

1316  
SEWER

LEVEL BOOK

No. 380 F



N rail Bridge

29.57

127-00-30  
63-50-15

MICROFILMED

DEC 2 1964

# 1316

Our Leather Bound Engineers Note Books are carried in the following rulings:

- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
- No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.
- No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.
- No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

We also carry the Note Books listed above, bound in extra strong Fabri-Hide (otherwise the same quality of book), which can be furnished at a somewhat lower price.

In ordering Fabri-Hide covered books, add the letter "F" to catalog number.

**THE FREDERICK POST CO.**  
*ENGINEERING and DRAFTING SUPPLIES*  
IRVING PARK STATION  
CHICAGO, ILL.



Index  
Hospital Sewer

Page  
1-16



0+00 = M#1

Profile 6<sup>th</sup> St Sowers M#1 - M#2  
 6th St Wash.  
 See P. 587

TP	449	290.10	428	2856.1
FL M#1 20 <sup>th</sup> W of M#1			1021	27989
opp. M#1			614	28396
0+00 = M#1			53	2848
0+24' ground			51	2850
0+24' S drive			491	28519
0+24' top cb			541	28469
0+37.9 = S Side Drive			557	28453
0+50			51	2850
+94			53	2848
1+09			50	2851
1+19			62	2839
1+23			95	280.6
1+25			110	279.1
1+31			145	278.6
TP	0.15	27731	1294	27716
1+39			65	27081
1+42			103	2670
1+48			129	2644
TP	0.47	26534	1244	26487
1+57			53	2600
1+58			72	258.1
1+62			103	255.0
1+70			11.5	2538
1+76			12.4	2529
1+77			142	251.1

Returning Chalk  
 1+19 to 1+31  
 1.5' east of line  
 Footings at north  
 from the low ground

265.34

0

PT	0.43	25332	1245	25289	
1+82			34	249.9	
+87			6.3	2470	
+91			71	246.2	
TP	0.06	24043	1295	24037	
+95			6.9	233.5	
2+02			9.7	230.7	
+07			10.8	229.6	
+31			11.7	228.7	
+60			11.5	228.9	
+81.62 = M#1			11.4	229.0	2481.62
TP			11.34	229.09	
TP	276	23185		229.10	
0+36			4.0	227.8	3+17.62
+52			3.4	228.4	3+38.62
+76			4.3	227.6	3+57.62
+85			7.1	224.8	3+66.62
1+00			8.6	223.2	3+81.62
TP	0.16	21940	1261	21924	
1+31			11.8	207.6	4+12.62
+37			13.2	206.2	4+18.62
1+61			14.6	204.8	4+42.62
TP	0.16	20695	1261	20679	

Platted



20695

1497		1.3	2056	4+78 <sup>62</sup>
2+06		6.0	201.0	4+87 <sup>62</sup>
2+31		8.3	1986	5+12 <sup>62</sup>
2+38		9.5	1974	5+9 <sup>62</sup>
2+68		11.6	1954	5+49 <sup>62</sup>
2+69		10.7	1962	+50 <sup>62</sup>
2+88		11.8	1952	+69 <sup>62</sup>
2+95		13.3	1938	+76 <sup>62</sup>
T <sub>10</sub>	204	19647	1252	19443
3+1450	= MH 3	661	18986	5+96 <sup>62</sup>
	MH. 3-MH. 4	0+00 = MH 3		
0+17		5.0	1915	6+13 <sup>62</sup>
+25		4.8	1917	6+21 <sup>62</sup>
+45		6.0	1905	6+41 <sup>62</sup>
+55		7.4	1891	6+51 <sup>62</sup>
+65		8.7	1878	6+61 <sup>62</sup>
+88		10.6	1859	6+76 <sup>62</sup>
+95		13.5	1830	6+91 <sup>62</sup>
1+36		13.8	1827	7+02 <sup>62</sup>
1+89		10.9	1856	7+05 <sup>62</sup>
1+21 <sup>25</sup>	008 = MH 4 18667	9.88	18659	7+17 <sup>37</sup>

0+00 = MH. 4  
MH 44 to MH 45  
18667

②

2

0+10		1.8	1849	7+27 <sup>37</sup>
+17		3.6	183.1	7+34 <sup>37</sup>
+20		5.8	180.9	7+37 <sup>37</sup>
+23		6.2	180.5	7+40 <sup>37</sup>
+48		7.3	179.4	7+65 <sup>37</sup>
+61		5.8	180.9	7+78 <sup>37</sup>
+70		5.5	181.2	7+87 <sup>37</sup>
+91		6.2	180.5	8+08 <sup>37</sup>
+95		6.8	179.9	8+12 <sup>37</sup>
1+00		6.9	179.8	8+17 <sup>37</sup>
1+10		8.6	178.1	8+27 <sup>37</sup>
1+25		9.9	176.8	8+42 <sup>37</sup>
+50		12.5	174.2	8+67 <sup>37</sup>
T <sub>10</sub>	093	17574	11.86	174.81
1+77		3.2	172.5	8+94 <sup>37</sup>
1+95		5.5	170.2	9+12 <sup>37</sup>
2+25		6.5	169.2	9+42 <sup>37</sup>
2+60		8.2	167.5	9+77 <sup>37</sup>
2+87		9.7	166.0	10+04 <sup>37</sup>
3+00		9.9	165.8	10+17 <sup>37</sup>
3+15		10.7	165.0	10+32 <sup>37</sup>
3+20		10.4	165.3	10.37 <sup>37</sup>
3+35		11.3	164.4	10+52 <sup>37</sup>
3+38	Platted.	12.4	163.3	10+55 <sup>37</sup>



MH 4 to MH 5

17574

3+47			14.0	161.7	10+62 <sup>2</sup>
TP	874	17263	1185	16389	
3+54 <sup>40</sup>	=MH 5		1205	16058	10+71 <sup>2</sup>
TP	1216	19433	046	17217	
TP	1149	19529	053	18388	
TP	1302	20779	052	19477	
TP	1249	22011	017	20762	
TP	1289	23255	045	21966	
TP	1279	24450	054	23201	
TP	1223	25693	010	24470	
TP	1269	26868	094	25599	
TP	1294	28151	011	26857	
TP	1030	29021	160	27991	
BM Beginning			621	28400	

MH 17 to MH 16 20 P 5

BM 5+9 W 3

BM	763	28665		28402	
TP	074	28508	231	28434	
	0+00 = MH 17		32	281.9	1+82 <sup>5</sup>
	0+27.2	E line 6 <sup>1</sup> st	31	282.0	2+10 <sup>20</sup>
	+59		28	282.3	2+41 <sup>50</sup>
	1+00		28	282.3	2+82 <sup>5</sup>
	1+11		35	281.6	2+93 <sup>5</sup>
	+12		44	280.7	2+98 <sup>5</sup>
	+20		53	279.8	3+02 <sup>5</sup>
	+23		76	277.5	3+05 <sup>4</sup>
	+26		88	276.3	3+08 <sup>5</sup>
	+31		113	273.8	3+13 <sup>15</sup>
	+41		185	271.6	3+23 <sup>5</sup>
	1+52		189	266.2	3+34 <sup>5</sup>
TP	055	27258	1305	27203	
TP	050	26057	1249	26009	
TP	054	24973	1240	24819	
H54			12	2475	3+31 <sup>5</sup>
+57			20	2467	3+39 <sup>5</sup>
+78			24	2463	3+60 <sup>2</sup>
2+03			28	2459	3+85 <sup>5</sup>
2+10 <sup>3</sup>			10	2477	3+92 <sup>5</sup>
2+18			28	2459	4+00 <sup>5</sup>
TP	247	23845	1275	23598	
TP	087	22705	1227	22618	

Platted



MH 176 MH 16

227.05

2+45			20	225.0	4+27 <sup>5</sup>
+47			4.7	222.3	4+29 <sup>5</sup>
+54			6.7	220.3	4+36 <sup>5</sup>
+57			9.2	217.8	4+39 <sup>5</sup>
+62			9.7	217.3	4+44 <sup>5</sup>
+85			13.0	214.0	4+67 <sup>5</sup>
TP	180	216.11	1274	214.31	
2+94			2.6	213.4	4+76 <sup>5</sup>
2+99 = MH 16			365	212.46	4+81 <sup>5</sup>
MH 16 to MH 3 0+00 = MH 16					
0+48			6.7	209.4	5+29 <sup>5</sup>
+74			9.5	206.6	5+55 <sup>5</sup>
TP	121	207.73	959	206.52	
0+84			2.8	204.9	5+65 <sup>5</sup>
1+85			4.2	203.5	5+86 <sup>5</sup>
1+21			5.4	202.3	5+02 <sup>5</sup>
+36			6.6	201.1	6+17 <sup>5</sup>
+51			7.4	200.3	6+32 <sup>5</sup>
+60			6.4	201.3	6+41 <sup>5</sup>
+68			7.2	200.5	6+49 <sup>5</sup>
1+85			9.2	198.5	6+66 <sup>5</sup>
1+87			10.5	197.2	6+68 <sup>5</sup>
2+08			11.7	196.0	6+81 <sup>5</sup>
2+08			12.5	195.2	6+89 <sup>5</sup>
2+18			12.9	194.8	6+99 <sup>5</sup>

MH 16 & MH 3

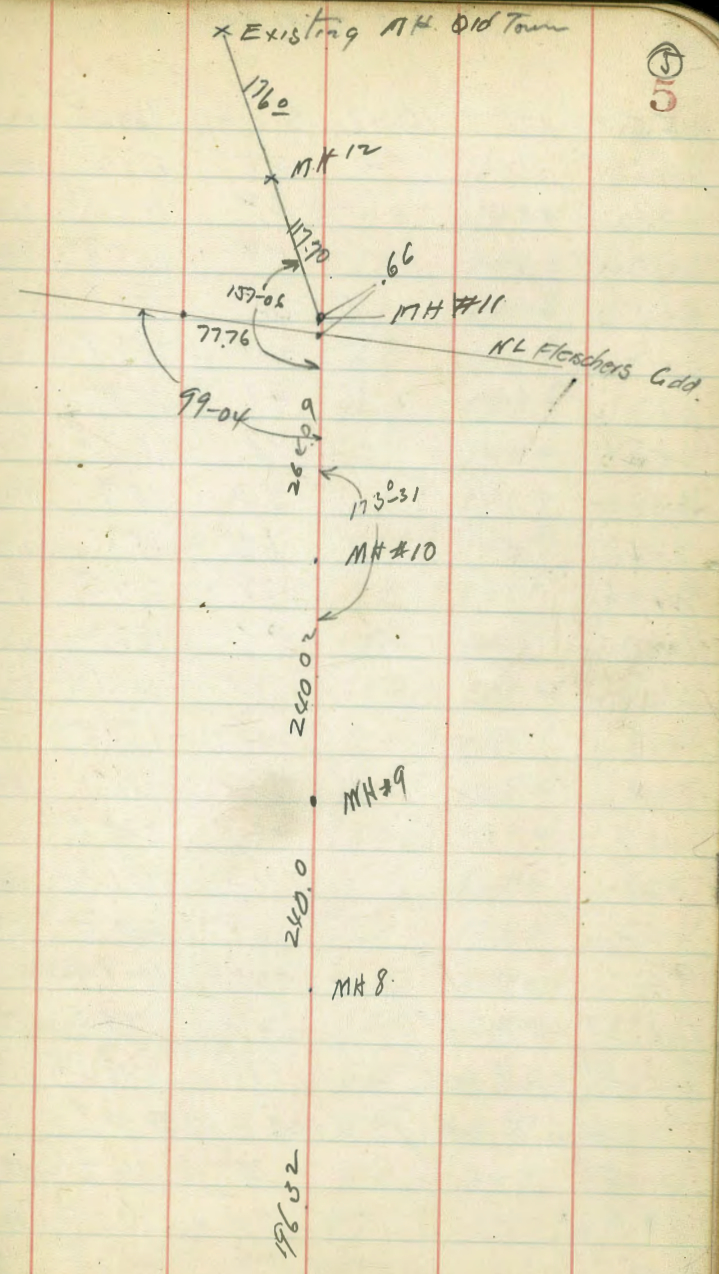
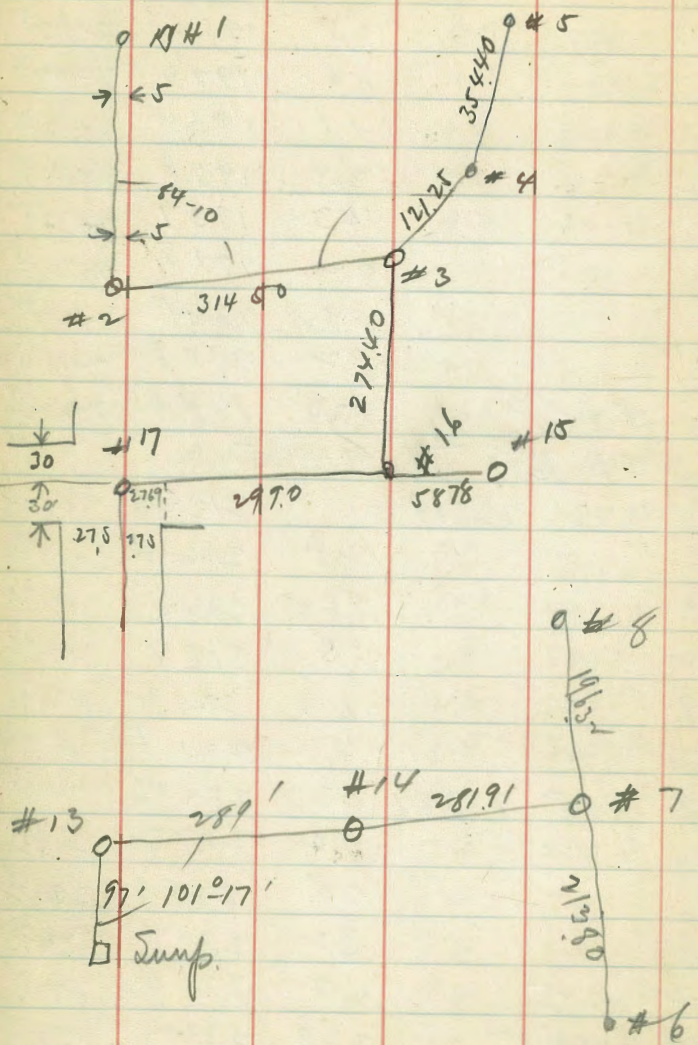
207.73

④  
4

TP	265	198.05	1233	195.4	
2+22			2.5	195.5	7+03 <sup>5</sup>
2+26			0.6	197.4	7+07 <sup>5</sup>
2+31			1.1	196.9	7+12 <sup>5</sup>
2+40			2.4	195.6	7+21 <sup>5</sup>
2+50			4.3	193.7	7+31 <sup>5</sup>
2+61			8.2	189.5	7+42 <sup>5</sup>
2+66			8.9	189.1	7+47 <sup>5</sup>
2+70			8.2	189.8	7+51 <sup>5</sup>
2+74			8.20	189.85	7+55 <sup>5</sup>
MH 3 to MH 16					
0+5828					
MH 16	1273	225.19		212.46	0+00
0+57			12.8	212.4	+01 <sup>75</sup>
0+50			8.6	216.6	+08 <sup>75</sup>
0+42			6.5	218.7	+16 <sup>75</sup>
0+37			4.0	221.2	+21 <sup>75</sup>
0+33			4.1	221.1	+25 <sup>75</sup>
TP	1205	236.91	033	224.86	
0+23			9.2	227.7	+35 <sup>75</sup>
0+11			7.9	229.0	+47 <sup>75</sup>
0+06			3.2	233.7	+52 <sup>75</sup>
0+02			2.0	234.9	+56 <sup>75</sup>
0+00 = MH 15			3.20	233.71	+58 <sup>75</sup>

Platted







MK #5 & MK #6

#6 & #7

6  
6

MK 5	171	15229	16058	10771 <sup>27</sup>
0+06		2.1	1602	10+77 <sup>27</sup>
0+11		3.2	159.1	10+82 <sup>27</sup>
0+13		5.4	1569	10+84 <sup>27</sup>
0+14		3.5	1588	10+85 <sup>27</sup>
0+16		2.4	1589	10+87 <sup>27</sup>
0+20		4.1	1582	10+91 <sup>27</sup>
0+34		48	157.5	11+05 <sup>27</sup>
0+46		5.3	157	11+17 <sup>27</sup>
0+54		6.3	156	11+25 <sup>27</sup>
0+76		7.8	154.5	11+47 <sup>27</sup>
1+00		9.1	153.2	11+71 <sup>27</sup>
1+12		10.1	152.2	11+83 <sup>27</sup>
1+18		10.8	151.5	11+89 <sup>27</sup>
1+19		12.2	150.1	11+90 <sup>27</sup>
1+27		13.2	149.1	11+98 <sup>27</sup>
1+28		11.3	151.0	11+99 <sup>27</sup>
1+32		11.1	151.2	12+03 <sup>27</sup>
TP	090	1507.3	1246	149.83
1+62 <sup>40</sup>	=MK 6	2.2	148.5	12+34 <sup>27</sup>
1+62 <sup>40</sup>	Hub for Bm.	1.88	148.85	
MK 6 & MK 7	-	0+00	=MK #6	
0+25		3.5	147.2	12+59 <sup>27</sup>
0+26		4.8	145.9	12+60 <sup>27</sup>
0+30		4.9	145.8	12+64 <sup>27</sup>
0+31		4.1	146.6	12+65 <sup>27</sup>

	15073			
0+50		5.6	145.4	12+84 <sup>27</sup>
5.2		7.3	143.4	12+86 <sup>27</sup>
5.5		6.1	144.6	12+89 <sup>27</sup>
6.8		6.1	144.6	13+02 <sup>27</sup>
7.81		6.8	143.9	13+15 <sup>27</sup>
7.83		10.1	140.6	13+17 <sup>27</sup>
7.95		12.1	140.6	13+29 <sup>27</sup>
7.96		7.5	143.2	13+30 <sup>27</sup>
1+00		7.0	143.7	13+34 <sup>27</sup>
7.15		7.9	142.8	13+49 <sup>27</sup>
7.34		8.9	141.8	13+65 <sup>27</sup>
7.65		12.3	140.4	13+99 <sup>27</sup>
7.68		10.6	140.1	14+02 <sup>27</sup>
7.72		12.3	138.4	14+06 <sup>27</sup>
7.80		13.3	137.4	14+14 <sup>27</sup>
7.82		11.1	139.6	14+16 <sup>27</sup>
2+00		12.2	138.5	14+34 <sup>27</sup>
TP	255	14065	1263	139.10
2+13 <sup>80</sup>	=MK #7	3.52	137.10	14+47 <sup>27</sup>
0+05	#7 & #8	4.5	136.1	14+52 <sup>27</sup>
7.17		5.0	135.6	14+64 <sup>27</sup>
7.40		5.7	134.9	14+87 <sup>27</sup>
7.41		4.9	135.7	14.88 <sup>27</sup>
7.47		4.9	135.7	14+94 <sup>27</sup>
7.60		4.2	136.4	15+07 <sup>27</sup>

Platted



14065			
0+76	15+23 <sup>22</sup>	47	135.9
1+00	15+47 <sup>22</sup>	59	134.7
+28	15+75 <sup>22</sup>	73	133.3
+50	15+97 <sup>22</sup>	77	132.9
+65	16+12 <sup>22</sup>	83	132.3
1+96 <sup>32</sup> = MH#8	16+44 <sup>29</sup>	91.2	131.53
MH#8 & #9 00 = MH#8			
0+25	16+69 <sup>29</sup>	98	130.8
+42	16+86 <sup>29</sup>	98	130.8
+55	16+99 <sup>29</sup>	105	130.1
+70	17+14 <sup>29</sup>	115	129.1
+72	17+16 <sup>29</sup>	119	128.7
+74	17+18 <sup>29</sup>	138	126.8
+79	17+23 <sup>29</sup>	117	128.9
+85	17+29 <sup>29</sup>	121	127.5
+90	17+34 <sup>29</sup>	148	125.8
+92	17+36 <sup>29</sup>	12.1	128.5
TP 104	129.66	1203	12962
+95	17+39 <sup>29</sup>	14	128.3
1+00	17+44 <sup>29</sup>	38	125.9
+03	17+47 <sup>29</sup>	45	125.2
1+30	17+74 <sup>29</sup>	53	124.4
+45	17+89 <sup>29</sup>	59	123.8
+52	17+96 <sup>29</sup>	48	124.9
1+60	18+04 <sup>2</sup>	40	125.7

12966			
1+70	50	1247	18+14 <sup>29</sup>
2+00	43	125.7	18+44 <sup>29</sup>
+27	64	123.3	18+71 <sup>29</sup>
2+40 = MH#9	75	122.2	18+84 <sup>29</sup>
#9 1/2 #10 00 = #9			
0+02	87	121.0	18+86 <sup>29</sup>
+05	93	120.4	18+89 <sup>29</sup>
+25	99	119.8	19+09 <sup>29</sup>
+30	96	120.1	19+14 <sup>29</sup>
+45	96	120.1	19+29 <sup>29</sup>
+47	11.8	117.9	19+31 <sup>29</sup>
+55	13.3	116.4	19+39 <sup>29</sup>
+60	12.8	116.9	19+44 <sup>29</sup>
+61	10.5	119.2	19+45 <sup>29</sup>
+70	10.9	118.8	19+54 <sup>29</sup>
+80	10.5	119.6	19+64 <sup>29</sup>
1+20	11.5	118.2	20+04 <sup>29</sup>
1+35	11.6	118.1	20+19 <sup>29</sup>
1+65	12.8	116.9	20+49 <sup>29</sup>
TP 230	119.25	1271	116.95
1+90	33	115.9	20+74 <sup>29</sup>
2+05	46	114.6	20+89 <sup>29</sup>
2+40 <sup>02</sup> MH#10	6.0	113.2	21+24 <sup>31</sup>

Platted



# 10 to # 11 00 = # 10

11925

0+10		67	1125	21+34 <sup>31</sup>
+11		81	111.1	21+35 <sup>31</sup>
+15		90	110.2	21+39 <sup>31</sup>
+16		99	109.3	21+40 <sup>31</sup>
+20		100	109.2	21+44 <sup>31</sup>
+21		77	111.5	21+45 <sup>31</sup>
+23		76	111.6	21+47 <sup>31</sup>
+33		8.1	111.1	21+57 <sup>31</sup>
+40		95	109.7	21+62 <sup>31</sup>
+50		10.9	108.3	21+74 <sup>31</sup>
+51		126	106.6	21+75 <sup>31</sup>
+58		128	106.4	21+82 <sup>31</sup>
+60		10.8	108.4	21+85 <sup>31</sup>
+70		10.4	108.8	21+94 <sup>31</sup>
+90		11.3	107.9	22+14 <sup>31</sup>
1705		12.3	106.9	22+29 <sup>31</sup>
+10		144	104.8	22+34 <sup>31</sup>
+12		14.6	104.6	22+36 <sup>31</sup>
+20		12.6	106.6	22+44 <sup>31</sup>
TP	249	10940	1234	10691
1455		47	104.7	22+79 <sup>31</sup>
1770		6.1	103.3	22+94 <sup>31</sup>
1782		5.1	104.3	23+06 <sup>31</sup>
2100		4.5	104.9	23+24 <sup>31</sup>
2+32		5.5	103.9	23+56 <sup>31</sup>
			1039	

# 10 to # 11  
10940

8

276424 = #11		713	10227	23+88 <sup>35</sup>
TP	1291	11952	249	10691
TP	1227	13179	030	11952
TP	1233	14297	115	13064
TP	1103	15304	096	14201
TP	1132	16232	204	15100
NH #5		176	16056	16058
# 11 to # 12	00 = #11			
#11	165	10393	16228	23+88 <sup>35</sup>
0+24		32	100.7	24+12 <sup>35</sup>
+31		27	101.2	24+19 <sup>35</sup>
+48		27	101.2	24+36 <sup>35</sup>
+58		30	100.9	24+46 <sup>35</sup>
+71		39	100.0	24+59 <sup>35</sup>
+77		36	100.3	24+65 <sup>35</sup>
1700		47	99.2	24+88 <sup>35</sup>
1717 <sup>20</sup> = #12		532	9861	25+06 <sup>05</sup>
# 12 to # 90 Old Town Bunker				
0+28		61	97.8	25+34 <sup>05</sup>
+29		75	96.4	25+35 <sup>05</sup>
+31		76	96.3	25+37 <sup>05</sup>
+32		63	97.6	25+38 <sup>05</sup>
+40		57	98.2	25+46 <sup>05</sup>
+57		64	97.5	25+63 <sup>05</sup>
+87	Plat	74	96.5	25+93 <sup>05</sup>



10393

1400		77	96.2	26+06 <sup>05</sup>
1427		9.0	94.9	26+33 <sup>05</sup>
1456		9.8	94.1	26+62 <sup>05</sup>
1+76 = N.H.#90		1061	9332	26+82 <sup>05</sup>

Swamp to #13		See	19.5	5 <sup>th</sup> Wash
BM	303	287.05		2840.2
T.P.	4.90	290.09	18.6	285.19
T.P.	0.11	277.44	12.76	277.33
T.P.	0.11	264.79	12.76	264.68
BM = N Side Swamp		2.02		257.77
T.P.	0.21	252.54	12.46	252.33
0+00 = N Side of Swamp		5.2		247.8
0+03		5.5		247.9
0+03.5		7.0		244.5
+08		7.8		244.7
+09		9.1		243.4
+13		9.3		243.2
+14		11.1		241.4
+16		11.2		241.3
+17		12.5		240.0
+20		13.0		239.5
T.P.	111	241.28	12.37	240.17
0+22	111	241.28	12.50	236.3
0+30			4.7	236.6

24.28

0+31			6.6	234.7	
0+31			6.6	234.7	
0+34			8.6	232.7	
0+42			9.2	232.1	
0+47			13.8	227.5	
T.P.	0.54	229.74	12.08	229.20	
0+49			30	226.7	
+55			87	221.0	
+56			99	219.8	
+58			134	216.3	
T.P.	0.78	219.73	11.79	217.95	
0+69			44	214.3	
+72			65	212.2	
+79			89	209.8	
+81			118	207.7	
T.P.	0.09	206.01	12.81	205.92	
0+97 = N.H.#13			6.0	200.0	0+97
#13 to #14					
0+00 = #13					
0+08			8.0	198.8	1+05
+13			11.9	194.1	1+10
T.P.	0.42	193.94	12.49	193.52	
0+19			3.9	190.0	1+16
+23			4.8	189.1	1+20
+25			7.6	186.3	1+22
+30			7.4	186.5	1+27
+31			6.2	187.7	1+28

79

Plotted



19394

0+50		58	188.1	1+47
+55		75	188.4	1+52
0+71		94	184.5	1+68
0+76		103	183.6	1+73
0+94		107	183.2	1+91
1+00		100	183.9	1+97
+08		8.9	185.0	2+05
1+16		9.3	184.6	2+13
1+24		11.0	182.9	2+21
1+30		13.5	180.4	2+27
TP	217	18450	1161	182.33
1+36		4.7	179.8	2+33
1+50		5.1	179.4	2+47
+54		6.5	178.0	2+51
+59		6.4	178.1	2+56
+70		7.6	176.9	2+67
+77		7.3	177.2	2+74
+98		8.2	176.3	2+87
2+86		9.0	175.5	3+03
2+87		7.9	176.6	3+04
+14		8.3	176.2	3+11
+15		9.2	175.3	3+12
+25		9.3	175.2	3+22
+62		10.1	174.4	3+59
+77		10.2	174.3	3+74
+89 = # 14		10.1	174.4	3+86

 MH # 14 & MH # 7  
 0100 = MH # 14  
 18450
10  
10

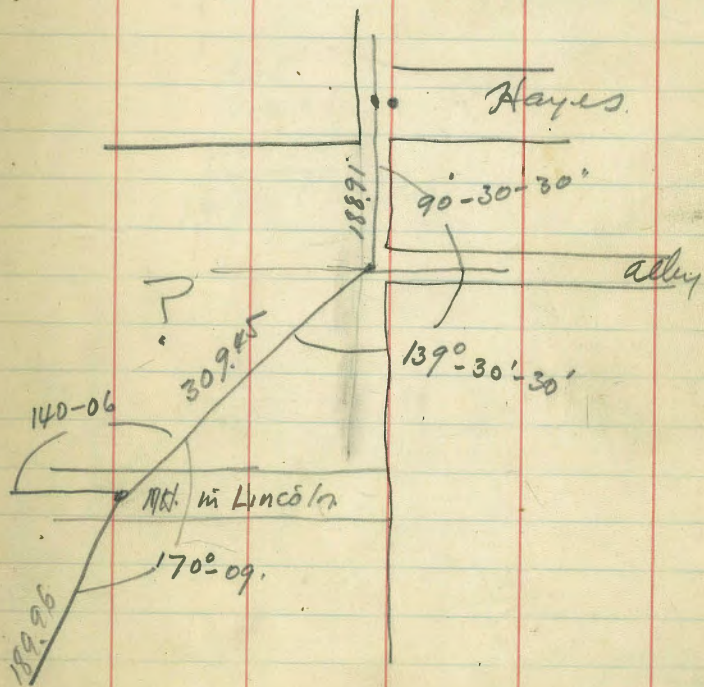
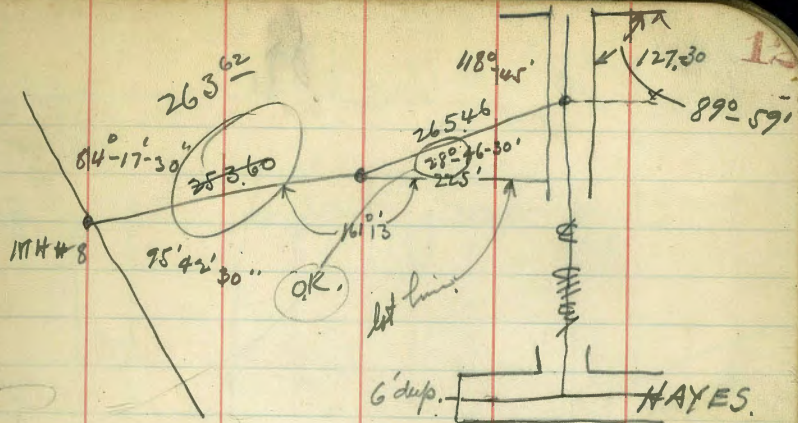
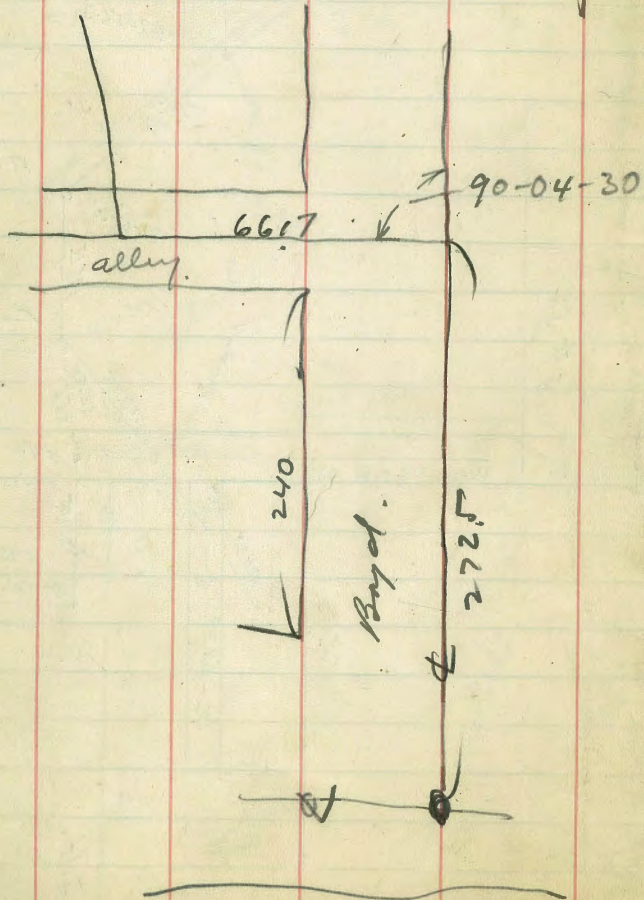
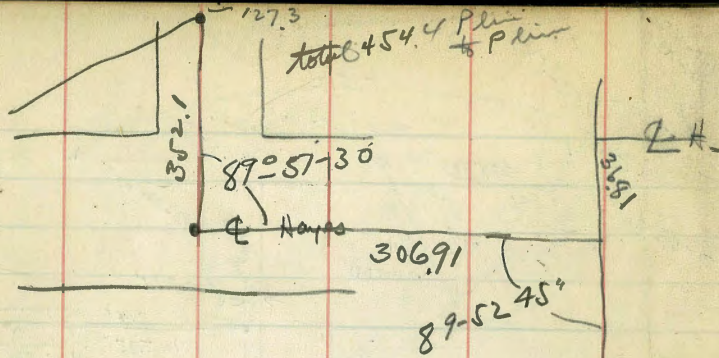
0+21		103	174.2	4+07
+24		94	175.1	4+10
+30		87	175.8	4+16
+33		98	174.7	4+19
TP	467	17690	1227	172.23
0+64		17.0	159.9	4+50
+75		18.0	158.9	4+61
TP	135	16518	1307	163.83
0+97		8.5	153.7	4+83
1+06		9.4	155.8	4+92
1+23		10.6	154.6	5+09
1+28		11.6	153.6	5+14
1+29		13.7	151.5	5+15
TP	072	15336	1254	152.64
1+35		3.2	150.2	5+21
+39		1.8	151.6	5+25
+41		1.3	152.1	5+27
+43		3.6	149.8	5+29
+57		3.9	149.5	5+43
+61		4.6	149.8	5+47
+67		4.9	148.5	5+53
+90		5.5	147.9	5+76
2+00		6.5	146.9	5+86
2+04		7.6	145.5	5+90
2+23		9.3	144.1	6+09

Plotted

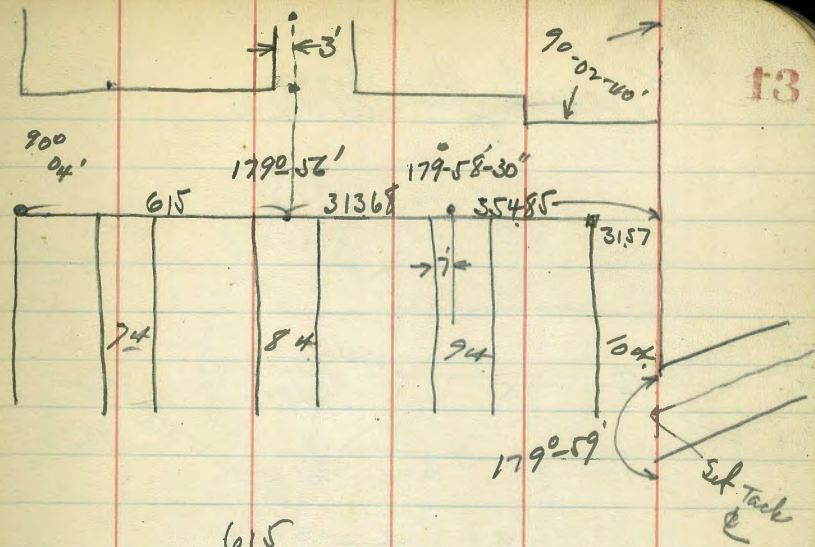












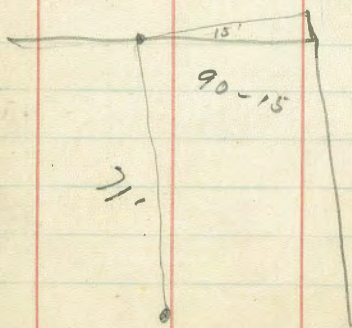
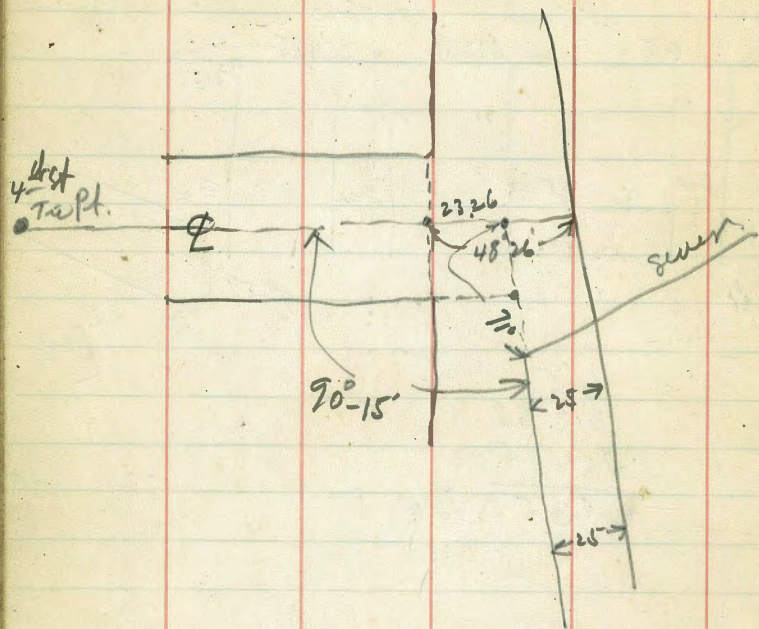
$615$   
 $31368$   
 $35485$   


---

 $1283.53$  total dist

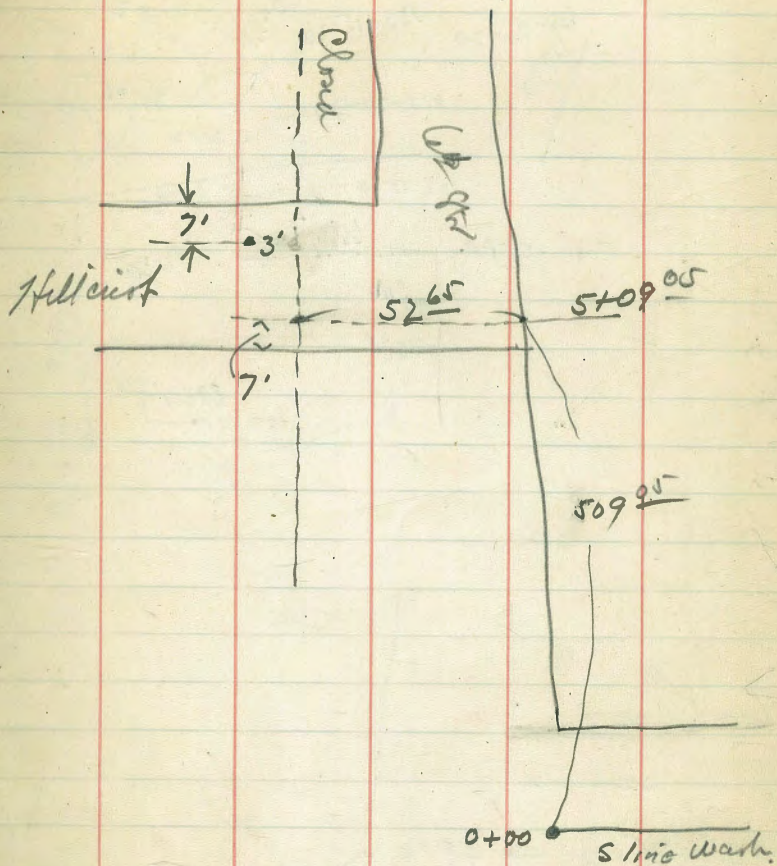


# Monticello Wm

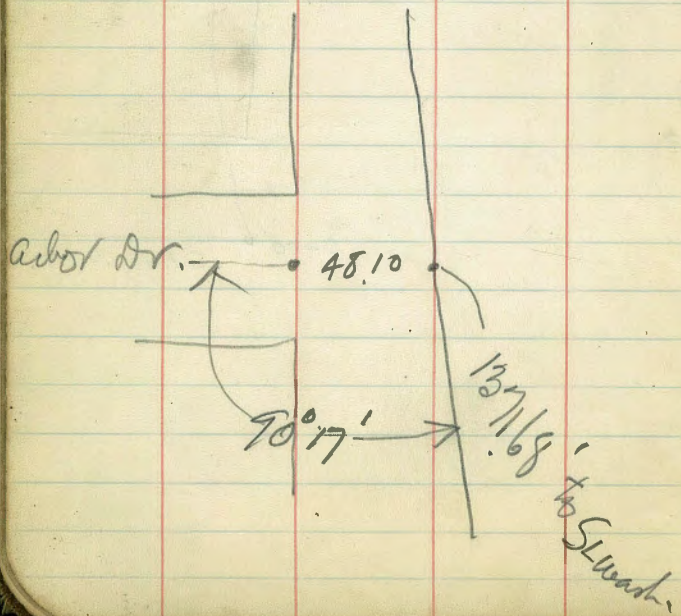
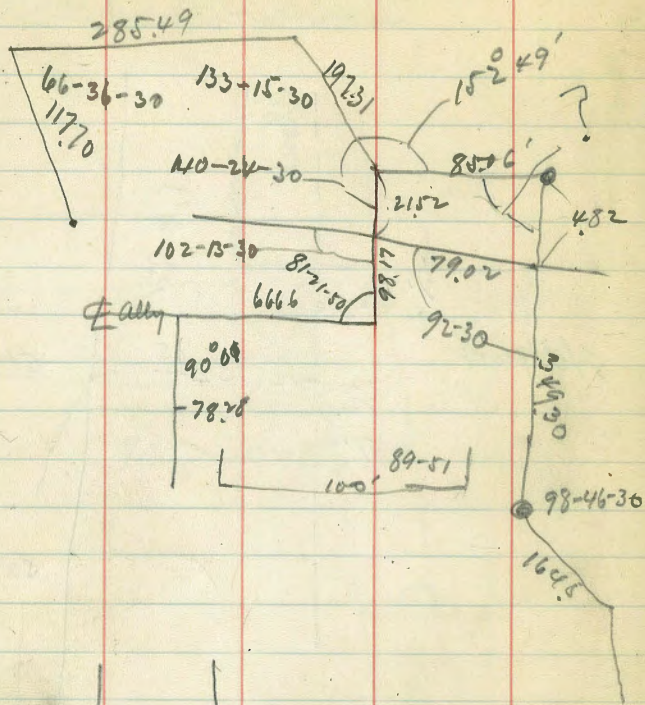


# Hillcut

14









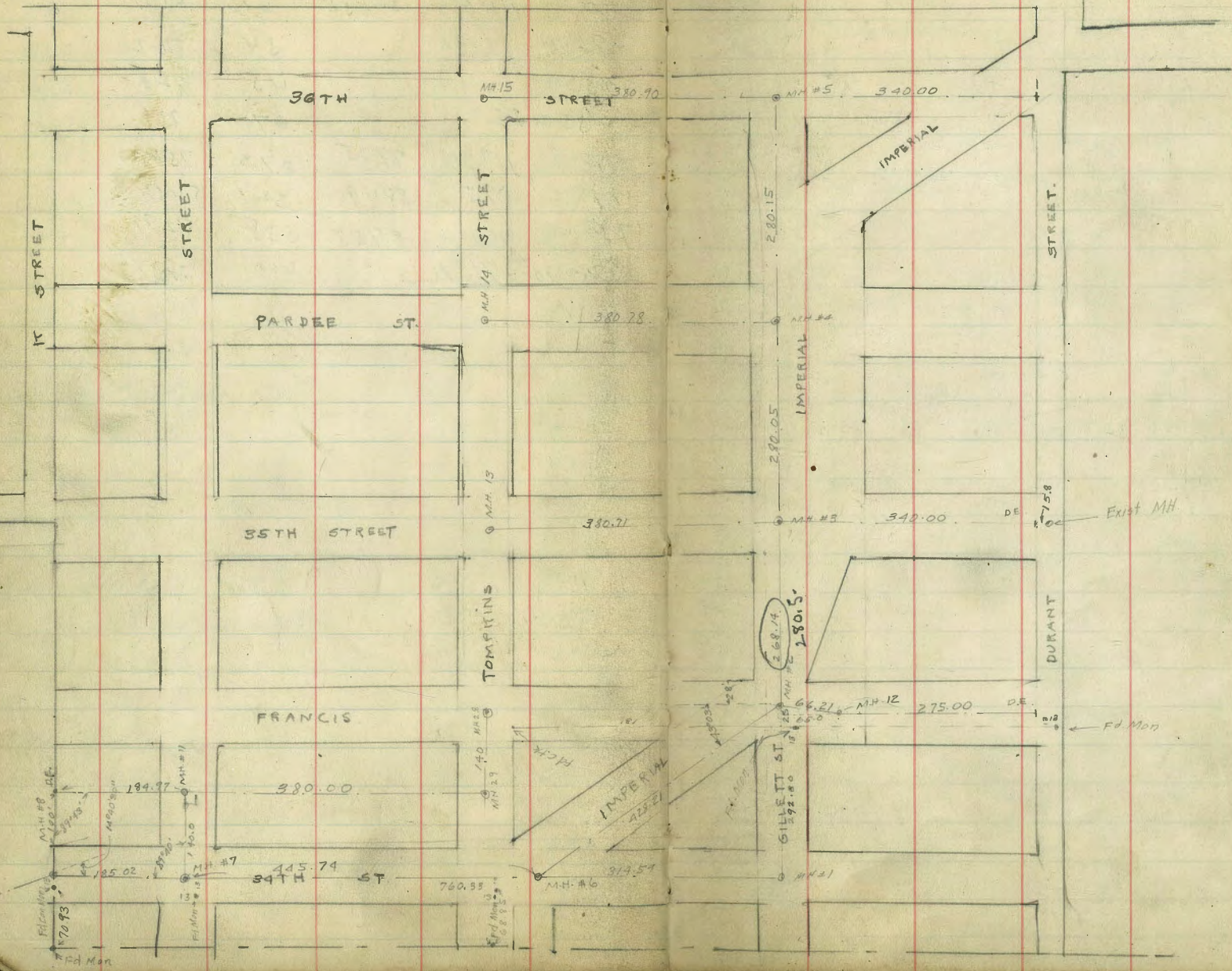
Price up 7<sup>th</sup> from Washington

00 = MH15	0458 <sup>75</sup>	1279	246.50	233.71	
0505	+66 <sup>75</sup>		74	39.71	
+13	+71 <sup>75</sup>		62	40.3	
+23	+81 <sup>75</sup>		42	42.3	
+24	+82 <sup>75</sup>		57	40.8	
+27	+85 <sup>75</sup>		82	38.3	
8' W of 0+27	Red Oak +85 <sup>75</sup>		134	33.1	
+32	+90 <sup>75</sup>		47	41.8	
+42	+100 <sup>75</sup>		20	44.5	
+46	+104 <sup>75</sup>		24	44.1	
+62	+120 <sup>75</sup>		18	44.7	
12' W of 0+62	B. B. 1+20 <sup>75</sup>		135	33.0	
+76	+134 <sup>75</sup>		19	44.6	
+86	+144 <sup>75</sup>		20	44.5	
TP.		1051	255.68	133	245.17
1+08	+158 <sup>75</sup>		119	243.8	
13' W of 1+08	B. B. 1+58 <sup>75</sup>		217	34.0	
1+32	Bambusa out. 1+90 <sup>75</sup>		154	40.3	
1+42	+200 <sup>75</sup>		148	40.9	
+52	+210 <sup>75</sup>		115	44.2	
+62	+220 <sup>75</sup>		69	48.8	
+72	+230 <sup>75</sup>		24	53.3	
TP		1172	267.25	0.15	555.3
1+76	+234 <sup>75</sup>		10.0	57.3	
1+81	+239 <sup>75</sup>		8.5	58.7	

1788			44	262.8	2746 <sup>75</sup>
TP	1146	276.55	216	650.9	
+96			34	61.2	2754 <sup>75</sup>
2763			4.5	62.8	2761 <sup>75</sup>
+55 = DE			0.7	75.8	2763 <sup>75</sup>
TP	1193	877.5	0.73	75.82	
TP	395	884.9	321	845.4	
TP	464	875.5	558	829.1	
Bm - 10 <sup>th</sup> of B. B.			440	253.15	

16











BP N rail  
Imp. 8342

BM	1.73	31.30	29.57
	M.H. 1 to	M.H. 6 to	M.H. 7 on 2 34 <sup>th</sup>
0+00 = M.H. 1		13.8	17.5
0+05		14.7	16.6
0+50		14.0	17.3
1+00		12.8	18.5
1+35		12.7	18.6
1+65		6.7	24.6
2+00		6.5	24.8
2+85		7.1	24.2
3+00		6.0	25.3
3+02 <sup>1/2</sup>	S imp. Pav	5.01	26.29
3+14 <sup>5/8</sup>	N.H. 6 on Pav	4.36	26.94
3+23 <sup>1/2</sup>	N imp. Pav.	4.16	27.14
3+60		4.4	26.9
3+75		2.0	29.3
T.P.	11.96	41.90	1.36 29.94
4+17		7.6	34.3
4+41		5.8	36.1
4+51	top S rail S.D&A	4.68	37.22
4+61 <sup>2</sup>	N rail	5.19	36.71
4+73		6.4	35.5
+95		4.0	37.9
T.P.	12.59	53.74	0.75 41.15

	53.74	
5+08	7.9	45.6
+50	3.2	50.5
+75	3.8	49.9
6+00	5.8	47.9
+36	10.8	42.9
+68	6.3	47.4
+90	0.6	53.1
T.P.	4.55	57.80
7+00	0.49	53.25
	4.0	53.8
7+60 <sup>35</sup> = M.H. 7	2.0	55.8
BM		
BM 13' N on 34 <sup>th</sup> L	2.83	54.97
M.H. 7 to M.H. 8		
0+00 = M.H. 7		
+10	2.8	55.0
+25	8.2	49.6
+44	11.9	45.7
+56	16.1	41.7
+86	8.8	49.0
1+00	8.0	49.8
+35	8.8	49.0
1+85 <sup>02</sup> = M.H. 8	3.83	53.77



57.80

M.H. 8 to M.H. 9		57.80	
0+00 = M.H. 8			
+20	2.6	55.2	
+36	6.7	51.1	
+45	9.9	47.9	
+80	11.4	46.4	
T.P. 0.48	45.46	12.82	44.98
1+00	3.3	42.2	
+26	1.8	43.7	
+55	2.4	43.1	
+70	6.5	39.0	
+90	12.5	33.0	
T.P. 4.59	37.26	12.79	32.67
2+30	7.6	29.7	
2+55 <sup>39</sup> M.H. #9	6.99	30.27	
M.H. 9 to M.H. 10			
0+00 = M.H. 9			
+25	6.5	30.6	
+60	6.5	30.8	
1+00	6.0	31.3	
1+57 <sup>59</sup> = M.H. 10	5.2	32.1	

37.26

M.H. 10 to Exist M.H. W in Alley		37.26	
0+00 = M.H. 10		32.1	
+50	5.8	31.5	
1+00	7.5	29.8	
+30	11.0	26.3	
+50	9.8	27.5	
(1+69 = Exist M.H. (grd))	9.3	28.0	
+0P	6.22	31.04	
FL	14.06	23.20	
T.P. 8.45	40.29	5.42	31.84
BM Beginning	10.70	29.59	(29.57)
M.H. 7 to M.H. 11 (E of Lot)			
=0+00			
M.H. 7	7.62	63.4	55.8
+19		6.8	56.6
+55		7.8	55.6
1+40 = M.H. 11		7.3	56.1
M.H. 11 to D.E. North			
0+00 = M.H. 11			
+30		5.3	58.1
+55		4.8	58.6
+85		7.6	55.8
1+30		5.3	58.1
1+84 <sup>92</sup> DE		+1.1	64.5



M.H. 6 to M.H. 2 (an imp. pair)

B.M.	3 26	32.83		29.57
0+00 = M.H. 6				
+30	S Pav Imp.	6.40		26.43
1+00		5.9		26.9
+50		5.6		27.2
2+00		5.2		27.6
+50		4.9		27.9
3+00		4.3		28.5
+50		3.8		28.0
+85		3.2		29.6
M.H. 2	12.38			
4+28 <sup>2</sup> = M.H. 2		40.02	5.19	27.64
	M.H. 2 to M.H. 12			
0+00 = M.H. 2				27.6
+56		11.5		28.5
0+66 <sup>2</sup> = M.H. 12		8.7		31.3
	M.H. 12 to DE South (E Francis)			
0+00 = M.H. 12				31.3
+15		3.4		36.6
T.P.	12.58	52.15	0.45	39.57
+36		10.1		42.0
+57		4.1		48.0
+72		2.1		50.0
1+02		6.7		45.4
1+17		9.4		42.7
+26		13.5		38.6
+37		9.6		42.5

		52.15		
+51			6.7	45.4
T.P.	13.10	65.20	0.05	52.10
1+72			10.6	54.6
2+12			3.0	62.2
+43			2.0	63.2
+75 = DE			+0.9	66.1
T.P.	9.81	74.96	0.05	65.15
B.M. 13' Men. SW Francis & Durant			7.95	67.01
	EXIST M.H. 35 <sup>th</sup> & Durant to M.H. 3 (E 35 <sup>th</sup> )			
3+55 <sup>2</sup> = EXIST M.H. FL		12.56		162.40
top			4.35	70.61
3+40		75.0	4.4	70.6
2+86			4.1	70.9
2+64			7.2	67.8
2+44			8.2	66.8
2+00			8.5	66.5
1+72			5.7	69.3
1+28			7.1	67.9
1+16			8.2	66.8
T.P.	0.04	62.51	12.46	62.50
0+98			2.3	60.2
0+97			5.6	56.9
T.P.	0.48	50.31	12.71	49.83
0+76			5.3	45.0
0+67 <sup>2</sup> S Imp. Pav.			5.23	45.08



50.31

0+48 <sup>6</sup>	N. Mt. Pav	578	44.53
0+43		63	44.0
0+40		58	44.5
T.P.	1.61	38.88	13.04 37.27
0+15		9.9	29.0
0+00	= MH 3	9.16	29.72
B.M.	Barrening	9.28	29.60
	MH 3 + 0 MH	13	
0+00	MH 3	38.85	
+22		9.8	29.0
+30		11.6	27.2
+42		11.4	27.4
+43		9.5	29.3
+70		8.7	30.1
1+00		8.4	30.4
+50		8.3	30.5
+90		4.8	34.0
+95		1.4	37.4
2+00		1.4	37.4
T.P.	13.09	51.70	0.23 38.62
2+06 <sup>+</sup>	S. rail SD3A	13.15	38.55
2+11	N. rail ✓	13.20	38.50
2+14		14.5	37.2
2+31		8.6	43.1
+71		2.7	49.0

51.70

T.P.	12.31	64.00	0.01 51.69
2+90		10.6	53.4
3+00		5.1	58.9
3+80 <sup>2L</sup>	5.56 = MH 13	68.64	0.92 63.08
	Green Horse w 35 <sup>th</sup> 100' N. of Tomkins	10.5	68.1
MH 14	0.22	66.92	1.93 66.71
MH 14	+ 0 MH 4	(+ Pardee)	
0+00	= MH 14		
+62		3.0	64.0
+75		9.8	57.2
T.P.	0.11	59.10	12.99 53.99
1+16		5.6	48.5
+51		11.0	43.1
+64		11.8	42.3
T.P.	3.35	44.44	13.01 41.09
+69		5.4	39.0
+75 <sup>E</sup>	N. rail SD3A	4.32	40.12
+80 <sup>E</sup>	S. rail ✓	4.42	40.02
2+10		6.9	37.5
+31		8.4	36.0
+53		10.0	34.4
+76		11.7	32.7
+92		11.6	32.8
3+06		14.3	30.1
+13		11.6	32.8







Feb 19-29  
London.

MH 27 to MH 26

MH 18	13.09	76.17		63.08
T.P.	12.99	89.05	0.11	76.06
<sup>MH 27</sup> 2 + 10 <sup>22</sup> = MH 27			9.29	77.76
1 + 95			9.7	79.3
1 + 50.	edge gutter slab	7.04		82.01
1 + 29 <sup>6</sup>	top Feb 35 <sup>M</sup>	4.05		85.00
0 + 99	back walk	0.56		88.49
T.P.	12.69	101.74	0.00	89.05
0 + 50			7.7	94.0
0 + 25			4.4	97.3
0 + 23			3.7	98.0
<sup>MH 26</sup> 0 + 00 = MH 26			2.68	99.06

MH 26 to MH 25

1 + 69 <sup>82</sup> = MH 26				
1 + 46			1.5	100.2
T.P.	12.58	114.03	0.29	101.45
1 + 00			11.9	102.1
0 + 85			10.8	103.2
0 + 75			11.2	102.8
0 + 45			10.9	103.1
<sup>MH 25</sup> 0 + 00 = MH 25			9.24	104.77

MH 25 to MH 24

1 + 89 <sup>22</sup> = MH 25				
1 + 75			9.1	104.9
1 + 60			9.6	104.4
1 + 30			12.1	101.9
1 + 00			12.1	101.9

114.03

24

0 + 55			10.7	103.1
0 + 45			10.1	103.9
0 + 25			8.8	105.2
<sup>MH 24</sup> 0 + 00 = MH 24			7.75	106.28

MH 24 to MH 23

1 + 90 = MH 24				106.3
1 + 45			4.5	109.5
1 + 30			3.1	110.9
1 + 00			1.9	112.1
T.P.	6.49	120.26	0.26	113.77
0 + 50			5.0	115.3
<sup>MH 23</sup> 0 + 00 = MH 23			1.97	118.29

MH 23 to MH 22

1 + 90 = MH 23				118.3
1 + 66			0.6	119.7
1 + 36			1.6	118.7
1 + 20			3.5	116.8
1 + 07			4.8	115.5
1 + 07			6.6	113.7
0 + 95			8.7	111.6
0 + 78			9.1	111.2
T.P.	0.25	107.62	12.89	107.37
0 + 05			24.0	83.6
0 + 00 = MH 22			23.2	84.4



MH 22 to MH 21

107.62

6+29 <sup>84</sup> = MH 22			84.4
6+01		18.0	89.6
5+71		13.5	94.1
5+46		8.0	99.6
5+11		3.8	103.8
T.P.	12.85	120.34	0.13 107.49
4+76		11.8	108.5
4+00		6.6	113.7
3+73		4.5	115.8
3+50		3.9	116.4
3+00		2.8	117.5
2+50		2.6	117.7
2+00		2.4	117.9
1+50		1.1	119.2
T.P.	3.48	123.69	0.13 120.21
1+00		2.9	120.8
0+50		1.7	122.0
<sup>MH 21</sup> 0+00 = MH 21		0.66	123.03
	MH 21 to MH 20		
0+00 = MH 21			123.0
0+03		0.8	122.9
+06		2.0	121.7
+50		6.3	117.4
1+00		8.9	114.8
+50		10.9	112.8
T.P.	0.45	111.71	12.43 111.26

25

111.71

1+89 <sup>80</sup> = MH 20		1.16	110.55
	MH 20 to MH 19		
0+00 = MH 20			110.5
+50		2.7	109.0
1+00		4.6	107.1
+10		4.5	107.2
+50		6.4	105.3
<sup>MH 19</sup> 1+89 <sup>83</sup> = MH 19		7.41	104.30
	MH 19 to MH 18		
0+00 = MH 19			104.3
+13		8.2	103.5
+20		10.5	101.2
+50		12.4	99.3
+80		15.2	96.5
1+00		15.3	96.4
1+10		14.8	96.7
1+35		16.2	95.5
1+50		15.9	95.8
1+73		13.3	98.4
T.P.	0.06	99.01	12.76 98.95
1+89 <sup>92</sup> = MH 18		2.76	96.25



MH 18 to MH 17  
9921

0+00 = MH 18		96.2
+24	3.1	95.9
+45	1.2	97.8
1+00	5.5	93.5
1+25	9.2	89.8
1+50	12.8	86.2
+65	12.9	86.1
1+70 <sup>09</sup> = MH 17	13.4	85.6

MH 17 to MH 16 to MH 26

0+00 = MH 17		85.6
+28	21.4	77.6
+37	21.8	77.2
+67	13.4	85.6
+80	7.2	91.8
<sup>MH 16</sup> 1+01 <sup>2</sup> = MH 16	3.66	95.35
+11	1.7	97.3
+30	1.8	97.2
T.P.	9.74	108.25
+40	6.7	101.5
+50	3.8	104.4
+80	1.8	106.4
2+25	1.8	106.4
+40	2.2	106.0
+80	5.4	102.8
3+05	8.3	99.9

108.25

26

3+35		10.9	97.3	
+45		13.4	94.8	
+55		17.3	90.9	
+75		19.5	88.7	
4+05		19.4	88.8	
+15		18.3	89.9	
+45		14.2	94.0	
+65		11.7	96.5	
5+15		9.6	98.6	
+75		7.4	100.8	
6+14		8.6	99.6	
<sup>MH 26</sup> 6+29 <sup>5</sup> = MH 26	0.34	99.40	9.19	99.06
T.P.	0.19	86.80	12.79	86.61
T.P.	0.20	74.07	12.93	73.87
T.P.	0.65	62.01	12.71	61.36
B.M.	13' Mon 34 <sup>2</sup> L		7.07	54.94 (54.97)



=MH 25	MH 25 to MH 18		
6+29 <sup>45</sup>	7.46	112.25	109.79
5+70		5.8	106.4
5+55		5.2	107.0
5+10		5.6	106.6
4+70		6.5	105.7
4+30		10.2	102.0
4+10		12.5	99.7
3+85		13.2	99.0
3+65		11.6	100.6
3+30		6.6	105.6
2+95		4.5	107.7
2+45		6.3	105.9
1+90		9.2	103.0
1+70		12.0	100.2
TP 008	100.72	11.61	100.64
1+40		4.1	96.6
1+00		9.1	91.6
0+60		14.5	86.2
0+10		6.7	94.0
0+00 = MH 18		4.46	96.26

27

	MH 19 to	MH 24	
=0+00			
MH 19	12.61	116.91	104.30
0+15		15.5	101.4
+52		18.5	98.4
+65		21.0	95.7
+80		18.2	98.7
1+00		16.8	100.1
+30		12.9	104.0
+50		12.3	104.6
+65		10.7	106.0
+80		7.9	109.6
2+05		6.5	110.4
+40		6.2	110.7
+65		5.5	111.4
3+00		5.1	111.8
3+40		4.9	112.1
+80		5.2	111.7
4+20		5.3	111.6
+50		4.2	112.7
+80		4.1	112.8
5+20		4.8	112.1
+35		4.0	112.7
+60		6.8	110.1
+80		7.8	109.1
6+15		10.2	106.7
6+29 <sup>00</sup> = MH 24		10.61	106.30



-6+29.69

MH. 23	5.77	124.06		119.29
6+10			6.4	117.7
5+60			5.5	118.6
5+15			3.2	120.9
4+80			1.7	122.4
4+45			1.9	122.2
4+10			0.9	123.2
3+85			3.7	120.4
3+50			5.1	119.0
3+43			6.9	117.2
3+13			8.1	116.0
3+00			9.9	114.2
2+50			13.3	110.8
2+15			14.2	109.9
2+00			13.5	110.6
1+60			16.8	107.3
1+50			16.0	108.1
1+30			17.0	107.1
1+00			16.3	107.8
0+60			15.1	109.0
0+15			13.9	110.2
0+00 = MH. 20			13.53	110.53

From hub. 65' South of MH.#2 to  
MH.#2 and north on E of Francis St.

28

Sta. on Hub 0+00	+	∞	-	Elev.
				31.3



MH #11 to MH 29 (917)

MH 11  $\angle$  of 100° E of E.L. 34

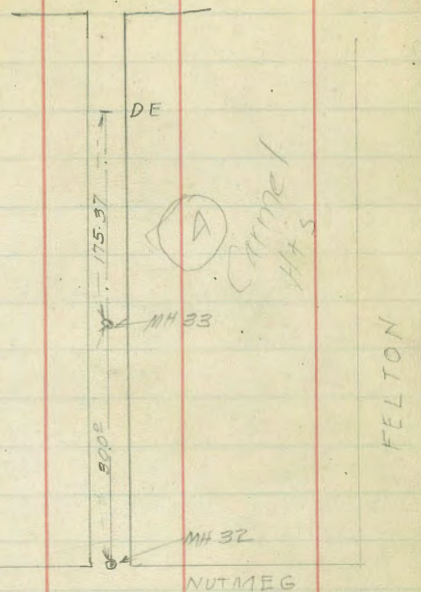
13 MON  
9 A.M.

BM	6.81	61.78	59.97
0+00 = MH 11		5.7	56.1
+40		7.6	54.2
1+00		8.5	53.3
+13		7.6	54.2
+30		7.1	54.7
+50		5.4	56.4
+63		3.4	58.4
2+00		1.5	60.3
+50		2.3	59.5
3+00		4.1	57.7
+40		5.9	55.9
+51		7.7	54.1
+65	tebet end.	8.32	53.46
+65	put.	9.0	52.8
3+80 = MH 29		8.7	53.1

MH 29 to MH 28

0+00 = MH 29			53.1
+50		11.0	50.8
1+00		13.2	48.6
+15		13.7	47.9
+40 = MH 28	( $\pm$ Francis & Tompkins)	13.3	48.5

129









Sewer Levels Eastern Ad.  
From DE North to MH 33

to MH. B.M.	12.40	270.70		258.26
T.P.	13.03	283.42	0.31	270.39
T.P.	9.36	292.20	0.58	282.84
S.E. 7' back B.M.	Frequency & Nutmeg.		4.09	288.11
T.P.	13.03	302.63	2.60	289.60
T.P.	5.29	304.98	2.94	299.69
DE = 1	+75.37		0.6	304.4
1+50			2.0	303.0
1+00			4.0	301.0
0+50			7.0	298.0
0+00 = MH 33			10.0	295.0
MH 33 to MH 32 0+00 = MH 33				
2+80			11.1	293.9
T.P.	0.70	292.64	13.04	291.94
2+50			2.3	290.3
2+00			7.8	284.8
1+50			13.0	279.6
1+20			15.6	277.0
1+00			18.3	274.3
0+87			20.0	272.6
0+67			26.2	266.4
0+52			27.1	265.5
0+42			30.0	262.6
0+30			24.7	267.9
0+16			22.4	270.2
0+00 = MH 32			11.5	281.1

## MH 32 to MH 34 0+00 = MH 32

		292.64		
0+05			10.8	281.8
0+27 <sup>6</sup>	N. 6 Nutmeg		12.50	280.14
T.P.	2.20	281.97	12.87	279.77
0+27 <sup>6</sup>	rather		2.61	279.36
0+50			3.3	278.7
0+89			5.6	276.4
1+01			5.0	277.0
T.P.	R.O.L.	270.16	12.82	269.15
1+36			11.0	259.2
1+62 <sup>2</sup>	= MH 34		13.2	257.0
MH 34 to MH 31 0+00 = MH 34				
0+37			11.2	259.0
0+60			11.1	259.1
T.P.	3.99	262.11	12.04	258.12
1+00			3.0	259.1
1+11			3.0	259.1
1+20			4.8	257.3
1+30			4.2	257.9
1+50			4.8	257.3
1+73			5.2	256.9
2+00			7.3	254.8
2+50			10.7	251.4
2+70			11.3	250.8
2+90			13.0	249.1
T.P.	0.10	249.27	12.94	247.17



249.27

3+17			8.3	241.0
3+35 <sup>27</sup>	33+37.0 MH 31		11.77	237.50 ✓
	MH 31 to MH 19	0+00 = MH 31		
0+15	33+52.		10.5	238.8
0+50	+87		14.5	234.8
T.P.	122	237.57	12.92	236.35
0+58	+95		3.7	233.9
0+65	34 02 channel		6.0	231.6
0+90	+27		7.2	230.4
1+09 <sup>74</sup>	34+46.74 MH 19		5.75	231.82
	MH 19 to MH 20	0+00 = MH 19		
0+11	+57.74		6.5	231.1
0+21	+67.74		4.3	233.3
0+50	34+96.74 35+02.74		8.6	229.0
0+61	channel +20.74		10.5	227.1
0+74	+23.74		12.0	225.6
0+77	+24.74		13.0	224.6
0+78	+35.74		12.0	225.6
0+89	+35.74		8.1	229.5
1+00	35+46.74		12.2	225.4
T.P.	663	231.15	13.05	224.52
1+17	+63.74		6.4	224.8
1+27	+73.74		3.4	227.8
1+37	+83.74		7.2	224.0
1+45	+91.74		8.0	223.2

231.15

1+50	35+96.74		8.1	223.1
1+76	36+22.74		9.0	222.2
1+85	+31.74		6.0	225.2
2+00	+46.74		4.8	226.4
2+22	+68.74		6.4	224.8
2+32	+78.74		9.1	222.1
2+38	+84.74		7.4	223.8
2+50	+96.74		7.6	223.6
2+90	37+36.74		8.0	223.2
3+00	37+46.74		7.4	223.8
3+37	37+63.74		5.3	225.9
3+53	37+99.74 38+18.74		5.7	225.5
3+72	MH 20		9.46	221.67
	MH 20 to MH 21	0+00 = MH 20		
0+22	38+46.74		14.1	217.1
T.P.	210	221.37	11.88	217.27
0+33	channel +51.74		7.5	213.9
0+40	+58.74		5.9	215.5
0+59	+77.74		5.0	216.4
1+00	39+18.74		6.0	215.4
1+50	+68.74		8.1	213.3
1+85	40+03.74		13.0	208.4
T.P.	0.90	209.82	12.45	208.92
1+98	+16.74		3.3	206.5
1+99	channel +17.74		5.0	204.8



	40+22.74	209.82		
2+04	channel		5.1	204.7
2+13	+31.74		4.4	205.4
2+26	+44.74		2.9	206.9
2+50	40+69.74		3.0	206.8
2+87	41+05.74		8.2	201.6
3+00	41+18.74		8.2	201.6
3+25 <sup>30</sup>	" +44.04 = MH. 21		8.82	201.00
	MH. 21 to MH. 5		0+00 = MH. 21	
0+39	41+83.04		5.8	204.0
0+50	+94.04		5.9	203.9
1+00	42+44.04		10.3	199.5
T.P.	3.22	200.91	12.13	197.69
1+15	+59.04		3.5	197.4
1+23	+62.04		5.2	195.7
1+50	channel 42+94.04		6.5	194.4
1+65	43+09.04		2.9	198.0
2+00	+44.04		6.8	194.1
2+13	+57.04		8.3	192.6
2+16	+60.04		10.3	190.6
2+50	channel 43+94.04		10.6	190.3
3+00	44+44.04		10.5	190.4
3+15	+59.04		9.9	191.0
3+30	+74.04		10.6	190.3
3+50	+94.04		10.6	190.3
3+66 <sup>40</sup>	45+04.04 = MH. 5		4.17	196.74

from D.E. North to MH. 19

SE 7<sup>th</sup> creek  
branch of N. 10<sup>th</sup>  
BN

	0.27	288.30		288.11
T.P.	0.37	275.68	12.99	275.31
0+00 = D.E.			3.4	272.3
0+23			5.1	270.6
0+50			8.8	266.9
1+00			12.7	263.0
T.P.	0.64	263.56	12.76	262.92
1+50			2.9	260.7
2+00			6.1	257.5
2+35			7.5	256.1
2+50			9.1	254.5
2+70			10.3	253.3
T.P.	0.10	250.80	12.86	250.70
2+85			1.1	249.7
3+08			3.8	247.0
3+25			6.2	244.6
3+45			9.5	241.3
3+60			12.5	238.3
3+75			17.8	233.8
3+85 <sup>31</sup>	= MH. 19		19.0	231.8



SE 7' to 6' 6" <sup>Notes</sup> MH 28 to MH 29 0+00 = MH 28

B.M.	9.30	297.41		288.11
sw. 7' to 6' 6" B.M.	8.88	305.79	0.50	296.91
T.P.	0.47	298.48	12.78	293.01
0+00	MH 28		6.75	286.73
0+06			5.6	287.9
0+17			7.8	285.7
0+50			10.6	282.9
0+70	0.76	281.29	12.95	280.53
0+85			3.2	278.1
0+98			7.6	273.7
1+00			6.9	274.4
1+25			9.4	271.9
1+36			14.6	266.7
1+42 <sup>02</sup> = MH 29			13.7	267.6
MH 29 to MH 30 0+00 = MH 29				
0+13 channel			12.5	268.8
T.P.	1.18	269.62	12.85	268.44
0+50 channel			5.7	263.9
0+85 channel			9.4	260.2
1+35 "			13.9	255.7
T.P.	1.76	258.50	12.88	256.74
1+43 <sup>40</sup> = MH 30			3.06	255.44

8/1/29 London. Swales Eastern Add.

MH 30 to MH 31 0+00 = MH 30				258.50
0+50			5.9	252.6
0+80			8.1	250.4
0+89			9.6	248.9
1+00			13.5	245.0
1+22			14.7	243.8
T.P.	1.92	247.62	12.80	245.70
1+29			2.2	245.4
1+47			5.4	242.2
1+60 channel			7.1	240.5
MH 31 1+85 <sup>44</sup> "			10.19	237.43 (237.50)
MH 27 to MH 26 0+00 = MH 27				
MH 28	6.82	293.55		286.73
T.P.	0.34	281.02	12.87	280.68
T.P.	0.38	268.54	12.86	268.16
0+00 = MH 27			5.20	263.34
0+19			6.9	261.6
T.P.	0.17	255.66	13.05	255.49
0+42			2.1	253.6
0+56			8.0	247.7
T.P.	0.09	242.77	12.98	242.68
0+73 <sup>65</sup> = MH 26			3.3	239.4



MH 26 to MH 25 0+00 = MH 26

212.77

0+07		4.9	237.9	
0+20		10.0	232.8	
0+21		11.9	230.9	
0+23		11.9	230.9	
0+24		10.7	232.1	
0+37		8.0	234.8	
0+60		7.5	235.3	
0+80		8.7	234.1	
0+90		11.6	231.2	
1+00		14.2	228.6	
T.P.	1.05	231.01	12.77	230.00
1+10 <sup>32</sup>	= MH 25	2.21	228.80	

MH 25 to MH 24

0+25		1.8	229.2	
0+60		3.1	227.9	
0+85		5.5	225.5	
1+30		10.6	220.4	
1+50		14.0	217.0	
T.P.	1.43	219.84	12.60	218.41
1+75	channel	8.6	211.2	
1+80		8.5	211.3	
1+92	channel	10.3	209.5	
2+00 <sup>11</sup>	= MH 24	9.17	200.67	210.67

MH 24 to MH 23 0+00 = MH 24

35

219.84

0+35		10.6	209.2	
0+40		9.9	209.9	
T.P.	3.03	210.43	12.44	207.40
0+73	channel	3.7	206.7	
1+45 <sup>03</sup>	channel = MH 23	6.52	203.32	203.71

= MH 23 to MH 22 0+00 = MH 23

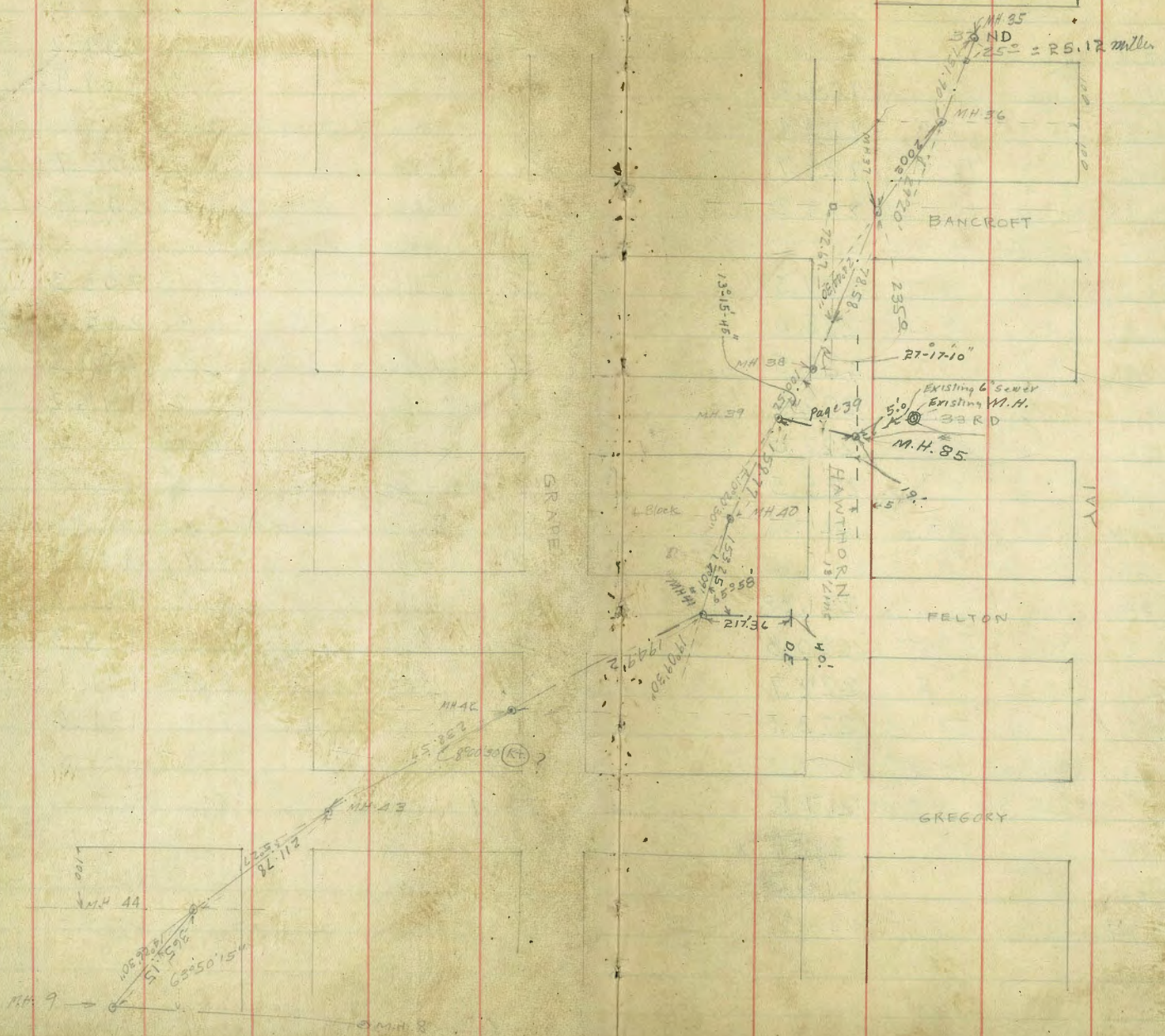
0+20		7.1	203.3	
0+30		6.4	204.0	
0+50		8.8	201.6	
1+00		12.2	198.2	
T.P.	2.24	199.58	13.09	197.34
1+44 <sup>19</sup>	= MH 22	3.25	196.33	

MH 22 to MH 5 0+00 = MH 22

0+40	channel	6.9	192.7	
0+54	"	6.8	192.8	
0+58	"	6.3	193.3	
0+90	"	8.5	191.1	
1+06		8.0	191.6	
1+27 <sup>25</sup>	= MH 5	2.95	196.63	196.71

PLOTTED TO HERE







MH 35 to MH 36 (P 36)

10/1/29  
London

242314 (B&amp;K 1351 P 26)

0+00 = MH 35		11.95	230.36
0+19 chl		12.7	229.6
0+25 "		11.4	230.9
0+33 "		12.6	229.7
0+50 "		13.0	229.3
T.P. 0.85	230.24	12.92	229.39
0+65		2.7	227.5
0+76		5.2	225.0
0+77 chl		7.7	222.5
0+80 chl		7.8	222.4
0+88		3.2	227.0
1+00		4.7	225.5
1+31 <sup>70</sup> = MH 36		8.86	221.38

MH 36 to MH 37

0+00 = MH 36			221.38
0+15		9.4	220.8
0+35		7.5	222.7
0+56		7.1	223.1
T.P. 3.30	220.45	13.09	217.15
1+00		2.9	217.5
1+50		8.0	212.4
1+70		3.7	216.7
2+00 = MH 37		6.87	213.58

MH 37 to MH 38

0+00 = MH 37	220.45		
0+26		12.0	208.4
T.P. 0.22	207.61	13.06	207.39
0+35		1.4	206.2
0+50		0.9	206.7
0+83		3.8	203.8
0+90		2.8	204.8
1+00		4.8	202.8
1+40		1.8	205.8
1+50		3.3	204.3
1+69		10.1	197.5
1+82		6.7	200.9
2+00		6.9	200.7
2+35 = MH 38		9.17	198.44

MH 38 to MH 39

0+00 = MH 38			198.44
T.P. 3.03	201.08	9.56	198.05
0+35		1.6	199.5
0+50		2.7	198.4
1+00 <sup>52</sup> = MH 39		7.24	193.84

MH 39 to MH 40

0+00 = MH 39			193.84
0+50 chl		12.5	188.6
T.P. 1.25	189.26	13.05	188.03
1+00		4.1	185.2
1+35		5.8	183.5
1+50		4.4	184.9

37



39-40

189.28

1+58 <sup>22</sup>	=MH 40	5.24	184.04
	MH 40 to MH 41		
0+00	=MH 40		
0+12		7.3	182.0
0+21		5.9	183.4
0+41	ehl	9.7	179.5
0+63		7.0	182.3
0+76		7.9	181.4
1+00		11.3	178.0
1+12		12.6	176.7
1+23		12.5	176.8
1+53 <sup>25</sup>	<sup>1.67</sup> =MH 41	178.95	12.00
	MH 41 to MH 42		177.28
0+00	=MH 41		177.28
0+08		2.2	176.8
0+23	ehl	5.5	173.5
0+40		6.3	172.7
0+45	ehl	7.2	171.8
0+57		5.2	173.8
0+78	ehl	9.4	169.6
0+91		7.4	171.6
1+02		7.4	171.6
1+35		11.3	167.7
1+50		11.0	168.0
1+65		12.8	166.2

41-42

178.95

1+94 <sup>22</sup>	=MH 42	11.56	167.39
	MH 42 to MH 43		
0+00	=MH 42		167.39
0+25		9.6	169.4
0+50		10.4	168.6
0+80		10.2	168.8
1+00		10.9	168.1
1+27		12.8	166.2
T.P.	9.37	167.70	12.62
1+50		6.3	161.4
1+60	ehl	10.5	157.2
1+70		9.0	158.7
2+00		9.8	157.9
2+38 <sup>51</sup>	=MH 43	11.49	156.21
	MH 43 to MH 44		
0+00	=MH 43		156.21
0+50		13.6	154.1
0+65		15.6	152.1
0+78		13.1	154.6
T.P.	11.5	155.93	12.92
1+00		2.2	153.7
1+25		5.9	150.0
1+38		6.6	149.3
1+42		5.2	150.7
1+68		7.6	148.3

38



A3-49

38-A

15593

1+79		9.5	146.4
1+87		8.1	147.8
2+11 <sup>28</sup>	= MH 49	7.99	147.94
	MH 49 to MH 9		
0+00	= MH 49		147.94
0+36		11.7	144.2
0+41		13.6	142.3
0+45		12.0	143.9
0+53		12.6	143.3
0+58		14.5	141.4
0+63		12.7	143.2
0+90		9.8	146.1
1+15		10.9	145.0
T.P.	1.15 144.58	13.10	142.83
1+50		2.8	141.8
1+90		4.3	140.3
2+00		5.6	139.0
2+23		3.1	141.5
2+50		3.5	141.1
2+85		3.2	141.4
3+00		3.9	140.7
3+12		4.0	140.6
3+40		8.3	136.3
3+65 <sup>15</sup>	= MH 9	11.45	133.13

PLOTTED TO HERE



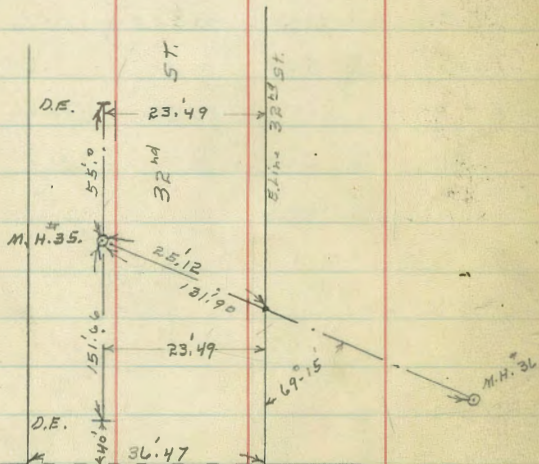




Cont. from Page 39

T 217.97

T.P.	0.10	204.88	13.19	204.78	
1+50			5.8	199.1	
1+68			14.6	190.3	N. sidewalk
1+77			15.6	189.3	S. " "
1+87 <sup>10</sup> = M.H. 39			11.02	193.86 = 193.84	



Prelim. Sewers  
1432<sup>nd</sup> St N. of Hawthorn  
Plat Opposite Page

B.M.	1.26	283.34		282.08	M.H. 32 <sup>10</sup> + Hawthorn
N. line Hawthorn			2.13	281.21	part.
00 = D.E. 40' N. of Hawthorn.			5.4	277.9	
T.P.	0.34	270.55	13.13	270.21	
0+60			1.8	268.8	
T.P.	0.32	258.15	12.72	257.83	
1+05			9.6	248.6	
T.P.	0.17	245.67	12.65	245.50	
1+20			3.3	242.4	
1+35			8.0	237.7	
1+51 <sup>66</sup> = M.H. 35 = 0+00 Hub			15.36	230.31 = 230.36	Wash.
0+26 M.H. 34			9.2	236.5	
T.P.	12.65	258.15	0.17	245.50	
0+55 = D.E.			10.0	248.2	

131.90  
106.95  
25.00

92  
17.95  
106.95

3.65  
11.73  
75.38

230.36  
15.37

248.15

10.0

PLOTTED TO HERE







Prelim Sewers  
 ♀ Gregory Juniper to Grape

1-6-30  
 Miller

H.I. Page 41	231.02			
0+00 DE 40'S. of Juniper		3.9	227.1	
0+10		4.7	226.3	
0+15		6.9	224.1	
0+19		4.2	226.8	
0+50		4.4	226.6	
1+00		7.1	223.9	
1+50		9.9	221.1	
1+85		11.8	219.2	M.H. 63 153.07 170.00
2+20		14.0	217.0	
T.P.	6.48	224.69	12.81	218.21 117.90 380.48
2+60		9.5	215.2	
3+00 M.H. 88 ♀ IVY = 0+00		10.75	213.94	
0+15		14.4	210.3	
0+22		22.6	202.1	
0+32		17.4	207.3	
0+80		17.5	205.2	
1+05		24.6	200.1	
T.P.	0.82	212.43	13.08	211.61
T.P.	0.21	199.78	12.86	199.57
1+35		12.3	187.5	
T.P.	0.04	186.70	13.12	186.66
1+53 M.H. 63 Old Location		5.09	181.61 = 181.61	
1+70 M.H. 63 New Location		8.59	178.11	
1+78 Wash		9.5	177.2	
T.P.	13.12	199.78	0.04	186.66

PLOTTED

181.61

42

		199.78		
T.P.	12.76	212.33	0.21	199.57
2+20			19.7	192.6
2+50			9.3	203.0
2+85			0.5	211.8
T.P.	12.81	224.87	0.27	212.06
T.P.	11.86	236.23	0.00	224.87
3+15			18.4	217.8
3+40			15.0	221.2
3+60			11.1	225.1
3+80 M.H. 90 ♀ Hawthorn			9.23	227.00 on stub
T.P.	12.28	247.94	0.57	235.66
4+30			15.6	232.3
T.P.	10.22	250.78	7.38	240.56
4+80			15.0	235.8
5+40			11.0	239.8
5+70			9.5	241.3
6+10			7.8	243.0
6+70			9.4	241.4
6+80 DE 40'S. of N. Line Grape			10.4	240.4

PLOTTED



Prelim. Sewers.

1/4 Ivy St. from M.H. #88. W. to Existing 6" C.I. Pipe

#				
0+00	M.H. #88.	12.17	226.21	213.94
0+10			8.9	217.3
0+15			12.4	213.8
0+20			9.0	217.2
0+55			2.9	223.3
0+90			1.1	225.1
1+15			3.1	223.1
1+55			13.4	212.8
1+80			19.8	206.4
2+00			28.0	198.2
2+06			27.1	199.1
2+21			14.9	211.3
2+39	5' ground		4.0	222.2
2+39	5' F.L. Existing 6" C.I. Pipe		3.24	222.97

PLOTTED

283.17  
 270.6  
 12  
 242.6

262  
 12  
 274

Prelim Sewer  
 from M.H. #63 To M.H. #63 New Location

1-8-30 Miller

H.I. 186.70 Page 42

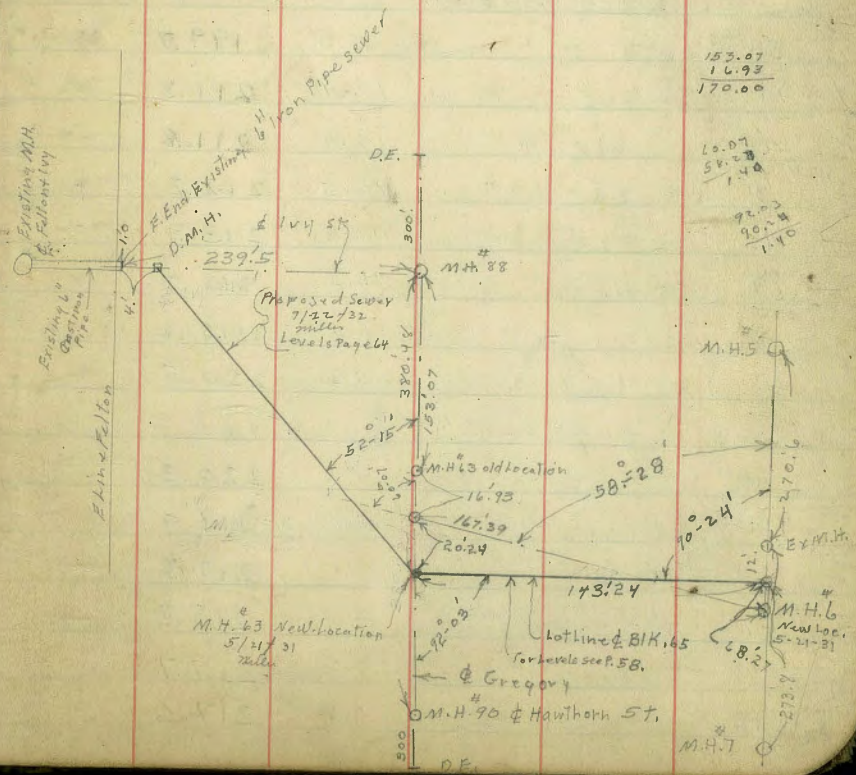
0+00	M.H. #63 New Location	8.59	178.11
0+17	Wash	10.4	176.3
0+20		9.8	176.9
0+55		9.9	176.8
0+75		12.0	174.7
T.P.	0.00	174.10	12.60
1+25		6.5	167.6
1+50		9.3	164.8
1+62		11.9	162.2
1+67 <sup>32</sup>	M.H. #63	11.43	162.67

PLOTTED

153.07  
 16.93  
 170.00

10.07  
 58.28  
 1.40

92.23  
 90.84  
 1.40





80' w. d. c.  
70' d. s.  
10' 1/4 s.

Gregory St X Sec  
1/4 To Grape

1-7-30  
mills

224.69

44

B.M. T.P.	6.4 1/4	224.69	218.21
	N. hinkelvy st		
W	3.7	221.0	
cb	6.2	218.5	
1/4	5.8	218.9	
±	9.4	215.3	
1/4	11.8	212.9	
cb	12.7	212.0	
+5	13.2	211.5	
E	22.9	201.8	
	20' s = N. d.		
E	25.0	199.7	
+17	13.4	211.3	
cb	12.9	211.8	
1/4	12.5	212.2	
±	10.8	213.9	
1/4	6.5	218.2	
cb	6.5	218.2	
W	4.2	220.5	
	30' s = N. 1/4		
W	4.4	220.3	
cb	6.8	217.9	
+4	7.1	217.6	
+7	9.0	215.7	
1/4	7.0	217.7	
+3	7.1	217.6	

Page 42

±	10.8	213.9
+6	12.6	212.1
1/4	13.1	211.6
cb	13.6	211.1
E	27.8	196.9
	40' s = ± 1/4	
E	29.6	195.1
cb	17.3	207.4
+3	14.3	210.4
1/4	13.5	211.2
+5	12.9	211.8
±	10.7	214.0
+6	7.3	217.4
1/4	7.4	217.3
+4	11.0	213.7
cb	7.5	217.2
W	4.0	220.7
	50' s = 5. 1/4	
W	3.2	221.5
+10	6.6	218.1
cb	8.0	216.7
+6	12.3	212.4
1/4	9.8	214.9
±	12.4	212.3
1/4	15.7	209.0
cb	20.5	204.2
E	32.0	192.7



224.69

60' S = S. curb of Ivy St.

E.	34.2	190.5
cb	25.6	199.1
1/4	21.5	203.2
1/4	22.6	202.1
+5	13.6	211.1
1/4	11.8	212.9
+6	8.7	216.0
cb	8.1	216.6
+10	7.0	217.7
W	4.0	220.7

00 = S. line Ivy

W	5.8	218.9
cb	9.2	215.5
1/4	13.3	211.4
1/4	17.8	206.9
1/4	22.0	202.7
cb.	27.0	197.7
E	39.0	185.7

25' S.

E	37.5	187.2
cb.	28.4	196.3
1/4	22.0	202.7
1/4	18.9	205.8
1/4	15.7	209.0
cb	13.6	211.1
W	12.7	212.0

224.69

Gregory St. YSec.

45

T.P.	0.82	212.43	13.08	211.61
		50' S.		
W			8.6	203.8
cb			6.3	206.1
1/4			7.0	205.4
1/4			8.6	203.8
1/4			12.0	200.4
cb			13.5	198.9
E			27.2	185.2
		75' S.		

E			28.9	183.5
cb.			22.0	190.4
1/4			18.7	193.7
1/4			16.4	196.0
1/4			15.8	196.6
cb			16.6	195.8
W			19.0	193.4
T.P.	0.21	199.78	12.86	199.57

100' S

W.			15.9	183.9
cb.			13.5	186.3
1/4			13.8	186.0
1/4			14.2	185.6
1/4			15.2	184.6
cb.			16.1	183.7
E			19.5	180.3



199.78

120'.5

E.	23.1	176.7
cb.	21.8	178.0
1/4.	20.8	179.0
1/4.	19.9	179.9
1/4.	19.6	180.2
cb.	19.6	180.2
W.	20.0	179.8

185'.5

W.	16.0	183.8
cb.	20.5	179.3
1/4	21.4	178.4
1/4	22.3	177.5
1/4	22.6	177.2
cb.	23.4	176.4
E.	24.7	175.1

150'.5

E.	23.3	176.5
cb.	21.2	178.6
1/4	19.5	180.3
1/4	18.1	181.7
1/4	17.0	182.8
cb.	16.2	183.6
W.	12.3	187.5

199.78

175'.5

Gregory St. X Sec.

46

W.	2.9	196.9
cb.	6.1	193.7
1/4	7.4	192.4
1/4	9.0	190.8
1/4	11.0	188.8
cb.	13.2	186.6
E	18.5	181.3

T.P. 12.76 R12.33 0.21 199.57

R+00

E	23.5	188.8
cb.	17.9	194.4
1/4	14.9	197.4
1/4	12.4	199.9
1/4	10.3	202.0
cb.	8.7	203.6
W	4.7	207.6

T.P. 12.81 R24.87 0.27 212.06

R25'.5

W	7.8	217.1
cb.	13.4	211.5
1/4	16.0	208.9
1/4	18.3	206.6
1/4	20.7	204.2
cb.	24.1	200.8
E	30.6	194.3



224.87  
250'S

E	24.4	200.5
cl	17.7	207.2
1/4	14.3	210.6
1/2	11.7	213.2
1/4	8.6	216.3
cl	6.3	218.6
W	2.1	222.8

T.P.	11.36	236.23	0.00	224.87
------	-------	--------	------	--------

275'S

W	8.9	227.3
cl	13.8	222.4
1/4	16.2	220.0
1/2	18.5	217.7
1/4	21.1	215.1
cl	24.0	212.2
E	31.6	204.6

8+00 = N. line Hawthorn

E	24.0	208.2
cl	20.4	215.8
1/4	17.5	218.7
1/2	15.0	221.2
1/4	11.9	224.3
cl	9.3	226.9
W	4.6	231.6

236.23

20'S = N. cl.

W	1.7	234.5
cl	5.9	230.3
1/4	8.7	227.5
1/2	11.1	225.1
1/4	14.1	222.1
cl	17.5	218.7
E	24.6	211.6

30'S = N. 1/4

E	24.2	212.0
cl	16.5	219.7
1/4	12.9	223.3
1/2	10.1	226.1
1/4	7.2	229.0
cl	4.7	231.5
W	0.5	235.7

40'S = cl

W	40.4	236.6
cl	4.0	232.2
1/4	6.1	230.1
1/2	9.2	227.0
1/4	12.3	223.9
cl	15.7	220.5
E	23.6	212.6

47

Gregory St.



236.23  
50' S = S. line Hawthorn

E		23.2	213.0
cb		15.1	221.1
1/4		10.9	225.3
£		8.1	228.1
T.P.	12.28	247.94	0.57 235.66
1/4		14.4	231.1
cb		14.4	233.5
W		10.5	237.4

60' S = S. line

W.		9.7	238.2
cb		13.2	234.7
1/4		14.9	233.0
£		18.4	229.5
1/4		21.3	226.6
cb		24.5	223.4
E		34.6	213.3

0+00 E S. line Hawthorn

E		32.3	215.6
cb.		22.5	225.4
1/4		19.3	228.6
£		16.3	231.6
1/4		13.6	234.3
cb		11.7	236.2
W		7.7	240.2
T.P.	10.22	250.78	7.38 240.56

Stub S.W. Cor

250.78  
25' S.

W		7.0	243.8
+10		10.5	240.3
cb		12.7	238.1
1/4		15.1	235.7
£		17.5	233.3
1/4		20.2	230.6
cb		22.8	228.0
E		31.0	229.8

40' E.

E		28.1	222.7
cb.		21.4	229.4
1/4		18.4	232.4
£		16.2	234.6
1/4		14.3	236.5
cb		11.7	239.1
+10		7.4	243.4
W.		5.7	245.1

65' S.

W		5.0	245.8
cb.		9.0	241.8
1/4		12.2	238.6
£		14.9	235.9
1/4		17.0	233.8
cb.		19.2	231.6
E		25.8	225.0

Gregory St

48



250.78  
100'.S.

E	22.9	227.9
cb	17.1	233.7
1/4	15.4	235.4
1/2	13.1	237.7
+5	10.6	240.2
1/4	9.7	241.1
cb	7.2	243.6
W	3.4	247.4

125'.S.

W	2.8	248.0
cb.	6.8	244.0
1/4	8.5	242.3
1/2	10.7	240.1
1/4	14.2	236.6
cb.	16.3	234.5
E.	20.6	230.2

150'.S.

E.	19.3.	231.5
cb.	14.6	236.2
1/4	11.5	239.3
1/2	9.5	241.3
1/4	7.4	243.0
cb.	5.7	245.1
W	2.4	248.0

250.78

175'.S.

W	3.9	246.9
cb.	5.3	245.5
1/4	6.4	244.4
1/2	8.7	242.1
1/4	10.6	240.2
cb	12.7	238.1
+12	16.2	234.6
E.	17.2	233.6

200'.S.

E.	16.0	234.8
+5	13.9	236.9
cb.	10.8	240.0
1/4	9.3	241.5
1/2	8.0	242.8
1/4	6.7	244.1
cb.	5.7	245.1
W.	6.1	244.7

225'.S.

W	9.4	241.4
cb	7.8	243.0
1/4	7.4	243.0
1/2	8.5	242.3
1/4	9.2	241.6
cb	10.3	240.5
E	13.8	237.0

Gregory St.

19



250.78  
250'S.

E.	12.5	238.3
cl.	10.4	240.4
1/4	9.6	241.2
1/4	9.7	241.4
1/4	9.9	240.9
cl.	11.0	239.8
W.	13.3	237.5

275'S.

W	17.0	233.8
cl.	14.5	236.3
1/4	13.0	237.8
1/4	12.1	238.7
1/4	11.3	239.5
cl.	11.1	239.7
E.	12.3	238.5
T.P.	1.06	239.32
	12.52	238.26

301'S. = N. line Grap. Co.

E	0.9	238.4
cl.	1.8	237.5
1/4	2.8	236.5
1/4	3.8	235.5
1/4	4.8	234.5
cl.	6.2	233.1
W.	10.0	229.3

239.32

20'S. = N. d.

W	14.1	225.2
cl.	10.1	229.2
1/4	8.2	231.1
1/4	6.6	232.7
1/4	5.3	234.0
cl.	4.2	235.1
E	2.4	236.9

30'S. = N. 1/4

E	3.7	235.6
cl.	5.7	233.6
1/4	7.2	232.1
1/4	8.6	230.7
1/4	10.1	229.2
cl.	12.1	227.2
W	15.9	223.4

40'S. = 1/4

W.	18.3	221.0
cl.	14.3	225.0
1/4	12.2	227.1
1/4	10.4	228.9
1/4	9.0	230.3
cl.	7.4	231.9
E.	5.7	233.6

Gregory St

50



239.32  
50' S = 5.44

E			7.5	231.8
el			9.7	229.6
1/4			10.9	228.4
1/2			12.6	226.7
T.P.	4.26	231.00	12.58	226.74
1/4			6.0	225.0
el			8.3	222.7
W			12.8	218.2

60' S = 5.44

W			15.5	215.5
el			9.8	221.2
1/4			8.1	222.9
1/2			5.9	225.1
1/4			4.3	226.7
el			3.0	228.0
E			0.6	230.4

80' S = 5.44

E			4.1	226.9
el			6.4	224.6
1/4			8.5	222.5
1/2			10.5	220.5
1/4			12.2	218.8
el			14.1	216.9
W			19.0	212.0



Prelim Sewers in Juniper St  
 From M.H. 89 Book 1316 P 41 to  
 M.H. 67 Book 1351 P. 32

2-27-30  
 miles

266.88

BM. 100	12.24	216.92		204.64	M.H. 89
T.P.	12.49	228.86	0.55	216.37	
9+57 <sup>15</sup> S. ch. line Juniper			6.19	222.67	15+84.70 Page 41
1+57 <sup>20</sup> S. gutter			6.79	222.07	15+84.70
T.P.	12.58	241.14	0.30	228.56	
2+00 on parmt			11.61	229.53	15+41.9
2+25. "			7.68	233.46	15+16.9
2+57 <sup>4</sup> N. gutter, line Juniper			3.98	237.16	+84.5
2+57 <sup>5</sup> N curb			3.28	237.86	+84.4
2+69 <sup>90</sup> M.H. 18			1.66	239.48	14+72 *
T.P.	12.65	253.76	0.03	241.11	
0+50			7.4	246.4	14+22
1+00			0.1	253.7	13+72
3' S. of 1+00 on curb			0.03	253.73	
T.P.	13.20	266.88	0.08	253.68	
1+20			10.0	256.9	13+52
3' S. of 1+20 on curb			10.43	256.45	
1+35			9.2	257.7	13+37
3' S. of 1+35 on curb			9.58	257.30	
1+65			8.5	258.4	13+07
2+00			7.5	259.4	12+72
3' S. of 2+00 on curb			7.86	259.32	
2+50			6.2	260.7	12+22
3+00			5.1	261.8	11+72
3+50			3.9	263.0	11+22
4+00			2.5	264.4	10+72

PLOTTED

4+50			1.3	265.6	10+22
5+00			0.0	266.9	9+72
T.P. BM	5.74	272.17	0.47	266.41	S.W. Juniper + Commonwealth 66.43
5+07 = W. line Commonwealth			5.06	267.11	9+65
5+14 = NW ch. Return			5.16	267.01	9+52.8
5+14 = gutter			5.82	266.35	+57.7
5+37 = M.H. 67 & Commonwealth			5.08	267.09	9+35.0

PLOTTED

52



Prelim. Sewers 7.5. of N. line Juniper  
 from D.E. 90' E. of E. line Commonwealth East. 227-30  
 To. M.H.# on & Pentucket. miller

H.I. Page 52 272.17

See Book 1351, p 33

**PLOTTED**

0+00 = D.E. 90' E. of E. line Commonwealth	1.3	270.9	1+20
3' S. of 0+00 on curb	1.35	270.82	
0+25	1.2	271.0	1+45
3' S. of 0+25 on curb	1.21	270.96	
0+50	1.5	270.7	1+70
3' S. of 0+50 on cl.	1.66	270.51	
1+75	2.5	269.7	1+95
3' S. of 1+75 on cl.	2.63	269.54	
1+00	3.9	268.3	2+20
3' S. of 1+00 on cl.	4.01	268.16	
1+25	5.7	266.5	2+45
3' S. of 1+25 on cl.	5.72	266.45	
1+50	8.0	264.2	2+70
3' S. of 1+50 on cl.	8.08	264.09	
T.P. 9.46	270.95	10.68	261.49
1+80	9.1	261.9	3+00
1+95	9.9	261.1	3+15
1+99 <sup>40</sup> M.H. # & Pentucket	11.69	259.26	3+19.4 Δ 83° 41' RT.
0+65	9.8	261.2	3+24.4
0+187 N. el Juniper on Curve	9.82	261.13	3+38.1
0+188 gutter parmt.	10.48	260.47	3+38.2
0+53 S. Line Juniper parmt.	10.84	260.11	3+72.4
0+75	9.0	262.0	3+94.4
0+93 D.E. 40' S. of Juniper	7.5	263.5	4+12.4

Book 1531  
 Page 31  
 Book 1351



Prelim Sewers  
& Feltan from MH # 24 North.  
Plat Page 30

2-24-30  
mills.

BM. MH. 24 0+00	13.07	223.74		210.67	Page 35
0+05 Wash			14.5	209.2	
0+25			7.7	216.0	
T.P.	12.60	236.13	0.21	223.53	
0+65			7.9	228.2	
T.P.	11.97	247.73	0.37	235.76	
1+00			9.1	238.6	
1+20			4.4	243.3	
T.P.	13.15	260.64	0.24	247.49	
1+50			8.9	251.7	
1+85			2.0	258.6	
T.P.	11.34	272.00	0.02	260.62	
2+43.2 <sup>o</sup> stub of Kalmia.			6.11	265.89	
3+00			3.3	268.7	
3+45			3.0	269.0	
3+90			6.7	265.3	
T.P.	0.44	259.45	12.99	259.01	

PLOTTED

54



Prelim Sewers  
2 BIK B at Fallant Gregory from M.H. 23 North  
Plat Page 30

2-24-30  
mills

B.M. M.H. 23 0+00

N.G.  
203.32  
203.91

Page 35

259.45 Page 54

R+35 N. of M.H. 23

9.2

250.2

13' 5.0 x 5'  
Line Kalmia

R+00

8.3

251.1

1+65

8.0

251.4

1+30

11.3

248.1

T.P.

0.11

246.32

13.24

246.21

7+00

3.6

242.7

0+77

9.6

236.7

T.P.

0.02

233.14

13.16

233.16

0+55

7.7

225.5

T.P.

0.12

220.33

12.97

220.21

0+35

3.5

216.8

T.P.

1.28

209.21

12.40

207.93

0+04

5.0

204.2

0+00 = M.H. 23

5.30

203.91 = 203.91

Page 35

55







226.51

T.P.	0.32	214.71	12.12	214.39	-	on stub
3+10 = M.H. 24	$\Delta$ 33° 39'	Lt. = 0+00	4.02	210.69	= 210.67	✓
0+20			5.3	209.4		✓
3' N. of 0+20			6.8	207.9		Wash -
0+42			5.0	209.7		✓
0+70			8.4	206.3		✓ Wash.
0+80			8.0	206.7		✓
4.5 of 0+80			8.7	206.0		✓ Wash. -
1+03			8.8	205.9		✓
4.5 of 1+03			9.9	204.8		✓ Wash -
1+30			9.7	205.0		✓
1+60			11.2	203.5		✓
1+75			10.7	203.0		✓
1+95			12.8	201.9		✓
T.P.	0.86	202.57	13.00	201.71		-
2+25			2.5	200.1		
2+45			3.6	199.0		✓ Wash
2+87 <sup>20</sup> M.H. 22	$\Delta$ 7° 09'	Lt.	5.9	196.7		✓ Wash.
" " " " " "			6.74	195.83		on Hub.
chk stub M.H. 5			5.93	196.64 = 196.71		

Plotted  
673731

57



Prelim Sewers bet M.H. 6 New Location + M.H. 63 New Location  
on Lot King & B.K. 45, Eastern Add.

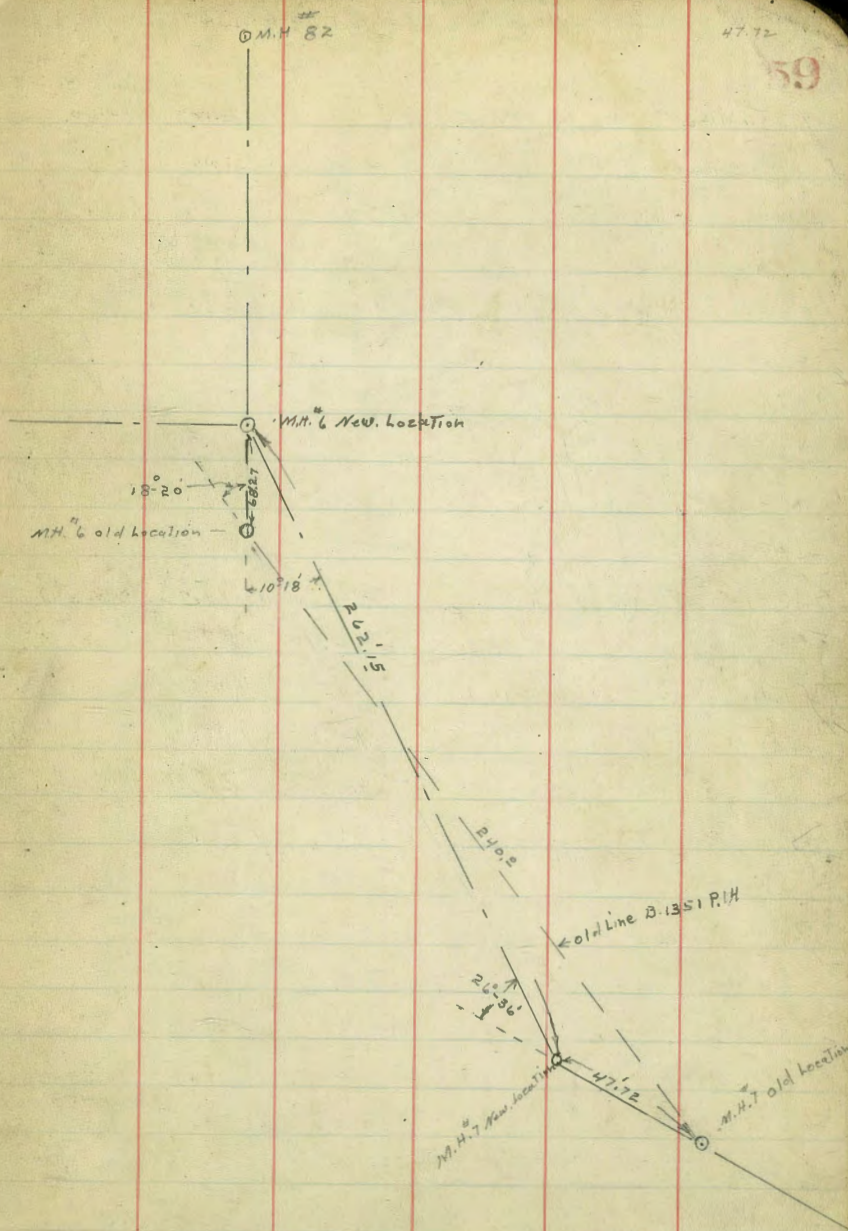
B.M. Stub	B.B.S.I. #				M.H. 6 Old Location
		11.05	173.76	162.71	
0+00	M.H. 6 New Location	11 Wash.	10.74	163.02	✓ on Hub.
0+08			7.8	166.0	✓
0+35			4.8	169.0	✓
0+65			1.7	172.1	✓
T.P.	✓	10.94	183.07	1.63	172.13
0+74			11.8	171.3	✓
4' N. of 0+74			14.0	169.1	✓
1+05			6.6	176.5	✓
1+43 <sup>24</sup>	M.H. 63 New Location		1.85	181.22	✓ on Hub
chk M.H. 63 old Location			4.89	178.18	✓

Plotted  
6-2-31  
L.B.H.



Station	Distance	Station	Distance	Notes
BM. strip inward } 0+00=	5.25	168.27	163.02	page 58 M.H. 6 New Location
0+17 wash	5.6	162.7	✓	
0+19	4.5	163.8	✓	
0+35	3.0	165.3	✓	
0+70	2.5	165.8	✓	
1+00	4.0	164.3	✓	
1+37	4.2	162.1	✓	
1+44 N. edge wash	8.8	159.5	✓	
1+59 S " "	9.0	159.3	✓	
1+62	5.9	162.4	✓	
2+00	6.8	161.5	✓	
5' E. of 2+00 Wash	10.2	158.1	✓	
2+35	7.3	161.0	✓	
2+62 <sup>15</sup> M.H. 7 New Location	6.98	161.29	on Hub	
chk M.H. 7 old Location B. 1351 P. 14	8.21	160.06	= 160.03	

Plotted  
 6-2-51  
 L.B.H.









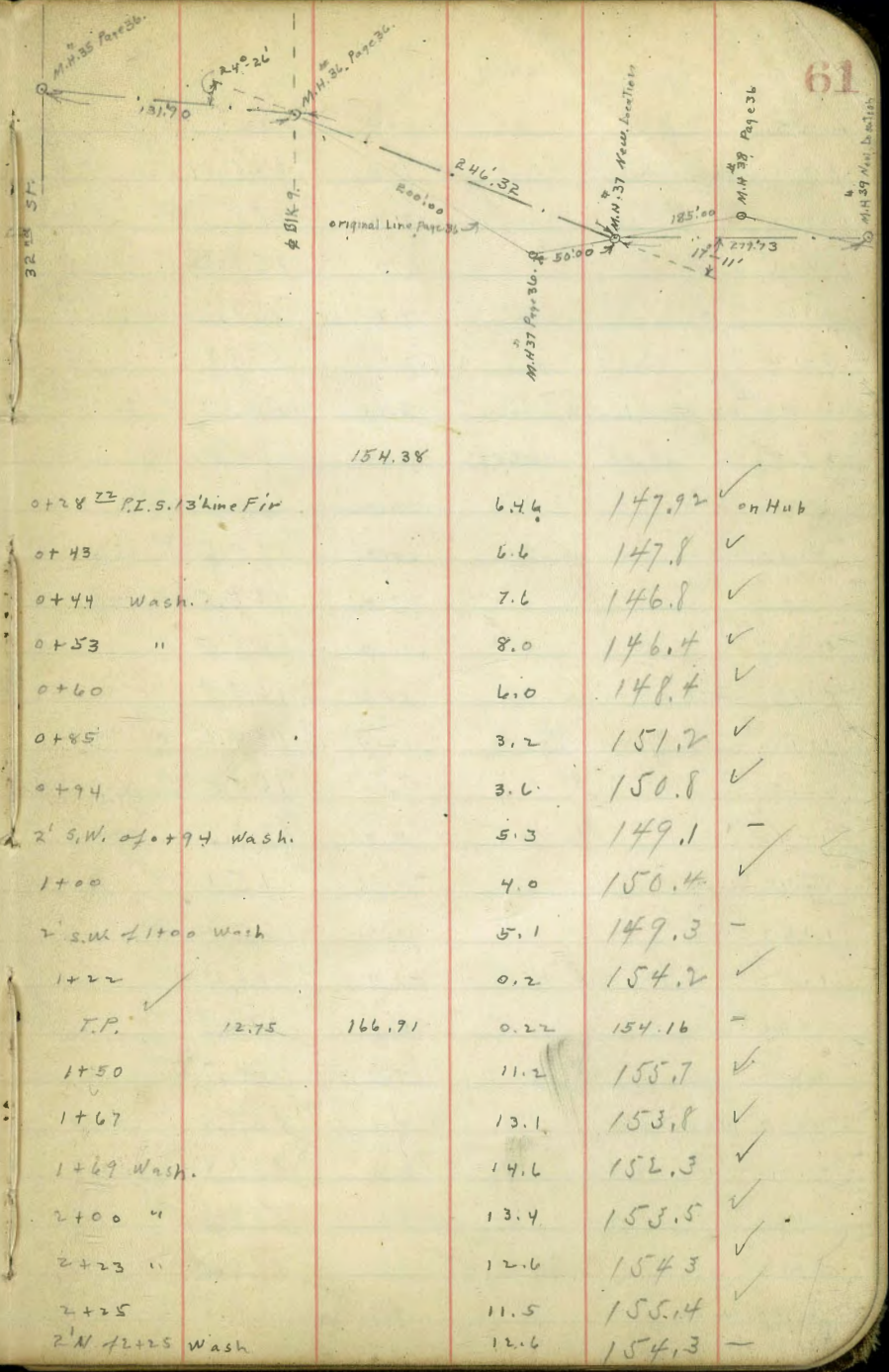
Prelim Sewers

Relocation line from M.H. 9 New location to M.H. 36 Page 36

5-27-31  
M.H. 36  
32 1/2 ft  
M.H. 36  
M.H. 36

0+00	B.M. M.H. 9 New Loc	11.91	173.39	131.48	✓
0+12			12.1	131.3	✓
0+20	wash		14.1	129.3	✓
0+29	"		13.3	130.1	✓
0+30			11.6	131.8	✓
0+60			9.6	133.8	✓
1+06			6.9	136.5	✓
1+08	wash		9.5	133.9	✓
1+15			7.2	136.2	✓
1+50			4.2	139.2	✓
1+85			4.4	139.0	✓
1+89	wash		6.4	137.0	✓
2+12			5.5	137.9	✓
2+14			3.4	140.0	✓
T.P.	12.50	154.38	1.51	141.88	-
2+55			11.1	143.3	✓
2+82			11.8	142.6	✓
2+83	wash		13.0	141.4	✓
2+99	"		13.0	141.4	✓
2+92			11.1	143.3	✓
3+02			10.8	143.6	✓
3+03			11.9	142.5	✓
3+11			11.9	142.5	✓
3+13			10.3	144.1	✓
3+32.30	M.H. 9 New Location = 0+00		6.93	147.45	✓
0+15	M.H. 4 old		6.50	147.88 = 147.94	✓

Plotted  
6-2-31  
L.B.H.



0+28	2' P.I. 5.13' line Fir	6.44	147.92	on Hub	
0+43		6.6	147.8	✓	
0+44	Wash.	7.6	146.8	✓	
0+53	"	8.0	146.4	✓	
0+60		6.0	148.4	✓	
0+85		3.2	151.2	✓	
0+94		3.6	150.8	✓	
2' S.W. of 0+94	Wash.	5.3	149.1	-	
1+00		4.0	150.4	✓	
2' S.W. of 1+00	Wash	5.1	149.3	-	
1+22		0.2	154.2	✓	
T.P.	12.75	166.91	0.22	154.16	-
1+50		11.2	153.7	✓	
1+67		13.1	153.8	✓	
1+69	Wash.	14.6	152.3	✓	
2+00	"	13.4	153.5	✓	
2+23	"	12.6	154.3	✓	
2+25		11.5	155.4	✓	
2' N. of 2+25	Wash	12.6	154.3	-	



166.91

2+50	10.4	156.5	✓
3A of 2+50 wash	11.8	155.1	-
3+00	8.4	158.5	✓
3+06 wash	9.7	157.2	✓
3+10 "	9.7	157.2	✓
3+12	7.1	159.8	✓
3+30 M.H. 43 New Location = 0+00	2.74	164.17	✓
T.P. 10.18 176.42	0.67	166.24	-
0+40	10.0	166.4	✓
0+75	10.9	165.5	✓
1+00	9.9	166.5	✓
1+10	10.9	165.5	✓
1+12 wash	12.5	163.9	✓
1+18 "	12.4	164.0	✓
1+20	10.9	165.5	✓
1+43	8.9	167.5	✓
1+45 wash	11.3	165.1	✓
1+53 "	11.2	165.2	✓
1+56	7.7	168.7	✓
1+90	5.1	171.3	✓
2+03	5.9	170.7	✓
2+07 wash	8.7	167.7	✓
2+11 "	8.8	167.6	✓
2+13	7.6	168.8	✓
2+33	6.4	170.0	✓
2+35 wash	7.5	168.7	✓

Plotted

176.42

62

2+74 wash	7.5	168.9	✓
2+76	6.0	170.4	✓
2+70	2.1	174.3	✓
2+85	3.4	173.0	✓
2+87 wash	4.6	171.8	✓
3+13 "	3.2	173.2	✓
T.P. 13.24 188.86	0.80	175.62	-
3+15	13.2	175.7	✓
3+29 <sup>30</sup> M.H. 44 Page 36 = 0+00	11.67	177.19 = 177.24	✓
0+34	11.9	177.0	✓
0+40 wash	13.4	175.5	✓
0+65 "	12.6	176.3	✓
0+67	10.8	178.1	✓
1+03	8.2	180.7	✓
1+05 wash	9.6	179.3	✓
1+09 "	9.9	179.0	✓
1+10	8.0	180.9	✓
1+35	3.6	185.3	✓
1+55	4.7	184.2	✓
1+90	0.7	188.2	✓
T.P. 13.27 201.93	0.20	188.66	-
2+25	11.7	190.2	✓
2+65	11.2	190.7	✓
3+06	11.5	190.4	✓
3+10 wash	12.8	189.1	✓
3+15 <sup>52</sup> M.H. 49 New Location in wash	12.76	189.17	✓

Plotted



201.93

0+03		11.2	190.7	✓	
0+25		7.7	194.2	✓	
0+50		3.3	198.6	✓	
T.P.	12.86	214.59	0.20	201.73	-
0+80		13.0	201.6	✓	
1+42		10.8	203.8	✓	
1+60		12.7	199.9	✓	
1+62 Wash.		17.4	197.2	✓	
1+64 "		17.4	197.2	✓	
1+66		15.3	199.3	✓	
1+93		10.0	204.6	✓	
2+23	Plotted	11.4	203.2	✓	
2+30 Wash.		11.5	203.1	✓	
2+43		8.8	205.8	✓	
2+48 Wash		10.5	204.1	✓	
2+65 "		9.2	205.4	✓	
2+79 <sup>23</sup> M.H. 37 West. Location = 0+00		8.02	206.57	✓	
0+40		5.3	209.3	✓	
0+43 Wash.		7.6	207.0	✓	
0+47 "		6.7	207.9	✓	
0+49		4.6	210.0	✓	
chk M.H. 37 Page 37		1.09	213.50 = 213.58		
0+75		3.2	211.4	✓	
0+76 Wash		3.7	210.9	✓	
0+82 "		3.4	211.2	✓	
0+84		2.4	212.3	✓	

214.59

T.P.	11.86	228.43	1.02	213.57	-
1+15			10.0	215.4	✓
1+37			10.9	214.5	✓
1+39 Wash			11.9	213.5	✓
1+48 "			12.1	213.3	✓
1+50 "			9.8	215.5	✓
1+80			5.6	219.8	✓
2+14			3.5	221.9	✓
2+30			5.0	220.4	✓
2+46 <sup>23</sup> M.H. 36 Page 36			4.27	221.16	New. Hub ✓

Plotted  
6-2-31  
L.B.H.

63







18-6-32  
Miller  
Walker  
Bliss

Sewer Cons  
Gregory Felton + Ivy  
Sketch Page 43

172.15

00 = Ev. M. H. F. L. Mainline

159.31

" " " " " Linstow  
181.14

5.55 166.60 ✓ 161.28

+ 5.32 ✓

0+50

11.90 169.84 ✓ 165.28

+ 4.56 ✓

1+00

5.09 176.65 ✓ 169.28

+ 7.37 ✓

1+43<sup>24</sup> M.H. 63 & Gregory

187.29

3.77 183.52 ✓ 172.74

+ 10.78 ✓

0+50

6.39 180.90 ✓ 176.74

+ 4.16 ✓

1+00

198.74

3.05 184.24 ✓ 180.74

+ 3.50 ✓

1+50

16.50 188.24 ✓ 184.74

+ 3.50 ✓

2+00

210.91

3.40 195.34 ✓ 188.74

+ 6.60 ✓

2+50 B.K.

223.27

8.67 202.24 ✓ 192.74

+ 9.50 ✓

2+97<sup>35</sup> D.M.H. & Ivy

3.21 220.06 ✓ 211.68

+ 8.38 ✓

" " "

3.21 220.06 ✓ 222.67

- 2.61 ✓

223.00

0.27

223.27 ✓

12.90

210.37 ✓

0.54

210.91 ✓

12.30

198.61 ✓

0.13

198.74 ✓

12.97

185.77 ✓

1.52

187.27 ✓

6.07

181.22 ✓

ctr Hub M.H. 63

0.52

181.74

12.30

169.44

2.71

172.15

B.K. 4.18

168.03

43.24

345.92

69.28

92.74

187.29

6.08

187.21

5.2

182.1

1.2

186.1

166.04

297.25

143.24

154.01



indexed  
C.S.K.

Pref. Sewer levels on  
Talbot Akron to Leroy

Moore  
Northway  
1-35

page 67 - level notes

8+71 → Ex M.H. 11.9' S. of N. Line Talbot St.  
6+49 → Ex 6" sewer at Δ 11.6 S. of N. Line 6  
6+41.00 = c.b. RL.

Leroy St.

Ex. curbs

Concrete

5+40.70 edge

0.8 CURTAIN WALL

Cabrillo Top

Talbot St.

8'25" LT. = STUB 2+88.30



AKRON

81°38'

Roseville  
HX.



8" x 14.5" STUB  
8" x 10" plug and starting sewer stub



1+54

1+10

0+90

0+83

0+50

0+1416 on stub

0+10

0+09

0+00 on stub Akron & Tabbot St. on plug and sensor

T.P. 7.87 108.84 0.43 100.97 ✓

T.P. 11.92 101.40 0.00 89.48 ✓

T.P. 12.68 89.48 0.37 76.80 ✓

T.P. 12.51 77.17 0.21 64.66 ✓

T.P. 13.10 64.87 6.49 51.77 ✓

Cannon & Evergreen 58.26 ✓ 49.51 ✓

Evergreen  
SWAP

+ Tabbot

LT 2 RT

67

89.7 93.8  
wash 19.1  $\frac{15.0}{3}$  Top bank

91.6 91.2  
17.2  $\frac{17.5}{10}$  bot. wash

97.4  
11.4

102.2  
6.6 Top bank

103.7  
5.1 S/W. edge road

105.90  
2.94

105.3  
3.5 S/W. edge road

106.8  
2.0

106.7  
2.4

108.84 π



+29

3 + 00

2 + 8830 = 4 stub

+80

+50

+45

+35

+30

2 + 00

1 + 80

T.P. 1.08

98.34 ✓

12.40

96.44 ✓

1 + 60

108.84

LT

C

RT

84.7	85.8
$\frac{13.6}{3}$	$\frac{12.5}{3}$
Wash	

86.1
$\frac{12.2}{3}$

85.9
$\frac{12.47}{3}$ = wash

84.0	90.5
$\frac{12.3}{3}$	$\frac{7.8}{3}$

86.2	89.8	92.1
$\frac{12.1}{8}$	$\frac{8.5}{8}$	$\frac{6.2}{4}$ Top
Wash		

92.6
$\frac{5.7}{3}$

93.3
$\frac{5.0}{3}$ Top bank

86.4	90.0	93.6
$\frac{11.7}{6}$	$\frac{8.3}{6}$	$\frac{4.7}{4}$ Top bank
Wash		

87.6	91.1	95.2
$\frac{10.7}{4}$	$\frac{7.2}{4}$	$\frac{3.1}{4}$ Top "
Wash		

88.2	93.4	95.9
$\frac{10.1}{10}$	$\frac{4.9}{10}$	$\frac{2.5}{3}$ Top "
Wash		

98.34 ✓

89.0

 $\frac{12.8}{3}$ 

Wash

93.2

 $\frac{12.6}{3}$  = Top "

108.84 ✓

98.34
$\frac{12.44}{3}$
85.88



check to P.M.

T.P.	5.99	57.84	12.46	51.85	49.51	0.03
T.P.	1.13	64.29	12.05	63.16		

6+41.0 approx. 6 of ex. sewer from Leroy St.

6+00

T.P.	0.39	75.21	12.11	74.82		
------	------	-------	-------	-------	--	--

+40.7 Top Cond. curtain wall & par

5+00

+75

+50

+25

4+00

T.P.	1.05	86.93	12.44	85.88		
------	------	-------	-------	-------	--	--

3+50

98.32

LT 2 RT

69

Sta L+49 Existing 6" sewer at Δ 116' from Property (F.L. Grade 65.00)

pc	Top of	70.35	69.5
		1.86	5.73
		2.00	par.

75.21
5.73
69.48

71.7

3.54 par.

75.21 T

74.8

12.11

76.5

10.4 wash

77.8

9.1 wash

79.3

7.6 "

79.7

7.2 wash

81.2

5.7 wash

86.93 T

83.4

14.9 wash

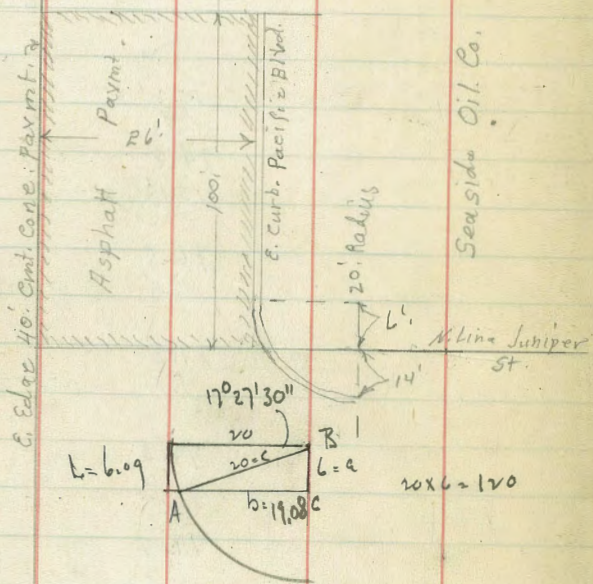
98.32 T



Area of Asphalt Pavmt.  
 E. of 40' Cmt. conc. Pavmt. on  
 Pacific Blvd. N. of Juniper St.

8-24-35  
 Miller  
 Bliss.

Indexed  
 E.S.K.



$$\begin{array}{r}
 100 \times 26 = 2600.00 \\
 + 1.96 \\
 \hline
 2601.96 = \text{Total Area}
 \end{array}$$

$$\cos B = \frac{a}{c} = \frac{6}{26} = \frac{10.7781513}{1.3010300} = 9.4771213$$

$$\text{Area } \Delta = 19.0823 = 59.24$$

$$\begin{array}{r}
 \text{"Sectn"} \\
 60.8 \\
 \hline
 118.04
 \end{array}$$

$$\begin{array}{r}
 6 \times 20 = 120 \\
 118.04 \\
 \hline
 1.96
 \end{array}$$



7-12-35  
Miller  
Walker  
Bliss

Location Trees + improvements  
Bet. curb + walk. on Imperial Ave  
28<sup>th</sup> + 32<sup>nd</sup> Sts  
N. side Imperial Ave

71

S. side Imperial Ave.

0+98 to 1+02

0+97 Meter box

0+93 Pine 2.5' High

0+83 Pine 2.5' High

0+65. B. Acacia 4" Diam.

0+59 Meter Box

0+50 to 0+55 cmt. walk

0+40 Elec Pole

0+35 Meter Box

0+21 to 0+25 cmt. walk

0+15 B. Acacia 6" Diam

0+00 = E. line 28<sup>th</sup> St.

0+00 = E. line 28<sup>th</sup> St



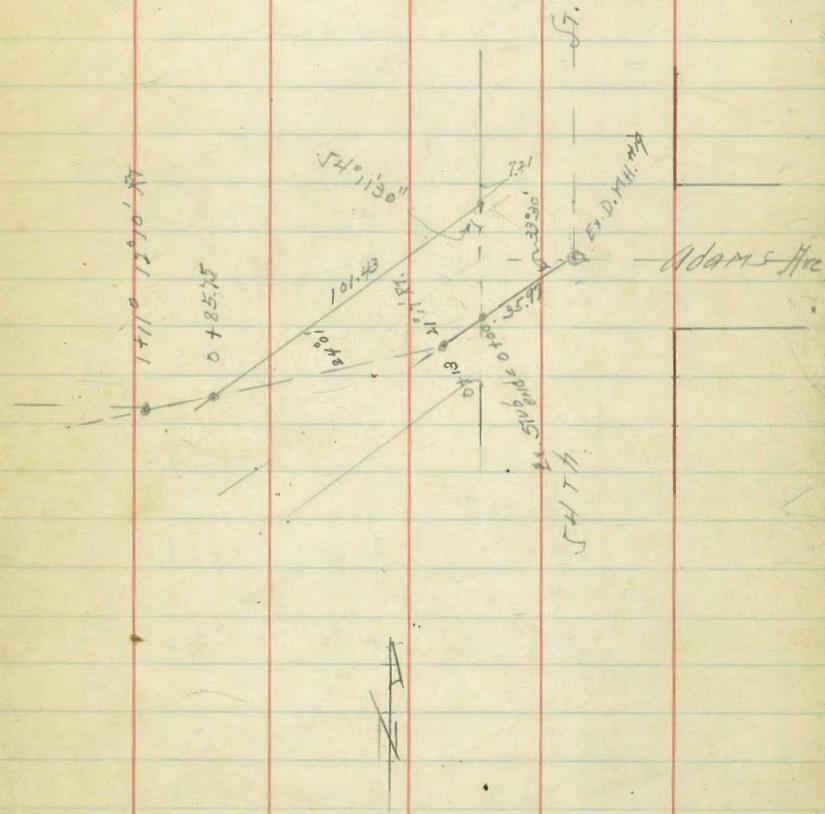
Moore  
3-14-36

Sewer Location at  
54th & Adams by Sewer Dept.  
no stakes set for job.

FL #19	14.05	415.55	401.50 S.M.H.
IRM top pav.		2.35	
0+00	DRY = NW 54th St.	3.23	
0+13	Δ 21° 17' RT	3.5	
1+11	Δ 12° 10' RT	6.2	
2		8.8	
✓ +50.5	ground	9.8	
" "	Top Cem. pipe Elbow.	10.22	405.33



4" C.M.P. sewer



Adams St



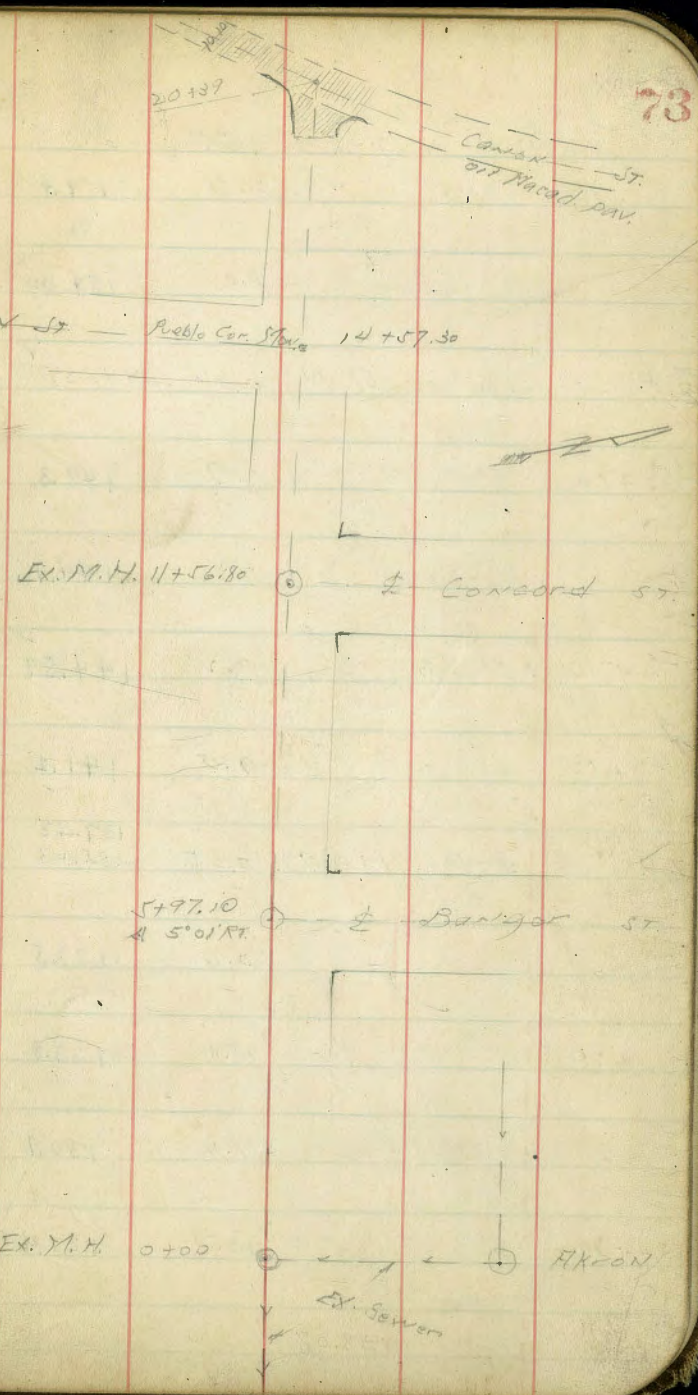
Sewer Levels  
 Talbot St.  
 Ex. M.H. on Arkon To Canon St.

Mount  
 12-15-34

Indexed  
 c.s.R.

T.P.	11.50	138.08	0.28	126.52
			2.4	124.4
+50			5.5	121.3
			8.4	118.4
+50			11.5	115.3
T.P.	12.77	126.80	0.78	114.03
			2.8	112.0
+50			5.8	109.0
0+00 = RIM T.M.			8.67	106.14
0+00 = Ex. M.H. on Arkon. FL.		19.63	9.518	(see 2114B) 94.97
T.P.	12.67	114.81	0.50	102.14
T.P.	12.79	102.64	0.62	89.85
T.P.	13.02	90.47	0.17	77.25
T.P.	12.11	77.62	0.52	64.51
N.W.B.P.	13.26	65.03	51.77	

Talbot  
 Evergreen





T.P. 12.82 174.36 ✓ 0.55 161.44 ✓

+50 2.6 159.4

7 8.0 154.00

T.P. 12.06 161.99 0.86 149.33 ✓

+50 0.9 149.3

6 5.3 144.9

5 + 97.10 AS 01 R 5.62 144.57 ON STUD

+50 9.0 141.2

T.P. 12.76 150.19 0.65 137.43  
~~138.43~~

5 0.6 137.5

+50 4.3 133.8

4 7.4 130.7

3 + 50 10.7 127.4

138.08

T.P. 12.94 224.28 ✓ 0.52 211.36 ✓

+25 1.2 210.7

11 4.6 207.3

T.P. 12.98 211.86 ✓ 0.65 198.90 ✓

+50 0.7 198.8

10 8.9 190.7

T.P. 12.95 199.55 ✓ 0.20 186.60

+50 3.7 183.2

40 S of 9x00 12.7 174.2 F.I.E. of House

9 10.2 175.7

T.P. 12.91 186.86 ✓ 0.11 174.15 ✓

+50 3.8 170.5

8x00 9.5 164.8

174.26



N		8.4	✓15.9
+57.3	on Mon. at 5th	7.25	✓17.03
+57.3	ground	6.6	✓17.7
+50		6.3	✓18.0
14		4.0	✓19.7
+50		3.5	✓20.8
13		3.0	✓20.7
+50		5.1	✓19.2
12		7.1	✓17.2
+56.8	Bin M.H.	10.20	✓14.08
+56.80	EX. M.H. F.L.	17.40	✓06.88
11+50		10.8	213.3

224.28

20	par.	3.3	✓32.9
+57	par	4.7	✓31.6
+50		5.2	✓31.1
19		9.4	✓26.8
TR	12.79	236.24	0.83 ✓
+50		2.6	✓21.7
18		6.6	✓17.7
+50		9.7	✓14.6
17		12.3	✓12.0
+50		12.5	✓11.8
16		12.0	✓12.3
15+50		10.5	✓13.8

224.28



NWAP  
Catalina  
Santa Barbara

T.P.			2.99	260.61	260.68	
					<u>2.07</u>	
T.P.	6.80	264.60	1.61	257.80		
T.P.	13.21	259.41	0.75	246.20		
Top N. end 10 cuv.					20.5 of	
W. Head wall	11.93	246.95	1.22	235.02	21.00	

20+39 approx. \$ par. 3.6 432.6

236.24



Walker  
Bliss  
1-26-38

Preliminary Sewer Levels  
Westland Terrace  
in Juniper, Westland, And Ivy streets

77

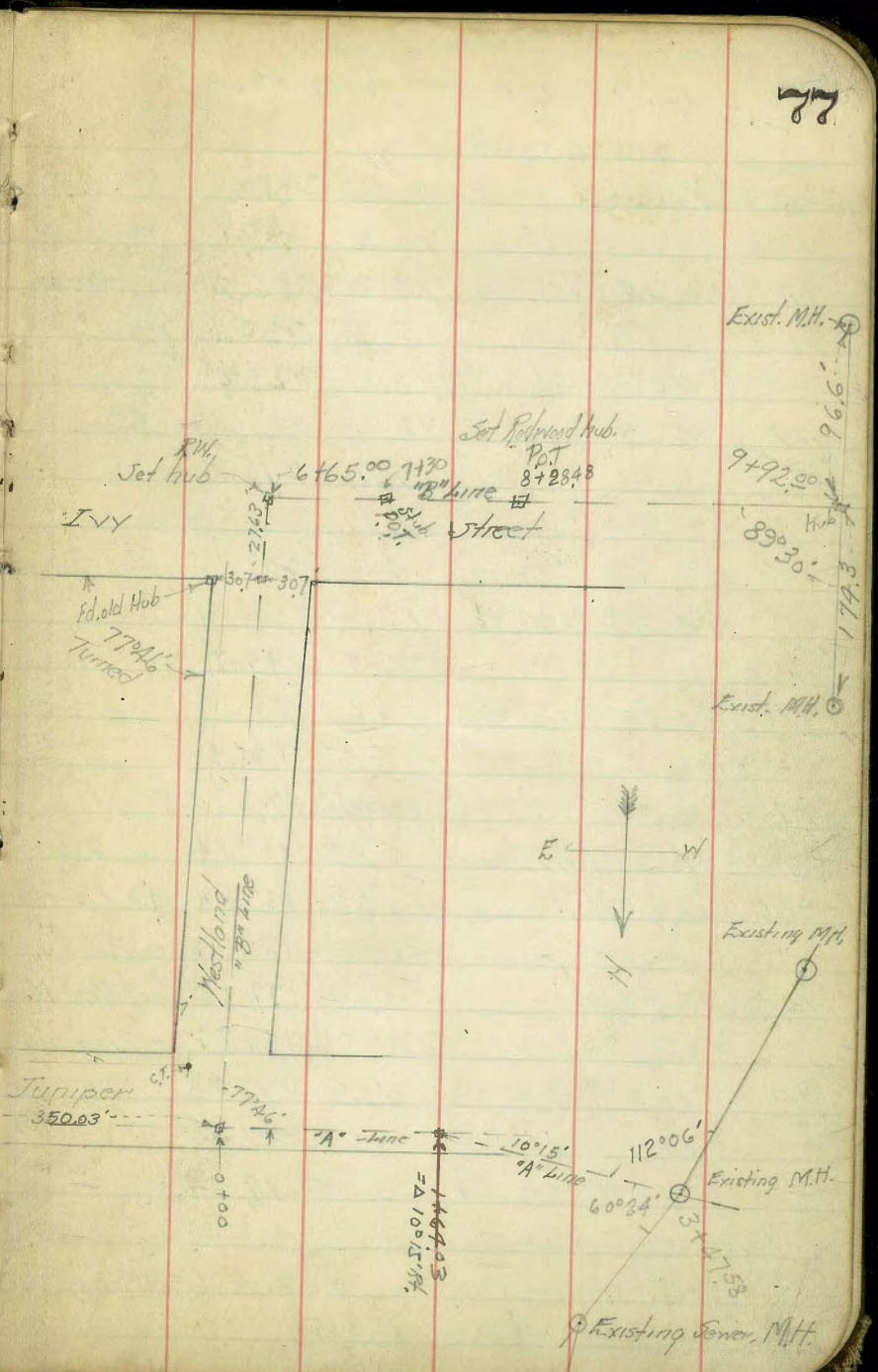
1.34 267.77 266.43 <sup>5 WSP</sup>  
Juniper + Commonwealth

"B" Line Levels

Westland & North 7' above Juniper = 0+00 on Hub.	9.54	258.23	13+08.03
+3.07 on cb.	9.50	258.27	13+11.10
" " Paving	10.16	257.61	"
+23.53 to Juniper on p.c.v.	9.87	257.90	13+31.56
+53.24 sh " " "	10.08	257.69	13+61.27
" " " " Ground	9.1	258.7	"
+56	6.5	261.3	13+64
1+00	5.8	262.0	14+08
+50	6.1	261.7	+58
2+00	6.8	261.0	15+08
+50	7.3	260.5	+58
3+00	7.3	260.5	16+08
T.P. 0.99 261.57	7.19	260.58	
+50	1.7	259.9	+58
4+00	2.8	258.8	17+08
+50	4.5	257.1	+58
5+00	6.5	255.1	18+08
+50	8.5	253.1	+58
6+00 (19+08.03)	12.1	249.5	19+58
T.P. 1.26 250.44	12.39	249.18	
+50 (19+58.03)	3.9	246.5	+73.03
+65 on Hub Δ 77'46'	4.55	245.89	20+08
7+00	1.6	248.8	

Continued on Page 76

Commonwealth Ave





"B" Line Levels  
Continued from Page 77

250.44

7+30 = P.O.T. on slab	2.76	247.68	20+38.03
+78	10.3	240.1	20+86.03
T.P. 0.44	237.94	12.94	237.50 (See Book 1539 page 31)
8+25	7.8	230.1	
+28.48 = P.O.T. on Hub.	8.71	229.23	
T.P. 0.17	225.51	12.60	225.34
8+75	9.7	215.8	
T.P. 0.40	213.52	12.39	213.12
9+00	4.8	208.7	
T.P. 0.25	200.96	13.81	200.71
+25	1.3	199.7	
T.P. 0.13	188.42	12.67	188.29
9+80	12.5	175.9	
T.P. 2.03	177.97	12.48	175.94
9+92 = Existing Sewer	4.83	173.14	on Hub.
96.6 South of Above station	10.03	167.94	on Rim M.H.
" " " 9+92 Floor	18.85	159.12	" Flow Line
174.3 North of 9+92	0.69	177.28	on Rim M.H.
" " " "	8.10	169.87	" Flow Line
T.P. 10.77	188.05	0.69	177.28
T.P. 12.17	199.99	0.23	187.82
T.P. 9.97	209.61	0.35	199.64
chk. S.E. B.P. Grogan + Juniper	3.13	206.48	
		206.56 = B.M. by Miller	
on Rim M.H. 3+47.58 on "A" line	14.1	195.20	

"A" Line Levels

78

145	259.68	258.23	Elev. Hub 0+00 Page 77
West end of North 7' line juniper = 0+00		1.45	258.23
+35		2.2	257.5
3' Lt. on cb.		2.56	257.12
0+50		3.8	255.9
3' Lt. on cb.		3.95	255.73
0+68		6.7	253.0
3' Lt. on cb.		6.53	253.15
1+00		11.5	248.2
3' Lt. on cb.		11.27	248.41
T.P. 0.45	247.27	12.86	246.82
1+40		4.7	242.6
3' Lt. on cb.		4.67	242.60
1+64.03 on Hub. = Δ 8/10/95		7.85	239.42
7' Lt. on cb.		8.07	239.20
1+95		11.1	236.2
T.P. 0.92	235.28	12.91	234.36
2+20		9.7	225.6
T.P. 0.60	223.05	12.83	222.45
+47		6.2	216.9
T.P. 1.67	212.02	12.70	210.35
2+90		11.30	200.7
T.P. 0.55	199.92	12.65	199.37
3+20		7.5	192.4
+23 = Bottom of ditch.		8.8	191.1

Cont. on Page 79



	W	E
60 N	98.00	97.70
40 N	96.30	96.00
20 N	94.10	93.80
10 N	92.90	
N. Line	91.70	91.25
5 S	91.56	90.75
16 S	91.02	90.50

"A" Line Cont from Page 78  
199.92

3+26	7.5	192.4	16+34
3+47.58 = East M.H. on Ground	7.0	192.9	+15.6
3+47.58 on Rim M.H.	4.67	195.25	
3+47.58 on Flow line	12.21	187.71	

Elev. of Rim M.H. P. 78 195.20  
Error in circuit of levels = 0.05

M.H. 26 = 239.4  
" 27 = 263.34

**DIRECTIONS FOR USE OF TABLES**

77/6  
155°52'

TABLE No. 1  
Distance of slope stake from side or shoulder stake for any width roadway, slope 1:1 to 1:1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not

**IMPROVED TABLES AND INFORMATION**

TABLE No. 2  
To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given L may be found by dividing tangent (or external), opposite L by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.



124.60

226.60

35-36-131.90

226.60

53.38

279.98

$$\begin{array}{r}
 13 \overline{) 0.40} \\
 \underline{39} \\
 70 \\
 \underline{65} \\
 50 \\
 \underline{39} \\
 11
 \end{array}$$

0359  
51770

11.70  
2.25

1 X.04

109.00

1.11

123.75

101-48-30

20-51-45

181-44-30  
40-51

160-51  
20-51  
80-09

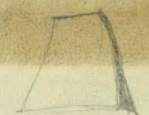
81-41-30

20-50-45

120  
115.26  
15.74

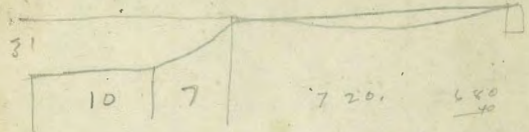
87-54+30

60.70  
53  
7.70



105-48  
43-17  
62-29

339.38  
281.55  
137.93



$$\begin{array}{r}
 330.00 \\
 \underline{28.72} \\
 301.28
 \end{array}$$

$$\begin{array}{r}
 275 \\
 \underline{259-73} \\
 129-3670
 \end{array}$$

$$\begin{array}{r}
 5013 \\
 \underline{270} \\
 91 \\
 \underline{26} \\
 .3510
 \end{array}$$

$$\begin{array}{r}
 .0013 \\
 760 \overline{) 100} \\
 \underline{76} \\
 240 \\
 \underline{228}
 \end{array}$$

270  
3  
810

