

1313

PASTS

LEVEL BOOK

No. 380F

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

3744
3685

59

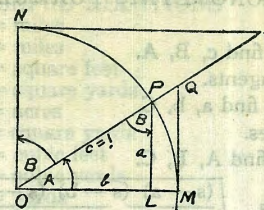


TABLE II

TRIGONOMETRIC FORMULÆ.

$$\angle A = \angle MOP \quad \angle B = \angle PON = \angle OPL$$

$$R = OB = c = 1$$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

$$\sin \frac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \quad \cos \frac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \quad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Sines} \quad \frac{\sin A}{a} = \frac{\sin B}{b} = \frac{\sin C}{c}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$$

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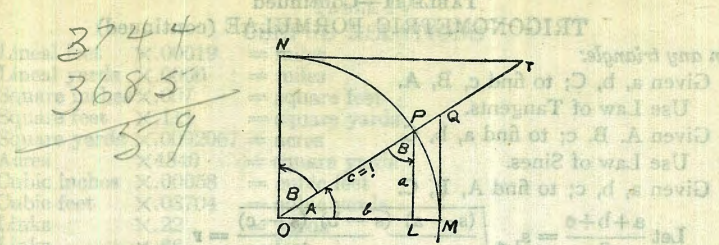


TABLE II
TRIGONOMETRIC FORMULÆ.

$$\begin{aligned} \angle A &= \angle MOP & \angle B &= \angle PON = \angle OPL \\ R &= OB = c = 1 \\ \sin A &= \frac{a}{c} = \frac{a}{1} = a = \cos B = LP \\ \cos A &= \frac{b}{c} = \frac{b}{1} = b = \sin B = OL \\ \tan A &= \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ \\ \cot A &= \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT \\ \sec A &= \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ \\ \csc A &= \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT \\ \text{vers } A &= \frac{LM}{OP} = LM = \text{covers } B \# \\ \text{covers } A &= \frac{OP - LP}{OP} = OP - LP = \text{vers } B \\ \text{exsec } A &= PQ = \text{coexsec } B \\ \text{coexsec } A &= PT = \text{exsec } B \\ \sin \frac{1}{2} A &= \sqrt{\frac{1 - \cos A}{2}} & \cos \frac{1}{2} A &= \sqrt{\frac{1 + \cos A}{2}} \\ \sin 2A &= 2 \sin A \cos A & \cos 2A &= \cos^2 A - \sin^2 A \\ \text{Law of Sines} & \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{C} \\ \text{Law of Cosines} & c^2 = a^2 + b^2 - 2ab \cos C \\ \text{Law of Tangents} & \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)} \end{aligned}$$

1313

ENGINEERING DEPARTMENT,
CITY OF SAN DIEGO,
CALIFORNIA.

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See opposite page 1313

201

1313

X sec. Winnett	Tooley to Orange	1
" " "	" " Lemon Grove	15
" " TOOLEY	Winnett to Republic	32
" " "	" " Oriole	36
" " Myrtle	Boundary to Nile	42
" " Alley BIK 36	Parish & Loomis	46

Emb 1

Hub
Tooley
ett.

Five toms 26 checked all

113.4

151.36
 59
 451.95

Jan 15-27
 London

X Sec Winett from N.L. Tooley
 to St. Ordway St Springfield
 60' St 10' 13' 40' 10'

bottom
 base
 Flag Pole
 Lot 168 Emp
 444

B.M.	7.34	459.29		451.95
T.P.	0.07	446.32	13.04	446.25
T.P.	0.13	433.44	13.01	433.31
T.P.	1.17	421.59	13.02	420.42
B.M.	2.68	419.32	4.95	416.64

Set by Hub
 N.W. Tooley
 & Winett.

N.L. Tooley

WL		2.6		416.7.
+5		3.0		416.3
eb		2.8		416.5
+5		3.1		416.2
1/4		3.1		416.2
+7		2.9		416.4
+		2.9		416.4
+3		2.7		416.6 146.6
+7		3.0		216.3 146.5
1/4		2.8		716.5 146.5
+6		2.4		716.9 146.9
eb		0.7		716.6 146.6
E.L.		0.7		418.4

Plotted Jan-24-29
 C.B.H.

Neb Tooley

F.L.		1.3		418.0
+3		1.5		417.8
+8		2.0		417.3
eb		2.7		416.6
+5		3.3		416.0
1/4		3.4		415.9
+2		3.7		415.6

419.32

Ncb Tooley

+8	3.4	415.9
±	3.5	415.8
1A	4.1	415.2
ob	3.7	415.6
wL	3.3	416.0

N 1/4 Tooley

wL	4.2	415.1
cb	4.5	414.8
1A	4.6	414.7
+2	4.7	414.6
±	4.4	414.9
1A	4.1	415.2
cb	4.0	415.3
EL	3.2	416.1

± Tooley

EL	3.5	415.8
+3	3.6	415.7
ob	4.5	415.8
+4	5.1	414.2
1A	5.0	414.3
±	5.2	414.1
1A	5.2	414.1
ob	4.9	414.4
+6	5.0	414.3
wL	4.6	414.7

419.32

S 1/4 Tooley

wL	5.2	414.1
cb	6.2	413.1
+5	6.0	413.3
1A	6.3	413.0
+2	6.7	412.6
+4	6.3	413.0
±	6.3	413.0
1A	6.1	413.2
+6	6.3	413.0
cb	5.8	413.5
+4	5.3	414.0
+6	5.8	413.5
EL	4.7	414.6

S ob Tooley

EL	5.3	414.0
+8	5.9	413.4
+7	8.7	410.6
cb	7.8	411.5
+3	7.9	411.4
+5	7.2	412.1
1A	7.7	411.6
±	7.7	411.6
+7	8.0	411.3
+8	7.6	411.7
1A	7.5	411.8

419.32
Seb Tooley.

eb	7.3	4120
+3	7.1	4122
+8	7.4	4119
w.L.	7.2	4121
<u>S.L. Tooley 0+00</u>		
w.L.	8.9	4104
eb	8.9	4104
+4	8.5	4108
1/4	8.9	4104
+4	9.0	4103
+6	9.3	4100
E	9.0	4103
+9	9.2	4101
1/4	9.4	4099
+1	9.6	4097
+4	8.8	4105
+7	8.6	4107
cb	9.7	4096
+1	10.6	4087
+4	7.5	4118
EL	6.6	4127

0+25

419.32

3

EL	8.6	4107
+6	10.3	4090
cb	13.6	405.7
+3	12.5	406.8
1/4	12.6	406.7
E	12.6	406.7
+2	13.2	406.1
+8	12.0	407.3
1/4	12.0	407.3
cb	13.0	406.3
+6	14.4	404.9
w.L.	14.3	405.0
5w	14.1	405.2
10w	12.5	406.8
T.P.	1.83	408.13
<u>0+50</u>		
10w	4.6	403.5
w.L.	6.3	401.8
cb	7.8	400.3
1/4	7.7	400.4
+7	6.7	401.4
E	5.4	402.7
+7	4.9	403.2
1/4	5.0	403.1
cb	5.5	402.6
+1	6.0	402.1

0 +50	408.43		
+4		2.0	406.1
EL		0.8	407.3
<u>0 +75</u>			
EL		5.1	403.0
+3		6.6	401.5
+7		6.6	401.5
+9		8.5	399.6
cb		9.2	398.9
1/4		8.8	399.3
⊕		9.1	399.0
+7		12.7	395.4
1/4		13.3	394.8
cb		14.1	394.0
W.L		10.6	397.5
7w		9.5	398.6
10w		9.6	398.5
T.P. 3.67	400.61	11.19	396.94

<u>1+00</u>			
15w		8.7	391.9
w.l.		10.9	389.7
cb		12.0	388.6
1/4		11.2	389.4
⊕		6.6	394.0
+2		5.5	395.1
1/4		5.0	395.6

<u>1+00</u>	400.61		
cb		5.6	395.0
+W		6.0	394.6
+8		0.8	399.8
EL		0.1	400.5
<u>1+25</u>			
EL		2.7	397.9
+6		5.7	394.9
cb		8.7	391.9
+1		9.0	391.6
1/4		8.0	392.6
+9		8.6	392.0
⊕		9.6	391.0
1/4		16.0	384.6
+2		16.9	383.7
cb		17.5	383.1
w.l.		18.0	382.6
15w		11.0	389.6

<u>1+50</u>			
20w		15.9	384.7
w.l.		20.8	379.8
cb		20.0	380.6
1/4		16.5	384.1
⊕		12.0	388.6
+2		11.2	389.4
1/4		11.3	389.3

1+50: 400.67

+5	11.6	
+9	12.5	
cb	10.3	
+4	7.1	
EL	5.3	395.3

1+75

EL	9.1	391.5
+2	9.6	
+3	11.4	
T.P.	1.26	388.81
cb	3.1	
+2	4.5	
+8	3.5	
1/4	2.9	
+8	2.7	
±	4.0	384.8
1/4	8.3	
cb	10.9	
w.l.	12.8	376.0
6w	12.5	
20w	8.5	

2+00 388.81 5

20w	11.2	
7w	15.5	
w.l.	15.3	373.5
+5	15.2	
cb	13.4	

1/4	10.4	
±	7.7	381.1
+4	5.5	
1/4	5.7	
+8	6.8	
+9	8.1	
cb	8.0	
+1	5.5	
+8	0.5	
EL	10.4	389.2

2+25

EL	4.4	384.4
+2	4.6	
+8	8.4	
+9	9.9	
cb	10.0	
+1	10.0	
+2	9.1	
+4	8.7	
1/4	8.5	

<u>2+25</u>	388.81		
+6	8.6		
+	10.6	378.2	
1/4	18.9		
cb	15.6		
+8	17.9		
wL	17.9	370.9	
10W	17.8		
20W	14.4		
T.P. 3.39	381.82	10.38	378.43

<u>2+50</u>			
22W	9.8		
12W	12.8		
wL	12.5	369.3	
cb	11.2		
+5	10.6		
1/4	9.1		
+	6.0	375.8	
+4	3.7		
1/4	3.5		
+9	4.2		
cb	4.8		
+1	5.8		
+5	1.0		
EL	+1.2	383.0	

<u>2+75</u>	381.82		
EL	2.0	379.8	
+7	4.3		
cb	7.2		
+1	7.5		
+2	6.0		
1/4	5.7		
+5	6.0		
+	7.7	374.1	
1/4	10.7		
cb	13.7		
wL	15.0	366.8	
15W	15.7		
25W	12.0		

<u>3+00</u>			
25W	15.6		
20W	18.0		
wL	17.7	364.1	
cb	16.5		
1/4	18.2		
+	10.0	371.8	
+4	7.8		
1/4	7.4		
+9	8.1		
cb	8.7		
+1	7.3		
+6	4.8		

<u>3+00</u>	381.92		
E.L.		3.1	378.7
<u>3+25</u>			
E.L.		5.4	376.4
+5		7.0	
+7		9.2	
cb		9.6	
+3		10.4	
1/4		9.8	
+9		9.6	
±		10.0	371.8
T.P.	3.69	11.55	370.27
1/4		6.9	367.0
cb		9.9	
+7		11.8	
W.L.		12.0	362.0
20W		12.0	
25W		8.8	
<u>3+50</u>			
25W		10.8	
18W		14.9	
W.L.		14.6	359.4
cb		12.8	
1/4		9.2	
±		4.2	369.8
+3		3.5	

Ganga 4 1/2 ft. on East of B+35

<u>3+50</u>	373.96		7
1/4		4.1	
+7		4.0	
cb		3.1	
+6		+0.3	
E.L.		+0.2	374.2
<u>3+75</u>			
E.L.		0.6	373.4
+5		1.7	
cb		5.1	
+1		5.9	
1/4		5.7	
+7		5.6	
±		7.1	366.9
1/4		10.8	
cb		14.6	
+2		15.3	
W.L.		15.5	358.5
10W		16.3	
20W		16.0	
25W		14.2	

373.96

A+00

30W	16.0	
20W	18.0	
10W	18.2	
wL	17.9	356.1
+5	17.9	
cb	15.6	
1/4	12.8	
+	10.0	364.0
+4	7.8	
1/4	7.5	
+9	8.2	
cb	7.2	
+5	4.3	
E.L.	2.6	371.4

A+25

E.L.	3.4	370.6
+5	5.6	
cb	8.7	
+1	9.4	
1/4	9.1	
+7	9.3	
+	11.1	362.9
1/4	15.7	
cb	18.0	
w.L.	20.0	354.0

A+25

373.96

8

20W	20.3
30W	17.8

A+50

35W	20.6	
30W	22.1	
15W	21.8	
w.L.	21.3	352.7
cb	18.0	
1/4	15.5	
+	12.0	362.0
+1	11.0	
1/4	10.4	
+9	10.9	
cb	9.5	
+5	6.9	
E.L.	3.9	370.1

A+75

E.L.	4.6	369.4
+1	4.8	
+7	8.4	
cb	12.0	
1/4	11.7	
+8	12.1	
+	13.5	360.5
T.P.	0.40	361.64
	12.72	361.24

4+75

36164

1/4	4.8	
eb	7.5	
w.L.	10.8	350.8
30W	11.7	
40W	8.0	

5+00

40W	11.3	
34W	14.1	
20W	13.4	
10W	14.0	
w.L.	11.5	350.1
cb	8.1	
1/4	5.2	
±	1.2	360.4
+8	0.8	
1/4	0.8	
cb	0.9	
+5	+3.8	
E.L.	+5.7	367.3

5+25

E.L.	+3.8	365.4
+5	+2.0	
cb	3.5	
1/4	3.0	
±	3.2	358.4

5+25

36164

9

+4	5.5	
1/4	6.8	
cb	8.9	
w.L.	12.0	349.6
15W	15.6	
30W	12.0	

5+50

40W	17.5	
20W	16.9	
w.L.	13.3	348.3
cb	11.0	
1/4	8.6	
+8	7.3	
±	5.6	356.0
1/4	5.4	
+7	5.0	
cb	5.9	
+6	0.3	
E.L.	+1.1	362.7

5+75

E.L.	0.3	361.3
+4	1.5	
+9	5.2	
cb	8.0	
+3	7.1	

5+75

361.64

1/4	7.5	
+8	7.9	
±	8.7	352.9
+4	10.6	
1/4	11.7	
cb	13.4	
w.l.	15.7	345.9
16w	19.7	
40w	19.5	
<u>6+00</u>		
34w	22.0	
10w	21.6	
w.l.	19.3	342.3
cb	16.2	
1/4	13.9	
+6	12.4	
±	10.1	351.5
+1	9.7	
1/4	9.5	
+7	9.4	
cb	10.2	
+2	7.0	
+6	4.4	
EL	3.4	358.2

6+25

361.64

10

EL	6.5	355.1
+3	6.9	
+8	9.4	
cb	12.4	
+5	11.7	
1/4	11.6	
+9	11.9	
±	12.5	349.1
+2	14.1	
1/4	16.0	
cb	18.6	
w.l.	21.9	339.7
3w	23.0	
34w	23.0	
<u>6+50</u>		
30w	24.9	
3w	24.8	
w.l.	23.6	338.0
cb	21.1	
1/4	18.2	
+7	16.8	
±	15.0	346.6
+2	14.2	
1/4	14.0	
+7	14.0	

<u>6+50</u>	361.04		
cb		14.6	
+1		12.2	
+7		8.6	
E.L.		8.0	353.6

<u>6+75</u>			
E.L.		10.2	351.4
+2		10.4	
T.P.	0.40	13.00	348.64
+9		3.7	
cb		3.5	
+4		3.1	
1/4		3.1	
+9		3.4	
±		4.3	344.7
+5		6.7	
1/4		8.1	
cb		10.7	
+4		12.7	
W.L.		13.4	335.6
25W		13.7	
35W		9.1	

<u>7+00</u>	349.04		11
25W		13.2	
10W		15.0	
W.L.		15.1	333.9
cb		14.1	
1/4		11.1	

±		6.8	342.2
+1		5.6	
1/4		5.2	
+7		5.3	
cb		5.9	
+2		3.4	
+8		0.3	
E.L.		10.0	349.0

<u>7+25</u>			
E.L.		1.7	347.3
+2		2.3	
+8		5.5	
cb		7.5	
+3		7.0	
1/4		6.8	
+8		7.3	
±		8.5	340.5
+3		10.1	
1/4		12.9	
cb		15.9	

7+25

349.04

W.L. 16.9 332.1

20W 16.3

30W 12.6

7+50

25W 15.2

15W 17.9

W.L. 18.0 331.0

cb 17.8

1/4 14.1

+6 11.9

+ 10.4 338.6

+2 9.4

1/4 8.8

cb 9.0

+8 6.5

EL 4.3 344.7

7+75

EL 5.7 343.3

+8 8.0

cb 10.7

1/4 10.6

+8 11.0

+ 12.2 336.8

+2 14.1

7+75

349.04

12

1/4 16.6

cb 19.0

W.L. 19.0 330.0

15W 19.2

25W 14.1

T.P. 0.73 336.71 13.06 335.98

8+00

30W 3.5

15W 8.0

W.L. 8.2 328.5

cb 8.1

1/4 5.9

+7 3.3

+ 1.5 335.2

+2 0.0

1/4 0.0

cb 0.6

+3 +1.6

EL +3.7 340.4

8+25

EL +3.1 339.8

+7 +0.7

cb 2.7

1/4 1.7

+8 1.7

+ 3.0 333.7

<u>8+25</u>	336.71	
+2	4.3	
1/4	6.8	
cb	9.2	
w.L.	9.7	327.0
14W	9.2	
25W	5.7	
<u>8+50</u>		
25W	7.1	
13W	11.0	
w.L.	11.0	325.7
cb	10.6	
1/4	8.5	
+8	6.0	
±	4.6	332.1
+3	3.4	
1/4	3.7	
+7	4.1	
cb	5.0	
+5	0.2	
E.L.	+0.8	337.5

<u>8+75</u>	336.71	
E.L.	1.0	335.7
+4	1.7	
+7	3.0	
cb	5.6	
+1	6.7	
+5	5.5	
1/4	5.4	
+7	5.4	
±	7.5	329.2
1/4	10.6	
cb	12.3	
w.L.	12.3	324.4
13W	11.7	
20W	9.0	
<u>9+00</u>		
20W	10.1	
w.L.	13.8	322.9
cb	13.7	
1/4	11.8	
+6	11.0	
±	8.8	327.9
+2	7.3	
1/4	7.1	
+3	7.1	
cb	8.4	
+7	3.1	

336.71

9+00

EL

2.7

334.0

9+40²¹Springfield
NL Orange St.

EL

9+39.9 ecc.

6.0

330.7

+8

8.7

cb

10.4

1/4

10.1

+7

9.9

±

11.3

325.4

1/4

14.0

cb

15.8

wL

15.8

320.9

10W

15.6

20W

12.4

9+70²¹ = ± Orange

20W

13.1

wL

17.8

318.9

cb

17.7

1/4

16.5

±

12.9

323.8

1/4

12.7

cb

12.0

E.L.

10.2

326.5

SEE
F.O. 1225.76
Xmittar to
Springfield.

14

336.71

10+00²¹ = 5L Orange

EL

11.5

325.2

+7

13.2

T.P.

0.28

324.81

12.18

324.53

+8

3.9

cb

3.9

1/4

3.7

+8

3.8

±

4.7

320.1

+4

6.4

1/4

7.0

cb

6.9

wL

7.0

317.8

15W

3.4

T.P.

0.49

312.39

12.91

311.90

BM

Hub NE Whitt & Orange

11.71

300.68 (300.64)

old Hub gone
New Hub set
1.0 ± Lower
see Xsec of Oriole

X 500 Winett from N.L.
Tooley to S.L. Leman Grove Dr.

15

BM 2.60 419.24 416.64

both by H.C.
N.W. Winett
& Tooley

0+75

419.24

0+00 = N.L. Tooley (P.1)

w.L.

4.9

414.3

0+25

+8

5.6

413.6

w.L.

1.7

417.5

+9

7.5

411.7

+8

1.3

417.9

cb

7.5

411.7

cb

2.3

416.9

1/4

6.8

412.4

1/4

3.0

416.2

+4

6.6

412.6

±

2.7

416.5

±

6.9

412.3

1/4

2.4

416.8

+7

6.3

412.9

+5

2.1

417.1

+9

5.4

413.8

+7

0.9

418.3

1/4

5.4

413.8

cb

1.0

418.2

+6

5.6

413.8

EL

0.9

418.3 ✓

cb

4.8

414.4

EL

0.9

418.3 ✓

cb

4.8

414.4

0+50

EL

3.7

415.5 ✓

EL

2.5

416.7 ✓

1+00

cb

2.9

416.3

EL

8.8

410.4 ✓

+7

3.0

416.2

cb

9.1

410.1

+8

3.8

415.4

1/4

8.1

411.1

1/4

4.0

415.2

+6

8.6

410.6

±

4.2

415.0

+8

10.3

408.9

+6

4.2

415.0

±

10.6

408.6

1/4

4.4

414.8

1/4

10.2

409.0

+6

4.8

414.4

cb

11.0

409.2

cb

4.4

414.8

+2

8.3

410.9

+2

3.0

416.2

w.L.

7.8

411.4

w.L.

2.6

416.6

Plotted Jan 25-1929

C.B.H.

1+25	419.24		
w.L		11.3	407.9
+7		11.8	407.4
+9		14.8	404.4
cb		15.0	404.2
1/4		14.2	405.0
±		14.1	405.1
+2		13.2	406.0
1/4		13.4	405.8
cb		13.7	405.5
E.L.		13.4	405.8 ✓
T.P. 0.27	406.63 ✓	12.88	406.36
1+50			
E.L.		5.2	401.4 ✓
cb		4.5	402.1
+5		4.5	402.1
1/4		4.8	401.8
+5		4.3	402.3
±		4.4	402.2
+7		5.7	400.9
1/4		5.6	401.0
+8		6.0	401.6
cb		6.3	400.3
+3		6.6	400.0
+4		4.1	402.5
w.L.		2.7	403.7

1+75	406.63		16
w.L.		7.7	398.9
+6		8.2	398.4
+6		10.9	395.7
cb		10.2	396.4
+1		10.0	396.6
1/4		9.7	396.9
±		8.9	397.7
1/4		10.0	396.6
cb		9.0	397.6
E.L.		7.8	398.8 ✓
2+00			
E.L.		13.1	393.5 ✓
+5		13.5	393.1
cb		14.1	392.5
+5		14.3	392.3
1/4		13.6	393.0
+3		13.5	393.1
+7		14.7	391.9
±		13.2	393.4
+4		13.0	393.6
1/4		13.5	393.1
+9		13.8	392.8
cb		14.4	392.2
+4		14.6	392.0
+4		12.3	394.3
w.L.		11.6	395.0

	406.63		
TP 0.10	393.75	12.98	393.65
2+25			
wL	2.1		391.9
+6	3.0		390.8
+6	5.2		390.6
cb	5.0		388.8
1/4	4.6		389.2
+6	3.8		390.0
±	4.5		389.3
1/4	6.1		387.7
+5	5.8		388.0
+7	4.5		389.3
cb	4.6		389.2
+3	4.6		389.2
+6	6.2		387.6
+9	5.5		388.3
EL	3.8		390.0 ✓
2+50			
10E	9.1		384.7 ✓
E.L.	9.2		384.6
+6	10.2		383.6
cb	13.0		380.8
1/4	11.0		382.8
+1	9.6		384.2
±	8.4		385.4
+3	7.9		385.9

2+50	393.75		
1/4		8.3	385.5
+5		8.8	385.0
cb		8.7	385.1
+3		8.6	385.2
+3		6.4	387.4
wL		5.1	388.7
2+75			
wL		8.5	385.3
+5		9.6	389.2
+6		12.2	381.6
cb		12.5	381.3
1/4		11.9	381.9
+9		12.1	381.7
±		12.7	381.1
+8		14.0	379.8
1/4		15.1	378.7
cb		19.9	373.9
+7		16.0	372.8
E.L.		15.1	378.7 ✓
10E		13.7	380.1 ✓

3+00 393.75

15E	17.5	375.3
FL	19.1	374.7 ✓
+3	20.0	373.8
cb	20.2	373.6
+4	20.3	373.5
1/4	18.0	375.8
♀	16.0	377.8
+3	15.2	378.6
1/4	15.3	378.5
cb	15.9	377.9
+3	16.3	377.5
+5	13.0	380.8
wL	11.8	382.0
TP 0.24	380.93	13.06 380.69 ✓
3+25		
wL	0.8	380.1
+6	3.0	377.9
+9	6.5	374.4
cb	6.5	374.4
+2	6.1	374.8
1/4	5.5	375.4
♀	5.1	375.8
1/4	8.6	372.3
cb	15.1	365.8
+3	17.3	363.6

3+25 380.93

E.L.	12.4	368.5
5E	11.6	369.3
10F	8.1	372.8 ✓
15E	7.5	373.4
3+50		
20E	11.4	369.5
10E	14.6	366.3
E.L.	20.2	360.7 ✓
cb	15.9	365.0
1/4	13.3	367.6
+5	12.1	368.8
♀	10.0	370.9
+3	8.4	372.5
1/4	8.7	372.2
+5	9.3	371.6
cb	9.3	371.6
+2	5.9	375.0
wL	3.3	377.6 ✓

380.93

3+75

w.L.	7.0	373.9
+8	8.9	372.0
cb	11.9	369.0
1/4	11.5	369.4
+7	11.5	369.4
±	13.1	367.8
+9	15.1	365.8
1/4	15.8	365.1
+4	17.2	363.7
cb	21.3	359.6
+7	22.7	358.2
E.L.	20.9	360.0 ✓
3E	19.1	361.8
10E	17.2	363.7
20E	19.3	366.6 ✓
A+00		
20E	17.3	363.6
11E	21.0	359.9
3E	22.1	358.8
E.L.	23.0	357.9 ✓
+5	26.4	354.5
cb	23.4	357.5
1/4	19.4	361.5
±	14.7	366.2
+3	13.4	

19

A+00

380.93

1/4	13.7	367.2	
+9	12.9	368.0	
cb	11.0	369.9	
w.L.	9.0	371.9 ✓	
A+25			
w.L.	10.7	370.2	
+3	11.3	369.6	
+5	12.6	368.3	
cb	13.3	367.6	
T.P. 060	368.51	13.02	367.91
1/4	3.4	365.1	
+8	3.3	365.2	
±	4.6	363.9	
1/4	9.9	358.6	
+4	11.7	356.8 ✓	
cb	14.9	353.6	
+5	17.5	351.0	
EL	14.4	354.1 ✓	
3E	12.6	355.9	
15E	10.3	358.2 ✓	

368.51

20

A+50		368.51	
15.E	13.2	355.3	
6E	15.1	353.4	
EL	17.7	350.8 ✓	
+4	20.3	348.2	
+7	18.4	350.1	
cb	16.6	351.9	
1/4	13.0	355.5	
+4	12.3	356.2	
±	8.5	360.0	
+3	5.8	362.7	
1/4	5.8	362.7	
cb	6.5	362.0	
+1	2.8	365.7	
+6	1.9	366.6	
wL	0.8	367.7 ✓	
A+75			
wL	2.7	365.6 ✓	
+3	4.4	364.1	
+9	5.1	363.4	
cb	9.1	359.4	
1/4	8.7	359.8	
+7	9.2	359.3	
±	11.5	357.0	
+6	15.6	352.9	

A+75		368.51	
1/4	16.8	351.7	
+8	19.8	348.7	
cb	20.8	347.7	
+4	21.9	346.6	
EL	18.7	349.8 ✓	
3E	17.1	351.4	
15E	15.0	353.5 ✓	
5+00			
15E	16.8	351.7	
EL	20.4	348.1 ✓	
+3	21.3	347.2	
+7	24.0	344.5	
cb	23.9	344.6	
+7	20.2	348.3	
1/4	19.1	349.4	
±	15.0	353.5	
+4	12.3	356.2	
1/4	12.2	356.3	
+6	12.0	356.5	
cb	12.5	356.0	
+4	8.0	360.5	
+8	9.7	360.8	
wL	6.1	362.4	

5+25		368.51		
WL			10.2	358.3
+2			11.4	357.1
+7			11.6	356.9
TP	0.06	355.62 ✓	12.95	355.56 ✓
cb			2.9	352.7
+3			2.5	353.1
2A			2.1	353.5
+5			2.3	353.3
+			5.5	350.1
+6			8.7	346.9
1/4			9.7	345.9
+4			10.6	345.0
cb			14.8	340.8
+3			14.8	340.8
EL			10.3	345.3 ✓
10E			8.7	346.9
15E			7.5	348.1 ✓
5+50				
15E			9.1	346.5 ✓
EL			12.3	343.3 ✓
+6			13.3	342.3
cb			16.2	339.4
+5			16.2	339.4
1/4			13.6	342.0

5+50		355.62	21
+5		12.1	343.5
+		8.8	346.8
+5		5.8	349.8
1/4		5.6	350.0
cb		6.0	349.6
+1		6.0	349.6
+4		2.3	353.3
+8		0.7	354.9
WL		+0.6	356.2 ✓
5+75			
WL		2.8	352.8 ✓
+3		4.4	351.2
+8		5.6	350.0
cb		9.6	346.0
1/4		9.3	346.3
+6		9.7	345.9
+		12.6	343.0
+8		16.1	339.5
1/4		18.4	337.2
+8		17.2	338.4
cb		16.4	339.2
+2		15.2	340.4
EL		13.8	341.8 ✓
15E		10.3	345.3 ✓

35562

6+00

15E	13.1	342.5
EL	17.2	338.4 ✓
+3	18.1	337.5
cb	19.1	336.5
+4	22.1	333.5
+8	21.5	334.1
1/4	20.1	335.5
+3	18.3	337.3
+7	17.8	337.8
Φ	15.4	340.2
+5	12.6	343.0
1/4	13.0	342.6
cb	13.5	342.1
+3	8.4	347.2
w.L.	6.6	349.9
6+25		
w.L.	9.9	345.7 ✓
+5	12.0	343.6
+8	13.6	342.0
cb	16.6	339.0
1/4	16.3	339.3
+6	16.4	339.2
Φ	18.9	336.7 ✓
+8	24.0	331.6
1/4	23.9	331.7 ✓

22

6+25

35562

+2	25.3	330.3
+4	24.0	331.6
+8	21.5	334.1
cb	21.1	334.5
EL	19.4	336.2 ✓
10E	17.8	337.8
TP 1.82	344.56	12.88 342.74 ✓
6+50		
10E	8.0	336.6
EL	9.9	334.7 ✓
cb	12.6	332.0
+3	13.0	331.6
1/4	16.7	327.9
Φ	11.2	333.4
+3	9.1	335.5 ✓
1/4	8.8	335.8
cb	9.3	335.3
+2	8.6	336.0
+5	4.4	340.2
w.L.	2.4	342.2

344.56

6+75

w.L.	5.2	339.4
+4	6.9	337.7
+9	12.2	332.4
cb	12.1	332.5
1/4	11.3	333.3
+6	11.1	333.5
+	13.3	331.3
1/4	18.4	326.2
+5	18.4	326.2
cb	15.4	329.2
E.L.	12.9	331.7 ✓
10E	10.8	333.8 ✓
7+00		
10E	12.9	331.7
E.L.	14.8	329.8 ✓
cb	17.4	327.2
+5	18.4	326.2
1/4	20.0	324.6
+4	19.8	324.8
+	16.0	328.6
+4	14.1	330.5
1/4	13.4	331.2
cb	13.8	330.8
+5	9.6	335.0
w.L.	8.1	336.5 ✓

23

7+25

344.56

w.L.	10.2	334.4
+6	11.8	332.8
T.P.	0.17	332.08
12.65		331.91
+9	1.8	330.3
cb	3.4	328.7
1/4	3.3	328.8
+6	3.1	329.0
+	5.0	327.1
1/4	10.9	321.2
+7	8.5	323.6
cb	7.7	324.4
E.L.	4.7	327.4 ✓
10E	2.3	329.8 ✓
7+50		
10E	5.5	326.6
E.L.	7.5	324.6 ✓
+7	10.1	322.0
cb	11.5	320.6
+3	12.8	319.3
1/4	10.6	321.5 ✓
+	6.3	325.8
+3	5.3	326.8
1/4	5.4	326.7
cb	5.2	326.9
+1	3.9	328.2 ✓
w.L.	0.0	332.1 ✓

332.08

7+75

w.L.	1.7	330.4
+5	3.1	329.0
cb	7.4	324.7
? = 1/4 +	7.9	324.2
+7	7.8	324.3
+	9.2	322.9
1/4	15.1	317.0
qb	12.6	319.5
EL	10.6	321.5 ✓
10E	8.2	323.9 ✓
8+00		
10E	11.6	320.5
EL	13.1	319.0 ✓
cb	16.0	316.1
1/4	14.9	317.2
+	10.7	321.4
+2	9.6	322.5
1/4	9.8	322.3
+9	7.8	322.3
cb	8.0	324.1
w.L.	4.3	327.8 ✓

24

8+25

332.08

w.L.	6.6	325.5
+8	7.9	324.2
cb	9.7	322.4
+2	12.0	320.1
1/4	11.9	320.2
+8	12.0	319.1
+	13.3	318.8
1/4	16.2	315.9
cb	18.0	314.1
EL	15.5	316.6 ✓
10E	13.6	318.5 ✓
8+50		
10E	15.3	316.8
EL	18.2	313.9 ✓
+7	19.1	13.0
cb	20.6	311.5
1/4	19.0	313.1
+	15.2	316.9
+4	13.4	318.7
1/4	13.6	318.5
+8	13.3	318.8
cb	10.7	321.4
w.L.	8.7	323.4 ✓
T.P.	0.48	319.62 ✓
	12.94	319.14

319.62

25

8+75		319.62	
w.L.	+2.0	321.6	
+9	0.0	319.6	
cb	1.8	317.8	
1/4	2.3	317.3	
+6	2.4	317.2	
±	4.4	315.2	
+5	7.0	312.6	
1/4	7.6	312.0	
cb	10.0	309.6	
EL	8.1	311.5 ✓	
10E	6.1	313.5 ✓	
9+00			
10E	9.7	309.9	
EL	11.7	307.9 ✓	
+5	12.3	307.3	
cb	10.1	309.5	
1/4	8.1	301.5	
±	4.7	314.9	
+5	2.6	317.0	
1/4	2.7	316.9	
+8	2.7	316.9	
cb	0.4	319.2	
w.L.	+1.6	321.2 ✓	

9+25		319.62	
w.L.	+0.5	320.1	
cb	1.5	318.1	
+2	1.8	317.2	
+3	3.3	316.3	
1/4	3.6	316.0	
+7	3.2	316.4	
±	3.9	315.7	
1/4	7.5	312.1	
cb	10.3	309.3	
EL	13.2	306.4 ✓	
10E	13.4	306.2	
20E	11.8	307.8	
9+50			
30E	14.1	305.5	
20E	16.8	302.8	
10E	14.8	304.8	
EL	12.6	307.0 ✓	
cb	10.1	309.5	
+5	8.4	311.2	
1/4	6.1	313.5	
+5	6.0	313.6	
±	4.0	315.6	
1/4	4.0	315.6	
+7	4.0	315.6	
+8	2.0	317.6	
cb	1.7	317.9	

319.62

9+50

W.L. +1.0 320.6

9+75

W.L. 0.5 319.1

Cb 2.2 317.4

+2 2.1 316.5

+3 4.6 315.0

1/4 4.5 315.1

+7 4.1 315.5

4 5.7 313.9

+5 7.8 311.8

1/4 8.1 311.5

Cb 10.7 308.9

EL 13.1 306.5 ✓

27E 18.8 300.8

40E 15.5 304.1

10+00

40E 19.5 300.1

30E 20.0 299.6

EL 12.6 307.0 ✓

Cb 10.2 309.4

+5 9.0 310.6

1/4 8.9 310.7

4 5.4 314.2

1/4 5.6 314.0

+7 5.6 314.0

319.62

26

10+00

Cb 3.2 316.4

W.L. 2.0 317.6

10+25

W.L. 3.2 316.4

Cb 4.6 315.0

+2 5.3 314.3

+3 7.2 312.4

1/4 7.0 312.6

4 6.7 312.9

1/4 10.2 309.4

+5 10.6 309.0

Cb 12.2 307.4

EL 14.4 305.2 ✓

30E 22.0 297.6

40E 21.6 298.0

10+50

40E 22.4 297.2

20E 23.0 296.6

EL 18.0 301.6 ✓

Cb 15.0 304.6

+5 13.3 306.3

1/4 12.7 306.9

+5 12.0 307.6

4 8.8 310.8

1/4 9.1 310.5

319.62

10+50		
+9	89	310.7
+9	58	313.8
cb	5.4	314.2
w.L	4.5	315.1
10+75		
w.L	6.8	312.8
cb	8.6	311.0
+3	12.0	307.6
1/4	12.2	307.4
±	12.1	307.5
+6	14.6	305.0
1/4	15.0	304.6
cb	18.0	301.6
EL	20.7	298.9 ✓
18E	24.0	295.6
11+00		
20E	23.0	296.6
EL	23.0	296.6 ✓
cb	20.4	299.2
1/4	17.0	302.6
±	14.8	304.8
1/4	14.2	305.4
+7	14.2	305.4
+8	12.7	306.9
cb	11.9	307.7
w.L	9.7	309.9

27

11+25	319.62	
w.L		12.5 307.1 ✓
+8		13.6 306.0
T.P.	0.37	307.35 12.64 306.98 ✓
cb		2.4 305.0
+3		4.1 303.3
1/4		4.5 302.9
±		4.8 302.6
1/4		7.0 300.4
cb		9.5 297.9
EL		11.9 295.5 ✓
10E		13.4 294.0
40E		10.9 296.5
11+50		
40E		15.8 291.6
26E		21.2 286.2
18E		22.0 285.4
16E		19.5 287.9
EL		14.9 292.5 ✓
cb		12.0 295.4
1/4		9.2 298.2
±		6.4 301.0
1/4		6.6 300.8
+6		6.2 301.2
+8		5.0 302.4
cb		4.2 303.2
w.L		2.3 305.1

11+75

307.35

w.L.	4.6	302.8
cb	6.5	300.9
+5	8.5	298.9
1/4	8.4	299.0
±	8.4	299.0
+5	8.0	299.4
1/4	9.3	298.1
cb	12.2	295.2
EL	16.0	290.4 ✓
11E	22.3	285.1
19E	22.1	285.3
30E	18.7	288.7
12+00		
30E	20.0	287.4
20E	23.1	284.3
8E	23.2	284.2
EL	18.5	288.9 ✓
cb	19.7	292.7
1/4	11.2	296.2
±	11.4	296.0
1/4	11.6	295.8
+4	11.5	295.9
+6	7.9	299.5
cb	7.5	299.9
w.L.	6.4	301.0

12+25

307.35

w.L.		8.4	299.0
cb		9.1	298.3
+2		9.6	297.8
+7		15.0	292.4
T.P.	0.54	294.89	1300 294.35
1/4		2.4	292.5
±		2.2	292.7
1/4		2.4	292.5
+2		1.3	293.6
+5		0.7	294.2
cb		3.4	291.5
EL		7.3	287.6 ✓
10E		10.9	284.0
21E		11.2	283.7
30E		7.3	284.6
12+50			
20E		8.3	286.6
14E		11.8	283.1
4E		11.4	283.5
EL		10.3	284.6 ✓
+8		9.4	285.5
cb		8.4	286.5
+6		4.9	290.6
1/4		4.7	290.2
+2		5.8	289.1

28

12+50	294.89		
¢	5.7	289.2	
1/4	6.0	288.9	
+5	6.2	288.7	
cb	+1.0	295.9	
+5	+1.0	295.9	
+6	+1.7	296.6	
wL	+2.0	296.9	
12+75			
wL	2.2	292.7	
+4	2.6	292.3	
+5	3.4	291.5	
+8	3.8	291.1	
cb	5.4	289.5	
+3	10.2	284.7	
1/4	19.6	285.3	
¢	9.2	285.7	
+7	9.0	285.9	
1/4	10.0	284.9	
+7	12.2	282.7	
cb	12.7	282.2	
EL	12.6	282.3 ✓	
2E	12.0	282.9	
10E	8.0	286.9	

29

13+00	294.89		
E.L.	12.1	282.8 ✓	
cb	12.3	282.6	
+2	13.0	281.9	
+5	15.0	279.9	
+7	14.6	280.3	
1/4	11.8	283.1	
+5	11.9	283.0	
+6	12.5	282.4	
¢	12.8	282.1	
1/4	13.0	281.9	
+9	13.8	281.1	
cb	11.9	283.0	
+2	7.7	287.2	
wL	7.1	287.8	
13+20			
wL	10.7	284.2	
+3	11.0	283.9	
T.P	0.64	282.50	13.03
+8	5.1	277.4	281.86
cb	4.6	277.9	
1/4	3.9	278.6	
¢	3.7	278.8	
+4	2.9	279.6	
+7	4.8	277.7	
+8	3.6	278.9	

282.50

13+20

1/4	3.4	279.1
cb	3.1	279.4
+5	2.8	279.7
EL	1.4	281.1 ✓

13+23

5E	8.1	274.4
EL	8.1	274.4 ✓
+4	6.0	276.5
+6	3.8	278.7
cb	4.0	278.5
1/4	4.0	278.5
+3	4.4	278.1
+4	5.8	276.7
+6	4.4	278.1
±	4.2	278.3
1/4	4.4	278.1
cb	5.0	277.5
+3	5.3	277.2
+6	+0.8	273.3
w.L.	+0.8	283.3 ✓

282.50

30

13+35

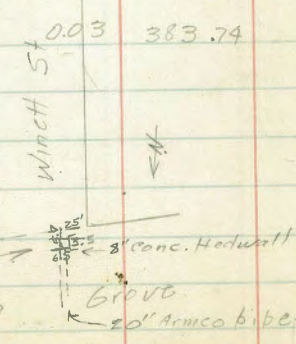
w.L.	1.1	283.6
+2	7.5	275.0
cb	7.0	275.5
1/4	6.6	275.9
+6	6.8	275.7
+8	8.2	274.3
±	6.0	276.5
+1	7.2	275.3
+3	6.0	276.5
1/4	5.7	276.8
cb	5.0	277.5
+2	8.5	274.0
EL	8.7	273.8 ✓
13+42 ^L = S.L. Lemon Grove on West		
EL	9.0	273.5
+8	8.8	273.7
cb	6.6	275.9
1/4	7.0	275.5
±	7.1	275.4
+2	8.8	273.7
+5	7.3	275.2
1/4	7.1	275.4
cb	7.9	275.6
w.L.	8.4	274.1

282.50

282.50

S.L. Lemon Grove	13+42 ⁺ = 13+52 ⁺		
w.L.	8.4	274.1	
cb	8.1	274.4	
1/4	7.4	275.1	
+4	8.2	274.3	
+5	9.6	272.9	
+7	9.2	273.3	
+8	7.6	274.9	
±	7.2	275.3	
1/4	7.5	275.0	
+8	7.6	274.9	
cb	8.6	273.9	
EL	9.1	273.4 ⁺	
Section South Hedge Pav.	west 13+54 ⁺ = East 13+65 ⁺		
EL	8.94	273.56 ⁺	
±	9.28	273.22	
w.L.	9.65	272.85	

FL Pipe on Drain	12.48		
Top Headwall	9.38		
Hub 30' South of S.W. Cor Lemon Grove Blvd & Winett. on top of South Bank			
B.M.	3.34	279.16	
T.P.	12.62	295.03	0.09 282.41
TP	12.01	306.87	0.17 294.86
TP	12.86	319.73	0.00 306.87
T.P.	12.98	332.55	0.16 319.57
T.P.	12.95	345.33	0.17 332.38
T.P.	12.79	358.06	0.06 345.27
TP	13.01	371.04	0.03 358.03
TP	12.74	383.77	0.01 371.03



12.54	396.18		383.74
T.P.	12.00	408.69	0.14 396.09
T.P.	11.84	419.72	0.81 407.88
B.M. Beginning	3.10	416.62	(416.64)

Xsec. Tooley St. from
W.L. Winnett to Republic.

B.M.	12.76	429.40	416.64
0+00 = W.L. Winnett			
N.L.	12.8	416.6	
cb	13.4	416.0	
+2	13.6	415.8	
+3	14.2	415.2	
1/4	14.3	415.1	
±	14.7	414.7	
+7	15.0	414.4	
1/4	15.8	413.6	
cb	17.4	412.0	
S.L.	19.6	409.8	
0+25			
S.L.	17.4	412.0	
cb	16.1	413.3	
1/4	14.0	415.4	
+6	12.7	416.7	
±	13.0	416.4	
1/4	13.0	416.4	
+6	12.8	416.6	
+9	10.6	418.8	
cb	10.6	418.8	
N.L.	9.7	419.7	

Plotted Jan. 25-29. C.B.H.

Bolt by Hub
N.W. Tooley
W. Winnett.

Jan. 17-28
London
Pierce
Morgan.

32

	429.40	
0+50		
N.L.	8.1	421.3
cb	8.9	420.5
+3	9.1	420.3
+5	10.6	418.8
1/4	10.8	418.6
±	10.9	418.5
+5	10.4	419.0
1/4	10.9	418.5
cb	11.2	418.2
S.L.	12.5	416.9
0+75		
S.L.	10.4	419.0
cb	9.2	
1/4	7.9	
+3	7.3	
+6	8.0	
±	8.2	421.2
1/4	7.9	
+5	7.7	
+7	6.0	
cb	5.9	
N.L.	5.3	424.1

1+00	429.40		
N.L.	0.2	429.2	
cb	2.0		
+5	2.3		
+6	3.5		
1/4	4.0		
±	4.4	425.0	
+6	3.9		
1/4	4.2		
cb	5.6		
S.L.	6.7	422.7	
1+25			
SL	0.8	428.6	
cb	0.9		
1/4	0.1		
+5	0.6		
±	0.6	428.8	
1/4	0.4		
+4	0.7		
TP	12.70	442.05	0.05
+7			429.35
cb			11.7
N.L.			11.4
			11.0
		431.1	

1+50	442.05		
N.L.	7.9	434.2	
cb	7.3		
+2	7.2		
+6	8.4		
+7	9.2		
1/4	9.0		
±	8.8	433.2	
+6	8.7		
+8	8.6		
1/4	8.8		
+5	10.1		
cb	10.4		
SL	10.7	431.4	
1+75			
SL	6.8	435.3	
cb	5.9		
+7	5.3		
1/4	4.4		
+5	4.8		
±	4.8	437.3	
1/4	4.8		
+3	5.1		
+4	4.8		
cb	4.3		
N.L.	4.1	438.0	

2+00	442.05		
N.L.		0.1	442.0
cb		0.0	
1/4		0.6	
⊕		0.6	441.5
+6		0.7	
+8		0.3	
1/4		0.4	
cb		0.7	
S.L.		1.1	441.0
TP 12-10	454.14	0.01	442.04
2+25			
S.L.		8.0	446.1
cb		7.8	
1/4		8.4	
+3		8.9	
⊕		8.7	445.4
1/4		9.2	
cb		7.3	
N.L.		7.6	446.5

2+50	454.14		
N.L.		3.5	450.6
cb		3.5	
+5		3.7	
1/4		4.7	
⊕		5.2	448.9
1/4		5.0	
+5		4.9	
+6		4.2	
cb		4.2	
S.L.		4.4	449.7
2+75			
S.L.		1.1	453.0
cb		1.4	
1/4		2.1	
⊕		2.2	451.9
1/4		1.9	
+5		0.8	
cb		0.7	
N.L.		1.6	452.5

454.14

35

3+00		
NL	2.6	451.5
cb	1.8	
1/4	2.3	
±	2.3	451.8
1/4	1.9	
+6	0.9	
cb	0.6	
S.L.	0.5	453.6
3+25		
S.L.	1.4	452.7
cb	1.4	
+4	1.6	
1/4	2.8	
±	3.5	450.6
1/4	3.6	
cb	3.9	
NL	5.0	449.1
3+50		
NL	10.8	443.2
cb	9.1	
+5	8.8	
1/4	7.1	
±	6.6	447.5
1/4	6.0	
+3	4.7	

3+50		
cb	4.3	
S.L.	3.4	450.7
3+75		
S.L.	6.2	447.9
cb	7.3	
+6	8.3	
1/4	9.4	
±	9.7	444.4
1/4	10.2	
cb	13.0	
NL	15.3	438.8
10N	16.8	
T.P.	10.50	453.01
11.63		442.51
4+00		
15N	21.4	
NL	17.5	435.5
cb	15.8	
1/4	12.2	
±	11.0	442.0
1/4	11.0	
cb	9.8	
S.L.	8.5	444.5

Xsec Tooley from E.L. Winnett
to W.L. Oriole.

= EL Republic.

A+35 ⁶	453.01		
S.L.	9.7	443.3	
cb	11.3		
1/4	12.5		
±	12.9	440.1	
1/4	13.1		
cb	17.2		
N.L.	19.9	433.1	
15N	23.1		
bolt in Base Flagpole N Side Tooley 300' W of Republic.			
B.M.	1.06	451.95 (451.95)	

B.M.	12.72	429.36	416.64
E.L. Tooley = 0+00 on South = 0+02 ¹ on North.			
N.L.		10.9	418.5
cb		11.3	418.1
+1		12.4	417.0
1/4		13.3	416.1
±		13.7	415.7
1/4		14.7	414.7
cb		15.3	414.1
S.L.		16.7	412.7
0+25			
S.L.		12.6	416.8
cb		11.5	417.9
1/4		10.5	418.9
+8		10.7	418.7
±		11.3	418.1
1/4		10.8	418.6
+7		10.7	418.7
±b		9.4	420.0
N.L.		9.2	420.2

Plotted Jan 25-29-29. C.B.H.

429.36

0+50

N.L.	7.0	422.4
cb	6.7	422.7
+3	6.9	422.5
+4	8.0	421.4
1/4	8.1	421.3
±	8.2	421.2
+6	7.6	421.8
1/4	7.4	422.0
cb	8.3	421.1
S.L.	8.6	420.8

0+75

S.L.	4.3	425.1
cb	4.0	
1/4	4.0	
±	4.1	425.3
1/4	4.2	
+5	4.2	
+6	3.5	
cb	3.5	
N.L.	3.4	426.0

1+00

429.36

N.L.		0.6	428.8
cb		0.2	
+3		0.3	
+4		1.7	
1/4		1.6	
±		1.6	427.8
+4		1.6	
+5		1.0	
1/4		1.2	
+2		1.8	
+4		0.8	
cb		0.9	
S.L.		1.2	428.2
T.P.	12.62	442.01	0.03 429.33
1+25			
S.L.		10.6	431.4
cb		10.5	
1/4		10.4	
+5		10.6	
+6		11.1	
±		11.3	430.7
1/4		11.3	
+5		11.4	
+6		10.8	
cb		10.6	
N.L.		11.2	430.8

37

1+50	442.01		
N.L.		8.7	433.3
cb		7.7	
+5		8.0	
+6		8.6	
1/4		8.5	
±		8.1	433.9
+5		7.8	
+6		7.5	
1/4		7.3	
cb		7.3	
S.L.		7.1	434.9
1+75			
SL		3.6	438.5
cb		3.6	
1/4		3.2	
+3		4.0	
+4		4.7	
±		5.1	436.9
1/4		5.5	
+3		5.5	
+4		5.3	
cb		5.3	
N.L.		6.3	435.7

2+00	442.01		
N.L.		3.1	435.9
cb		2.3	
1/4		2.5	
±		2.5	439.5
+8		2.3	
1/4		1.6	
+6		1.3	
cb		0.3	
S.L.		0.2	441.8
T.P. 6.19	448.05	0.15	441.86
2+25			
SL		4.5	443.5
cb		5.5	
1/4		6.3	
±		6.6	441.4
1/4		6.7	
cb		7.2	
N.L.		7.9	440.1

448.05

2+50		
N.L.	8.1	439.9
cb	7.1	
1/4	6.5	
+6	5.9	
+7	5.4	
⊕	5.4	442.6
1/4	5.3	
+7	5.3	
cb	2.7	
SL	2.1	445.9
2+75		
SL	2.7	445.4
cb	3.8	
+3	5.6	
1/4	5.8	
⊕	5.8	442.3
+2	6.9	
1/4	7.8	
cb	8.8	
N.L.	10.0	438.1
10N	10.8	

448.05

39

3+00		
10N	13.8	
N.L.	12.6	435.5
cb	11.1	
1/4	9.5	
⊕	8.1	440.0
+4	7.0	
1/4	7.2	
+9	6.9	
cb	5.9	
+2	5.0	
SL	3.4	444.7
3+25		
SL	5.3	442.8
+5	6.5	
cb	8.1	
1/4	8.3	
+5	8.2	
⊕	9.4	438.7
+5	10.5	
1/4	11.0	
cb	12.8	
N.L.	14.7	433.4
15N	17.0	

448.05

3 + 50

15N	20.2	
NL	17.1	431.0
cb	14.5	
1/4	12.4	
+8	11.2	
±	10.3	437.8
+5	8.7	
1/4	8.9	
+7	8.8	
+8	8.0	
cb	8.1	
+4	7.7	
S.L.	5.1	443.0
3 + 75		
S.L.	6.4	441.7
cb	6.4	
1/4	8.5	
+3	8.4	
±	11.6	436.5
+5	12.1	
1/4	14.7	
cb	16.8	
NL	17.8	430.3
15N	21.6	

448.95

40

4 + 00		
15N	20.4	
NL	17.1	431.0
cb	15.0	
1/4	13.6	
+8	12.7	
±	11.8	436.3
+8	7.6	
1/4	7.7	
cb	7.6	
+5	6.7	
S.L.	5.6	442.5
W.L. Oriole	4 + 36° on South = 4 + 38° on North	
S.L.	2.4	445.7
+3	3.7	
cb	4.7	
1/4	5.5	
+2	5.2	
±	7.4	440.7
+4	8.7	
1/4	9.6	
cb	11.3	
NL	13.3	434.8
15N	16.4	

44805

3 corner of guard stake s.w. Tooley & Oriole.

B.M.			1.99	446.06
T.P.	0.03	435.06	13.02	435.03
T.P.	0.81	423.02	12.85	422.21
B.M.	Beginning		6.39	416.63 (416.64)

1300.9
Moore
Cross Section of Myrtle St
Boundary to Nile

60' wide
10' curbs
10' 1/4"

42

NW 30' (956 32191' 312.95' upon
FELTON

00 = EL Boundary = 42.6 on section

S gutter on paving	6.87	315.04
1/4 " "	6.44	314.47
C " "	6.21	315.70
1/4 " "	6.09	314.82
N gutter " "	6.00	315.91

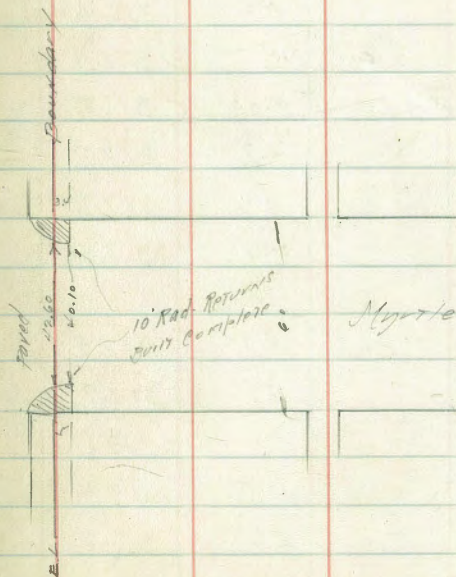
00 + 32' on North + 0 + 5' on South = end curb returns

NL Top curb return (con)	5.17	316.2
cb " " "	5.29	316.62
g.T.	5.7	316.2
1/4	5.9	316.0
C	6.1	315.8
1/4	6.2	315.7
g.T.	6.7	315.2
cb Top curb return (con)	6.36	315.55
SL " Cor. " "	6.29	315.62

Plotted
H.C.H. 4/30/29

0 + 50

S	5.7	316.2
cb	5.6	316.3
1/4	5.4	316.5
C	5.3	316.6
1/4	4.8	317.1
cb	4.8	317.1
N	4.7	317.2



Reverse of
complete at
Nile + Myrtle

321.91

1700

N	4.8	317.1
cb	4.8	317.1
1/4	4.7	317.1
C	5.0	316.9
1/4	5.1	316.8
cb	4.7	317.2
S	5.2	316.7

1746

S	5.4	316.5
cb	5.3	316.6
1/4	5.0	316.9
C	5.03	316.9
1/4	4.7	317.2
cb	4.6	317.3
N	4.4	317.5

2100

N	4.0	317.9
cb	4.0	317.9
1/4	4.3	317.6
C	4.5	317.4
1/4	4.7	317.2
cb	4.9	317.0
S	4.8	317.1

2150

S	3.6	318.3
cb	3.6	318.3

321.91

My 7/10 ST

43

1/4	3.4	318.5
C	3.4	318.5
1/4	3.3	318.6
cb	3.1	318.8
N	3.0	318.9

2+68

N	2.9	319.0
cb	3.0	318.9
+3	3.4	318.5
1/4	3.4	318.5
C	3.2	318.7
1/4	3.4	318.5
cb	3.4	318.5
S	3.6	318.3

2+91

S	3.6	318.3
cb	3.7	318.2
1/4	3.9	318.0
C	3.7	318.2
+5	5.2	316.7
1/4	5.7	316.2
cb	5.4	316.5
N	4.8	317.1

2+96 - W Nile = 80' wide 14' cuabs 13 1/4"

N	5.9	316.0
cb	6.8	315.63

top com return

321.91

gut	6.4	315.5
TV	6.4	315.7
1/4	6.4	315.5
TV	6.5	315.6
C	6.1	315.8
1/4	6.1	315.8
gut	6.5	315.4
cb Top cem return	6.81	315.10
S	6.4	315.5
W curb on Mile		
S Top cem curb	6.88	315.03
gut	7.6	314.3
cb	7.6	314.3
1/4	7.5	314.4
C	7.4	314.5
1/4	7.1	314.8
cb	7.1	314.6
N gut	7.1	314.8
N Top cem	6.30	315.61
W 1/4		
N	6.9	315.0
cb	6.9	315.0
1/4	7.0	314.9
C	7.0	314.9
1/4	7.2	314.7
cb	7.3	314.6
S	7.3	314.6

321.91

		1/4 Mile		
S	7.4	314.5		
cb	7.2	314.7		
1/4	7.1	314.8		
0	7.0	314.9		
1/4	6.9	315.0		
cb	6.9	315.0		
N	6.8	315.1		
E 1/4				
N	7.1	314.8		
cb	7.1	314.8		
1/4	7.2	314.7		
C	7.2	314.7		
1/4	7.3	314.6		
cb	7.5	314.4		
S	7.6	314.3		
E curb				
S Top cem	7.34	314.57		
gut	8.1	313.8		
cb	8.1	313.8		
1/4	8.0	313.9		
C	7.7	314.2		
1/4	7.6	314.3		
cb	7.5	314.4		
gut	7.7	314.2		
N Top cem curb	6.82	315.09		

Myrtle

44

321.91

Myrtle St 45

El Nile St

NL			6.6	315.3
Neb Top cont return			6.83	315.08
gut			7.2	314.7
1/4			7.0	314.9
c			7.0	314.9
1/4			7.4	314.5
gut			7.5	314.4
Scrub Top cont return			7.36	314.55
S			7.1	314.8
ON SEBP	Myrtle Nile		7.35	314.56
T.P.	5.68	322.27	5.32	316.59
T.P.	10.14	324.32	8.07	314.20
TO NEBP	Myrtle 330	322.06	2.28	322.04
				0.02 error

X See Alley Bk 36 Parish & Loomis 2-13-29 mill.

Bet E + F Sts + 26th + 27th Sts

Office Record
N.W. 26th + E. Sts.

OOT

1962

188.01

188.01 + E. Sts.

B.M. B.P. 1.05 189.06

T.P. 2.78 176.80 13.04 176.02

N + S. Alley 7' First Alley E. of 26th St.

00 = S. Line E. St.

W. 9.35 167.45 emt. ck

W 9.81 166.99 parmt

E 11.00 165.80 "

E 12.14 167.66 " + curb

20's

E - 0.10 9.72 167.08 Top emt wall

E 10.4 166.4

C 10.2 166.6

N 9.7 167.1

60's

W 9.1 167.7

E 9.3 167.5

+ 9.6 W. edge emt. wall 9.4

E on top wall 9.10 166.70

67.85 = S. end emt. wall

80's

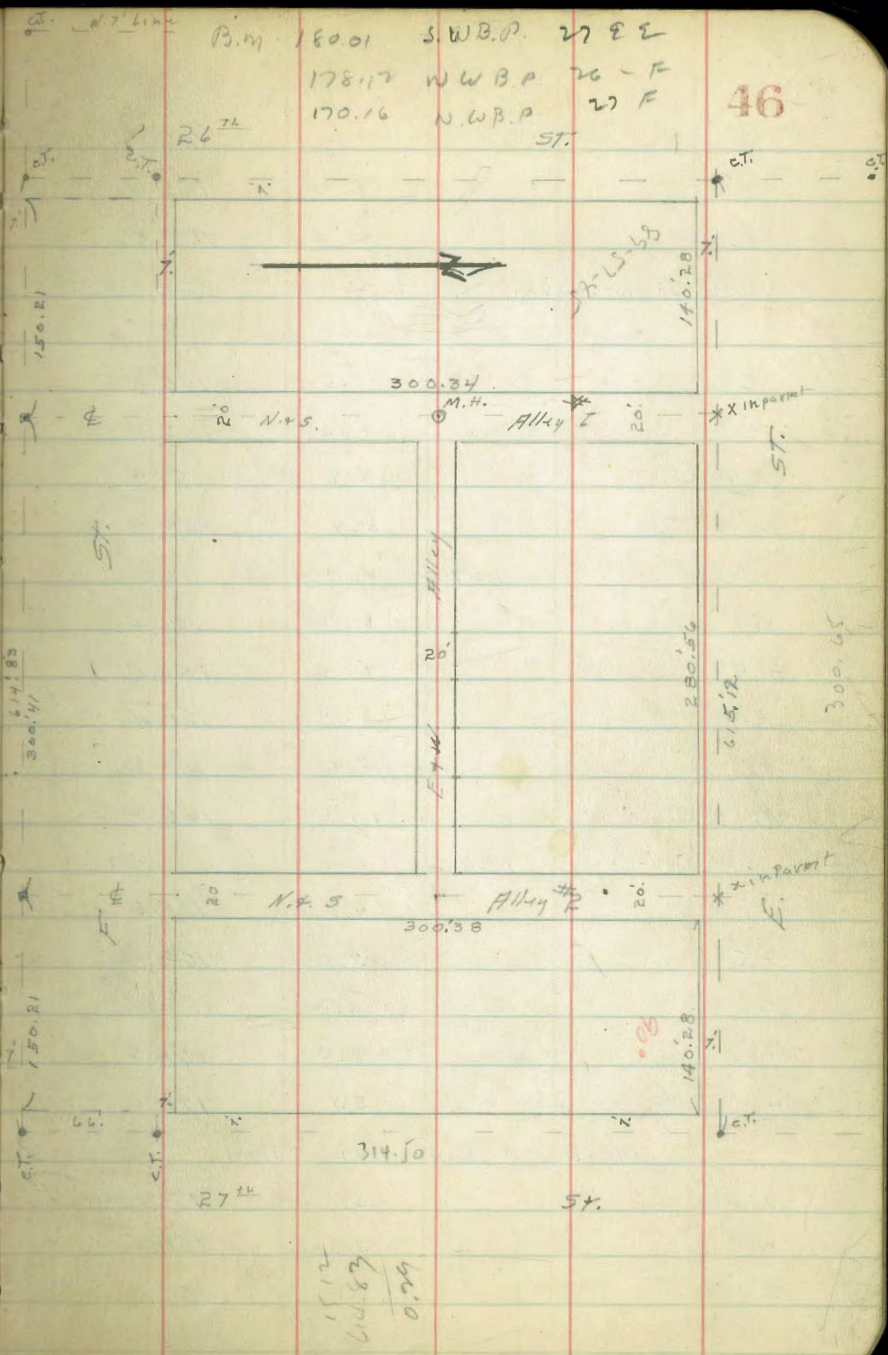
E - 0.10 = emt wall 9.94 166.86

E 10.2 166.6

C 9.5 167.3

W 9.1 167.7

Plotted 8-19-29-CBH



176.80

100.5

W	9.2	167.6
E	9.9	166.9
E	10.2	166.6
+ 0.10 Top cnt. porch.	8.40	168.20 ✓

115.5

E	10.5	166.3
C	9.2	167.6
+ 6	8.9	167.9
W	6.9	169.9

127.5

W	6.2	170.6
+ 4	8.2	168.6
C	8.4	168.4
+ 8	8.6	168.2
E	10.6	166.2

130.5

E	9.3	167.5
+ 5	8.0	168.8
C	8.2	168.6
+ 6	8.0	168.8
W	5.9	170.9

140.5 = N. Line E+W Alley

W	5.7	171.1
C	7.3	169.5
E	9.1	167.7

176.80

150.5 = E+W Alley

E	9.2	167.6
+ 6	6.7	170.1
C on Top M.H	6.4	170.4
W	5.3	171.5

140.5 = S. Line E+W Alley

W	5.0	171.8
C	6.3	170.5
+ 9	6.5	170.3
E	9.0	167.8

162.5 = N. End garage on E. Line Wood floor

E	6.2	170.5 floor ✓
C	6.3	170.5
W	5.0	171.8

175.5 = garage on E. Line Wood floor 0.7 Back

W	4.7	172.1
C	5.9	170.9
E	6.3	170.5 floor

179.5 = S. Line Garage

E-15	11.7	165.1
E-1	9.7	167.1
E	6.7	170.4
C		
W		

182.5. Tree stump 2' Diam. w. edge 7' E. of E

176.80
189.5

Alley BIK 36 Parish + Loomis

176.80
260.5

48

E-15	11.0	
E-0.5	8.3	
E	6.0	170.8
C	5.3	171.5
W	4.2	172.6

E-0.4 = House.

E

4.8 172.0

C

3.6 173.2

+6

3.1 173.7

W

0.1 176.7

276.5

198.5 S. Pepper Tree 2' Diam W. edge 87 E. of Alley

215.5

W

0.0 176.8

+4

3.0 173.8

W

2.1 174.7

C

3.3 173.5

+W

4.0 172.8

+7.5

3.9 172.9

C

4.7 172.1

E

4.7 172.1

+8

5.4 171.4

E+0.6 Wall House

+9

7.4 169.4

277.5

E

7.5 169.3

E-5

5.4 171.4

+10

10.0 166.8

E

5.4 171.4

234.5

+2

5.3 171.5

E-5

6.6 170.2 on wood porch

+3

3.8 173.0

E

6.5 170.9 on wood porch

C

3.3 173.5

+2

5.1 171.7

+6

3.0 173.8

C

4.0 172.8

W

0.0 176.8

+6

3.7 173.1

300.5 = N. line of ST.

W

2.2 174.6

W

+0.5 177.3

235.5

+5

1.7 175.1

W

2.1 174.7

C

2.5 174.3

+4

3.6 173.2

+7

3.2 173.6

C

3.9 172.9

+8

4.9 171.9

E

5.0 171.8

E

5.0 171.8

E+0.3 = N. edge House

176.80

Alley BK 36 Parish & Loomis

49

E & W. Alley

00 = E. Line N + S. Alley E. of 26th St.

152.04
105' E Garage on dirt floor 3' Back
" " " N. ent. floor 4.5 "

N		9.1	167.7
E		9.2	167.6
S		9.0	167.8
T.P.	0.26	164.84	12.22
	15' E		167.58
S	Plotted 2/19/49 CDH	1.4	163.2
E		2.2	162.6
N		1.3	163.5
		35' E.	
N		7.0	157.8
E		6.6	158.2
S		6.3	158.5
	from 48' E to 56' E shadow N. 1.0 in Alley		
	65' E		
S		10.6	154.2
E		10.7	154.1
N		10.4	154.4
T.P.	0.14	152.04	12.98
	75' E Garage on N. 4.5 Back ent. floor		151.86
N-4.5		0.65	151.39 floor ✓
N-1.5		0.85	151.19 ent. Apron
N		0.9	151.1
E		0.9	151.1
S		0.5	151.5

S		1.7	150.2 floor
E		1.7	150.3
N		2.1	149.9
	+ 2.0	2.15	149.89 ent. apron
	+ 4.5	2.19	149.85 " floor.
	110' E = W. edge double garage ent. floor 4.5 Back		
N-4.5		2.65	149.39 ent. floor.
N-2		2.72	149.22 " Apron
N		2.6	149.4
E		2.3	149.7
S		2.6	149.4
	128' E = E. edge above double garage ✓		
S		4.5	147.5
E		4.6	147.4
	+ 4	4.6	147.4
N		2.9	149.1
	+ 2	2.83	149.21 ent. apron ✓
	+ 4.5	2.72	149.32 " floor ✓
	130' E		
N.		5.5	146.5
E.		4.8	147.2
S.		4.7	147.3
	145' E.		
S		7.0	145.0
E		7.8	144.2
N		8.0	144.0

	152.04		
T.P.	6.70	146.46	12.28 139.76
		170.8	
N.		8.0	138.5
C		7.9	138.6
S		7.4	139.1
		195.8	
S		12.0	134.5
C		11.9	134.6
N		11.8	134.7
		210.8	
-10		13.0	133.5
N		13.3	133.2
C		13.3	133.2
S		13.4	133.1
+10		14.2	132.3
		230.8	
-10		15.0 (7.5) inditch	
-1		14.5 (17.2) " "	
S		13.5	133.0
C		12.3	134.2
N		13.5	133.0
+10		13.1	133.4
		250.8	
-10		12.7	133.8
N		13.0	133.5
C		12.9	133.6

	146.46	
S.	12.3	134.2
+10	12.5	
280' E. = W. Line N+S. Alley # R W. of R7 th		
S	8.0	138.5
C	7.8	138.7
N	6.5	140.0
N+S. Alley # R W. of R7 th St		
oo = N. Line F. St.		
W	10.3	136.2
C	10.2	136.3
+2	10.2	136.3
E	5.5	141.0
from oo to 43.5' N House only		
25' N		
E	5.0	141.5
+2	8.0	138.5
+6	8.9	137.6
C	9.2	137.3
W	9.2	137.3
50' N		
W	9.8	136.7
C	9.2	137.3
+9	7.5	139.0
E	6.3	140.2

Plotted 2-12-29 - CBH

1. A at .00
0.4 " 43.5' N

146.46
80' N.

E	5.3	141.2
+1	7.9	138.6
E	9.0	137.5
W	9.8	136.7

105' N

N	9.3	137.2
E	8.5	138.0
E	6.4	140.1

140' N = S line E & W Alley

E	4.2	142.3
+4	6.2	140.3
E	6.7	139.8
W	8.0	138.5

150' N = E & W Alley

W	7.8	138.7
E	6.1	140.4
+6	5.6	140.9
E	3.8	142.7

160' N = N line E & W Alley

E	3.2	143.3
+3	4.5	142.0
E	5.0	141.5
W	6.5	140.0

146.46

185' N

N	5.5	141.0
e	3.0	143.5
+8	2.9	143.6
E	1.7	144.8
T.P.	12.95	138.53
		0.88
		145.58

210' N.

E	11.4	147.1
+1	12.6	145.9
E	12.6	145.9
W	16.1	142.4
+10	18.4	140.1

258' N

-10	14.4	144.1
W	12.4	146.1
e	10.3	148.2
+9	9.8	148.7
E	8.6	149.9

263' N

E	8.3	150.2
+1	9.5	149.0
e	9.8	148.7
+6	11.0	147.5
W	14.2	144.3
+10	14.6	143.9

Alley B1K3L Parish + 600' N

51

158.53
285' N.

W-10	13.1	
W	12.3	146.2
+7	6.9	151.6
E	6.8	151.7
+8	6.2	152.3
E	7.1	151.4
+10	5.5	153.0

295' N.

-10	4.7	153.8
E	5.9	152.6
+3	4.5	154.0
E	5.5	153.0
+6	6.5	152.0
W	8.5	150.0
+10	11.9	146.5

300' N. = S. Line E. SF.

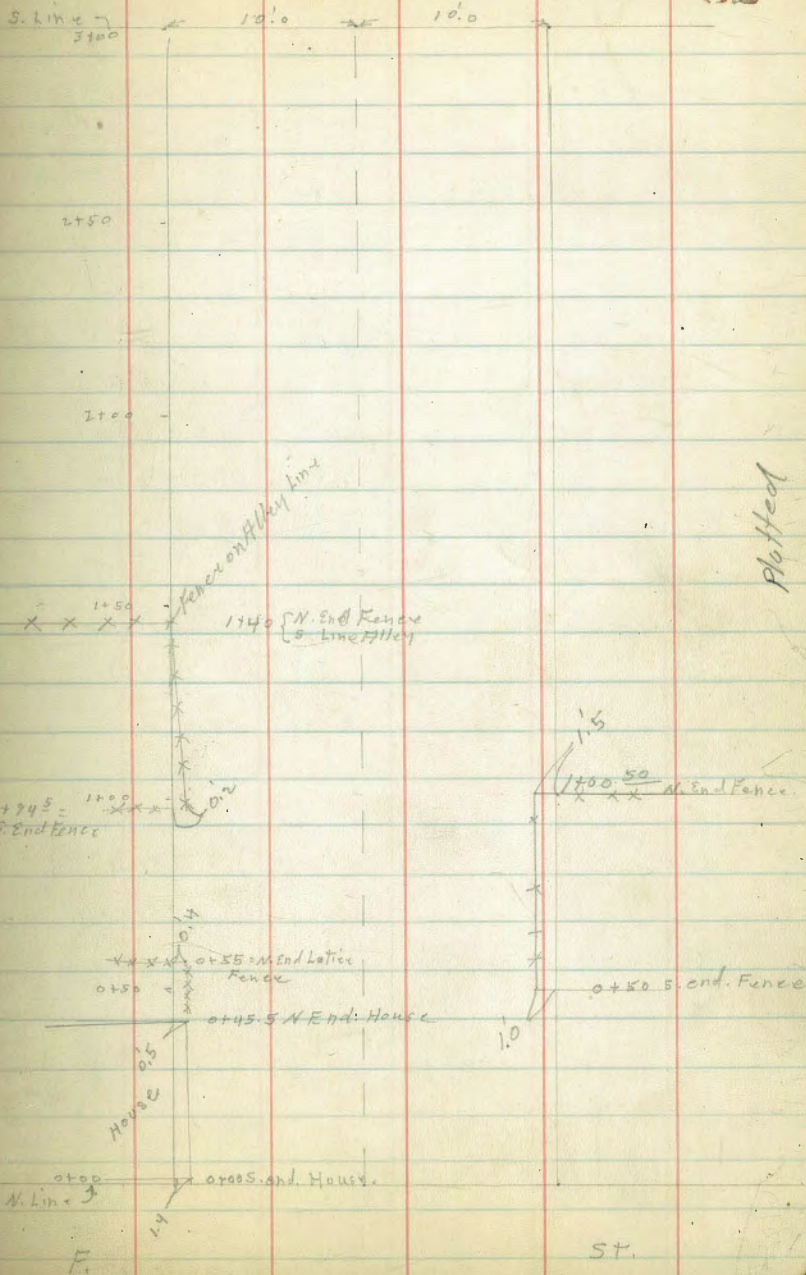
W	6.24	151.29	ch + Pavmt.
E	4.71	153.82	pavmt
E	3.17	155.36	"
E	2.56	155.97	ent. ch
T.P.	12.45	170.95	0.03
T.P.	11.39	182.17	0.17

chk on B.M. S.W. 27th 42 2.02 180.15 = 180.02

chk on first T.P. Page 46 6.15 176.02 = 176.02

B.M. do not ch K.

9/25/32 Survey of Improvements Alley Bk 36 Parrish + Lewis
Miller, Walker, Henderson
E ST. 52



B.M.	0.92	416.97		416.05	
	0.54	404.51	13.00	403.97	
	0.18	391.69	13.00	391.51	
	0.06	378.88	12.87	378.82	
	0.25	366.20	12.93	365.95	
	0.02	353.47	12.80	353.40	
	0.30	340.72	13.00	340.42	
B.M.			10.74	329.98	
T.P.	0.07	328.22	12.57	328.15	
	0.22	315.69	12.75	315.47	
	2.73	306.27	12.15	303.54	
B.M.			6.22	300.05	300.64
top IXI by Hrb			5.71	300.56	

3-7-29 X-section - Milbrae Street - Ocean View
 J.C. Bliss Blvd. to Harding Street - Improved with curb
 Drebert + Sidewalks from Harding to Franklin - 50' wide
 Rayner 10' cbs
 7 1/2' 45

H.L. 78.45

54

B.M. N.W. B.P. 38 th +5	89.90	W
+1.67 91.57	-13.12 78.45	47
+0.00	H.L. 78.45	cb
M.L. Ocean View = 0400 - Pared		44
W	8.5 70.0	4
W-Top	8.20 70.25	14
G	8.81 69.64	+3
14	8.71 70.04	cb
4	8.04 70.41	+1
14	7.94 70.51	E
G	8.00 70.45	
E-Top	7.24 71.21	E
+5	6.5 71.95	+8
E	5.3 73.2	cb
	0402	+3
E	4.5 74.0	44
cb	5.4 73.1	4
+1	7.1 71.4	46
+5	8.2 70.3	cb
44	8.2 70.3	+4
4	8.2 70.3	W
44	8.5 70.0	
cb	8.6 69.9	
+3	8.2 70.3	
W	8.5 70.0	cb

0425

74	69.1
92	69.3
9.8	68.7
10.0	68.5
9.8	68.7
9.7	68.8
9.6	68.9
7.5	71.0
5.4	73.1
4.6	73.9

0450

5.9	72.6
7.3	71.2
9.3	69.2
11.2	67.3
11.1	67.4
11.0	67.5
11.1	67.4
11.2	67.3
10.2	68.3
10.5	68.0

0475

11.8	66.7
12.5	66.0
12.3	66.2

Plotted 3-22-29 - E Britain

H.I. 78.45

1/4	12.3	66.2
¢	12.2	66.3
1/4	12.3	66.2
cb	11.7	66.8
+3	9.3	69.2
E	8.0	70.5

1400

E	11.0	67.5
cb	13.2	65.3
1/4	13.5	65.0
¢	13.4	65.1
1/4	13.5	65.0
cb	13.5	65.0
W	13.1	65.4

T.P. - Pres Hub West Side Sta 1400

+1.49

-13.10 65.35

H.I. 66.84

1425

w	9.1	63.7
cb	3.1	63.7
1/4	3.0	63.8
¢	2.8	64.0
1/4	2.7	64.1
cb	2.2	64.6

H.I. 66.84

55

E	0.3	66.5
---	-----	------

1450

E	0.8	66.0
+8	1.6	65.2
cb	2.6	64.2
1/4	3.5	63.3
¢	3.4	63.4
1/4	3.6	63.2
cb	3.7	63.1
W	3.7	63.1

1475

W	4.2	62.6
cb	4.1	62.7
1/4	4.0	62.8
¢	4.0	62.8
1/4	4.4	62.4
cb	3.5	63.3
E	1.8	65.0

2400

E	3.3	63.5
cb	4.6	62.2
1/4	5.2	61.6
¢	4.9	61.9
1/4	5.1	61.7
cb	5.1	61.7
1/4	4.7	62.1

H.I. 66.84

W	46	62.2
	2+25	
W	54	61.4
cb	61	60.7
1/4	60	60.8
¢	60	60.8
1/4	55	61.3
cb	49	61.9
E - Concrete Drive at E.L.	436	62.38
	2+50	
E	47	62.1
+5	54	61.4
cb	60	60.8
1/4	62	60.6
¢	64	60.4
1/4	64	60.4
cb	65	60.3
W	63	60.5
	2+75	
W	71	59.7
cb	68	60.0
1/4	68	60.0
¢	67	60.1
1/4	66	60.2
cb	64	60.4

H.I. 66.84

56

E	5.5	61.3
	3+09 ⁶⁸ = S.L. Franklin ^{30' wide} 5' cbs	
E	5.9	60.9
cb	6.3	60.5
1/4	6.8	60.8
¢	7.0	59.8
1/4	7.5	59.3
+4	8.1	58.7
cb	8.0	58.8
+3	7.4	59.4
W	7.5	59.3
	5' cb Franklin	
W	7.8	59.0
+7	8.2	58.6
cb	8.6	58.2
+3	8.0	58.8
1/4	7.5	59.3
¢	7.1	59.7
1/4	6.8	60.0
cb	6.4	60.4
E	6.0	60.8
	¢ Franklin	
E	7.2	59.6
cb	7.1	59.7 ^{59.5}
1/4	7.3	64.5

H.I. 66.84

♀	77	59.1
1/4	82	58.6
cb	86	58.2
W	91	57.7

N cb Franklin

W	89	57.9
cb	86	58.2
1/4	80	58.8
♀	76	59.2
1/4	75	59.3
cb	74	59.4
E	68	60.0

Note on N 1/4 of Franklin & 3' West of E.L. Milbrae
there is an Inlet Grating 10.00 18" Concrete Culvert.

Shot on Grating 7.94 59.10

" " Flowline Culvert 10.07 56.77

N.W. Franklin corner start of cur & walk

E	61	60.7
Topcb	680	60.04
G	71	59.7
1/4	74	59.4
♀	75	59.3
1/4	80	58.8
G	83	58.5

H.I. 66.84

57

Topcb	782	59.02
W	78	59.0
T.P. - N.W. Top Pillar Franklin & Milbrae	-5.66	61.18
	0+25	

W Topcb 685 59.99

G 75 59.3

1/4 70 59.8

♀ 66 60.2

1/4 66 60.2

G 67 60.1

E Topcb 591 60.93

0+50

E Topcb 504 61.80

G 57 61.1

1/4 57 61.1

♀ 57 61.1

1/4 62 60.6

G 64 60.4

W Topcb 583 61.01

0+75

W 487 61.97

G 57 61.1

1/4 52 61.6

♀ 47 62.1

1/4 49 61.9

H.I. 66.84

G	4.2	61.9
E Tpcb	4.12	62.72
	1400	
E Tpcb	3.20	63.64
G	4.0	62.8
1/4	3.9	62.9
£	3.8	63.0
1/4	4.3	62.5
G	4.8	62.0
W Tpcb	3.75	63.09
	1425	
W Tpcb	2.95	63.79
G	2.8	63.0
1/4	3.2	63.6
£	2.8	64.0
1/4	2.9	63.9
G	3.1	63.7
E Tpcb	2.21	64.63
	1450	
E Tpcb	1.82	65.52
G	2.2	64.6
1/4	1.8	65.0
£	1.8	65.0
1/4	2.2	64.6
G	2.4	64.4

H.I. 66.84

58

W Tpcb	1.90	64.9
	1475	
W Tpcb	1.10	65.74
G	1.3	65.5
1/4	1.1	65.7
£	0.8	66.0
1/4	0.9	65.9
G	1.2	65.6
E Tpcb	0.42	66.42
T.P		-0.00 66.84
	+ 11.23	
	H.I. 78.07	
	1490	
E Tpcb	11.12	66.95
G	11.8	66.3
1/4	11.4	66.7
£	11.4	66.7
1/4	11.7	66.4
G	12.1	66.0
W Tpcb	11.62	66.55
	2400	
W Tpcb	11.00	67.07
G	11.5	66.6
1/4	11.1	67.0
£	10.8	67.3

H.J. 78.07

1/4	11.0	67.1
G	11.0	67.0
E Tpcb	10.52	67.55
2+25		
E Tpcb	9.02	69.05
G	9.6	68.5
1/4	9.8	67.6
£	9.4	68.7
1/4	9.7	68.4
G	10.0	68.1
W Tpcb	9.32	68.75
2+50		
W Tpcb	7.2	70.45
G	8.7	69.4
1/4	8.1	70.0
£	7.8	70.3
1/4	8.0	70.1
G	8.0	70.1
E Tpcb	7.55	70.52
2+75		
E Tpcb	6.10	71.97
G	6.2	71.9
1/4	6.3	71.8
£	6.2	71.9
1/4	6.7	71.4

H.I. 78.07

59

G	7.0	71.1
W Tpcb	5.93	72.14
3+00		
W Tpcb	4.32	73.75
G	5.4	72.7
1/4	4.9	73.2
£	4.4	73.7
1/4	4.8	73.3
G	4.8	73.3
E Tpcb	4.57	73.50
3+25		
E Tpcb	3.01	75.06
G	3.6	74.5
1/4	3.3	74.8
£	3.0	75.1
1/4	3.3	74.8
G	3.5	74.6
W Tpcb	2.66	75.41
3+50		
W Tpcb	0.95	77.12
G	2.0	76.1
1/4	1.7	76.4
£	1.4	76.7
1/4	1.8	76.3
G	2.4	75.7

H.I. 78.07

E Tpcb	158	76.49
	3+75	
E Tpcb	0.03	78.04
G	0.5	77.6
1/4	0.3	77.8
T.P		-0.60 77.47
	+6.97	
	H.I. 84.44	
¢	6.3	78.1
1/4	6.4	78.0
G	6.8	77.6
w Tpcb	5.74	78.70
	4+00	
w Tpcb	4.17	80.27
G	5.0	79.4
1/4	5.1	79.3
¢	5.0	79.4
1/4	5.3	79.1
G	5.3	79.1
E Tpcb	4.83	79.61
	4+75	
E Tpcb	3.34	80.90
G	4.0	80.4
1/4	3.4	81.0

H.I. 84.44

60

¢	3.1	81.3
1/4	3.2	81.2
G	3.5	80.9
w Tpcb	2.50	81.94
	4+40 ⁶⁵ = S.L. Harding	
w Tpcb	1.47	82.97
G	2.4	82.0
1/4	2.3	82.1
¢	2.2	82.2
1/4	2.5	81.9
G	3.0	81.4
E Tpcb	2.5	81.99
T.P.		-13.11 71.33
	+1.10	72.43

T.P. N.W. Top Pillar Franklin v. Milbrs -11.24 61.19
 Correct 61.18

~~B.M. N.W. Top Pillar Milbrs of Franklin
 +11.77 72.90
 6L. Milbrge = 100 - Toward 38th
 in Basement of Stucco House
 1455 ¢ 10' Garage 1' Back N.L. Dirt Floor 2.3
 1473 ¢ Bottom Step Concrete on Stucco House 0.57
 5' Back N.L.
 196- ¢ 10' Garage 1' Back S.L. Dirt Floor 1.0~~

3-7-29
J.C. Bliss
Drebert
Rover

X-section Franklin St. 38th to 37th
St. 30' wide 5' cbs 20' Roadway.

H.I. 73.25

61

B.M. N.W. Top Pillar Franklin + Milbrae

61.18

cb

8.3

65.0

+12.07

N

7.9

65.4

H.I. 73.25

1400

EL. Milbrae = 0400

N

5.9

67.4

N

12.5

60.8

cb

6.5

66.8

cb

13.3

60.0

φ

7.5

65.8

φ

13.4

59.9

cb

7.7

65.6

cb

12.5

60.8

S

7.7

65.6

S

12.3

61.0

1425

0425

S

5.1

68.2

S

11.5

61.8

cb

5.2

68.1

cb

11.7

61.6

φ

5.1

68.2

φ

12.2

61.1

cb

4.3

69.0

cb

11.6

61.7

N

4.0

69.3

N

11.1

61.2

1450

0450

N

2.5

70.8

N

9.5

63.8

cb

2.9

70.4

cb

9.7

63.6

φ

3.0

70.3

φ

10.5

62.8

cb

3.1

70.2

cb

10.4

62.9

S

3.3

70.3

S

10.2

63.1

1475

0475

S

1.6

71.7

S

8.8

64.5

cb

1.7

71.6

cb

9.1

64.2

φ

1.7

71.6

φ

9.1

64.2

cb

1.6

71.7

Plotted 3/30-29- CBH

H.I. 73.25

N	1.0	72.3
T.P.		
T.P.	-1.49	71.76

+ 6.56

H.I. 78.32

2+00

N	2.4	75.9
Tr	5.0	73.3
cb	5.4	72.9
£	5.5	72.8
cb	5.5	72.8
S	5.4	72.9

2+25

S	4.8	73.5
cb	4.7	73.6
£	4.6	73.7
cb	4.7	73.6
43	4.8	74.0
N	2.0	76.3

2+50

N	3.2	75.1
cb	3.8	74.5
£	3.8	74.5
cb	3.7	74.6
S	3.0	74.7

H.I. 78.32

62

2+75 = W.L. 38th St

Regular Alley

Note - There are returns at 38th & Franklin -
One at the N.W. Franklin & one 20' South.

S	2.6	75.7
cb	2.5	75.8
+5 - Tr existing return	2.42	75.90
Gutter	3.0	74.3
£	2.9	75.4
cb	2.7	75.6
Gutter	2.6	75.7
Tr existing return at N.W. Franklin	2.10	76.22

T.P.

-129.4 65.38

+0.06

H.I. 65.44

W.L. Milbrae = 2000

N	6.4	59.0
cb	7.6	57.8
£	7.7	57.7
cb	6.4	59.0
S	6.3	59.1

0+25

S	7.4	58.0
cb	7.6	57.8
£	8.2	57.2
cb	8.1	57.3
N	8.0	57.4

H.1.65.44

0450

N	8.4	57.0
cb	8.4	57.0
£	8.4	57.0
cb	8.0	57.4
S	8.5	56.9

0475

S	8.3	57.1
cb	8.5	56.9
£	8.6	56.8
cb	8.6	56.8
N	8.2	57.2

1400

N	8.7	56.7
cb	8.8	56.6
£	8.8	56.6
cb	8.6	56.8
S	8.9	56.5

1425

S	8.9	56.5
cb	8.8	56.6
£	9.0	56.4
cb	8.9	56.5
N	9.0	56.4

1450

N	8.0	57.4
---	-----	------

H.1.65.44

63

cb	8.8	56.6
£	9.1	56.3
cb	9.0	56.4
S	9.4	56.0

1475

S	9.3	56.1
cb	9.2	56.2
£	9.2	56.2
cb	8.7	56.7
N	7.1	58.3

2400

N	6.4	59.0
cb	9.2	56.2
£	9.3	56.1
cb	9.1	56.3
S	9.2	56.2

2425

S	9.3	56.1
cb	9.5	55.9
£	9.7	55.7
cb	9.6	55.8
tv	9.3	56.1
N	6.1	59.3

2450

N	9.9	55.5
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H.I. 65.44

cb	10.1	55.3
¢	10.4	55.0
cb	10.4	55.0
S	10.3	55.1
R + 75 = E.L. 37 th		
There are regular Alley returns at 37 th + Franklin. One at the N.L. Franklin + one 20' South		
S	10.4	55.0
cb	10.4	55.0
+5 - Top existing return	10.15	55.29
Gutter	10.6	54.8
¢	10.3	55.1
cb	10.4	55.0
Gutter	10.2	55.2
N - Top existing return at N.L. Franklin	9.94	55.50
T.P. - Prop. Hub Sta. 1400 N.L. Milbrae		
	+11.87	77.20
T.P.		-0.41
	+894	85.73
T.P.		-3.96
	+1019	91.96
B.M. S.E. B.P. 37 th + J		-9.11
		82.85
	Correct	82.82

3-8-29 X-section - La Jolla Blvd - Sea Lane
 J.C. Bliss to N.L. Pearl - 40' Roadway front
 Drebert Sea Lane to Marine - 46.6' wide from
 Rauter Marine to Angle Point - 52' Roadway from Angle Point to Pearl

B.M. N.E. B.P. - Sea Lane + La Jolla Blvd		70.51
	+3.31	
	H.I.	73.82
	N.L. Sea Lane =	0400
E Tpcb	3.32	70.50
G	3.85	69.97
H	3.73	70.09
¢	3.75	70.07
H	4.15	69.67
G	4.80	69.02
W Tpcb	4.35	69.47
	0425	
W Tpcb	4.40	69.42
G	4.92	68.90
H	4.25	69.57
¢	3.78	70.05
H	3.93	69.89
G	3.93	69.89
E Tpcb	3.42	70.40
	0450	
E Tpcb	3.54	70.28
G	4.00	69.82
H	3.86	69.96
¢	3.89	69.93

1/4	439	69.43
G	499	68.83
WTpcb	446	69.36
	0725	
w Tpcb	457	69.25
G	5.00	68.82
1/4	4.34	69.48
♀	3.96	69.86
1/4	4.00	69.82
G	4.14	69.68
E Tpcb	3.61	70.21
	1100	
E Tpcb	3.72	70.10
G	4.24	69.58
1/4	4.04	69.78
♀	4.07	69.75
1/4	4.54	69.28
G	5.12	68.70
w Tpcb	4.63	69.19
	1725	
w Tpcb	4.73	69.09
G	5.20	68.62
1/4	4.66	69.15
♀	4.12	69.70
1/4	4.15	69.67

G	422	69.60
E Tpcb	3.70	70.12
	1747 = S.L. Alley East side	
E Tpcb	3.74	70.08
G	4.28	69.54
1/4	4.15	69.67
♀	4.23	69.59
1/4	4.77	69.05
G	5.31	68.51
WTpcb	4.85	68.97
	1750 = S.L. Alley West side	
Tpcb	4.90	68.92
G	5.36	68.46
	1765 = N.L. Alley West side	
Tpcb	4.82	69.00
G	5.32	68.50
	1767 = N.L. Alley East side	
WTpcb	4.79	69.03
G	5.34	68.48
1/4	4.65	69.17
♀	4.20	69.62
1/4	4.16	69.66
G	4.33	69.49
E Tpcb	3.76	70.06

H.I. 7382

2+00

ETpcb	3.91	69.91
G	4.45	69.37
1/4	4.31	69.51
¢	4.32	69.50
1/4	4.82	69.00
G	5.47	68.35
W Tpcb	4.90	68.92

2+25

W Tpcb-Driveway	5.50	68.32
G	5.50	68.32
1/4	4.26	69.06
¢	4.48	69.42
1/4	4.46	69.36
G	4.60	69.22
ETpcb-Driveway	4.60	69.22

2+50

ETpcb	4.12	69.70
G	4.66	69.16
1/4	4.54	69.28
¢	4.57	69.25
1/4	4.97	68.85
G	5.47	68.35
W Tpcb	5.09	68.73

H.I. 7382

66

2+63 = E.C. Return on East Side

W Tpcb	5.12	68.70
G	5.63	68.19
1/4	5.03	68.79
¢	4.62	69.80
1/4	4.57	69.25
G	4.69	69.13
ETpcb	4.15	69.67

2+75

E Tpcb on Return	4.10	69.72
G	4.68	69.14
+12 = cb line La Jolla Blvd.	4.74	69.08
1/4	4.60	69.22
¢	4.67	69.15
1/4	5.09	68.73
G	5.66	68.16
W Tpcb	5.18	68.64

3+00

W Tpcb	5.30	68.52
G	5.78	68.04
1/4	5.23	68.59
¢	4.80	69.02
1/4	4.65	69.17
cb line	4.65	69.17
+7 = gutter	4.75	69.07
ETpcb on Return	4.14	69.68

738^v

3715 = S.L. Marine -

60' Wide
10' cbs
10' / 4s

E Tpcb on Return	3.90	69.92
G	4.47	69.95
+ 25' = CB Line	4.78	69.04
1/4	4.96	68.86
¢	5.20	68.62
1/4	5.38	68.44
G	5.86	67.96
W Tpcb	5.30	68.52
T.P. N.W. 7' Tact La Jolla + Marine	-3.72	70.10
+ 6.84		

H.I. 76.94

X-section Marine St at Joq in La

Jolla Blvd from W.L. La Jolla Blvd to E.L. La

Jolla Blvd - 60' Wide 10' cbs 10' / 4s
W.L. La Jolla Blvd

N Tpcb	8.45	68.49
G	8.92	68.02
1/4	8.44	68.50
¢	8.36	68.58
1/4	8.60	68.34
G	9.23	67.71
S Tpcb	8.50	68.44
10' Wcb La Jolla		
Tpcb S.L. Marine	8.51	68.43
G	9.06	67.88
CB	8.93	68.01

H.I. 76.94

67

1/4	8.38	68.56
¢	8.50	68.44
1/4	8.22	68.72
Ncb Line in Alley	8.54	68.40
W 1/4 La Jolla		
Ncb Line in Alley	8.57	68.37
1/4	8.06	68.88
¢	7.89	69.05
1/4	8.10	68.84
CB	8.56	68.38
S	8.62	68.32
¢ La Jolla Blvd =		
S	8.43	68.51
CB	8.25	68.69
1/4	7.87	69.07
¢	7.64	69.30
1/4	7.82	69.12
G	8.19	68.75
N Tpcb	7.74	69.20
E 1/4 La Jolla		
N Tpcb	7.47	69.47
G	7.98	68.96
1/4	7.69	67.25
¢	7.47	69.47
1/4	7.68	69.26

H.I. 76.94

cb	7.93	69.01
S	8.11	68.83
Ecb. La Jolla		
S	7.99	68.95
cb	7.64	69.30
1/4	7.37	69.57
¢	7.22	69.72
1/4	7.41	69.53
G	7.74	69.20
N Tpcb	7.20	69.74
E.L. La Jolla		
N Tpcb	6.97	69.97
G	7.65	69.29
1/4	7.30	69.64
¢	7.10	69.84
1/4	7.29	69.65
cb	7.68	69.26
S	7.86	69.08
E.L. La Jolla + 11 = 25. N cb aka Jolla Blvd Jcg + H.L. Marine		
Out 5 - Tpcb on Return	7.24	69.70
G	7.77	69.17
S	7.67	69.27
cb	7.43	69.51
1/4	7.02	69.92
¢	6.89	70.05

H.I. 76.94

RR

1/4	7.02	69.92
cb	7.37	69.57
+5.5 - End return - gutter	7.44	69.50
Tpcb	6.99	69.95
14 E.L. La Jolla + 25		
N	6.82	70.12
cb	6.70	70.24
1/4	6.61	70.33
¢	6.53	70.41
1/4	6.80	70.14
cb	7.19	69.75
+5.9. G on Return	7.42	69.52
Tpcb on Return	6.91	70.03
E.L. La Jolla + 50 = E.C. S.E. Return		
S Tpcb	6.15	70.79
G	6.74	70.20
1/4	6.30	70.64
¢	6.05	70.89
1/4	6.09	70.85
cb	6.22	70.72
N	6.10	70.84
Section along E.L. La Jolla Blvd Jcg		
E.L. + 55 on S cb line E.L. + 76 on N cb line		
N Tpcb	5.41	71.53
G	5.98	70.96

1/4	5.80	71.14
♀	5.76	71.18
1/4	6.02	70.92
G	6.58	70.36
5 Tpcb	6.00	70.94
T.P. N.W. 7' Pt Marine la Jolla		
+ 5.92		
H.I. 76.02		
Section Along N.L. Marine		
W. Tpcb	5.96	70.06
G	6.54	69.48
1/4	5.85	70.17
♀	5.30	71.72
1/4	5.17	70.85
G	5.11	70.91
ETpcb	4.60	71.42
0400 = See Sketch Pg 74		
ETpcb	5.11	70.91
G	4.50	71.41
1/4	5.08	70.94
♀	5.10	70.92
1/4	5.63	70.39
G	6.37	69.65

W Tpcb	5.80	70.22
0725		
W Tpcb	5.68	70.34
G	6.25	69.77
1/4	5.36	70.66
♀	4.93	71.09
1/4	4.95	71.07
G	4.92	71.10
ETpcb	4.40	71.62
0750		
ETpcb	4.26	71.56
G	4.80	71.22
1/4	4.75	71.27
♀	4.74	71.28
1/4	5.30	70.72
G	6.07	69.95
W Tpcb	5.52	70.50
0725		
W Tpcb	5.37	70.65
♀	5.97	70.05
1/4	5.04	70.98
♀	4.63	71.39
1/4	4.60	71.42
G	4.60	71.42
ETpcb	4.10	71.92

H.I. 76.02

1400

E Tpcb	3.93	72.09
G	4.50	71.52
1/4	4.40	71.62
φ	4.44	71.58
1/4	5.08	70.94
G	5.78	70.24
w Tpcb	5.25	70.77

1421.70 - See sketch Page 74

w Tpcb	5.15	70.87
G	5.66	70.36
1/4	4.70	71.32
φ	4.33	71.69
1/4	4.26	71.76
G	4.32	71.70
E Tpcb	3.79	72.23

Section at L Pt = 1400 - see sketch Page 74

E Tpcb	3.52	72.50
G	4.16	71.86
1/4	4.20	71.82
φ	4.28	71.74
1/4	4.88	71.14
G	5.66	70.36
w Tpcb	5.15	70.87

0725

w Tpcb	5.62	70.40
--------	------	-------

H.I. 76.02

70

G	6.18	69.84
1/4	5.27	70.75
φ	4.72	71.30
1/4	4.58	71.44
G	4.54	71.48
E Tpcb	3.94	72.08

0750

E Tpcb	4.37	71.65
G	5.03	70.99
1/4	5.02	71.00
φ	5.13	70.89
1/4	5.74	70.28
G	6.63	69.39
w Tpcb	6.03	69.99

0775

w Tpcb	6.48	69.54
G	7.07	68.95
1/4	6.18	69.84
φ	5.53	70.49
1/4	5.37	70.55
G	5.49	70.53
E Tpcb	4.81	71.21

1400

E Tpcb	5.23	70.79
G	5.96	70.06

H.I. 76.02

1/4	5.84	70.18
¢	5.97	70.05
1/4	6.46	69.56
G	7.47	68.55
W T p c b	6.88	69.14

1+25

W T p c b	7.34	68.68
G	7.96	68.06
1/4	7.03	68.99
¢	6.39	69.63
1/4	6.26	69.76
G	6.33	69.69
E T p c b	5.64	70.38

+50

E T p c b	6.10	69.92
G	6.81	69.21
1/4	6.75	69.27
¢	6.91	69.11
1/4	7.52	68.50
G	8.35	67.67
W T p c b	7.75	68.27

1+75

W T p c b	8.23	67.79
¢	8.77	67.25
1/4	7.86	68.16

H.I. 76.02

71

¢	7.34	68.68
1/4	7.10	68.92
G	7.20	68.82
E T p c b	6.56	69.46

2+00

E T p c b	7.06	68.96
G	7.72	68.30
1/4	7.58	68.44
¢	7.78	68.24
1/4	8.44	67.58
G	9.24	66.78
W T p c b	8.63	67.39

2+25

W T p c b	9.03	66.99
G	9.63	66.39
1/4	8.80	67.22
¢	8.40	67.62
1/4	7.96	68.06
G	8.18	67.84
E T p c b	7.50	68.52

2+50

E T p c b	7.95	68.07
G	8.57	67.45
1/4	8.52	67.50
¢	8.60	67.42

H.I. 76.02

1/4	9.31	66.71
G	10.02	66.00
W Tpcb	9.40	66.62
2475		
W Tpcb	9.85	66.17
G	10.52	65.50
1/4	9.59	66.43
¢	9.04	66.98
1/4	8.84	67.18
G	9.00	67.02
E Tpcb	8.33	67.69
3400		
E Tpcb	8.72	67.30
G	9.34	66.68
1/4	9.28	66.74
¢	9.47	66.55
1/4	10.06	65.96
G	10.86	65.16
W Tpcb	10.30	65.72
3425		
W Tpcb	10.74	65.28
G	11.34	64.68
1/4	10.50	65.52
¢	9.95	66.07
1/4	9.74	66.28

H.I. 76.02

72

G	9.79	66.23
E Tpcb	9.12	66.90
3450		
E Tpcb - Driveway	10.30	65.72
G	10.30	65.72
1/4	10.26	65.76
¢	10.47	65.55
1/4	11.10	64.92
G	11.80	64.22
W Tpcb	11.20	64.82
3475		
W Tpcb	11.61	64.41
G	12.26	63.76
1/4	11.35	64.67
¢	8.86	67.16
1/4	10.65	65.37
G	10.70	65.32
E Tpcb	10.08	65.94
4400 = 5 L. Peck / 80' wide 1 3/4" / 24' deep		
E Tpcb on return	10.35	65.67
G	11.08	64.94
¢	11.16	64.86
1/4	11.05	64.97
¢	11.21	64.81
1/4	11.92	64.10

H.I. 76.02

G	12.60	63 42	W
W Top	12.00	64 02	cb
T.P.	-9.34	66.68	1/4
+ 2.25			¢

H.I. 68.93

S cb Pearl			1/4
W.L. cb Top	5.08	63 85	E
G	5.69	63 24	E
cb	5.31	63 62	cb
1/4	4.81	64 12	1/4
¢	4.27	64 66	¢
1/4	4.26	64 67	1/4
cb	4.24	64 69	1/4
E	4.02	64 91	cb
+ 15 = East end S.E. Return in Dive way	2.32	66.61	W

S 1/4 Pearl

E	4.02	64 91
cb	4.32	64 61
1/4	4.26	64 67
¢	4.30	64 63
1/4	4.69	64 24
cb	5.00	63 93
W	5.25	63.68

H.I. 68.93

73

¢ Pearl

5.16	63 77
4.99	63 94
4.74	64 19
4.44	64 49
4.29	64 64
4.41	64 52
4.01	64 92

N 1/4 Pearl

4.25	64 68
4.55	64 38
4.43	64 50
4.50	64 43
4.83	64 10
5.14	63 79
5.44	63 49

N cb Pearl

W.L. Top cb	5.50	63 43
G	6.12	62 81
cb	5.72	63 21
1/4	5.06	63 87
¢	4.60	64 33
1/4	4.44	64 49
cb	4.62	64 31
G	4.66	64 27
E.L. Top cb	3.99	64 94

3-9-27
J. C. Bliss
Diebert
Rauwer

X-section - Landis
38th - 14' cbs - 13' 145

St. 36th to
V.B. 13 Pg 10
4-17-29
K.

H.I. 342.62

75

B.M. N.W. B.P. 36th + Landis -
+7.37

335.25

G

7.1

334.5

STpcb

6.55

336.07

H.I. 342.62

0+75

EL. 36th on Pavement = 0+100

N Tpcb

6.88

335.74 ✓

STpcb - Driveway

6.83

335.79

G

7.55

335.07

G

6.9

335.7

14

7.29

335.33

14

6.3

336.3

G

7.18

335.44

G

6.0

336.6

14

7.30

335.32

14

6.2

336.4

G

7.68

334.94

G

6.7

335.9

STpcb

7.10

335.52

N Tpcb - Driveway

6.70

335.92

1+00

0+75

N Tpcb

5.85

336.77

STpcb

6.92

335.70

G

6.4

336.2

G

7.4

335.2

14

6.0

336.6

14

7.2

335.4

G

5.8

336.8

G

6.8

335.8

14

6.2

336.4

14

6.9

335.7

G

6.5

336.1

G

7.2

335.4

STpcb

6.14

336.48

N Tpcb

6.68

335.94

1+40 = W.L. Alley

0+50

STpcb

5.82

336.80

N Tpcb

6.31

336.31

G

6.3

336.3

G

6.8

335.8

14

5.7

336.9

14

6.5

336.1

G

5.4

337.2

G

6.4

336.2

14

5.7

336.9

14

6.8

335.8

G

6.1

336.5

H.J. 342.62

4 T p c b	5.34	337.28
	1460 = E. L. Alley	Note Alley is paid to cb line on farm side
4 T p c b	5.05	337.57
G	5.7	336.9
1/4	5.3	337.3
♀	5.2	337.4
1/4	5.7	336.9
G	6.0	336.6
5 T p c b	5.55	337.07
	2400	
5 T p c b	5.15	337.47
G	5.7	336.9
1/4	5.2	337.4
♀	4.8	337.8
1/4	5.1	337.5
G	5.4	337.2
4 T p c b	4.80	337.8
	2425	
4 T p c b	4.52	338.10
G	5.1	337.5
1/4	4.8	337.8
♀	4.6	338.0
1/4	5.1	337.5
G	5.5	337.1
5 T p c b	4.94	337.68

H.J. 342.62

76

2750

5 T p c b	4.66	337.96
G	5.1	337.5
1/4	4.9	337.9
♀	4.5	338.1
1/4	4.6	338.0
G	4.7	337.9
4 T p c b	4.15	338.47
	2775	
4 T p c b	3.89	338.73
G	4.4	338.2
1/4	4.4	338.2
♀	4.1	338.5
1/4	4.5	338.1
G	5.1	337.5
5 T p c b	4.43	338.19
	3400 = W. L. Cherokee	
5 T p c b	4.19	338.43
G	4.89	337.73
1/4	4.34	338.28
♀	4.04	338.58
1/4	4.03	338.59
G	4.32	338.30
4 T p c b	3.62	339.00

H.I. 342.6~

E.L. Cherokee = 0700

N Tpcb	4.03	338.59
G	4.22	337.90
1/4	4.43	338.19
¢	4.35	338.27
1/4	4.67	337.95
G	5.00	337.62
S Tpcb	4.29	338.33
	0725	
S Tpcb	4.82	337.80
G	5.3	337.3
1/4	4.8	337.8
¢	4.4	338.2
1/4	4.8	337.8
G	5.0	337.6
N Tpcb	4.50	338.1
	0750	
N Tpcb	4.95	337.67
G	5.4	337.2
1/4	5.2	337.4
¢	5.1	337.5
1/4	5.4	337.2
G	5.8	336.8
S Tpcb	5.30	337.3
	0775	
S Tpcb	5.80	336.82

H.I. 342.6~

77

G	6.4	336.2
1/4	5.7	336.9
¢	5.5	337.1
1/4	5.7	336.9
e	6.2	336.4
N Tpcb	5.52	337.10
	1700	
N Tpcb	6.15	336.57
G	6.7	335.9
1/4	6.3	336.3
¢	6.1	336.5
1/4	6.4	336.2
G	6.9	335.7
S Tpcb	6.51	336.31
	1740 = W.L. Alley	
S Tpcb	7.15	335.47
G	7.7	334.9
1/4	7.2	335.4
¢	6.9	335.7
1/4	7.2	335.4
G	7.4	335.2
N Tpcb	6.71	335.91
	1760 = E.L. Alley	
N Tpcb	7.20	335.42
G	7.6	335.0

H.I. 342.62

1/4	7.5	335.1
R	7.4	335.2
5/4 cb	7.7	334.9
G	2+00 8.0	334.6
STp cb	7.60	335.02
	2+00	
STp cb	8.40	334.22
G	9.0	333.6
1/4	8.6	334.0
Q	8.2	334.4
1/4	8.2	334.4
G	8.6	334.0
N Tpcb	7.95	334.67
	2+25	
N Tpcb	8.48	334.14
G	9.2	333.4
1/4	8.9	333.7
Q	8.7	333.9
1/4	9.2	333.4
G	9.6	333.0
STp cb	9.00	333.6
	2+50	
STp cb	9.57	333.05
G	10.0	332.6
1/4	9.3	333.3

H.I. 342.62

78

Q	9.1	333.5
1/4	9.4	333.2
G	9.8	332.8
N Tpcb	9.00	333.6
	2+75	
N Tpcb	9.53	333.09
G	10.2	332.4
1/4	9.8	332.8
Q	9.7	332.9
1/4	10.0	332.6
G	10.6	332.0
STp cb	10.09	332.53
	3+00 = WL. 37 th	
STp cb	10.60	332.02
G	11.0	331.52
1/4	10.88	331.74
Q	10.48	332.14
1/4	10.45	332.17
G	10.62	332.00
N Tpcb	9.93	332.69
	S.M. N.W. S.P. 37 th Landis	-10.07 332.55

Cont. in Book 1306-75

4-2-29

569

J.C. Bliss
Drebert
RounerAdditional Notes on Milbrae +
Franklin

B.M. N.W. Top Pillar Milbrae + Franklin 61.18

+11.72

H.I. 72.90

E.L. Milbrae = 0 + 00

+5.5

φ 10' Garage in basement Stucco House

1' Back N.L. Franklin - Dirt Floor 2.3 70.6

+17.3

φ Top of Bottom step in Stucco House - Concrete 0.57 72.93

1' Back N.L. Franklin

+19.6

φ 10' Garage 14' Back S.L. Franklin - Dirt Floor 1.0 71.9

B.M. - N.W. Top Pillar Milbrae + Franklin 61.18

+5.69

H.I. 66.87

W.L. Milbrae = 0 + 00

0 + 7.6 = φ 12' Garage 8.5' Back of N.L.

Franklin - Dirt Floor 9.4 57.5

+18.4

φ 14' Garage 5' Back N.L. Franklin

Dirt Floor 7.9 59.0

H.I. 66.87

79

N.L. - Ocean View = 0 + 00

1403 - Concrete Driveway 4.5' in street

from E.L. 0.86 66.01

+5.4

Concrete steps 19' Back E.L. 0.00 66.87

+10.1

Concrete Driveway 20' Back W.L. 1.74 65.13

+12.0

Concrete steps 14' Back W.L. 2.21 64.66

+14.0

Concrete drive - 20' Back W.L. 3.51 63.36

+23.5

Concrete Steps 15' Back W.L. 5.40 61.47

All step shots are on top bottom step.

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 1/2 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body

of table in same row and column gives distance from side stake to slope stake. If ground is not nearly level, the side stake and slope stake, lower tangent by the amount of cut, elevation of fill. Add this amount to cut or fill and find distance in table. Set up rod at this point and line of sight should cut target.

IMPROVED TABLES AND INFORMATION

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add connection found in column of connections. Degree of curve with a given L may be found by dividing tangent (or external), opposite L by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

3744
3685
59

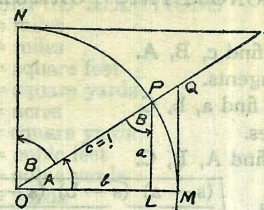


TABLE II

TRIGONOMETRIC FORMULÆ.

$$\angle A = \angle MOP \quad \angle B = \angle PON = \angle OPL$$

$$R = OB = c = 1$$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

$$\sin \frac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \quad \cos \frac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \quad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Sines} \quad \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{C}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$$

ENGINEERING DEPARTMENT
CITY OF SAN DIEGO
CALIFORNIA

406.36
 0.54
 406.90
 12.65
 394.25
 0.27
 394.52
 12.72
 381.80
 0.28
 369.79
 12.93
 356.81
 0.37
 357.20
 12.82
 344.38
 0.18
 344.56
 1.82
 342.74

6416

Winnets Orange
 Hub N.E 330.56

Orlando SW Hub 329.86

Radio & Paradise Hub 351.36

14 298.0
 292.5
 5.5

263
 167
 96