1322

DESK

LEDGER BOOK

No. 3607

Our Leather Bound Engineers Note Books are carried in the following rulings:

No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.

No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.

No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.

No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

We also carry the Note Books listed above, bound in extra strong Fabri-Hide (otherwise the same quality of book), which can be furnished at a somewhat lower price.

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THE FREDERICK POST CO.

ENGINEERING and DRAFTING SUPPLIES

IRVING PARK STATION

CHICAGO, ILL.

1321

1322

Table of contents after this

Index

B. Bliss
Joe Diermit
Jacobstroon
Kiernan
Feb 8, 1929

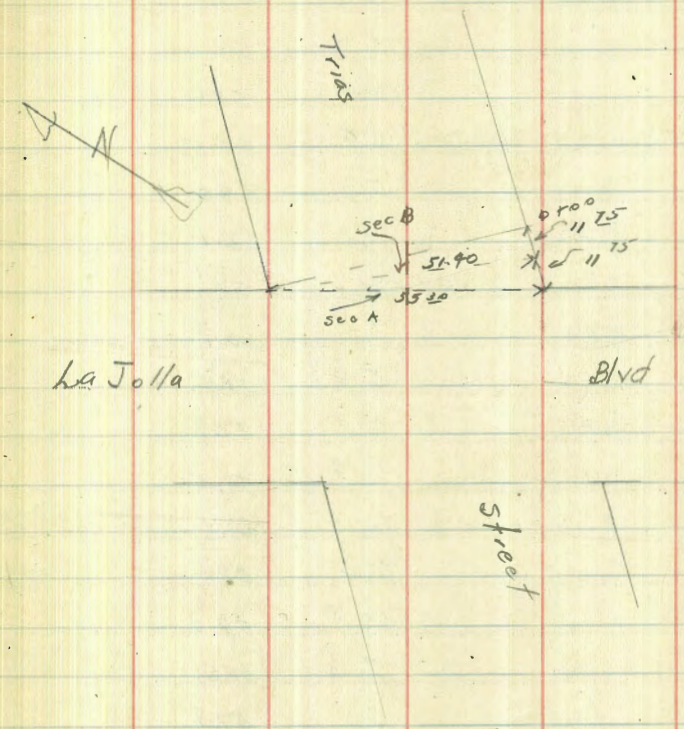
X Sections Trias St from La Jolla Blvd N. East

50 St.
10 cbs
75 1/4s

+	HI	−	Elev
BM 3 Nails in Light Pole N.W. Trias & La Jolla Blvd Walkers Construction Notes La Jolla Blvd 1.03	64.87		53.84
	Sec A	See Sketch	Page 2
N Line		7.5	57.4
+2		8.—	56.7
+5		9.0	55.9
+15		9.3	55.6
+20		8.9	56.0
+30		8.9	56.0
+40		8.1	56.8
+44 Existing paving in Gutter		10.6	54.71
+44 Top existing cb		9.03	55.84
+50		6.9	58.0
+55.30 S. Line		6.3	58.6
	Sec B		
−51.40 S. Line		5.6	59.3
−40		6.0	58.9
−32		7.2	57.7
−22		8.4	56.5
−13		6.8	58.1
−8		7.4	57.5
−4		8.7	56.2
N Line		7.5	52.4
	0+00		
N		7.5	57.4

Plotted 2/28/29

Tab



	+	H.I. 64.87	−	Elev
+4			8.4	56.5
cb			6.5	58.4
+5			6.5	58.4
1/4			7.2	57.7
℄			7.7	57.2
1/4			6.9	58.0
+3			6.4	58.5
cb			5.9	59.0
S			4.8	60.1
		0+25		
S			4.1	60.8
cb			5.4	59.5
+5			6.1	58.8
1/4			6.4	58.5
℄			6.3	58.6
1/4			6.5	58.4
cb			6.7	58.2
N			7.3	57.6
+2			7.5	57.4
+4			9.2	55.7
+10			10.4	54.5
		0+40		
−10			8.9	56.0
−2			9.0	55.9
N			6.5	58.4
cb			5.9	59.0

	+	H.I. 64.87	−	Elev
1/4			5.8	59.1
℄			5.8	59.1
1/4			5.8	59.1
cb			4.7	60.2
S			3.6	61.3
		0+50		
S			2.9	62.0
cb			4.5	60.4
+5			5.0	59.9
1/4			5.6	59.3
℄			5.6	59.3
1/4			5.4	59.5
cb			5.3	59.6
+3			5.3	59.6
+10			8.0	56.9
+10			8.1	56.8
		0+62		
−10			4.7	60.2
−3			4.7	60.2
N			7.6	57.3
cb			7.5	57.4
1/4			7.1	57.8
+2			5.7	59.2
℄			5.3	59.6
1/4			5.3	59.6
+4			4.1	60.8

	+	H.I. 64.87	−	Eley
cb			3.8	61.1
S			2.5	62.4
		0+68		
S			2.3	62.6
cb			3.8	61.1
+3			4.1	60.8
1/4			5.1	59.8
℄			5.1	59.8
+6			4.8	60.1
1/4			5.5	59.4
+3			6.3	58.6
cb			7.1	57.8
+3			6.9	58.0
N			4.3	60.6
		0+80		
N			3.3	61.6
cb			2.9	62.0
1/4			3.5	61.4
℄			3.8	61.1
+5			4.1	60.8
1/4			4.5	60.4
cb			4.6	60.3
+1			3.1	61.8
S			1.9	63.0
			1.9	63.0

	+	H.I. 64.87	−	Eley
+1			4.4	60.5
cb			4.5	60.4
+5			4.0	60.9
1/4			3.5	61.4
℄			1.6	63.3
1/4			1.8	63.1
cb			1.9	63.0
N			2.1	62.8
		1+09 · N Line Congress		
N			1.0	63.9
cb			0.7	64.2
1/4			0.4	64.5
℄			0.0	64.9
+4			0.8	64.1
1/4			1.1	63.8
cb			1.6	63.3
+6			1.9	63.0
+7			4.1	60.8
S			4.2	60.7
+3			4.1	60.8
+7			1.2	63.7
TP	12.26	76.16	0.97	63.90
		E Line of Congress	= 00	
S			6.9	69.3
cb			6.8	69.4
1/4			7.0	69.2

	+	HI 76.16	−	Elev
+3			7.1	69.1
℄			7.0	69.2
1/4			7.7	68.5
cb			8.5	67.7
N			9.1	67.1
		0+12		
N			8.3	67.9
cb			7.3	68.9
1/4			6.9	69.3
℄			6.0	70.2
1/4			6.1	70.1
cb			5.6	70.6
S			5.5	70.7
		0+25		
S			2.7	73.5
cb			3.5	72.7
1/4			4.3	71.9
+3			4.5	71.7
℄			5.0	71.2
1/4			5.2	71.0
cb			5.6	70.6
N			6.1	70.1
0+52. E End ~.75	73.41	0+40	W. End Garage 3° Back	
Concrete floor			3.93	72.23
		0+50		
N			2.5	73.7

5.

	+	HI 76.16	−	Elev
cb			1.2	75.0
1/4			0.3	75.9
Set BM NE Tree 1" Pipe			7.96	68.70
TP	12.41	87.16	1.41	74.75
+5			10.3	76.9
℄			10.3	76.9
1/4			9.2	78.0
cb			8.9	78.3
S			8.0	79.2
		0+52. East end Single Garage on N		
Concrete floor 3° Back			13.75	73.41
		0+64 W end. Single Garage on N		
3° Back Concrete			10.73	76.43
		0+75 East end Single Garage on N		
3° Back Concrete			9.25	77.91
		0+75		
S			1.3	85.9
cb			3.4	83.8
1/4			4.4	82.8
+5			5.8	81.4
℄			5.9	81.3
1/4			6.5	80.7
cb			7.5	79.7
N			9.0	78.2
		0+87.5 W end Single Garage on N		
3° Back			6.82	80.34

	+	HI. 87.16		
			0+98. East end Single Garage on	
	4° Back		5.95	81.21
			N 00	
N			3.6	83.6
cb			2.2	85.0
1/4			1.2	86.0
℄			0.5	86.7
T.P.	6.60	93.15	0.61	86.55
1/4			5.0	88.2
cb			3.7	89.5
S			1.7	91.5
TP	0.61	87.16	6.60	86.55
TP	2.08	77.31	11.93	75.23
check BM	1" Iron Pipe N.E. Trias + Congress		8.61	68.70

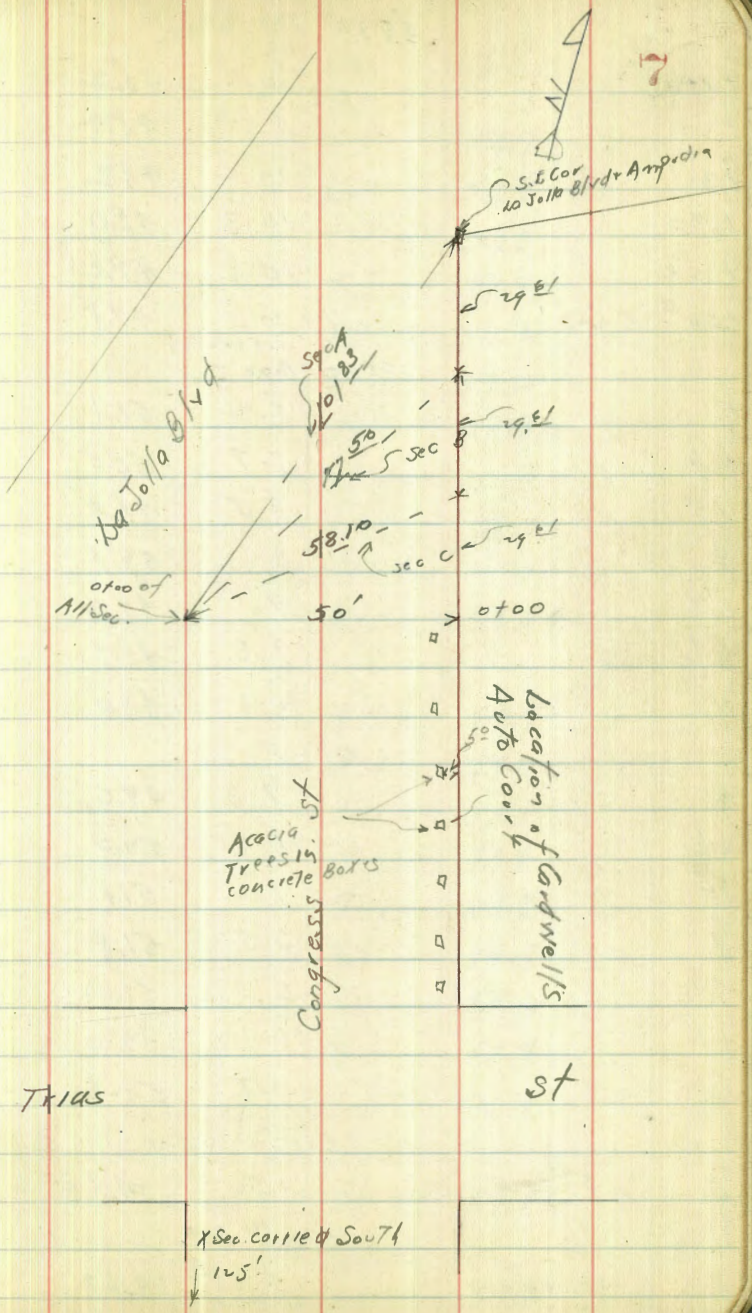
8 Bliss
Feb 28. 1929

X-Sections Congress Street

50' St
10' OBS
75 1/4S

	from Ampudia +	S. East Ht.	Elev	
BM. N.W. Lt Pole Trees & La Jolla Blvd	4.50	58.34	53.84	
			see sketch Page 7	
		Sec A		
0+00		10.3	48.0	
+10		10.8	47.5	
+20		10.8	47.5	
+30		11.3	47.0	
+40		11.9	46.4	
+50		12.6	45.7	
+60		13.0	44.3	
+70		13.3	44.0	
+80		13.3	44.0	
+90		13.5	43.8	
1+01	83.56 Prop Ampudia & Congress S.E.	13.5	43.8	
Set BM cut stake Ampudia & Congress		12.72	45.62	
		Sec B 77.50		
− 77.50		12.2	46.1	
− 70		11.9	46.4	
− 60		11.8	46.5	
− 50		11.4	46.9	
− 40		11.1	47.2	
− 30		10.6	47.7	
− 20		10.4	47.9	
− 10		10.3	48.0	
00		10.3	48.0	
		Sec C 58.10		
00		10.3	48.0	

Plotted 3/4/29 TM.



8 Bliss

	+	H.I.	—	Elev
		58.34		
			10.1	48.2
+10			9.9	48.4
+20			10.1	48.2
+30			10.3	48.0
+40			10.3	48.0
+50			10.5	47.8
+58 10 E Line			see sketch	
		0+00	Page 7	
			7.2	51.1
E			7.7	50.5
cb			8.5	49.8
1/4			8.6	49.7
℄			9.1	49.2
1/4			9.6	48.7
cb			10.3	48.0
W				
		0+25		
			9.3	49.0
W			7.8	50.5
cb			7.2	51.1
1/4			6.5	51.8
℄			6.3	52.0
1/4			6.3	52.0
cb			5.7	52.6
E				
		0+31 70 N. End Single Garage		
	3° BK. Concrete		3.99	54.35
		0+43 70 S. End Single		
	3° BK "		3.85	54.49

	+	H.I.	—	Elev
		58.34		
		0+50		
E			3.6	54.7
cb			4.4	53.9
1/4			4.7	53.6
℄			4.9	53.4
1/4			5.1	53.2
cb			5.3	53.0
W			5.6	52.7
		0+55 E. N. End Single Garage on East		
	3° Back concrete		2.32	56.02
		0+67 70 S. End Single Garage		
	3° Back concrete		1.95	56.39
		0+75		
W			4.4	53.9
+3			4.3	54.0
+8			5.0	53.3
cb			4.9	53.4
1/4			4.0	54.3
℄			3.6	54.7
1/4			3.1	55.2
cb			2.6	55.7
E			1.8	56.5
		0+79 5 N. End Single Garage on E		
	3° BK. concrete		0.62	57.72
		0+91.50 S "	"	" " "
	3° Back concrete		0.38	57.96

	+	HI	−	Elev
		58.34		
		1+00		
E			0.1	58.2
cb			0.7	57.6
1/4			1.3	57.0
℄			1.6	56.7
1/4			2.1	56.2
+5			2.2	56.1
cb			3.0	55.3
+5			2.4	55.9
W			2.5	55.8
+10			3.1	55.2
T.P.	12.57	70.72	0.19	58.15
		1+04 N End Single Garage on E		
	3° Back	concrete floor	10.98	60.74
		1+15 & S. End " " " "		
	3° Back	concrete	10.18	60.54
		1+25		
-10			13.9	56.8
W			12.7	58.0
+5			12.7	58.0
+7			13.1	57.6
cb			12.5	58.2
1/4			12.3	58.4
℄			11.9	58.8
1/4			11.2	59.5
cb			10.9	59.8
E			10.1	60.6

	+	HI	−	Elev
		70.72		
		1+28 N. End Single Garage on E		
	3° Back	concrete	8.36	62.36
		1+40 S. End Single Garage		
	3° Back	concrete	8.17	62.55
		1+50		
E			8.0	62.7
cb			8.7	62.0
1/4			9.1	61.6
℄			9.7	61.0
1/4			9.9	60.8
+5			10.1	60.6
cb			10.5	60.2
+3			10.9	59.8
+5			10.3	60.4
W			10.5	60.2
+10			11.0	59.7
		1+52 N. End Single Garage on E		
	3° Back	concrete	6.51	64.21
		1+64 S. End " " " "		
			6.33	64.39
		1+75		
-10			9.7	61.0
W			8.9	61.8
+4			8.8	61.9
+8			9.3	61.4
cb			8.9	61.8

	+	H.I. 70.72	−	Elev
+~			8.2	62.5
1/4			8.2	62.5
℄			7.9	62.8
1/4			7.4	63.3
cb			6.8	63.9
E			5.7	65.0
		1+76	N. End Single Garage on E	
	3" Back concrete		4.39	66.33
		1+88	5.1 " " " " 5	
	3" Back "		4.19	66.53
		2+00		
E			4.1	66.6
cb			5.1	65.6
1/4			5.7	65.0
℄			5.8	64.9
1/4			6.2	64.5
cb			7.0	63.7
+5			7.1	63.6
W			7.8	62.9
+10			8.4	62.3
		2+11 40	N. Line Trees	
W			6.9	63.8
cb			6.0	64.7
1/4			5.1	65.6
+3			4.8	65.9
℄			4.8	65.9

	+	H.I. 70.72	−	Elev
1/4			4.6	66.1
cb			4.1	66.6
E			4.7	66.0
		N cb.		
E			3.0	67.7
cb			3.3	67.4
1/4			3.6	67.1
℄			4.1	66.6
1/4			4.6	66.1
cb			5.3	65.4
W			6.4	64.3
		N. 1/4		
W			6.1	64.6
cb			5.1	65.6
+5			4.6	66.1
1/4			4.0	66.7
℄			3.5	67.2
1/4			3.3	67.4
cb			3.2	67.5
E			2.3	68.4
		℄		
E			1.5	69.2
+5			2.2	68.5
cb			2.9	67.8
1/4			3.2	67.5

	+	HI 70.72	−	Eley
℄ on Ground			3.6	67.1
℄ on Rim Manhole			3.60	67.12
1/4			3.5	67.2
cb			4.5	66.2
W			5.2	66.5
		S 1/4		
W			6.9	63.8
+3			6.3	64.4
+8			4.6	66.1
cb			4.1	66.6
1/4			3.5	67.2
℄			2.9	67.8
1/4			2.8	67.9
cb			2.2	68.5
E			1.6	69.1
		S cb.		
E			1.3	69.4
cb			2.1	68.6
1/4			2.2	68.5
℄			3.3	67.4
1/4			3.8	66.9
cb			5.9	64.8
W			7.9	63.3
		S. Line Trials	= 00	
W			10.0	60.7
cb			9.7	61.0

	+	HI 70.72	−	Eley
1/4			9.7	61.0
+3			9.0	61.7
℄			5.8	64.9
1/4			3.5	67.2
+4			2.2	68.5
cb			2.1	68.6
+5			2.3	68.4
E			1.5	69.2
		0+03		
E			2.0	68.7
cb			2.2	68.5
1/4			4.8	65.9
℄			9.3	61.4
1/4			9.6	61.1
cb			9.7	61.0
W			10.0	60.7
		0+10		
W			6.5	64.2
cb			6.9	63.8
1/4			6.6	64.1
+6			6.9	63.8
℄			9.0	61.7
+5			8.8	61.9
1/4			6.7	64.0
cb			3.2	67.5
+3			2.3	68.4

	+	H.I. 70.72	−	Elev
E			2.4	68.3
		0+25		
E			2.9	67.8
+4			3.8	66.9
cb			7.2	63.5
+4			7.2	63.5
1/4			3.8	66.9
℄			3.9	66.8
1/4			4.3	66.4
cb			4.7	66.0
W			5.1	65.6
		0+39		
W			3.7	67.0
cb			3.5	67.2
1/4			3.2	67.5
℄			2.7	68.0
1/4			2.7	68.0
cb			2.4	68.3
+1			2.4	68.3
+2			6.5	64.2
+7			6.5	64.2
E			4.6	65.1
+10			3.3	67.4
		0+44		
−10			3.8	66.9
−4			4.4	66.3

	+	H.I. 70.72	−	Elev
E			6.3	64.4
+5			6.4	64.3
+7			2.0	68.7
cb			2.2	68.5
1/4			2.4	68.3
℄			2.4	68.3
1/4			2.8	67.9
cb.			3.1	67.6
W			3.4	67.3
		0+47		
W			3.2	67.5
cb			3.1	67.6
1/4			2.9	67.8
℄			2.3	68.4
1/4			2.1	68.6
cb			2.1	68.6
E			1.7	69.0
+1 Top			1.7	69.0
+1 Bottom			6.2	64.5
+4			4.2	66.5
+10			3.6	67.1
		0+66		
−10			3.4	66.8
−5			3.4	67.3
−4			0.1	70.6
E			0.2	70.5

	+	HI 70.72	−	Elev
cb			0.7	70.0
1/4			1.0	69.7
℄			1.1	69.6
1/4			1.1	69.6
cb			1.0	69.7
N			0.9	69.8
T.P.	0.69	80.51	0.90	69.82
		0A75		
W			8.0	72.5
+5			8.5	72.0
cb			9.2	71.3
1/4			10.3	70.2
℄			10.5	70.0
1/4			10.3	70.2
cb			10.0	70.5
E			9.3	71.2
+5			9.4	71.1
+7			13.3	67.2
+10			13.3	67.2
+15			12.8	67.7
		1400		
−30			8.4	72.1
−26			10.3	70.2
−19			11.1	69.4
−16	On Nom ditch		12.4	68.1
−9			12.4	68.1

	+	HI 80.51	−	Elev
−6			7.5	73.0
E			7.6	72.9
+7			7.2	73.3
cb			6.8	73.7
1/4			5.9	74.6
℄			5.5	75.0
+5			4.7	75.8
1/4			4.4	76.1
cb			3.5	77.0
+4			3.3	77.2
+6			6.1	74.4
W			7.0	73.5
+3			3.3	77.2
+10			3.4	77.1
T.P.	8.00	85.61	2.90	77.61
		1425		
W			4.7	80.9
cb			5.1	80.5
+2			8.4	77.2
1/4			8.4	77.2
+2			7.5	78.1
+4			4.9	80.7
℄			4.9	80.7
+5			5.4	80.2
TP	2.90	80.51	800	77.61
1/4			0.9	79.6

	+	HI	–	Elev
		80.51		
ob			2.0	78.5
E			3.9	76.6
+5			5.9	75.1
+13 Edge of ditch			5.9	74.6
Check out on BM.			11.8 ~	68.69
				68.70
				0.01 ~
NE 1" Iron Pipe Trias & Congress				
set on x section of Trias				

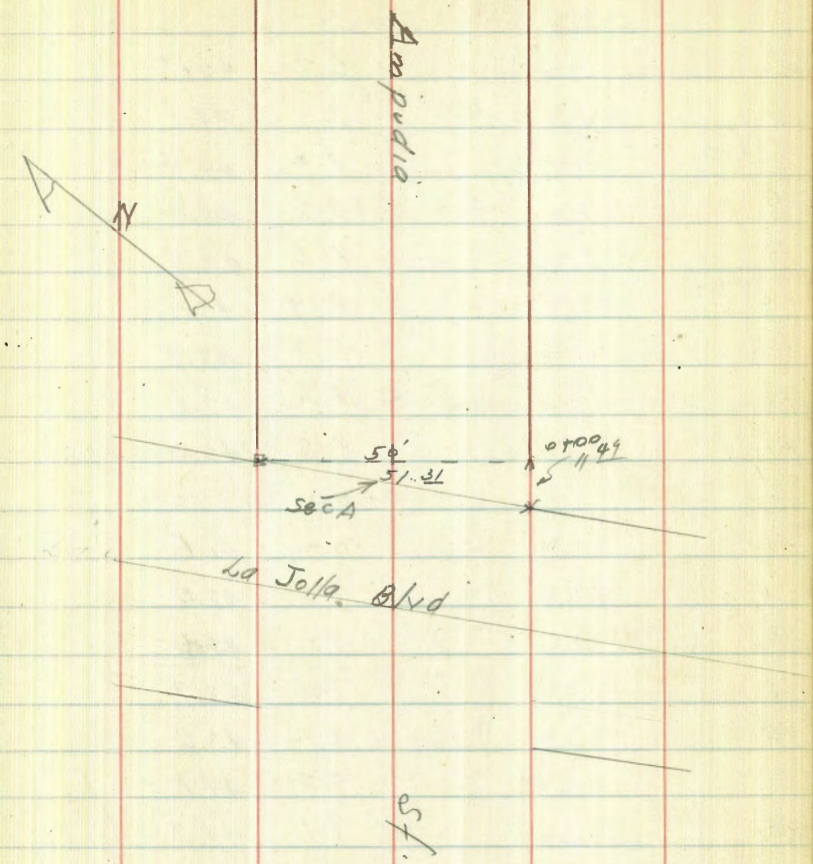
Bill Bliss
Feb. 28, 29

X Section Ampudia. La Jolla Blvd

	N East				50' St
BM SE Cut Ampudia & La Jolla Blvd	6.17	51.79		45.62	10' cbs 75 1/4
			Sec A.	51.31 + 11.40	
X NW 0+00 Prop Cor			8.4	43.4	
0+10			7.6	44.2	
+15			7.9	43.9	
+20			7.7	44.2	
+30			7.1	44.7	
+40			7.0	44.9	
+51.31 S.P.			7.0	44.9	
		0+00			
5			6.1	45.7	
+5			7.0	44.8	
cb			7.0	44.8	
1/4			7.5	44.3	
℄			7.2	44.6	
1/4			7.5	44.3	
cb			7.3	44.6	
N			8.4	43.4	
		0+13			
N			8.3	43.5	
cb			8.3	43.5	
1/4			8.2	43.6	
+4			8.0	43.8	
℄			7.5	44.3	
1/4			7.0	44.8	
cb			6.6	45.2	

Tied 2-28-29

Plotted



	+	H.I. 51.79	−	Elev
S			6.6	45.2
		0+25		
S			6.7	45.1
cb			7.2	44.6
1/4			7.4	44.4
℄			7.8	44.0
1/4			8.1	43.7
+4			8.4	43.4
cb			8.9	42.9
N			9.2	42.6
+10			9.8	42.0
		0+50		
−15			10.2	41.6
−5			9.8	42.0
N			9.2	42.6
cb			8.1	43.7
1/4			8.2	43.6
℄			7.7	44.1
1/4			7.1	44.7
cb			6.3	45.5
S			5.9	45.9
		0+75		
S			4.9	46.9
+5			5.5	46.3
cb			5.7	46.1
+3			6.2	45.6

	+	H.I. 51.79	−	Elev
1/4			6.4	45.4
+4			6.7	45.1
℄			6.5	45.3
+2			6.6	45.2
1/4			7.2	44.6
cb			8.1	43.7
N			8.4	43.4
+5			8.4	43.4
+15			10.0	41.8
		0+84. West end 4 car Garage on South		
	2.50 Back dirt floor		3.4	48.4
		1+00		
−10			8.2	43.6
N			7.6	44.2
cb			6.7	45.1
1/4			6.6	45.2
℄			6.4	45.4
1/4			5.8	46.0
cb			5.1	46.7
S			3.5	48.3
		1+16 East End 4 car Garage		
	2.50 Back Dirt floor		3.1	48.7
		1+18 West End 2 car Garage		
	Apron on Line		2.78	49.01
	2.50 Back Concrete floor		2.31	49.48
		1+25		
S			2.8	49.0

	+	HI 51.79	−	Elev
+5			3.6	48.2
ob			4.9	47.4
+5			5.1	46.7
1/4			5.9	46.4
+6			5.9	45.9
℄			5.9	45.9
1/4			6.8	45.0
ob			7.3	44.5
N			7.3	44.5
+10			8.1	43.7
			1+34 East End 2 car Garage	
	on South Apron of lime concrete		2.96	49.33
	Floor 2.50 Back		2.20	49.59
			1+50	
−10			8.5	43.3
N			7.9	43.9
ob			6.9	44.9
1/4			6.2	45.6
℄			5.3	45.5
1/4			4.5	47.3
ob			3.9	48.4
S			1.8	50.0
			1+75	
S			0.2	51.6
ob			1.6	50.2
1/4			2.1	49.7

	+	HI 51.79	−	1+66 Mn Hole Elev	4.75
℄			3.3	48.5	16
1/4			3.8	48.0	
ob			5.1	46.7	
N			6.3	45.5	
+15			8.4	43.4	
			2+00		
−20			7.5	44.3	
−10			5.6	46.2	
N			4.4	47.4	
+5			3.6	48.2	
ob			2.3	49.5	
1/4			0.6	51.2	
TP	13.13	63.99	0.93	50.86	
℄			11.7	52.3	
1/4			10.6	54.4	
ob			10.3	54.7	
S			8.9	55.1	
			2+25		
S			3.3	60.7	
ob			6.2	57.8	
+3			6.8	57.2	
1/4			7.0	57.0	
℄			8.4	55.6	
+5			9.0	55.0	
1/4			9.9	54.1	
ob			11.3	52.7	

	+	HI	-	Elev
		63.99		
+5			12.5	51.5
N			13.3	50.7
+2			14.3	49.7
+10			14.6	49.4
+30			19.0	45.0
		2A50		
-30			16.8	47.2
N			11.1	52.9
+5			9.0	55.0
cb			7.0	57.0
1/4			4.5	59.5
℄			3.7	60.3
+3			3.2	60.8
+4			2.1	61.9
1/4			0.8	63.2
TP	10.80	73.99	0.80	63.19
cb			9.2	64.8
S			6.2	67.8
TP	0.80	63.99	10.80	63.19
TP.	1.61	52.48	13.12	50.87
Check out on Starting BM			6.86	45.62
				45.62
				.00 ✓

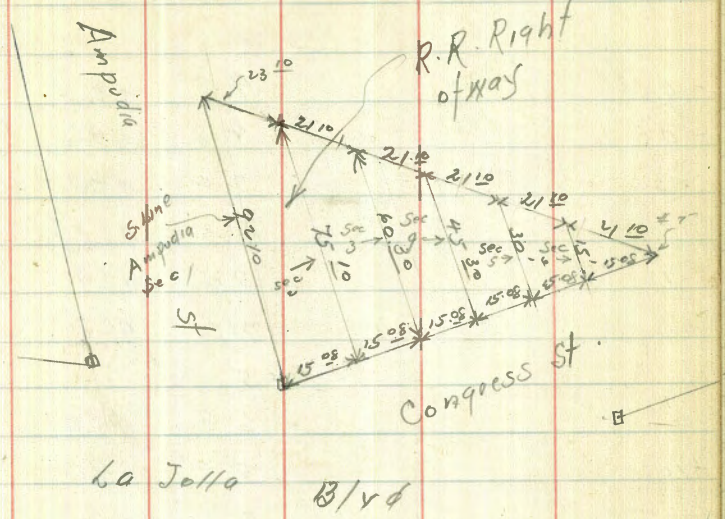
Bill Bliss
Feb 26, 1927

X. Sections of R.R. Right of Way Between Congress & Ampudia

AM S.E. cut stake Ampudia & La Jolla Blvd	8.80	54.42	45.62
		Sec 1 Along S. Prop Line Ampudia	
0+00		9.6	44.8
+5		8.8	45.6
+10		8.5	45.9
+20		9.1	45.3
+30		9.6	44.8
+45		9.0	45.4
+55		8.6	45.8
+75		8.1	46.3
+83		7.3	47.1
+92.10		7.0	47.4
		Sec 2	
-75 E		6.7	47.7
-60		6.8	47.6
-50		7.2	47.2
-37		8.3	46.1
-20		8.5	45.9
-10		8.6	45.8
00		9.1	45.3
		60.30 Sec 3	
00		8.2	46.2
+10		8.1	46.3
+20		7.8	46.6
+30		7.2	47.2

15.08
21.10

18



	54.42		
+40		6.6	47.8
+50		6.0	48.4
+60 30		5.5	48.9
	Sec 4		
-45 30		4.9	49.5
-40		4.8	49.6
-30		5.4	49.0
-20		6.3	48.1
-10		7.0	47.4
00		7.6	46.8
	Sec 5 30°		
00		6.4	48.0
+10		5.4	49.0
+15		5.1	49.3
+20		4.7	49.7
+30		4.1	50.3
	Sec 6		
-15		3.7	50.7
-7		4.3	50.1
00		4.6	49.8
	Sec 7 = 90 5° South along East line of Congress		
00		3.1	51.3
check out on BM		8.80	45.62 ✓

Bill Bliss
Joe Duermot
J Jacobs Zoon
Pete Kiernan
March 13, 1929

1/25.70
1251

Place

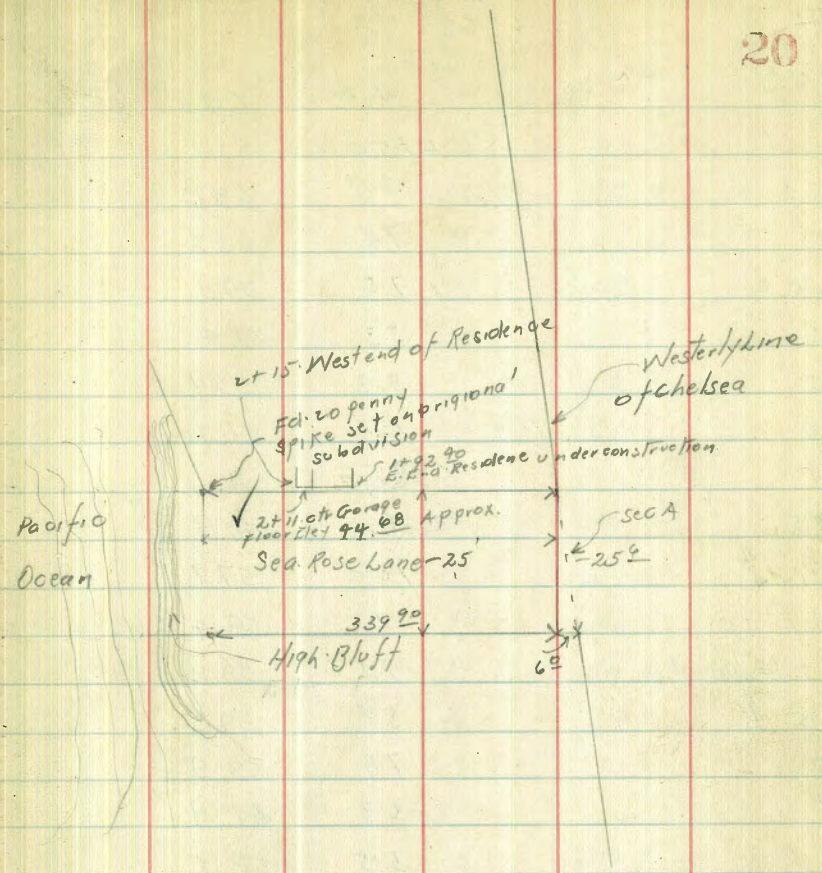
X. Sections Sea Rose Lane
Rumseys Subdivision. Bird Rock by the Sea

BM S W B.P. La Jolla Blvd forward	0.60	75.55		74.95
Set BM. S.E Top Hy. Chelsea forward	3.01	67.68	10.88	64.67

Sec A. = Westerly Line of Chelsea

N Top cb	on paving	3.6 ~	64.06
G		9.0 ~	63.66
72.85 ℄		9.38	63.30
G		9.2 ~	63.46
S Top cb		9.07	63.61
		0+00	
-35		7.0	60.7
-25 S Line		5.4	62.3
-23		4.8	62.9
-12.5 ℄		4.5	63.2
N		4.0 ~	63.66
		0+10	
N		4.5	63.2
+12.5 ℄		4.9	62.8
+25 S Line		5.3	62.4
+35		11.2	56.5
+40		12.2	55.5
		0+25	
-45		16.9	50.8
-28		6.2	61.5
-25 S Line		5.8	61.9
-12.5 ℄		5.5	62.2

Plotted 3-15-29 G.M. Jain



	+	H.I. 67.68	−	Elev
N			4.4	63.3
			0+50	
N		67.7	4.7	63.0
+8			7.1	60.6
+12.5 ℄			7.8	59.9
+25 Shine			8.3	59.4
+35			8.3	59.4
+50			16.6	51.1
			0+75	
−55			16.8	50.9
−42			10.0	57.7
−32			9.3	58.4
−25 Shine			9.5	58.2
−12.5 ℄			8.1	59.6
−10			7.8	59.9
−5			6.3	61.4
N			5.5	62.2
			0+90	
N			6.3	61.4
+10			7.3	60.4
+12.5 ℄			8.0	59.7
+20			8.9	58.8
+25			10.0	57.7
+29			10.8	56.9
+35			10.8	56.9
+40			11.8	55.9

	+	H.I. 67.68	−	Elev
			1+00	
−40		67.7	14.1	53.6
−30			12.4	55.3
−25			11.1	56.6
−20			9.6	58.1
−12.5 ℄			8.1	59.6
−5			7.2	60.5
N			6.6	61.1
			1+25	
N			8.5	59.2
+12.5 ℄			10.4	57.3
+17			10.9	56.8
+25			13.3	54.4
+35			16.0	51.7
+40			16.8	50.9
			1+50	
−40			18.0	49.7
−25 Shine			15.3	52.4
−12.5 ℄			13.1	54.6
N			11.5	56.2
TP	0.77	56.24	12.21	55.47
			1+63	
N		56.2	1.7	54.5
+12.5 ℄			3.4	52.8
+25 Shine			5.2	51.0
+45			8.8	47.4

W1

	+	HI	−	Elev
		56.24		1+92 40 E Edge Bldg 1e Back
		1+75		
−45			10.8	45.4
−25 S.line		56.2	7.8	48.4
−12.5 ℄			6.1	50.1
N			4.3	51.9
		1+88		
N			6.2	50.0
+5			7.2	49.0
+12.5 ℄			8.5	47.7
+20			9.5	46.7
+25 S.line			10.1	46.1
+45			13.0	43.2
		2+00		
−45			15.0	41.2
−35			13.8	42.4
−25 S.line			12.9	43.3
−15			11.8	44.4
−12.5 ℄			11.2	45.0
−5			10.1	46.1
N			9.1	47.1
		2+15		
N			12.9	43.3
T.P.	0.80	44.84	12.20	44.04
		2+11		0.16 Floor Grade
+12.5 ℄			3.0	41.8
+25		44.8	4.2	40.6
+35			4.6	40.2

	+	HI	−	Elev
		44.84		
		2+25		
−35		44.8	5.6	39.2
−25			5.7	39.1
−12.5 ℄			4.7	40.1
N			3.2	41.6
		2+38		
N			6.2	38.6
+12.5 ℄			7.0	37.8
+25			6.7	38.1
+35			6.6	38.2
		2+50		
−25 S.line			7.3	37.5
−12.5 ℄			7.9	36.9
N			8.1	36.7
		2+75		
N			9.0	35.8
+12.5 ℄			9.2	35.6
+25 S.line			8.8	36.0
		3+00		
−25 S.line			9.4	35.4
−12.5 ℄			10.0	34.8
N			10.4	34.4
		3+40		
N			11.6	33.2
+12.5 ℄			11.5	33.3
+25 S.line			11.0	33.8

	+	HI	-	Elev	
		44.84			32.6 / 5 / 37.6
		3+53			
-25			11.6	33.2	
-16			11.8	33.0	
-12.5			11.9	32.9	
N			12.2	32.6	
		3+56			
N			12.2	32.6	
+7			12.0	32.8	
+12.5 ℄			15.4	29.4	
+20			11.8	33.0	
+23			11.8	33.0	
+25 Breaks over edge			16.2	32.6	
		3+62 Extreme Westerly Edge of Bluff			
-25			17.6	27.2	
-12.5 ℄			18.5	26.3	
N			14.6	30.2	
		3+82 N Bottom Bluff			
N	Elev of Beach determined by Triangulation			-1.6	
℄				-2.7	
S				-2.8	
TP.	10.03	53.68	1.19	43.65	
TP	12.73	65.65	0.76	52.92	
TP	10.73	75.56	0.82	64.83	
Check BM SE BP La Jolla Blvd & Midway			3.80	71.76 / 71.80 / 0.04	

Walker
McHugh
Lerty
McHugh
3-22-29

PRELIMINARY LEVELS for SEWER
2' N'ly & W'ly from N'ly line Lot 7 Blk 21
Ocean Beach from ℄ Santa Cruz to ℄ Alley N

	12.90	108.32		95.42	BM Con. Mon SW Santa Cruz & Ebers
℄ Santa Cruz St. = 0+00			0.3	108.0	
+11			0.5	107.8	
+18			3.7	104.6	
+30			5.0	103.3	
+40 = N'ly Line Santa Cruz.			5.0	103.3	
+70			5.1	103.2	
1+00			6.4	101.9	
+25			6.9	101.4	
+50			8.1	100.2	
1+80			9.4	98.9	
+90 = ℄ Alley			10.0	98.3	

Walker
3-22-29

LEVELS ON Top EXISTING Water Main
Located 10' South of SANTA CRUZ St.
Bet. Ebers St. and Guizot St.

108.32 = Above H.I.

−9' = 3' East East cb Line Ebers St.			16.78	91.54	
0+00 = East Line Ebers St.					
+96 on top Water Main			8.73	99.59	
T.P.	12.58	120.87	0.01	108.31	
2+00.5 on Pipe.			10.95	109.94	
+85.5 " "			3.20	117.7	117.69
T.P.	12.92	133.57	0.24	120.65	

133.57

4+11 on Pipe			4.36	129.21
T.P.	12.18	145.44	0.31	133.26
5+74 on Pipe.			2.7	142.74
T.P.	13.01	157.85	0.60	144.84
6+39 on Pipe			9.92	147.93
7+39 " "			2.05	155.8
T.P.	12.96	170.24	0.57	157.28
7+86 on Pipe			9.64	160.60
8+52 " "			3.72	166.52
T.P.	12.94	183.11	0.07	170.17
9+67 on Pipe			5.93	177.18
T.P.	13.05	196.02	0.14	182.97
10+97 on Pipe			6.32	189.70
T.P.	12.96	208.77	0.15	195.87
12+22 on Pipe			5.92	202.85
T.P.	12.71	220.13	1.35	207.42
T.P.	13.25	232.55	0.83	219.30
13+08.3 = East cb Line Guizot St.				
T.P.	12.47	244.74	0.28	232.27
T.P.	12.94	257.54	0.14	244.60
Cut on BM SW BR Santa Barbara & Santa Cruz			2.14	255.40

255.50 = BM.
0.10 = difference

Diamond St Cross Section
Cross to Pendleton

From Cross to Pl. Down
90' Wide
14' Cbs
13' Qts

BM	9.22	53.29		44.07	SE. B.P Diamond & Cross
		E.L Cross			
S			9.0	44.3	
Cb Top			9.06	44.23	
Gutter on Paving			9.46	43.83	
+10 = Edge " From East			9.09	44.20	
¼ on "			9.01	44.28	
℄ " "			8.77	44.52	
¾ = Edge " From East			8.58	44.71	
Gutter on "			8.43	44.86	
Cb " "			7.72	45.57	
N			7.4	45.9	
		10' E of E.L Cross			
N			6.6	46.7	
Cb			7.3	46.0	
¼			8.3	45.0	
+3 = Edge Paving			8.48	44.81	
℄ on "			8.40	44.89	
+10 = Edge "			8.56	44.73	
¼			8.3	45.0	
Cb			9.0	44.3	
S			8.8	44.5	
		50' E			
S			8.3	45.0	
Cb			7.9	45.4	

Plotted 5-28-30
CBH

53.29

26
12-12-29
Sussex
Mt Hope
Northern
Remmen

		53.3
+2	7.8	45.5
¼	8.7	44.6
¼	8.1	45.2
+3 = Edge Paving	8.00	45.3
℄ on "	7.83	45.46
+10 = Edge "	7.87	45.42
¼	7.9	45.4
+5	7.4	45.9
Cb	6.8	46.5
N	6.4	46.9
	100' E	
N	6.0	47.3
Cb	6.3	47.0
+10	7.4	45.9
¼	7.3	46.0
+3 = Edge Paving	7.23	46.06
℄ on "	7.12	46.17
+10 = Edge "	7.29	46.00
¼	7.4	45.9
+8	8.5	44.8
Cb	7.3	46.0
S	7.6	45.7
	150' E	
S	7.1	46.2
Cb	6.9	46.4
+6	8.2	45.1

Diamond St

5329

		53.3
¼	6.8	46.5
+3 = Edge Pav	6.64	46.65
℄ on "	6.48	46.81
+10 = Edge "	6.53	46.76
¼	6.6	46.7
Cb	6.0	47.3
H	5.7	47.6
200' E		
H	5.1	48.2
Cb	5.5	47.8
+7	6.3	47.0
¼	6.0	47.3
+3 = Edge Pav	5.84	47.45
℄ on "	5.78	47.51
+10 = Edge "	5.94	47.35
¼	6.1	47.2
+7	6.9	46.4
Cb	6.2	47.1
S	6.5	46.8
250' E		
S	6.0	47.3
Cb	5.5	47.8
+6	6.3	47.0
¼	5.5	47.8
+3 = Edge Pav	5.31	47.98
℄ on "	5.14	48.15

5329

		53.3
+10 = Edge Pav	5.16	48.13
¼	5.3	48.0
+6	5.8	47.5
Cb	4.8	48.5
H	4.5	48.8
300' E		
H	3.6	49.7
Cb	4.0	49.3
+9	5.0	48.3
¼	4.6	48.7
+3 = Edge Pav	4.50	48.79
℄ on "	4.47	48.82
+10 = Edge "	4.64	48.65
¼	4.7	48.6
+7	6.0	47.3
+10	4.7	48.6
Cb	4.9	48.4
S	5.2	48.1
350' E		
S	4.5	48.8
○○ Conc Drive	4.22	49.07
Cb	4.1	49.2
+4	4.2	49.1
+6	4.9	48.4
¼	4.1	49.2
+3 = Edge Pav	3.93	49.36

53.29

		53.3		
℄ on Paving	3.82	49.47		
+10 = Edge "	3.88	49.41	3.28' E on ℄ Conc Walk	
¼	3.9	49.4	3.69	49.60
+4	4.1	49.2		
Cb	3.0	50.3		
N	2.9	50.4		
400' E				
N	2.0	51.3		
Cb	2.3	51.0		
+4	2.3	51.0		
+8	3.5	49.8		
¼	3.3	50.0		
+3 = Edge Paving	3.14	50.15		
℄ on "	3.12	50.17		
+10 = Edge	3.24	50.05		
¼	3.3	50.0		
+6	4.3	49.0		
+9	3.2	50.1		
Cb	3.2	50.1		
S	3.6	49.7		
450' E = Beginning of Curb + Walk on N				
S	2.4	50.9		
Cb	2.2	51.1		
+5	2.3	51.0		
+7	3.3	50.0		
¼	2.6	50.7		

53.29

		53.3		
+3 = Edge Pav	2.59	50.70		
℄	2.44	50.85		
+10 = Edge	2.47	50.82		
¼	2.4	50.9		
+7 = Gutter	2.3	51.0		
+7 Top Existing Cb	1.93	51.36	Dawes 50' wide 20' Cbs 16' Qts	
Cb	1.9	51.4		
N	1.6	51.7		
500' E = N.L. Dawes			Note: Existing top of Curb + Walk + Return N.M. Cor. Diamond + Dawes was put in 20' Cbs	
N	1.1	52.2		
Cb	1.3	52.0		
+6 = Top Existing Cb	1.30	52.00		
Gutter	1.6	51.7		
¼	1.7	51.6		
+3 = Edge Pav	1.77	51.52	From N.L. Dawes East Cross St. 50' wide 20' Cbs 16' Qts	
℄ on "	1.77	51.52		
+10 = Edge "	1.91	51.38		
¼	2.2	51.1		
+6	2.2	51.1		
+8	1.4	51.9		
Cb	1.3	52.0		
S	1.0	52.3		
B.M. 7.70 59.96	1.23	52.06	N.W. Cor Diamond + Dawes	
N Cb of Dawes		59.8		
S	7.8	52.0		
Cb	8.1	51.7		

Diamond St.

	59.76		Diamond 80' Wide joints
			59.80 Cbs
¼ = Edge Pav		8.11	51.65
℄ on "		8.00	51.76
¼ = Edge "		8.03	51.73
Cb		8.0	51.8
N		7.4	52.4
	¼		
N		6.4	53.4
Cb		7.2	52.6
¼ = Edge Paving		7.90	51.86
℄ on "		7.86	51.90
¼ = Edge "		7.97	51.79
Cb		7.9	51.9
S		8.1	51.7
	℄ Dam		
S		8.0	51.8
Cb		7.6	52.4
¼ = Edge Pav		7.87	51.89
℄ on "		7.72	52.04
¼ = Edge "		7.76	52.00
Cb		7.1	52.7
N		5.9	53.9
	¼		
N		6.3	53.5
Cb		7.1	52.7
¼ = Edge Pav		7.44	52.12
℄ on "		7.60	52.16

	59.76		59.8
¼ = Edge Pav		7.74	52.02
Cb		7.5	52.3
S		7.8	52.0
	℄ Cb		
S		7.2	52.6
Cb		7.3	52.5
¼ = Edge Pav		7.63	52.13
℄ on "		7.51	52.25
¼ Edge "		7.51	52.25
Cb		7.1	52.7
N		5.9	53.9
	℄ Line of Dam		
N		5.1	54.7
Cb		5.8	54.0
+3		7.3	52.5
¼ = Edge Pav		7.32	52.48
℄ on "		7.24	52.52
¼ = Edge "		7.38	52.38
+5		7.1	52.2
Cb		6.7	53.1
S		6.8	53.0
	50' E of ℄ Dam		
S		6.3	53.5
Cb		6.0	53.8
+2		7.4	52.4
¼ = Edge Pav		6.53	53.23

	59.76		
			59.8
℄ on Paving		6.38	53.38
⅓ = Edge "		6.40	53.36
+8		6.7	53.1
Cb		5.2	54.6
N		4.6	55.2
	100 E		
N		4.2	55.5
Cb		4.6	55.2
+2		6.1	53.7
⅓ = Edge Pav		5.59	54.17
℄ on "		5.54	54.22
⅓ = Edge "		5.66	54.10
+8		6.9	52.9
Cb		5.4	54.4
S		5.5	54.3
	150 E		
S		5.2	54.6
Cb		5.1	54.7
+1		5.6	54.2
⅓ = Edge Pav		4.83	54.93
℄ on "		4.70	55.06
⅓ = Edge "		4.71	55.05
+8		4.9	54.9
Cb		4.0	55.8
N		3.6	56.2
	200 E		

179 E = Tree 15.5 of PL of Boulevard

	59.76		
			59.8
N = Conc. Walk		2.25	57.51
Cb		3.4	56.4
⅓ = Edge Pav		3.87	55.89
℄ on "		3.84	55.92
⅓ = Edge "		3.96	55.80
Cb		5.1	54.7
+1		4.3	55.5
S		4.7	55.1
	250 E		
S		3.3	56.5
Cb		3.0	56.8
+1		4.0	55.8
⅓ = Edge Pav		3.12	56.64
℄ on "		3.00	56.76
⅓ = Edge "		2.98	56.78
+9		3.4	56.4
Cb		2.1	57.7
N		1.7	58.1
	300 E		
N		0.5	59.3
+18		0.8	59.0
Cb		2.5	57.3
⅓ = Edge Pav		2.15	57.61
℄ on "		2.12	57.64
⅓ = Edge		2.28	57.48
+8		2.7	57.1

220 E = Tree 17.5 of PL of Boulevard

Diamond St.

		59.76		59.8
Cb			1.9	57.9
S			1.9	57.9
	350 E			
S			1.0	58.8
Cb			0.7	59.1
+2			1.8	58.0
1/4 = Edge Pav			1.43	58.33
1/2 on "			1.27	58.49
1/4 Edge "			1.29	58.47
Cb			1.8	58.0
+4			0.0	59.8
H			0.1	59.7
TP	6.11	64.53	1.34	58.42
	400 E			64.5
H			4.3	60.2
+16			4.3	60.2
Cb			5.5	59.0
1/4 = Edge Pav			5.22	59.31
1/2 on "			5.19	59.34
1/4 = Edge "			5.31	59.22
Cb			5.9	58.6
+1			5.2	59.3
S			5.5	59.0
	411 E = Beginning Cb. Walk + Solid Paving			
S			5.3	59.2
Cb Top of Existing			5.57	58.96

		64.53		64.5
Gutter on Paving			6.02	58.51
1/4 " "			5.13	59.40
1/2 " "			5.01	59.52
1/4 " "			5.03	59.50
Gutter " "			5.25	59.28
Cb Top			4.55	59.98
H			4.2	60.3
	450 E			
H			3.6	60.9
Cb Top			3.95	60.58
Gutter on Paving			4.71	59.82
1/4 " "			4.39	60.14
1/2 " "			4.35	60.18
1/4 " "			4.47	60.06
Gutter " "			5.41	59.12
Cb Top			4.90	59.63
S			4.80	59.73
	486.5 E = PC of Cb Return			
S			4.0	60.5
Cb Top			4.15	60.38
Gutter on Pav			4.69	59.84
1/4 " "			3.86	60.67
1/2 " "			3.75	60.78
1/4 " "			3.76	60.77
Gutter " "			4.17	60.36
Cb Top			3.45	61.08

6453

N			3.1	61.4	
BM	9.52	70.59	3.46	61.07	NW Cor Diamond & Everts
TP	6.67	75.39	1.87	68.72	NW Cor
BM			5.02	70.37	Diamond & Gresham
		F.L. Gresham		75.4	
N			4.4	71.0	
+18 = End Cb Ret Top			4.72	70.67	
Gutter on Paving			5.35	70.04	
¼ = Edge "			5.50	69.89	
℄ on "			5.43	69.96	
¼ = Edge "			5.49	69.90	
Cb on "			5.90	69.49	
+15 = End Cb Ret			5.99	69.40	
Top Cb			5.42	69.97	
S			5.0	70.4	
		50' E of F.L. Gresham			
S			5.0	70.4	
Cb			5.0	70.4	
¼ = Edge Pav			4.70	70.69	
℄ on "			4.56	70.83	
¼ = Edge "			4.60	70.79	
+6			5.2	70.2	
+7			4.0	71.4	
Cb			4.1	71.3	
N			3.6	71.8	
	100' E				

Plotted 5-28-30 C.D.H.

7539

			75.4
N		3.4	72.0
Cb		3.8	71.6
+3		3.8	71.6
+4		4.8	70.6
¼ = Edge Pav		3.94	71.45
℄ on "		3.90	71.49
¼ = Edge "		4.05	71.34
+7		5.0	70.4
+8		4.3	71.1
Cb		4.1	71.3
S		4.7	70.7
	150' E		
S		3.9	71.5
Cb		3.4	72.0
+2		3.7	71.7
+3		4.3	71.1
¼ = Edge Pav		3.43	71.96
℄ on "		3.29	72.10
¼ = Edge		3.34	72.05
+6		3.7	71.7
+7		2.9	72.5
Cb		2.9	72.5
N		2.7	72.7
	200' E		
N		1.9	73.5
Cb		2.3	73.1

Diamond St.

75.39

			75.4
+3	2.4	73.0	
+4	3.3	72.1	
½ = Edge Par	2.68	72.71	
℄ on "	2.65	72.74	
½ = Edge	2.81	72.58	
+7	3.3	72.1	
+8	2.5	72.9	
Cb	2.6	72.8	
S	3.1	72.3	
250' E			
S	1.2	74.2	
Cb	1.5	73.9	
+2	1.6	73.8	277' E on S.L. = Conc. walk 0.93
+3	2.6	72.8	74.61
½ = Edge Par	2.18	73.21	
℄ on "	2.07	73.32	294' E on S.L. Solid Conc. Dr. 0.56
½ = Edge "	2.10	73.29	74.83
+6	2.7	72.7	
+7	1.9	73.5	
Cb	1.7	73.7	
N	1.6	73.8	
300' E			
N	0.4	75.0	
Cb	0.8	74.6	
+2	0.8	74.6	
+3	2.2	73.2	

			75.4
½ = Edge Par		1.46	73.93
℄ on "		1.42	73.97
½ = Edge "		1.53	73.86
+8		1.9	73.5
Cb		1.0	74.4
S		0.6	74.8
TP	8.72	83.69	0.42	74.97
350' E			83.7
S		7.9	75.8
Cb		8.8	74.9
+4		9.7	74.0
½ = Edge Par		9.22	74.47
℄ on "		9.10	74.59
½ = Edge "		9.16	74.53
+6		9.4	74.3
+7		8.0	75.7
Cb		7.9	75.8
N		7.8	75.9
400' E			
N		7.0	76.7
Cb		7.1	76.6
+3		7.1	76.6
+4		8.7	75.0
½ = Edge		8.56	75.20
℄ on "		8.46	75.23
½		8.61	75.08

	83.69		83.7
+7		8.5	75.2
+8		7.9	75.8
Cb		7.9	75.8
S		7.1	76.6
	450' E		
S		6.9	76.8
Cb		7.5	76.2
+2		7.6	76.1
+4		8.9	74.8
½ = Edge Par		7.98	75.71
⅛ " "		7.84	75.85
½ = Edge "		7.89	75.80
+6		8.3	75.4
+8		6.6	77.1
Cb		6.8	76.9
N		6.6	77.1
	500' E = N L Haines		
N		6.1	77.6
Cb		6.4	77.3
+3		6.3	77.4
+4		7.5	76.2
½ = Edge Par		7.34	76.35
⅛ " "		7.28	76.41
½ = Edge "		7.31	76.38
+7		8.2	75.5
+8		7.1	76.6

80' W side 30' Cb S

	83.69		83.7
Cb		7.0	76.7
S		6.7	77.0
	N Cb		
S		6.5	77.2
+10		5.0	78.7
Cb		6.6	77.1
+4		7.8	75.9
½ = Edge Par		7.48	76.21
⅛ " "		7.32	76.37
½ = Edge "		7.32	76.37
+6		7.3	76.4
+8		5.9	77.8
Cb		6.2	77.5
N		5.8	77.9
	½		
N		6.2	77.5
Cb		7.3	76.4
½ = Edge Par		7.36	76.33
⅛ " "		7.40	76.29
½ = Edge "		7.57	76.12
+6		7.7	76.0
Cb		6.7	77.0
+5		5.6	78.1
S		6.0	77.7
	L. Haines		
S		6.4	77.3

Diamond St.

	83.69		83.7
+15		6.2	77.5
Cb		6.8	76.9
+5		7.8	75.9
¼ = Edge Pav		7.68	76.01
⊼ on "		7.47	76.22
¼ = Edge "		7.43	76.26
+6		7.3	76.4
Cb		6.0	77.7
N		5.7	78.0
	¼		
N		5.4	78.3
Cb		5.6	78.1
+3		5.9	77.8
+4		7.5	76.2
¼ = Edge Pav		7.49	76.20
⊼ on "		7.56	76.13
¼ Edge "		7.76	75.93
+5		7.9	75.8
+6		6.9	76.8
Cb		6.3	77.4
S		6.4	77.3
	Cb		
S		6.4	77.3
Cb		6.3	77.4
+4		6.8	76.9
+5		7.9	75.8

	83.69		83.7
¼ = Edge Pav		7.83	75.86
⊼ on "		7.62	76.07
¼ = Edge "		7.59	76.10
+6		7.6	76.1
+7		5.7	78.0
Cb		5.5	78.2
N		5.5	78.2
	E L Haines		
N		5.8	77.9
Cb		5.8	77.9
+3		5.8	77.9
+4		7.7	76.0
¼ = Edge Pav		7.47	76.32
⊼		7.42	76.27
¼ = Edge		7.52	76.17
+5		7.5	76.2
+6		6.1	77.6
Cb		6.5	77.2
S		6.5	77.2
	50 E of E L Haines		
S		5.7	78.0
Cb		6.3	77.4
+3		6.6	77.1
+4		7.5	76.2
¼ = Edge Pav		7.02	76.67
⊼		6.88	76.81

	83.69		83.7
1/4 = Edge Pav.		6.91	76.78
+6		7.5	76.2
+7		5.7	78.0
Cb		5.7	78.0
H		5.7	78.0
	100' E		
H		5.3	78.4
Cb		5.2	78.5
+2		5.7	78.0
+3		7.1	76.6
1/4 = Edge Pav		6.58	77.11
⊥ on "		6.55	77.14
1/4 = Edge "		6.70	76.99
+6		7.2	76.5
+7		6.4	77.3
Cb		6.3	77.4
+13		6.4	77.3
S		5.8	77.9
	150' E		
S		5.7	78.0
+7		6.6	77.1
Cb		6.1	77.6
+4		6.7	77.0
1/4 = Edge Pav		6.37	77.32
⊥ on		6.24	77.45
1/4 =		6.26	77.43

	83.69		83.7
+6		6.9	76.8
+7		5.3	78.4
Cb		5.2	78.5
H		5.3	78.4
	200' E		
H		5.3	78.4
Cb		5.3	78.4
+2		5.3	78.4
+3		6.4	77.3
1/4 = Edge Pav		5.92	77.77
⊥ on "		5.91	77.78
1/4 = Edge "		6.04	77.65
+5		6.4	77.3
+6		5.6	78.1
Cb		5.6	78.1
+13		6.4	77.3
S		5.7	78.0
	250' E		
S		5.1	78.6
+7		6.0	77.7
Cb		5.7	78.0
1/4 = Edge Pav		5.72	77.97
⊥ on "		5.56	78.13
1/4 = Edge "		5.60	78.09
+6		6.0	77.7
+8		4.9	78.8

Diamond St.

		83.69		83.7	
Cb			4.7	79.0	
H			4.9	78.8	
TP	971	87.91	5.49	78.80	
	30' E			87.9	271' E = TPC 13.5 of HL
H			8.6	79.3	
Cb			9.2	78.7	308' E = TPC 13.5 of HL
1/4 = Edge Pav			9.42	78.49	
2 on "			9.41	78.50	
1/4 = Edge "			9.57	78.34	
Cb			9.5	78.4	
+13			9.6	78.3	344' E = TPC 13.5 of HL
S			9.0	78.9	
	850' E				
S			8.7	79.2	
+8			9.3	78.6	
Cb			9.0	78.9	
1/4 = Edge Pav			8.59	79.32	
2 on "			8.44	79.47	
1/4 = Edge "			8.50	79.41	388' E = TPC 13.5 of HL
Cb			8.8	79.1	
H			8.3	79.6	
	400' E				
H			8.2	79.7	
Cb			7.6	80.3	
1/4 = Edge Pav			7.47	80.44	
2 on "			7.45	80.46	

		87.91		87.9	37
1/4 = Edge Pav			7.63	80.28	
Cb			7.8	80.1	434' E = TPC 13.5 of HL
+13			8.3	79.6	
S			7.5	80.4	
	450' E				
S			6.6	81.3	459' E = TPC 13.5 of HL
+9			7.3	80.6	
Cb			6.8	81.1	
1/4 = Edge Pav			6.60	81.31	470' E Concrete 20' S of HL
2 on "			6.45	81.46	6.70
1/4 = Edge			6.48	81.43	81.81
Cb			6.4	81.5	
H			6.2	81.7	
	500' E = HL Ingraham				80' Hydr 20' Cbc
H			4.6	83.3	
Cb			5.1	82.8	
1/4 = Edge Pav			5.55	82.36	
2 on "			5.54	82.37	
1/4 = on "			5.65	82.26	
+5 = Edge "			5.56	82.35	
Cb			5.6	82.3	
S			6.2	81.7	
	H Cb				
S			6.0	81.9	
+7 = Edge Pav			5.55	82.36	
Cb " 7 "			5.41	82.45	

	87.91		87.9
			87.52
¼ on Pav		5.39	87.66
℄		5.25	82.62
¼ = Edge Pav		5.29	82.7
+5		5.2	83.5
Cb		4.4	84.1
H		3.8	
	¼		
N		4.1	83.8
Cb		4.8	83.1
¼ = Edge Pav		5.14	82.77
℄ on "		5.13	82.78
¼ " "		5.24	82.67
Cb " "		5.30	82.61
S " "		5.40	82.51
	℄ Ingraham		
S on Paving		5.38	82.53
Cb " "		5.14	82.77
¼ " "		5.08	82.83
℄ " "		4.97	82.94
¼ = Edge "		5.02	82.89
Cb		4.5	83.4
H		3.9	84.0
	¼		
N		3.7	84.2
Cb		4.3	83.6
¼ = Edge Pav		4.82	83.09

	87.91		87.9
			83.09
℄ on Pav		4.82	83.00
¼ " "		4.91	82.90
Cb " "		5.01	82.50
S " "		5.41	
	E Cb		
S		5.3	82.6
+1.35 = Edge Pav		5.08	82.83
Cb on "		4.90	83.01
¼ " "		4.76	83.15
℄ " "		4.63	83.28
¼ = Edge "		4.66	83.25
Cb		4.1	83.8
H		3.9	84.0
	E.L. Ingraham		
N		2.9	85.0
Cb		3.3	84.6
¼ = Edge Pav		4.41	83.50
℄ on "		4.35	83.56
¼ " "		4.47	83.44
+3 = Edge "		4.52	83.39
Cb		4.5	83.4
S		4.6	83.3
B.M.		5.16	82.75	Sept Diamond & Ingraham 83.8° NE Mon
B.M.		2.69	85.22	Diamond & Ingraham 85.22

Diamond St.

BM	814	93.36		85.22	NE Mon Diamond & Ingraham
		50' E of E & Ingraham		93.4	
S			8.5	84.9	
Cb			9.1	84.3	
+3			8.8	84.6	
+4			9.4	84.0	
1/4 = Edge Pav			9.07	84.29	
℄ on "			8.91	84.45	
1/4 = Edge "			8.92	84.44	
+6			9.2	84.2	
Cb			7.5	85.9	
N			7.2	86.2	
		100' E			
N			5.8	87.6	
Cb			6.1	87.3	
+4			8.2	85.2	
1/4 = Edge Pav			8.00	85.36	
℄ on "			7.97	85.39	
1/4 Edge "			8.10	85.26	
+6			8.2	85.2	
Cb			7.9	85.5	
S			7.6	85.8	
		150' E			
S			6.4	87.0	
Cb			6.5	86.9	

93.36

		93.4
+4	7.3	86.1
1/4 = Edge Pav	7.13	86.23
℄ on "	7.01	86.35
1/4 = Edge "	7.04	86.32
+6	7.1	86.3
Cb	4.9	88.5
N	4.8	88.6
170' E = Beg of Cb & Walk on S		
N	4.5	88.9
Cb	4.7	88.7
+4	6.6	86.8
1/4 = Edge Pav	6.72	86.64
℄ on "	6.68	86.68
1/4 Ed	6.76	86.60
Cb Existing	7.17	86.19
S	1.2	87.2
220' E = End of Cb & Walk on S		
S	5.5	87.9
Cb Existing Ground	6.19	87.17
1/4 = Edge Pav	5.83	87.53
℄ on "	5.28	87.68
1/4 = Edge "	5.91	87.65
79	5.1	88.3
Cb	4.0	89.4
N	3.7	89.7
250' E		

	93.36		93.4
N		3.5	89.9
cb		3.9	89.5
+1		5.1	88.3
½ = Edge Par		5.13	88.23
L on "		5.14	88.22
½ = Edge "		5.28	88.08
+7		5.9	87.5
cb		5.1	88.3
S		5.4	88.0
	300 E		
S		4.7	88.7
cb		4.2	89.2
+4		4.6	88.8
½ = Edge Par		4.31	89.05
L on "		4.20	89.16
½ = Edge "		4.20	89.16
+9		4.7	88.7
cb		3.1	90.3
N		3.0	90.4
	350 E		
N		2.2	91.2
cb		2.6	90.8
+1		3.9	89.5
½ = Edge Par		3.26	90.10
L on "		3.22	90.14
½ = Edge "		3.37	89.99

	93.36		93.4
+6		3.8	89.6
cb		3.3	90.1
S		3.8	89.6
	400 E		
S		3.2	90.2
cb		2.6	90.8
+4		2.9	90.5
½ = Edge Par		2.41	90.95
L on "		2.37	91.09
½ = Edge "		2.29	91.07
+9		2.4	91.0
cb		1.8	91.6
N		1.5	91.9
	450 E		
N		0.8	92.6
cb		1.1	92.3
+1		1.6	91.8
½ = Edge Par		1.34	92.02
L on "		1.29	92.07
½ = Edge "		1.42	91.94
+6		2.1	91.3
cb		2.0	91.4
S		2.7	90.7
	500 E		
S		1.5	91.9
cb		0.8	92.6

446 E = Lg Palm 145 of HL

Diamond St.

		9336			
			1.3	93.4 / 92.1	
+4					
1/4 = Edge Pav			0.43	92.93	
⅛ on "			0.32	93.04	495 E = 4 Palm
1/4 = Edge "			0.38	92.98	14.5 of ft.
+9			0.7	92.7	
Cb			0.3	93.1	
H			0.2	93.2	
TP	7.59	10051	0.44	92.92	
		520 E = 92.2	Sewell	100.5	80 Hide 20 Cbs 10 Qts
N			6.9	93.6	
Cb			7.1	93.4	
+1			7.4	93.1	
1/4 = Edge Pav			7.15	93.36	
⅛ on "			7.14	93.37	
1/4 = Edge "			7.22	93.29	
+6			7.9	92.6	
Cb			7.7	92.8	
S			7.8	92.7	
8H			6.54	93.95	3 H Pol Diamond & Sewell 9207
		N Cb			
S			8.2	92.3	
Cb			7.5	93.0	
+4			8.1	92.4	
1/4 = Edge Pav			7.30	93.2	
⅛			7.11	93.35	
1/4 " "			7.18	93.33	
+9			7.3	93.2	

		10051			
			6.6	100.5 / 93.9	
Cb			6.4	94.1	
H					
		1/4			
H			6.7	93.8	
Cb			6.9	93.6	
1/4 = Edge Pav			7.20	93.3	
⅛ on "			7.30	93.31	
1/4 = Edge "			7.36	93.15	
Cb			7.8	92.7	
S			8.7	91.8	
		⅛ Sewell			
S			8.2	92.3	
Cb			7.4	93.1	
1/4 = Edge Pav			7.42	93.09	
⅛ on "			7.27	93.24	
1/4 = Edge			7.25	93.26	
Cb			6.8	93.7	
H			6.4	94.1	
		1/4			
H			5.9	94.6	
Cb			7.3	93.2	
1/4 = Edge Pav			7.39	93.12	
⅛ on "			7.41	93.10	
1/4 = Edge "			7.59	92.92	
Cb			7.5	93.0	
S			7.9	92.6	

100+51

			ECb
S	7.9	92.6	100.5
Cb	7.6	92.9	
¼ = Edge Pav	7.77	92.74	
℄	7.54	92.97	
¼ = " "	7.45	93.06	
Cb	7.2	93.3	
H = Top Cb & Ground	6.64	93.87	
			F L Sewell = Beginning of Cb & Walk on M
H	5.8	94.7	N E Cb Return & Walk
Cb Top Existing	6.51	94.00	
Gutter	7.1	93.4	
¼ = Edge Pav	7.21	93.30	
℄ on "	7.31	93.20	
¼	7.51	93.00	
+6	7.4	93.1	
Cb	6.6	93.9	
S	7.5	93.0	
			50' E of F L Sewell
S	7.8	92.7	
Cb	6.4	94.1	
¼	6.14	94.37	
℄	6.01	94.50	
¼	6.60	94.51	
Gutter	6.30	94.21	
Cb Top Existing	5.47	95.04	

100+51

			100.5
H	4.9	95.6	
	100' E		
H	3.9	96.6	100' E of S = Shed 16' long 19' in Street
Cb Top Existing	4.41	96.10	
Gutter	5.3	95.2	
¼ = Edge Pav	4.90	95.61	
℄ on "	4.91	95.60	
¼ = Edge "	5.07	95.44	
+7	5.3	95.2	
Cb	6.5	94.0	
S	7.5	93.0	
	150' E		
S	7.3	93.2	
Cb	4.8	95.7	
¼ = Edge Pav	3.99	96.52	
℄ on "	3.82	96.69	
¼	3.83	96.68	
Gutter	4.21	96.30	
Cb Top Existing	3.32	97.19	
H	2.8	97.7	
	200' E		
H	1.7	98.8	
Cb Top Existing	2.20	98.31	
Gutter	2.8	97.7	
¼ = Edge Pav	2.71	97.80	
℄ on "	2.71	97.80	

Diamond St.

		100.51		100.5
½ = Edge Pav			2.88	97.63
Cb			3.4	97.1
S			5.4	95.1
	250' E			
S			2.5	98.0
Cb			1.6	98.9
+6			2.1	98.4
½ = Edge Pav			1.80	98.71
℄ on "			1.65	98.86
½ = Edge "			1.73	98.78
Gutter			1.7	98.8
Cb Top Existing			1.12	99.39
H			0.8	99.7
TP	12.65	111.91	1.25	99.26
	290' E = End Walk + Cb on H			111.9
H			11.3	100.6
Cb Top			11.65	100.26
Gutter			11.9	100.0
½ = Edge			12.17	99.74
℄			12.10	99.81
½ = Edge			12.23	99.68
+6			12.5	99.4
Cb			11.3	100.6
S			12.0	99.9
	300' E			
S			11.8	100.1

		111.91		111.9
Cb			11.1	100.8
+3			11.0	100.9
+5			12.4	99.5
½ = Edge Pav			12.01	99.90
℄ on "			11.88	100.03
½ = Edge "			11.96	99.95
+6			11.9	100.0
Cb			11.1	100.8
H			9.2	102.7
	350' E			
H			7.0	104.9
Cb			7.2	104.7
+4			11.0	100.9
½ = Edge Pav			10.84	101.07
℄ on "			10.81	101.10
½ = Edge "			10.91	101.00
+6			11.3	100.6
Cb			7.9	104.0
S			8.7	103.2
	400' E			
S			6.0	105.9
Cb			5.8	106.1
+5			9.5	102.4
½ = Edge Pav			9.85	102.06
℄			9.71	102.20
½ = Edge			9.74	102.17

314' E = West End of 11 Cypress Trees 14' N of SL

		111.91		
				111.9
+5			9.9	102.0
Cb			4.6	107.3
H			5.0	106.9
	426' E			
H			4.1	107.8
Cb			3.8	108.1
+5			9.7	102.2
1/4 - Edge Pav			9.34	102.57
℄ on "			9.25	102.66
1/4 - Edge "			9.34	102.57
+5			8.9	103.0
Cb			4.6	107.3
S			5.1	106.8
	460' E			
S			3.7	108.2
+15			3.5	108.4
Cb			5.7	106.2
+5			9.1	102.8
1/4 - Edge Pav			8.54	103.37
℄ on "			8.44	103.47
1/4 - Edge "			8.52	103.39
+5			9.0	102.9
Cb			2.9	109.0
H			3.3	108.6
	500' E			
H			3.3	109.6

		111.91		
				111.9
Cb			2.5	109.4
+4			8.3	103.7
1/4 - Edge Paving			7.95	103.96
℄ on "			7.92	103.99
1/4 - Edge "			8.01	103.90
+6			8.5	103.4
Cb			3.0	108.9
S			3.0	108.9
	540' E			
S			3.0	108.9
Cb			3.5	108.4
+4			8.4	103.5
1/4 - Edge Paving			7.64	104.27
℄ on "			7.53	104.38
1/4 - Edge "			7.56	104.35
+6			7.9	104.0
Cb			2.1	109.8
H			2.2	109.7
	600' E			
H			2.9	109.0
Cb			3.1	108.8
+4			7.3	104.6
1/4 - Edge Pav			7.37	104.54
℄ on "			7.30	104.61
1/4 - Edge "			7.44	104.47
+6			7.8	104.1

485' E = East End of 11 Cypress Tree 14" at GSL

543' E = Large Palmetto 15' of PL

559' E = Large Poppy Tree 5' of PL

Diamond St

		111.91			
Cb			8.6	108.3	
S			4.7	107.2	
TP	4.93	109.60	7.24	104.67	
	650' E			109.6	
S			4.3	105.3	
Cb			3.2	106.4	
43			5.3	104.3	
44 = Edge Pav			4.92	104.68	
4			4.80	104.80	
44 = " "			4.87	104.73	
45			5.3	104.3	
Cb			1.7	107.9	
H			1.4	108.2	
	700' E				
H			2.4	107.2	
Cb			3.4	106.2	
45			5.0	104.6	
44 = Edge Pav			4.15	104.95	
8 on "			4.58	105.02	
44 = Edge			4.70	104.90	
Cb			4.6	105.0	
S			5.1	104.5	
	750' E				
S			6.5	103.1	
Cb			4.9	104.7	
44 = Edge Pav			4.52	105.08	

		109.60			
				109.6	
E on Pav			4.39	105.21	
44 = Edge "			4.47	105.13	774 E of HL = Solid Conc Drive 246
Cb			4.1	105.5	
8			2.2	107.4	107.14
		800' E			
7			2.6	107.0	782' E = Olive Tree 15' S of HL
Cb			3.9	105.7	
44 = Edge Pav			4.29	105.31	
8			4.25	105.35	808' E = Olive Tree 15' S of HL
44 = " "			4.37	105.23	
Cb			5.6	104.0	830' E = Olive Tree 15' S of HL
S			6.9	102.7	
		850' E			
S			6.7	102.9	
Cb			5.5	104.1	856 E = Olive Tree 15' S of HL
44 = Edge Pav			4.19	105.41	
8			4.04	105.56	
44 = " "			4.09	105.51	878' E = Olive Tree 15' S of HL
46			4.6	105.0	
Cb			4.0	105.6	
7			2.7	106.9	
		900' E			
H			2.8	106.8	
Cb			2.3	106.3	905' E = Olive Tree 15' S of HL
44			4.3	105.3	
44 = Edge Pav			3.86	105.74	

	109.60			
			109.6	
Z on Pav		3.84	105.76	
⅊ = Edge "		4.01	105.59	
Cb		5.1	104.5	
S		6.1	103.5	
950' E				
S		4.9	104.9	950' E = Olivetti 15' S of ML
Cb		4.2	105.4	
⅊ = Edge Pav		3.76	105.84	
Z		3.14	105.96	952' E = Olivetti 15' S of ML
⅊ = " "		3.15	105.95	
+6		4.0	105.6	
Cb		2.8	106.8	975' E = Olivetti 15' S of ML
H		2.4	107.2	
1000' E				
H		1.4	108.2	
Cb		1.8	107.8	
+4		3.2	106.4	
⅊ = Edge Pav		3.43	106.17	
Z		3.43	106.17	
⅊ = " "		3.59	106.01	1045' E = Olivetti 15' S of ML
Cb		3.6	106.0	
Z		4.4	105.2	
1050' E				
S		4.2	105.4	
Cb		3.0	106.7	
⅊ = Edge Pav		3.38	106.22	

			109.6	
Z on Pav		3.23	106.37	
⅊ = Edge "		3.24	106.36	
+6		3.0	106.6	
Cb		2.2	107.4	
H		1.3	108.3	
1080' E = ML Lamont				
H		2.3	107.3	Lamont lot is Paved + 4 Pillars in
Cb Top		2.66	106.94	
Gutter on Paving		3.23	106.37	
⅊ " "		3.08	106.52	
Z " "		3.11	106.49	
⅊ " "		3.23	106.37	
Gutter " "		3.76	105.84	
Cb Top		3.38	106.22	
S		3.5	106.1	
BM 375 109.66		3.69	105.91	S 4.8 P Dumont + Lamont 105.95
H Cb			109.66	
S		3.75	105.91	
Gutter on Paving		4.41	105.25	
Cb " "		3.86	105.80	
⅊ " "		3.59	106.07	
Z " "		3.50	106.16	
⅊ " "		3.47	106.19	
Cb " "		3.45	106.21	
H Gutter " "		3.20	106.46	
Top Cb		2.67	106.99	

Diamond St.

	109.66		
			109.66
	¼		
H on Paving		3.08	106.58
Cb " "		3.57	106.09
¼ " "		3.58	106.08
℄ " "		3.60	106.06
¼ " "		3.71	105.95
Cb " "		3.88	105.78
S " "		4.37	105.29
	℄ Lamont		
S on Paving		4.43	105.23
Cb " "		4.03	105.63
¼ " "		3.83	105.83
℄ " "		3.74	105.92
¼ " "		3.72	105.94
Cb " "		3.75	105.88
H " "		3.12	106.54
	¼		
H on Paving		3.57	106.09
Cb " "		3.94	105.72
¼ " "		3.88	105.78
℄ " "		3.86	105.80
¼ " "		3.98	105.68
Cb " "		4.36	105.30
S " "		4.79	104.87
	E Cb		
S Top Cb		4.65	105.01

12-16-29

47

	109.66		
			109.66
Gutter on Paving		5.27	104.39
Cb " "		4.78	104.88
¼ " "		4.16	105.50
℄ " "		4.01	105.65
¼ " "		4.00	105.66
Cb " "		4.26	105.40
H " "		4.07	105.59
Top Cb		3.56	106.10
	E. L. Lamont		
H		2.3	107.4
¼		3.4	106.3
Cb Top		3.73	105.93
Gutter on Pav		4.52	105.14
¼ " "		4.23	105.43
℄ " "		4.21	105.45
¼ " "		4.32	105.34
Gutter " "		4.93	104.73
Cb Top		4.62	105.04
S		4.1	105.6
	50' E of E L Lamont		
S		3.9	105.8
Cb		4.5	105.2
¼ Edge Pav		4.53	105.13
℄ " "		4.39	105.27
¼ " "		4.45	105.21
Cb		4.3	105.4

	109.66			109.7
+16		38		105.9
N		39		106.8
	100'E			
N		23		107.4
+6		41		105.6
Cb		45		105.2
½ = Edge Pav		476		104.90
½ on "		418		104.98
½ = Edge "		479		104.87
+6		49		104.8
Cb		37		106.0
S		42		105.5
	150'E			
S		44		105.3
Cb		39		105.8
+2		40		105.7
+4		53		104.4
½ = Edge Pav		508		104.58
½ on "		495		104.71
½ = Edge "		500		104.66
Cb		45		105.2
+15		40		105.7
N		14		108.3
	200'E			
N		19		107.8
+2		30		106.7

	109.66			109.7
Cb		4.6		105.1
½ = Edge Pav		5.54		104.12
½ on "		5.56		104.16
½ = Edge "		5.63		104.03
+8		6.6		103.7
Cb		4.9		104.8
S		4.9		104.8
	250'E			
S		6.6		103.1
Cb		6.0		103.7
+6		6.6		103.1
½ = Edge Pav		6.64		103.02
½ on "		6.49		103.17
½ = Edge "		6.55		103.11
+5		6.1		103.6
Cb		4.8		104.9
N		3.7		106.0
	300'E			
N		6.1		103.6
Cb		6.7		103.0
½ = Edge Pav		7.79		101.87
½ on "		7.84		101.82
½ = Edge "		7.95		101.71
+7		8.8		100.9
Cb		5.6		104.1
S		6.9		102.8

212'E on S.L. = Conc Walk 6.06 — 103.60

240'E on S.L. = Solid Conc Dr. 6.55 — 103.11

335'E on S.L. = Conc Stoplog 7.83 — 101.84

Diamond St

		109.66			
	350'			109.7	
S			8.9	100.8	
Cb			8.7	101.0	315' E on H = Conc. Drive
+2			9.9	99.8	8.91 100.75
1/4 = Edge Pav			9.39	100.37	
2 on "			9.18	100.48	
1/4 = Edge "			9.24	100.42	
Cb			9.2	100.5	
H			8.6	101.1	
	400' E				
H			9.5	100.2	
Cb			10.5	99.2	
1/4 = Edge Pav			10.55	99.11	
2 on "			10.50	99.16	
1/4 = Edge "			10.61	99.05	
+8			11.1	98.6	
Cb			10.1	99.6	
S			10.7	99.0	
	450' E				
S			11.5	98.2	
Cb			10.0	99.7	
+2			12.2	97.5	
1/4 = Edge Pav			11.94	97.72	
2 on "			11.84	97.82	
1/4 = Edge "			11.88	97.78	
Cb			11.8	97.9	

		109.66			
H			11.3	98.4	
TP	1.49	99.29	11.86	97.80	
	497' E			99.3	
H			1.8	97.5	
Cb			2.5	96.8	
1/4 = Edge Pav			2.76	96.53	
2 on "			2.67	96.62	
1/4 = Edge "			2.73	96.56	
+7			2.8	96.5	
Cb			0.8	98.5	
S			0.6	98.7	80' W. of 20' Cbs to H
	500' E = H2		Morrell		
S			2.8	96.5	
Cb			2.5	96.8	
+5			3.2	96.1	
1/4 = Edge Pav			2.79	96.50	
2 on "			2.72	96.57	
1/4 = Edge "			2.81	96.48	
Cb			2.5	96.8	
H			1.8	97.5	
	H Cb				
H			2.4	96.9	
Cb			2.8	96.5	
1/4 = Edge Pav			3.11	96.18	
2 on "			3.05	96.24	
1/4 = Edge "			3.15	96.14	

9929

		99.3
Cb	3.7	95.6
S Ground	4.1	95.2
Top Fdcb	3.37	95.92
1/4		
S	4.3	95.0
Cb	3.7	95.6
1/4 = Edge Pav	3.29	96.00
℄ on "	3.18	96.11
1/4 = Edge "	3.24	96.05
Cb	2.8	96.5
N	2.4	96.9
℄ Morrell		
N	2.4	96.9
Cb	3.0	96.3
1/4 = Edge Pav	3.35	95.94
℄ on "	3.33	95.96
1/4 = Edge "	3.44	95.85
Cb	3.7	95.6
S	4.3	95.0
1/4		
S	4.9	94.4
Cb	4.1	95.2
1/4 = Edge Pav	3.58	95.71
℄ on "	3.43	95.86
1/4 = Edge "	3.48	95.81
Cb	3.2	96.1

9929

		99.3
N	2.3	97.0
E Cb		
N	1.8	97.5
Cb	3.1	96.2
1/4 = Edge Pav	3.61	95.68
℄ on "	3.59	95.70
1/4 = Edge "	3.71	95.58
Cb	4.3	95.0
S Ground	5.3	94.0
Top Cb	4.38	94.91
E L Morrell		
S	4.2	95.1
Cb	3.6	95.7
8N	2.36	96.93
+3	4.4	94.9
1/4 = Edge Pav	3.98	95.31
℄ on "	3.83	95.46
1/4 = Edge "	3.88	95.41
Cb	3.2	96.1
+2	1.7	97.6
N	1.0	98.3
38' E of E L Morrell		
N	2.0	97.3
+15	2.8	96.5
Cb	4.9	94.4
1/4 = Edge Pav	4.80	94.49

S E Top Hyd
Diamond Morrell

Diamond St.

		99.29			
				99.3	
℄	on Paving		4.82	94.47	
½	Edge "		4.97	94.32	
+1			5.3	94.0	
Cb			4.8	94.5	
S			4.8	94.5	
		42' E			
S			5.1	94.2	
Cb			4.9	94.4	75' E = N of 5 Palm Tree
+3			5.5	93.8	14' S of N 2
½	Edge Pav		5.12	94.17	
℄	on "		4.92	94.37	
½	Edge "		4.93	94.36	
Cb			5.2	94.1	
N			5.4	93.9	
		100' E			
N			6.3	93.0	
Cb			6.6	92.7	
½	Edge Pav		6.45	92.84	
℄	on "		6.43	92.86	
½	Edge "		6.63	92.66	
+7			7.3	92.0	
Cb			6.7	92.6	
S			7.2	92.1	
		158' E			
S			8.6	90.7	
Cb			7.6	91.7	

Note: 175' E to 400' E Big Drainage Area From North

		99.29			
				99.3	51
+2			8.4	90.9	
½	Edge Pav		7.92	91.37	
℄	on "		7.74	91.55	142' E = E of 5 Palm Tree 14' S of N 6
½	Edge		7.78	91.51	
Cb			7.8	91.5	
N			7.4	91.9	
		200' E			
N			7.6	91.7	219' E on 55 Cone Walk
Cb			8.7	90.6	8.14 91.15
½	Edge Pav		8.99	90.30	
℄	on "		9.00	90.29	
½	Edge "		9.20	90.09	
+7			9.2	90.1	
Cb			8.4	90.9	
S			9.7	89.6	
		250' E			
S			10.3	89.0	
Cb			9.1	90.2	
+4			9.9	89.4	
½	Edge Pav		9.72	89.57	
℄	on "		9.52	89.77	
½	Edge "		9.53	89.76	
Cb			9.6	89.7	
N			8.8	90.5	
		300' E			
N			8.6	90.7	

		99.29		99.3	
Cb			9.5	89.8	
1/4 = Edge Pav			9.91	89.38	330' E = Lat Tree 18' S of N.L.
& on "			9.88	89.41	
1/4 = Edge "			10.05	89.24	
+5			10.4	88.9	
Cb			9.8	89.5	
S			10.5	88.8	
TP	9.09	98.41	9.94	89.55	
				98.4	
		350' E			
S			10.0	88.4	
Cb			9.3	89.1	
+			10.0	88.4	
1/4 = Edge Pav			9.61	88.78	
& on "			9.41	88.98	
1/4 = Edge "			9.48	88.96	
+7			7.6	90.8	
Cb			8.6	89.8	
N			8.6	89.8	
		400' E			
N			8.8	89.6	
Cb			9.1	89.3	
+5			8.5	89.9	
1/4 = Edge Pav			9.91	88.53	
& on "			9.91	88.53	
1/4 = Edge "			10.06	88.38	
+6			10.4	88.0	

		98.44		98.4	
Cb			9.5	88.9	
S			9.6	88.8	
		450' E			
S			9.4	89.0	
Cb			10.2	88.2	
+3			11.1	87.3	
1/4 = Edge Pav			10.45	87.99	
& on "			10.33	88.11	
1/4 = Edge "			10.34	88.10	
Cb			8.1	90.3	
+3			9.0	89.4	
N			7.8	90.6	80' N. dr 20' Cbs 10' 1/4
		500' E = N.L. Hayes			
N			8.0	95.4	
Cb			4.9	93.5	
+5			10.4	88.0	
1/4 = Edge Pav			10.77	87.67	
& on "			10.75	87.69	
1/4 = Edge "			10.89	87.55	
+5			11.1	87.3	
Cb			10.0	88.4	
S			10.7	87.7	SE Tap 1119 Diamond & Hayes
			7.07	91.37	
		N Cb			
S			10.2	88.2	
Cb					

Diamond St

	98.44		98.4
Cb		8.6	89.8
+5		11.5	86.9
1/4 = Edge Pav		11.14	87.30
⅛ on "		10.91	87.53
1/4 = Edge "		10.88	87.56
+5		10.8	88.2
Cb		5.7	92.7
+3		3.5	94.9
N		0.8	97.6
	7' E of N Cb		
N		1.2	97.2
+15		3.6	94.8
Cb		9.1	89.3
1/4 = Edge Pav		10.86	87.58
⅛ on "		10.93	87.51
1/4 = Edge "		11.18	87.26
Cb		11.3	87.1
S		11.8	86.6
	N 1/4		
S		12.0	86.4
Cb		11.4	87.0
1/4 = Edge Pav		11.14	87.30
⅛		10.90	87.54
1/4 = " "		10.79	87.65
Cb		9.0	89.4
N		5.4	93.0

	98.44		98.4
	⅛ of Hydr		
N		5.4	93.0
Cb		9.3	89.1
1/4 = Edge Pav		10.57	87.87
⅛		10.70	87.74
1/4 = " "		10.94	87.50
Cb		11.2	87.2
S		11.6	86.8
	E 1/4		
S		11.6	86.8
Cb		11.1	87.3
1/4 = Edge Paving		10.80	87.64
⅛		10.53	87.91
1/4 = " "		10.43	88.01
Cb		9.1	89.3
N		5.4	93.0
	E Cb		
N		4.5	93.9
Cb		8.9	89.5
1/4 = Edge Pav		10.30	88.14
⅛		10.33	88.11
1/4 = " "		10.52	87.92
Cb		10.7	87.7
+10		6.5	91.9
S		7.6	90.8
	4' E of E Cb		

		98.44		98.4	
S			7.2	91.2	
+N			5.5	92.9	
Cb			9.6	88.8	
1/4 = Edge Pav			10.44	88.00	16' E = Lg Pepper Tree
L			10.25	88.19	10' S of NL
1/4 = " "			10.24	88.20	
+7			9.5	88.9	
Cb			7.2	91.2	43' E = Lg Pepper Tree
+8			1.7	96.7	10' S of NL
N			0.0	98.4	
		E.L. of Hoyes			
N			0.0	98.4	98' E = Lg Pepper Tree
Cb			1.4	97.0	8' S of NL
+4			8.2	90.2	
1/4 = Edge Pav			9.86	88.58	
L			9.80	88.64	
1/4 = " " "			9.89	88.55	
+6			9.4	89.0	
Cb			3.3	95.1	
S			5.2	93.2	
TP	3.91	101.81	0.54	97.96	Nail's Pole 150' E of EL Hoyes 97.95
		50' E of EL Hoyes			
S			9.9	91.9	
Cb			7.5	94.3	
+5			10.7	91.1	
1/4 = Edge			10.05	91.76	

		101.81		101.8	
L on Pav			10.89	90.92	
1/4 = Edge "			10.90	90.91	
Cb			9.4	92.4	
+10			4.4	97.4	
N			3.1	98.7	
		100' E			
N			2.3	99.5	
Cb			3.7	98.1	
+3			8.5	93.3	
1/4 = Edge Pav			8.67	93.14	
L			8.65	93.16	
1/4 = " "			8.77	93.04	
+6			9.1	92.7	
Cb			5.8	96.0	
+3			4.3	97.5	
S			5.6	96.2	
		120' E			
S			5.3	96.5	
Cb			3.6	88.2	
+4			7.9	93.9	
1/4 = Edge Pav			7.88	93.93	
L			7.74	94.07	
1/4 = " "			7.79	94.02	
Cb			6.7	95.1	
+4			1.5	100.3	
N			0.6	101.2	

Diamond St.

	101.81		101.8
160 E			
H		0.3	101.5
Cb		1.9	99.9
+3		5.3	96.5
1/4 = Edge Pav.		6.33	95.48
Z		6.30	95.51
1/4 = " "		6.41	95.40
+6		6.8	95.0
Cb		4.0	97.8
S		5.5	96.3
200 E			
S		5.8	96.0
Cb		3.6	98.2
+4		6.0	95.8
1/4 = Edge Pav		5.75	96.06
Z		5.63	96.18
1/4 = " "		5.70	96.11
+6		5.0	96.8
Cb		2.1	99.7
H		0.0	101.8
240 E			
H		1.7	100.1
Cb		4.0	97.8
+3		5.7	96.1
1/4 = Edge Pav		5.79	96.02
Z		5.76	96.05

	101.81		101.8
1/4 = Edge Pav		5.93	95.88
+6		6.2	95.6
Cb		5.5	96.3
S		7.1	94.7
280 E			
-5		9.5	92.3
S		8.4	93.4
Cb		7.5	94.3
1/4 = Edge Pav		6.85	94.96
Z		6.71	95.10
1/4 " "		6.75	95.06
Cb		6.3	95.5
H		4.4	97.4
300 E			
H		5.0	96.8
Cb		6.8	95.0
1/4 = Edge Pav		7.44	94.37
Z		7.40	94.41
1/4 " "		7.52	94.29
Cb		8.5	93.3
S		10.4	91.4
+5		10.7	91.1
350 E			
-5		11.5	90.3
S		11.3	90.5
Cb		9.6	92.2

328 E = Very large Eucalyptus tree

		101.81		101.8	
¼ = Edge Par			9.17	92.64	
℄			9.08	92.73	376 E = Large Apple Tree 115 of ML
¼ = " "			9.10	92.71	
Cb			8.4	93.4	
N			6.8	95.0	384 E = Lg. Apple Tree 115 of ML
	400 E				
N			5.6	96.2	
Cb			7.3	94.5	
+3			10.4	91.4	
¼ = Edge Par			10.67	91.14	
℄			10.66	91.15	
¼ = " "			10.81	91.00	
+7			11.3	90.5	
Cb			10.6	91.2	
S			12.6	89.2	
+5			13.0	88.8	
	450 E				
-5			13.5	88.3	
S			13.0	88.8	
Cb			10.6	91.2	
+3			12.6	89.2	
¼ = Edge Par			12.49	89.32	
℄			12.32	89.49	
¼ = " "			12.30	89.51	
+7			11.2	90.6	
Cb			6.1	95.7	

		101.81		101.8	
N			4.2	97.6	80' Wide 20' Cb 5' ¼
	500 E = N.L. of Orch				
N			5.1	96.7	
Cb			6.7	95.1	
+5			12.1	89.7	
TP	2.53	91.38	12.96	88.85	
¼ = Edge Par			3.59	91.4 87.79	
℄			3.57	87.81	
¼ = " "			3.68	87.70	
Cb			3.0	88.4	
S			3.3	88.1	
	N Cb				
S			6.2	85.2	
Cb			4.5	86.9	
¼ = Edge Par			4.25	87.13	
℄			4.11	87.27	
¼ = " "			4.10	87.28	
+6			2.8	88.6	
Cb			+0.6	92.0	
N			+5.6	93.0	
	N ¼				
N			0.0	91.4	
Cb			1.2	90.2	
¼ = Edge Par			4.25	87.13	
℄			4.30	87.08	
¼ = " "			4.44	86.94	

Diamond St

	91.38		91.4
Cb		5.0	86.4
S		6.6	84.8
	℄ Olney		
S		6.5	84.9
Cb		5.0	86.4
1/4 = Edge Pav		4.71	86.67
℄		4.54	86.84
1/4 = " "		4.46	86.92
Cb		2.4	89.0
H		0.5	90.9
	E 1/4		
H		1.0	90.4
Cb		2.9	88.5
1/4 = Edge Pav		4.15	86.73
℄		4.73	86.65
1/4 " " "		4.95	86.43
Cb		5.1	86.3
S		6.8	84.6
	E Cb		
-5		8.8	82.6
S		7.6	83.8
+5		5.4	86.0
Cb		4.2	87.2
1/4 = Edge Pav		5.06	86.32
℄		4.88	86.50
1/4 = " "		4.83	86.55

	91.38		91.4	57
Cb		3.1	88.3	
H		1.8	89.6	
	E. L. of Olney			
H		3.5	87.9	
Cb		3.9	87.5	
1/4 = Edge Pav		4.69	86.69	
℄		4.72	86.66	
1/4 = " "		4.88	86.50	
Cb		4.5	86.9	
+1.5		5.6	85.8	
S		8.6	82.8	
+10		10.0	81.4	
BM		3.10	88.28	56.7 up Hyd Diamond & Olney
	50' E of EL Olney			
-10		10.6	80.8	
S		9.6	81.8	87' E - Concrete 25' of N Line
+10		5.2	86.2	3.11 88.22
Cb		5.2	86.2	
1/4 = Edge Pav		5.18	86.20	
℄		5.04	86.34	
1/4 = " "		5.06	86.32	
Cb		5.0	86.4	
H		4.1	87.3	
	100' E			
H		3.4	88.0	
Cb		5.0	86.4	

91.38

			91.4
1/4 = Edge Pav		5.45	85.93
⊥		5.41	85.97
1/4 = " "		5.54	85.84
+6		5.6	85.8
Cb		4.8	86.6
+8		4.4	87.0
S		9.3	87.1
+10		9.4	82.0
150' E			
-5		7.9	83.5
S		7.7	83.7
Cb		6.5	84.9
1/4 = Edge Pav		5.94	85.44
⊥	" "	5.82	85.56
1/4 =	" "	5.86	85.52
Cb		5.3	86.1
N		3.4	88.0
200' E			
N		4.0	87.4
Cb		5.3	86.1
1/4 = Edge Pav		6.21	85.12
⊥		6.21	85.17
1/4 =	" "	6.33	85.05
+7		6.7	84.7
Cb		5.5	85.9
S		6.9	84.5

180' E = East of 5 Pepper Trees 175 of +6

91.38

		91.4
250' E		
S	7.3	84.1
Cb	5.8	85.6
+4	6.9	84.5
1/4 = Edge Pav	6.76	84.62
⊥	6.65	84.73
1/4 = " "	6.66	84.72
Cb	5.2	86.2
N	4.1	87.3
300' E		
N	4.4	87.0
Cb	5.5	85.9
1/4 = Edge Pav	7.07	84.31
⊥	7.03	84.35
1/4 = " "	7.16	84.22
+6	7.4	84.0
Cb	6.5	84.9
S	8.0	83.4
350' E		
S	8.2	83.2
Cb	7.2	84.2
+4	8.2	83.2
1/4 = Edge Pav	7.60	83.8
⊥	7.45	83.93
1/4 = " "	7.48	83.90
Cb	6.5	84.9

Diamond St.		91.38			
				91.4	
N			48	86.6	
	400'E				
N			5.3	86.1	
Cb			6.7	84.7	
¼ = Edge Pav			7.86	83.52	
℄			7.84	83.54	
¼ = " "			7.98	83.40	
+6			8.2	83.2	
cb			7.5	83.9	
S			8.7	82.7	
TP	2.33	85.78	7.93	83.45	
	450'E			85.8	
S			3.0	82.8	
cb			2.4	83.4	
+1			3.5	82.3	
¼ = Edge Pav			2.75	83.03	
℄			2.62	83.16	
¼ " "			2.64	83.14	
cb			1.4	84.4	
N			0.0	85.8	
	500'E = N.L. Pendleton				80' N to 26' Cb 26' N
N			1.6	84.2	
cb Top			2.64	83.14	
Gutter on Paving			3.24	82.54	
¼ on "			3.04	82.74	
℄ " "			3.04	82.74	

		85.78			Note - 1 Cob Return 20' Wide in N. Walk At Diamond & Pendleton
¼ on Pav Cng			3.20	82.58	59
Gutter " "			3.36	82.42	
Cb Top			2.66	83.12	
S			3.6	82.2	
BM			2.67	83.11	SW BP Diamond & Pendleton
TP	0.30	73.36	12.72	73.06	
TP	0.89	61.70	12.55	60.81	
TP	2.05	50.92	12.83	48.87	
BM			5.74	45.18	NW BP Garnett & Grey 45.10

12-26-49
Sisson
McHugh
Northbir
Remmen

Proposed Lease
Animal Rescue League
La Jolla Canyon Drive

Mon 660.47 659.06 N 89° 38' 10" W 1320.62

660.47
659.06
1319.53

La Jolla Canyon Drive

949.98 to POT

C.T. 19 Paving 500 291.41 242' R.W. Hwy

100° 13'

90° 00'

1911.64

C.T. 10 Paving 50 R = 1350

Δ 12° 24'

L = 292.17

Proposed Lease
Animal Rease
League Lease

N 0° 21' 62" E 2627.49

302.99 297.17

735.0

C.T. 50 10 Paving

Paving

256.101

27° 12' 60"

90° 00'

335.734

500 C.T. 10 Paving 1320.65

Mon

Cont. FB 2007 / 79

P.L. 1299

N 0° 21' 26" E 2628.26

660.47 N 89° 35' 38" W South Line P.L. 1299 Mon.

P.L. 1296

Leavitt's Add

Sapphire St. Cross Section
Dawes to Everts

Platted 5-28-30 C.D.H.

				70' Wide 15' Cbs 10' Qts	
BM	0.06	134.91		134.85	S.F.B.P. Turquoise & Gar.
TP	7.66	132.59	9.98	124.93	N.W. 7' Hub
BM			3.69	128.90	Sapphire & Dawes
		W-L Dawes			
N			3.4	129.2	Dawes 80' Wide 25' Cbs 10' Qts
cb			3.7	128.9	
¼			3.8	128.8	
¼			4.4	128.2	
¼			4.7	127.9	
cb			5.2	127.4	
S			5.5	126.1	
		W cb			
S			6.2	126.4	
cb			5.4	127.2	
¼			5.1	127.5	
¼			5.0	127.6	
¼			4.5	128.1	
cb			3.9	128.7	
N			3.1	129.5	
		W ¼			
N			3.3	129.3	
cb			3.9	128.7	
¼			4.3	128.3	
¼			4.6	128.0	
¼			5.0	127.6	

		132.59			5-9-30 S.F.B.P. Sapphire North
cb			5.4	127.2	
S			5.9	126.7	
		¼ Dawes			
S			5.9	126.7	
cb			5.3	127.3	
¼			4.9	127.7	
¼			4.5	128.1	
¼			4.2	128.4	
cb			3.9	128.7	
N			3.5	129.1	
		E ¼			
N			4.0	128.6	
cb			4.1	128.5	
¼			4.4	128.2	
¼			5.0	127.6	
¼			5.5	127.1	
cb			6.1	126.5	
S			6.4	126.2	
		E cb			
S			5.9	126.7	
cb			4.7	127.9	
¼			4.8	127.8	
¼			4.6	128.0	
¼			4.3	128.3	
cb			3.8	128.8	
N			3.2	129.4	

Sapphire St.

132.59

	EL Dawn			
N			3.0	129.6
Cb			3.5	129.1
1/4			3.8	128.8
1/2			3.9	128.7
3/4			4.1	128.5
Cb			4.0	128.6
S			4.7	127.9
	50' E of EL Dawn			
S.			3.9	128.7
Cb			3.4	129.2
1/4			3.3	129.3
1/2			3.0	129.6
3/4			2.9	129.7
Cb			2.7	129.9
N			2.5	130.1
	100' E			
N			1.8	130.8
Cb			2.2	130.4
1/4			2.3	130.3
1/2			2.7	129.9
3/4			2.5	130.1
Cb			2.7	129.9
S			2.4	129.2
	150' E			
S			2.5	130.1

132.59

Cb			1.9	130.9
1/4			1.4	131.2
1/2			1.7	130.9
3/4			1.2	131.4
Cb			1.0	131.6
N			0.8	131.8
TP	1133	143.39	0.53	132.06
	200' E			
N			11.1	132.3
Cb			11.1	132.3
1/4			11.2	132.2
1/2			11.2	132.2
3/4			11.4	132.0
Cb			11.6	131.8
S			12.0	131.4
	250' E			
S			11.0	132.4
Cb			11.4	132.0
1/4			10.9	132.4
1/2			10.7	132.6
3/4			10.5	132.9
Cb			10.2	133.2
N			9.8	133.6
	350' E			
N			9.0	134.4
Cb			9.2	134.2

Sapphire St.

143.39

¼	9.3	134.1	
⊿	9.4	134.0	
¼	9.3	134.1	
Cb	10.0	133.4	
S	9.5	133.9	
350'E			
S	8.3	135.1	
Cb	8.0	135.4	
¼	7.7	135.7	
⊿	7.8	135.6	
¼	7.7	135.7	
Cb	7.7	135.7	
N	7.8	135.6	
400'E			
N	6.0	137.4	
Cb	6.0	137.4	
¼	6.1	137.3	
⊿	6.4	137.0	
¼	6.4	137.0	
Cb	6.6	136.8	
S	6.4	137.0	
450'E			
S	4.6	138.8	
Cb	4.7	138.7	
¼	4.4	139.0	
⊿	4.5	138.9	

143.39

63

¼	4.1	139.3	
Cb	4.0	139.4	
N	4.3	139.1	
500'E = N.L. Everts			
N	2.2	141.2	
Cb	2.9	140.5	
¼	2.4	141.0	
⊿	2.4	141.0	
¼	2.6	140.8	
Cb	2.9	140.5	
S	2.9	140.5	
BM	3.4	140.25	SM 7' Hub Sapphire St Everts

Tourmaline St Cross Section
Down to Fanuel

Plotted 5-26-30 - C.B.H.

					70' Wide 15 Cbs 10 Qts
BM	1.49	130.39		128.90	HW 7" Hub Sapphire & Down
TP	12.15	131.56	10.98	119.41	SW 7" Hub Tourmaline & Down
	W ℄ Down				
S			12.1	119.5	Down 80' Wide
Cb			11.9	119.7	20 Cbs 10 Qts
¼			11.6	120.0	
⅛			11.3	120.4	
¼			11.1	120.5	
Cb			11.1	120.5	
N			11.0	120.6	
	N Cb				
N			10.8	120.8	
Cb			11.0	120.6	
¼			11.1	120.5	
⅛			11.1	120.5	
¼			11.2	120.4	
Cb			11.9	119.9	
S			12.1	119.5	
	N ¼				
S			11.9	119.7	
Cb			11.5	120.1	
¼			11.3	120.3	
⅛			11.0	120.6	
¼			10.8	120.8	
Cb			10.5	121.1	

	131.56		
N		10.2	121.4
	℄ Down		
N		9.9	121.7
Cb		10.3	121.3
¼		10.5	121.1
⅛		10.7	120.9
¼		11.1	120.5
Cb		11.3	120.3
S		11.6	120.0
	E ¼		
S		12.0	119.6
Cb		11.7	119.9
¼		11.3	120.3
⅛		11.1	120.5
¼		10.8	120.8
Cb		10.6	121.0
N		10.1	121.5
	E Cb		
N		10.0	121.6
Cb		10.5	121.1
¼		10.6	121.0
⅛		10.8	120.8
¼		11.0	120.6
Cb		11.2	120.4
S		11.6	120.0
	E ℄ of Down		

Tourmaline 131.56

S	11.2	120.4	
cb	10.7	120.9	
¼	10.4	121.2	
½	10.4	121.2	
¼	10.1	121.5	
cb	9.8	121.8	
N	9.3	121.3	
50' E of E L Dower			
N	8.2	123.4	
cb	8.5	123.1	
¼	8.6	123.0	
½	8.8	122.8	
¼	9.0	122.6	
cb	9.2	122.4	
S	9.4	122.2	
100' E			
S	7.2	124.4	
cb	7.0	124.6	
¼	7.2	124.4	
½	7.8	124.8	
¼	7.2	124.4	
cb	7.3	124.4	
N	6.8	124.8	
150' E			
S	5.0	126.6	
N	6.0	125.6	

131.56

N	6.4	125.2	
+9	5.4	126.2	
cb	5.2	126.4	
¼	5.1	126.5	
½	5.4	126.2	
¼	5.8	125.8	
cb	6.0	125.6	
+3	5.1	126.5	
S	5.5	126.1	
200' E			
S	3.7	127.8	
cb	3.4	128.2	
¼	3.8	127.8	
½	3.8	127.8	
¼	3.9	127.7	
+2	4.9	126.7	
+4	4.1	127.5	
cb	3.3	128.3	
N	2.5	128.1	
250' E			
N	1.1	130.5	
cb	1.3	130.3	
¼	1.3	130.3	
½	1.3	130.3	
+5	2.2	129.4	
¼	3.3	128.3	

Tourmaline

		131.56		
t3			2.0	129.6
cb			1.7	129.9
S			1.4	130.2
	275°F			
S			0.9	130.7
t7			0.8	130.8
cb			2.7	128.9
t2			0.9	130.7
H			0.2	131.3
t			0.4	131.2
t2			0.5	131.1
H			0.5	131.1
cb			0.1	131.5
H				
TP	12.97	143.61	0.92	130.64
	300°F			
H			10.9	132.7
cb			11.6	132.0
H			11.5	132.1
t			11.7	131.9
t2			11.3	132.3
cb			11.4	132.2
S			12.1	131.5
	325°F			
S			10.5	133.1
cb			10.4	133.2
H			10.4	133.2

		143.61		
t			10.3	133.3
H			10.2	133.4
cb			10.0	133.6
H			10.0	133.6
	350°F			
H			8.9	134.7
cb			9.1	134.5
H			9.2	134.4
t			9.2	134.4
H			9.4	134.2
cb			9.5	134.1
S			9.5	134.1
	400°F			
S			7.7	135.9
cb			7.4	136.2
H			7.4	136.2
t			7.3	136.3
t2			7.2	136.4
cb			7.2	136.4
H			7.1	136.5
	450°F			
H			5.3	138.3
cb			5.5	138.1
H			5.5	138.1
t			5.7	137.9
t2			5.6	138.0

Tourmaline 143.61

Cb			5.6	138.0
S			5.9	137.7
	499.90 E: WL Events			
S			4.3	139.3
Cb			4.1	139.5
¼			4.0	139.6
½			3.6	140.0
¼			3.6	140.0
Cb			3.6	140.0
N			3.5	140.1
TP	139.6	153.08	4.19	139.12 SW 9.46 Tourmaline + Events
	EL Events			
N			10.0	143.1
Cb			10.2	142.9
¼			10.3	142.8
½			10.5	142.6
¼			10.6	142.5
Cb			10.8	142.3
S			10.9	142.2
	50' E of EL Events			
S			9.7	143.4
Cb			9.3	143.8
¼			8.9	144.2
½			8.6	144.5
¼			8.5	144.6
Cb			8.4	144.7

153.08

N			8.3	144.8
	100' E			
N			6.5	146.6
Cb			6.8	146.3
¼			7.0	146.1
½			7.2	145.9
¼			7.3	145.8
Cb			7.6	145.5
S			7.8	145.3
	150' E			
S			6.1	147.0
Cb			5.8	147.3
¼			5.7	147.4
½			5.5	147.6
¼			5.2	147.9
Cb			5.1	148.0
N			4.9	148.2
	200' E			
N			3.5	149.6
Cb			3.5	149.6
¼			3.3	149.8
½			3.4	149.7
¼			4.0	149.1
Cb			4.0	149.1
S			4.2	148.9
	250' E			

Tourmaline

153.08

S			2.2	150.4
Cb			2.5	150.6
¼			2.2	150.9
¾			2.1	151.0
¼			2.0	151.1
Cb			2.0	151.1
N			1.8	151.3
TP	10.80	162.59	1.29	151.79
	300' E			
N			10.0	152.6
Cb			9.9	152.7
¼			9.8	152.8
¾			9.8	152.8
¼			10.1	152.5
Cb			10.4	152.2
S			10.8	151.8
	350' E			
S			9.8	153.4
Cb			9.0	153.6
¼			8.8	153.8
¾			8.6	154.0
¼			8.6	154.0
Cb			8.5	154.1
N			8.4	154.2
	380' E			
N			7.3	155.3

162.59

68

Cb			7.1	155.5
¼			7.2	155.4
¾			7.5	155.1
¼			7.7	154.9
Cb			7.9	154.7
S			8.3	154.3
	400' E			
S			7.4	155.2
Cb			6.9	155.7
¼			6.4	156.2
¾			6.0	156.6
¼			5.9	156.7
Cb			5.8	156.8
N			5.9	156.7
	425' E			
N			4.8	157.8
Cb			4.8	157.8
¼			4.5	158.1
¾			4.6	158.0
¼			4.7	157.9
Cb			4.9	157.7
S			5.0	157.6
	450' E			
S			4.5	158.1
Cb			4.0	158.6
¼			3.8	158.8

Tourmaline 162.59

℄	3.6	159.0	
¼	3.9	158.7	
Cb	4.3	158.3	
H	4.7	157.9	
48.5' E			
H	2.8	159.8	
Cb	3.0	159.6	
¼	3.1	159.5	
℄	3.2	159.4	
¼	3.4	159.2	
Cb	3.5	159.1	
S	4.0	158.6	
50.0' E = H.L. Fanuel			
S	4.3	158.3	
Cb : End Return	4.10	158.49	
Gutter on Edge Paving	4.69	157.90	
¼ " " "	4.26	158.33	
℄ " "	3.92	158.67	
¼ " " "	3.86	158.73	
Gutter " " "	3.85	158.74	
Cb : End Return	3.13	159.46	
H	3.0	159.6	
H Cb. of Fanuel			
-105.0 Top Cb	1.98	160.61	
Gutter on Paving	2.43	160.16	
-55' Top Cb	2.53	160.06	

162.59

-55 Gutter on Paving	3.05	159.54	
-5 : Cb E.C. 20' Rad.	3.08	159.51	
Gutter " "	3.67	158.92	
H. on Paving	3.72	158.87	
Cb " "	3.92	158.67	
¼ " "	4.09	158.50	
℄ " "	4.22	158.37	
¼ " "	4.45	158.14	
Cb " "	4.68	157.91	
S " "	5.02	157.57	
+5 : Cb E.C. 20' Rad	4.61	157.98	
Gutter on Paving	5.17	157.42	
+55 Cb	6.20		
Gutter on Paving	6.79		
+105 Cb	7.73		
Gutter on Paving	8.33		
Center S.W. Return			
Cb	3.99	158.60	
Gutter on Paving	4.64	157.95	
Center N.W. Return			
Cb	3.13	159.46	
Gutter on Paving	3.80	158.79	
BM	1.31	161.28	S.E. Tor Hyd tourmaline & Fanuel

Experts St Cross Section
Loring to Turquoise

80' Wide
20' Cbs
10' Qts

BM.	1.47	140.59		139.12	SW 7th Tourmaline & Emerald
TP	1.90	130.73	11.76	128.83	
	N. Cb of Loring				
			10.11	120.62	
-10 = Top Cb CbEC on Paving			10.76	119.97	
W	"	"	10.47	120.26	
Cb	"	"	9.95	120.78	
¼	"	"	9.70	121.03	
½	"	"	9.40	121.33	
¾	"	"	9.20	121.53	
Cb	"	"	9.00	121.73	
E	"	"	8.45	122.28	
+10 = CbEC 30' Rad			8.22	122.51	
Top Cb			7.48	123.25	
	24' N of N Cb = N.L of Loring or L.O.T. of Imp.				
E			7.2	123.5	
+19.3 = End of Existing Cb			7.43	123.30	
Gutter on Paving			8.14	122.49	
¼	"	"	8.28	122.45	
½	"	"	8.46	122.27	
¾			8.84	121.89	
Cb			9.33	121.40	
+ 0.6 = End of Existing Cb			8.74	121.99	
W			9.4	121.3	
	1' N of N.L Loring				
W			7.6	123.1	

Plotted 5-27-30
F.D.H.

Mar 1930
Simon
Scott
Norling
Osborn

	130.73			
Cb		7.5	123.2	
¼		8.8	121.9	
½		8.8	121.9	
¾		8.4	122.3	
¼		8.2	122.5	
Cb		8.0	122.7	
+2		7.0	123.7	
E		5.9	124.8	
	20' N of N.L Loring			
E		4.9	125.8	
Cb		6.0	124.7	
¼		6.6	124.1	
½		6.9	123.8	
¾		7.0	123.7	
Cb		7.1	123.6	
W		6.9	123.8	
	50' N			
W		5.9	124.8	
Cb		5.5	125.2	
¼		5.2	125.5	
½		5.0	125.7	
¾		4.6	126.1	
Cb		4.4	126.3	
E		3.8	126.9	
	100' N			
E		2.1	128.6	

Everts 130.73

cb			2.1	128.1
¼			2.9	127.8
½			3.2	127.5
¼			3.6	127.1
cb			3.8	126.9
W			4.2	126.5
	150 N			
W			2.6	128.1
cb			2.3	128.4
¼			2.1	128.6
½			1.7	129.0
¾			1.5	129.2
cb			1.2	129.5
E			0.7	130.0
TP	12.92	143.16	0.49	130.24
	200 N			
E			11.5	131.7
cb			12.0	131.2
¼			12.3	130.9
½			12.5	130.7
¾			12.8	130.4
cb			12.9	130.3
W			13.1	130.1
	250 N			
W			11.5	131.7
cb			11.2	132.0

143.16

¼			10.9	132.3
½			10.5	132.7
¾			10.6	132.7
cb			10.5	132.7
E			9.9	133.3
	289.61 N: 52.4	Hyacinth		Hyacinth 70°17'
E			8.6	134.6 15 cbs
cb			9.2	134.0 10.9 ¼
¼			9.4	133.8
½			9.5	133.7
¾			9.7	133.5
cb			9.8	133.4
W			10.2	133.0
	5 cb			
W			9.9	133.3
cb			9.4	133.8
¼			9.2	134.0
½			9.2	134.0
¾			8.9	134.3
cb			8.8	134.4
E			8.2	135.0
	5 ¼			
E			7.9	135.2
cb			8.5	134.7
¼			8.8	134.4
½			8.8	134.4

Everts

143.16

¼	9.1	134.1
cb	9.4	133.8
N	9.6	133.6
S Hyacinth		
N	8.9	134.3
cb	8.5	134.7
¼	8.2	135.0
S	7.9	135.3
¼	7.9	135.3
cb	7.7	135.5
E	6.4	136.8
N ¼		
E	7.4	135.8
cb	7.7	135.5
¼	7.9	135.3
S	8.1	135.1
¼	8.6	134.6
cb	8.7	134.5
W	9.0	134.2
N cb		
W	9.1	134.1
cb	8.6	134.6
¼	8.5	134.7
S	8.1	135.1
¼	8.0	135.2
cb	7.6	135.6

143.16

72

E	7.2	136.0
N.L. Hyacinth		
E	6.6	136.6
cb	6.8	136.4
¼	7.1	136.1
S	7.4	135.8
¼	7.6	135.6
cb	7.7	135.5
W	8.3	134.9
50' N of N.L. Hyacinth		
W	7.0	136.2
cb	6.4	136.8
¼	6.4	136.8
S	5.8	137.4
¼	5.2	138.0
cb	5.4	137.8
E	5.5	137.7
68 N		
E	6.5	136.7
43	5.8	137.4
cb	5.9	137.3
¼	6.0	137.2
S	5.7	137.5
¼	5.6	137.6
cb	5.9	137.3
W	6.6	136.6

Everts 1431L

75' N			
W	1.2	137	0
cb	1.2	137	0
¼	1.2	137	0
℄	1.3	136	9
¼	1.0	137	2
+8	1.1	137	1
cb	1.9	136	3
+5	1.0	137	2
E	4.7	138	5
110' N			
E	4.0	139	2
cb	4.3	138	9
¼	4.7	138	5
℄	4.8	138	4
¼	5.5	137	7
cb	6.6	136	6
+5	7.9	135	3
+10	6.9	136	2
W	6.5	136	7
120' N			
W	7.9	135	3
+9	6.8	136	4
cb	5.6	137	6
¼	4.9	138	3
℄	4.7	138	5

1431L

¼	4.5	138	7
cb	4.2	139	0
E	3.8	139	4
132.5' N = ℄ Alley			
E	3.1	140	1
cb	3.8	139	4
¼	4.1	139	1
℄	4.5	138	7
¼	4.7	138	5
cb	4.9	138	3
W	5.9	137	3
150' N			
W	5.4	137	8
cb	4.9	138	3
¼	4.4	138	8
℄	4.0	139	2
¼	3.8	139	4
cb	3.7	139	5
E	3.4	139	8
200' N			
E	2.4	140	8
cb	2.9	140	3
¼	3.4	139	8
℄	3.8	139	4
¼	4.2	139	0
cb	4.5	138	7

Eberts 143.16

N		4.8	138.4
	240' N		
N		4.4	138.8
Cb		3.5	139.7
¼		3.2	140.0
⅛		2.8	140.4
¼		2.5	140.7
Cb		2.1	141.1
F		1.6	141.6
	264.92' N-SL	Tourmaline	Tourmaline 70' N.E. 15' Cbs
F		1.1	142.1
Cb		1.9	141.3
¼		2.1	141.1
⅛		2.3	140.9
¼		2.7	140.5
Cb		3.0	140.2
N		3.8	139.4
	5 Cb		
N		3.7	139.5
Cb		3.0	140.2
¼		2.6	140.6
⅛		2.3	140.9
¼		1.9	141.3
Cb		1.4	141.8
F		0.8	142.4
	5 ¼		

143.16

F		0.7	142.5
Cb		1.5	141.7
¼		1.8	141.4
⅛		2.2	141.0
¼		2.6	140.6
Cb		3.0	140.2
N		3.5	139.7
	⅛ Tourmaline		
N		3.3	139.9
Cb		2.8	140.4
¼		2.4	140.8
⅛		2.0	141.2
¼		1.7	141.5
Cb		1.3	141.9
F		0.5	142.7
	N ¼		
F		0.3	142.9
Cb		1.3	141.9
¼		1.6	141.6
⅛		2.1	141.1
¼		2.4	140.8
Cb		2.6	140.6
N		3.2	140.0
	N Cb		
N		3.4	139.8
Cb		2.6	140.6

Fierts		143.16			
¼			2.2	141.0	
⅛			1.8	141.4	
¼			1.4	141.8	
cb			0.9	142.3	
F			0.1	143.1	SN 7 Hus Tourmaline Fierts 139.16
TP	BM 8.75	147.87	4.04	139.12	
	NL Tourmaline				
F			4.8	143.0	
cb			5.6	142.2	
¼			6.0	141.8	
⅛			6.3	141.5	
¼			6.7	141.1	
cb			7.0	140.8	
N			7.8	140.0	
		50' N of NL Tourmaline			
N			7.1	140.7	
cb			6.2	141.6	
¼			5.8	142.0	
⅛			5.6	142.2	
¼			5.3	142.5	
cb			5.0	142.8	
F			4.2	143.6	
		100' N			
F			3.7	144.1	
cb			4.6	143.2	
¼			4.9	143.0	

	147.87			
⅛			5.3	142.6
¼			5.8	142.1
cb			6.1	141.8
N			6.8	141.0
	132.5' N of NL			
N			6.8	141.0
cb			6.0	141.8
¼			5.5	142.3
⅛			4.8	143.0
¼			4.5	143.3
cb			4.5	143.3
F			3.7	144.1
	165' N			
F			3.7	144.1
cb			4.6	143.2
¼			5.0	142.9
⅛			5.2	142.6
¼			5.6	142.2
cb			6.1	141.8
N			7.0	140.9
	200' N			
N			7.3	140.6
cb			6.5	141.3
¼			6.1	141.8
⅛			5.6	142.3
¼			5.2	142.7

Events

147.87

cb	4.7	143.2
F	3.6	144.3
230' N		
F	4.1	143.8
cb	5.8	142.6
¼	5.7	142.1
⅛	5.9	142.0
¼	6.3	141.5
cb	6.6	141.2
W	7.5	140.3
265' N: 5 L. Sapphire		Sapphire 70 N.E. 15 Cb 15 Qtz
W	7.3	140.5
cb	6.3	141.5
¼	6.2	141.7
⅛	5.8	142.0
¼	5.5	142.3
cb	5.4	142.4
F	4.2	143.7
S cb		
F	4.6	143.2
cb	5.8	142.6
¼	5.6	142.2
⅛	6.0	141.9
¼	6.1	141.7
cb	6.4	141.5
W	7.3	140.6

147.87

S ¼		
W	7.0	140.9
cb	6.4	141.5
¼	6.1	141.8
⅛	5.9	142.0
¼	5.4	142.5
cb	5.1	142.8
F	4.5	143.3
⅛ Sapphire		
F	4.5	143.3
cb	4.9	143.0
¼	5.8	142.7
⅛	5.7	142.2
¼	5.8	142.1
cb	6.1	141.8
W	6.9	141.0
N ¼		
W	6.8	141.1
cb	6.3	141.6
¼	6.0	141.9
⅛	5.7	142.2
¼	5.1	142.8
cb	4.8	143.1
F	4.4	143.5
N cb		
F	4.0	143.9

Everts

		147.87			
Cb			4.7	143	2
¼			4.9	143	0
½			5.3	142	6
¼			6.0	141	9
Cb			6.4	141	5
N			7.4	140.	5
		N.L. Sapphire			
N			6.6	141.	3
Cb			6.0	141	9
¼			5.7	142	2
½			5.6	142	3
¼			5.0	142	9
Cb			4.4	143.	5
E			3.8	144	1
		40 N of N.L. Sapphire			
E			3.5	144.	4
Cb			4.2	143.	7
¼			4.5	143.	4
½			4.8	143.	1
¼			4.7	143.	2
TP	11.59	154.72	4.74	143.13	
Cb			11.9	142	8
N			12.3	142.	4
		160 N			
N			11.4	143	3
Cb			10.9	143.	8

		154.72			
¼			10.4	143	3
½			10.1	144.	6
¼			9.9	144	8
Cb			9.5	145.	2
E			9.0	145	7
		132.5 N = ½ Alley			
E			7.3	147.	4
Cb			7.9	146	8
¼			8.2	146	5
½			8.5	146	2
¼			8.8	145	9
Cb			8.9	145	8
N			9.2	145	5
		165 N			
N			9.1	145.	6
Cb			8.4	146	3
¼			8.1	146.	6
½			7.8	146	9
¼			7.3	147.	4
Cb			7.1	147	6
E			6.5	148	2
		200 N			
E			5.3	149	4
Cb			6.0	148	7
¼			6.4	148	3
½			6.7	148.	0

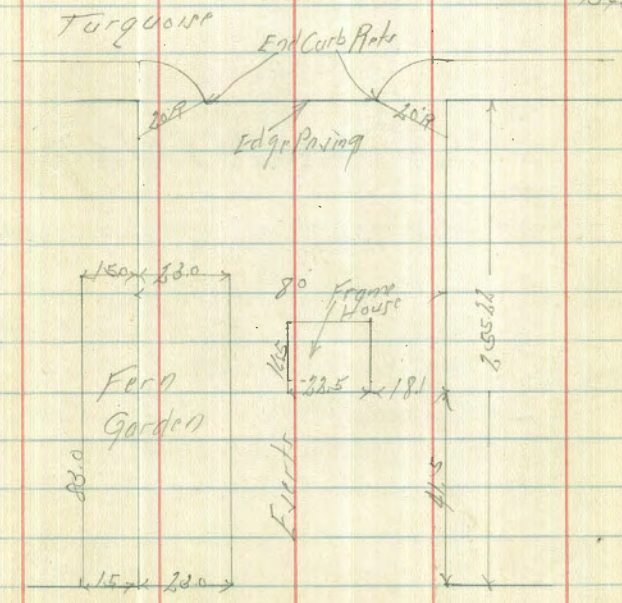
Ferns

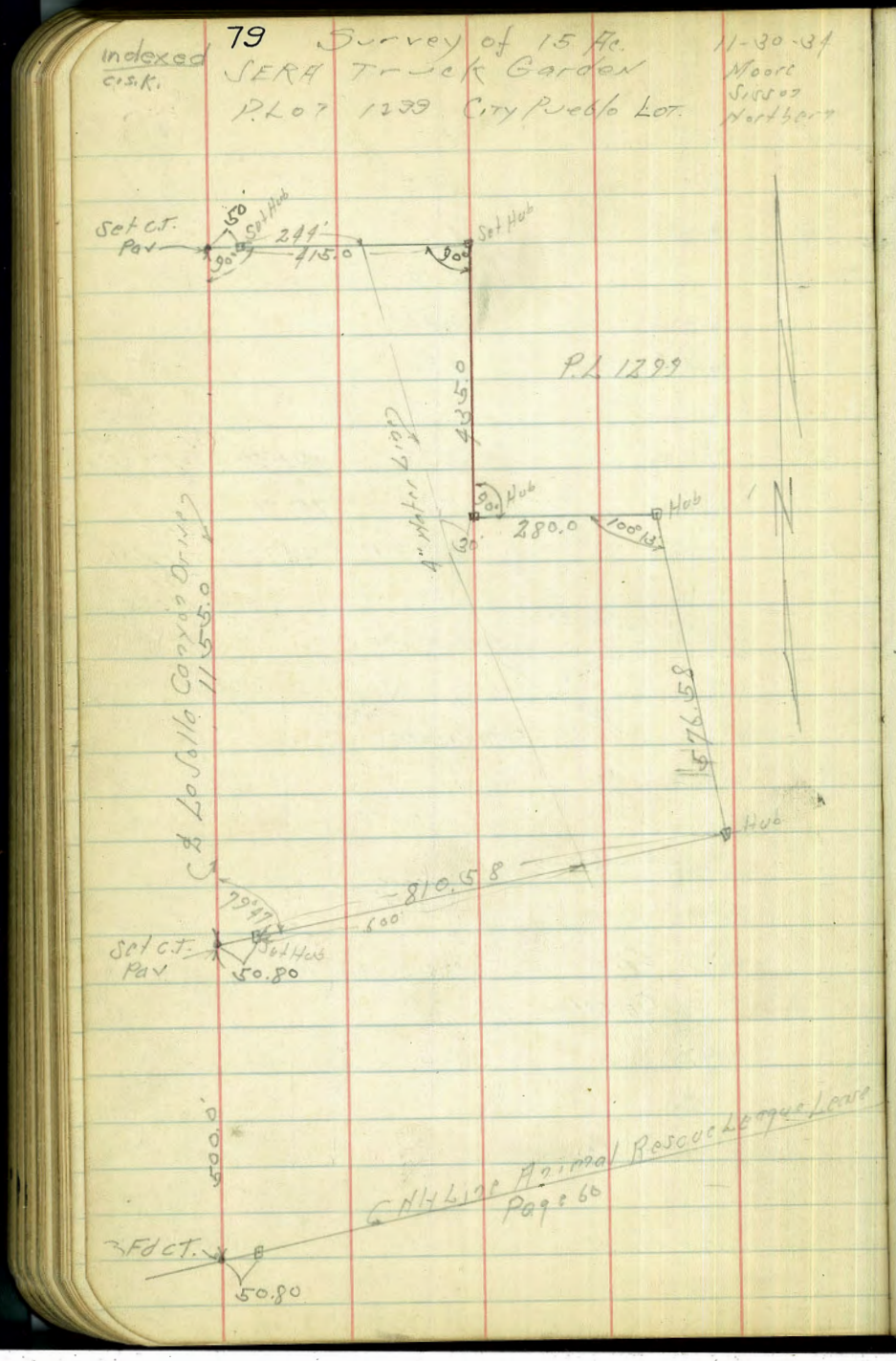
15472

W	6.9	147.8	
Cb	7.3	147.4	
W	7.9	146.8	
280 N			
W	6.5	148.2	
Cb	5.9	148.8	
W	5.7	149.0	
Z	5.4	149.3	
W	4.9	149.8	
Cb	4.7	150.0	
E	4.0	150.7	
25522 N : S.L. Turquoise			
E	2.8	151.9	
+17.6 = End of Existing Cb Return	3.38	151.34	
Gutter on Paving	4.01	150.71	
Cb " "	4.05	150.67	
W " "	4.08	150.64	
Z " "	4.30	150.42	
W " "	4.64	150.08	
Cb " "	5.11	149.61	
+2.8 = End of Cb Return on Paving	5.34	149.48	
Top Cb	4.63	150.09	
W	5.3	149.4	
W on Cb	5.21		
Gutter	5.81		

15472

Cb on Paving	5.18			
W " "	4.85			
Z " "	4.47			
W " "	4.19			
Cb " "	3.94			
E " "	3.34			
Top Cb	2.69			
BM	0.23	154.49		SE Top Nut Turquoise Ferns
TP 286	14472	12.86	141.86	
BM	9.87	134.85		SE BP Turquoise Cast 134.85





77
48
1255
2555
4110

IMPROVED TABLES AND INFORMATION

Table II—Continued

TRIGONOMETRIC FORMULAE (continued)

In any triangle:

Given a, b, C; to find c, B, A.
Use Law of Tangents.

Given A. B. c; to find a, b, C.
Use Law of Sines.

Given a, b, c; to find A, B, C.

$$\text{Let } \frac{a+b+c}{2} = s, \quad \sqrt{\frac{(s-a)\,(s-b)\,(s-c)}{s}} = r$$

$$\cos \tfrac{1}{2} A = \sqrt{\frac{s(s-a)}{bc}}$$

$$\tan \tfrac{1}{2} A = \frac{r}{s-a}$$

$$\tan \tfrac{1}{2} B = \frac{r}{s-b}$$

$$\tan \tfrac{1}{2} C = \frac{r}{s-c}$$

Area of a triangle:

Area $= \tfrac{1}{2}$ ab Sin C

$$\text{Area} = \sqrt{s\,(s-a)\,(s-b)\,(s-c)}$$

PRISMOIDAL FORMULA.

$$\text{Vol.} = \frac{h}{6}\,(B+b+4M)$$

h = altitude; b, B = bases; M = midsection

Table III

INCHES AND FRACTIONS OF AN INCH IN DECIMALS OF A FOOT

	0	1	2	3	4	5	6	7	8	9	10	11	
1/16	.0052	.0885	.1719	.2552	.3385	.4219	.5052	.5885	.6719	.7552	.8385	.9219	1/16
1/8	.0104	.0938	.1771	.2604	.3438	.4271	.5104	.5938	.6771	.7604	.8438	.9271	1/8
3/16	.0156	.0990	.1823	.2656	.3490	.4323	.5156	.5990	.6823	.7656	.8490	.9323	3/16
1/4	.0208	.1042	.1875	.2708	.3542	.4375	.5208	.6042	.6875	.7708	.8542	.9375	1/4
5/16	.0260	.1094	.1927	.2760	.3594	.4427	.5260	.6094	.6927	.7760	.8594	.9427	5/16
3/8	.0313	.1146	.1979	.2813	.3646	.4479	.5313	.6146	.6979	.7813	.8646	.9479	3/8
7/16	.0365	.1198	.2031	.2865	.3698	.4531	.5365	.6198	.7031	.7865	.8698	.9531	7/16
1/2	.0417	.1250	.2083	.2917	.3750	.4583	.5417	.6250	.7083	.7917	.8750	.9583	1/2
9/16	.0469	.1302	.2135	.2969	.3803	.4635	.5469	.6302	.7135	.7969	.8802	.9635	9/16
5/8	.0521	.1354	.2188	.3021	.3854	.4688	.5521	.6354	.7188	.8021	.8854	9688	5/8
11/16	.0573	.1406	.2240	.3073	.3906	.4740	.5573	.6406	.7240	.8073	.8906	.9740	11/16
3/4	.0625	.1458	.2292	.3125	.3958	.4792	.5625	.6458	.7292	.8125	.8958	.9792	3/4
13/16	.0677	.1510	.2344	.3177	.4010	.4844	.5677	.6510	.7344	.8177	.9010	.9844	13/16
7/8	.0729	.1563	.2396	.3229	4063	.4896	.5729	.6563	.7396	.8229	.9063	.9896	7/8
15/16	.0781	.1615	.2448	.3281	.4115	.4948	.5781	.6615	.7448	.8281	.9115	.9948	15/16
1	.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167	1.000	1
	0	1	2	3	4	5	6	7	8	9	10	11	

Table IV

USEFUL RELATIONS.

Lineal feet	×.00019	= miles
Lineal yards	×.0006	= miles
Square inches	×.007	= square feet
Square feet	×.111	= square yards
Square yards	×.0002067	= acres
Acres	×4840	= square yards
Cubic inches	×.00058	= cubic feet
Cubic feet	×.03704	= cubic yards
Links	×.22	= yards
Links	×.66	= feet
Feet	×1.5	= links

57
65
639

360° = 21600′ = 1296000″

Radius = arc of 57.2957790°

Arc of 1° (radius = 1) = .017453292

Arc of 1′ (radius = 1) = .000290888

Arc of 1″ (radius = 1) = .000004848

$\pi = 3.141592654$ $\qquad \sqrt{\frac{1}{4}} = 0.564190$

$\frac{\pi}{4} = 0.785398163$ $\qquad \sqrt[3]{\frac{6}{\pi}} = 1.240700982$

$\frac{\pi}{6} = 0.523598776$ $\qquad \pi^2 = 9.869604401$

$\sqrt{\frac{4}{\pi}} = 1.128379167$ $\qquad \frac{1}{\pi^2} = 0.101321184$

$\frac{\pi}{6} = 0.523598776$ $\qquad \sqrt{\pi} = 1.772453851$

$\frac{4.\pi}{3} = 4.188790205$ $\qquad \frac{1}{\pi} = 0.3183099$

Curvature of Earth's surface = about 0.7 feet in 1 mile

Curvature in feet = 0.667 (Dist. in miles)²

Difference between arc and chord length, 0.05 feet in 11½ miles

$$\text{Probable error of a single observation} = 0.6754\sqrt{\frac{\Sigma v^2}{n-1}}$$

Error in chaining of 0.01 feet in 100 feet:

Due to—

1. Length of tape error of 0.01 feet
2. Alignment. One end 1.4 feet out of line
3. Sag of tape at centre of 0.61 feet.
4. Temperature difference of 15°
5. Difference of pull of 15 lbs.

STADIA REDUCTION FORMULÆ.

Horizontal Distance $= R - R \sin^2 a + C \cos a$

Vertical Distance $= R\ \tfrac{1}{2} \sin 2a + C \sin a$

$$R = \text{Reading} \times \frac{\text{distance from Object glass to cross hairs}}{\text{distance between cross hairs}}$$

C = distance from Object glass to cross hairs + distance from Object glass to center of instrument.

a = angle of elevation for mid Reading

Table IX. TANGENTS AND EXTERNALS TO A 1° CURVE

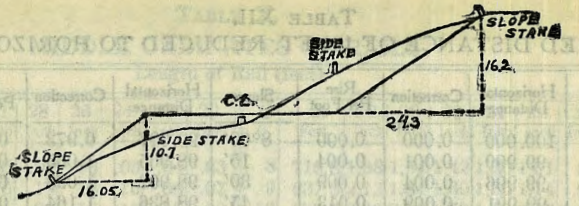
I	T	E	I=10°	I	T	E	I=20°	I	T	E	I=30°
1°	50.00	.218	+	11°	551.70	26.500	+	21°	1061.9	97.577	+
10′	58.34	.297	5° C.	10′	560.11	27.313	5° C	10′	1070.6	99.155	5° C
20′	66.67	.388	T	20′	568.53	28.137	T	20′	1079.2	100.75	T
30′	75.01	.491	.03	30′	576.95	28.974	.06	30′	1087.8	102.35	.10
40′	83.34	.606	E	40′	585.36	29.824	E	40′	1096.4	103.97	E
50′	91.68	.733		50′	593.79	30.686		50′	1105.1	105.60	
2°	100.01	.873	.001	12°	602.21	31.561	.006	22°	1113.7	107.24	.013
10′	108.35	1.024		10′	610.64	32.447		10′	1122.4	108.90	
20′	116.68	1.188		20′	619.07	33.347		20′	1131.0	110.57	
30′	125.02	1.364		30′	627.50	34.259		30′	1139.7	112.25	
40′	133.36	1.552		40′	635.93	35.183		40′	1148.4	113.95	
50′	141.70	1.752		50′	644.37	36.120		50′	1157.0	115.66	
3°	150.04	1.964	10° C.	13°	652.81	37.070	10° C.	23°	1165.7	117.38	10° C.
10′	158.38	2.188	T	10′	661.25	38.031	T	10′	1174.4	119.12	T
20′	166.72	2.425	.06	20′	669.70	39.006	.13	20′	1183.1	120.87	.19
30′	175.06	2.674	E	30′	678.15	39.993	E	30′	1191.8	122.63	E
40′	183.40	2.934	.003	40′	686.60	40.992	.011	40′	1200.5	124.41	.025
50′	191.74	3.207		50′	695.06	42.004		50′	1209.2	126.20	
4°	200.08	3.492		14°	703.51	43.029		24°	1217.9	128.00	
10′	208.43	3.790		10′	711.97	44.066		10′	1226.6	129.82	
20′	216.77	4.099		20′	720.44	45.116		20′	1235.3	131.65	
30′	225.12	4.421		30′	728.90	46.178		30′	1244.0	133.50	
40′	233.47	4.755		40′	737.37	47.253		40′	1252.8	135.35	
50′	241.81	5.100	15° C.	50′	745.85	48.341	15° C.	50′	1261.5	137.23	15° C.
5°	250.16	5.459	T	15°	754.32	49.441	T	25°	1270.2	139.11	T
10′	258.51	5.829	.09	10′	762.80	50.554	.19	10′	1279.0	141.01	.29
20′	266.86	6.211	E	20′	771.29	51.679	E	20′	1287.7	142.93	E
30′	275.21	6.606	.004	30′	779.77	52.818	.017	30′	1296.5	144.85	.038
40′	283.57	7.013		40′	788.26	53.969		40′	1305.3	146.79	
50′	291.92	7.432		50′	796.75	55.132		50′	1314.0	148.75	
6°	300.28	7.863		16°	805.25	56.309		26°	1322.8	150.71	
10′	308.64	8.307		10′	813.75	57.498		10′	1331.6	152.69	
20′	316.99	8.762		20′	822.25	58.699		20′	1340.4	154.69	
30′	325.35	9.230		30′	830.76	59.914		30′	1349.2	156.70	
40′	333.71	9.710	20° C.	40′	839.27	61.141	20° C.	40′	1358.0	158.72	20° C.
50′	342.08	10.202	T	50′	847.78	62.381	T	50′	1366.8	160.76	T
7°	350.44	10.707	.13	17°	856.30	63.634	.26	27°	1375.6	162.81	.39
10′	358.81	11.224	E	10′	864.82	64.900	E	10′	1384.4	164.86	E
20′	367.17	11.753	.006	20′	873.35	66.178	.022	20′	1393.2	166.95	.051
30′	375.54	12.294		30′	881.88	67.470		30′	1402.0	169.04	
40′	383.91	12.847		40′	890.41	68.774		40′	1410.9	171.15	
50′	392.28	13.413		50′	898.95	70.091		50′	1419.7	173.27	
8°	400.66	13.991		18°	907.49	71.421		28°	1428.6	175.41	
10′	409.03	14.582		10′	916.03	72.764		10′	1437.4	177.55	
20′	417.41	15.184	25° C.	20′	924.58	74.119	25° C.	20′	1446.3	179.72	25° C.
30′	425.79	15.799	T	30′	933.13	75.488	T	30′	1455.1	181.89	T
40′	434.17	16.426	.16	40′	941.69	76.869	.32	40′	1464.0	184.08	.49
50′	442.55	17.065	E	50′	950.25	78.264	E	50′	1472.9	186.29	E
9°	450.93	17.717	.007	19°	958.81	79.671	.028	29°	1481.8	188.51	.065
10′	459.32	18.381		10′	967.38	81.092		10′	1490.7	190.74	
20′	467.71	19.058		20′	975.96	82.525		20′	1499.6	192.99	
30′	476.10	19.746		30′	984.53	83.972		30′	1508.5	195.25	
40′	484.49	20.447		40′	993.12	85.431		40′	1517.4	197.53	
50′	492.88	21.161		50′	1001.7	86.904		50′	1526.3	199.82	
10°	501.28	21.887	30° C.	20°	1010.3	88.389	30° C.	30°	1535.3	202.12	30° C.
10′	509.68	22.624	T	10′	1018.9	89.888	T	10′	1544.2	204.44	T
20′	518.08	23.375	.19	20′	1027.5	91.399	.39	20′	1553.1	206.77	.59
30′	526.48	24.138	E	30′	1036.1	92.924	E	30′	1562.1	209.12	E
40′	534.89	24.913	.008	40′	1044.7	94.462	.034	40′	1571.0	211.48	.078
50′	543.29	25.700		50′	1053.3	96.013		50′	1580.0	213.86	

T = R tan ½ I E = R exsec ½ I

Table IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=40°	I	T	E	I=50°	I	T	E	I=60°
31°	1589.0	216.3	+	41°	2142.2	387.4	+	51°	2732.9	618.4	+
10′	1598.0	218.7	5° C.	10′	2151.7	390.7	5° C.	10′	2743.1	622.8	5° C.
20′	1606.9	221.1	T	20′	2161.2	394.1	T	20′	2753.4	627.2	T
30′	1615.9	223.5	.13	30′	2170.8	397.4	.17	30′	2763.7	631.7	.21
40′	1624.9	226.0	E	40′	2180.3	400.8	E	40′	2773.9	636.2	E
50′	1633.9	228.4		50′	2189.9	404.2		50′	2784.2	340.7	
32°	1643.0	230.9	.023	42°	2199.4	407.6	.037	52°	2794.0	645.2	.056
10′	1652.0	233.4		10′	2209.0	411.1		10′	2804.9	649.7	
20	1661.0	235.9		20′	2218.6	414.5		20′	2815.2	654.3	
30′	1670.0	238.4		30′	2228.1	418.0		30′	2825.6	658.8	
40′	1679.1	241.0		40′	2237.7	421.4		40′	2835.9	663.4	
50′	1688.1	243.5		50′	2247.3	425.0		50′	2846.3	668.0	
33°	1697.2	246.1	10° C.	43°	2257.0	428.5	10° C.	53°	2856.7	672.7	10° C.
10′	1706.3	248.7	T	10′	2266.6	432.0	T	10′	2867.1	677.3	T
20′	1715.3	251.3	.26	20′	2276.2	435.6	.34	20′	2877.5	682.0	.42
30′	1724.4	253.9	E	30′	2285.9	439.2	E	30′	2888.0	686.7	E
40′	1733.5	256.5	.046	40′	2295.6	442.8	.075	40′	2898.4	691.4	.112
50′	1742.6	259.1		50	2305.2	446.4		50′	2908.9	696.1	
34°	1751.7	261.8		44°	2314.9	450.0		54°	2919.4	700.9	
10′	1760.8	264.5		10′	2324.6	453.6		10′	2929.9	705.7	
20′	1770.0	267.2		20′	2334.3	457.3		20′	2940.4	710.5	
30′	1779.1	269.9		30′	2344.1	461.0		30′	2951.0	715.3	
40′	1788.2	272.6		40′	2353.8	464.6		40′	2961.5	720.1	
50′	1797.4	275.3	15° C.	50′	2363.5	468.4	15° C.	50′	2972.1	725.0	15° C.
35°	1806.6	278.1	T	45°	2373.3	472.1	T	55°	2982.7	729.9	T
10′	1815.7	280.8	.40	10′	2383.1	475.8	.51	10′	2993.3	734.8	.63
20′	1824.9	283.6	E	20′	2392.8	479.6	E	20′	3003.9	739.7	E
30′	1834.1	286.4	.070	30′	2402.6	483.4	.116	30′	3014.5	744.6	.168
40′	1843.3	289.2		40′	2412.4	487.2		40′	3025.2	749.6	
50′	1852.5	292.0		50′	2422.3	491.0		50′	3035.8	754.6	
36°	1861.7	294.9		46°	2432.1	494.8		56°	3046.5	759.6	
10′	1870.9	297.7		10′	2441.9	498.7		10′	3057.2	764.6	
20′	1880.1	300.6		20′	2451.8	502.5		20′	3067.9	769.7	
30′	1889.4	303.5		30′	2461.7	506.4		30′	3078.7	774.7	
40′	1898.6	306.4	20° C.	40′	2471.5	510.3	20° C.	40′	3089.4	779.8	20° C.
50′	1907.9	309.3	T	50′	2481.4	514.3	T	50′	3100.2	784.9	T
37°	1917.1	312.2	.53	47°	2491.3	518.2	.68	57°	3110.9	790.1	.84
10′	1926.4	315.2	E	10′	2501.2	522.2	E	10′	3121.7	795.2	E
20′	1935.7	318.1	.093	20′	2511.2	526.1	.151	20′	3132.6	800.4	.225
30′	1945.0	321.1		30′	2521.1	530.1		30′	3143.4	805.6	
40′	1954.3	324.1		40′	2531.1	534.2		40′	3154.2	810.9	
50′	1963.6	327.1		50′	2541.0	538.2		50′	3165.1	816.1	
38°	1972.9	330.2		48°	2551.0	542.2		58°	3176.0	821.4	
10′	1982.2	333.2		10′	2561.0	546.3		10′	3186.9	826.7	
20′	1991.5	336.3	25° C.	20′	2571.0	550.4	25° C.	20′	3197.8	832.0	25° C.
30′	2000.9	339.3	T	30′	2581.0	554.5	T	30′	3208.8	837.3	T
40′	2010.2	342.4	.67	40′	2591.0	558.6	.85	40′	3219.7	842.7	1.05
50′	2019.6	345.5	E	50′	2601.1	562.8	E	50′	3230.7	848.1	E
39°	2029.0	348.6	.117	49°	2611.2	566.9	.189	59°	3241.7	853.5	.283
10′	2038.4	351.8		10′	2621.2	571.1		10′	3252.7	858.9	
20′	2047.8	354.9		20′	2631.3	575.3		20′	3263.7	864.3	
30′	2057.2	358.1		30′	2641.4	579.5		30′	3274.8	869.8	
40′	2066.6	361.3		40′	2651.5	583.8		40′	3285.8	875.3	
50′	2076.0	364.5		50′	2661.6	588.0		50′	3296.9	880.8	
40°	2085.4	367.7	30° C.	50°	2671.8	592.3	30° C.	60°	3308.0	886.4	30° C.
10′	2094.9	371.0	T	10′	2681.9	596.6	T	10′	3319.1	892.0	T
20′	2104.3	374.2	.80	20′	2692.1	600.9	1.02	20′	3330.3	897.5	1.27
30′	2113.8	377.5	E	30′	2702.3	605.3	E	30′	3341.4	903.2	E
40′	2123.3	380.8	.141	40′	2712.5	609.6	.227	40′	3352.6	908.8	
50′	2132.7	384.1		50′	2722.7	614.0		50′	3363.8	914.5	.340

T = R tan ½ I E = R exsec ½ I



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.

4314.20
0

1.11061
20
41.1220

3+56
37
3+93
11
3+82

21.10
6
126.60

1.11061
37
777427
333183
41.09257

BM. SW Bath Pole 53.86 29.13
Trias Ave La Jolla
Stob NW S.L.B. = 93.90

15.00
6 | 90.5
6
30
30
5

167
95.37
11.75

Trias 2 | 23.5

Sec A = 11.75 = L 55.30
Sec B 11.75 = L 51.90

+75
96
105
200.5

0+90.50
165
2 | 88.85
29.61
59.22
29.61
88.83

1+00 = 1+15

1069
609
1678

76.16
275
7341

87.16
7341
13.75

Sec. 1 = 101.86
Sec 2 = 77.50
Sec 3 = 58.10

2+11.90

Bird Rock Ave. SW B.P. 79.06
Forward S.W BP 74.95
Midway S.E BP 71.80
Sea Lone N.E BP 70.51

32.6
5
37.6
92.2
-96

7556
7180
8.76

3 | 60.90

101.86