L. 4.0 221.1

1+80

E.L. 2.0 223.1

$\pm$  4.5 220.6

W.L. 7.0 218.1

230.6  
234.7  
S.L. Hill  
N.L. Hill

+    ̂    -    E.I.

225.07

2+30

W.L.	13.0	212.1
±	9.2	215.9
E.L.	5.4	219.7

2+80

E.L.	9.7	215.4
±	11.5	213.6
W.L.	13.3	211.8

3+30 S.L. Hill St.

W.L.	13.8	211.3
±	11.8	213.3
E.L.	10.5	214.6

T.P. Top of stake  
at Sta 3+30

4.30 218.29

4+00 N.L. Hill St.

E.L.	6.4	211.9
±	8.6	209.7
W.L.	10.7	207.6

5+00

W.L.	15.5	202.8
±	13.0	205.3
E.L.	9.7	208.6

+    ̂    -    E.I.

218.29

6+00

E.L.	9.5	208.8
±	12.1	206.2
W.L.	19.8	198.5
T.P. Hand level	12.1	206.2

2.8 209.0

7+00

W.L.	14.0	195.0
±	9.3	199.7
E.L.	3.9	205.1

96.21

X Sec. Hill St.  
from Dover to Concord.

+ T - El

0+00 = E.L. Dover St.

T.P. Top of Stake  
at Sta 3+30

- 213.99  
10.99 224.93

0+00

S.L. 10.4 214.5

± 11.5 213.4

N.L. 13.4 211.5

0+60

N.L. 7.3 217.6

± 7.2 217.7

S.L. 7.2 217.7

1+20

S.L. 4.3 220.6

± 3.4 221.5

N.L. 2.4 222.5

1.74 223.19

11.89 235.08

1+80

N.L. 6.7 228.4

± 8.2 226.9

S.L. 9.9 225.2

57

+ T - El.

235.08

2+40 = W.L. Concord St.

S.L.

4.3 230.8 on Hub

±

1.3 232.8

N.L.

0.6 234.5 on Hub.

X Sec. of Dover  
from Talbot to Inez

+  $\pi$  - E.L.

217.98

11.68 229.46

0+30 = S.L. Talbot St.

E.L. 10.2 219.3

$\Phi$  11.4 218.1

W.L. 12.1 217.4

0+80

W.L. 10.8 218.7

$\Phi$  10.0 219.5

E.L. 8.2 221.3

1+30

E.L. 5.0 224.5

$\Phi$  7.5 222.0

W.L. 8.7 220.8

1+80

W.L. 5.4 224.1

$\Phi$  4.4 225.1

E.L. 2.2 227.3

T.P. 0.32 229.14

11.35 240.49

2+30

E.L. 7.8 230.7

$\Phi$  11.8 228.7

W.L. 12.3 228.2

B.M.#5 Int. of Dover + Talbot Sts.

+  $\pi$  - E.L.

240.49

2+80

W.L. 8.4 232.1

$\Phi$  8.1 232.4

E.L. 7.2 233.3 Wedge at  
end of Bd. walk.

3+37<sup>20</sup> = S.L. Inez St.

E.L. 2.5 238.0

$\Phi$  3.4 237.1

W.L. 2.80 237.7

3+80

$\Phi$  + 0.1 240.6

Flood  
 Terrace  
 Kemper

X section Voltaire St. Sidewalks  
 Venice to Froude  
 10' Walks

	+	π	-	Elev		+	π	-	Elev
N.W. B.P. Prop.	4.15	90.65		86.50	Voltaire & Bolinas	+ 2		8.6	82.0
EL Venice So Walk of Voltaire			12.0			S.L.		7.6	83.0
+ 2.5 = edge of walk			12.03				1 + 00		
Cb.			12.27			S.L.		5.4	85.2
E Cb Venice Cb line on front			12.49			+ 4		7.2	83.4
+ 3			12.0			Top Cb.		7.94	82.71
prop top Ret & dirt			11.69				1 + 47	Back in Cb. Grade	
E 1/4 Venice prop			10.6			Top Cb.		6.69	83.96
+ 8			11.1			+ 7		6.3	84.3
Cb top			11.74			S.L.		5.1	85.5
& Venice Cb top			11.43				2 + 00		
+ 2			10.7			S.L.		3.1	87.5
prop Line			10.2			+ 3		5.0	85.6
W 1/4 Venice - prop			9.8			Cb Top		5.88	84.77
+ 8			10.8				2 + 10		
Cb. top			11.14			Cb Top		5.73	84.92
W Cb. Venice Cb top			10.85	79.80		+ 3		5.3	85.3
+ 2			10.2			+ 8		4.6	86.0
prop			9.7			S.L.		3.8	86.8
W.L. Venice = 0 + 00							3 + 50		
prop			9.5	81.1		S.L.		2.7	87.9
+ 8			10.1	80.5		+ 3		3.7	86.9
Top Cb.			10.60	80.05		+ 7		3.4	87.2
+ 50						Cb Top		5.15	85.50
Top Cb.			9.38	81.37					

S.M. Notes for yardage  
 11/28/29

	+	T	-	F	-
		9065			
		2+88			
Top Cb.		5'	3'	4.60	86.05
+ 6				4.0	86.6
+ 3				3.7	86.9
+ 8				3.5	87.1
S.L.				3.0	87.6
		2+89.8 = Beginning of Walk			
		5' wide 3' Back of Cb face			
S.L.				4.3	86.3
+ 3 = Edgewalk				4.38	86.27
+ 7 = " "				4.45	86.20
Top Cb				4.56	86.09
		3+29.8 = End of Walk			
Top Cb.				3.93	86.72
+ 3 = Edge walk				3.98	86.77
+ 8 = " "				3.80	86.85
S.L.				3.9	86.7
		3+32			
S.L.				2.5	88.1
+ 2				3.3	87.3
Top Cb				3.97	86.78
T.P.	1.80	89.01	3.44	<sup>Elev.</sup> 87.81	
		3+70 = Beginning of walk			
		5' wide 3' Back of face of Cb			
Top Cb.		1.94		87.81	

	+	T	-	Elev
		87.01		
+ 3 = Edgewalk				1.78
+ 8 = " "				1.54
S.L.				1.5
		4+00 = Back of Grade		
S.L. on walk				0.73
+ 7 Edgewalk				1.90
Top Cb				1.89
		4+32		
Top Cb.				2.58
+ 6.7 dirt				2.8
+ 3 " "				2.8
+ 3 on walk				2.57
+ 8 " "				2.85
+ 8 " dirt				2.5
S.L. " "				2.4
		4+70 <sup>3</sup> = End walk		
S.L.				4.1
+ 2 dirt				4.3
+ 2 walk				4.31
+ 7 " "				4.37
Top Cb				4.15
		4+75		
Top Cb				4.64
+ 5				4.0
+ 9				3.7

89.01

	+	π	-	Elev
S.L.			3.1	85.9
		5+00		
S.L.			3.8	85.2
+2			4.5	84.5
Top Cb.			5.63	83.38
		5+35		
Top Cb.			7.02	81.99
+3			6.4	82.6
+8			6.0	83.0
S.L.			5.3	83.7
		5+37		
S.L.			4.1	84.9
+3			5.2	83.8
+7			5.6	83.4
Top Cb.			7.18	81.83
		5+60		
Top Cb.			7.98	81.03
+1			7.1	81.9
+4			6.8	82.2
S.L.			3.8	85.2
		5+68		
S.L.			5.2	83.8
+6			7.4	81.6
Top Cb.			8.34	80.67
T.P.	0.94	81.34	8.61	80.40

81.30

61

	+	π	-	Elev
		5+48.3		beginning walk built solid to st.
Top Cb.			0.68	80.66
S.L. on Walk			0.50	80.84
		6+10.7		End of walk
S.L. on Walk			2.03	79.31
Top Cb.			2.39	78.95
		6+11		
Top Cb.			2.41	78.93
+4			2.1	79.2
S.L.			0.9	80.4
		6+20		
S.L.	0.20			81.54
+6			2.3	79.0
Top Cb.			2.79	78.55
		6+40		
Top Cb.			3.60	77.74
+6			3.1	78.2
S.L.			1.6	79.7
		6+70		Brk in Grade
S.L.			3.9	77.4
Top Cb.			4.80	76.54
		6+90		
Top Cb.			6.40	74.94
S.L.			6.0	75.3



8134

	+	-	Elev
	7400		
S.L.		7.3	740
+ 5		7.5	78.5
Top Cb.		7.22	74.12
	7415	8	
Top Cb.		8.44	72.90
+ 5		8.7	72.6
S.L.		8.5	72.8

7438.5 = I.L. Guizot 10' R. Return

S.L. on solid Retwalk = dirt		12.12	71.22
Top Cb.		10.38	70.96
T.P. Top Hydt 0.32	73.90	7.76	73.58

0400 = W.L. Guizot on S side of Voltaire

10' R. Return built solid to hills

5' Walk 2.5' back from face of Cb

parking strips between walk &amp; Cb

4' Walk and Trap filled with plantlet shrubs

S.L. on walk = dirt level		3.70	
+ 3.5 = walk edge dirt level		3.78	
+ 7.5 = " " " "		3.89	
Cb Top		3.95	

1400

Cb Top		9.99	
+ 2.5		9.10	
+ 7.5		9.71	

62

7390

	+	-	Elev
S.L.		9.6	
T.P.	1.43	13.20	12.13
			61.97
			2419.7 = End of Walk
S.L.		5.8	57.4
+ 3.5 on walk		5.67	57.53
+ 7.5 " "		5.87	57.33
Top Cb.		5.91	57.29
			2420

Top Cb		5.95	57.25
+ 4		5.6	57.6
+ 8		5.6	57.6
S.L.		5.9	57.3

2450

S.L.		8.2	55.0
+ 4		7.7	55.5
Top Cb		7.45	55.75

3400

Top Cb		10.05	53.15
+ 0.67		10.3	52.9
S.L.		11.0	52.2
T.P.	1.24	53.10	11.34
			51.96

3441 = Brk in Grade = E.L. Seaside  
Projected 5

S.L.		2.1	51.0
+ 8		1.8	51.3
Top Cb.		2.08	50.02

115

53.10  
+ π - Elev.  
3+68

Top Cb. 2.96 50.04  
+ 5 2.6 50.5  
S.L.

3+80 =  
S.L. 3.3 49.8

+ 7 3.5 49.6  
Top Cb 3.32 49.78

3+81 = beginning of walk  
5' wide 2.5' back of face of Cb.

Top Cb 3.36 49.74  
+ 2.5 = walk - dirt level 3.34 49.76

+ 7.5 = " 3.27 49.83  
S.L. 3.4 49.7

4+56 = Δ in S. Cb. + walk

S.L. 5.0 48.1  
+ 2.5 = walk dirt level 5.02 48.08

+ 7.5 = " " 5.10 48.00  
Top Cb 5.14 47.96

5+70 = Δ in S. prop. line

Top Cb. 6.10 47.00  
+ 4.5 = edge of walk dirt level 3.94 47.16

+ 9.5 = " " 5.87 47.28  
+ 4.5 = St. on <sup>concrete</sup> strip drive 5.85 47.25

53.10  
+ π - Elev.  
5+50

S.L. 6.6  
+ 4.5 walk - dirt level 6.45  
+ 9.5 " " " 6.56  
Top Cb. " " 6.62

5+98 = E.L. Froude <sup>10' P. Ret on 10x14 obs</sup> Ret built solid to prop

Top Cb 7.12  
+ 4.5 } dirt level 6.97

+ 9.5 } 6.92  
S.L. on net 6.78

T.P. 3.77 +6.52 9.35 43.75  
0+00 = W.L. Froude

14' walks on S side of Voltaire  
10' P. Return on 10x14 Cbs built solid to prop line  
first 50' ft no walk in but Service Sta. proprietor  
says he has taken out permit for it & let contract

S.L. on Cot walk 0.62 45.90  
St. on dirt 0.7 45.8

+ 4.5 " walk 0.74 45.78  
+ 4.5 " dirt 0.8 45.7

+ 9.5 " walk 0.82 45.66  
+ 9 " dirt 0.9 45.6

Top Cb. 1.05 45.47  
+ 3.5 Cb broken out for drive

Top Cb. 1.88 44.64

46.52

	+	x	-	Elev
S.L.			1.4	45.1
		0 + 53 =	End of broken out cb	
S.L.			2.2	44.3
+ 6			2.7	43.8
+ 10			2.5	44.0
Top Cb.			2.77	43.75

1 + 0.0

Top Cb.			4.20	42.32
+ 3			3.9	42.6
+ 7			3.9	42.6
+ 10			4.2	42.3
S.L.			3.8	42.7

1 + 0.5 beginning of walk

5.5' wide 6.5' back of Cb face

S.L.			3.8	42.7
+ 2 = edgewalk			4.01	42.51
+ 7.5			4.14	42.38
Top Cb.			4.23	42.29

1 + 4.1 = A in S.L. - walk + Cb.

Top Cb			5.49	41.03
+ 6.5 = Edgewalk			5.98	41.24
+ 12 = " "			5.29	41.23
S.L.			5.3	41.2

1 + 50.7 = End of 5.5 walk

beginning of 5' walk 6.5'  
Back of Cb

64

16.52

	+	x	-	Elev
S.L.				5.5
+ 2 = Edgewalk				5.63
+ 2.5 = " "				5.65
+ 7.5				5.75
Top Cb				5.90

2 + 50.7

Top Cb				9.22
+ 6.5 = edgewalk dirt level				9.14

T.P.	2.91	39.10	10.33	35.19
------	------	-------	-------	-------

+ 11.5 = " "				1.69
--------------	--	--	--	------

S.L.				1.8
------	--	--	--	-----

3 + 50.7 = End of walk

S.L.			4.3	34.8
------	--	--	-----	------

+ 2.5 = walk			4.58	34.52
--------------	--	--	------	-------

+ 7.5 = " "			4.61	34.49
-------------	--	--	------	-------

Top Cb.			4.79	34.31
---------	--	--	------	-------

3 + 55

Top Cb.			4.88	34.22
---------	--	--	------	-------

+ 2			4.4	34.7
-----	--	--	-----	------

+ 6.5			4.4	34.7
-------	--	--	-----	------

S.L.			4.5	34.6
------	--	--	-----	------

3 + 90

S.L.			5.1	34.0
------	--	--	-----	------

+ 5			5.4	33.7
-----	--	--	-----	------

+ 10			5.1	34.0
------	--	--	-----	------

39.10  
39.10

36.57

65

	+	⊖	Elev.
Top Cb.		5.83	33.27
	4 + 01.7 = beginning of walk <sup>built</sup> Solid top prop.		
Top Cb.		6.07	33.03
+ 12		5.80	33.20
S.L.		5.59	33.51
	4 + 52 = end of walk		
S.L.		6.4	32.7
+ 2		6.61	32.49
Top Cb.		6.80	32.30
	4 + 50		
Top Cb.		6.90	32.20
+ 6.5		6.7	32.4
S.L.		6.5	32.6
	5 + 00		
S.L.		6.9	32.2
+ 5		7.3	31.8
Top Cb.		7.42	31.68
	5 + 50		
Top Cb.		7.97	31.13
+ 10		7.7	31.4
S.L.		7.5	31.6
T.P. S.W.B.P. Voltaire Ebers		8.99	30.12 30.12 record.
	5 + 99		
S.L.		5.1	31.5
+ 6		5.3	31.3

	+	⊖	
Top Cb.		6.00	30.57
	6 + 01.7 = E.L. Ebers Ret solid		
Top Cb.		6.05	30.52
S.L.		5.86	30.71
	0 + 00 = E.L. Ebers on N Side of Voltaine		
Top Cb.		6.00	30.57
+ 6.5 = Edge of walk		5.82	30.75
12 = " " "		5.79	30.84
N.L.		5.7	30.9
	0 + 25		
N.L.		5.5	
+ 3 = Edge of walk camel drive		5.60	
Cb line " " " "		6.82	
	0 + 50		
Top Cb. 1st edge of camel drive		5.47	
+ 6.5 = walk		5.29	
+ 12 = "		5.19	
N.L.		4.7	
	1 + 00		
N.L.		4.2	
+ 1		4.3	
+ 2 = walk		4.61	
+ 7.5 = "		4.73	
Top Cb.		4.89	

20' of this drive is broken out

Cb from 1 + 00 to 1 + 15 broken down.

36.57

1775 = Brkin grade

Top Cb. 3.95  
 + 6.5 = walk 3.79  
 + 12 = " 3.66  
 + 13 3.2  
 N.L. 3.0

2+00 = Brkin Cb grade

A.L. 2.7  
 + 1 2.8  
 + 2 = walk 2.18  
 + 7.5 = " 3.28  
 Top Cb. 3.18

T.P. 8.92 42.64 2.85 33.72

3700

Top Cb. 6.94  
 + 6.5 6.84  
 + 12 6.72  
 N.L. 6.5

3720

N.L. 6.1  
 + 2 6.17  
 + 7.5 6.38  
 Top Cb. 6.41

3765

Top Cb 5.03  
 + 6.5 4.92

Cb from 180 to 1770 broken down

Cb from 2145 to 2100 broken down

Cb from 3720 to 3765 gone

4264

+ 12 4.80  
 N.L. 4.8

3783

N.L. 4.3  
 + 2 4.26  
 + 7.5 4.39  
 Top Cb 4.47

4430

Top Cb 3.12  
 + 6.5 2.95  
 + 12 2.86  
 N.L. 2.5

4755

N.L. 2.0  
 + 2 2.06  
 + 7.5 2.17  
 Top Cb 2.33

4785

Top Cb 1.47  
 + 6.5 1.34  
 + 12 1.22  
 N.L. 1.1  
 T.P. 6.53 48.51 0.66 41.98

66

Cb from 3783 to 4780 broken down

Cb from 4755 to 4785 broken down

	+	-	
			5+35
N.L.		5.7	
+ 2		5.58	
+ 7.5		5.70	
Top Cb.		5.82	
			5+99.2 = W.L. Freude
Top Cb		3.99	
+ 6.5		2.81	
+ 12		3.72	
N.L.		3.7	
T.P. N.W.B.R. 7.32	51.88	3.95	44.56
			0+00 = E.L. Freude 10'R Ret. built solid top
N.L. on corner of walk		6.68	45.20
Cb.		6.68	45.20
Prmt in gutter		7.35	44.53
			0+5
brmt (no Cb.)		7.32	44.56
+ 5		5.9	46.0
+ 15 = N.L.		5.6	46.3
			0+50
N.L.		5.8	46.1
+ 11		6.1	45.8
+ 19.4 = edge prmt		6.52	45.36
			0+92 = Cb line of old ret 5'R
Edge prmt		5.84	46.04

Cb from 51.88 to  
 W.L. Freude broken, labeled  
 & broken down again.

	+	-	
			+ 5 = Top Cb R Cold Ret. 5.59 45.29
			+ 17 5.3 46.6
			+ 26 = N.L. 4.9 47.0
			0+97.37 = Jog in N.L.
			N.L. from W. 5.4 46.5
			+ 30 = N.L. from E on walk 5.34 46.54
			Top Cb (comb Cb walk 5.6 wide) 5.42 46.46
			Cut on prmt. 5.82 46.06
			1+43.37 = An Cb = 10' Cbs
			Comb walk of Cb 5.67 wide
			Top of Cb. 4.33
			+ 5.67 = edgewalk 4.20
			N.L. 4.3
			1+97.37 = W.L. Seaside St.
			10'R Ret. built solid top
			N.L. 3.15
			+ 4.33 = edgewalk 3.16
			Top Cb. 3.22
			T.P. 10.47 60.45 19.0 49.98
			0+00 = E.L. of Seaside St.
			10'R solid Ret.
			5' walk 5' wide 2.5' back of Cb face
			N.L. on cor of Ret 10.22
			+ 2.5 = edgewalk 10.27
			+ 7.5 10.42
			Top Cb. 10.47

60.45

1+00 = end of walk

+	π	-	
Top C6		4.81	55.64
+ 2.5		4.94	55.51
+ 7.5		4.74	55.71
N.L.		5.2	55.2

1+15

N.L.		3.7	56.7
+ 3		4.5	55.9
+ 6		4.4	56.0
+ 9.3		4.1	56.3

Top C6		3.90	56.55
--------	--	------	-------

1+50

Top C6		1.92	58.53
+ 4		2.2	58.2
+ 7		2.7	57.7
N.L.		2.1	58.9

T.P.	1154	71.28	0.31	60.44
------	------	-------	------	-------

1+90

N.L.		1.10	60.7
+ 2		1.11	60.6
+ 5		1.14	60.3
+ 8		1.10	60.7
Top C6		10.34	60.84

2+00 = W.L. Eliwanda St

10' R. Solid Ret.

Top C6		10.31	61.37
--------	--	-------	-------

71.28

+	π	-	
+ 2.5 on walk		10.18	61.50
+ 2.5 dirt		10.2	61.5
+ 7.5 on walk		9.93	62.75
+ 7.5 dirt		10.1	61.6
N.L. on walk		9.80	61.88
N.L. dirt		10.1	61.6

0+00 = E. Eliwanda St  
10' R. Solid Ret.

N.L.		8.07	63.61
+ 2.5 } on walk		7.76	63.72
+ 7.5 }		7.77	63.90
Top C6		7.70	63.98

0+03

Top C6		7.51	64.17
+ 4		6.6	65.1
N.L.		6.4	65.3

0+25

N.L.		5.71	66.6
+ 6		5.3	66.4
Top C6		6.16	65.52

0+65

Top C6		3.70	67.98
+ 4		3.8	68.9
N.L.		2.6	69.1

		71.68	
	+	+	-
		1+00	
N.L.		0.7	71.0
+4		1.2	70.5
Top Cb		1.56	70.12
T.P.	10.33	80.43	1.58
			70.10

		1+50	
Top Cb		7.14	72.29
+3		7.2	73.2
+5		6.8	73.6
A.L.		6.8	73.6

		1+75	
N.L.		3.7	76.7
+4		4.1	76.3
Top Cb		4.10	76.33

		2+00 = W.L. 50 to ST	
		10'R Solid Ret.	
Top Cb		3.83	76.60
+2.5	} on walk	3.77	76.66
+7.5		3.68	76.75
N.L.		3.63	76.80

0+00 = E.L. 50 to ST  
 10'R Ret Solid  
 7' wide S. Walk 3' Back of Cb face

N.L.	} on walk	1.17	
+7		1.33	
Top Cb		1.42	

		80.43	
	+	+	-
		10.40	89.42
T.P.		1.41	77.02
		1+00	
Top Cb (indirect)		7.0	
+3 on walk		6.58	
A.L. " "		6.32	

2+00 = W.L. Bolinas  
 10'R Solid Ret

N.L.		2.57	
+7		2.82	
Top Cb.		2.92	

T.P. N.W. B.P. 323	89.70	2.95	86.47	Voltaire & Bolinas
		04.00 = E.L. Bolinas St		
		10'R Solid Ret	5' walk 3' Back of Cb face	

Top Cb.		2.91	
+3		2.71	
+8		2.63	
N.L.		2.60	

0+80 = end of walk

N.L.		4.0	85.7
+2		3.91	85.79
+7		3.96	85.74
Top Cb		3.97	85.71

0+83

Top Cb		4.03	85.67
+3		3.2	86.5



89.70

+

T

-

+ 9 3.1 86.6

N.L. 3.5 86.2

1+30

N.L. 3.7 86.0

+ 7 3.9 85.8

Top Cb 4.74 84.96

1+55

Top Cb 5.12 84.58

+ 3 4.6 85.1

N.L. 4.5 85.2

2+00

N.L. 5.8 83.9

+ 4 5.5 84.2

+ 8 5.4 84.3

Top Cb 5.74 83.96

2+40 <sup>5' wide 5' back</sup> beginning of walk

Top Cb 6.81 82.89

+ 3 on walk 6.80 82.90

+ 3 dirt 7.0 82.7

+ 8 on walk 6.73 82.97

+ 8 " dirt 7.0 82.7

N.L. 7.1 82.6

2+80

N.L. 8.4 81.3

+ 1.9 8.2 81.5

89.70

+

T

-

+ 2 = walk 7.98

+ 7 7.90

Top Cb 7.98

3+30

Top Cb 9.32

+ 3 on walk 9.33

+ 8 " " 9.32

+ 8.1 dirt 9.6

N.L. 10.0

3+80 = Brk in grade

N.L. 11.3

+ 1.9 10.8

+ 2 = walk 10.63

+ 7 = " 10.64

Top Cb. 10.66

4+03 <sup>5'</sup> on Cb: 4+02 <sup>5'</sup> on prep = Mt. Mendocino

Top Cb. 11.40

+ 3 11.47

+ 8 11.54

N.L. 11.48

T.P.N.W.B.P. 3.23

Veltair &  
Belinas  
86.50 record  
.03 error

70

Cross Section Alley Block 23 Univ. Hts.  
From Madison to Adams Between Georgia + Florida

2-14-30  
S. Gray  
1500  
0560  
**71**

BM	12.76	341.85	339.09	JFBP Madison + Florida
TP	11.11	357.84	112	340.73

N. E. of Madison

E on Paving	11.90	339.94
"	11.53	340.51
"	10.67	341.17

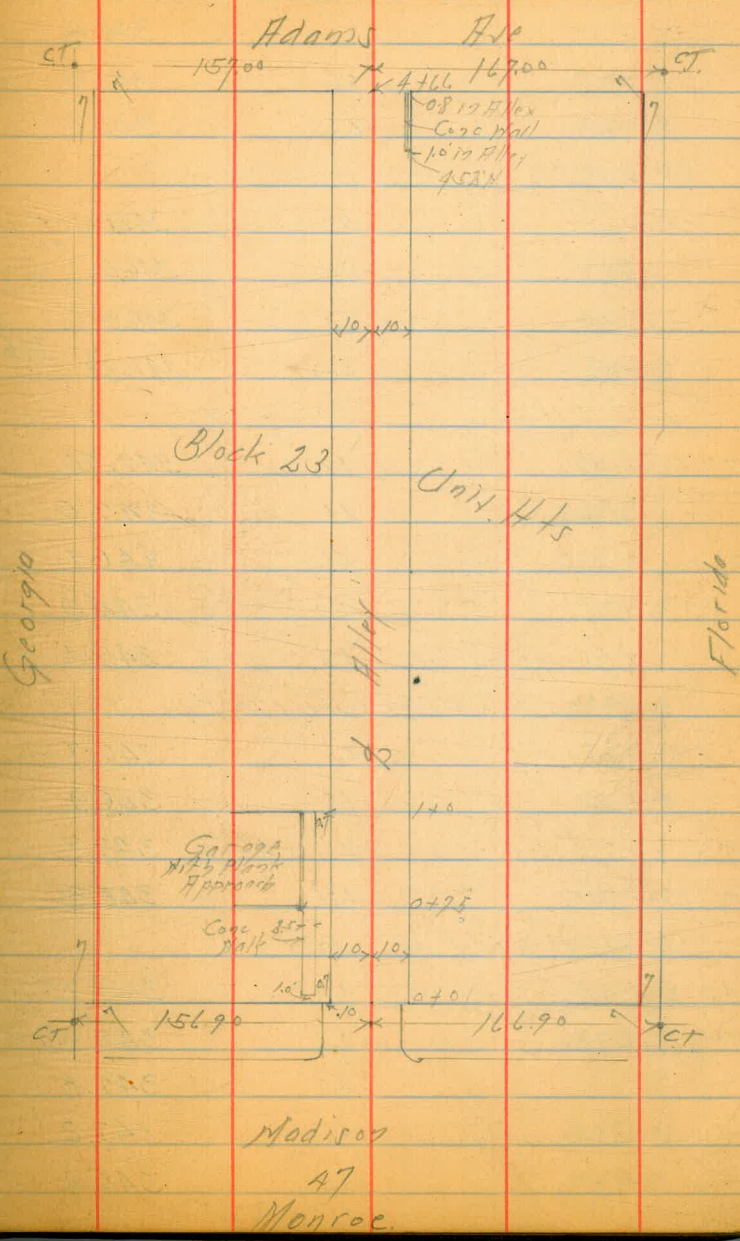
N. E. of Madison

N Top cb	9.77	342.07
Gutter on Paving	10.23	341.61
"	10.82	341.02
E Top cb + Paving	11.03	340.81
Dirt	10.02	341.5

Plotted 2-20-30  
CBH.

4 ft of Hb. Madison

E	7.1	344.7
+3	7.1	344.7
+6	9.2	342.6
8	8.9	342.9
+8	8.9	342.9
+4	6.5	345.3
N	5.0	346.8
+0.7 - Conc Walk	4.73	347.11
-0.7 - Conc Walk	4.68	347.16
N	5.0	346.8
+6	5.2	346.6
+8	6.6	345.2



35.84

2	68	3450	
+5	70	3448	
+7	58	3460	
F	60	3458	
	25.7		
F	57	3461	36.7 on top
2	58	3460	+ 1/2 floor
11	49	3469	80.15 on top
+0.7 = Conc Walk	158	347.32	346.21
	41.11		
-0.7 = Conc Walk	430	347.54	
11	48	347.0	
2	51	3467	
F	59	3459	
+4.7 = 1/2 Garage 2nd Floor	64	3454	✓
	75.11 = 1/2 of Garage on 11		
F	51	3467	
2	49	3469	
11	41	3477	
+0.7 = Conc Walk	398	347.86	
	88.11 = 1/2 of Garage on 11		
-8.3 = 1/2 Garage Conc Floor	259	349.25	✓
	With Plank Approach		
-0.7 = Conc Walk	391	347.93	✓
11	40	3478	
2	46	347.2	
F	54	3464	

35.84

72

	100.11 = 1/2 of Garage on 11		
F	52	3466	
2	49	3469	
11	40	3478	
+0.7 = 1/2 of Conc Walk	285	347.99	
	125.11		
11	37	348.1	
2	47	347.1	
F	50	3468	
	159.11		
F	40	347.8	178.11 =
2	36	348.2	Conc landing
11	25	349.3	to house
		4.55	9' E of 11
+6.2 = 1/2 Garage 2nd Floor	24	349.4	✓
	185.11		
11	22	349.4	
2	36	348.2	
F	40	3478	
	211.11		
-1.0 = Conc Floor	288	348.96	✓
	1/2 of Garage		
F	69	348.9	
2	28	3490	
11	21	349.7	
	230.11		
11	19	349.9	
2	37	349.1	

351.84

F		28	349.0
	2.55 N		
F		27	349.1
	2.42 N		
F		24	349.4
	2.21 = 249.03		
N = 1/2 Garage Dirt Floor		19	349.9
TP	4.75	354.33	349.58
	2.75 N		
N = Garage Dirt		42	350.1
		46	349.7
F		44	349.9
	2.95 N		
F		41	349.7
		42	350.1
N		41	350.2
+0.5 = 1/2 Garage Dirt Floor		41	350.2 ✓
	3.04 N		
-2.2 = 1/2 Line of 10 Garages on Conc Floor		3.10	350.73
N		3.7	350.6
		41	350.2
F		45	349.8
	3.25 N		
F		46	349.7
		45	349.8
N		3.9	350.4
+2.2 = 10 Garages on Conc Floor		3.50	350.83

354.68

73

	3.55 N		
-2.2 = 10 Garages on Conc Floor		3.57	350.76
		3.8	350.5
		4.5	349.8
		5.0	349.3
+1.2 = 1/2 Garage on Conc Floor		5.00	349.33 ✓
	3.80 N		
-1.0 = 1/2 Garage Dirt Floor		5.1	349.2 ✓
		4.9	349.4
		4.5	349.8
		3.8	350.5
+1.2 = 10 Garages on Conc Floor		3.47	350.86
	3.95 N		
-2.2 = 1/2 Line of 10 Garages on Conc Floor		3.48	350.85
		4.0	350.3
		4.7	349.6
		5.0	349.3
	4.07 N		
-1.5 = 1/2 Garage Dirt Floor		5.3	349.0 ✓
		4.8	349.5
		4.9	349.4
		3.9	350.4
	4.25 N		
		3.6	350.7
		4.8	349.5

35483

F		51	349.2
	+39.7 H		
F		51	349.2
+8		51	349.2
S - MH on Rim		4.48	349.85 ✓
H		3.9	350.4
	+51 H		
H		38	350.5
+5		52	349.1
S		5.4	348.9
+9 = Sly End Conc Wall Top		581	348.52 ✓
F		59	348.4
	+52 H		
F		75	346.8
+1.0 = Top Wall		581	348.51
S		5.5	348.8
+5		52	349.1
H		38	350.5
	46 H		
H		42	349.1
S		67	347.6
+9.2 = Conc Wall Hgt		582	348.51
	5' Top Down Top		
	Bottom	681	347.52
F		72	346.5
	46.6 H = S.E. of Adams		
F	Top of Cb.	731	347.02 ✓

35483

74

Gutter on Paving	753	346.80 -
+0.8 Top Conc Wall	682	347.51 ✓
S on Paving	733	347.00 -
H on Paving	669	347.64 ✓
on Top Cb	651	347.82 ✓
	S Curb of Adams	
H on Paving	726	347.07
S " "	766	346.67
F " "	814	346.19
TP	2.00	349.01
BM		732
		898
		347.01
		340.02

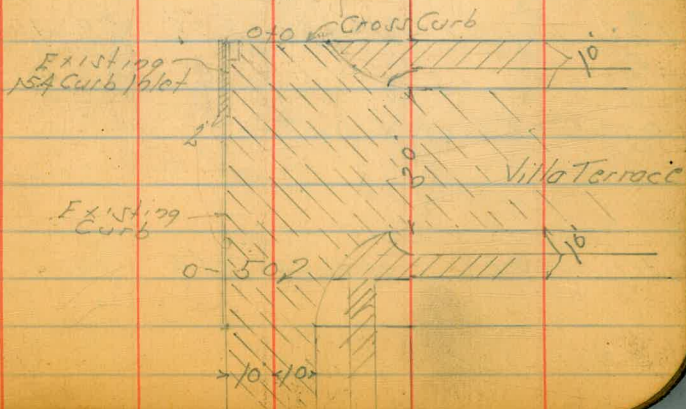
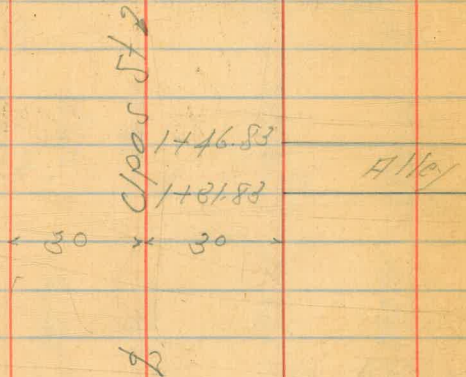
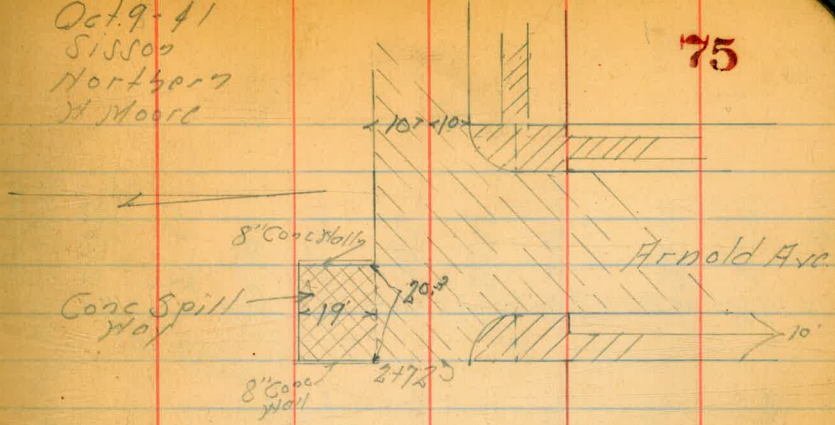
OK (B.P. out)  
Adams +  
Florida  
340.00

Cross Section 107 Upas &  
Villa Terrace to Arnold

Indexed  
LM

Oct. 9-41  
Sisson  
Northey &  
H Moore

75



Lt. 5

A

0+0 = White Villa Terrace

0-10 = XCB

0-25 = X

0-40 = FCB

TP 1.57 294.98 2.38 293.41

0-50 = White Villa Terrace

TP 2.38 295.79 8.64 293.41

BM 2.04 303.05 300.01

Red. 10/1/41 (2)

19.4  
160-Top Slope  
41  
275.6  
288.2

16.6  
135-Top Slope  
278.4

10.4  
41-T.S.  
284.6

6.9  
30  
288.1

6.0  
37  
289.0

5.5  
37  
289.9

2.5  
10  
292.5

1.5  
16  
294.3

288.87

7.4  
10-Gutter  
287.84

6.0  
30  
289.0

5.9  
30  
291.1

2.0  
10  
293.0

1.6  
16  
294.2

5.38  
10-Top  
287.60

5.4  
10-CB  
289.57

4.5  
10-CB  
290.63

2.8  
10-CB  
292.2

2.5  
16-CB  
293.25

5.88  
13-CB  
289.10

6.1  
10-Gut.  
287.55

5.05  
10-Gut  
289.93

3.25  
10-Gutter  
291.73

2.8  
10-Gutter  
292.80

5.85  
00-CB  
289.13

5.46  
5  
289.52

4.18  
290.80

2.88  
292.10

2.91  
10-Gutter  
292.88

6.46  
288.52

4.96  
10-Crossed  
290.22

5.56  
10  
291.42

2.80  
292.18

2.97  
12.5-Gutter  
292.87

5.26  
12.7-CB  
289.72

5.51  
20-Gutter  
291.46

2.86  
30  
292.42

2.80  
30-Gutter  
292.75

2.81  
12.5-CB  
293.48

5.38  
12.7-Gutter  
289.60

5.05  
30-CB  
291.95

1.69  
30-CB  
293.29

1.69  
30-CB  
293.29

2.92  
30  
293.49

3.0  
292.0

Lt 5  
2 pos Feat  
3' 5" Villa Terrace

N.M.B.P.  
N.Y. City  
Villa Terrace

295.79

Upas St.

1731.85 FL Alley

140

0788

0778

0756

TP 0.53 284.22 1129 288.69

0740

294.98

268.2	265.7	264.6	263.8	261.6
283.8	281.6	279.2	277.7	269.5
283.5	282.1	279.3	278.1	275.6
284.1	281.6	279.8	278.4	273.1
283.9	282.8	279.7	278.4	276.2
283.9	283.2	279.7	279.2	276.8
284.8	282.0	273.9	271.9	268.1
284.6	276.9	270.1	269.2	267.6
281.2	274.4	271.1	269.2	267.6

77

294.98



2+50

2+25

2+0

1+75

1+57

TP 0.28 272.15 1135 272.87

1+46.83 H.L. Flory

284.22

$\frac{16.0}{80} \frac{257.2}{75}$   
 $\frac{5.9}{50} \frac{263.4}{80}$   
 $\frac{8.6}{50} \frac{264.7}{80}$   
 $\frac{10.7}{26} \frac{262.5}{80}$   
 $\frac{9.9}{5.9} \frac{263.3}{80}$   
 $\frac{8.0}{80} \frac{265.2}{80}$

15.1  
70.75  
258.1

$\frac{8.8}{59} \frac{264.4}{72}$   
 $\frac{8.2}{72} \frac{265.0}{72}$   
 $\frac{10.2}{37} \frac{263.0}{72}$   
 $\frac{9.8}{18} \frac{263.4}{72}$   
 $\frac{7.8}{14} \frac{265.9}{72}$   
 $\frac{6.6}{6.6} \frac{266.6}{72}$

13.5  
88.75  
80.0  
259.7

$\frac{7.6}{50} \frac{265.6}{72}$   
 $\frac{6.7}{72} \frac{266.5}{72}$   
 $\frac{9.0}{37} \frac{264.2}{72}$   
 $\frac{9.0}{24} \frac{264.2}{72}$   
 $\frac{6.5}{20} \frac{266.7}{72}$   
 $\frac{6.4}{6.4} \frac{266.8}{72}$

$\frac{13.0}{55} \frac{260.9}{72}$   
 $\frac{8.0}{55} \frac{268.2}{72}$   
 $\frac{5.5}{42} \frac{267.2}{72}$   
 $\frac{9.8}{35} \frac{264.8}{72}$   
 $\frac{10.0}{50} \frac{265.2}{72}$   
 $\frac{5.5}{18} \frac{267.7}{72}$   
 $\frac{6.4}{6.4} \frac{267.7}{72}$

$\frac{13.0}{55} \frac{261.5}{72}$   
 $\frac{5.5}{55} \frac{267.9}{72}$   
 $\frac{7.0}{70} \frac{266.0}{72}$   
 $\frac{7.0}{50} \frac{267.2}{72}$   
 $\frac{9.8}{50} \frac{268.2}{72}$   
 $\frac{6.4}{6.4} \frac{268.0}{72}$

$\frac{13.0}{55} \frac{261.2}{72}$   
 $\frac{15.2}{53} \frac{268.9}{72}$   
 $\frac{15.6}{30} \frac{268.6}{72}$   
 $\frac{15.1}{5} \frac{269.1}{72}$   
 $\frac{16.6}{16.6} \frac{269.2}{72}$

$\frac{8.0}{10} \frac{265.2}{72}$   
 $\frac{10.4}{15.75} \frac{262.8}{72}$   
 $\frac{10.4}{30} \frac{262.8}{72}$

$\frac{7.4}{80} \frac{265.8}{72}$   
 $\frac{9.9}{12.75} \frac{263.3}{72}$   
 $\frac{8.8}{30} \frac{264.4}{72}$

$\frac{6.5}{14} \frac{266.7}{72}$   
 $\frac{8.7}{28.75} \frac{264.5}{72}$   
 $\frac{5.8}{30} \frac{265.0}{72}$

$\frac{6.0}{6.0} \frac{267.2}{72}$   
 $\frac{8.1}{20.75} \frac{265.1}{72}$   
 $\frac{7.0}{30} \frac{265.3}{72}$

$\frac{5.5}{55} \frac{267.9}{72}$   
 $\frac{7.0}{70} \frac{266.2}{72}$   
 $\frac{8.7}{30} \frac{266.1}{72}$

$\frac{14.7}{15} \frac{269.5}{72}$   
 $\frac{17.4}{17.4} \frac{266.8}{72}$   
 $\frac{17.4}{30} \frac{266.8}{72}$

284.22

77

78

Red. 10/1/41

BM 1.06 270.04

N 11 B.P.  
Upas St.  
H 13070  
26495

TP 4.48 271.10 6.53 266.62

2+83 = F.C. Line Arnold

261.07  
12.08  
10

261.20  
11.95

261.28  
11.78

261.44  
11.71

261.92

261.71  
11.68  
11.69  
11.70  
11.71  
11.72  
11.73

2+72 = F.L. Arnold Ave

255.8  
17.4  
17.35  
17.30  
17.30  
17.30

256.1  
16.6  
16.6  
16.6  
16.6  
16.6

257.72  
15.42

258.94  
14.71

262.26  
13.29

260.98  
12.17

261.19  
11.96

262.5  
10.7

261.45  
11.50

262.06  
11.09

262.2  
11.30

2+60

273.15

262.1  
15.5

262.2  
15.30

262.2  
15.15

262.2  
15.00

262.2  
14.85

262.5  
14.70

262.5  
14.55

262.6  
14.40

262.6  
14.25

29 = F.L. Arnold  
29 = F.L. Arnold

29 = Top Hall  
29 = Top Hall

10 = Top  
10 = Top

11 = Top  
11 = Top

12 = Top  
12 = Top

257.72  
15.42

258.94  
14.71

262.26  
13.29

260.98  
12.17

261.19  
11.96

262.5  
10.7

261.45  
11.50

262.06  
11.09

262.2  
11.30

257.72  
15.42

258.94  
14.71

262.26  
13.29

260.98  
12.17

261.19  
11.96

262.5  
10.7

261.45  
11.50

262.06  
11.09

262.2  
11.30

29 = F.L. Arnold  
29 = F.L. Arnold

29 = Top Hall  
29 = Top Hall

10 = Top  
10 = Top

11 = Top  
11 = Top

12 = Top  
12 = Top

TABLE VI (continued)  
SINES, COSINES, TANGENTS, COTANGENTS (continued)

degs.	sin 0'	tan 0'	sin 10'	tan 10'	sin 20'	tan 20'	sin 30'	tan 30'	sin 40'	tan 40'	sin 50'	tan 50'	degs.
46	7193	1.0355	7214	1.0416	7234	1.0477	7254	1.0533	7274	1.0599	7294	1.0661	43
47	314	.0724	333	.0736	353	.0850	373	.0913	392	.0977	412	.1041	42
48	431	.1106	451	.1171	470	.1237	490	.1303	509	.1369	528	.1436	41
49	547	.1504	566	.1571	585	.1640	604	.1708	623	.1778	642	.1847	40
50	660	1.1918	7679	1.1938	7698	1.2059	7716	1.2131	7735	1.2203	7753	1.2276	39
51	771	2349	790	.2423	808	.2497	826	.2572	844	.2647	862	.2723	38
52	880	2799	898	.2876	916	.2954	934	.3032	951	.3111	969	.3190	37
53	986	3270	8004	.3351	8021	.3452	8039	.3514	8056	.3597	8073	.3680	36
54	8090	.3764	107	.3848	124	.3934	141	.4019	158	.4106	175	.4193	35
55	192	.4281	208	.4370	225	.4460	241	.4550	258	.4641	274	.4733	34
56	290	.4826	307	.4919	323	.5013	339	.5108	355	.5204	371	.5301	33
57	387	.5399	403	.5497	418	.5597	434	.5697	450	.5798	465	.5900	32
58	480	.6003	496	.6107	511	.6212	526	.6319	542	.6426	557	.6534	31
59	572	.6643	587	.6753	601	.6864	613	.6977	631	.7090	646	.7205	30
60	660	1.7321	8675	1.7437	8689	1.7556	8704	1.7675	8718	1.7797	8732	1.7917	29
61	746	.8040	760	.8165	774	.8291	788	.8418	802	.8546	816	.8676	28
62	829	.8807	843	.8940	857	.9074	870	.9210	884	.9347	897	.9486	27
63	910	.9626	923	.9768	936	.9912	949	2.0057	962	2.0204	975	2.0353	26
64	988	2.0503	9001	2.0655	9013	2.0809	9026	.0965	9038	.1123	9051	.1283	25
65	9083	.1445	075	.1609	088	.1775	100	.1943	112	.2113	124	.2286	24
66	135	.2460	147	.2637	159	.2817	171	.2998	182	.3183	194	.3369	23
67	205	.3559	216	.3750	228	.3945	239	.4142	250	.4342	261	.4545	22
68	272	.4751	283	.4960	293	.5172	304	.5386	315	.5605	325	.5826	21
69	336	.6051	346	.6279	356	.6511	367	.6746	377	.6985	387	.7228	20
70	397	2.7475	9407	2.7725	9417	2.7980	9426	2.8239	9436	2.8502	9446	2.8770	19
71	455	.9042	465	.9319	474	.9600	483	.9887	492	3.0178	502	3.0475	18
72	511	3.0777	520	3.1084	528	3.1397	537	3.1716	546	.2041	555	.2371	17
73	563	.2709	572	.3052	580	.3402	588	.3759	596	.4124	605	.4495	16
74	613	.4374	621	.5261	628	.5656	636	.6059	644	.6470	652	.6891	15
75	659	.7321	667	.7760	674	.8208	681	.8657	689	.9136	696	.9617	14
76	703	4.0108	710	4.0611	717	4.1126	724	4.1653	730	4.2193	737	4.2747	13
77	744	.3315	750	.3897	757	.4494	763	.5107	769	.5736	775	.6382	12
78	781	.7046	787	.7729	793	.8430	799	.9152	805	.9894	811	5.0658	11
79	816	.1446	822	5.2257	827	5.3093	833	5.3955	838	5.4845	843	.5764	10
80	9348	5.6713	9853	5.7694	9858	5.8708	9863	5.9758	9868	6.0844	9872	6.1970	9
81	877	6.3138	881	6.4348	886	6.5606	890	6.6912	894	.8269	899	.9682	8
82	903	7.1154	907	7.2637	911	7.4287	914	7.5958	918	7.7704	922	7.9530	7
83	925	8.1443	929	8.3450	932	8.5555	936	8.7769	939	9.0098	942	9.2553	6
84	945	9.5144	948	9.7882	951	10.078	954	10.385	957	10.711	959	11.059	5
85	962	11.430	964	11.826	967	12.250	969	12.706	971	13.197	974	13.727	4
86	976	14.300	978	14.924	980	15.605	981	16.350	983	17.169	985	18.075	3
87	986	19.081	988	20.206	989	21.470	990	22.903	992	24.542	993	26.432	2
88	994	28.636	9995	31.242	9996	34.363	997	38.189	997	42.964	9998	49.104	1
89	9998	57.290	9999	68.750	9999	85.940	9999	114.58	1.000	171.88	1.000	343.77	0
degs.	60'	60'	50'	50'	40'	40'	30'	30'	20'	30'	10'	10'	degs.
	cos	cot	cos	cot	cos	cot	cos	cot	cos	cot	cos	cot	

23° 0'

9147

914750

75

9147

175

957.35

4029

9147

160.0725

9187

75

45935

64309

6890

91.47

689025

60.37

9730

886023

9



Card  
The Great...

11° 58'

$$\begin{array}{r} 83.57 \\ 30 \\ \hline 113.57 \end{array}$$

$$\begin{array}{r} 3+49 \\ 21 \\ \hline 370 \end{array}$$

$$\begin{array}{r} 10 \\ 4 \\ \hline 14 \end{array} \quad \begin{array}{r} 10 \\ 4 \\ \hline 14 \end{array}$$

$$\begin{array}{r} 125.5 \\ 10 \\ \hline 135.5 \end{array}$$

120'

$$\begin{array}{r} 8980 \\ 277 \\ \hline 8701 \end{array}$$

$$\begin{array}{r} 28.75 \\ + 2.64 \\ \hline 31.39 \checkmark \\ - 8.74 \\ \hline 22.65 \checkmark \\ + 6.44 \\ \hline 29.09 \checkmark \\ - 8.60 \\ \hline 20.49 \checkmark \\ + 4.50 \\ \hline 24.99 \checkmark \\ - 5.90 \\ \hline 19.09 \checkmark \\ + 3.17 \\ \hline 22.26 \checkmark \\ - 2.58 \\ \hline 19.68 \checkmark \\ + 14.21 \\ \hline 31.89 \\ 28.75 \\ \hline 3.14 \end{array}$$

$$\begin{array}{r} 11.0 \\ 3.5 \\ \hline 7.7 \\ 2.1 \\ \hline 9.8 \end{array}$$

$$\begin{array}{r} 89.80 \\ 2.87 \\ \hline 86.83 \\ 8.5 \\ \hline 10.3 \end{array}$$

$$\begin{array}{r} 89.70 \\ 3.01 \\ \hline 16.89 \\ 86.72 \\ \hline 3 \end{array}$$