1314

DATA

DETAIL BOOK

TO-38C-F

All Lines indexed 6/20/00 [illegible]

1314

All Ives indexed 6/20/00 AH

Index

Bill Bliss
Duemmit
Jacobson
Kiernan
1/14/1929

X-Section Marlborough from the N Line of Dwight to the North Line of Lexington

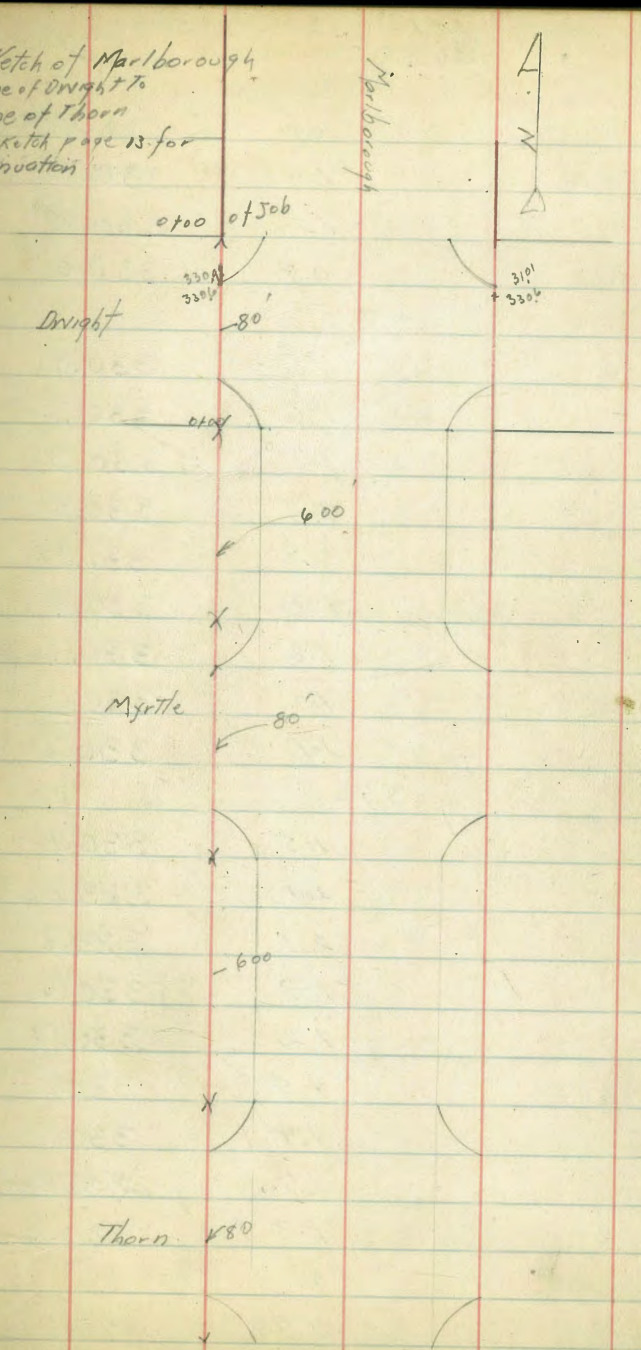
BM N.W.B.P. Dwight + Marlborough	0.86	331.85		330.99	80.5 st 14 cbs 13 1/4 s
			N Line Dwight		
		on Paving			
W Top cb			0.87	330.98	
G			1.56	330.29	
1/4			0.97	330.88	
℄			0.75	331.20	
1/4			0.92	330.93	
G			1.76	330.09	
E Top cb			0.97	330.88	
			N cb		
E on top cb			0.84	331.01	
E on Ground			1.3	330.6	
cb			1.5	330.4	
1/4			0.9	331.0	
℄			0.7	331.2	
1/4			0.9	331.0	
cb			1.3	330.6	
W on Ground			1.3	330.6	
W on Top cb			0.90	330.95	
			N 1/4		
W			1.4	330.5	
cb			1.8	330.1	
+3			1.7	330.2	
1/4			1.1	330.8	
℄			0.8	331.1	

Dwight to Redwood figured in Est Bk #11-446 8-12-29 by G.M.T.

Plotted 4/17/29 - CBH

Sketch of Marlborough N Line of Dwight to S Line of Thorn

See sketch page 13 for continuation



	+	H.I. 331.85	−	Elev.
1/4			0.9	331.0
cb			1.9	330.5
+4			1.5	330.4
E			0.9	331.0
		℄		
E			1.1	330.8
+10			1.6	330.3
cb			1.6	330.3
1/4			1.1	330.8
℄			0.8	331.1
1/4			1.0	330.9
cb			1.8	330.1
+2			1.8	330.1
W			1.1	330.8
		5 1/4		
W			1.5	330.4
+11			2.1	329.8
cb			2.1	329.8
1/4			1.3	330.6
℄			1.2	330.7
1/4			1.4	330.5
cb			1.9	330.0
+5			1.9	330.0
E			1.3	330.6
		S. cb		
E on Top cb			1.99	330.36

	+	H.I. 331.85	−	Elev.
E on Ground			2.0	329.9
cb			2.1	329.8
+2			2.0	329.9
1/4			1.6	330.3
℄			1.5	330.4
1/4			1.6	330.3
+10			2.3	329.6
cb			2.3	329.6
W on Ground			2.1	329.8
W on Top cb			1.54	330.31
		S. Line Onright = 00		
W Top cb			1.73	330.12
G			2.5	329.4
1/4			1.9	330.0
℄			1.9	330.0
1/4			1.8	330.1
G			2.4	329.5
E Top cb			1.40	330.45
		045-0		
E Top cb			3.14	328.71
G			3.7	328.2
1/4			3.6	328.3
℄			3.5	328.4
1/4			3.6	328.3
G			3.9	328.0
W Top cb			3.21	328.64

	+	HI 331.85	−	Elev
		1+00		
W Top Cb			4.88	326.97
G			5.6	326.3
+7			5.7	326.2
1/4			5.3	326.6
℄			5.0	326.9
1/4			5.1	326.8
G			5.5	326.4
E Top Cb			4.87	326.98
		1+50		
E Top Cb			6.53	325.32
G			7.3	324.6
1/4			6.8	325.1
℄			6.5	325.4
1/4			7.1	324.8
+7			7.6	324.3
G			7.5	324.4
W Top Cb			6.65	325.20
		2+00		
W Top Cb			8.33	323.52
G			9.0	322.9
+5			9.0	322.9
1/4			8.7	323.2
℄			8.1	323.8
1/4			8.6	323.3
G			9.1	322.8
E Top Cb			8.29	328.61

	+	HI 331.85	−	Elev
		2+50		
E Top Cb			9.99	321.91
G			10.7	321.2
+9			10.7	321.2
1/4			10.0	321.9
℄			9.8	322.1
1/4			10.3	321.6
G			10.6	321.3
W Top Cb			9.97	321.88
		3+00		
W Top Cb			11.65	320.20
G			12.3	319.6
+9			12.4	319.5
1/4			11.8	320.1
℄			11.5	320.4
1/4			11.8	320.1
+8			12.0	319.9
G			12.6	319.3
E Top Cb	0.92	320.65	11.6 2/3	320.23
		3+50		
E Top Cb			2.12	318.53
G			2.7	318.0
+2			2.8	317.9
+7			2.3	317.4
1/4			2.6	318.1
+1			2.4	318.3
℄			2.1	318.6

	+	HI. 320.65	−	Elev
1/4			2.3	318.4
E			2.8	317.9
W Top cb			2.10	318.55
		4+00		
W Top cb			3.82	316.83
E			4.6	316.1
1/4			4.2	316.5
1/E			3.9	316.8
1/4			4.1	316.6
+4			4.6	316.1
E			4.5	316.2
E Top cb			3.77	316.88
		4+50		
E Top cb			5.51	315.14
E			6.2	314.5
+8			6.0	314.7
1/4			6.2	314.5
+4			5.7	315.0
℄			5.5	315.2
1/4			5.8	314.9
E			6.2	314.5
W Top cb			5.52	315.13
		5+00		
W Top cb			7.29	313.41
E			7.8	312.9
+4			7.8	312.9

	+	HI. 320.65	−	Elev
1/4			7.9	313.3
℄			7.1	313.6
+10			7.3	313.4
1/4			7.7	313.0
E			7.9	312.8
E Top cb			7.18	313.47
		5+50		
E Top cb			8.99	311.71
E			9.6	311.1
+5			9.1	311.6
1/4			9.0	311.7
℄			9.0	311.7
1/4			9.1	311.6
+7			9.6	311.1
E			9.8	310.9
W Top cb			8.90	311.75
		6+00 N Line Myrtle		
W Top cb			10.59	310.06
E			11.1	309.6
+2			10.6	310.1
1/4			10.6	310.1
℄			10.3	310.4
+7			10.7	310.0
1/4			10.3	310.4
+10			10.7	310.0
E			11.1	309.6

	+	H.I. 320.65	−	Elev
E Top Cb			10.61	310.04
		N Cb		
E on Top Cb			10.64	310.01
E on Ground			10.8	309.9
Cb			11.2	309.5
+1			11.4	309.3
1/4			11.0	309.7
℄			10.9	309.8
1/4			10.9	309.8
Cb			10.8	309.9
W on Ground			10.7	310.0
W on Top Cb			10.68	309.97
		N 1/4		
W			10.2	310.5
Cb			10.4	310.3
1/4			10.7	310.0
℄			10.8	309.9
1/4			11.1	309.6
+11			11.4	309.3
Cb			11.3	309.4
E			11.1	309.6
		℄		
E			11.1	309.6
Cb			11.6	309.1
+3			11.6	309.1
1/4			11.0	309.7

	+	H.I. 320.65	−	Elev
℄			10.6	310.1
1/4			10.6	310.1
Cb			10.5	310.2
W			10.5	310.2
		5 1/4		
W			11.2	309.5
Cb			10.9	309.8
1/4			10.7	310.0
℄			10.7	310.0
1/4			11.2	309.5
+10			12.0	308.7
Cb			12.0	308.7
E			11.4	309.3
		S Cb		
E on Concrete Cutter			12.0	308.7
E on Top Cb			11.15	309.2
Grating of Cb Inlet			12.33	308.32
Flow Line 30" Storm Drain (Corrugated Pipe Out Return)			15.23	305.42 ✓
Cb			12.2	308.5
1/4			11.0	309.7
℄			10.7	310.0
1/4			11.1	309.6
Cb			11.5	309.2
Grating of Inlet. P.pe is vertical			11.53	309.12
W on Ground			11.7	309.0
W on Top Cb			11.72	308.93

	+	H.I. 320.65	−	Elev
			Sline My-tle = 00	
W Top Cb			11.68	308.97
G			11.7	309.0
1/4			11.3	309.4
℄			11.0	309.7
1/4			11.1	309.6
G			11.2	309.5
E Top Cb			11.16	309.49
T.P.	0.91	309.99	11.07	309.58
			0+37 Break in Cb on East	
E Top Cb			1.02	308.97
G			1.3	308.7
1/4			1.2	308.8
℄			1.2	308.8
1/4			1.4	308.6
G			1.8	308.2
W Top Cb			1.50	308.49
			0+95	
inside Edge			0.96	309.03
outside "			0.92	309.07
			0+60	
W Top Cb			1.61	308.38
G			2.2	307.8
℄			2.2	307.8
1/4			1.8	308.2
℄			1.7	308.3
1/4			1.8	308.2

	+	H.I. 309.99	−	Elev
G			2.0	308.0
E Top Cb			2.40	307.59
inside Edge walk			2.14	307.85
outside " "			2.15	307.84
			0+68	
E Top Cb			2.20	307.79
			0+83	
E Top Cb.			2.37	307.62
G			2.6	307.4
1/4			2.4	307.6
℄			2.4	307.6
1/4			2.4	307.6
G			2.5	307.5
W Top Cb			2.5	307.5
			1+00	
W Top Cb			1.98	308.01
G			2.5	307.5
1/4			2.5	307.5
℄			2.8	307.2
1/4			2.7	307.2
G			2.0	308.0
E Top Cb			2.50	307.49
			1+23	
E Top Cb			2.95	307.04
G			3.0	307.0
1/4			2.7	307.3

	+	HI 309.99	−	Elev
℄			2.9	307.1
1/4			2.7	307.3
G			2.9	307.1
W Top Cb			2.03	307.93
		1+50		
W Top Cb			2.41	307.58
G			3.3	306.7
1/4			3.0	307.0
℄			2.9	307.1
1/4			3.1	306.9
G			3.4	306.6
E Top Cb			3.42	306.57
		2+00		
E Top Cb			3.62	306.37
G			4.0	306.0
1/4			3.3	306.7
℄			3.3	306.7
1/4			3.4	306.6
G			4.0	306.0
W Top Cb			3.07	306.92
		2+27		
W Top Cb			3.42	306.57
G			4.2	305.8
1/4			3.7	306.3
℄			3.5	306.5
1/4			3.8	306.2

	+	HI 309.99	−	Elev
G			4.4	305.6
E Top Cb			3.67	306.32
Inside Edge Walk			3.57	306.42
Outside " "			3.50	306.49
		2+50		
E Top Cb			3.97	306.02
G			4.7	205.3
1/4			4.0	306.0
℄			3.8	306.2
1/4			3.9	306.1
℄			4.4	305.6
G			4.3	305.7
W Top Cb			3.73	306.26
		3+00		
W Top Cb			4.34	305.65
G			5.0	305.0
1/4			4.4	305.6
℄			4.4	305.6
1/4			4.7	305.3
G			5.4	304.6
E Top Cb			4.67	305.32
		3+50		
E Top Cb			5.33	304.66
G			6.1	303.9
1/4			5.3	304.7
℄			5.1	304.9

	+	H.I.	-	Elev
		309.99		
1/4			5.4	304.6
+6			5.8	304.2
G			5.8	304.2
W.Top cb			5.01	304.98
			4+00	
			5.67	304.32
G			6.5	303.5
+5			6.4	303.6
1/4			6.0	304.0
℄			5.7	304.3
1/4			6.1	303.9
G			6.9	303.1
E Top cb			5.99	304.00
			4+50	
E Top cb			6.86	303.13
G			7.3	302.7
1/4			6.8	303.2
℄			6.4	303.5
1/4			6.7	303.3
G			7.2	302.8
W.Top cb			6.35	303.64
			5+00	
W.Top cb			6.96	303.03
G			7.8	302.2
+5			7.8	302.2
1/4			7.4	302.6

	+	H.I.	-	Elev
		309.99		
℄			7.1	302.8
1/4			7.4	302.6
G			8.2	301.8
E Top cb			7.79	302.20
			5+50	
E Top cb			8.29	301.70
G			8.8	301.2
1/4			8.2	301.8
℄			7.7	302.3
1/4			7.9	302.1
G			8.2	301.8
W Top cb			7.63	302.36
			5+67	
E Top cb			8.61	301.38
			6+00 = N Line	Thorn
W.Top cb			8.25	301.74
G			8.7	301.3
1/4			8.2	301.8
℄			8.2	301.8
1/4			8.5	301.5
+6			8.9	301.1
E			9.6	300.4
E. Top cb			9.09	300.90
T.P. on B.M. NW Thorn & Marlboro	0.65	302.47	8.17	301.82
		N Cb		
E on Top cb			1.37	301.10

	+	HI 302.97	−	Elev
E on Ground			2.0	300.5
cb			1.8	300.7
1/4			1.1	301.4
℄			0.7	301.8
1/4			0.9	301.6
cb			1.3	301.2
W on Ground			1.0	301.5
W on Top cb			0.71	301.76
		N 1/4		
W			0.9	301.6
cb			1.5	301.0
1/4			1.0	301.5
℄			0.8	301.7
1/4			0.9	301.6
cb			1.1	301.4
E			1.3	301.2
		~~N~~ ℄		
E			1.2	301.3
cb			1.2	301.3
1/4			1.0	301.5
℄			1.0	301.5
1/4			1.2	301.3
cb			1.6	300.9
W			0.9	301.6
		S 1/4		
W			1.2	301.3

	+	HI 302.97	−	Elev
cb			1.7	300.8
℄			1.7	300.8
1/4			1.4	301.1
℄			1.3	301.2
1/4			1.3	301.2
cb			1.4	301.1
E			1.7	300.8
		S cb		
E on Top cb			1.92	300.55
G			1.9	300.6
cb			1.8	300.7
1/4			1.5	301.0
℄			1.4	301.1
1/4			1.5	301.0
℄			1.7	300.8
cb			1.8	300.7
W on Ground			1.6	300.9
W on Top cb			1.29	301.18
		Shine Thorn = 00		
W Top cb			1.35	301.12
G			2.1	300.4
1/4			1.6	300.9
℄			1.5	301.0
1/4			1.9	300.6
G			2.1	300.4
E Top cb			1.94	300.53

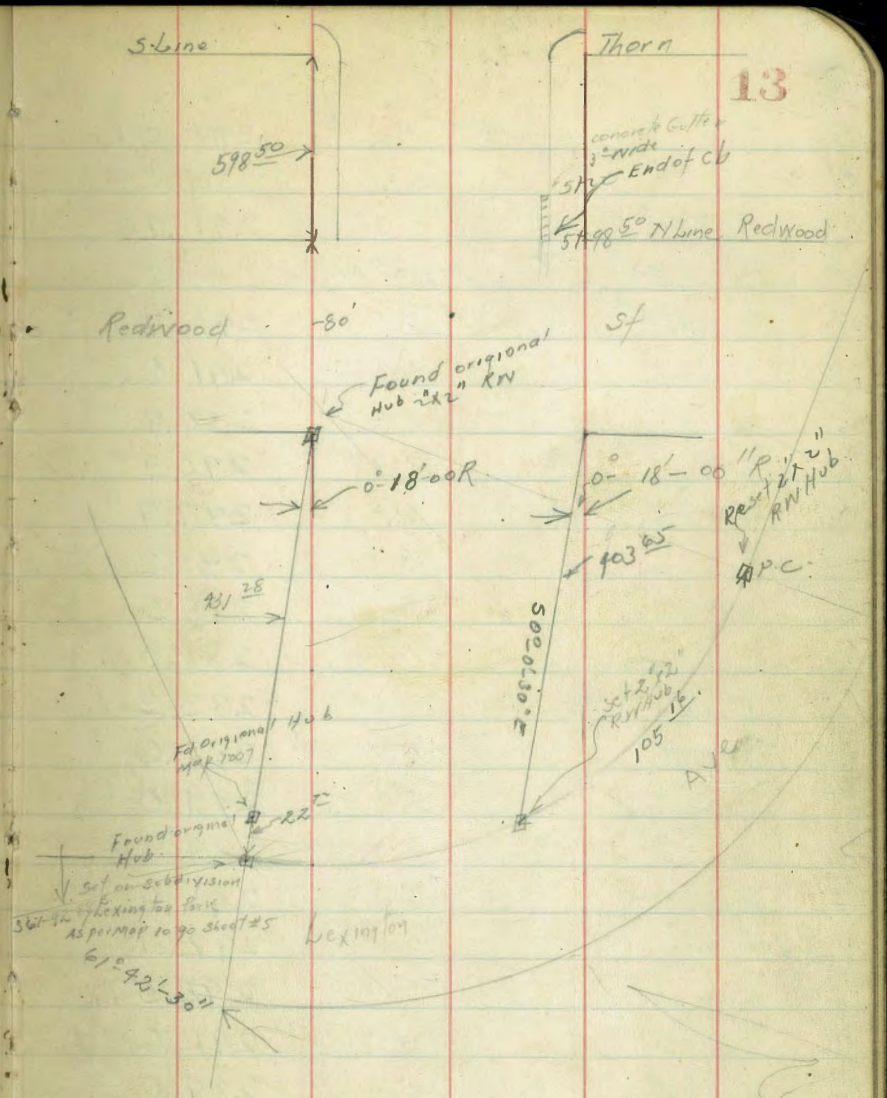
	+	H.I. 302.47	−	Elev
		0+50		
E Top Cb			2.60	299.87
G			3.2	299.3
1/4			2.7	299.8
℄			2.3	300.2
1/4			2.5	300.0
G			2.7	299.8
W Top Cb			2.05	300.42
		1+00		
W Top Cb			2.75	299.72
G			3.2	299.3
1/4			3.3	299.2
℄			2.9	299.6
1/4			3.7	298.8
G			37	298.8
E Top Cb			3.34	299.13
		1+50		
E Top Cb			4.05	298.42
G			4.5	398.0
1/4			4.0	398.5
℄			3.6	298.9
1/4			3.8	298.7
G			4.0	298.5
W Top Cb			3.95	299.02
		2+00		
W Top Cb			4.10	298.37
G			9.7	297.8

	+	H.I. 302.47	−	Elev
1/4			4.5	298.0
℄			4.4	298.1
1/4			4.7	297.8
G			5.3	297.2
E Top Cb			4.70	297.8
		2+50		
E Top Cb			5.41	297.06
G			5.9	296.6
+10			5.6	296.9
1/4			5.6	296.9
℄			5.2	297.3
1/4			5.5	297.0
G			5.4	297.1
W Top Cb			4.87	297.60
		3+00		
W Top Cb			5.55	296.92
G			6.1	296.4
+10			6.1	296.4
1/4			5.8	296.7
℄			5.7	296.8
1/4			6.2	296.3
G			6.6	295.9
E Top Cb			6.05	296.42
		3+50		
E Top Cb			6.81	295.66
G			7.4	295.1

	+	HI 302.47	−	Elev
1/4			6.7	295.8
℄			6.4	296.1
1/4			6.6	295.9
+8			6.9	295.6
G			6.9	295.6
W.Top cb			6.20	296.27
		4+00		
W.Top cb			6.93	295.54
G			7.6	294.9
+9			7.6	294.9
1/4			7.3	295.2
℄			6.9	295.6
1/4			7.4	295.1
+7			8.0	294.5
G			7.8	294.7
E.Top cb			7.47	295.00
		4+50		
E Top cb			8.21	294.26
G			8.7	293.8
1/4			8.0	294.5
℄			7.6	294.9
1/4			8.1	294.4
+3			8.4	294.1
G			8.4	294.1
W.Top cb			7.63	294.84
		5+00		

	+	HI 302.47	−	Elev
		5+00		
W.Top cb			8.28	294.19
G			9.0	293.5
1/4			8.7	293.8
℄			8.5	294.0
1/4			8.8	293.7 9.27
G			9.5	293.0 .55 (5+23 concrete)
E Top cb			8.93	293.54
		5+50		
E Top cb			9.88	292.59
G			10.5	292.0
+6			10.3	292.2
1/4			9.4	293.1
℄			9.1	293.4
1/4			9.2	293.3
G			9.5	293.0
W.Top cb TP	0.58	294.06	8.99	293.48
		5+80		
W.Top cb			1.24	292.82
G			1.6	292.5
+6			1.0	293.1
1/4			1.2	292.9
℄			1.3	292.8
1/4			1.7	292.4
+7			2.1	292.0
+10 ℄ Edge	see sketch page 13 concrete gutter		2.60	291.46
G			2.68	291.38

	+	H.I. 294.06	−	Elev
E Top cb			2.03	292.03
		5787		
E Top cb			2.20	291.86
G			2.90	291.16
+3 Edge Concrete Gutter			2.76	291.30
+7			2.2	291.9
1/4			1.7	292.4
℄			1.8	292.3
1/4			1.5	292.6
+6 Top			1.5	292.6
+6 Bottom			4.1	290.0
+10			3.4	290.7
+11			2.0	292.1
G			1.5	292.6
W Top cb			1.41	292.65
		5793		
W. Top cb			1.51	292.55
G			1.9	292.2
+8			5.1	289.0
1/4			5.8	288.3
+7			7.1	287.0
℄			4.7	289.4
+2			4.3	289.7
+4			3.2	290.9
1/4			2.6	291.5
+7			2.4	291.7



		HI 294.06			
+10			3.02	291.04	
G			3.07	290.99	
E Top cb			2.36	291.70	
	Yardage figured to here 8-12-29 Bk #11-446	G.M.T. →	5+98 50 N. Line Redwood		
E			2.9	291.7	
E Top cb			2.93	291.63	
G			3.26	290.80	
+3 edge			3.15	290.91	
1/4			6.2	287.9	
+7			8.9	285.2	
E			8.6	285.5	
+2			10.1	284.0	
+10 B. line			10.8	283.3	
+10 Top			5.5	288.6	
1/4			5.1	289.0	
+10			4.2	289.9	
G			2.7	291.4	
W Top cb			1.68	292.48	
+12 Edge walk			1.97	292.59	
W			2.5	291.6	
+6			5.1	289.0	
+15			4.5	289.6	
		N cb			
-15			4.9	289.2	
W			6.5	287.6	
+5			5.8	289.3	

		HI 294.06			
+10			6.3	287.8	
cb			6.2	287.9	
1/4			5.9	288.2	
+3			6.4	287.7	
+8			10.1	284.0	
E			12.1	282.0	
+2			13.9	180.2	
+3			15.9	278.2	
+6			17.9	276.2	
+9			16.6	277.5	
1/4			14.4	279.2	
+8			10.8	283.3	
cb			10.7	283.4	
+4			9.7	284.4	
E			10.0	284.1	
+7			11.1	283.0	
+15			12.7	281.4	
+22			14.8	279.3	
		N 1/4			
-20			19.6	274.5	
-15			17.7	276.4	
-7			13.9	180.2	
E			12.9	281.2	
cb			13.9	280.2	
+2			14.8	299.3	
+4			20.2	273.9	

	+	H.I. 294.06	−	Elev	
¼			23.7	270.4	
+6			23.8	270.3	
+10			16.9	277.2	
℄			17.6	276.5	
+10			13.7	280.4	
¼			11.0	283.1	
+5			9.1	285.0	
○6			8.6	285.5	
N			6.6	287.5	
+15			5.5	288.6	
		N¼	+7		
−15			5.8	288.3	
N			6.3	287.8	
+7			9.6	289.5	
+12			5.0	289.1	
○6			8.2	285.9	
¼			9.5	284.6	
℄			12.9	284.2	
+6			17.0	277.1	
+7			22.3	272.8	
+10			23.6	271.5	
¼			26.7	267.4	
+3			23.9	270.2	
+7			19.7	274.4	
○6			16.0	278.1	
+12			15.1	279.0	

	+	H.I. 294.06	−	Elev	
E			14.0	280.1	
+5			14.2	279.9	
+15			18.0	276.1	
+20			21.1	273.0	
+30			29.3	270.8	
+35			18.7	276.4	
		℄			
E−35			19.0	275.1	
−25			25.2	268.9	
−15			20.1	274.0	
E			15.0	279.1	
+7			16.0	278.1	
○6			18.1	276.0	
+4			17.9	276.2	
+8			22.4	271.7	
¼			28.7	265.4	
+3			23.7	270.4	
+5			18.6	275.5	
℄			13.6	280.5	
¼			10.4	283.7	
○6			9.1	~~295.0~~ 285.0	
+5			4.8	289.3	
N			5.3	288.8	
+5			6.7	287.4	
+15			6.2	287.9	

	+	HI 294.06	−	Elev
			S 1/9	
W-20			6.5	287.6
-10			6.8	287.3
-6			5.2	288.9
W			4.9	289.2
+5			5.3	288.8
cb			10.0	284.1
1/4			11.8	282.3
+9			13.5	280.6
℄			15.3	278.8
1/9			21.7	272.4
+9			25.9	268.7
+6			30.2	263.9
cb	Bottom		31.4	262.7
+2			24.0	270.1
+7			21.9	272.2
℄			20.9	273.2
+4			20.5	273.6
+13			23.8	270.3
+15			26.2	267.9
+25			27.3	266.8
+35			21.5	272.6
			S cb	
-35			22.2	271.9
-20			30.2	263.9
-5			26.6	268.5
℄			27.2	266.9

	+	HI 294.06	−	Elev
+8			30.8	263.3
+10	Bottom		33.5	260.6
+12			30.6	263.5
cb			27.1	267.0
1/4			19.6	274.5
℄			15.4	278.7
1/4			12.7	282.4
cb			11.2	282.9
+6			10.4	283.7
W			7.1	287.0
+6	old RR Fill		5.4	288.7
+14			5.4	288.7
+18			7.0	287.1
			S Lime of Redwood = 0.0	
-2	old RR Fill		5.6	288.5
-10			5.7	288.4
W			10.0	284.1
TP	0.36	283.73	10.69	283.37
cb			1.2	282.5
1/4			3.0	280.7
℄			6.1	277.6
1/4			9.7	274.0
cb			15.6	268.1
+10			21.1	262.6
℄			23.2	260.5
+3	Bottom		29.6	259.1

	+	H.I. 283.73	−	Elev	
+8			21.6	262.1	
+15			20.8	262.9	
+20			17.3	266.4	
+30 Slope. Runs up Regularly			13.0	~~260.7~~ 270.1	
		0+25			
−30			12.2	271.5	
−10			19.5	264.2	
E			25.8	257.9	
+2 Bottom ditch			28.2	255.5	
+5			24.1	259.6	
cb			18.9	265.3	
1/4			13.7	270.0	
℄			8.2	275.5	
1/4			4.5	279.2	
cb			2.4	281.3	
W			0.8	282.9	
		0+50			
W			2.4	281.3	
cb			4.0	279.7	
+11			5.8	277.9	
1/4			6.5	277.2	
℄			10.8	272.9	
1/4			16.6	267.1	
+5			19.3	264.4	
cb			25.2	258.5	
+7 Bottom ditch			29.6	254.1	

	+	H.I. 283.73	−	Elev	
+12			26.3	257.4	
E			25.4	258.3	
+10			19.8	263.9	
−20			14.4	269.3	
		0+75			
E-20			16.3	267.4	
−10			21.8	261.9	
E			27.2	255.5	
+3			29.1	254.6	
+5 Bottom ditch			31.5	252.2	
+8			30.3	253.4	
cb			25.4	258.3	
1/4			19.9	263.8	
℄			13.4	270.3	
1/4			9.3	274.4	
+7			6.8	276.9	
cb			5.5	278.2	
W			3.3	280.4	
		1+00			
W			5.4	278.3	
+11			6.9	276.8	
cb			8.0	275.7	
1/4			10.7	273.0	
℄			15.1	268.6	
1/4			22.1	261.6	
+7			25.4	258.3	

	+	H.I. 283.73	−	Elev
cb			27.6	256.1
+4			30.8	252.9
+7 Bottom ditch			33.7	250.0
+11			30.4	253.3
E			28.0	255.7
+10			23.3	260.4
+20			17.7	266.0
		1725		
-20			21.6	262.1
-10			26.1	257.6
E			31.9	251.8
+5 Bottom ditch			35.4	248.3
+10			31.7	252.0
cb			29.8	253.9
1/4			23.6	260.1
E			17.5	266.2
1/4			12.2	271.5
cb			10.0	273.7
W			7.3	276.4
		1750		
W			9.1	274.6
cb			11.5	272.2
1/4			13.9	269.8
T.P.	1.66	273.16	12.23	271.50
+5			4.9	268.3
E			8.2	265.0

	+	H.I. 273.16	−	Elev
1/4			14.5	258.7
cb			19.5	253.7
+2			20.4	252.8
+8 Bottom ditch			26.7	246.5
+11			25.1	248.1
E			24.2	249.0
+7			20.4	252.8
+14			18.2	255.0
+20			16.1	257.1
		1725		
-20			19.3	253.9
-10			22.6	250.6
-3			26.0	247.2
E Bottom			28.3	244.9
+4			27.3	245.9
+7			24.6	248.6
cb			20.3	252.9
+7			16.2	257.0
1/4			13.9	259.3
E			8.1	265.1
1/4			4.4	268.8
cb			2.3	270.9
W			0.6	272.6
		2+00		
W			2.2	271.0
cb			4.0	269.2

	+	HI 273.16	−	Elev
¼			6.0	267.2
℄			11.4	261.8
¼			17.5	255.7
cb			22.6	250.6
+8			25.9	247.3
+10 Bottom Ditch			29.3	243.9
+13 " "			29.2	244.0
E			27.8	245.4
+10			27.4	245.8
+19			25.2	248.0
+20			23.4	249.8
+30			20.1	253.1
		2+25		
−40			20.2	253.0
−30			22.8	250.4
−20			25.7	247.5
−10			27.9	245.3
−6 Bottom			31.4	241.8
E			31.1	242.1
+6			26.4	246.8
cb			23.5	249.7
¼			18.2	255.0
℄			12.6	260.6
+4			10.0	263.2
¼			7.8	265.4
cb			6.0	267.2

	+	HI 273.16	−	Elev
W			4.2	269.0
		2+50		
W			6.6	267.6
cb			8.5	264.7
¼			10.0	263.2
℄			11.6	261.6
T.P.	3.81	265.30	11.67	261.49
+8			5.3	260.0
¼			7.0	258.3
cb			12.9	253.4
E			19.0	246.3
+13			23.6	241.7
+20 Bottom ditch			27.1	238.2
+30			23.1	242.2
+40			19.2	246.1
		2+75		
−40 Bottom Ditch			29.6	235.7
−30			26.7	238.6
−25			25.5	239.8
E			16.6	248.7
cb			10.2	255.1
¼			7.2	258.1
℄			5.3	260.0
¼			3.9	261.4
cb			3.3	262.0
W			1.8	263.5

	+	H.I. 265.30	−	Elev
		3+00		
W			9.6	260.7
cb			6.0	259.3
1/4			6.6	258.7
℄			7.7	257.6
1/4			9.5	255.8
+10			10.8	254.5
cb			11.1	254.2
+3			11.5	253.8
E			14.2	251.1
+20			20.0	245.3
+27			22.2	243.1
+39 Toe slope			27.9	237.4
+51 Bottom Ditch			30.4	234.9
		3+25		
−90			25.2	240.1
−20			18.4	246.9
−15			16.2	249.1
E			14.3	251.0
cb			12.8	252.5
1/4			12.2	253.1
℄			11.2	254.1
1/4			9.8	255.5
cb			8.8	256.5
W			7.9	257.4

	+	H.I. 265.30	−	Elev
		3+40		
W			10.1	255.2
cb			10.9	254.4
+6			11.5	253.8
T.P.	1.74	254.62 ~~262.48~~	12.42	252.88 ~~260.74~~
1/4			1.9	252.7
℄			2.6	252.0
1/4			3.4	251.2
cb			4.4	250.2
E			5.7	248.9
+20			10.4	244.2
+40			15.9	238.7
		3+50		
−40			22.5	232.1
−25			18.0	236.6
−12			11.9	242.7
E			9.2	245.4
+9			7.3	247.3
cb			6.5	248.1
1/4			4.6	250.0
℄			3.6	251.0
1/4			3.0	251.6
cb			2.1	252.5
W			1.2	253.4
		3+65		
W			3.5	251.1

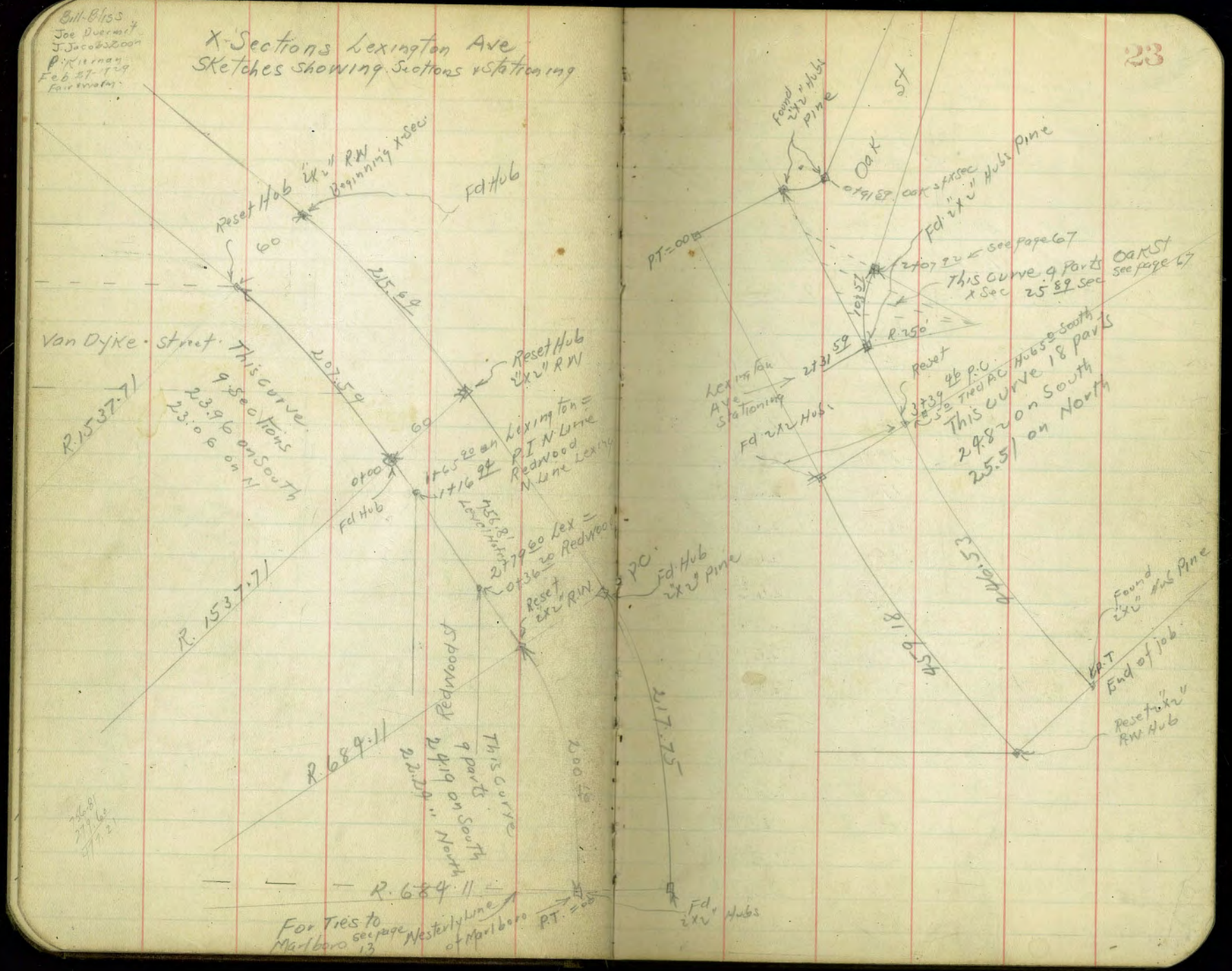
	+	H.I. 254.62	−	Elev
cb			4.6	250.0
1/4			5.8	248.8
℄			6.4	248.2
1/4			7.9	246.7
cb			10.2	244.4
E			14.1	240.5
+10			17.9	237.2
+35			22.6	232.0
		3+75		
−27. Toe slope.			26.6	228.0
−15			22.7	231.9
E			18.3	236.3
+5			15.8	238.8
cb			13.2	241.4
1/4			10.3	244.3
℄			8.4	246.2
1/4			7.5	247.1
cb			6.4	248.2
W			5.1	249.5
		3+90		
W			7.9	246.7
cb			8.6	246.0
1/4			9.7	244.9
+7			10.4	244.2
℄			11.5	243.1
1/4			13.2	241.4

	+	H.I. 254.62	−	Elev
+10			16.8	237.8
cb			18.0	236.6
E			22.9	231.7
+10 Toe slope			26.6	228.0
+19 intersects N. Line Lex. Ave			27.9	226.7
			4+03[65] Inter. ℄ Line of Mad. & N. Line Lex. Ave	
E			26.9	227.7
+5			24.4	230.2
cb			22.2	232.4
1/4			20.1	234.5
℄			17.8	236.8
+7			15.9	238.7 ✓
1/4			14.2	~~230~~.4 40.4
+5			12.8	~~231~~.8 41.8
cb			12.3	242.3
+11			11.0	243.6
W			10.4	244.2
TP	0.33	243.19	11.76	242.86
		Sec A 4+03[65] = 4+25[83]		
N			5.0	238.2
+5			7.1	236.1
+12			9.4	233.8
+20			10.9	232.3
+30			12.7	230.5
+43			13.9	229.3
+50			14.2	229.0

	+	H.I. 243.19	−	Elev	
+60			13.3	229.9	
+75			14.0	229.2	
+83 E Line			15.9	227.7	8 10
		Sec. B	9+03 65 = 9+35		
N-86 10 E Line			15.9	227.3	
-80			13.9	229.3	
-60			14.4	228.8	
-95			15.3	227.9	
-30			15.0	228.2	
-20			14.2	229.0	
-10			12.3	230.9	
N Line			10.4	232.8	
+10			9.1	234.1	
T.P.	3.83	234.81	12.71	230.98	94.80 Top of Nail
		Sec. C	9+03 65 = 9+54 P.C.		
W			9.9	224.4	
W+10			10.9	223.4	
+18			11.6	222.7	
+30			11.8	222.5	
+40			11.5	222.8	
+55			10.8	223.5	
+67			9.3	225.0	
+75			7.6	226.7	
+87			5.9	228.9	
+99 80 E Line			6.6	227.7	
Set BM NW Prop Hub Marlborough & Lexington Ave.			9.90	224.41	

Bill-Bliss
Joe Duermit
J. Jacobszoon
P. Kiernan
Feb 27-1959
Fair warm

X-Sections Lexington Ave
Sketches showing Sections & Stationing



X Sections Lexington Ave from the E Line of Van Dyke to the E Line of Central

60 st 10 cbs 10/45

	+	H.I.	−	Elev
BM NYWBP Marlborough & Thorn	3.09	304.86		301.82
TP	8.65	311.03	2.48	302.38
Set BM. N.E. Brass plug Van Dyke & Thorn			2.33	308.70
TP	0.19	298.31	12.91	298.12
TP	0.46	285.96	12.81	285.50
TP	3.06	277.34	11.68	274.28

This curve 0+00 — 0+00 P.C. Curve = see sketch page 23. This curve 9 parts

			−	Elev
N−10			13.3	264.0
N			17.9	259.4
cb			18.8	258.5
1/4			18.1	259.2
℄			17.2	260.1
1/4			16.0	261.3
cb			14.0	263.3
S			12.2	265.1

Sec #1

			−	Elev
S			17.8	259.5
+7			20.6	256.7
cb			20.9	256.4
1/4			21.0	256.3
℄			20.8	256.5
1/4			20.7	256.6
+5			20.7	256.6
+8			19.5	257.8
cb			18.1	259.2

	+	H.I. 277.34	−	Elev
+2			15.8	261.5
N			12.8	264.5

Sec 1 + 17.5 N+S

	+	H.I.	−	Elev
N			6.7	270.6
+5			8.8	268.5
cb			10.6	266.7
+5			12.1	265.2
1/4			13.5	263.8
+7			16.6	260.7
℄			17.5	259.8
+7			20.4	256.9
1/4			20.0	257.3
cb			20.5	256.8
S			22.6	254.7
+5			21.3	256.0
+15			14.3	263.0

Sec 2

	+	H.I.	−	Elev
−15			15.7	261.6
−5			22.4	254.9
S			22.5	254.8
cb			21.1	256.2
1/4			19.9	257.4
℄			16.7	260.6
1/4			13.4	263.9
cb			10.2	267.1
N			6.5	270.8

	+	HI 27.34	−	Elev.
		Sec 3		
N			8.7	268.6
cb			11.5	265.8
1/4			14.4	262.9
+5			17.1	260.2
℄			21.0	256.3
+5			23.8	253.5
1/4 Bottom ditch			23.8	253.5
cb			22.7	254.6
S			21.0	256.3
+15			18.1	259.2
		Sec 4		
-15			19.3	258.0
S			21.8	255.5
cb			22.7	254.6
1/4			23.4	253.9
℄ Bottom ditch			25.3	252.0
+5			25.2	252.1
1/4			19.8	257.5
cb			13.7	263.6
N			8.7	268.6
		Sec 5		
N			10.7	268.6
cb			15.3	262.0
1/4			20.0	257.3
℄			24.5	252.8
+5 Bottom			26.1	251.2

	+	HI 27.34	−	Elev
				25
1/4			24.5	252.8
cb			23.8	253.5
S			23.2	254.1
+10			22.7	254.6
+20			19.6	257.7
		Sec 6		
-20			22.3	255.0
S			25.2	252.1
cb			25.9	251.4
+5			26.1	251.2
+6			27.0	250.3
1/4			27.2	250.1
+1			26.1	251.2
℄			22.9	254.4
1/4			20.2	257.1
cb			16.6	260.7
N			12.3	265.0
TP	8.55	275.51	10.38	266.96
		Sec 7		
N			5.0	270.5
cb			8.9	266.6
1/4			12.5	263.0
℄			15.8	259.7
+4			17.1	258.4
1/4			19.2	256.3
+2			21.0	254.5

	+	HI 275.51	−	Elev
ob			29.5	251.0
+4			25.3	250.2
+5 Bottom ditch			26.2	249.3
+8			26.0	249.5
S			25.5	250.0
+15			23.2	252.3
+25			21.2	254.3
		Sec 7 +15' on N +9' on S.		
−25			21.8	253.7
−15			24.9	250.6
−10 Bottom Ditch			26.3	249.2
S			26.1	249.4
+5			23.9	251.6
ob			20.8	254.7
¼			15.8	259.7
℄			12.4	263.1
¼			9.9	266.1
ob			6.5	269.0
N			3.1	272.4
		Sec 8		
N			3.8	271.7
ob			6.6	268.9
¼			9.5	266.0
℄			12.5	263.0
¼			15.7	259.8
ob			19.3	256.2

	+	HI 275.51	−	Elev
S			24.1	251.4
+4			26.2	249.3
+8 Bottom ditch			26.9	248.6
+12			26.7	248.8
+15			26.1	249.4
+25			29.9	250.6
+35			21.9	253.6
		Sec 9 P.C = 00		
−35			22.1	253.4
−20 Bottom ditch			27.4	248.1
−15			27.3	248.2
S			26.2	249.3
+2			25.0	250.5
ob			22.2	253.3
¼			18.9	257.1
℄			15.3	260.2
¼			11.6	263.9
ob			8.6	266.9
N			5.9	269.6
		0 +15		
N			6.9	268.6
ob			9.0	266.5
¼			11.8	264.7
+4			13.2	262.3
℄			17.6	257.9
¼			22.8	252.7

	+	HI 225.51	−	Elev
cb			26.0	249.5
S			26.5	249.0
+12			27.2	248.3
+15			27.8	247.7
+25			22.4	253.1
		0+25		
−15			25.0	250.5
−7			27.6	247.9
S	Bottom Ditch		28.0	247.5
+2			27.0	248.5
cb			27.0	248.5
¼			25.9	249.6
℄			21.4	254.1
¼			15.0	260.5
cb			9.7	265.8
N			8.0	267.5
		0+50		
N			9.9	265.6
cb			11.8	263.7
+5			13.0	262.5
¼			16.4	259.1
℄			22.5	253.0
¼			27.0	248.5
+2	Bottom ditch		29.6	245.9
+4			28.8	246.7
+5			28.0	247.5

	+	HI 275.51	−	Elev
cb			28.6	246.9
S			28.6	246.9
+15			26.3	249.2
+25			24.2	251.3
		0+75		
+15			26.8	248.7
+10			29.3	246.2
S			30.3	245.2
+8			30.5	245.0
cb			28.6	247.9
+5			28.0	247.5
¼			24.5	251.0
℄			19.6	255.9
¼			16.6	258.9
+3			16.0	259.5
+7			15.8	259.7
cb			15.0	260.5
N			13.3	262.2
TP	0.70	263.99	12.22	263.29
		1+00		
N			5.7	258.3
cb			8.8	255.2
+4			9.8	254.2
+7			11.4	252.6
¼			12.7	251.3
+4			13.5	250.5

	+	HI 263.99	−	Elev
℄			16.9	247.6
+5			18.0	246.0
1/4			18.6	245.4
+5			18.0	246.0
CL			18.1	245.9
S			19.0	245.0
+6	Bottom ditch		20.0	244.0
+8			18.6	245.4
+15			15.6	248.4
		1+19		
−15			14.8	249.2
−2			19.5	244.5
S	Bottom ditch		20.8	243.2
+3			20.7	243.3
+5			19.7	244.3
CL			19.6	244.4
+6			19.0	245.0
1/4			20.2	243.8
+7			20.0	244.0
℄			18.3	245.7
+7			17.8	246.2
1/4			16.1	247.9
+4			14.3	249.7
+7			13.6	250.4
CL			11.6	252.4
N			7.9	256.1

	+	HI 263.99	−	Elev
TP	2.66	259.62	12.03	251.96
		1+25		
N			1.5	253.1
CL			5.5	249.1
13			7.4	247.2
1/4			9.1	245.5
℄			11.0	243.6
1/4			11.0	243.6
CL			11.0	243.6
+2	Bottom ditch		11.3	243.3
+8			11.5	243.1
S			10.3	244.3
+5			6.0	248.6
		1+42		
S			9.1	250.5
CL			9.5	245.1
+2			10.6	244.0
1/4			11.4	243.2
℄			12.0	242.6
1/4			12.4	242.2
+2			13.0	241.6
CL			13.6	241.0
+8			12.9	241.7
N			11.9	243.2
+10			9.7	244.9

	+	HI 2546	−	Elev
		1+97		
N-10			11.2	243.4
N	Bottom ditch		13.9	240.7
cb			13.2	241.4
+9			12.0	242.6
1/4			12.0	242.6
℄			11.8	242.8
1/4			11.1	243.5
cb			8.3	246.3
S			3.5	251.1
		1467	Fork in Stream	
S			1.2	253.4
cb			6.6	248.0
1/4			9.9	244.7
℄			10.7	243.9
1/4			11.5	243.1
cb			12.8	241.8
N			13.0	241.6
+10			14.8	239.8
+25			15.0	239.6
+30			15.0	239.6
+35			12.0	242.6
		1778		
-20			11.3	243.3
-10			14.0	240.6
N			15.0	239.6

	+	HI 2546	−	Elev
				29
+3			13.3	241.3
cb			13.6	241.0
+7			11.6	243.0
1/4			11.6	243.0
℄			11.5	243.1
1/4			8.0	246.6
T.P.	8.92	26038	2.66	25196
cb			10.7	249.7
S			6.6	253.8
		1+87		
S			6.0	254.4
cb			10.1	250.3
1/4			19.6	245.8
℄			18.0	242.4
1/4			19.2	241.2
cb			21.0	239.4
N			21.0	239.4
+10			19.0	241.4
+15			18.0	242.4
+25			17.0	243.4
		2+00		
+5			18.6	241.8
-15			18.8	241.6
N			19.0	241.4
cb			20.5	239.9
+5			21.5	238.9

	+	HI 260.38	−	Elev
1/4			22.0	238.4
+5			20.1	240.3
℄			19.0	241.4
1/4			15.2	245.2
cb			9.8	250.6
S			5.0	255.4
		2+25		
S			4.1	256.3
TP	9.45	261.41	8.42	251.96
cb			9.5	251.9
1/4			15.0	246.4
℄			22.0	239.4
1/4			23.3	238.1
cb			21.9	239.5
N			21.0	240.4
+25			19.0	242.4
+35			16.0	245.4
		2+96		
−30			16.0	245.4
−15			19.0	242.4
N			21.1	240.3
cb			22.0	239.4
+7			22.4	239.0
1/4			23.3	238.1
+2	Bottom ditch		24.5	236.9
℄			23.5	237.9

	+	HI 261.41	−	Elev
+4			23.5	237.9
1/4			20.7	240.7
cb			13.6	247.8
+8			8.5	252.9
S			4.9	256.5
		2+67		
S			10.2	251.2
TP	1.62	252.06	10.97	250.44
cb			6.2	245.9
1/4			12.9	239.7
+4			15.8	236.3
+7			15.1	237.0
℄			14.5	237.6
1/4			13.1	239.0
cb			12.6	239.5
N			11.4	240.7
+22			8.1	244.0
+30			5.2	246.9
		3+00		
−20			8.2	243.9
N			11.0	241.1
cb			12.2	239.9
+5			13.2	238.9
1/4			14.6	237.5
℄			14.8	237.3
+2			15.3	236.8

used this TBM the K Sec. of Bar

	+	HI 252.06	−	Elev	
+6	Bottom Ditch		16.2	235.9	
1/4			16.5	235.6	
+3			15.8	236.3	
cb			13.2	238.9	
S			11.1	241.0	
+10			5.0	247.1	
TP	6.37	296.58	11.85	240.21	This TP used as a check Redwood St. X. Section 4 See Page 54
		3+20			
−15			4.9	241.7	
−7			7.3	239.3	
S			8.0	238.6	
cb			8.7	237.9	
+4			9.0	237.6	
+8			10.2	236.4	
1/4			11.4	335.2	
+6			10.4	236.2	
℄			9.9	236.7	
1/4			9.9	236.7	
+5			9.7	236.9	
cb			7.9	238.7	
+7			5.5	241.1	
N			5.0	241.6	
TP	11.57	251.78	6.37	240.21	
		3+50			
N			8.8	243.0	
+5			10.2	241.6	

	+	HI 251.78	−	Elev	
cb			14.0	237.8	
+5			16.6	234.2	
1/4			16.7	235.1	
℄	Bottom ditch		18.6	233.2	
+4			16.1	235.7	
1/4			15.5	236.3	
+6			15.2	236.6	
S			15.0	236.8	
+20			14.0	237.8	
+30			11.5	240.3	
+38			9.7	242.1	
		3+75			
−30			15.5	236.3	
−20			15.0	236.8	
S			16.0	235.8	
cb			15.2	236.6	
1/4			15.6	236.2	
+7			17.1	234.7	
℄			17.8	234.0	
+7			18.0	233.8	
1/4			12.6	339.2	
+4			11.8	240.0	
cb			9.5	242.3	
N			5.6	246.2	
		9+00			
N			2.2	249.6	

	+	H.I. 251.78	−	Elev	
+5			5.1	246.7	
cb			8.0	243.8	
+9			10.1	241.7	
1/4			11.7	240.1	
℄			14.9	237.4	
1/4			16.0	235.8	
+4	Bottom Ditch		18.9	232.9	
+8			18.9	232.9	
cb			17.3	234.5	
S			16.0	235.8	
+30			13.8	238.0	
		4+25			
−30			13.5	238.3	
−10			17.0	234.8	
−5			19.0	232.8	
S			18.9	232.9	
+5			18.0	233.8	
cb			17.2	234.6	
1/4			15.4	236.4	
+5			14.3	237.5	
℄			14.3	237.5	
+3			13.7	238.1	
1/4			11.8	240.0	
cb			7.8	244.0	
N			3.1	248.7	

	+	HI 251.78	−	Elev	
			4+38		
N			4.9	247.4	
cb			10.2	241.6	
T.P.	4.56	246.99	9.35	242.43	
+5			7.0	240.0	
1/4			8.1	238.9	
+4			9.5	237.5	
℄			10.1	236.9	
1/4			11.1	235.9	
cb			12.2	234.8	
S			13.1	233.9	
+3			14.0	233.0	
+7	Bottom ditch		14.6	232.4	
+13			14.7	232.3	
+15			13.1	233.9	
+25			10.4	236.6	
		4+50			
−25			10.6	236.4	
−15			13.2	233.8	
−14			15.3	231.7	
−6			14.−	232.8	
S			13.2	233.8	
+5			12.6	234.4	
cb			12.2	234.8	
+7			11.8	235.5	
1/4			11.0	236.0	

	+	HI 246.99	−	Elev
+6			10.8	236.2
℄			9.8	237.2
¼			8.3	238.7
cb			6.5	240.5
N			2.9	244.1
		4+75		
N			5.8	241.2
+5			7.7	239.3
cb			8.7	238.3
¼			10.1	236.9
℄			11.4	235.6
¼			11.7	235.3
cb			12.6	234.4
S			13.0	234.0
+7			14.1	232.9
+10			15.3	231.7
+17			15.5	231.5
+25			11.1	235.9
+30			8.0	239.0
		5+00		
−25			12.7	234.3
−20			16.2	230.8
−17			16.5	230.5
−15			14.7	232.3
S			13.4	233.6
cb			13.1	233.9

	+	HI 246.99	−	Elev
¼			12.5	234.5
℄			11.4	235.6
+7			11.4	235.6
¼			10.4	236.6
cb			9.7	237.3
N			8.2	238.8
		5+50		
N			9.5	237.5
+5			11.4	235.6
cb			12.4	234.6
¼			13.3	233.7
℄			13.4	233.6
¼			13.8	233.2
cb			14.0	233.0
S			14.6	232.4
+13			15.7	231.3
+25			17.5	229.5
+30			15.0	232.0
TP	3.70	241.50	9.19	237.80
		5+75	Water course	
−25			10.6	230.9
−20			11.6	229.9
−15			11.1	229.4
−10			10.3	231.2
S			10.5	231.0
cb			10.3	231.2

	+	H.I. 241.50	−	Elev
1/4			9.8	231.7
℄			8.8	232.7
+5			9.3	232.2
1/4			8.7	232.8
+7			8.5	233.0
CB			7.5	234.0
+5			6.4	234.1
N			5.0	236.5
		6+00		
N			3.8	237.7
CB			8.9	232.6
1/4			10.6	230.9
℄			10.4	231.1
1/4			11.3	230.2
CB			11.6	229.9
S			11.3	230.2
+5			10.9	230.6
+10 Bottom ditch			12.1	229.4
+20			12.1	229.4
+25			9.5	231.7
		6+10		
-25			8.8	232.7
-20			9.8	231.7
-15 Bottom			12.7	228.8
-5			12.2	229.3
-3			11.4	230.1

	+	HI 241.50	−	Elev
S			11.8	229.7
CB			11.8	229.7
1/4			11.4	230.1
℄			11.0	230.5
1/4			11.1	230.4
+5			10.4	231.1
CB			8.9	232.6
N			3.8	237.7
		6+33		
N			6.5	335.0
CB			10.4	231.1
+5			11.7	229.8
1/4			11.9	229.6
℄			12.0	229.5
1/4			12.2	229.3
CB			12.7	228.8
+5			13.1	228.4
S			13.7	227.8
+3			12.2	229.3
+15			11.4	230.1
+25			9.0	232.5
		6+50		
-30			9.5	232.0
S			11.4	230.1
CB			12.2	229.3
+5			12.5	229.0

	+	HI 24150	−	Elev
1/4	stream bed		13.6	227.9
+6			13.9	227.6
℄			13.1	228.4
1/4			12.6	228.9
cb			11.0	230.5
N			7.9	233.6
		6+75		
N			10.2	231.3
+4			12.4	229.1
+6	edge stream bed		15.0	226.5
cb			14.6	226.9
1/4			12.8	228.7
℄			12.5	229.0
1/4			12.7	228.8
cb			12.4	229.1
S			12.0	229.5
+15			11.6	229.9
+30			11.0	230.5
		7+00		
−30			12.2	229.3
−15			12.6	229.9
S			13.2	228.3
cb			13.3	228.2
1/4			13.9	227.6
℄			13.4	228.1
1/4			13.6	227.9

	+	HI 24150	−	Elev
+2			13.6	227.9
+5	Edge wash		15.0	226.5
cb			15.8	225.7
+8	Edge wash		14.8	226.7
N			9.5	232.0
TP	1.52	234.21	8.81	232.69
		7+25		
N			3.3	230.9
+6			4.0	230.2
cb			6.0	228.2
+3			7.0	227.2
1/4			7.7	226.5
℄			8.9	225.3
+5			8.6	225.6
1/4			7.5	226.7
cb			7.1	227.1
S			7.3	226.9
+15			6.3	227.9
+25	Toe		5.1	229.1
		7+40	Water course from N	
−20			7.0	227.2
−10			8.2	226.0
S			7.8	226.4
+4			7.7	226.5
+7			8.9	225.3
cb			8.7	225.5

	+	HI 234.21	−	Elev
1/4			9.0	225.2
+5			8.2	226.0
℄			7.3	226.9
1/4			6.9	227.3
cb			4.9	229.3
N			5.2	229.0
		7+56 31 P.C. of curve		
N			3.3	230.9
cb			4.5	229.7
1/4			5.8	228.4
℄			7.1	227.1
1/4			7.9	226.3
+5			8.9	225.3
1/4			9.7	224.5
+5			8.6	225.6
S			8.4	225.8
+20			8.6	225.6
+25			7.3	226.9
TP	6.36	232.02	8.55	225.66
		Sec 1		
-40 r			9.0	223.0
-20			8.8	223.2
-5			8.2	223.8
S			7.8	224.4
+5			8.3	225.7
cb			5.7	226.3

	+	HI 232.02	−	Elev
1/4			4.8	227.2
℄			4.8	227.2
1/4			3.7	228.3
cb			2.5	229.5
N			1.7	230.3
T.P.	5.31	230.97	6.36	225.66
		Sec 2		
N			2.7	228.3
cb			3.1	227.9
1/4			4.1	226.9
℄			4.6	226.4
1/4			4.9	226.6
cb			5.4	225.6
S			5.7	225.3
+15			5.7	225.3
+25			5.8	225.2
+35			6.3	224.7
		Sec 3		
-35 edge ditch			7.3	223.7
S			6.8	224.2
cb			6.4	224.6
1/4			5.3	225.7
℄			5.9	225.1
1/4			5.4	225.6
+2			4.7	226.3
cb			4.5	226.5

	+	HI 230.97	−	Elev
N			3.8	227.2
		Sec 4		
N			9.5	221.5
cb			5.8	225.2
1/4			6.3	224.7
℄			6.6	224.4
1/4			6.6	224.4
cb			7.3	223.7
S			7.7	223.3
+15			8.6	222.4
+23 edge ditch			9.1	221.9
		Sec 5		
−30			9.1	221.9
−25			11.3	219.7
−10			10.8	220.2
S			10.4	220.6
cb			9.8	221.2
+3			8.9	222.1
1/4			8.5	222.5
℄			7.6	223.4
1/4			7.3	223.7
cb			6.6	224.4
N			3.0	227.0
		Sec 5 +14 on S. +12 on N		
N			3.9	227.1
+8			7.0	224.0

	+	HI 230.97	−	Elev
cb			7.3	223.7
1/4			8.1	222.9
℄			9.0	222.0
+5			9.7	221.3
1/4			10.9	220.1
+3			11.3	219.7
cb			11.6	219.4
S			12.4	218.6
+4			10.4	220.6
+15			9.5	220.5
+25			9.3	221.7
		Sec 6		
−25			9.3	221.7
S			10.3	220.7
+8			10.2	220.8
cb			11.7	219.3
1/4			12.1	218.9
+4			11.8	219.2
℄			10.4	220.6
+8			9.2	221.8
1/4			9.1	221.9
cb			8.3	220.7
TP	4.78	226.05	9.70	221.27
N			1.4	224.7
		Sec 7		
N			3.4	222.7

	+	HI 226.05	−	Elev
cb			5.1	221.0
+6			6.2	219.9
¼			7.1	219.0
+3			7.3	218.8
+5			8.1	218.0
℄			7.6	218.5
+3			6.9	219.2
¼			6.2	219.9
cb			5.8	220.3
S			5.5	220.6
+25			4.3	221.8
		Sec 8		
−20			3.7	222.4
−5			5.8	220.3
S			6.4	219.7
cb			6.5	219.6
¼			6.6	219.5
+5			6.9	219.2
℄			7.5	218.6
+5			8.4	217.7
¼			8.0	218.1
+3			8.0	218.1
+5			7.1	219.0
cb			6.6	219.5
N			3.6	222.5
		Sec 9		

	+	HI 226.05	−	Elev
		Sec 9 PT of Curve = 00		38
Check on BM NW Prop	Marlboro094 + Lexington			224.39
			1.66	224.39
N			1.7	224.4
cb			6.7	219.4
+2			7.7	218.4
¼			8.2	217.9
+3			9.1	217.0
+5			8.2	217.9
℄			7.9	218.2
¼			7.5	218.6
cb			6.9	219.2
S			6.0	220.1
+15			4.3	221.8
		of 25		
−10 Free Slope			5.5	220.6
S			6.5	219.6
cb			7.2	218.9
¼			8.0	218.1
+5			8.9	217.7
+7			10.0	216.1
℄			9.0	217.1
+5			8.5	217.6
¼			9.1	217.0
+5			8.5	217.5
cb			7.2	218.9
N			1.2	224.9

	+	HI 226.05	−	Elev
			0+35	
N			2.1	224.0
cb			7.3	218.8
+3			8.9	217.2
1/4			9.3	216.8
+7			8.9	217.2
℄			9.9	216.2
+4			8.5	217.6
1/4			8.0	218.1
cb			7.4	218.7
S			6.8	219.3
+5			6.6	219.5
+15			2.9	223.2
			0+50	
−10			5.0	221.1
−5			6.9	219.2
S			7.2	218.9
cb			7.5	218.6
+5			7.6	218.5
1/4			8.7	217.4
+7			8.7	217.4
℄			10.2	215.9
1/4			9.7	216.4
cb			8.7	217.4
N			5.3	220.8
			0+75	
−5			6.0	220.1

	+	HI 226.05	−	Elev
N			7.8	218.3
cb			9.5	216.6
+5			10.4	215.7
1/4			11.0	215.1
+5			10.9	215.2
+7			9.8	216.3
℄			9.3	216.8
1/4			9.5	216.6
+5			9.1	217.0
cb			8.1	218.0
S			7.9	218.2
+5			7.8	218.3
+10 Toeslope			6.6	219.5
		1+00		
−10			6.3	219.8
S			8.7	217.4
cb			9.2	216.9
1/4			9.7	216.4
℄			9.8	216.3
12			10.9	215.7
+5			11.2	214.9
1/4			11.3	214.8
+4			11.3	214.8
+4			10.5	215.6
cb			9.7	216.4
+3			9.0	217.1

	+	HI 226.05	−	Elev	
N			8.1	218.0	
+5 Too			6.9	219.2	
+10			4.3	221.8	
		1+17			
-10			7.5	218.6	
N			9.9	216.2	
cb			10.3	215.8	
+5			11.7	214.4	
1/4			11.5	214.6	
+5			11.0	215.1	
℄			10.8	215.3	
+5			9.9	216.2	
1/4			9.6	216.5	
cb			8.6	217.5	
S			7.0	219.1	
TP	9.11	219.30	10.86	215.19	
		1+50	water course from North		
-5			0.7	218.6	
S			1.5	217.8	
cb			2.5	216.8	
1/4			3.1	216.2	
℄			3.2	216.1	
+2			9.8	214.5	
1/4			5.6	213.7	
+6			4.9	214.9	
cb			9.0	215.3	

	+	HI 219.30	−	Elev	
N			3.5	215.8	
-15			3.6	215.7	
		1+75			
-10			2.0	217.3	
-5			4.8	214.5	
N			5.5	213.8	
cb			5.6	213.7	
+5			6.3	213.0	
1/4			6.1	213.2	
+5			5.8	213.5	
℄			4.8	214.5	
1/4			4.4	214.9	
cb			3.5	215.8	
S			2.7	216.6	
+5			2.1	217.2	
+15			0.3	219.0	
		2+00			
-15			2.0	217.3	
-5			3.1	216.2	
S			3.7	215.6	
cb.			4.7	214.6	
1/4			5.3	214.0	
℄			5.6	213.7	
+8			5.5	213.8	
1/4			6.8	212.5	
cb			6.3	213.0	

	+	HI 219.30	−	Elev
N			5.9	213.4
+2 Toe			5.9	213.4
+10			0.1	219.2
		2+31	±7 Oak St. Entrance	
−3			2.1	217.2
−2			5.8	213.5
N			7.2	212.1
eb			7.3	212.0
+7			7.0	212.3
1/4			6.2	213.1
+5			6.7	212.6
℄			6.9	212.4
+3			6.8	212.5
+5			6.3	213.0
1/4			6.1	213.2
cb			5.6	213.7
S			5.0	214.3
+10			4.2	215.1
+15			3.2	216.1
		2+34		
−15			3.2	216.1
−10			4.3	215.0
S			5.2	214.1
cb			5.7	213.6
1/4			6.0	213.3
+5			6.2	213.1

	+	HI. 219.30	−	Elev
+7			6.9	212.4
℄			7.1	212.2
+7			6.1	213.2
1/4			6.1	213.2
+3			7.0	212.3
cb			7.4	211.9
+9			7.0	212.3
N			3.0	216.3
+5			1.8	217.5
		2+50		
−5			3.3	216.0
N			5.0	214.3
+3 Top			5.7	213.6
+3 Bottom			8.0	211.3
cb			8.2	211.1
+7			6.8	212.5
1/4			6.8	212.5
℄			7.0	212.3
+4			7.6	212.7
1/4			6.7	212.6
cb			6.3	213.0
AS			5.9	213.9
+15			4.2	215.1
		2+75		
−15			5.3	214.0
S			6.0	213.3

	+	HI 219.30	−	Elev
CL			7.0	212.3
+5			8.1	211.2
1/4			7.9	211.4
℄			7.8	211.5
+5			8.0	211.3
1/4			8.4	210.9
+8			9.4	209.9
CL			6.9	212.4
N			6.7	212.6
+10			5.8	213.5
+15			4.6	214.7
		3+00		
−15			6.8	212.5
N			7.6	211.7
CL			7.5	211.8
1/4			7.6	211.7
℄			8.1	211.2
+7			7.9	211.4
+8			9.2	210.1
1/4			9.2	210.1
CL			9.5	209.8
+7			10.1	209.2
+8			8.7	210.6
S			7.3	212.0
+15			4.9	214.4

	+	HI 219.30	−	Elev
		3+15		
−15			5.5	213.8
S			7.9	211.9
+1			10.3	209.0
CL			9.0	210.3
+5			8.6	210.7
1/4			9.0	210.3
℄			8.6	210.7
1/4			8.9	210.9
CL			7.8	211.5
N			7.8	211.5
+20			7.7	211.9
		3+30		
−20			7.9	211.4
N			8.3	211.0
CL			8.5	210.8
1/4			9.0	210.3
℄			9.2	210.1
1/4			9.5	209.8
+5			10.1	209.2
CL			9.9	209.4
+9			10.2	209.1
S			7.9	211.4
+10			6.5	212.8
+15			6.0	213.3
		3+39	86 P.C to Left = 00	18 Pa-15
−15			5.7	213.6

	+	HI 219.30	−	Elev
S			7.7	211.6
+3			7.9	211.4
+5			10.3	209.0
cb			10.3	209.0
+5			9.9	209.4
1/4			10.1	209.2
+5			10.0	209.3
℄			9.5	209.8
1/4			9.3	210.0
cb			9.0	210.3
N			8.7	210.6
+20			8.9	210.9
		Sec 1		
−20			9.4	209.9
N			9.1	210.2
+5			10.3	209.0
cb			10.1	209.2
1/4			10.0	209.3
+1			12.0	207.3
+5			12.1	207.2
℄			10.8	208.5
1/4			10.9	208.9
cb			9.9	209.4
S			8.0	211.3
+10			6.5	212.8
+15			5.3	214.0

	+	HI 219.30	−	Elev
		Sec 2		
−15			5.4	213.9
S			7.6	211.7
cb			8.7	210.6
+2			9.3	210.0
+5			10.6	208.7
1/4			10.8	208.5
℄			11.0	208.3
1/4			11.5	207.8
cb			12.6	206.7
+3			12.3	207.0
+4			10.9	208.4
N			11.1	208.2
+5			10.6	208.7
+20			10.4	208.9
		Sec 3		
−20			11.8	207.5
N			11.9	207.4
+3			13.1	206.2
cb			12.6	206.7
+6			12.0	207.3
1/4			12.3	207.0
+5			11.2	208.1
℄			10.6	208.7
1/4			9.8	209.5
cb			8.9	210.4

	+	HI 219.30	−	Elev.
S			7.8	211.5
+15			5.8	213.5
TP.	5.20	213.98	11.02	208.28
		Sec 3 +10 S +12 N		
-15			0.4	213.1
S			2.6	210.9
cb			3.7	209.8
1/4			4.5	209.0
℄			5.1	208.4
1/4			4.8	208.7
+8			5.5	208.0
cb			7.0	206.5
N			7.1	206.4
+8			5.8	207.7
+20			6.3	207.2
		Sec 4		
-20			7.0	206.5
-10			7.8	205.7
-1			6.4	207.1
N			6.2	207.3
cb			5.7	207.8
1/4			5.4	208.1
℄			5.7	207.8
1/4			4.9	208.6
cb			4.5	209.0
S			3.9	209.6

	+	HI 213.98	−	Elev.
+15			1.4	212.1
		Sec 5		
-15			0.9	212.6
S			4.3	209.2
cb			5.1	208.4
1/4			5.8	207.7
℄			6.6	206.9
1/4			6.8	206.7
cb			7.2	206.3
+6			7.5	206.0
N			8.3	205.2
+10	Bottom ditch		9.4	204.1
+12			8.9	204.6
+13			7.3	206.2
+20			6.9	206.6
		Sec 6		
-20			8.2	205.3
-10			8.5	205.0
N			8.7	204.8
+5			9.5	204.0
cb			10.3	203.2
+3			8.5	205.0
1/4			8.5	205.0
+5			7.6	205.9
℄			7.4	206.1
1/4			6.6	206.9

	+	HI 213.98	−	Elev
cb			5.7	207.8
S			4.5	209.0
+15			1.4	212.1
		Sec 7		
-15			1.6	211.9
S			5.7	207.8
cb			6.7	206.8
1/4			8.1	205.4
+5			9.7	203.8
℄			10.0	203.5
1/4			10.4	203.1
cb			10.3	203.2
+5			10.3	203.2
N			10.1	203.4
+5			9.5	204.0
+20			9.3	204.2
		Sec 7 & 8 N +5 S		
-20			7.4	206.1
N			8.8	204.7
+5			9.7	203.8
cb			10.4	202.6
1/4			10.5	203.0
℄			10.5	203.0
1/4			10.5	203.0
+3			9.8	203.7
+5			7.9	205.6

	+	HI 213.98	−	Elev
cb			7.2	206.3
S			6.1	207.4
+15			3.0	210.5
		Sec 8		
-15			3.8	209.7
S			7.3	206.2
+6			8.3	205.2
+8			11.7	201.8
cb			11.7	201.8
1/4			11.3	201.2
+7			10.8	202.7
℄			10.3	203.2
1/4			9.7	203.8
cb			9.3	204.2
N			9.0	204.5
+10			8.1	205.4
+25			8.2	205.3
		Sec 9		
-30			8.0	205.5
-15			8.4	205.1
N			9.3	204.2
cb			10.0	203.5
1/4			10.1	203.4
℄			10.3	203.2
+5			12.2	201.3
1/4			11.8	201.7

	+	HI 213.48	-	Elev
cb			12.8	200.7
+2			13.0	200.5
+3			10.7	202.8
S.			8.8	204.7
+15			9.7	208.8
		Sec 10		
-10			4.4	209.1
S			8.7	204.8
cb			12.1	201.4
1/4			12.7	200.8
℄			13.4	200.1
+1			12.0	201.5
+4			11.0	202.5
1/4			11.2	202.3
+6			10.2	203.3
cb			10.0	203.5
N			9.9	203.6
+15			9.7	203.8
+17			8.9	204.6
+30			8.6	204.9
		Sec 11		
-20			9.5	204.0
-16			10.4	203.1
N			10.5	203.0
cb			10.7	202.8
+5			11.5	202.0

	+	HI 213.48	-	Elev
1/4			11.9	202.1
+8			12.1	201.4
℄			14.2	199.3
1/4			13.3	200.2
+6			12.9	200.6
cb			12.2	201.3
S			10.0	203.5
		Sec 12		
-5			9.2	204.3
S.			11.0	202.5
cb			12.1	201.4
+2			13.0	200.5
+8			13.0	200.5
1/4			15.0	198.5
℄			14.0	199.5
1/4			12.2	201.3
cb			11.8	201.7
N			11.4	202.1
+15			11.4	202.1
+20			10.7	202.8
T.P.	5.39	206.08	12.79	200.69
		Sec 13		
-20			3.2	202.9
-5			6.1	200.0
N			6.1	200.0
cb			7.0	199.1

	+	HI 206.08	−	Elev
1/4			7.2	198.9
℄			7.6	198.5
+1			5.5	200.6
1/4			4.8	201.3
cb			4.6	201.5
S			4.3	201.8
+10 Toe			3.0	203.1
		Sec 14		
−10			3.2	202.9
S			3.8	202.3
cb			4.5	201.6
1/4			5.0	201.1
℄			5.4	200.7
1/4			5.8	200.3
cb			6.7	199.4
+6			7.9	198.7
+7			8.6	197.5
N			8.7	197.4
+10			7.8	198.3
+16			7.7	198.4
+20			5.2	200.9
		Sec 15	Between 4. 15-16 water course from N	
−25			9.3	196.8
−20			9.8	196.3
−15			8.1	198.0
−5			7.6	198.5

	+	HI 206.08	−	Elev
N			6.8	199.3
cb			6.5	199.6
1/4			6.3	199.8
℄			5.9	200.2
1/4			5.3	200.8
cb			4.1	202.0
S			3.2	202.9
+15			1.5	204.6
		Sec 16		
−15			1.7	204.4
S			3.8	202.3
cb			4.8	201.3
1/4			6.0	200.1
℄			7.1	199.0
1/4			7.4	198.7
cb			7.5	198.6
N			7.3	198.8
+5			7.6	198.5
+15			8.4	197.7
+25			9.6	196.5
+33			10.1	196.0
+35			7.6	198.5
		Sec 17		
−30			6.6	199.5
−25			10.8	195.3
−20			10.8	195.3

	+	HI 206.08	−	Elev
-15			9.0	197.1
N			8.5	197.6
cb			8.4	197.7
1/4			8.4	197.7
℄			7.6	198.5
1/4			6.3	199.8
cb			5.5	200.6
S			4.4	201.7
+15			2.5	203.6
		Sec 18	PT of curve + East Line of Central on North	
-10			3.5	202.6
S			4.7	201.4
cb			5.4	200.7
1/4			6.0	200.1
℄			7.2	198.9
1/4			8.7	197.4
cb			9.3	196.8
N			9.7	196.4
+8			10.1	196.0
+10			11.8	194.3
+20			11.0	195.1
+30			7.7.	198.4
Set BM N.E. Prop Cor Central + Lexington Ave Also PT of curve			9.78	196.30
T.P.	11.91	216.87	1.12	204.96
Set BM PC of Curve S Side 210.70 Radius			5.29	211.58

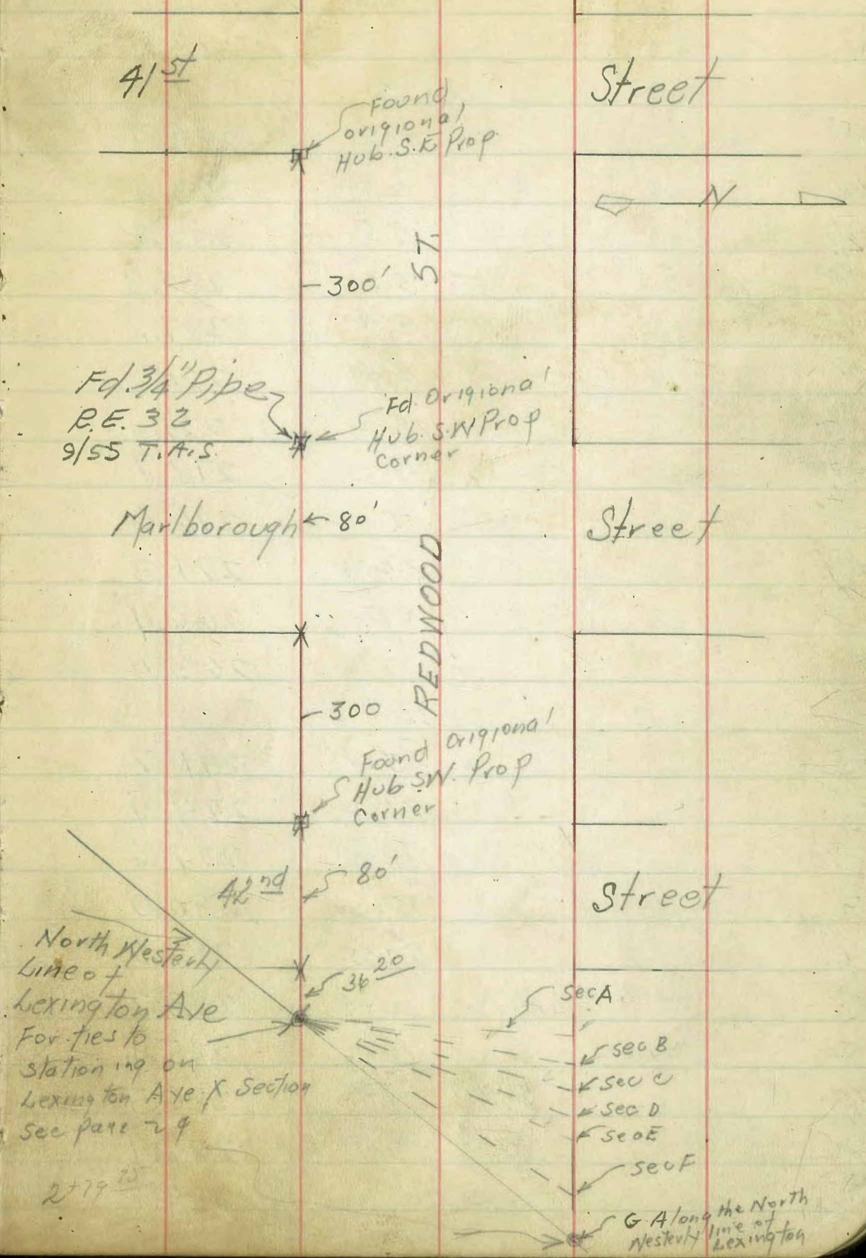
	+	HI 216.87	−	Elev
	12.33	228.16	1.04	215.83
Check out on BM N.W. Prop Cor Lexington + Kent Borough.			~~12~~	
			3.75	229.41
				224.39
				0.02 −

Bill Bliss
Duermit
Jacobszoon
Kiernan
March 9, 1929
'Inagural Day'

X Section Redwood St
from the E Line of 41st to the Westerly Line of Lexington Ave

BM. N.W. Top Curb Marlborough + Redwood set on X Sec of Marlboro	5.61	299.09		293.48
TP	4.35	295.58	7.86	291.23
	Top	0+00 . E Line of 41st		
N.			7.9	287.7
+7			6.0	289.6
cb			6.8	288.8
1/4			7.6	288.0
℄			10.5	285.1
1/4			13.6	282.0
cb			16.3	279.3
S.			19.5	276.1
+10			25.8	269.8
+20			31.2	264.4
+30			36.5	259.1
		0+02		
-30			34.8	260.8
-20			29.7	265.9
-10			25.2	270.4
S			19.1	276.5
cb			16.0	279.6
1/4			13.0	282.6
℄			10.2	285.4
+8			8.6	287.0
1/4			7.0	288.6
cb			4.6	291.0

Plotted 4/18-29- CBH



	+	HI 295.58	−	Elev			+	HI 295.58	−	Elev
+10			3.3	292.3	1/4				3.9	291.7
N			2.8	292.8	cb				2.3	293.3
		0+15			N.				1.3	294.3
N			1.9	293.7				0+50		
+6			2.2	293.4	N				1.3	294.3
cb			3.5	292.1	cb				2.2	293.4
1/4			5.7	289.9	1/4				3.2	292.4
℄			8.9	287.2	℄				4.8	290.8
1/4			11.4	284.2	+9				6.3	289.3
cb			14.2	281.4	1/4				7.2	288.4
+10			17.5	278.1	cb				10.4	285.2
S.			19.0	276.6	S				14.1	281.5
+10			24.3	271.3	+20				19.2	276.4
+20			29.2	266.4	+30				23.7	271.9
+30			32.2	263.4				0+75		
		0+30			-30				17.1	278.5
-30			23.9	271.7	-10				13.9	281.7
-20			21.2	274.4	S.				11.9	283.7
-10			18.0	277.6	cb				8.7	286.9
S.			15.6	280.0	1/4				6.1	289.5
+6			14.5	281.1	+5				5.1	290.5
cb			12.4	283.2	℄				4.4	291.2
+8			10.2	285.4	1/4				2.7	292.9
1/4			9.1	286.5	cb				1.4	294.2
+8			6.7	288.9	N				0.3	295.3
℄			5.9	289.7	T.P.	5.48	299.09	1.97		293.61

	+	HI 299.09	−	Elev.
		1+00		
N			3.6	295.5
cb			4.2	294.9
1/4			5.6	293.5
℄			6.5	292.6
+8			7.4	291.7
1/4			7.9	291.2
cb			9.7	289.4
S			12.1	287.0
+20			15.3	283.8
+30			16.8	282.3
		1+40 N&Line Alley		
-30			12.5	283.6
-10			9.8	289.3
S			9.3	289.8
cb			7.1	292.0
1/4			5.8	293.3
℄			5.0	294.1
1/4			4.2	294.9
cb			3.5	295.6
N			2.8	296.3
		1+60 E Line Alley		
N			2.5	296.5
cb			3.1	296.0
1/4			4.1	295.0
℄			4.7	294.4

	+	HI 299.09	−	Elev.
				51
1/4			5.7	293.4
cb			6.9	292.2
S			7.6	291.5
+20			9.7	289.4
		2+00		
-20			8.0	291.1
S			6.8	292.3
cb			6.1	293.0
1/4			5.4	293.7
℄			4.7	294.4
1/4			4.2	294.9
cb			3.6	295.5
N			3.2	295.9
		2+25		
N			4.0	295.1
cb			4.5	294.6
1/4			4.9	294.2
℄			5.5	293.6
1/4			6.1	293.0
cb			6.7	292.4
S			7.3	291.8
+20			8.5	290.6
		2+50		
-20			10.5	288.6
S			9.5	289.6
cb			8.9	290.2

	+	HI 299.09	−	Elev
1/4			8.2	290.9
℄			7.3	291.8
1/4			6.9	292.2
cb			6.2	292.9
N			5.8	293.3
		2+92		
N			8.1	291.0
cb			8.6	290.5
1/4			9.2	289.9
℄			9.7	289.4
1/4			10.5	288.6
+7			11.0	288.1
cb			11.5	287.6
S			12.3	286.8
+5 Toe RR Fill			12.2	287.9
+15 Top " "			10.6	288.5
+20 " " "			10.6	288.5
		2+85		
−20			13.4	285.7
−10			10.6	288.5
S			10.3	288.8
+9			10.5	288.6
cb			11.6	287.5
+3. Toe RR Fill			12.1	287.0
1/4			11.9	287.2
℄			11.2	287.9

	+	HI 299.09	−	Elev
1/4			10.5	288.6
cb			10.0	289.1
N			9.4	289.7
		2+95		
N			10.0	289.1
cb			10.8	288.3
+6			11.0	288.1
1/4			11.5	287.6
℄			11.8	287.3
+5 Toe RR Fill			11.8	287.3
1/4			10.6	288.5
cb			10.5	288.6
+7			10.5	288.6
S			12.7	286.4
+10			14.8	284.3
℄		3+00 W. Line Marlboro		
S			15.1	284.0
cb			12.3	286.8
1/4			10.0	289.1
℄			10.4	288.7
1/4			11.7	287.4
+2			12.7	286.4
cb			11.6	287.5
+9			9.0	290.1
N			7.4	292.0
TP	10.32	296.61	12.80	286.29

	+	HI 296.61	−	Elev
		E Line	Marlboro = 00	
N1			4.9	291.7
+2			5.0	291.6
+5			7.2	289.4
cb			12.5	284.1
+7			14.6	282.0
1/4			15.5	281.1
℄			17.4	279.2
1/4			23.3	273.3
cb			29.5	267.1
+6			31.8	264.8
+10			33.7	262.9
+12			37.3	259.3
S			36.0	260.6
		Of X3		
−25			27.3	269.3
−10			31.3	265.3
S			33.3	263.3
+5			33.4	263.2
+12			32.0	264.6
cb			31.0	265.6
1/4			25.5	271.1
℄			21.8	274.8
+8			19.3	277.3
1/4			19.2	277.4
+7			18.7	277.9

	+	HI 296.61	−	Elev
cb			15.8	280.8
+6			13.4	283.2
+10			9.7	286.9
N			6.9	289.7
TP	0.39	286.68	10.32	286.29
		Of 25		
N			2.6	284.1
+5			4.4	282.3
+10			6.5	280.2
cb			8.2	278.5
+6			11.0	275.7
+9			13.9	272.8
1/4			14.3	272.4
+7			15.7	271.0
℄			17.5	269.2
+10			17.5	269.2
1/4			16.8	269.9
cb			17.7	269.0
S			17.0	269.7
+20			14.9	271.8
		Of 35		
−20			9.0	277.7
S			11.4	275.8
cb			13.0	273.7
1/4			11.9	274.8
+3			11.5	275.2

	+	H.I. 286.68	−	Elev
+5			12.5	274.2
℄			12.7	274.0
+5			11.3	275.4
~~℄~~			10.7	276.0
+7			8.9	277.8
cb			6.9	279.8
+7			4.7	282.0
N			3.9	282.8
		0+45		
N			3.0	283.7
cb			4.0	282.7
+10			5.0	281.7
1/4			5.4	281.3
℄			6.9	279.8
1/4			8.1	278.6
cb			8.9	277.8
S			7.8	278.9
+20			6.7	280.0
		0+55		
−10			6.0	280.7
S			6.0	280.7
cb			5.9	280.8
1/4			5.5	281.2
℄			4.7	282.0
1/4			3.7	283.0
cb			3.3	283.4

	+	HI 286.68	−	Elev
N			2.5	284.2
		0+75		
N			1.3	285.4
cb			1.7	285.0
1/4			2.4	286.3
℄			2.8	283.9
1/4			3.0	283.7
cb			4.0	282.7
S			4.7	282.0
+10			5.2	281.5
		1+00		
−10			4.4	282.3
S			3.9	282.8
cb			3.1	283.6
1/4			2.1	284.6
℄			1.9	284.8
1/4			1.9	285.3
cb			0.7	286.0
N			0.3	286.4
FP.	446	290.59	0.55	286.13
		1+40 W. Line Alley.		
N			2.2	288.4
cb			2.8	287.8
1/4			3.6	287.0
℄			4.2	286.4
1/4			5.1	285.5

	+	HI 290.59	−	Elev
cb			6.1	284.5
S			7.1	283.5
+10			7.9	282.7
		1+60 5' Line Alley		
−10			7.6	283.0
S			7.0	283.6
cb			5.9	284.7
1/4			4.7	285.9
℄			3.5	287.1
1/4			2.9	287.7
cb			2.2	288.4
+7			1.5	289.1
N			0.6	290.0
		2+00		
N			1.0	289.6
+5			2.0	288.6
cb			2.7	287.9
1/4			3.5	287.1
℄			4.3	286.3
1/4			5.3	285.3
cb			6.8	283.8
S.			8.0	282.6
+10			8.9	281.7
		2+25		
−20			12.2	278.4
S			9.9	280.7

	+	HI 290.59	−	Elev
cb			8.1	282.5
1/4			6.6	284.0
℄			5.4	285.2
1/4			4.5	286.1
cb			3.6	287.0
N			2.1	288.5
		2+50		
N			3.6	287.0
cb			4.7	285.9
1/4			5.9	284.7
℄			7.2	283.4
1/4			8.8	281.8
cb			10.6	280.0
S			12.3	278.3
+20			14.8	275.8
		2+75		
−20			17.1	273.5
S			14.9	275.7
cb			12.8	277.8
1/4			11.4	279.2
℄			10.2	280.4
1/4			8.7	281.9
cb			7.0	283.6
N			5.4	285.2
		3+00 West Line of 42nd Street		
N			9.0	281.6

	+	HI 290.59	−	Elev
cb			10.8	279.8
1/4			11.9	278.7
℄			13.0	277.6
T.P.	2.20	279.75	13.04	277.55
1/4			3.8	276.0
cb			5.2	274.6
S			6.5	273.3
+20			8.5	271.3
		11' East of the NW Line of 42nd		
−20			13.2	273.6
S			8.8	271.0
cb			6.8	273.0
1/4			5.3	274.5
℄			4.1	275.7
1/4			2.9	276.9
cb			1.4	278.4
N			0.1	279.7
		25' East		
N			3.1	276.7
cb			4.1	275.7
1/4			5.2	274.6
℄			6.4	273.4
1/4			8.0	271.8
cb			11.4	268.4
S			14.6	265.2
+20			18.0	261.8

	+	HI 279.75	−	Elev
+30			20.1	259.7
		40' East	℄ of 42nd & Redwood	
−30			25.4	254.4
−15			21.6	258.2
S			19.2	260.6
+10			17.0	262.8
cb			15.9	263.9
1/4			12.5	267.3
℄			8.8	271.0
1/4			7.6	272.2
cb			6.3	273.5
N			5.3	274.5
		60' East		
N			10.3	269.5
cb			11.5	268.3
1/4			12.6	267.2
T.P.	0.43	267.22	12.96	266.79
℄			2.2	265.0
1/4			4.5	262.7
cb			8.6	258.6
S			12.8	254.4
+15			16.8	250.4
+30			20.9	246.8
		68' East		
−30			22.9	244.8
−15			19.5	247.7

	+	H.I. 267.22	−	Elev
		68' East		
S			15.2	252.0
cb			10.1	257.1
1/4			6.8	260.4
℄			4.6	262.6
1/4			2.6	264.6
cb			1.5	265.7
N			0.2	267.0
		80' East = East Line of 42nd = 00		
N			2.8	264.4
cb			4.6	262.6
1/4			6.7	260.5
℄			8.9	258.3
1/4			10.7	256.5
+7			12.3	254.9
cb			15.0	252.2
S			20.4	246.8
+15			23.8	243.4
+25			25.6	241.6
		0+15		
−20 N Line Lexington			26.2	241.0
S			29.1	243.1
cb			20.2	247.0
+10			16.3	250.9
1/4			15.4	251.8
℄			13.4	253.8
1/4			11.0	256.2

	+	H.I. 267.22	−	Elev
cb			8.9	248.3
N			6.7	260.5
		0+28		
N			11.5	255.7
TP	2.28	256.69	12.81	254.41
cb			3.8	252.9
1/4			6.8	249.9
℄			9.2	247.5
1/4			11.8	244.9
cb			13.8	242.9
S			14.9	241.8
+10 N Line Lexington			15.7	241.0
		0+36.20 P.T. S Line of Redwood & N Line of Lexington		80
S			15.6	241.1
cb			14.5	242.2
1/4			13.4	243.3
℄			11.2	245.5
1/4			9.1	237.6
cb			6.2	250.5
+9			4.0	252.7
N			3.3	253.4
		Sec A 0+36.20 S Line = 0+45 N Line		80.6
−80.6 N Line			6.1	250.0
cb			9.0	247.7
1/4			10.6	246.1
℄			12.2	244.5

(over)

	+	HI	−	Elev
		256.69		
		248.68		245.08
TP	360	259.21	11.61	~~255.61~~
1/4			5.5	243.2
cb			6.6	242.1
S			7.6	241.1
		Section B 0+36 $^{82\,40}_{20}$ = 0+55 N		
0+00			7.6	241.1
+15			6.7	242.0
+30			5.7	243.0
+41			4.7	244.0
+55			3.5	245.2
+68			2.8	245.9
+77			2.2	246.5
+82 ^{40} N. Line			1.5	247.2
		Sec C. 0+36 $^{85\,35}_{20}$ = 1+65 N		
−55 ^{35} N. Line			2.3	246.4
−53			2.4	246.3
−80			4.1	244.6
−74			5.6	243.1
−40			5.6	243.1
−42			6.0	242.7
−30			6.5	242.2
−15			6.8	241.9
S			7.6	241.1
		Sec D. 0+36 $^{91\,70}_{20}$ = 0+80 N		
S			7.6	241.1
+15			7.2	241.5

	+	HI	−	Elev
		248.68		
				55 47.56
+30			7.0	241.7
+45			7.4	241.3
+60			7.2	241.5
+80			6.8	241.9
+85			6.4	242.3
+88			5.1	243.6
+91 ^{20} N. Line			5.2	243.5
			Sec E 0+36 $^{99\,80}_{20}$ = 0+95 N	
−99 ^{80}			5.8	242.9
−93			5.9	242.8
−90			6.6	242.1
−80			6.7	242.0
−65			7.6	241.1
−50			7.9	240.8
−35			7.5	241.2
−15			7.5	241.2
S			7.6	241.1
			Sec F 0+36 $^{104\,20}_{20}$ = 1+03 N.	
S			7.6	241.1
+15			7.7	241.0
+30			7.8	240.9
+50			8.2	240.6
+70			7.6	241.1
+85			6.7	242.0
+95			7.5	241.2
+104 ^{20} N. Line			8.9	239.8

Sec G Along N. Line of Lexington 113 70

0+36 20 = 1+16 94 N

	+	HI 248.68	−	Elev
−113 70 N Line			7.2	241.5
−105			8.4	241.5
−101			9.5	239.2
−95			9.3	239.4
−85			7.5	241.2
−65			8.1	240.6
−50			8.3	240.4
−35			7.9	240.8
−15			7.9	240.8
0			7.6	241.1
Check out on T.P. x Sec of Lexington (set in) see page 31 This Book			8.48	240.20
				240.21
				0.01

1465 90 T.P.
113 70
1479.60

1435
30 90

−61.70
55
11 670

1+02 80
14 14
1+16.94

Bill Bliss
Joe Quermit
J Jacobs 2004
Kiernan
March 7, 1929
"Foggy"

X Sections Oak Street Lexington

Park from the N Line of Poplar to the S. Line of Lexington Ave

BM T.P set on the x Section of Lexington See page 30 This Book

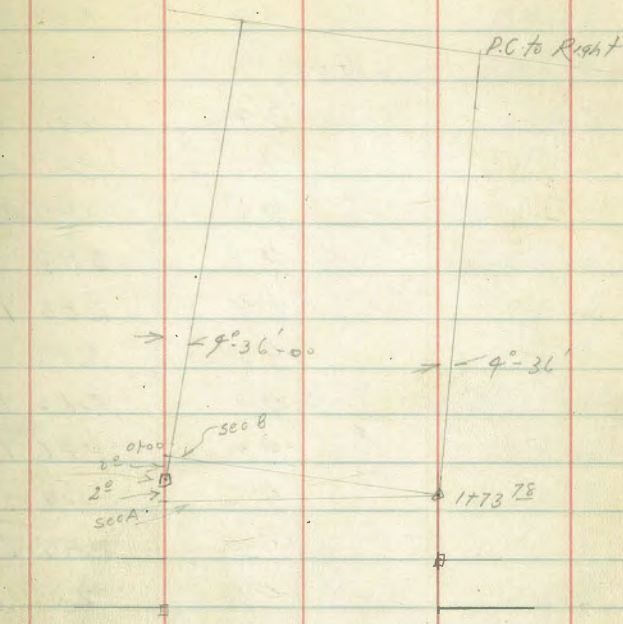
	+	H.I.	−	Elev
	11.87	262.31		250.44
TP	12.48	273.86	0.93	261.38
TP	11-60	284.58	0.88	272.98
T.P Set BM NW 1" Pipe Poplar + Oak	8:29	291.82	1.05	283.53
			4.36	287.46

0+00 N Line Poplar

50 St 10 cbs 75/4

W			9.2	287.6
cb			3.7	288.1
t2			3.7	288.1
t5			5.1	286.7
1/4			5.2	286.6
E			5.2	286.6
1/4			5.4	286.4
t3			5.4	286.4
t5			5.0	286.8
cb			4.9	286.9
E			5.0	286.8
		0+50		
E			4.8	287.0
cb			4.9	286.9
t2			4.9	286.9
1/4			5.0	286.8
E			4.8	287.0
1/4			5.0	286.8
t2			4.9	286.9

Plotted 5/6/29 / CAH



	+	HI ~~28159~~ 291.8 ~	−	Elev
+4			3.6	288.2
cb			3.8	288.0
W			3.9	287.9
		1+00		
W			3.9	287.9
cb			4.0	287.8
+3			4.0	287.8
+4			4.7	287.1
1/4			4.9	286.9
℄			4.8	287.0
1/4			4.9	286.9
+4			4.9	286.9
+6			4.6	287.2
cb			4.6	287.2
E			4.6	287.2
		1+25 S line Alley		
E			5.0	286.8
cb			5.0	286.8
+3			5.0	286.8
+4			5.4	286.4
1/4			5.4	286.4
℄			5.1	286.7
1/4			5.0	286.8
+4			4.9	286.9
cb			4.9	287.4
W			4 ~	287.6

	+	H.I. ~~28159~~ 291.8 ~	−	Elev
		1+40 N Line of Alley		
W			4.3	287.5
cb			5.0	286.8
1/4			5.0	286.8
℄			5.4	286.6
1/4			5.5	286.3
+3			5.6	286.2
+5			5.2	286.6
cb			5.2	286.6
E			5.0	286.8
		1+73 28 = Sec A	A on East	
E			6.2	285.6
+9			6.1	285.7
cb			6.7	285.1
+5			6.0	285.8
1/4			6.0	285.8
℄			5.9	285.9
1/4			5.4	286.4
cb			5.2	286.6
W			4.7	287.1
		Sec B	See Sketch = 00	
W			4.9	286.9
cb			5.2	286.6
1/4			5.5	286.3
℄			5.9	285.9
1/4			6.0	285.8

	+	HI ~~281.59~~ 291.82	−	Elev
cb			6.7	285.1
+1			6.0	285.8
E			6.2	285.6
		0+22		
E			7.8	284.2
cb			6.7	285.1
1/4			6.6	285.2
℄			6.6	285.2
1/4			6.1	285.7
cb			5.8	286.0
W			5.3	286.5
		0+37		
W			6.4	285.4
cb			7.0	284.8
1/4			7.7	284.1
℄			8.3	283.5
+3			8.1	283.7
1/4			8.8	283.0
cb			8.2	283.6
+3			7.4	284.4
E			7.5	284.3
		0+49		
E			8.0	283.8
cb			11.4	280.4
+2			13.1	278.7
1/4			12.5	279.3

	+	H.I. ~~281.59~~ 291.82	−	Elev
+2			11.8	280.0
+5			9.7	282.1
℄			8.8	283.0
1/4			8.0	283.8
cb			7.2	284.6
W			6.7	285.1
		0+60		
W			6.9	284.9
cb			7.8	284.0
1/4			8.6	283.2
+3			9.3	282.5
℄			12.1	279.7
1/4			16.2	275.6
+4			16.6	275.2
℄			16.8	275.0
+1			14.7	277.1
+5			13.0	278.8
E			11.6	280.2
		0+74		
E			14.2	277.6
cb			18.3	273.5
+1			19.1	272.7
+5			18.6	273.2
1/4			18.6	273.2
℄			13.8	278.0
1/4			10.2	281.6

	+	HI ~~281.59~~ 291.82	−	Elev
cb			8.5	283.3
W			7.3	284.5
		0+81		
W			7.8	284.0
cb			9.4	282.4
1/4			11.0	280.8
℄			14.0	277.8
1/4			17.9	273.9
+3			19.3	272.5
+5			20.6	271.2
cb			21.0	270.8
+4			21.3	270.5
E			18.5	273.3
		0+97		
E			21.8	270.0
+5			24.5	267.3
cb			23.7	268.1
1/4			19.8	272.0
℄			16.1	275.7
1/4			13.8	278.0
cb			10.2	281.6
W			8.5	283.3
		1+30 opposite		
W			11.7	280.1
TP	2.30	282.29	11.83	279.99
cb			5.4	276.9

	+	~~272.06~~ HI 282.29	−	Elev
				63
1/4			8.3	274.0
℄			11.3	271.0
1/4			13.9	268.9
cb			16.5	265.8
+5			19.3	263.0
E			19.5	262.8
+10	Slope up		14.4	267.9
		1+50		
-10			17.8	264.5
E			20.2	262.1
+3			22.4	259.9
+6			22.1	260.2
cb			19.4	262.9
1/4			15.1	267.2
℄			13.2	269.1
1/4			9.7	272.6
cb			7.4	274.9
W			3.3	279.0
		1+76		
W			4.1	278.2
cb			7.6	274.7
1/4			11.0	271.3
℄			13.7	268.6
1/4			16.8	265.5
cb			20.2	262.1
E			26.1	256.2

	+	~~272.06~~ HI 282.29	−	Elev	
+4			26.1	256.2	
+15			19.6	262.7	
		2+01			
−25			24.7	257.6	
−15			28.3	254.0	
−5			28.4	253.9	
E			26.3	256.0	
cb			20.7	261.6	
1/4			16.4	265.9	
℄			13.4	268.9	
1/4			10.4	271.9	
cb			7.5	274.8	?
W			4.1	278.2	See sheet 2 Lexington Park
	See ○	2+21	66 P.C. Left	7 Parts	(2221) on West 26.5 on East
W			4.6	277.7	
cb			7.4	274.9	
1/4			10.6	271.7	
℄			13.5	268.8	
1/4			17.1	265.2	
cb			20.1	262.2	
E			24.7	257.6	
+15 Bottom			32.2	250.1	
+20			32.0	250.3	
+25			29.6	252.7	
		Sec 1			
−25 Bottom			36.9	245.4	

	+	~~272.06~~ HI 282.29	−	Elev
−20			33.4	248.9
−10			29.1	253.2
E			24.5	257.8
cb			20.1	262.2
1/4			16.5	265.8
℄			13.1	269.2
1/4			9.9	272.4
cb			7.7	274.6
W			5.2	277.1
			Sec 2	
TP.	1.26	277.16 ~~266.93~~	6.39	275.90 ~~265.67~~
W			0.9	276.3
cb			3.5	273.7
1/4			5.5	271.7
℄			7.6	269.6
1/4			9.7	267.5
cb			12.5	264.7
E			17.1	260.1
+33			31.6	245.6
+38			33.5	243.7
+40 Bottom			36.1	241.1
+46			36.1	241.1
+50			32.0	245.2
			Sec 3	
−60 Bank			36.0	241.2
−54 Bottom			41.3	235.9

	+	H.I.	−	Elev
		~~266.93~~ 277.16		
-49			41.3	235.9
-40 Edge Bank			32.6	244.6
E			15.3	261.9
cb			11.6	265.6
1/4			9.5	267.7
℄			7.9	269.3
1/4			5.9	271.3
cb			3.9	273.3
W.			1.7	275.5
		Sec. 4		
W			3.3	273.9
cb			5.9	271
1/4			7.9	693
℄			9.5	267.7
1/4			10.7	665
cb			13.2	640
E.			16.9	260.3
+45			35.4	41.8
+58			42.7	345
+64 Bottom			47.6	230.0
+74			46.3	220.9
		Sec. 5 = New Notes at H&L		
-75			54.3	22.9
-65 Bottom			56.3	220.9
-55			53.5	25.7
-45			50.7	26.5

	+	H.I.	−	Elev
		~~266.93~~ 277.16		
-35			39.0	28.2
E			27.8	243.4
cb			23.4	53.8
1/4			20.6	56.6
℄			17.2	260.0
1/4			14.8	62.4
cb			12.8	64.4
W.			10.4	266.8
T.P.	0.66	264.86 ~~254.63~~	12.96	264.20 ~~253.97~~
		Sec. 6.		
W.			3.3	261.6
cb			8.4	56.5
1/4			12.3	52.6
℄			14.8	250.1
1/4			17.6	47.3
cb			19.8	45.1
E.			24.4	240.5
+30			41.0	24.9
+40			43.3	21.6
+42 Bottom			44.3	220.6
+50			44.3	20.6
		P.C. Sec. 7 = 0+00		
-45 Bottom			45.0	219.9
-40			42.9	22.0
-25			40.8	24.1
E			32.4	232.5

		~~254.63~~ HI 264.86		
cb			27.8	37.1
¼			24.0	40.9
℄			20.0	44.9
¼			16.0	258.9
cb			12.8	57.1
W.			6.8	258.1
		0+25		
W.			10.3	254.6
TP.	0.99	254.29 ~~254.06~~	11.56	253.30 ~~253.07~~
cb			5.4	48.9
¼			9.0	45.3
℄			12.9	241.4
¼			16.6	37.7
cb			19.9	34.4
E			25.3	229.0
+20			31.4	22.9
+35	Bottom		32.8	221.5
		0+50		
-45	S. Line Lexington		34.0	20.3
-20			32.3	222.0
E			28.3	226.0
cb			24.2	30.1
¼			21.0	33.3
℄			17.6	236.7
¼			13.6	40.7
cb			9.4	44.9

		+	HI ~~244.06~~ 254.29	−	Elev.
W				2.7	251.6
			0+75		
W.				5.0	249.3
cb				10.3	44.0
¼				14.3	40.0
℄				18.3	236.0
¼				22.5	31.8
cb				26.0	28.3
E				30.0	224.3
+10				32.0	22.3
+32	S. Line Lexington			34.6	19.7
		−	0+91.29		See Sketch Page 23
-24	S. Line Lexington			34.0	21.3
E.	P.C. of Pat. - Oak & Lexington			31.4	222.9
cb				27.3	27.0
¼				23.5	30.8
℄				20.0	234.3
¼				16.3	38.0
cb				12.4	41.9
W.				6.6	247.7
			1+00		
W				8.0	246.3
cb				12.6	41.7
¼				16.4	37.9
℄				20.1	234.2
¼				23.3	31.0

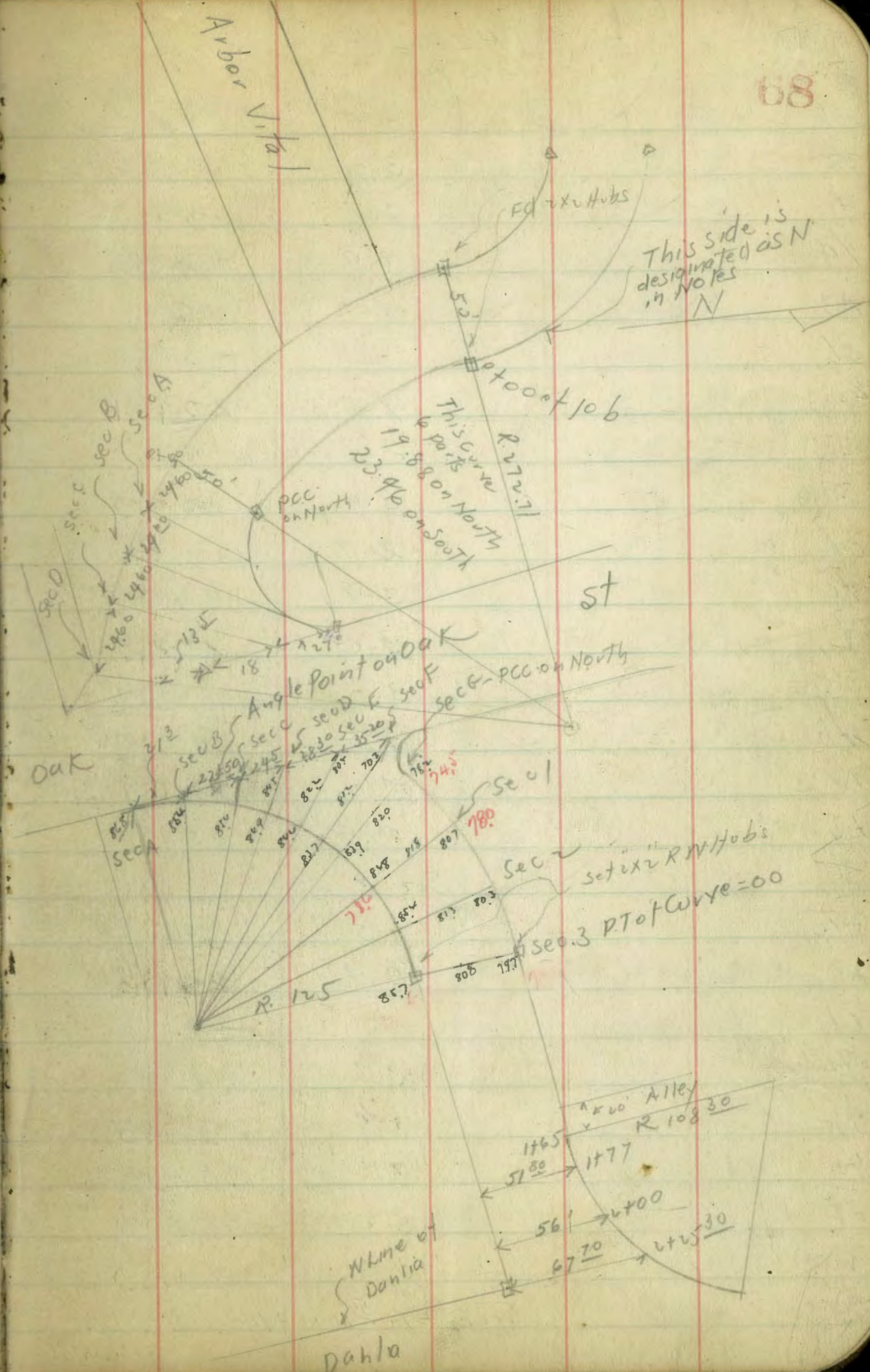
	+	HI ~~244.06~~ 259.29	−	Elev
cb			26.6	27.7
E			31.6	222.7
+21	S. Line Lexington		34.3	200
		1+25		
-09	S Line Lexington		35.0	19.3
E.			34.1	220.2
cb			30.3	24.0
¼			27.3	27.0
¼			23.4	230.9
¼			20.0	34.3
cb			17.4	36.9
W.			12.7	241.6
TP	1.91	243.54 ~~233.31~~	12.66	241.63 ~~221.40~~
		1+50		
W			7.4	236.1
+10			11.2	32.3
+20			14.9	228.6
+39			24.0	219.5
+48	S. Line Lexington		25.0	218.5
		1+75		
-38	S. Line Lexington		26.0	217.5
-26			24.0	219.5
-19			21.2	22.3
-15			18.5	25.0
-10			16.0	27.5
W.			12.7	330.8

	+	~~233.31~~ HI 243.54	−	Elev
		231.92		230.57
TP	1.35	~~221.69~~	12.97	~~220.34~~
		2+07.92 PC. see sketch Page 3		(4 parts) 25.89
W			7.8	224.1
+12			10.8	221.1
+23	S. Line Lexington		13.1	218.8
		Sec. 1		
-12	S. Line Lexington		14.2	217.7
W			11.9	220.0
		Sec. 2		
W.			15.0	216.9
+6	S. Line Lexington		15.9	216.5
		Sec. 3		
-01	S. Line Lexington		16.4	215.5
W			16.9	215.1
		Sec. 4		
Intersection	S. Line Lexington & Westerly Line Oak		17.6	214.3
				224.40 Marlborough
TP			7.52	224.41 BM @ Lex
	+	HI	−	0.01 error
BM NW Marl Boro	8.56	232.97		224.41
TP	8.64	236.82	4.79	228.18
TP	10.92	244.99	2.25	234.57
T.P.	10.72	250.95	4.76	240.23
Check on starting T.P.			0.50	250.45

X Section of Manzanita St Lexington Park from PRC North of Arbor Vita to the West Line of Dahlia

	+	HI	−	Elev	
BM N.W. 1" Pipe Oak + Poplar	8.47	295.94		287.47	50' st 10' cbs 7.5' 1/4s
		0+00 =			
N			3.6	292.3	
cb			2.9	293.0	
1/4			2.3	293.6	
℄			2.1	293.8	
1/4			2.3	293.6	
+3			2.5	293.4	
+4			1.9	294.0	
cb			1.8	294.1	
S			1.5	294.4	
			Sec 1		
S			1.5	294.4	
cb			2.0	293.9	
+5			2.2	293.7	
+6			3.0	292.9	
1/4			2.9	293.0	
℄			2.6	293.3	
1/4			2.8	293.1	
cb			3.3	292.6	
N			3.8	292.1	
+10			4.5	291.4	
			Sec 1 +8 on N +9.6 on S = N Line Arbor Vita		
−10			4.7	291.2	
N			4.0	291.9	

Plotted Fl. 5-15-29



	+	HI 295.94	−	Elev
cb			3.9	292.5
1/4			3.0	292.9
℄			2.7	293.2
1/4			2.9	293.0
+3			2.3	293.6
cb			2.1	293.8
S			1.8	294.1
			Sec 2	
S			2.0	293.9
cb			2.7	293.2
1/4			2.8	293.1
℄			3.0	292.9
1/4			3.2	292.7
cb			3.6	292.3
N			4.2	291.7
+10			4.9	291.0
			Sec 3	
-10			5.5	290.4
N			4.7	291.2
cb			4.1	291.8
1/4			3.7	292.2
℄			3.4	292.5
1/4			3.2	292.7
cb			3.2	292.7
S			3.0	292.9

Sec 3 + 12.5 on N + 14.8 on S = S. Line Arbor Vitae

	+	HI 295.94	−	Elev
S			3.0	292.9
cb			3.2	292.7
+2			3.2	292.7
+3			3.7	292.2
1/4			3.8	292.1
℄			3.9	292.0
1/4			4.2	291.7
cb			4.6	291.3
N			5.3	290.6
+10			6.2	289.7
			Sec 4	
-10			6.4	289.5
N			5.5	290.4
cb			4.8	291.1
1/4			4.3	291.6
℄			4.2	291.7
1/4			4.1	291.8
+4			4.2	291.7
+5			3.3	292.6
cb			3.3	292.6
S			3.2	292.7
			Sec 5	
S			4.0	291.9
cb			4.4	291.5
+2			4.5	291.4
+3			5.3	290.6

	+	HI 295.94	−	Elev
1/4			5.1	290.8
℄			5.0	290.9
1/4			5.5	290.4
cb			5.7	290.2
N			6.4	289.5
+10			7.1	288.8
	Sec 6 P.C.C on N = 00 See Sketch			
−10			8.1	287.8
N			7.4	288.5
cb			6.8	289.1
1/4			6.5	289.4
℄			5.7	290.2
1/4			6.0	289.9
+3			6.1	289.8
+4			5.2	290.7
cb			5.1	290.8
S			4.9	291.0
	Sec A			
S			5.8	290.1
+13			6.4	289.5
+14			7.2	288.7
+26			6.9	289.0
+40			7.6	288.3
+50			7.8	288.1
+58[3]			8.3	287.5

	+	HI 295.94	−	Elev
		Sec B = +45' N of Angle on Oak		
−75			10.6	285.3
−65			9.9	286.0
−50			8.7	287.2
−35			8.0	287.9
−27			7.8	288.1
−17			8.1	287.8
−16			7.5	288.4
		Sec C = +18' N. of Angle on Oak		
S			7.4	288.5
+18			8.1	287.8
+19			8.7	287.2
+25			8.5	287.4
+38			8.7	287.2
+50			9.3	286.6
+52[3] inter N. Line Lex				
		Sec D −13[5] S of Δ on Oak		
−30[5]			8.9	287.0
−20			8.7	287.2
−19			8.1	287.8
−5			7.9	288.0
S			7.5	288.4
	see sketch page 68			This curve 6 par to 21.24 on S. side to pcc on N
		Sec A E. Side of Oak		
E			9.1	286.8
		Sec B		
−3 E Line of Oak = at 21[3]			9.8	286.1
E			9.8	286.1

	+	H.I.	-	Elev
		285.94		
Sec C intersects 10' N of A				
S			10.5	285.4
+6^8			10.6	285.3
Sec D Intersects 34^5 N of A				
S			11.0	284.9
+4			11.0	284.9
+6			11.8	284.1
+14^8			11.4	284.5
Sec E Intersects 62^8 N of A				
S			11.5	284.4
+1			11.7	284.2
+2			12.4	283.5
+10			12.1	283.8
+20			12.4	283.5
+23			12.9	283.0
+25 ℄			13.7	282.2
+28^7 E Line Oak			15.7	280.2
TP	3.41	286.73	12.62	283.32
Sec F Intersects 98' N of A				
S			3.0	283.7
+1			3.1	283.6
+2			4.0	282.7
+8			3.7	283.0
cb			3.7	283.0
1/4			4.0	282.7
+6			4.3	282.4

	+	H.I.	-	Elev
		286.73		
℄			5.5	281.2
1/4			8.6	278.1
+4			10.4	276.3
cb			11.2	275.5
N			16.4	270.3
-1 E. Line of Oak Bottom			16.8	269.9
curve from pcc on N. 3 Parts. 22.96 on S, 32.14 on N. Sec G. See sketch = pcc on N Line				
-33 Bottom			24.7	262.0
-21			19.1	267.6
-13			15.0	271.7
N			8.5	278.2
+7			5.3	281.4
cb			5.4	281.3
1/4			4.8	281.9
℄			4.7	282.0
1/4			4.4	282.3
cb			4.5	282.2
+3			4.3	282.4
+6			3.1	283.6
S			2.8	283.9
Sec I				
S			1.9	284.8
cb			2.5	284.2
+5			4.7	282.0
1/4			5.0	281.7
℄			4.9	281.8

	+	HI 286.73	−	Elev
1/4			5.2	281.5
cb			5.6	281.1
N			6.0	280.7
+20 Top of Bank. Breaks Ave.			6.7	280.0
+25			8.8	277.9
		Sec 2		
−15			6.7	280.0
N			6.4	280.3
cb			5.8	280.9
1/4			5.5	281.2
℄			5.4	281.3
1/4			5.8	280.9
+3			5.5	281.2
+6			2.2	284.5
cb			1.8	284.9
+5			1.2	285.5
S			1.3	285.4
		Sec 3 P.T. = 00		
S			1.0	285.7
cb			1.2	285.5
+1			5.8	280.9
1/4			6.2	280.5
℄			5.9	280.8
1/4			6.1	280.6
cb			6.6	280.1
N			7.0	279.7

	+	HI 286.73	−	Elev
+20			7.4	279.3
		0+50		
−20			8.0	278.7
N			7.5	279.2
cb			6.8	279.9
1/4			6.6	280.1
1/4			6.4	280.3
℄			6.4	280.3
+5			6.7	280.0
1/4			6.7	280.0
+5			6.1	280.6
cb			3.0	283.7
+5			2.4	284.3
S			2.0	284.7
		0+91		
S			3.7	283.0
cb			4.5	282.2
+2			6.9	279.8
1/4			7.1	279.6
℄			7.2	279.5
1/4			7.2	279.5
+3			7.4	279.3
cb			8.0	278.7
N			8.3	278.4
+20			9.2	277.5

	+	HI 286.73	−	Elev
		0+98		
-20			9.3	277.4
N			8.2	278.5
cb			8.0	278.7
1/4			7.4	279.3
℄			7.3	279.4
1/4			7.2	279.5
cb			7.3	279.4
+7			6.8	279.9
S			4.4	282.3
		1+00		
S			6.8	279.9
cb			7.3	279.4
1/4			7.3	279.4
℄			7.4	279.3
1/4			7.4	279.3
cb			8.0	278.7
N			8.3	278.4
		1+18		
N			8.9	277.8
cb			8.3	278.4
1/4			7.9	278.8
℄			7.4	279.3
+5			7.1	279.6
1/4			7.1	279.6
cb			7.4	279.3
TP	5.54	285.23	7.04	279.69

	+	HI 285.23	−	Elev
+3			5.4	279.8
S			5.6	279.6
		1+23		
S			4.8	280.4
+7			5.3	279.9
cb			5.8	279.4
+4			5.7	279.5
1/4			5.6	279.6
+3			5.6	279.6
℄			6.2	279.0
+5			6.7	278.5
1/4			6.8	278.4
cb			7.2	278.0
N			7.3	277.9
+20			8.3	276.9
		1+30		
-10 Top slope			8.6	276.6
N			8.1	277.1
cb			7.1	278.1
1/4			6.7	278.5
+3			6.9	278.3
℄			6.3	278.9
+6			5.6	279.6
1/4			5.6	279.6
cb			6.1	279.1
+3			5.2	280.0

	+	HI 285.23	−	Elev
S			4.6	280.6
		1+38		
S			4.6	280.6
cb			5.5	279.7
+5			5.6	279.6
1/4			5.4	279.8
+2			5.5	279.7
℄			6.0	279.2
1/4			6.7	278.5
+2			7.1	278.1
cb			8.3	276.9
+5			10.7	274.5
N			11.8	273.4
+10			13.1	272.1
+20			14.7	270.5
		1+45 W. Line Alley		
−24			18.8	266.4
−13			17.3	267.9
−8			15.9	269.3
N			14.5	270.7
+5			11.8	273.4
cb			10.7	274.5
+2			9.2	276.0
1/4			7.3	277.9
+3			6.3	278.9
℄			5.9	279.3

	+	HI 285.23	−	Elev
+6			5.3	279.9
1/4			5.4	279.8
cb			5.3	279.9
S			4.5	280.7
		1+55		
S			3.6	281.6
+1			4.8	280.4
cb			5.3	279.9
℄			5.3	279.9
℄			5.8	279.4
+5			6.3	278.9
1/4			7.9	277.3
cb			10.9	274.3
+3			12.9	272.3
N			17.7	267.5
+5 Bottom Wash			20.0	265.2
+20 " "			23.0	262.2
+27 Bottom Wash			26.3	258.9
		1+65 P.C of curve E Line Alley on North		See Sketch Page 68
−23			19.8	265.4
−12			17.4	267.8
N			15.4	269.8
+5			13.4	271.8
+8			12.3	272.9
cb			10.9	274.3
1/4			6.9	278.8

	+	HI 285.23	−	Elev.
+3			5.5	279.7
℄			5.2	280.0
+3			4.9	280.3
¼			5.0	280.2
○6			4.9	280.3
S			3.6	281.6
		1+77		
S			3.6	281.6
+10			4.5	280.7
+15			4.9	280.3
+20			4.5	280.7
+33			5.0	280.2
+45			10.1	275.1
+50			10.6	274.6
+51 80 N Line			10.6	274.6
+30			13.8	271.4
		2+00		
30' out			6.8	278.4
15 out			6.1	279.1
-56 N Line			4.9	280.3
-50			4.4	280.8
-42			4.6	280.6
-35			3.2	282.0
-20			2.9	282.3
-15			3.1	282.1
-9			2.4	282.8

	+	HI 285.23	−	Elev	67.20
					75
S			1.9	283.3	
TP	10.41	292.65	2.96	282.47	
			2+25.30 N Line Dahlia		
S			7.1	285.6	
+9			7.3	277.9	
+12			8.0	277.2	
+17			7.6	277.6	
+40			8.1	284.6	
+50			8.9	276.8	
+60			8.8	276.4	
+67.70 N Line			9.0	283.7	
13'00 +			9.9	275.8	
T.P.	2.36	291.25	3.79	288.89	
Check out on Starting BM			3.76	287.49	

Bill Bliss
March 9-1929

X-Section Poplar Street from the E. Line of Snowdrop to the W. Line of Oak.

	+	H.I.	−	Elev	
BM NW 1" Pipe Poplar x Oak	6.60	294.07		287.47	80' St 14' CBS 13 1/95
			0+00 E. Line Snowdrop		
N		(294.1)	4.1	290.0	
+11			4.2	289.9	
CL			5.6	288.5	
+1			5.6	288.5	
1/4			5.8	288.3	
+2 E dge			5.8	288.3	
℄			5.8	288.3	
+8			5.8	288.3	
+12 Edg.			6.2	287.9	
1/4			6.2	287.9	
+12 Edge	Approx		6.7	287.4	
CL			6.6	287.5	
+2			6.3	287.8	
S			6.1	288.0	
			0+50		
S			5.9	288.2	
+10			5.7	288.4	
+12			6.2	287.9	
CL			6.3	287.8	
+1 Edge			6.3	287.8	
1/4			5.9	288.2	
+1 Edge			5.9	288.2	
+10			5.3	288.8	
℄			5.9	288.7	

Plotted 5-6-29 C.B.H.

	+	H.I. 294.07	−	Elev
+10			5.9	288.7
1/4			5.5	288.6
+12			5.6	288.5
CL			5.5	288.6
+2			4.0	290.1
N			3.8	290.3
		1+00		
N			3.7	290.4
+12			4.2	289.9
CL			5.2	288.9
+1 Edge			5.3	288.8
1/4 "			5.3	288.8
+2			5.3	288.8
℄			5.2	288.9
+12 Edge			5.6	288.5
1/4			5.6	288.5
+12			6.1	288.0
CL			6.1	288.0
+2			6.0	288.1
+4			5.5	288.6
S			5.2	288.9
		1+25 W. Line of		
S			5.2	288.9
+10			5.2	288.9
+12			6.0	288.1
+13 Edge			6.0	288.1

	+	HI 299.07	−	Elev
cb			5.9	288.2
1/4			5.6	288.5
+1			5.6	288.5
℄			5.3	288.8
+10			5.1	289.0
1/4			5.1	289.0
+12 Edge			5.3	288.8
cb			5.3	288.8
+2			4.4	289.7
N			3.4	290.7
		1+25 ℄ of		on South
N			3.8	290.3
+12			4.1	290.0
cb			5.3	288.8
+1			5.3	288.8
1/4			5.1	289.0
+3			5.1	289.0
℄			5.3	288.8
+12 Edge			5.6	288.5
1/4			5.6	288.5
cb			5.7	288.4
+1			5.7	288.4
S			5.3	288.8
		1+50 E. Line		
S			5.0	289.1
+10			5.2	288.9

77

	+	HI 299.07	−	Elev
+12			5.6	288.5
+13 Edge			5.8	288.3
cb			5.8	288.3
1/4			5.4	288.7
+1 Edge			5.9	288.7
℄			4.9	289.2
+10 Edge			5.1	289.0
1/4			5.1	289.0
+12			5.1	289.0
cb			5.0	289.1
+2			4.1	290.0
N			3.9	290.2
		2+00		
N			3.4	290.7
+12			4.2	289.9
cb			5.0	289.1
+1 Edge			5.1	289.0
1/4			5.2	288.9
+3 Edge			5.0	289.1
+8			4.6	289.5
℄			5.0	289.1
+12 Edge			5.3	288.8
1/4			5.3	288.8
cb			5.6	288.5
+1 Edge			5.6	288.5
1			5.6	288.5

	+	H.I. 294.07	−	Elev
+4			5.1	289.0
S			4.8	289.3
		2+50		
S			4.9	289.2
+12			4.9	289.2
+13 Edge			5.6	288.5
cb			5.6	288.5
1/4			5.3	288.8
+1 Edge			5.2	288.9
℄			4.5	289.6
+5			4.4	289.7
+10 Edge			5.0	289.1
1/4			5.1	289.0
+12			5.2	288.9
cb			5.2	288.9
+3			3.9	290.2
N			3.8	290.3
		3+00		
N			4.0	290.1
+11			4.4	289.7
cb			5.3	288.8
+1			5.3	288.8
1/4			5.2	288.9
+3 E			5.1	289.0
+8			4.7	289.4
℄			4.8	289.3

	+	H.I. 294.07	−	Elev
+11			5.3	288.8
1/4			5.3	288.8
cb			5.6	288.5
+1			5.6	288.5
+2			4.9	289.2
S			4.9	289.2
		3+30		
S			4.5	289.6
+10			4.9	289.2
+13			5.7	288.4
cb			5.7	288.4
1/4			5.4	288.7
+1 E			5.4	288.7
℄			5.0	289.1
+5			4.8	289.3
+10			5.2	288.9
1/4			5.2	288.9
+12			5.5	288.6
cb			5.5	288.6
+1			5.5	288.6
+3			4.2	289.9
N			3.5	290.6
		3+50		
N			4.4	289.7
+12			4.8	289.3
cb + Paving			5.6	288.5

	+	HI 294.07	−	Elev
1/4 + Paving			5.4	288.7
+3			5.2	288.9
+8			4.9	289.2
℄			5.0	289.1
+11			5.6	288.5
1/4			5.6	288.5
cb			6.0	288.1
+1 Paving			6.0	288.1
+4			5.4	288.7
S			5.3	288.8
			4+00	
S			6.1	288.0
+11			6.1	288.0
+12			6.7	287.4
+13 Paving			6.7	287.4
cb			6.7	287.4
1/4			6.4	287.7
+1 Paving			6.4	287.7
+8			6.1	288.0
℄			5.6	288.5
+5			5.6	288.5
+10 Paving			6.0	288.1
1/4			6.1	288.0
cb + Paving			6.3	287.8
+1			6.3	287.8
+2			5.3	288.8

	+	HI 294.07	−	Elev
N			5.1	289.0
			4+50	
N			5.7	288.4
+12			6.4	288.7
cb + Paving			7.0	287.1
1/4			6.8	
+3 Paving			6.8	
+8			6.5	
℄			6.6	287.5
+11 Paving			7.2	
1/4			7.2	
cb			7.4	
+1 Paving			7.5	286.6
+3			7.0	
S			6.9	287.2
			4+75 35. W Line of Canon N	
S			7.6	286.5
+11			7.6	
+13			7.9	
cb			7.8	
1/4			7.4	
+12 Paving			7.5	286.6
℄			7.0	287.0
+5			6.8	
+10 Paving			7.1	
1/4			7.1	

	+	HI	−	Elev
		294.07		
cb + Paving			7.3	286.8
+ 2			6.4	
+ N			6.9	287.7
Check out on BM. N.W. 1" Pipe				
+ Poplar + Oak.			6.60	287.47

IMPROVED TABLES

AND

INFORMATION

TABLE VI (continued)
SINES, COSINES, TANGENTS, COTANGENTS (continued)

deg.	sin 0′	tan 0′	sin 10′	tan 10′	sin 20′	tan 20′	sin 30′	tan 30′	sin 40′	tan 40′	sin 50′	tan 50′	deg.
46	7193	1.0355	7214	1.0416	7234	1.0477	7254	1.0533	7274	1.0599	7294	1.0661	43
47	314	.0724	333	.0786	353	.0850	373	.0913	392	.0977	412	.1041	42
48	431	.1106	451	.1171	470	.1237	490	.1303	509	.1369	528	.1436	41
49	547	.1504	566	.1571	585	.1640	604	.1708	623	.1778	642	.1847	40
50	660	1.1918	7679	1.1988	7698	1.2059	7716	1.2131	7735	1.2203	7753	1.2276	39
51	771	.2349	790	.2423	808	.2497	826	.2572	844	.2647	862	.2723	38
52	880	.2799	898	.2876	916	.2954	934	.3032	951	.3111	969	.3190	37
53	986	.3270	8004	.3351	8021	.3452	8039	.3514	8056	.3597	8073	.3680	36
54	8090	.3764	107	.3848	124	.3934	141	.4019	158	.4106	175	.4193	35
55	192	.4281	208	.4370	225	.4460	241	.4550	258	.4641	274	.4733	34
56	290	.4826	307	.4919	323	.5013	339	.5108	355	5204	371	.5301	33
57	387	.5399	403	.5497	418	.5597	434	.5697	450	5798	465	.5900	32
58	480	.6003	496	.6107	511	.6212	526	.6319	542	6426	557	.6534	31
59	572	.6643	587	.6753	601	.6864	616	.6977	631	.7090	646	.7205	30
60	660	1.7321	8675	1.7437	8689	1.7556	8704	1.7675	8718	1.7797	8732	1.7917	29
61	746	.8040	760	.8165	774	.8291	788	.8418	802	.8546	816	.8676	28
62	829	.8807	843	.8940	857	.9074	870	.9210	884	.9347	897	.9486	27
63	910	.9626	923	.9768	936	.9912	949	2.0057	962	2.0204	975	2.0353	26
64	988	2.0503	9001	2.0655	9013	2.0809	9026	.0965	9038	.1123	9051	.1283	25
65	9063	.1445	075	.1609	088	.1775	100	.1943	112	.2113	124	.2286	24
66	135	.2460	147	.2637	159	.2817	171	.2998	182	3183	194	.3369	23
67	205	.3559	216	.3750	228	.3945	239	.4142	250	.4342	261	.4545	22
68	272	.4751	283	.4960	293	.5172	304	.5386	315	.5605	325	.5826	21
69	336	.6051	346	.6279	356	.6511	367	.6746	377	.6985	387	.7228	20
70	397	2.7475	9407	2.7725	9417	2.7980	9426	2.8239	9436	2.8502	9446	2.8770	19
71	455	.9042	465	.9319	474	.9600	483	.9887	492	3.0178	502	3.0475	18
72	511	3.0777	520	3.1084	528	3.1397	537	3.1716	546	.2041	555	.2371	17
73	563	.2709	572	.3052	580	.3402	588	.3759	596	.4124	605	.4495	16
74	613	.4874	621	.5261	628	.5656	636	.6059	644	.6470	652	.6891	15
75	659	.7321	667	.7760	674	.8208	681	.8657	689	.9136	696	.9617	14
76	703	4.0108	710	4.0611	717	4.1126	724	4.1653	730	4.2193	737	4.2747	13
77	744	.3315	750	.3897	757	.4494	763	.5107	769	.5736	775	.6382	12
78	781	.7046	787	.7729	793	.8430	799	.9152	805	.9894	811	5.0658	11
79	816	.1446	822	5.2257	827	5.3093	833	5.3955	838	5.4845	843	.5764	10
80	9848	5.6713	9853	5.7694	9858	5.8708	9863	5.9758	9868	6.0844	9872	6.1970	9
81	877	6.3138	881	6.4348	886	6.5606	890	6.6912	894	.8269	899	.9682	8
82	903	7.1154	907	7.2687	911	7.4287	914	7.5958	918	7.7704	922	7.9530	7
83	925	8.1443	929	8.3450	932	8.5555	936	8.7769	939	9.0098	942	9.2553	6
84	945	9.5144	948	9.7882	951	10.078	954	10.385	957	10.711	959	11.059	5
85	962	11.430	964	11.826	967	12.250	969	12.706	971	13.197	974	13.727	4
86	976	14.300	978	14.924	980	15.605	981	16.350	983	17.169	985	18.075	3
87	986	19.081	988	20.206	989	21.470	990	22.903	992	24.542	993	26.432	2
88	994	28.636	9995	31.242	9996	34.368	997	38.189	997	42.964	9998	49.104	1
89	9998	57.290	9999	68.750	9999	85.940	9999	114.58	1.000	171.88	1.000	343.77	0
deg.	60′ cos	60′ cot	50′ cos	50′ cot	40′ cos	40′ cot	30′ cos	30′ cot	20′ cos	30′ cot	10′ cos	10′ cot	deg.

TABLE VII
RODS IN FEET AND INCHES

Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches
1	16—6	21	346—6	41	676—6	61	1006—6	81	1336—6
2	33—0	22	363—0	42	693—0	62	1023—0	82	1353—0
3	49—6	23	379—6	43	709—6	63	1039—6	83	1369—6
4	66—0	24	396—0	44	726—0	64	1056—0	84	1386—0
5	82—6	25	412—6	45	742—6	65	1072—6	85	1402—6
6	99—0	26	429—0	46	759—0	66	1089—0	86	1419—0
7	115—6	27	445—6	47	775—6	67	1105—6	87	1435—6
8	132—0	28	462—0	48	792—0	68	1122—0	88	1452—0
9	148—6	29	478—6	49	808—6	69	1138—6	89	1468—6
10	165—0	30	495—0	50	825—0	70	1155—0	90	1485—0
11	181—6	31	511—6	51	841—6	71	1171—6	91	1501—6
12	198—0	32	528—0	52	858—0	72	1188—0	92	1518—0
13	214—6	33	544—6	53	874—6	73	1204—6	93	1534—6
14	231—0	34	561—0	54	891—0	74	1221—0	94	1551—0
15	247—6	35	577—6	55	907—6	75	1237—6	95	1567—6
16	264—0	36	594—0	56	924—0	76	1254—0	96	1584—0
17	280—6	37	610—6	57	940—6	77	1270—6	97	1600—6
18	297—0	38	627—0	58	957—0	78	1287—0	98	1617—0
19	313—6	39	643—6	59	973—6	79	1303—6	99	1633—6
20	330—0	40	660—0	60	990—0	80	1320—0	100	1650—0

TABLE VIII
LINKS IN FEET AND INCHES

Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches
1	0- 7.92	18	11-10.56	35	23- 1.20	52	34- 3.84	69	45- 6.48	86	56- 9.12
2	1- 3.84	19	12- 6.48	36	23- 9.12	53	34-11.76	70	46- 2.40	87	57- 5.04
3	1-11.76	20	13- 2.40	37	24- 5.04	54	35- 7.68	71	46-10.32	88	58- 0.96
4	2- 7.68	21	13-10.32	38	25- 0.96	55	36- 3.60	72	47- 6.24	89	58- 8.88
5	3- 3.60	22	14- 6.24	39	25- 8.88	56	36-11.52	73	48- 2.16	90	59- 4.80
6	3-11.52	23	15- 2.16	40	26- 4.80	57	37- 7.44	74	48-10.08	91	60- 0.72
7	4- 7.44	24	15-10.08	41	27- 0.72	58	38- 3.36	75	49- 6.00	92	60- 8.64
8	5- 3.36	25	16- 6.00	42	27- 8.64	59	38-11.28	76	50- 1.92	93	61- 4.56
9	5-11.28	26	17- 1.92	43	28- 4.56	60	39- 7.20	77	50- 9.84	94	62- 0.48
10	6- 7.20	27	17- 9.84	44	29- 0.48	61	40- 3.12	78	51- 5.76	95	62- 8.40
11	7- 3.12	28	18- 5.76	45	29- 8.40	62	40-11.04	79	52- 1.68	96	63- 4.32
12	7-11.04	29	19- 1.68	46	30- 4.32	63	41- 6.96	80	52- 9.60	97	64- 0.24
13	8- 6.96	30	19- 9.60	47	31- 0.24	64	42- 2.88	81	53- 5.52	98	64- 8.16
14	9- 2.88	31	20- 5.52	48	31- 8.16	65	42-10.80	82	54- 1.44	99	65- 4.08
15	9-10.80	32	21- 1.44	49	32- 4.08	66	43- 6.72	83	54- 9.36	100	66- .000
16	10- 6.72	33	21- 9.36	50	33- 0.00	67	44- 2.64	84	55- 5.28	101	66-7.92
17	11- 2.64	34	22- 5.28	51	33- 7.92	68	44-10.56	85	56- 1.20	102	67- 3.84

Table X.

MIDDLE ORDINATES OF RAILS

Length of Rail (feet)

C ° ′	R Feet	30 Inch	28 Inch	26 Inch	24 Inch	22 Inch	20 Inch	C °	R Feet	30 Inch	28 Inch	26 Inch	24 Inch	22 Inch	20 Inch
0–20	17189	.08	.07	.06	.05	.04	.03	8	716.8	1.88	1.64	1.42	1.20	1.01	84
0–40	8594	.16	.14	.12	.10	.08	.07	9	637.3	2.12	1.84	1.60	1.35	1.14	.94
1–0	5730	.24	.20	.18	.15	.13	.10	10	573.7	2.36	2.05	1.78	1.50	1.27	1.04
1–20	4297	.31	.27	.23	.20	.17	.13	11	521.7	2.59	2.26	1.95	1.65	1.39	1.15
1–40	3438	.39	.34	.29	.25	.21	.17	12	478.3	3.83	2.47	2.15	1.81	1.54	1.26
2–0	2865	.47	.41	.35	.30	.25	.20	13	441.7	3.05	2.66	2.30	1.96	1.66	1.36
2–20	2456	.55	.48	.41	.35	.29	.23	14	410.3	3.30	2.87	2.48	2.10	1.78	1.46
2–40	2149	.63	.55	.47	.40	.33	.27	15	383.1	3.54	3.08	2.68	2.26	1.91	1.57
3–0	1910	.71	.62	.53	.45	.38	.31	16	359.3	3.76	3.28	2.83	2.40	2.04	1.67
3–20	1719	.78	.68	.59	.50	.42	.35	17	338.3	4.00	3.48	3.02	2.57	2.16	1.78
3–40	1563	.86	.75	.65	.55	.46	.38	18	319.6	4.21	3.67	3.18	2.70	2.28	1.87
4–0	1433	.94	.82	.71	.60	.50	.42	19	302.9	4.45	3.89	3.36	2.86	2.41	1.98
4–20	1323	1.02	.89	.77	.65	.55	.45	20	287.9	4.70	4.09	3.55	3.00	2.54	2.09
4–40	1228	1.10	.96	.83	.70	.59	.48	22	262.0	5.16	4.44	3.84	3.30	2.80	2.29
5	1146	1.18	1.03	.89	.75	.63	.52	24	240.5	5.64	4.92	4.20	3.59	3.04	2.50
6	955.3	1.41	1.23	1.06	.90	.76	.62	26	222.3	6.07	5.29	4.58	3.88	3.29	2.70
7	819.0	1.65	1.44	1.24	1.05	.89	.73								

Table XI.

SHORT RADIUS CURVES

Radius Feet	Chord Feet	Central Angle	Deflection Angle	Deflection for 1 Foot
35	10	16-26	8-13	49.3
45	10	12-46	6-23	38.3
50	15	17-16	8-38	34.5
60	15	14-22	7-11	28.8
75	15	11-30	5-45	23.0
100	20	11-30	5-45	17.3
120	20	9-34	4-47	14.3
150	20	7-39	3-49	11.5
190	25	7-32	3-46	9.15
200	25	7-10	3-35	8.6
225	25	6-25	3-12	7.7
240	25	5-58	2-59	7.2
250	25	5-44	2-52	6.9
275	25	5-12	2-36	6.2
288	50	9-58	4-59	6.0
300	50	9-32	4-46	5.7
350	50	8-12	4-06	4.9
376	50	7-40	3-50	4.6
400	50	7-10	3-35	4.3
410	50	7-00	3-30	4.2

To find length of curve divide angle from P. C. to P. T. by central angle of chord and multiply by length of chord.

Table XII.

INCLINED DISTANCE OF 100 FT. REDUCED TO HORIZONTAL

Slope	Horizontal Distance	Correction	Rise Per Foot	Slope	Horizontal Distance	Correction	Rise Per Foot
0°00′	100.000	0.000	0.000	8°00′	99.027	0.973	0.139
15′	99.999	0.001	0.004	15′	98.965	1.035	0.143
30′	99.996	0.004	0.009	30′	98.902	1.098	0.148
45′	99.991	0.009	0.013	45′	98.836	1.164	0.152
1 00	99.985	0.015	0.017	9 00	98.769	1.231	0.156
15	99.976	0.024	0.022	15	98.700	1.300	0.161
30	99.966	0.034	0.026	30	98.629	1.371	0.165
45	99.953	0.047	0.031	45	98.556	1.444	0.169
2 00	99.939	0.061	0.035	10 00	98.481	1.519	0.174
15	99.923	0.077	0.039	15	98.404	1.596	0.178
30	99.905	0.095	0.044	30	98.325	1.675	0.182
45	99.885	0.115	0.048	45	98.245	1.755	0.187
3 00	99.863	0.137	0.052	11 00	98.163	1.837	0.191
15	99.839	0.161	0.057	15	98.079	1.921	0.195
30	99.813	0.187	0.061	30	97.992	2.008	0.199
45	99.786	0.214	0.065	45	97.905	2.095	0.204
4 00	99.756	0.244	0.070	12 00	97.815	2.185	0.208
15	99.725	0.275	0.074	15	97.723	2.277	0.212
30	99.692	0.308	0.078	30	97.630	2.370	0.216
45	99.657	0.343	0.083	45	97.534	2.466	0.221
5 00	99.619	0.381	0.087	13 00	97.437	2.563	0.225
15	99.580	0.420	0.092	15	97.338	2.662	0.229
30	99.540	0.460	0.096	30	97.237	2.763	0.233
45	99.497	0.503	0.100	45	97.134	2.866	0.238
6 00	99.452	0.548	0.105	14 00	97.030	2.970	0.242
15	99.406	0.594	0.109	15	96.923	3.077	0.246
30	99.357	0.643	0.113	30	96.815	3.185	0.250
45	99.307	0.693	0.118	45	96.705	3.295	0.255
7 00	99.255	0.745	0.122	15 00	96.593	3.407	0.259
15	99.200	0.800	0.126	15	96.479	3.521	0.263
30	99.144	0.856	0.131	30	96.363	3.637	0.267
45	99.087	0.913	0.135	45	96.246	3.754	0.271

Table XIII.

MINUTES IN DECIMALS OF A DEGREE.

0 30″	.00833	10′ 30″	.17500	20′ 30″	.34167	30′ 10″	.50833	40′ 30″	.67500	50′ 10″	.84167
1 00	.01667	11 00	.18333	21 00	.35000	31 00	.51667	41 00	.68333	51 00	.85000
30	.02500	30	.19167	30	.35833	30	.52500	30	.69167	30	.85833
2 00	.03333	12 00	.20000	22 00	.36667	32 00	.53333	42 00	.70000	52 00	.86667
30	.04167	30	.20833	30	.37500	30	.54167	30	.70833	30	.87500
3 00	.05000	13 00	.21667	23 00	.38333	33 00	.55000	43 00	.71667	53 00	.88333
30	.05833	30	.22500	30	.39167	30	.55833	30	.72500	30	.89167
4 00	.06667	14 00	.23333	24 00	.40000	34 00	.56667	44 00	.73333	54 00	.90000
30	.07500	30	.24167	30	.40833	30	.57500	30	.74167	30	.90833
5 00	.08333	15 00	.25000	25 00	.41667	35 00	.58333	45 00	.75000	55 00	.91667
30	.09167	30	.25833	30	.42500	30	.59167	30	.75833	30	.92500
6 00	.10000	16 00	.26667	26 00	.43333	36 00	.60000	46 00	.76667	56 00	.93333
30	.10833	30	.27500	30	.44167	30	.60833	30	.77500	30	.94167
7 00	.11667	17 00	.28333	27 00	.45000	37 00	.61667	47 00	.78333	57 00	.95000
30	.12500	30	.29167	30	.45833	30	.62500	30	.79167	30	.95833
8 00	.13333	18 00	.30000	28 00	.46667	38 00	.63333	48 00	.80000	58 00	.96667
30	.14167	30	.30833	30	.47500	30	.64167	30	.80833	30	.97500
9 00	.15000	19 00	.31667	29 00	.48333	39 00	.65000	49 00	.81667	59 00	.98333
30	.15833	30	.32500	30	.49167	30	.65833	30	.82500	30	.99167
10 00	.16667	20 00	.33333	30 00	.50000	40 00	.66667	50 00	.83333	60 00	1.00000

0.39

2228
4
2
16.04

76
47
29

430
3.38 40
4
91.60

215 00 Break
213. Mn. Hole

115.05 S.E. Pearl + Girard
Center + Draper S.W. BD. 106.48

1121.06
91 49
29.57

1187

1711.2
1714
1695

Thorn + Marlboro = 301.82

4716 50 0.24

104° - 58' - 00
90 00
14° 58' - 00

460
07
467
08
475
08
483
07
490
07
497

.094363

2272 / 10760
9088
16720
15894
8260
4816
14446
13432
8080

2.9

12.8
32
96

481
951
0130 075

451
075
4585
075
4660
075
4735
075
4810

S 61.42 E

1233
290
1523
596
552
5196

552
04
561
09
570
09
579

108
96
204

90 - 00 - 00
25 - 39 - 00
64 - 21 - 00

2430
226
178
0.48

400 04 N
330 on East