

1323

PASTS

FIELD BOOK

No. 385F

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CITY OF SAN DIEGO,
CALIFORNIA.

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1331-1314
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101
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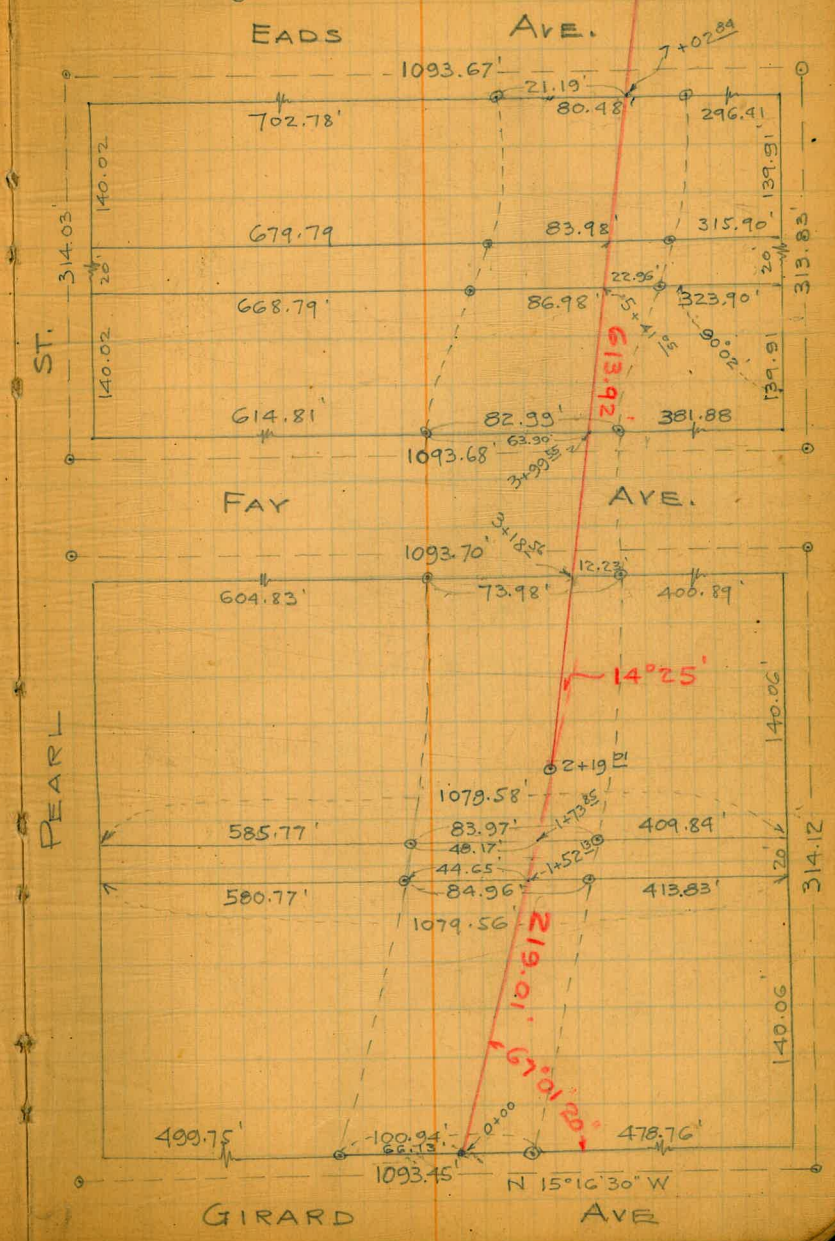
X Sec TENNYSON	Centraloma to Warrington	10
" " Wabaska Dr.	Chatsworth to Tennyson	18
Cb levels S side ELCAJON AVE	Seminole to El Cajon ^{Pl.}	24
X sec. Central.	Redwood to Lexington	27
" " 42 nd	Thorn " "	34
" " Palermo	Villa Dr to Alcott	41
Proposed Ravina Storm Drain	{ Draper Ave. La Jolla Blvd.	54

B.M.	SW. Girard & Kline	B.P.	103.97
"	SE. Fay & Kline	B.P.	95.99
"	NE. Fay & Ravina	B.P.	87.04
"	SE. Cor. inside Property	L. B.P. Conc. Mon.	88.95
"	NE. Cuvier & Kline	B.P.	76.486

RAVINA STORM DRAIN -

Jaeger
Bailey
Clavert
Brooks } Jan. 25th 1928

8°47'40"
8+32.93



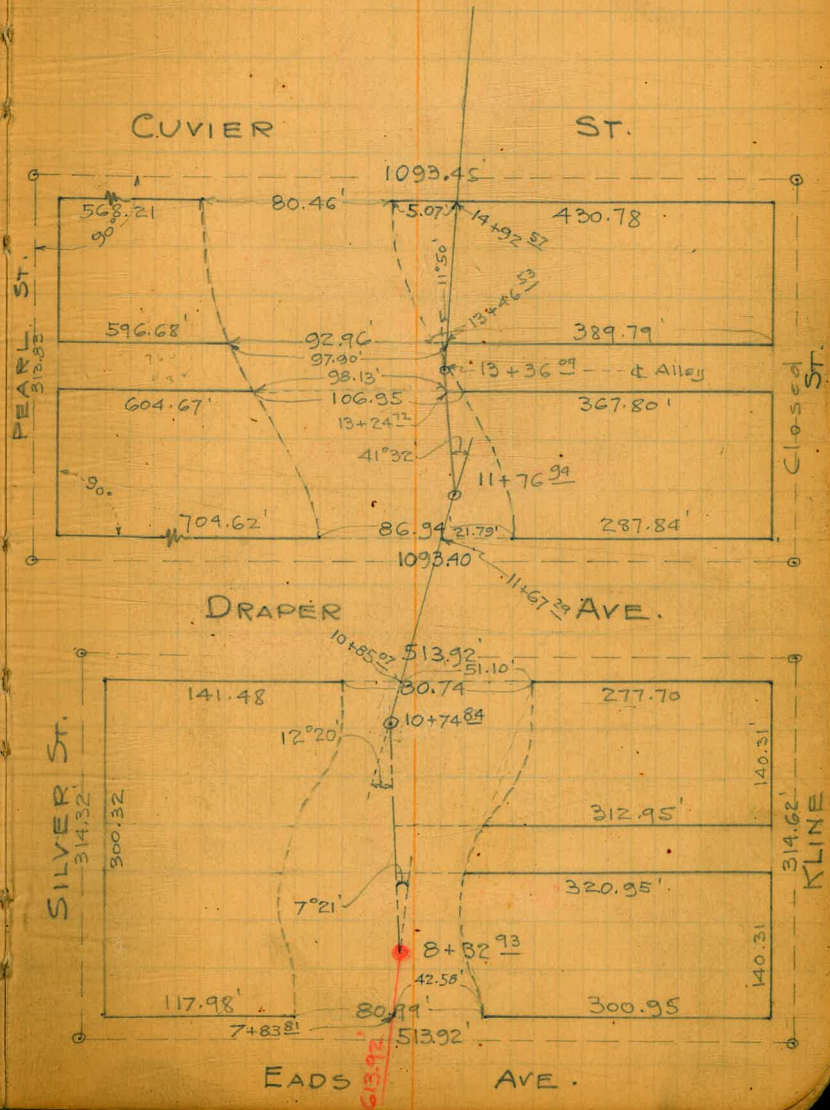
PEARL ST.

EADS AVE.

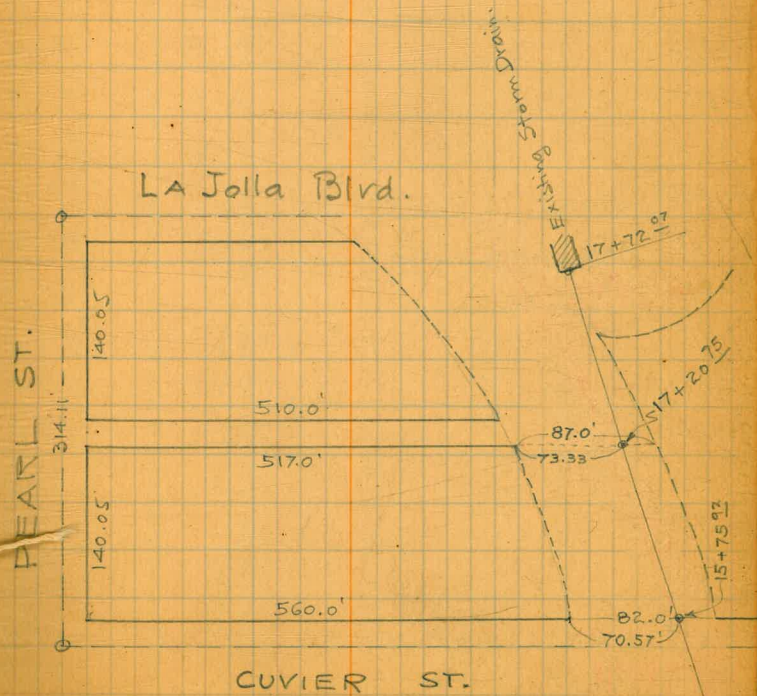
FAY AVE.

GIRARD AVE

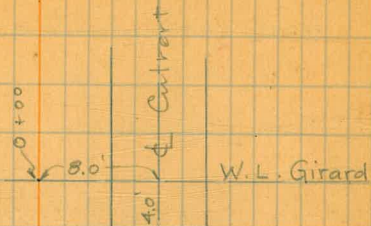
N 15°16'30" W



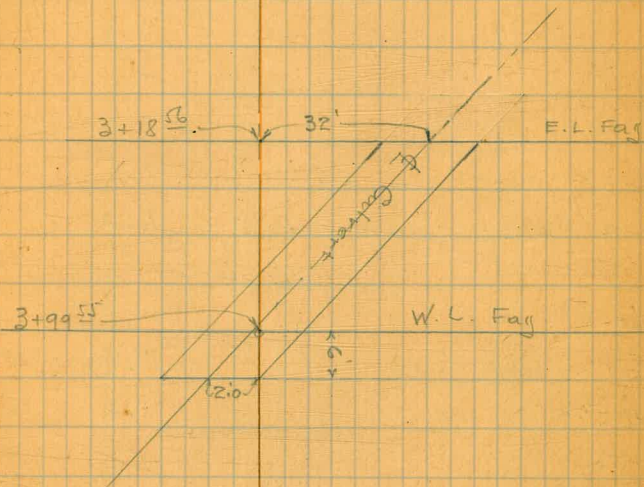
17+72.07

$$\begin{array}{r} 17+25 \\ - 4.25 \\ \hline 17+20.75 \end{array}$$


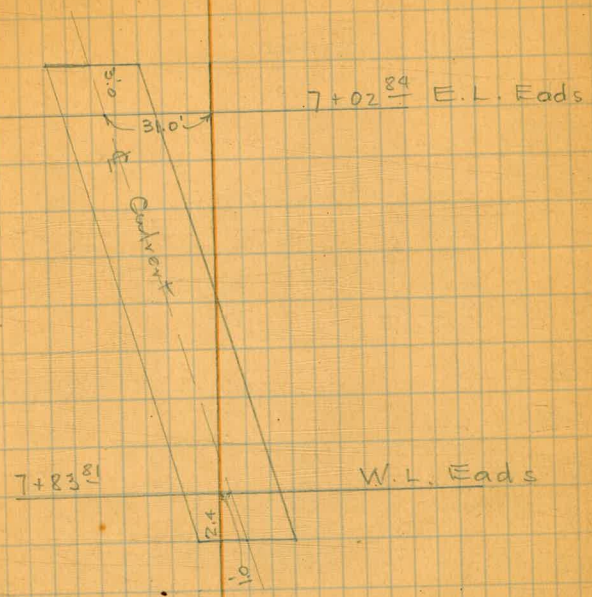
STA	+	H.I.	-	Elev.
	P.M.	SW. Cor. Girard & Kline		103.97
		3.52	107.49	
			12.25	95.24
		2.13	97.37	
0+00			4.2	93.17
		Top of Culvert	5.45	91.92
0+25			4.6	92.8
0+50			5.6	91.8
0+75			6.4	91.0
1+00			6.8	90.6
1+25			6.0	91.4
1+50			5.6	91.8
1+52 ¹³		East Line of alley	6.3	91.1
1+73 ⁸⁵		West Line alley	6.35	91.02
1+88			5.7	91.7
1+93			7.2	90.2
2+00			7.9	89.5
2+19 ²⁴		A L	8.06	89.31
2+50			8.6	88.8
2+75			9.1	88.3
3+00			9.5	87.9
3+18 ⁵⁴		East Line of Fay	9.7	87.7
		East curb top	10.66	86.71
		East curb Bottom	11.31	86.16



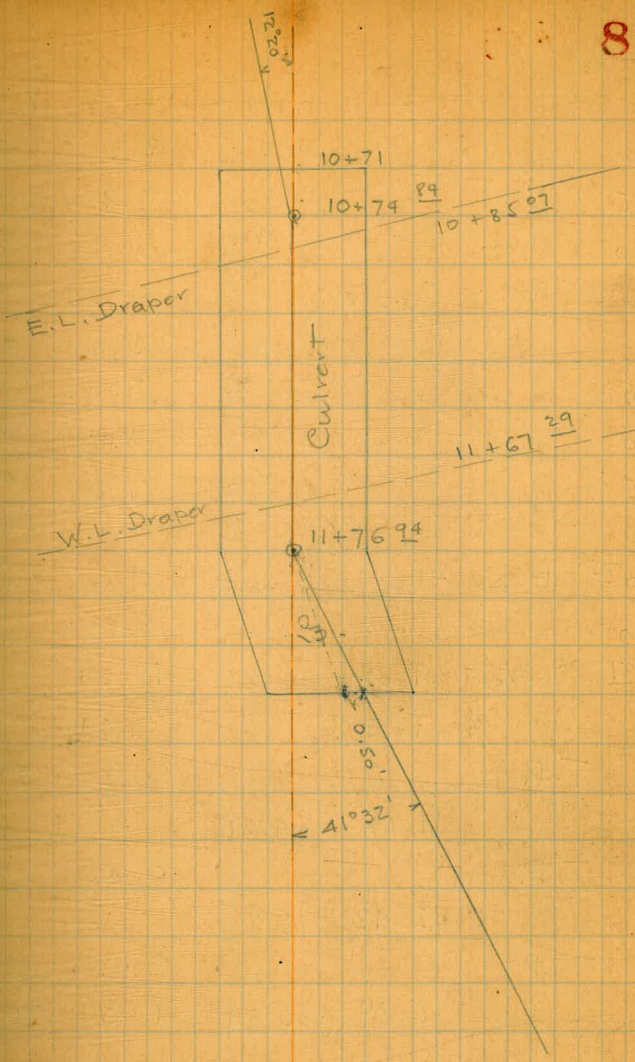
STA	+	H.I.	-	Elev.
	¢	Fay	10.96	86.41
		West curb Bottom	12.04	85.33
		Top	11.45	85.92
3+99 ⁵⁵		West Line Fay	12.53	84.84
T.P.			12.51	84.86
	6.48	91.34		
		East Culvert top	4.92	86.42
		East Culvert Bottom	7.88	83.46
		West Culvert top	8.47	82.87
		West Full of mud and water		
4+25			8.00	83.34
4+50			8.20	83.14
4+75			8.90	82.44
5+00			8.30	83.04
5+25			8.1	83.24
T.P.			9.24	82.10
	2.49	84.59		
5+41 ⁵⁵		East Line alley	2.4	82.2
5+60			2.4	82.2
5+75			2.7	81.9
6+00			2.8	81.8
6+25			3.3	81.3
6+50			3.5	81.1
6+75			4.7	79.9
7+02 ³⁴		East Line of Eads	5.7	78.9



STA		H.I.	-	Elev.
	E. Culvert top	7.48		77.11
	E. Culvert Bottom	10.69		73.90
	East Curb Line	7.3		77.3
	☉ Eads	7.8		76.8
	West Curb Line	9.1		75.5
	+1 Ft.	7.9		76.7
7+83 ⁸¹	West Line Eads	8.4		76.2
7+84	West Culvert top	9.24		75.35
	Bottom	12.61		71.98
8+00		11.50		73.09
8+01		7.7		76.9
8+32 ⁸³		8.8		75.8
8+50		11.6		73.0
8+75		13.1		71.5
T.P		13.10		71.49
	4.57	76.06		
9+00		4.6		71.5
9+25		4.8		71.3
9+50		4.8		71.3
9+75		5.4		70.7
10+00		5.2		70.9
10+25		4.9		71.2
10+50		7.5		68.6
+71	E. Side Culvert Top	6.81		69.25
+71	" " Bottom	13.71		62.35



STA.	+	H.L.	-	Elev.
10+78 ⁸⁰			3.9	72.2
+85 ⁹⁷	E.L. Draper		4.2	71.9
11+67 ²⁹	W.L. "		5.2	70.9
+76 ⁹⁴			7.3	68.8
+86 ⁴⁴	Top of Culvert		9.83	66.23
	T.P.		13.05	63.01
		1.38	64.39	
+86 ⁴⁴	Bottom of Culvert		4.73	59.66
12+00			3.9	60.5
+75			4.3	60.1
+50			4.7	59.7
+75			5.4	59.0
13+00			6.5	57.9
+24 ¹²	E.L. Alleg		6.3	58.1
+46 ¹³	W.L. "		7.7	56.7
+56			9.4	55.0
+75			5.4	59.0
14+00			9.7	54.7
+75			9.0	55.4
+50			9.8	54.6
+74			14.0	52.4
	T.P.		14.89	51.50
		1.95	53.45	
+75			3.3	50.2
+75 ⁹⁴	E.L. CUVIER		3.2	50.3



STA	+	H.I.	-	Elev.
15+00			3.3	50.2
+25			4.8	48.7
+50			2.4	51.1
15+75 ⁹⁴	W.L. Currier		4.0	49.5
16+00			5.0	48.5
+30			7.4	46.1
+50			8.2	45.3
+75			7.5	46.0
17+00			7.7	45.8
+20 ⁷⁵	E.L. Alleg		9.6	43.9
+50			9.3	44.2
+72 ⁷¹	Culvert Bolt.		12.24	41.21
	" Top		7.51	45.94
T.P.			0.32	53.13
	11.08	64.21		
T.P.			0.66	63.55
	12.43	75.98		
T.P.			2.03	73.95
	6.84	80.79	4.27	76.52

76.486 N.E. B.P. Currier & Kline

60' wid.
10' elev
10' 1/2"

Tennyson St X Sec
Centraloma To Warrington

5-27-29
mills

98.58

89.58

Tennyson St.

10

B.M. 1.93 98.58 96.65
P.C. N.W. Cor.
00 = N. end Parvnt. Intersection Tennyson & Centraloma
s.w. chatoworth & Tennyson

s. emt. dr	4.06	94.52
gutter parvnt	4.78	93.80
"	4.39	94.19
e "	4.17	94.41
"	4.35	94.23
gutter "	4.70	93.88
N. emt. dr.	4.06	94.52
0+0' 0" W.		
N. emt. dr	4.06	94.52
emt. gutter	5.06	93.52
+ 1.8 = s. edge emt. gutter	4.88	93.70
"	4.5	94.1
e	4.2	94.4
"	4.5	94.1
+ 7.6 = N. edge emt. gutter	4.86	93.72
+ 8.8 e " "	5.01	93.57
+ 10.5 " " "	4.89	93.69
s. emt. dr	4.08	94.50
0+25' W.		
s. emt. dr	4.53	94.05
emt. gutter	5.32	93.26
+ 1.2 e emt. gutter	5.47	93.11
+ 2.4 N. edge emt. gutter	5.35	93.23
"	5.2	93.4

e	4.8	93.8
"	5.0	93.6
+ 8.2 = s. edge emt. gutter	5.23	93.25
+ 10 emt. gutter	5.42	93.16
N. emt. dr	4.48	94.10
0+40' W. = N. end emt. gutter on S		
N. emt. dr	4.74	93.84
emt. gutter	5.66	92.92
+ 1.2 = s. edge emt. gutter	5.62	92.96
"	5.3	93.3
e	5.1	93.5
"	5.6	93.0
+ 7.6 = N. edge emt. gutter	5.61	92.97
+ 8.8 e " "	5.76	92.82
+ 10.5 " " "	5.60	92.98
s. emt. dr.	4.78	93.80
0+50' W.		
s. emt. dr	5.00	93.58
gutter	6.0	92.6
"	5.8	92.8
e	5.2	93.4
"	5.6	93.0
+ 8.2 = s. edge emt. gutter	5.78	92.80
+ 10 = N. " " "	5.90	92.68
N. emt. dr	4.93	93.65

98.58
0+75' W.

N. ent. ch	5.43	93.15
ent. gutter	6.34	92.24
+1.8 = s. edge ent. gutter	6.31	92.27
"4	5.9	92.7
c	5.7	92.9
"4	6.2	92.4
gutter	6.6	92.0
s. ent. ch.	5.43	93.15

From 0+87^E W. to 1+22^E W. Walk road on W. cracked & buckled

" 1+95	" 2+01	" " " " " " " "
" 3+12 ^E	" 3+15 ^E	" " " " " " " "
" 3+21 ^E	" 3+77 ^E	" " " " " " " "
" 3+85 ^E	" 3+92 ^E	" " " " " " " "

1+00 W.

s. ent. ch	5.90	92.68
gutter	7.1	91.5
"4	6.6	92.0

98.58

Tennyson St

11

c	6.0	92.6
"4	6.2	92.4
+8.2 = s. edge ent. gutter	6.72	91.86
+10 N " " "	6.78	91.80
N. ent. ch	5.85	92.73

1+25 W

N. ent. ch	6.29	92.29
ent. gutter	7.17	91.41
+1.8 = s. edge ent. gutter	7.17	91.41
"4	6.6	92.0
c	6.4	92.2
"4	7.0	91.6
gutter	7.5	91.1
s. ent. ch	6.32	92.26

1+50 W

s. ent. ch	6.91	91.67
gutter	8.0	90.6
"4	7.4	91.2
c	6.8	91.8
"4	7.1	91.5
+8.2 = s. edge ent. gutter	7.65	90.93
+10 " " "	7.74	90.84
N. ent. ch	6.80	91.78

98.58

1 + 75 W.

N. ent. cl.	7.37	91.21
ent. gutter	8.29	90.29
+1.8 = s. edge ent. gutter	8.12	90.46
$\frac{1}{4}$	7.6	91.0
c	7.3	91.3
$\frac{1}{4}$	7.8	90.8
gutter	8.3	90.3
S. ent. cl.	7.33	91.25

R + 00 W

S. ent. cl.	7.88	90.70
gutter	8.8	89.8
$\frac{1}{4}$	8.3	90.3
c	7.8	90.8
$\frac{1}{4}$	8.1	90.5
+8.2 = s. edge ent. gutter	8.62	89.96
+10 " "	8.71	89.87
N. ent. cl.	7.78	90.80

R + 25 W

N. ent. cl.	8.24	90.34
ent. gutter	9.15	89.43
+1.8 = s. edge ent. gutter	9.07	89.49
$\frac{1}{4}$	8.5	90.1
$\frac{1}{4}$	8.3	90.3
$\frac{1}{4}$	8.8	89.8
gutter	9.3	89.3
S. ent. cl.	8.39	90.19

98.58

R + 50 W

Tennyson

12

S. ent. cl.	8.86	89.72
gutter	9.8	88.8
$\frac{1}{4}$	9.3	89.3
c	8.8	89.8
$\frac{1}{4}$	9.0	89.6
+8.2 = s. edge ent. gutter	9.58	89.00
+10 " "	9.64	88.94
N. ent. cl.	8.74	89.84

R + 75 W

N. ent. cl.	9.24	89.34
ent. gutter	10.16	88.42
+1.8 = s. edge ent. gutter	10.06	88.52
$\frac{1}{4}$	9.7	88.9
c	9.4	89.2
$\frac{1}{4}$	9.8	88.8
gutter	10.3	88.3
S. ent. cl.	9.23	89.35

R + 00

S. ent. cl.	9.63	88.95
gutter	10.8	87.8
$\frac{1}{4}$	10.3	88.3
c	10.0	88.6
$\frac{1}{4}$	10.2	88.4
+8.2 = s. edge ent. gutter	10.47	88.11
+10 = N " " "	10.62	87.96
N. ent. cl.	9.71	88.87

98.58

T.P.	2.44	90.66	10.36	88.22
	3+R5 W.			
N. ent. cl.		2.23		88.43
ent. gutter		3.12		87.54
+1.8 = s. edge ent. gutter		2.94		87.72
"		2.8		87.8
c		2.5		88.1
"		2.9		87.7
gutter		3.3		87.3
S. ent. cl.		2.23		88.43
	3+50 W.			
S. ent. cl.		2.60		88.06
gutter		3.5		87.1
"		3.2		87.4
c		2.9		87.7
"		3.1		87.5
+8.2 = s. edge ent. gutter		3.21		87.45
+10 " "		3.40		87.26
N. ent. cl.		2.44		88.22
	3+75' W			
N. ent. cl.		2.75		87.91
ent. gutter		3.71		86.95
+1.8 = s. edge ent. gutter		3.55		87.11
"		3.4		87.2
c		3.3		87.3
"		3.5		87.1

90.66

Tennyson. St.

13

gutter		3.9		86.7
S. ent. cl.		2.88		87.78
	4+00 W.			
S. ent. cl.		3.15		87.51
gutter		4.0		86.6
"		3.8		86.8
c		3.7		86.9
"		3.7		86.9
+4.2 = s. edge ent. gutter		3.89		86.77
+10 " "		4.04		86.62
N. ent. cl.		3.07		86.59
	4+34 ²⁵ W = E. line Wabaska Drive on W. - see A Page 14			
N. ent. cl.		3.48		87.18
ent. gutter		4.48		86.18
+1.8 = s. edge ent. gutter		4.31		86.35
"		3.9		86.7
c		4.0		86.6
"		4.1		86.5
gutter		4.4		86.2
N. ent. cl. P.C. 10' Radius Return		3.55		87.11
T.P.	2.72	90.81	2.57	88.09

90.81

Sec. D. (con)

+8.2 = s. edge covered with dirt emt. gutter	5.32	85.49	No yardage
+10 " " & dirt	5.45	85.36	
N. emt. cl.	4.50	86.31	

5+44.40 = Sec. E, 58' wide

N. emt. cl.	4.89	85.92		
gutter, dirt.	5.4	85.4		
emt. gutter	5.85	84.96		no yardage
+1.8 = s. edge emt. gutter	5.70	85.11		" "
+2 dirt for yardage	4.6	86.2		" "
"	4.5	86.3		" "
cl	4.7	86.1		" "
"	4.8	86.0		" "
s. cl. produced	4.9	85.9		" "
s	5.0	85.8		" "

Sec. F.

5+74.40 = E. line Warrington 60' wide

s.	5.0	85.8		
s. cl. line produced	4.6	86.2		
"	4.6	86.2		
c	4.5	86.3		
"	4.5	86.3		
+8. dirt for yardage	4.5	86.3		
+8.2 = W. End. S. side emt. gutter	6.00	84.81		no yardage
+10 " " "	6.08	84.73		" "
+10 dirt in gutter for yardage	4.8	86.0		" "
N. End. N. emt. cl. + walk	5.21	85.61		" "
N. cl. on dirt	4.6	86.2	" "	
+10 = N. Line	4.5	86.3	" "	

90.81

Tennison St.

15

5+78.15 W = Sec. G. 60.2 Bet. emt curbs

N. Line	4.4	86.4	
N. cl. line	4.5	86.3	
"	4.5	86.3	
cl	4.5	86.3	
"	4.5	86.3	
s. cl. Line Produced	4.6	86.2	
s. gutter	5.0	85.8	
s. emt. cl.	4.46	86.35	

5+89.40 W. = E. cl. Warrington 56.8 Bet. cl. lines

s. emt. cl.	4.56	86.25	
gutter	5.0	85.8	
s. cl. line Tennison Produced	4.7	86.1	
"	4.5	86.3	
c	4.5	86.3	
"	4.5	86.3	
cl	4.6	86.2	
N. line +	4.5	86.3	

5+96.20 = E. 1/4 Warrington 54.8 Bet. cl. lines

N. line	5.0	85.8	
cl	4.7	86.1	
"	4.4	86.4	
c	4.4	86.4	
"	4.5	86.3	
S. cl. line Tennison Produced	4.6	86.2	
s. gutter	4.9	85.9	
s. emt. cl.	4.46	85.35	

90.81
6+04.40 W. = Warrington.

s. emb. ch	4.33	85.48
gutter	4.8	86.0
S. ch. line Tennyson Produced	4.6	86.2
"4	4.4	86.4
c	4.4	86.4
"4	4.4	86.4
ch	4.7	86.1
N. line	5.2	85.6

6+09.45 = S.E. Cor Tennyson & Alicia Drive ? 52.5 Bet ch. lines

N. line	5.0	85.8
ch	4.5	86.3
"4	4.4	86.4
c	4.4	86.4
"4	4.4	86.4
S. ch. line Tennyson Produced	4.6	86.2
S. gutter	4.7	86.1
S. emb. ch.	4.29	86.52

6+11.20 = W. 1/2 Warrington 52.7 Bet ch. lines

S. emb. ch. on 10' Rad. Return	4.27	86.53
gutter	4.7	86.1
S. ch. line Tennyson Produced	4.6	86.2
"4	4.4	86.4
c	4.4	86.4
"4	4.4	86.4
ch	4.4	86.4
N. line	4.9	85.9

90.81

Tennyson St

16

6+19.40 W. = W. ch. line Warrington

N. Line	5.5	85.3
ch	4.4	86.4
"4	4.4	86.4
c	4.4	86.4
"4	4.4	86.4
S. ch. Tennyson Produced	4.5	86.3

6+20.20 W. = S. ch. line Alicia ?

S. emb. ch. of Alicia	4.14	86.67
gutter	4.5	86.3
S. ch. Tennyson Produced	4.6	86.2
"4	4.5	86.3
c	4.4	86.4
"4	4.4	86.4
N. ch. line	4.5	86.3
N. line	4.9	85.9

6+32.45 W. = S. 1/4 Alicia ?

N. Line	4.7	86.1
N. ch. line	4.7	86.1
"4	4.5	86.3
c	4.4	86.4
"4	4.4	86.4
S. ch. Tennyson Produced	4.3	86.5
S.	4.4	86.4

90.81
6+34⁴⁰ N. = W. Line Warrington.

S.	4.3	86.5	} 40' 58.7
S. db. line Tennyson Produced.	4.3	86.5	
"	4.4	86.4	
"	4.4	86.4	
"	4.5	86.3	
N. ent. db. + ground. E. End ent. db. + walk	4.73	86.08	
N. line	4.5	86.3	

6+44²⁰ N = Alicia ?

N. ent. db. + ground. in gutter	4.70	86.11	} 40' 57.5
"	4.5	86.3	
"	4.4	86.4	
"	4.4	86.4	
S. db. Tennyson Produced	4.2	86.6	
S	4.1	86.7	

6+55²⁵ = N. by Alicia ans. ?

S	4.1	86.7	} 40' 55.7
S. db. Tennyson Produced	4.1	86.7	
"	4.4	86.4	
"	4.4	86.4	
"	4.6	86.2	
N. ent. db. + ground. in gutter	4.58	86.23	

90.81

Tennyson St.

17

6+67²⁰ = N. N. db. Alicia ?

N. ent. db. + gutter	4.51	86.30	} 40' 53.9
"	4.6	86.2	
"	4.5	86.3	
"	4.3	86.5	
S. db. line Tennyson Produced	4.1	86.7	
S. gutter	4.1	86.7	
S. ent. db. on 10' Rad. Ret.	3.66	87.15	

6+74⁴⁰ = N. End. ent. db. + walk on N. of Tennyson.

S. ent. db. on 10' Rad Ret	3.68	87.13	} 40' 43.0
gutter	4.2	86.6	
S. db. Tennyson Produced	4.1	86.7	
"	4.3	86.5	
"	4.4	86.4	
"	4.5	86.3	
N. ent. db. + gutter dirt	4.50	86.31	
N. line	4.2	86.6	

6+77²⁰ N = N. W. line Alicia ?

N. line	4.1	86.7	} 40' 42.2
N. db. line	4.4	86.4	
"	4.5	86.3	
"	4.4	86.4	
"	4.3	86.5	
S. db. line Tennyson Produced.	4.7	86.7	
gutter	4.2	86.6	
S. ent. db.	3.66	87.15	

Wabaska Drive X Sec
Tennyson to Chatsworth Blvd

5-24-29
mills

90.81

18

90.81 Page 17

31' N. W. 1/4 sec H. Page 14.

SW. cont. cl.	4.46	86.35
gutter	5.0	85.8
Sec. H. Page 14. on Radial Line		
SW. cont. cl.	4.62	86.19
gutter	5.3	85.5
12.4 N.E. = S. line Tennyson	5.0	85.8
30' S. on W. cl. = Sec. I.		
S.W. cont. cl.	4.79	86.02
gutter	5.5	85.3
13.2 N.E.	5.2	85.6
26.4 N.E. = S. line Tennyson	5.2	85.6
20.9 S. of Jan w. cl. = Sec. J = N. Alley Ret. on Radial Line		
W. line on Alley Ret + ground.	4.99	85.82
W. cont. cl.	4.92	85.89
gutter	5.2	85.6
19.75 E	5.4	85.4
39.5 E = S. line Tennyson	5.1	85.7
16.7 S. of Jan w. cl. Sec. K = S. Alley Ret on Radial Line		
W. line Alley Ret + ground	4.92	85.89
W. cont. cl.	4.98	85.83
gutter	5.4	85.4
24.5 E	5.4	85.4
49.8 = S. line Tennyson	5.1	85.7

15' S. of Kan w. cl. = Sec L on Radial Line

W. cont. cl.	4.97	85.84
gutter	5.5	85.3
+ 14.85	5.5	85.3
+ 29.70	5.4	85.4
+ 44.55	5.2	85.6
+ 59.35 gutter	4.8	86.0
+ 59.95 = cont. cl. Ret.	3.90	86.91
22.5 S. of Kan w. cl. = Sec M. on Radial Line 56' wide		
W. cont. cl.	5.07	85.74
gutter	5.5	85.3
+ 14 = 14.14	5.6	85.2
+ 28 = 28	5.4	85.4
+ 42 = 42.14	5.1	85.7
+ 56.5 = gutter	5.0	85.8
+ 56 = S. cont. cl.	4.04	86.77
T.P. 0.09	88.14	2.72
21.5 S. of M. on W. cl. } Sec. N 58.4 Ret. cl.s		
25.7 " " " " " " }		
E. cont. cl.	1.69	86.49
gutter	2.6	85.6
+ 14.6 = 14	2.6	85.6
+ 29.2 = 29	2.9	85.3
+ 43.8 = 43	3.0	85.2
gutter	3.0	85.2
W. cont. cl.	2.65	85.53

88.18

22.5 2.0 x N. on W. ch } = Sec. O. 60' bet chs
25.7 " " N. on E. ch }

W. cont. ch	2.74	85.34
gutter	3.1	85.1
+15 = 1/4	3.1	85.1
+30 = ϕ	2.9	85.3
+45 = 1/4	2.7	85.5
gutter	2.9	85.3
E. cont. ch	1.93	86.15

22.5 5.0 x 0. on W. ch } = Sec. P. = P.C. curb lines 60' wide
25.7 5 " 0 " E. ch }

E. cont. ch	2.27	85.91
gutter	3.2	85.0
+15 = 1/4	3.0	85.2
+30 = ϕ	3.2	85.0
+45 = 1/4	3.2	85.0
gutter	3.2	85.0

N. cont. ch }
15' S. on E. ch } = Sec Q = N. line ATASCADERO Drive 60' wide
15' S. on W. ch }

W. cont. ch	2.97	85.21
gutter	3.2	85.0
"	3.2	85.0
e	3.2	85.0
"	3.1	85.1
gutter	3.5	84.7
E. cont. ch	2.38	85.80

88.18

Wapaska

19

N. ch

E. cont. ch	2.48	85.70
gutter	3.6	84.6
"	3.2	85.0
e	3.3	84.9
"	3.1	85.1
W. ch. line	3.0	85.2
W. on Mend cont. ch Ret	2.62	85.56
W. king gutter	2.9	85.3

N 1/4

W. line	2.8	85.4
ch. line	2.9	85.3
"	3.3	84.9
e	3.4	84.8
"	3.2	85.0
gutter	3.6	84.6
E. cont. ch	2.56	85.62

Atascadero Drive

E. cont. ch	2.66	85.52
gutter	3.8	84.1
"	3.3	84.9
e	3.5	84.7
"	3.4	84.8
ch. line	2.9	85.3
W. "	2.4	85.6

88.18

S. 14

W. line	3.1	85.1
ch "	3.2	85.0
" "	3.5	84.7
c	3.6	84.6
" "	3.4	84.8
gutter	3.9	84.3
E. ent. ch	2.77	85.41

S. ch.

E. ent. ch	2.91	85.29
gutter	4.0	84.2
" "	3.5	84.7
c	3.7	84.5
" "	3.5	84.7
W. ch. line	3.2	85.0
W. line gutter	3.1	85.1
" " W. end ent. ch. Ret.	2.74	85.44

Earnice

00 - S. line ~~Atasadero~~ Drive 60' Rdw.

W. ent. ch	3.02	85.16
gutter	3.4	84.8
" "	3.5	84.7
c	3.8	84.4
" "	3.6	84.6
gutter	4.0	84.2
E. ent. ch	3.01	85.17

89.18

52.55

Wabaska

20

E. ent. ch	3.72	84.46
gutter	4.6	83.6
" "	4.1	84.1
c	4.2	84.0
" "	3.9	84.3
gutter	4.1	84.1
W. ent. ch.	3.49	84.69

105.5 = N. ch. Ret on W.

W. line ground	3.7	84.5
105.5 - W. end. ent. ch. Alley Ret.	3.72	84.46
N. ent. ch.	4.08	84.10 ✓
gutter	4.7	83.5
" "	4.6	83.6
c	4.7	83.5
" "	4.6	83.6
gutter	5.3	82.9
E. ent. ch.	4.44	83.74

120.5 = S. Alley Ret

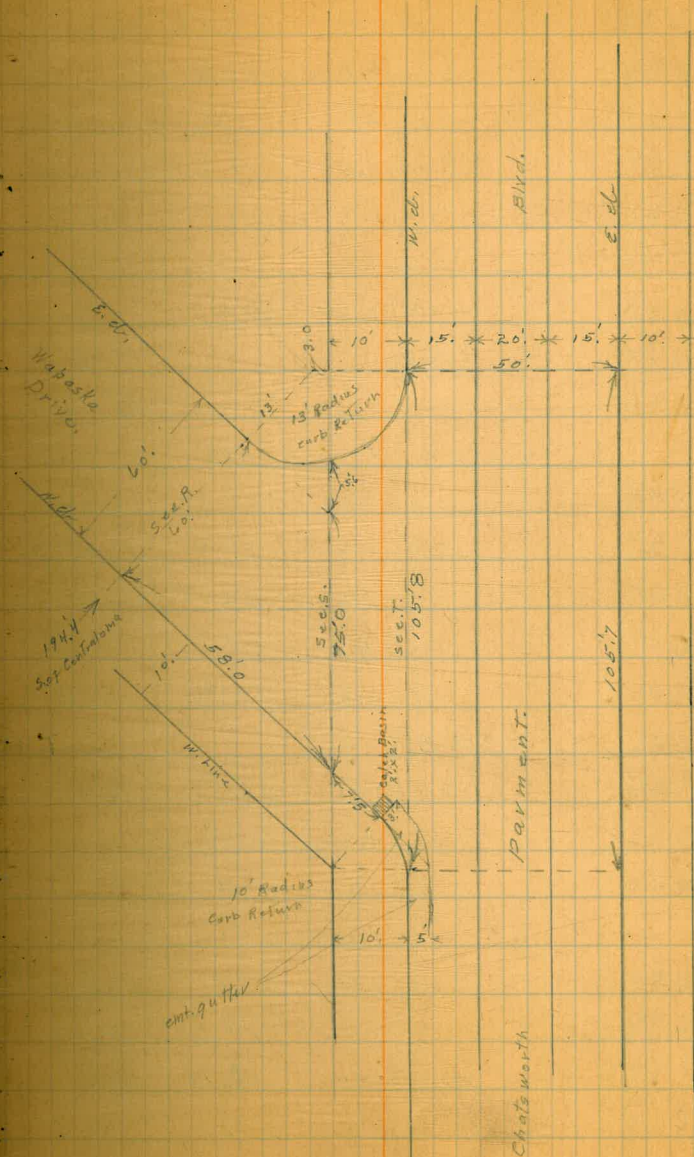
E. ent. ch	4.63	83.55
gutter	5.4	82.8
" "	4.8	83.4
c	5.0	83.2
" "	4.8	83.4
gutter	5.0	83.2
N. ent. ch	4.35	83.83
#9.2 = W. end ent. ch. Alley Return	4.06	84.2
W. line ground	4.3	83.9

88.18
172.5 5

W. ent. ch	4.99	83.19
gutter	5.5	82.7
"	5.5	82.7
c	5.5	82.7
"	5.4	82.8
gutter	6.2	82.0
E. ent. ch	5.28	82.90
225' S. = N. line Centraloma Drive 60' wide Paved		
E. ent. ch	5.98	82.20
gutter Pavmt.	6.61	81.57
" "	6.11	82.07
c "	5.84	82.34
" "	5.82	82.36
gutter "	6.18	82.00
W. ent. ch	5.61	82.57
002 S. line Centraloma Drive		
W. ent. ch	6.05	82.13
gutter pavmt	6.82	81.36
" "	6.41	81.77
c "	6.38	81.80
" "	6.66	81.52
gutter "	7.18	81.00
E. ent. ch	6.42	81.76
T.P.	3.72	84.00
	7.90	80.28

Wabaska

21



84.00

40' S. of Centraloma

E. end. ch	2.71	81.29
gutter	3.7	80.3
"	3.3	80.7
c	3.3	80.7
"	3.4	80.6
gutter	3.3	80.7
W. end. ch	2.60	81.40

40' S.

W. end. ch	2.95	81.05
gutter	3.7	80.3
"	3.7	80.3
c	3.6	80.4
"	3.6	80.4
gutter	4.0	80.0
E. end. ch	3.01	80.99

80' S.

E. end. ch	3.41	80.59
gutter	4.2	79.8
"	3.9	80.1
c	4.0	80.0
"	4.0	80.0
gutter	4.2	79.8
W. end. ch	3.30	80.70

84.00

Wabaska

22

105' S. = N. Line Alley on W.

N. line ground	4.6	79.4
+ 9.0 = W. end. ch. Alley Ret.	3.65	80.35
W. ch. line end. ch	3.80	80.20
" " gutter	4.7	79.3
"	4.5	79.5
c	4.5	79.5
"	4.4	79.6
gutter	4.9	79.1
E. end. ch	3.87	80.13

120' S. = S. Line Alley on W.

E. end. ch	4.21	79.79
gutter	5.3	78.7
"	4.7	79.3
c	4.7	79.3
"	4.7	79.3
gutter	4.9	79.1
W. end. ch	3.98	80.05
+ 9.0 = W. end. ch. Alley Ret.	3.95	80.05
N. line ground	4.6	79.4
157' 2" S		
W. end. ch	4.68	79.32
gutter	5.6	78.4
"	5.3	78.7
c	5.3	78.7
"	5.5	78.5
gutter	5.9	78.1
E. end. ch	5.03	78.97

84.00

194.4 S = See R. = P.C. 13' Rad. Return on E

S. cont. db	5.75	77.25
gutter	6.6	77.4
"	5.9	78.1
e	5.8	78.2
"	6.0	78.0
gutter	6.1	77.9
W. cont. db.	5.44	78.56

Sec. S. = N.W. Line Chatsworth 80.6 wide

W. cont. db	6.43	77.57
gutter	7.0	77.00
+ 18.75 = "y	6.6	77.4
+ 37.5 = "	6.2	77.8
+ 56.25 = "	6.2	77.8
+ 75 = E. db. Line Produced.	6.5	77.5
+ 80.6 = gutter	6.3	77.7
+ 80.6 = E. cont. db. Return	6.00	78.0

Sec. T. = N.W. db. Line Chatsworth 105.8 wide

on E. End 13' Rad. Return	5.88	78.12
gutter	6.0	78.0
+ 25.8 = E. db. Line Wakasaka produced	6.6	77.4
E. db + 18.75 = E. "y	6.6	77.4
E. db + 37.50 = "	6.4	77.6
" " + 56.25 = W. "y	6.6	77.4
" " + 75. = W. db. Line Produced.	7.3	76.7
cont gutter at S. End. 10' R. Return	7.26	76.64
Top cont. db " " " " "	6.47	77.53

84.00

Wakasaka

15' S. of N. db. Chatsworth = N. Edge Farm

23

5.75 S. of S. End. 10' Rad. Ret = 0.0 = W. db. Line Produced.	4.99	77.01	
+ 5.75 N.E. = 90' from S. End 10' Rad. Ret.	7.05	76.95	
+ 18.75 = W. "y Produced	7.09	76.91	
+ 37.50 = "	7.09	76.91	
+ 56.25 = E. "y	7.12	76.88	
+ 66.25	6.98	77.02	
+ 75 = E. db. Line "	6.70	77.30	
+ 80.6 = E. End 13' Rad. Ret.	5.30	78.70	
T.P. 12.65	91.76	4.89	77.11 ✓
T.P. 6.19	96.84	1.11	90.65 ✓
check original B.M. Page 10	0.19	96.65 = 96.65	

6-28-29 Curb Levels - South side El Cajon
 J.C. Bliss Seminole to El Cajon Place
 Drebert
 Ranner

B.M.S. W.B.P. El Cajon + Polando 452.51
 4.44

T 456.95

South end - S.E. Return - El Cajon + Seminole

Tp cb 0.60 456.35
 Gutter 1.25

+20 = East end S.E. Return = 0+00 - Curve - Seminole to Campo

Tp cb 0.81 456.14
 G 1.44

0+25

Tp cb 1.33 455.62
 G 1.92

0+50

Tp cb 1.86 455.09
 G 2.45

0+75

Tp cb 2.28 454.67
 G 2.90

1+00

Tp cb 2.85 454.10
 G 3.47

1+25

Tp cb 3.39 453.56
 G 4.02

2.44
 8.529
 1.541

T 456.95

1+50

Tp cb 3.78 453.17
 G 4.50

1+80 = Grating cb Inlet

Tp cb 4.43 452.52
 Tp Grating 5.38

2+38 = West end - S.W. Return = 0+00 ^{El Cajon + Campo}

Tp cb 4.05 452.96
 G 4.43

+11 = South end S.W. Return

Tp cb 3.89 453.06
 G 4.16

South end - S.E. Return = 0+00 ^{El Cajon + Campo}

Tp cb 3.71 453.24
 G 4.40

0+16.5

Tp cb 3.85 453.10
 G 4.55

0+33 = S.L. El Cajon

Tp cb 3.97 452.98
 G 4.57

0+51

Tp cb 4.06 452.89
 G 4.66

T 456.95

0+69 = East end S.E. Return - 0+00

Tpcb 4.05 452.90

G 4.75

0+25

Tpcb 4.13 452.82

G 4.83

0+50

Tpcb 4.19 452.76

G 4.87

0+75

Tpcb 4.25 452.70

G 4.90

1+00

Tpcb 4.32 452.63

G 5.02

1+25

Tpcb 4.40 452.55

G 5.10

1+50

Tpcb 4.40 452.55

G 5.17

1+75

Tpcb 4.45 452.50

G 5.25

T 456.95

2+07.5 = West end S.W. Return - El Cajon + Rolando = 0+00

25

Tpcb 4.45 452.50

G 5.30

T.P. S.W.B.P. El Cajon + Rolando - 4.44 452.51

+0.47 T 452.98

0+25

Tpcb 0.65 452.33

G 1.38

0+45 = S.L. El Cajon

Tpcb 0.78 452.20

G 1.43

0+77 = South end - S.W. Return

Tpcb 0.85 452.13

G 1.43

South end S.E. Return El Cajon + Rolando = 0+00

Tpcb 1.16 451.82

G 1.82

0+18

Tpcb 1.13 451.85

G 1.85

0+35 = S.L. El Cajon

Tpcb 1.13 451.85

G 1.85

0+50

Tpcb 1.19 451.89

G 1.98

π 452.98

0+68 = East end - S.E. Return - 0+100

Tpcb 1.20 451.78

G 2.15

0+25

Tpcb 1.76 451.22

G 2.64

0+50

Tpcb 2.28 450.70

G 3.13

0+90 = West end S.W. Return El Cajon * El Cajon Place - 0+100

Tpcb 3.37 449.61

G 4.05

0+25

Tpcb 4.20 448.78

G 4.86

0+50

Tpcb 5.31 447.67

G 5.93

0+75

Tpcb 6.31 446.67

G 7.00

1+00

Tpcb 7.35 445.63

G 8.03

1+25

π 452.98

26

1+50

Tpcb 9.32 443.66

G 9.88

1+91 = South end S.W. Return

Tpcb 10.53 442.45

G 11.18

B.M. S.E. Nails in Pole El Cajon * El Cajon Place -7.50 445.48

Correct 445.49

6-28-29

J. C. Bliss
Drebert

X-section Central Ave -
Redwood to Lexington.

Rauner 80' Wide - 14' cbs - 13 1/4

End 200

Σ 306.14

27

B.M. N.W.B.P. 40th & Redwood 302.97

+6.20 309.17

T.P. S.W. Prop. Hub. Central & Redwood -5.08 304.09

+2.05

Σ 306.14

S.W. Redwood = 0+00

N 1.9 3042

cb 2.1 3040

1/4 1.9 3042

ϕ 2.0 3041

1/4 2.3 3038

cb 2.8 3033

E 3.3 3028

Plotted 7-5-28
G.M.J.

E +25 3.0 3031

cb 2.1 3040

1/4 2.2 3039

ϕ 2.2 3039

1/4 2.1 3040

cb 1.8 3043

W 1.3 3048

0+50

W 1.9 3042

cb 2.3 3038

1/4 2.5 3036

ϕ 2.3 3038

1/4 2.4 3037

cb 2.6 3035

E 2.9 3032

0+75

E 2.9 3032

cb 2.8 3033

1/4 2.5 3036

ϕ 2.5 3036

1/4 2.8 3033

cb 2.3 3038

W 2.4 3037

1+00

W 2.5 3036

cb 2.7 3034

1/4 2.9 3032

ϕ 3.0 3031

1/4 3.1 3030

cb 3.0 3031

E 3.1 3030

1+25

E 3.5 3026

cb 3.3 3028

1/4 3.6 3025

ϕ 3.4 3027

π 306.14

1/4	3.5	3026
cb	3.4	3027
W	3.1	3030
1450		
W	3.6	3025
cb	4.0	3021
1/4	3.6	3025
♀	3.9	3022
1/4	4.1	3020
cb	4.0	3021
E	4.1	3020

1475

E	4.7	3014
cb	4.4	3017
1/4	4.7	3019
♀	4.6	3015
1/4	4.4	3017
cb	4.2	3019
W	4.3	3018

2400

W	4.6	3015
cb	4.7	3019
1/4	5.0	3011
♀	5.1	3010
1/4	5.3	3008

π 306.14

28

cb	5.2	3009
E	5.5	3006
2425		
E	6.3	2998
cb	6.0	3001
1/4	6.2	2999
♀	5.9	3002
1/4	5.6	3005
cb	5.5	3006
W	5.3	3008

0-78 to 2426 - Row of 5 small trees
10' in St. from E.L.

2450

W	6.0	3001
cb	6.2	2999
1/4	6.5	2996
♀	6.6	2995
1/4	6.9	2992
cb	7.3	2988
E	7.4	2987

2454

♀ 8' Garage at W.L.	6.1	3000
2463		
♀ 8' Garage at W.L.	6.4	2997

π 306.14

2475

E	9.2	2969
cb	8.6	2975
1/4	8.1	2980
£	7.5	2986
1/4	7.0	2991
cb	6.7	2994
W	6.7	2994

3400

W	7.6	2985
cb	8.0	2981
1/4	8.3	2978
£	8.7	2974
1/4	9.8	2963
cb	10.6	2955
E	11.7	2944

3425

E	14.6	2915
cb	13.0	2931
1/4	11.8	2943
£	11.0	2951
1/4	9.7	2964
cb	9.3	2968
W	9.1	2970

π 306.14

29

3450

W	11.0	2951
cb	11.3	2948
1/4	13.6	2925
T.P		-12.85 293.29

+0.26

π 293.55

£	2.3	2913
1/4	3.4	2902
cb	3.3	2903
E	4.5	2891

3475

E	6.7	2869
cb	6.6	2870
1/4	6.0	2876
£	6.0	2876
1/4	5.8	2878
cb	3.6	2900
W	2.9	2907

4400

W	7.1	2865
cb	7.2	2864
1/4	8.9	2847
£	9.5	2841
1/4	10.1	2835
cb	9.5	2841

T 293.55

E	9.9	2837
	4+25	
E	12.8	2808
cb	12.2	2814
1/4	12.5	2811
♀	12.5	2811
1/4	11.0	2826
cb	10.4	2832
W	10.6	2830
T.P.		-12.77 280.78

+1.21

T 281.99

4+50

W	3.4	2786
cb	2.9	2791
1/4	3.0	2790
♀	3.6	2784
1/4	3.2	2788
cb	3.2	2788
E	3.5	2785

4+75

E	7.1	2749
cb	7.2	2748
1/4	6.9	2751
♀	7.2	2748
1/4	7.3	2747

T 281.99

30

cb	7.7	2743
W	8.6	2757
	5+00	
W	12.6	2699
cb	11.8	2702
1/4	11.6	2704
♀	12.6	2694
1/4	11.5	2705
cb	11.6	2704
E	11.2	2708
E-♀ 3' Concrete Wall Kot EL.	11.00	2710

T.P.

-12.73 269.26

+0.31

T 269.57

5+25

E-Base Cobble Wall-Top 1' Higher	2.8	2668
cb	4.3	2653
1/4	4.3	2653
♀	4.1	2655
1/4	3.7	2659
cb	4.3	2653
W	5.4	2642
	5+50	
W	12.2	2574
cb	8.9	2607
1/4	8.9	2607

T 269.57

‡	9.5	2601
1/4	8.5	2611
cb	8.1	615
E-Base Cobble Wall-Top 2.7 Higher	5.1	645
5+62		
E-Base Cobble Wall-Top 2.5 Higher	5.1	645
cb	7.0	626
1/4	8.5	611
‡	9.5	601
1/4	12.7	569
cb	19.0	506
W	26.5	431

Drain drops very steeply from W.

5+75		
Out 30	41.8	278
W	20.6	490
cb	15.9	537
1/4	13.8	558
‡	12.6	570
1/4	10.7	589
cb	8.3	613
E-Base Cobble Wall-Top 2.2 Higher	5.1	645

Wall stops at 5+77 - started at 5+00

T 269.57

31

T.P		-13.04	256.53
	+2.27		T 258.80
6+00 = N.L. Quince			
E	2.5		256.3
cb	5.4		53.4
1/4	10.1		48.7
‡	14.4		44.4
1/4	16.3		42.5
cb	17.0		41.8
W	22.3		36.5

Intersection of Central + Quince X-sectioned on Quince - Book 1331 - Pgs 57-58

T.P		-12.67	246.13
	10.81		246.94
T.P		-13.07	233.87

+ 5.77
T 239.64
S.L. Quince = 0+00

W	19.7		219.9
cb	24.7		14.9
1/4	27.4		12.2
E-Bottom ditch	27.9		11.7
1/4	24.2		15.4
cb	19.4		20.2
E	16.4		23.2

T 239.64

0+25

E	26.2	213.4
cb	27.1	12.5
1/4	28.2	11.4
+9-Bottom ditch	31.0	8.6
♀	28.5	11.1
1/4	24.0	15.6
cb	19.1	20.5
W	13.8	25.8

0+50

W	9.0	30.6
cb	15.7	23.9
1/4	18.0	21.6
♀	22.5	17.1
1/4	28.3	11.3
cb	31.1	08.5
E-Bottom Ditch	36.0	203.6
Out 10	31.0	208.6

0+75

E	34.4	205.2
cb-Bottom Ditch	37.8	201.8
+5	33.3	206.3
1/4	31.0	208.6
♀	24.5	215.1
1/4	15.4	224.2
cb	8.9	230.7

T 239.64

32

W	28	236.8
	1400	
W	20	237.6
cb	7.5	232.1
1/4	14.5	225.1
♀	20.0	219.6
1/4	25.0	214.6
cb	31.5	208.1
E	35.0	204.6
Out 15-Bottom Ditch	40.4	199.2
Out 25-	36.4	203.2

1+25

Out 15-Bottom ditch - also junction with wash on Lexington	42.2	197.4
E	33.2	206.4
cb	29.0	210.6
1/4	24.0	215.6
♀	18.7	220.9
1/4	12.9	226.7
cb	8.1	231.5
W	4.3	235.3

1+50

W	10.3	229.8
cb	13.8	225.8
T.P.		- 12.5 227.39

+0.32 227.71

T 227.71

1/4	8.5	219 ✓
¢	14.5	213 ✓
T.P.		-1301 214.70
+ 0.59	T 215.29	
1/4	5.6	209 ✓
cb	9.1	206 ✓
E-Base Bank	19.1	196 ✓
Out 5 - £ Lexington Wash	19.3	176 0
	147.5	
E	18.5	196.8
+V	18.4	196.9
cb-£ Lexington Wash	21.2	194.1
16	20.1	195.2
1/4	18.0	197.3
¢	14.7	200.6
1/4	6.4	208.9
cb	7.2	208.1
W	5.0	210.3
T.P.		-12.98 202.31

+ 1.63

T 203.94

N.L. Lexington & E.L. Central intersect at
Sta 1490 on E.L. Central

2400

W

6.8

1971

T 203.94

33

cb	8.1	195.8
1/4	8.2	195.7
¢	8.1	195.8
+5.5	8.0	195.9
+7	10.2	193.7
1/4-£ Lexington Wash	10.5	193.4
cb	9.0	194.9
+3 = N.L. Lexington	8.2	195.7
	2425 - Intersection £ Central & N.L. Lexington	
¢	7.8	196.1
+5	8.8	195.1
1/4	11.2	192.7
cb-£ Lexington Wash	11.8	192.1
+5	11.8	192.1
+6	9.9	194.0
W	9.1	194.8
	2460 = Inter section N.L. Lexington & N.L. Central	
W	11.7	192.2
	Sta 2450 West Line Central	
£ Lexington Wash	12.6	191.3
B.M. N.E. Hub Lexington & Central		-2.57 196.55
		Correct 196.30
B.M. Top N.H. 100' E of E.L. Central & on N.L. Lexington		-4.29 199.65
		Correct 199.63

7-1-29 X-section 42nd St. Thorn to
 J.C. Bliss. Lexington 80' wide
 Dreber 12' cbs
 Ranner 13' 1/45

B.M. NE B.P. Van Dyke & Thorn 308.70
 0.18

π 308.88

Sub line Thorn

E Tpcb	9.92	298.96
G	10.54	298.34
cb-Tpcb	9.87	299.01
G	10.63	298.25
1/4-Tpcb	9.78	299.10
G	10.80	298.08
£ Tpcb	9.76	299.12
G - Grating Flowline Inlet	10.74	298.14
cb Inlet	27.80	281.08
1/4-Tpcb	9.80	299.08
G	10.68	298.20
cb-Tpcb	9.78	299.10
G	10.47	298.41
W-Tpcb	9.65	299.23
G	10.15	298.73
40 = S.L. Thorn = 0+00		
W	9.6	299.3
cb	9.6	299.3
1/4	9.8	299.1
£	9.8	299.1
1/4	9.8	299.1
cb	10.0	298.9

Plotted - 7-3-29 - G.M.I.



π 308.88

34

E	9.8	299.1
0+09		
E	10.1	298.8
cb	10.1	298.8
1/4	10.0	298.9
£	9.6	299.3
1/4	9.9	299.0
cb	9.7	299.2
W	9.6	299.3
T.P.		-12.84 296.04
+0.03		
π 296.07		
0+25		
W	7.7	288.9
cb	7.8	288.3
1/4	10.4	285.7
£	9.5	286.6
1/4	6.9	289.2
cb	5.3	290.8
E	6.4	289.7
0+50		
E	8.4	287.7
cb	12.1	284.0
T.P.		-12.23 283.24
11.80 285.04		

T 285.04

1/4	3.6	2814
¢	9.3	2757
1/4	12.7	2723
cb	17.4	2676
W	17.9	2671

0+53

Next cb line 472nd-Flowline 24" Corr. Iron Culvert

from cb inlet on Thorn 19.0 2660

0+75

W	20.6	2644
+5	20.4	2646
cb-Bottom Water Course	21.6	2634
+4	19.0	2660
1/4	12.7	2723
¢	9.5	2755
1/4	7.5	2775
cb	4.5	2805
E	3.3	2817

1+80

E	9.8	2752
cb	11.0	2740
1/4	13.2	2718
¢	15.4	2696
1/4	18.2	2668
+7	19.0	2660

T 285.04

35

cb - Bottom Water Course	23.0	2620
+6	19.3	2657
W	22.0	2630

1+25

W	22.3	2627
cb	23.1	2619
1/4 - Bottom Water Course	24.0	2610
¢	23.6	2614
1/4 - Bottom Water Course	24.9	2601
cb	24.1	2604
E	20.0	2650

1+50

E - Bottom Water Course	27.0	2580
cb	25.6	2594
1/4	24.6	2604
¢	23.6	2614
1/4	20.5	2645
cb	17.4	2676
W	15.0	2700

1+75

W	9.2	2758
cb	14.0	2710
1/4	18.0	2670
¢	22.3	2627
1/4	24.7	2603

T 2 85.04

cb	26.0	259.0
+8 - Bottom water course	28.4	256.6
E	26.5	258.5
	24.00	.
E	25.5	259.5
cb - Bottom water course	29.0	256.0
1/4	26.1	258.9
£	23.0	262.0
1/4	18.2	266.8
cb	14.0	271.0
W	7.6	277.4
	24.25	
W	8.2	276.8
cb	14.8	270.2
1/4	19.8	265.2
£	25.9	259.1
+8	28.5	256.5
1/4	29.0	256.0
+5 - Bottom water course	29.5	255.5
cb	28.5	256.5
E	26.5	258.5
	24.50	
E	28.0	257.0
cb	29.4	255.6
+6 - Bottom water course	30.4	254.6

36

T 2 85.04

1/4	29.4	255.6
£	25.0	260.0
1/4	19.0	266.0
cb	13.6	271.4
W	7.0	278.0
	24.75	
W	3.3	281.7
T.O.		-0.48 284.56
	11.56	296.12
cb	18.6	277.5
1/4	24.6	271.5
£	29.4	266.7
1/4	36.7	259.4
cb	41.5	254.6
+7 - Bottom water	42.0	254.1
E	41.2	254.9
	34.00	
Out 2.0	42.2	253.9
E	42.0	254.1
cb	35.0	261.1
1/4	28.0	268.1
£	24.0	272.1
1/4	18.5	277.6
cb	13.2	282.9
W	8.0	288.1

T 296.14

3+25

W	6.3	289.8
cb	11.1	285.0
1/4	15.5	280.6
£	21.6	274.5
1/4	27.4	268.7
cb	33.0	263.1
E	38.5	257.6
Out 30	42.0	254.1

T.P. - Nails in fence Post. W.L. 4+25 - 2.51 293.61

+3.32 296.93

3+50

Out 30	15.1	251.8
E	35.2	261.7
cb	29.5	267.4
1/4	25.	271.9
£	20.	276.9
1/4	14.7	282.2
cb	10.8	286.1
W	6.6	290.3

3+75

W	6.0	290.9
cb	8.6	288.3
1/4	11.2	285.7
£	15.0	281.9
1/4	18.0	278.9

T 296.93

37

cb	23.7	273.2
E	28.7	268.2
Out 30	38.7	258.2

4+00

Out 30	34.1	260.8
E	28.0	268.9
cb	23.3	273.6
1/4	19.0	277.9
£	15.3	281.6
1/4	11.7	285.2
cb	8.8	288.1
W	6.2	290.7

4+25

W	6.5	290.4
cb	9.3	287.6
1/4	11.8	285.1
£	15.1	281.5
1/4	18.6	278.3
cb	21.1	275.5
E	27.0	269.9
Out 30	36.6	260.3

4+50

Out 30	36.0	260.9
E	24.2	272.7
cb	20.2	276.7

π 296.93

1/4	17.0	2719
E	14.4	2825
1/4	12.1	2848
CB	9.4	2875
W	6.5	2904
	475	
W	7.2	2897
CB	9.8	2871
1/4	12.4	2845
E	16.0	2809
1/4	18.2	2787
CB	21.0	2759
E	24.0	2729
Out 20	30.5	2669
	5+00	
Out 20	33.0	2639
E	27.1	2698
CB	22.6	2743
1/4	19.6	2773
E	17.1	2798
1/4	14.8	2821
CB	11.9	2850
W	9.4	2875
	5+25	
W	10.8	2861

π 296.93

38

CB		
T.P.		13.02 283.91
	1.81	285.72
1/4	4.6	281.1
E	7.0	278.7
1/4	9.8	275.9
CB	13.2	272.5
E	18.5	267.2
Out 30	27.7	258.0
	5+50	
Out 30	29.0	256.7
E	19.0	266.7
CB	15.0	270.7
1/4	11.7	274.0
E	8.8	276.9
1/4	5.7	280.0
CB	3.4	282.3
W	0.6	285.1
	5+75	
W	1.9	283.8
CB	4.9	280.8
1/4	7.0	287.7
E	9.7	276.0
1/4	12.1	273.6
CB	15.7	270.0

Σ 285.72

E	19.4	266.3
Out 30	29.5	256.2
6+00 = N.L. Redwood		
Out 30	30.5	255.2
E	21.0	264.7
CB	17.6	268.1
1/4	14.1	271.6
E	11.5	274.2
1/4	9.5	276.2
CB	6.4	279.3
W	4.4	281.3

Sa. line Redwood = 0+00

W	12.5	273.2
T.P.	13.05	272.67

+ 0.85 273.52

+11	2.9	271.1
CB	3.9	269.6
1/4	8.6	264.9
E	12.9	260.6
1/4	16.6	256.9
CB	20.0	253.5
E	23.5	248.0
Out 20	30.1	243.1

39

Σ 273.52

0+25

out 12 N.L. Lexington	32.3	241.2
E	30.4	243.1
CB	27.8	245.7
1/4	23.0	250.5
E	18.5	255.0
1/4	13.2	260.3
CB	8.7	264.8
W	3.0	270.5

0+50

W	8.0	265.5
CB	11.8	261.7
1/4	16.0	257.5
E	20.5	253.0
1/4	26.0	247.5
CB = N.L. Lexington	30.1	243.4

0+75

E = N.L. Lexington	26.5	247.0
1/4	19.2	254.3
CB	15.5	258.0
W	12.7	260.8

143 = Intersection N.L. 47rd & N.L. Lexington

W = intersection of Lexington	25.5	248.0
T.P.	4.12	269.40

+ 11.683 281.08

0.07 281.01

T 5 27 1

281.01

TP 12.12 293.13

0.00 293.13

11.44 304.57

4.52 300.05

3.60 303.65

1.38 302.27

8.44 310.71

NE. BR Thornt Van Dyke 2.10 308.61 308.70

correct

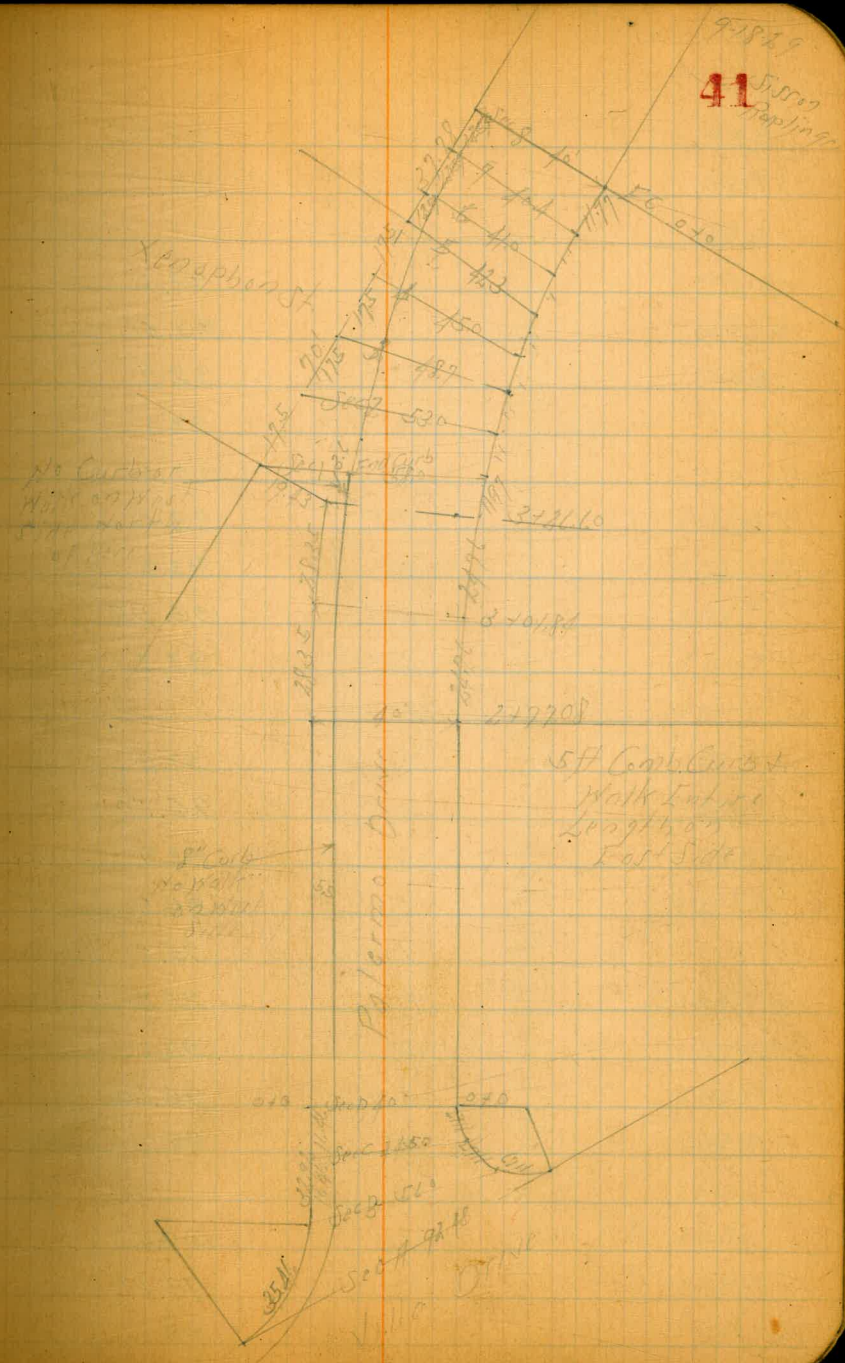
CH 06009

Palermo Drive Cross Section
Villo Drive to Alcott

16' x 40'
55' Cb
735' 6"

41

BM	5.97	102.82	91.35
Sec A			
H		10.2	92.0
+155 - Eushing Cb Top		10.4	92.08
Gutter		10.7	91.6
+41		10.4	91.9
+55		10.4	91.9
+80 - Gutter		10.2	92.0
Cb Top		9.6	92.68
+92.45 = 1		9.4	92.9
Sec B			
E		9.6	92.7
+85 - Eushing Cb		9.7	92.60
Gutter		10.1	91.9
+35		10.1	91.9
+40		10.5	91.8
+50 - Gutter		10.6	91.7
Cb Top		10.0	92.32
+110 - H		10.3	92.0
Sec C			
H		9.7	92.6
+55 - Cb Top		9.8	92.51
Gutter		10.3	92.0
+20		10.2	92.1
+35 - Gutter		10.2	92.3



Palermo Dr

10232

Cb Top	90	92.65
1445-F	91	92.7
	Sec D. FC on F	
F	87	93.6
Cb Top	88	93.51
Gutter	91	92.9
"	92	93.1
L	93	93.0
"	93	93.0
Gutter	95	92.8
Cb Top	877	93.55
"	86	93.7
	15' N of FC	
"	5.3	97.0
Cb Top	5.82	96.50
Gutter	6.4	95.9
"	6.3	96.0
L	16	95.7
"	15	95.8
Gutter	67	96.1
Cb Top	876	96.60
F	5.7	96.6
	50'	
F	32	100.0
Cb Top	271	99.61
Gutter	32	99.1

10322

42

"		3.5	98.8	
L		3.5	98.8	
"		3.3	99.0	
Gutter		3.3	99.0	
Cb Top		2.80	99.52	
"		2.5	99.8	
TF	1242	11401	0.74	10158
		75'		
"		11.6	102.4	
Cb Top		11.50	102.54	
Gutter		13.1	101.9	
"		12.3	101.7	
L		12.5	101.5	
"		12.3	101.8	
Gutter		12.0	102.0	
Cb Top		11.50	102.54	
F		11.1	101.2	
		100'		
F		8.3	105.7	
Cb Top		8.51	105.53	
Gutter		9.1	104.9	
"		9.3	104.8	
L		9.6	104.4	
"		9.1	104.6	
Gutter		9.0	105.0	
Cb Top		8.50	105.54	

114.04

H	8.2	105.8
	125.11	
H	5.7	108.3
cb Top	5.81	108.23
Gutter	6.3	107.7
H	6.6	107.4
H	6.8	107.2
H	6.5	107.4
Gutter	6.8	107.8
cb Top	5.78	108.26
F	5.3	108.7
	150.11	
F	3.2	110.8
cb Top	3.47	110.57
Gutter	4.2	109.8
H	4.2	109.8
H	4.5	109.5
H	4.2	109.8
Gutter	4.0	110.0
cb Top	3.18	110.56
H	2.9	110.1
	175.11	
H	2.0	112.0
cb Top	1.58	112.46
Gutter	2.1	111.9
H	2.1	111.6

114.04

43

H		2.6	111.4	
H		2.3	111.7	
Gutter		2.2	111.8	
cb Top		1.52	112.52	
F		1.3	112.7	
H	12.48	121.39	0.12	113.91
	200.11			
F		12.0	114.4	
cb Top		12.28	114.11	
Gutter		12.7	113.7	
H		13.0	113.4	
H		13.3	113.1	
H		13.0	113.4	
Gutter		13.2	113.6	
cb Top		12.27	114.11	
H		12.4	114.0	
	205.11			
H		10.8	115.6	
cb Top		10.62	115.70	
Gutter		11.2	115.1	
H		11.2	115.1	
H		11.6	114.8	
H		11.4	115.0	
Gutter		11.3	115.1	
cb Top		10.65	115.74	
F		10.3	116.1	

12139

+20	36	122.8
+33	36	122.8
+475-Gutter	28	123.6
Cb Top	221	124.13
+530-F	20	124.4
	Spec 3	18.7
F	15	124.9
+55-Cb Top	110	124.79
Gutter	20	124.4
+15	27	123.7
+22	28	123.6
+30	26	123.8
+45-W	24	124.0
	Spec 4	45.0
H	12	125.0
+5	11	125.3
+9	20	124.4
+30	22	124.2
+395-Gutter	16	124.8
Cb Top	108	125.31
+45-F	00	125.5
	Spec 5	41.3
F	04	126.0
+55-Cb Top	046	125.93
Gutter	11	125.3
+20	15	124.9

12139

45

+25	1.3	125.1
+29	0.3	126.1
+124-W	0.1	126.3
TP	6.77	132.75
	Spec 6	125.98
H	2.0	126.7
+19	7.0	125.7
+21	7.3	125.4
+355-Gutter	7.0	125.7
Cb Top	630	126.45
+410-F	4.3	126.4
	Spec 7	40.7
F	5.8	126.9
+55-Cb Top	532	126.93
Gutter	64	126.3
+11	7.0	125.8
+34	6.6	126.1
+704-W	5.8	127.0
	Spec 8 - TC. 2040	41.0
H	5.7	127.0
Cb	6.1	126.6
H	6.5	126.2
L	6.6	126.1
H	6.5	126.2
Gutter	6.8	126.5
Cb Top	545	127.30

F	53	127.4
	25% of FC	
F	47	128.0
Cb Top	49	127.84
Gutter	56	127.1
1/4	58	126.9
2	60	126.7
1/4	58	126.9
Cb	58	126.9
H	49	127.8
	50% of FC	
H	46	128.1
Cb	54	127.3
1/4	56	127.1
2	56	127.1
1/4	54	127.3
Gutter	53	127.4
Cb Top	46	128.15
F	45	128.2
	75%	
F	44	127.3
Cb	44	128.29
Gutter	50	127.7
1/4	53	127.4
2	51	127.3
1/4	54	127.3

Cb	54	127.3
H	45	128.2
	100%	
H	45	128.2
Cb	50	127.7
1/4	51	127.6
2	52	127.5
1/4	51	127.6
Gutter	48	127.9
Cb Top	43.5	128.40
F	47	128.6
	125%	
F	47	128.6
Cb Top	42.6	128.49
Gutter	50	127.7
1/4	50	127.7
2	51	127.6
1/4	50	127.7
Cb	47	128.0
H	43	128.4
	122.22 = Opp of 100% and	
H	42	128.5
Cb	49	127.8
1/4	49	127.8
2	50	127.7
1/4	48	127.9

13275

Gutter	47	128.0
cb Top	49	128.66
F	38	128.8

17928'N

F	40	128.7
cb Top	399	128.76
Gutter	46	128.1
W	46	128.1
S	56	127.7
W	47	128.0
cb	46	128.1
W	43	128.4

19722'N

W	42	128.5
cb	46	128.1
W	47	128.0
S	49	127.8
W	47	128.0
Gutter	45	128.2
cb Top	394	128.81
F	39	128.8

21472

F	37	129.0
cb Top	376	128.99
Gutter	43	128.4
W	44	128.3

13275

47

S	46	128.1
W	45	128.2
cb	48	128.5
W	42	128.5

23221'N Opp. Hb. Young on W

W	37	129.0
cb	40	128.7
W	41	128.6
S	41	128.4
W	40	128.7
Gutter	40	128.7
cb Top	345	129.30
F	35	129.2

25722'N

F	26	130.1
cb Top	269	130.06
Gutter	33	129.4
W	33	129.4
S	34	129.3
W	33	129.4
cb	38	129.5
W	30	129.7

28222'N

W	19	130.8
cb	34	130.3
W	24	130.3

2	26	130.1
1/4	24	130.3
Gutter	23	130.4
Cb Top	168	131.07
L	15	131.2

307227

L	0.3	132.4
Cb Top	0.41	132.29
Gutter	11	131.6
1/4	12	131.5
2	13	131.4
1/4	12	131.5
Cb	12	131.5
N	0.4	132.3

TP 127° 14524 0.21 132.57

332227

N	117	133.5
Cb	125	132.7
1/4	121	132.8
L	125	132.7
1/4	123	132.9
Gutter	123	132.9
Cb Top	1158	133.66
L	114	133.8

357077 - PC 40P 2010 on I

95 135.7

Cb Top	995	135.29
Gutter	104	134.8
1/4	106	134.6
L	110	134.2
1/4	108	134.4
Cb	109	134.3
N	102	135.0

38227

N	78	137.4
Cb	85	136.7
1/4	86	136.6
L	86	136.6
1/4	82	136.9
Cb	78	137.4
L	71	137.8

40227

L	48	140.4
Cb	52	139.9
1/4	57	139.5
L	58	139.4
1/4	58	139.4
Cb	58	139.4
N	49	140.3
BN	203	143.21

4322677 - SL 2010 on I

N 20 143.2

Top Hyd
Mid Palermo
Sub of 2010

145.84

cb	28	142.4
1/4	27	142.5
2	28	142.4
1/4	28	142.4
cb	26	142.6
F	25	142.7

TP	1243	15760	0.07	145.17
----	------	-------	------	--------

44972 H

F	132	144.4
cb	133	144.3
1/4	131	144.5
2	130	144.6
1/4	132	144.4
cb	133	144.3
H	122	145.4

46720 H

H	105	147.1
cb	113	146.3
1/4	110	146.6
2	110	146.6
1/4	113	146.3
cb	115	146.1
F	118	145.8

48472 H

F	96	148.0
-1.5 - Kristoffel	96.1	147.96

157.60

Gutter	10.3	147.3
cb	99	147.7
1/4	95	148.1
2	93	148.3
1/4	94	148.2
cb	96	148.0
H	85	149.1

50272 H - Zola on H

H	69	150.7
cb	78	149.8
1/4	75	150.1
2	73	150.3
1/4	76	150.0
Gutter	80	149.6
cb Top	78	150.32
F	72	150.4

51972 H - FC Zola on F

F	60	151.6
cb Top	60.9	151.51
Gutter	69	150.7
1/4	66	151.0
2	63	151.3
1/4	67	150.9
cb	70	150.6
H	59	151.7

53781 H

Palermo Dr.

15760

N	42	153.4
Cb	45	
1/4	39	
2'	36	154.0
1/4	39	
Gutter	42	
Cb Top	3.33	154.27
E	31	

56490'N

E	1.7	
Cb Top	1.84	155.76
Gutter	2.0	
1/4	2.0	
2'	2.2	155.4
1/4	2.2	
Cb	2.3	
N	2.4	155.2

59198'N

N	2.0	155.6
Cb	2.4	
1/4	1.8	
2'	1.6	156.0
1/4	1.1	
Gutter	1.9	
Cb Top	1.26	156.34
E	1.2	

157.60

50

619.07'N - PC 00E R-127.33

E	1.2	
Cb Top	1.30	156.30
Gutter	2.0	
1/4	1.5	
2'	1.4	156.2
1/4	1.7	
Cb	2.1	
N	2.1	155.0
1.5	2.3	

626.79'N

-1.5	1.3	
N	2.5	155.1
Cb	1.7	
1/4	2.1	
2'	1.4	156.2
1/4	1.3	
Cb	1.7	

636.42'N

Cb Fickling	1.38	156.22
E	1.3	
624.51'N		
E	1.7	155.9
Cb	1.4	
1/4	1.6	
2'	2.1	155.5

15760

1/4	19	
cb	22	
M	3.5	154.1
+15	9.3	
70222N = SL 17/col on road		
-15	15.0	
M	10.4	147.2
cb	7.2	
1/4	3.0	
1/2	2.2	155.4
1/4	2.1	
cb	2.3	
E	1.9	155.7
719.72		
E	2.6	155.0
cb	2.6	
1/4	2.2	
1/2	3.6	154.4
+5	3.5	
1/4	4.6	
cb	10.7	
M	11.9	145.7
+25	19.3	
73722N = 2 17/col on M		
-25	21.4	
M	13.8	143.8

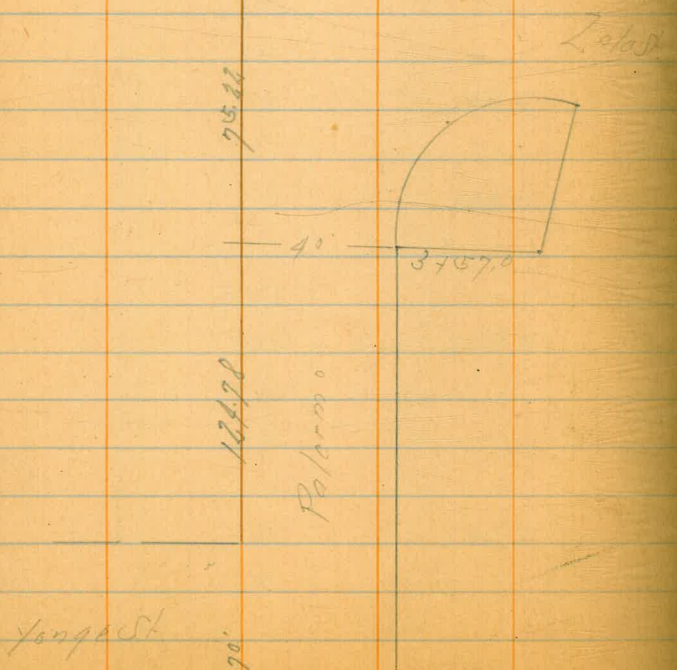
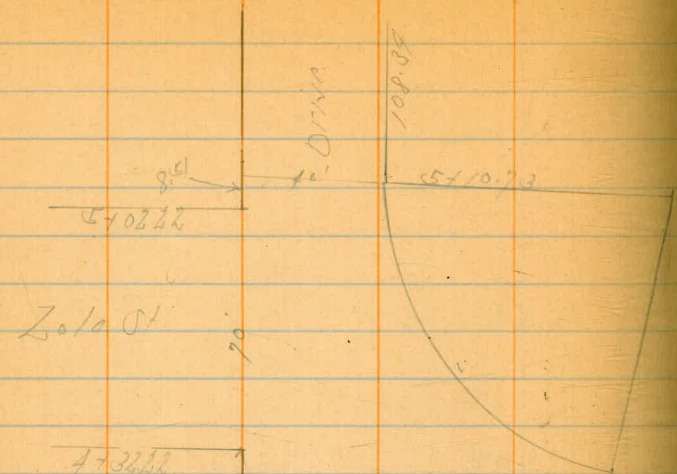
15760

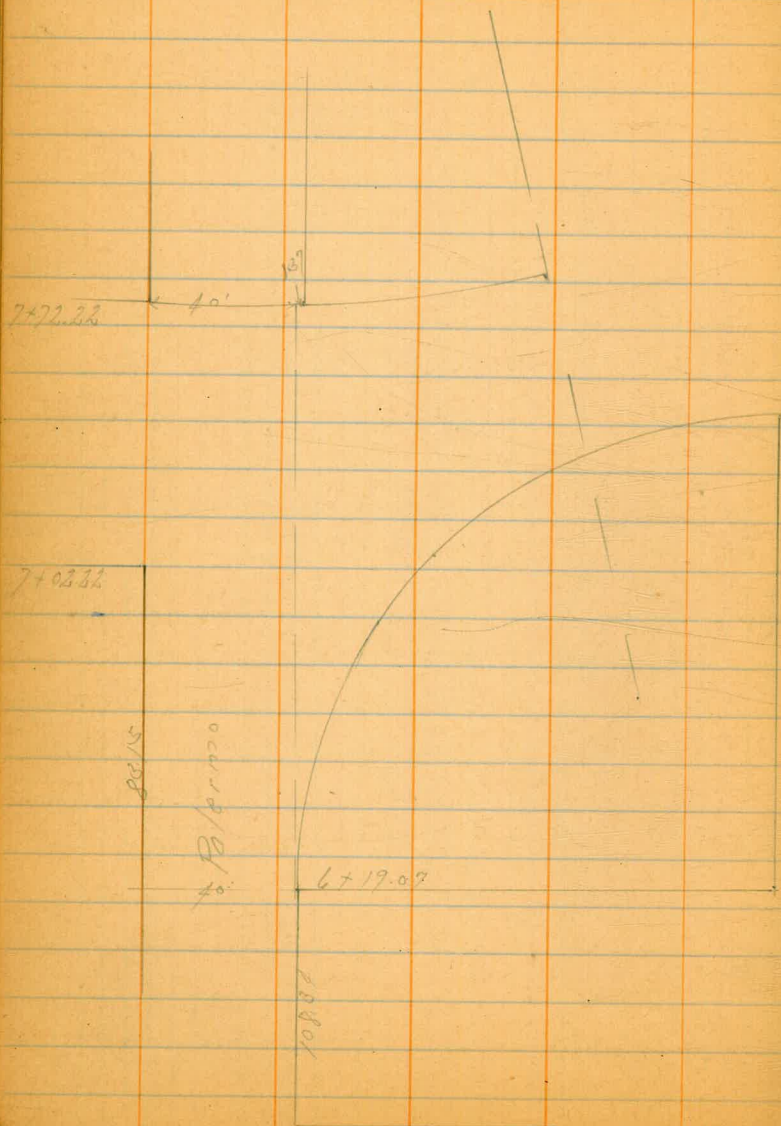
51

cb	10.7	
1/4	8.4	
5	6.3	151.3
1/4	3.6	
cb	2.1	
E	2.2	155.4
75422N		
E	3.5	154.1
cb	1.9	
1/4	8.1	
5	10.7	146.9
1/4	12.5	
cb	16.2	
M	17.9	139.7
+25	23.4	
77222 = 17.6 17/col on M		
-15	24.5	
M	30.3	137.3
cb	18.0	
1/4	15.1	
5	11.6	146.0
1/4	8.8	
cb	6.0	
E	5.7	151.9
B.M.	5.48	152.12

St. Prothas
Palermo
17/col

Palermo Dr.

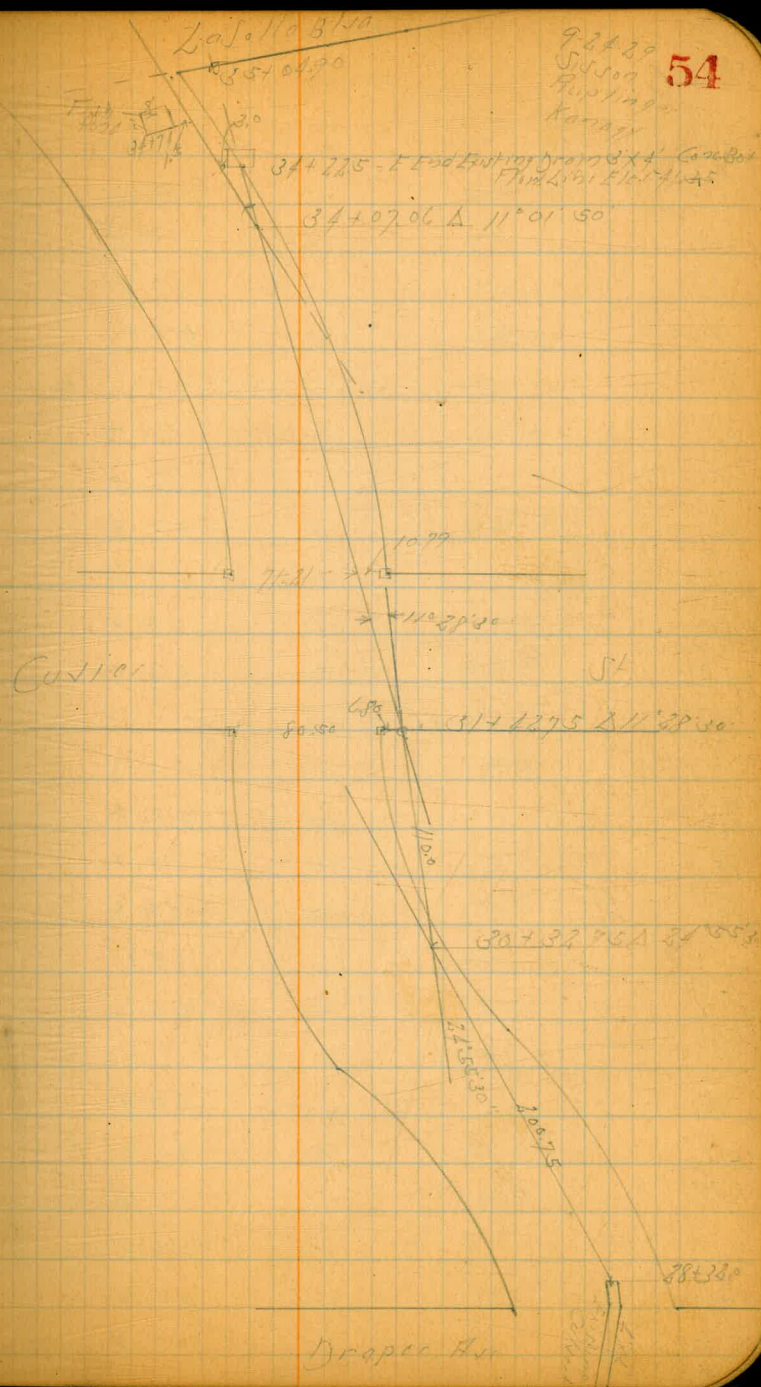




Proposed Ravine St
Starks Drain

BM	341	80.10	76.49	NEBP
TP	422	71.99	1233	17.77
				18+82 = West End of f.H. Existing Culvert
18' N of		1.3	70.7	
20' E of West End of Culvert		12.42	59.57	
16.5		1.2	70.8	
	19+50			
21.5		2.3	69.7	
7.5		10.7	61.3	
8		11.3	60.7	
7.11		11.0	61.0	
23.11		0.7	71.3	
	19+0			
26.11		5.5	66.5	
11.11		11.7	60.3	
2		13.3	53.7	
8.5		11.2	60.8	
20.5		4.5	67.5	
	19+56			
25.5		4.0	68.0	
12.5		12.0	60.0	
2		13.3	58.7	
17.11		12.0	59.0	
21.11		5.0	66.0	

31+0



7197

29H		65	65.5
17H		131	58.6
8		145	57.5
10S		143	57.7
25S		30	69.0

30+3275 A.P. 29°55'30"

18S		33	68.7	
7P	124	6643	680	1519
2		91	57.3	
12H		118	54.6	
18H		80	58.4	
35N		33	63.1	

30+50

37H		38	62.6
22H		92	57.2
15H		117	54.7
2		98	56.6
11S		83	58.1
21S		02	66.2

31+0

25S		26	63.8
21S		50	61.4
1S		85	57.9
2		196	55.8
28H		160	52.4
33H		40	64.4

6613

55

31+25

24H		27	63.7
13H		160	50.0
24		158	50.6
2		124	53.0
12S		110	55.4
25S		12	65.2

31+4325 A.L. 11°58'30"

29S		31	63.3
15S		119	54.5
81		170	49.4
2		156	50.8
5H		117	51.7
20H		21	64.3

31+65

15H		84	63.0
7H		141	52.0
2		166	49.8
7S		196	48.8
12S		14	60.0

31+91

8S		82	58.2
250 - Top Billon		27	58.7
150 - Middle Billon			
2		110	50.4
7		180	48.4

Boath/100
210.0

66.43

13' N	20	CapofBuckN	10.0	56.4
16' N	20			63.4
			32+85 ✓	
10' N	22			59.2
11' N	28.4			48.0
12' N	17.1			49.3
TP	2.46	6.27	7.62	58.81
21' S			4.3	57.0
			32+50 ✓	
27' S			5.8	56.0
28' S			12.9	48.6
12' N			11.8	48.5
22' S			5.8	56.1
			32+75 ✓	
23' N			2.1	58.7
21' N			7.6	51.7
28' S			15.6	45.7
1' S			15.6	45.7
25' S			11.5	49.8
27' S			3.6	57.7
			33+0 ✓	
28' S			3.2	58.1
4' S			11.0	45.3
28' N			1.1	46.9
2' N			4.8	56.5
3' TP	5.48	57.56	9.19	52.8

2.5 of 33.17
 as Bick by
 1.27.17

57.56

9-30-29

56

			33+85 ✓	
17' N			3.0	54.6
16' N			9.7	47.9
2' N			12.2	44.4
2' S			10.9	46.7
10' S			9.2	48.4
20' S			1.6	56.0
			33+50 ✓	
20' S			3.0	54.6
13' S			10.2	47.4
2' S			11.5	46.1
1' N			12.5	44.1
17' S			9.0	48.6
10' S			0.0	57.6
			33+75 ✓	
17' S			3.3	54.3
27' S			16.1	45.5
2' S			16.2	44.8
15' S			9.8	47.8
22' S			3.2	54.3
			3410206 AL 11° 01' 50" ✓	
20' S			2.8	54.8
12' S			5.8	51.8
2' S			14.7	42.9
25' N			4.9	52.7
			34111	

35.1	34114	57.56	81	49.5
11.1			10.8	46.8
2			15.7	41.9
10.5			3.7	53.9
15.5			0.3	57.3
	✓ 341225 = End of Ex. No. 311 Pangea Col. v. 1			
11.5			0.0	57.6
2			9.0	48.6
5.1	2. Freshing Drain		16.21	41.35
12.11	Flashed		12.6	45.0
15.11			9.0	48.6
26.1			7.9	49.7
	34140 ✓			
21.1			3.0	54.6
17.1			6.3	51.3
TP	10.43	75.93	20.6	55.50
2			7.8	58.9
10.5			4.7	61.2
20.5			4.7	61.2
	34171			
15.5			5.3	60.6
2			5.4	60.6
15.1			5.8	60.6
	35104.20 = 11. 10/10 3rd > /			
15.11			5.9	60.0
2			5.9	60.0
15.5			7.0	59.9

57

		65.93		
TP	2.57	63.65	67.0	60.13
TP	4.7	67.24	0.96	63.19
21.1			2.23	65.03
	2.23	67.29		65.01
21.1			4.57	63.22

NEBP
Pangea Col. v. 1
65.06

SNTT
Lafayette
& Province

X-Section Alley - Bl. 26 - Teralta
 betw. 41st & Marlborough from El Cajon
 Blvd. - Orange.

STA	+	H.I.	-	Elev.
B.M. SW. B.P. El Cajon & 41st				364.42
	4.97	369.39	*	
SE. Gutter El Cajon & 41st			5.33	
SW. " " & Alley			5.11	
SE " " "			5.03	
SW " " & Marlborough			4.72	
	0+00	S.L. El Cajon		
W. Curb Top			4.40	
✓ Bolt			4.56	
⊕		Paved	4.82	
E. Curb Bolt			4.53	
✓ Top			4.37	
	0+19	70		
Top Manhole			4.99	
Flow line 6" Sewer			10.64	
	0+23			
8-R Top W.S.			4.71	
	0+32			
EL			5.2	
⊕			5.0	
W.L.			5.1	
+ 4'			5.1	

Jaeger, Charvert, } Dec. 19th 1929
 Bailey, Morgan }

58

STA	+	H.I.	-	Elev.
				0+34
G-E W.S.			5.2	
				0+35
G-E W.S.			5.25	
				0+50
EL			5.3	
⊕			5.3	
W.L.			5.3	
+ 5			5.5	
				0+57
G-W W.S.			5.4	
				0+66
+ 10' Conc. Floor			4.72	Garage on West
W.L.			5.4	
⊕			5.4	
E.L.			5.0	
				0+75
G-R W.S.			5.41	
				0+87
G-L W.S.			5.25	
				1+00
EL			5.0	
⊕			5.4	
W.L.			5.3	

Sta	+	H.I.	-	Elev.
	1+14			Garage on West
+10'			4.98	Conc. Floor
			5.2	W.L.
			5.1	☐
			4.7	E.L.
	1+23			Garage on West
			4.9	E.L.
			5.1	☐
			5.2	W.L.
+9.5			5.2	Dirt Floor
	1+28			
7.5-W			4.93	W.L.
			5.28	T.P.
		368.83		
	1+41			
5.5-E			4.91	W.S.
	1+42 ⁵³			
7-W			4.53	W.S.
	1+51			Garage on West
+9.5			4.53	Conc. Floor
			4.7	W.L.
			4.9	☐
			4.6	E.L.

Sta	+	H.I.	-	Elev.
	1+65			Garage on West
			5.0	E.L.
			5.0	☐
			4.9	W.L.
+8'			4.67	Apron N. } 10' Long
			4.68	" S. }
+12'			4.46	☐ Conc. Floor
	1+71			
7-E			5.16	Water Service
	1+85			
8-W			4.95	W.S.
	1+97			Garage on West
+11.5			4.46	☐ Conc. Floor
+7.5			4.85	Apron N. } 10' Long
			4.82	" S. }
			5.1	W.L.
			5.3	☐
			5.3	E.L.
	2+12			Garage on West
			5.3	E.L.
+6.5			5.35	W.S.
			5.3	☐
			5.2	W.L.
+3'			5.0	Dirt Floor

Sta	+	H.I.	-	Elev.
	2+73			Garage on East
W.L.			4.6	
☐			4.8	
E.L.			4.9	
+7' ☐ Conc. Floor			4.58	
	2+33			
8-W W.S.			4.45	
	2+40			
7-E W.S.			4.67	
	2+49			Garage on East
+6.5' ☐ Conc. Floor			4.62	
+1.5' Con. Apron N.			4.81	
✓ S. 15' wide			4.71	
E.L.			4.8	
☐			4.7	
W.L.			4.7	
+3'			4.6	
	2+75			
W.L.			4.97	
6-W W.S.			5.0	
☐			4.7	
E.L.			4.7	
	2+85			
7-E W.S.			4.81	

Sta	+	H.I.	-	Elev.
	3+00			Garage on East
+10.5' Dirt Floor			5.0	
E.L.			5.0	
☐			5.2	
W.L.			4.5	
	3+14			Garage on East
W.L.			5.2	
☐			5.2	
E.L.			5.4	
+9.5' Conc. Floor			5.09	
T.P.			5.33	363.50
	5.10	368.60	*	
	3+25			
7-W W.S.			5.4	
	3+29 ⁷⁰			
☐ M.H. Top			5.56	
✓ F.W.			11.39	
	3+31			
8-E W.S.			5.38	
	3+34 ⁵⁰			
8-E W.S.			5.41	
	3+50			Garage on East
+9.0' ☐ conc. Floor			4.65	
E.L.			5.2	
☐			5.1	

Sta	+ H.I.	- Elev.
W.L.		5.4
	3+75	
W.L.		4.7
☐		5.4
E.L.		5.5
	3+90 ⁵⁰	
7.5-W W.S.		5.04
	4+22	
7.0'E W.S.		5.29
	4+23 Garage on West	
E.L.		5.3
☐		5.2
W.L.		5.1
+10.5' ☐ Conc. Floor		4.78
	4+31 ⁵⁰	
7.5-W W.S.		5.4
	4+37 ⁵⁰	
7.5 W. W.S.		4.87
	4+49 Garage on West	
+11' ☐ Conc. Floor		4.83
W.L.		5.1
☐		5.1
E.L.		5.1

61

Sta	+ H.I.	- Elev.
	4+75 ☐ of 3 Garage on West	
E.L.		5.0
S.S.-E W.S.		5.22
☐		4.8
W.L.		5.0
+0.5' 3" Apron South E.		5.10
	✓ North E.	5.16
+3.5' ☐ Conc. Floor		5.16
	5+15 Garage on West	
+4.0' ☐ Conc. Floor		5.30
+1.5'-8' Apron S.E.		5.41
	✓ N.E.	5.38
W.L.		5.4
☐		5.0
	5+17 Double Garage on East	
☐		5.0
E.L.		5.2
+4' ☐ Conc. Floor		5.02
	5+50	
E.L.		5.0
☐		5.0
W.L.		5.6
	5+51	
7-W W.S.		5.28

Sta		H.I.	-	Elv.
	5+57 ⁵⁰			
7-W	W.S.			5.28
	5+54			
7-W	W.S.			5.28
	T.P.			4.74
	2.44	366.30	+	363.86
	5+77			
W.L.				2.9
¢				2.7
G-E	W.S.			2.9
E.L.				2.9
	6+07	N.L.	Orange	
E.L.	Top Curb			3.53
¢				3.1
W.L.	"	"		3.6
	6+21	N.Curb	Orange	
NE.	Gutter Orange	& 41 ⁵		4.45
NW.	"	" & Alley		4.53
¢				3.8
NE	"	"		4.51
NW	"	" & Marlbor.		4.04
	T.P.			3.59
	6.08	368.79		364.71
SW. B.P.	El Cajon & Marlborough	365.14	3.6W	365.17

FL. Corrugated Culvert
 " " "

33rd St. Recross Section

Juniper to 70' of N.L. Kalmia Sea Sketch by Page 67

26676

4-25-20
D.V. 20
S.C. 20
H.P. 20
O.S. 20
S.H. 20
63
264.8

Note: - East Line 21' E of E.C. Entire Length

BM	0.74	278.81	278.12	34' BP Top NW
				Juniper to 35'
				150' of N.L. Juniper
21' N of E.L. - Existing Cb		11.32	267.54	
E.L.		11.2	267.7	
		17.5' N		
10' E of E.L. - Top Slope		14.4	264.4	
E.L.		12.3	266.5	
5' N of E.L.		11.8	267.0	
31' N of E.L. - Existing Cb		12.00	266.86	
TP	0.21	266.76	12.31	266.55
		200' N		
21' N of E.L. - Cb		0.51	266.20	
E.L.		0.1	266.1	
6' E of E.L. - Top		3.2	263.5	
		22.5' N		
8' E of E.L. - Top		6.2	260.5	
E.L.		1.0	265.7	
31' N of E.L. - Cb		1.86	265.50	
		24.6' N		
Cb		1.79	264.97	
E.L.		1.7	265.0	
2' E of E.L.		2.3	264.4	
10' E of E.L.		7.7	258.8	
		25.0' N - End of stalk on F		
10' E of E.L.		8.1	258.6	

E.L.		1.9	
21' N of E.L. - Cb		1.90	264.86
		25.9' N	
21' N of E.L. - Cb		2.15	264.61
E.L.		2.6	264.1
13' E of E.L. - Top		9.7	257.0
		26.5' N	
13' E of E.L. - Top		10.4	256.3
5' E of E.L. - Top		5.8	261.5
E.L.		3.0	263.7
31' N of E.L.		2.1	264.6
21' N of E.L. - Cb		2.29	264.47
		27.5' N	
Cb		2.54	264.20
6' N of E.L.		3.1	263.6
E.L.		6.1	260.6
6' E of E.L.		9.4	257.3
15' E of E.L.		11.9	254.8
		29.5' N	Trail 13.5' Under
18' E of E.L.		17.2	249.5
9' E of E.L.		13.8	252.9
E.L.		9.3	257.4
7' N of E.L.		5.7	261.0
15' N of E.L.		3.2	263.5
21' N of E.L. - Cb		2.88	263.88
		29.1' N	

33rd St.

26676

21' N of EL - Cb	3.09	263.67
15' N " "	3.3	263.4
7' N " "	8.1	258.6
EL	11.8	254.9
8' E of EL	16.2	250.5
14' E " " = Top	19.2	247.5
300' N of SL Kalmia		
22' E of EL = Top	25.2	241.5
14' E " "	22.5	244.2
7' E " "	19.3	247.4
EL	15.1	251.6
8' N of EL	9.7	257.0
15' N " "	3.6	263.1
21' N " " = Cb	3.27	263.48
5' N of SL Kalmia		
21' N of EL - Cb	3.36	263.40
15' N of EL	3.5	263.2
9' N " "	9.0	257.7
EL	15.6	251.1
8' E of EL	20.8	245.9
16' E " "	24.5	242.2
28' E " "	29.1	237.6
15' N of SL Kalmia		
22' E of EL	26.9	239.8
11' E " "	21.0	244.7
EL	15.8	250.9

26676

64

11' N of EL	8.3	258.4
16' N " "	3.6	263.1
21' N " " = Cb	3.38	263.38
20' N of SL Kalmia		
21' N of EL - Cb	3.40	263.36
17' N " "	3.6	263.1
10' N " "	9.0	257.7
EL	15.3	251.4
22' E of EL = Top	16.1	250.6
25' N of SL Kalmia		
EL	13.2	253.5
8' N of EL	11.3	255.4
11' N " "	8.5	258.2
17' N " "	8.7	264.0
21' N " " = Cb	3.41	263.32
35' N of SL Kalmia		
21' N of EL - Cb	3.47	263.29
17' N " "	3.6	263.1
9' N " " = Top	8.7	258.0
43' N		
EL = Top	13.1	253.6
8' N of EL	8.5	258.2
16' N " "	3.6	263.1
21' N " " = Cb	3.50	263.26
45' N		
21' N of EL - Cb	3.50	263.26

16' N of EL	3.6	263.1
8 " " "	8.9	257.9
EL	12.9	253.8
8 E of EL	16.9	249.8
50' N of S.L. Kalmia		
5 E of EL	17.0	249.7
EL	14.4	252.3
8 W of EL	8.4	258.3
15 W " " "	3.6	263.1
31 W " " " - Cb	3.48	263.28
55' N		
31 W of EL = Cb	3.47	263.29
15 W " " "	3.5	263.2
8 W " " "	9.4	257.3
EL	14.8	251.9
8 E of EL = Toe	19.2	247.5
70' N of N.L. Kalmia		
25 E of EL = Toe	29.0	237.7 Note:
20 E " " "	27.3	239.4 East Line of 33rd
10 E " " "	21.8	244.9 N of Kalmia
EL	14.5	252.2 1/2 produced from South
8 W of EL	8.7	258.0
14 W " " "	3.8	262.9
31 W " " " = Cb	3.42	263.34
3' N of N.L. Kalmia		
31 W of EL = Cb	3.44	263.32

14 W of EL	3.6	263.1
16 W of EL = old East Line As Cracked	6.4	260.3
EL	14.5	252.2
8 E of EL	21.2	245.5
20 E of EL = Toe	27.7	239.0
10' N of N.L. Kalmia		
20 E of EL = Toe	26.4	240.3
8 E " " "	20.5	246.2
EL	13.7	253.0
18 W of EL	6.8	259.9
14 W " " "	3.4	263.3
31 W " " " = Cb	3.38	263.38
17' N of N.L. Kalmia		
31 W of EL = Cb	3.29	263.47
14 W " " "	3.3	263.4
16 W " " "	6.5	260.2
EL	13.4	253.3
8 E of EL	19.0	247.7
13 E " " "	21.7	245.0
17 E " " "	25.0	241.7
23' N of N.L. Kalmia		
16 E of EL	22.2	244.5
8 E " " "	17.5	249.2
EL	13.2	254.5
5 W of EL	10.0	256.7
10 W " " "	6.5	260.2

33rd St.

266.76

15 N of EL	2.9	263.8
21 N " " = Cb	3.08	263.68
26 N		
21 N of EL - Cb	3.00	263.76
14 N " " "	2.7	264.0
10 N " " "	6.2	260.5
EL	11.8	254.9
8' E of EL	16.9	249.8
15' E " " = Top	21.0	245.7

33 N

13 E of EL	18.8	247.9
9' E " " "	14.4	252.3
EL	10.8	255.9
7' N of EL	7.5	259.2
10 N " " "	5.3	261.4
14 N " " "	2.3	264.4
21 N " " = Cb	2.90	263.96

37 N

21 N of EL - Cb	2.2	264.14
13 N " " "	2.3	264.4
10 N " " "	4.5	262.2
EL	9.4	257.3
11' E of EL	16.7	250.0

40 N

10' E of EL	15.9	251.8
EL	9.0	257.7

266.76

66

10 N of EL	4.0	262.7
13 N " " "	2.1	264.6
21 N " " = Cb	2.42	264.34
47 N		
21 N of EL - Cb	2.00	264.76
10 N " " "	1.6	265.1
9' N " " "	1.6	265.1
EL	7.7	259.0
8' E of EL - Top	12.5	254.2

55 N

4' E of EL	10.3	256.4
EL	7.7	259.0
3' N of EL	5.5	261.2
16 N " " "	1.1	265.6
21 N " " = Cb	1.46	265.30

60 N

21 N of EL - Cb	1.16	265.60
10 N " " "	0.9	265.8
EL - Top	7.7	259.0

70 N

10 N of EL - Top	0.5	266.3
21 N of EL - Cb	0.53	266.23

Walker
Bliss
Drebert
4-17-31

ROSS SECTION 20' Alley
Blk. 356 - Univ. Heights
Between Georgia and Florida.
From N.L. Robinson Ave to 26th Univ. Ave.
Sketch Page 69 for tie points

1.28 313.27 311.29 ^{NLRP} Robinson Georgia
T.P. #1 3.40 303.81 12.86 300.41
N.C.B. Line Robinson Ave = 14' South of N.L.

N top cb.	8.05	95.76	✓
" " Paring	8.73	95.08	✓
L "	9.25	93.86	✓
E "	11.21	92.60	✓
E top cb.	10.74	93.07	✓

N.L. Robinson Ave = 0+00

E top cb.	10.34	93.47	✓
" " Paring	10.41	93.40	✓
L "	9.54	94.27	✓
N "	8.12	95.69	✓
" top cb.	7.94	95.87	✓

0+05

N	3.2	300.6
+5	7.0	96.8
L	7.6	96.2
+9'	6.3	97.5
E	4.6	99.2
+1	3.4	00.4
+5	3.7	00.1

Plotted 4-21-31

0+25

303.81

68

-5'	1.1	02.7
-1'	0.7	03.1
E	1.6	02.2
L	2.8	01.0
+8	1.8	02.0
N	0.1	03.7
+3	7.0	06.8
+5 ²	7.2	07.2
T.P. 12.70	316.10	09.1
		303.40
	0+40	
-5'	9.2	06.9
N	11.3	04.8
+3	13.1	03.0
L	13.2	01.9
+8	12.9	03.2
E	10.1	06.0
+5	12.2	03.9
	0+50	
-5'	8.4	07.7
E	8.2	07.9
+2	8.4	07.7
+2.5'	11.5	04.6
L	11.9	04.2
+9'	11.7	04.4
N	10.9	05.2
+5	9.2	06.9

ROSS SECTION 20' ALLEY

316.10

0+65

-5'	8.0	08.1
W	8.9	07.2
+2'	10.1	06.0
L	10.3	05.8
+8'	10.2	05.9
E	8.8	07.3
+5'	8.8	07.3

0+90

-5'	7.3	08.8
E	7.0	09.1
L	6.9	09.2
W	6.4	09.2
+5'	5.8	10.3

1+10

-5'	3.7	12.4
W	4.2	11.9
L	5.1	11.0
E	5.8	10.3
+5'	6.1	10.0

1+25

12'	5.9	10.8
E	3.7	12.4
L	2.7	13.4
W	1.8	14.3
+5'	1.3	14.8

316.11
316.10

70

49
TP 120332802
328.03 0.11315.99
316.00

1+50

-5'	7.9	20.1
W	9.3	18.7
L	11.1	16.9
E	12.4	15.6

+15' $R = 14.8$ 13.2
 $R = 9.0$ 31.0
 1+51 = beginning board fence on West 1' back. ✓

1+70

-15'	11.6	16.4
-4'	10.6	17.4
E	9.4	18.6
+5'	9.0	19.0
L	7.3	20.7
W	5.8	22.2
10.9' - fence on ground	5.0	23.0

1+80

-10' = fence	3.3	24.7
W	3.6	24.4
+8'	4.4	23.6
L	4.9	23.1
E	7.2	20.8
+15'	10.8	17.2

TP 1244

340.13 0.34

327.69

3 Nails in Pole
on West side of Pole
Station 1+82

2+00

-15'	18.9	21.2
------	------	------

340.13

E	340.12	14.5	25.6	
L		11.6	28.5	
N		10.2	29.9	
+0.9' = Fence on Ground		10.0	30.1	✓
2+25				
-0.9' = Fence		8.4	31.7	✓
N		8.9	31.2	
L		9.6	30.5	
E		10.0	30.1	
+15		15.1	25.0	
2+37 = L Exist. Sewer M.H. 0.4' E L ✓				
on Rim M.H.		9.28	330.84	✓
" Floor base M.H.		14.85	325.27	✓
2+42 = L Euc. tree on west. 18" dia. 30' High. ✓				
-15'		12.0	328.1	
E		9.1	331.0	
L		7.9	32.2	
N		6.4	33.7	
+0.9' = Fence		6.1	34.0	✓
+3' = L Euc tree		6.0	34.1	✓
2+60 = South edge of House on E 16' Back ✓				
-0.9' = Fence		3.7	36.4	
N		3.8	36.3	
L		5.0	35.1	
E		6.5	33.6	
+16' at House Foundation on Ground		3.1	31.0	✓

340.13

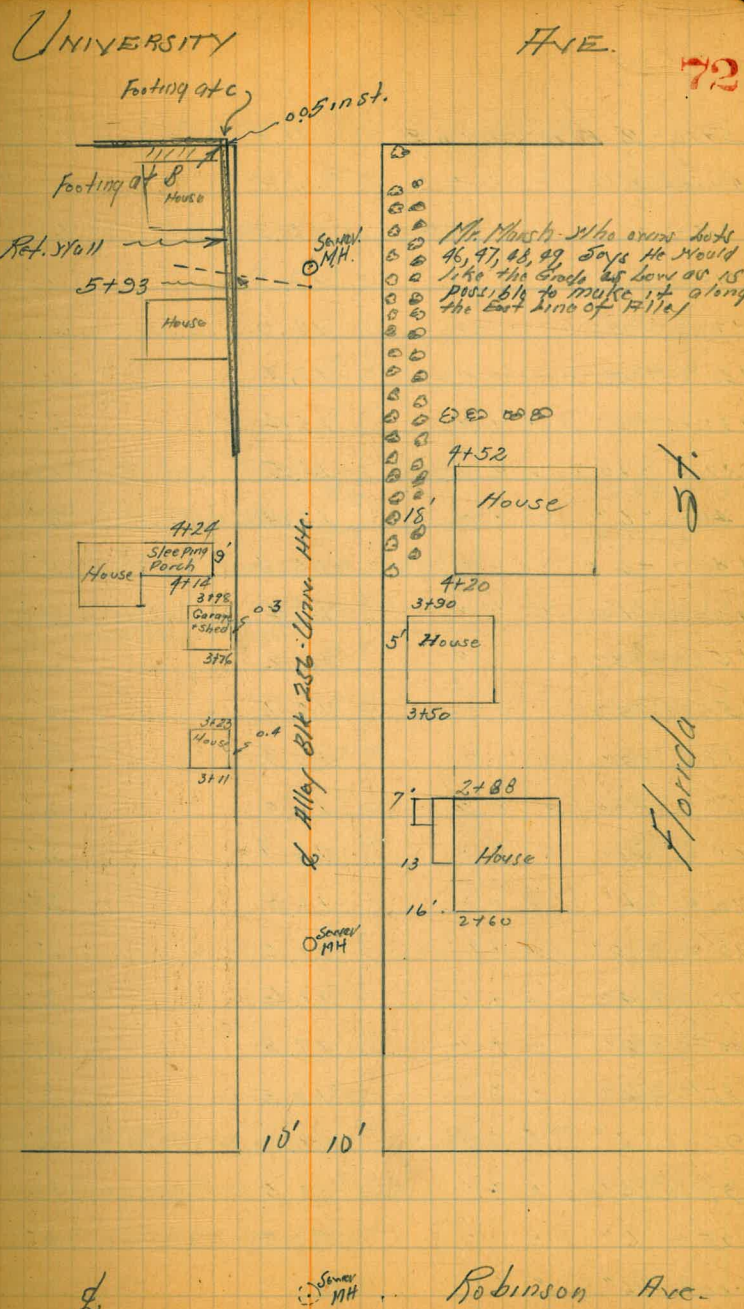
71

2+75				
-13' at House on Ground		5.3	34.8	
E		3.1	37.0	
L		2.6	37.5	
N		2.1	38.0	
+0.9' at Fence		2.0	38.1	
2+88 = N. edge House on East 13' Back ✓				
-2' = L Euc. tree 1' dia. 30' High		0.9	39.2	✓
-0.9' at Fence		0.9	39.2	✓
N		0.9	39.2	
L		1.2	38.9	
E		1.5	38.6	
+13' at House on Ground		3.9	36.8	✓
+13' on Wooden Bench		0.85	39.27	✓
¹⁶ TP. 6.04		345.17	100	339.13 ₁₂
3+17 = L Garage or cottage on west ✓				
-5'		6.1	39.1	
E		5.9	39.3	
L		5.6	39.6	
N		5.6	39.6	
+0.4' on 2" C.I. Vent Pipe ^{at Ground}		5.44	39.72	✓
3+50 S. End of House on East 5' Back ✓				
-0.5' at Fence		5.2	40.0	
N		5.2	40.0	
L		5.1	40.1	
E		5.0	40.2	
+5'		5.4	39.8	✓

on Hub 5' N of
2+88' 13

345.17

3705 = 2 18" Palm tree 1' W L	5.7
3705 = " 3" Luc. tree 5' E E.L.	6.3
+14 = " 6" " " 2.5' E.E.L.	6.0
+22 = " 6" " " 2.0' " " "	6.0
+30 = " 6" " " 2.0' " " "	6.0
+33 = " 3" " " 1.0' " " "	6.0
+36 = " 6" " " 2.0' " " "	5.5
+50 = " 6" " " 2' " " "	5.0
+55 = " 4" " " 3' " " "	5.0
+60 = " 10' " " 3' " " "	5.0
+65 = " 10' " " 3' " " "	5.0
+75 = " 8" " " 5' " " "	5.4
+82 = " 3' " " 2' " " "	5.0
+90 = " 10" " " 2' " " "	5.2
+95 = " 6" " " 3' " " "	5.4
4700 = " 6" " " 2' " " "	5.2
703 = " 10' " " 6' " " "	6.0
717 = " 3" " " 15' " " "	5.7
+30 = " 2" " " on Line	5.6
+56 = " 6" " " 4' E.E.L.	7.2
+80 = " 6" " " 1' " " "	2.5
+80 = " 1.5' " " 7' " " "	10.6
+85 = " 4" " " 7' " " "	11.3
+90 = " 6" " " 10' " " "	11.4
5700 = " 10' " " 1' " " "	10.9
5700 = " 6" " " 6' " " "	11.4



5710 = 2 6" Buc. tree on E	11.8	1' Back
5710 = " " " " " "	12.3	6' "
715 = " 6" " " " "	13.3	6' "
720 = " 6" " " " "	12.9	1' "
727 = " 3" " " " "	14.0	6' "
730 = " 10" " " " "	13.8	1' "
732 = " 6" " " " "	15.4	6' "
737 = " 10" " " " "	14.5	1' "
740 = " 6" " " " "	16.0	6' "
740 = " 6" " " " "	15.1	1' "
750 = " 10" " " " "	15.4	15' "
752 = " 3" " " " "	16.2	6' "
755 = " 3" " " " "	15.7	2' "
758 = " 3" " " " "	16.3	2' "
762 = " 3" " " " "	16.0	2' "
765 = " 3" " " " "	16.7	2' "
770 = " 6" " " " "	16.8	2' "
770 = " 6" " " " "	17.6	6' "
775 = " 4" " " " "	17.6	2' "
780 = " 8" " " " "	17.8	2' "
785 = " 6" " " " "	18.5	2' "
792 = " 6" " " " "	19.0	2' "
792 = " 6" " " " "	19.0	3' "
795 = " 6" " " " "	20.3	6' "
6700 = " 6" " " " "	20.0	2' "
733 = " 20" " " " "	24.8	6' "

3776 S. End of Garage on West ✓	4.6	340.6 ✓
- 0.3		
3790 N. End House on East ✓		
- 5	5.6	339.6 ✓
E	5.0	340.2
£	4.9	340.3
W	4.7	340.5
3798 N. End Garage on West ✓	4.6	340.6 ✓
- 0.3		
714 S. End House & Porch	4.9	340.3
- 7		
4120 S End House on East ✓		
- 18 on foundation	9.48	335.69 ✓
7124 N. End House Sleeping Porch	4.9	340.3
- 9		
4125	5.0	340.2
W	5.4	339.8
£	5.2	340.0
- 10	6.4	338.8
4150		
- 10	8.4	336.8
E	6.6	338.6
£	6.2	339.0
W	5.5	339.7
4152 N. End of House' on East ✓		
- 18 on foundation	9.80	335.37 ✓
4165 Garage on West		
- 8' Dirt floor	5.9	339.3

4775. S. End Double Garage on West

on line
Con. Floor 1
Ent. on Georgia st

W. on Floor	6.14	339.03 ✓
℄	7.8	337.4
E	8.2	337.0
-10	10.2	335.0
TP #6	3.00	340.05
	8.12	337.05

5+00

-15	9.8	330.3
E	4.9	335.2
℄	3.4	336.7
M	2.2	337.9

5+25

M	4.0	336.1
℄	5.1	335.0
E	7.1	333.0
+2	8.7	331.4
+15'	11.3	328.8

5+41 Beginning Con. Ret. Wall

-15'	12.7	327.4
-2'	9.8	330.3
E	8.8	331.3
℄	6.7	333.4

+9.5 = toe Wall of Bottom Footing
M on Natl. Ground+10.0 = East edge top of Wall
Have

5+50 on Footing Ret. Wall on West

5+60

-0.5 = E edge Ret. Wall	4.90	335.15
M = on Natl. Ground	6.6	333.4
M = toe of Footing of Ret. Wall	7.6	332.5
℄	9.1	331.0
E	10.3	329.8
+15'	14.4	325.7

5+75 = End Ret. Wall on West = Beginning Con. Foundation for Houses Etc. on M

-0.6 = E edge Wall on top	4.90	335.15 ✓
-0.1 = toe Wall = Edge Con. Foundation	9.5	330.6 ✓

5+93 = 4" Con. Sewer Lateral on West.

-0.3 of Foundation Footing = top Con. Pipe 11.87		328.18 ✓
M on Natl. Ground	10.1	330.0
℄	10.8	329.3
E	13.0	327.1
+15'	17.1	323.0

5+97 = Sewer M.H. 0.2' M.E. Alley

on Rim M.H. Flush tank?	7.73	332.32 ✓
" Flow Line	14.93	325.62 ✓
" top 4" x 4" overflow	10.50	329.55 ✓

TP 100 330.80 10.34 329.71

6+03

-15'	8.9	321.9
E	5.7	325.1
℄	3.4	327.4
+4	1.8	329.0
M on Natl. Ground	0.7	330.1
6+12 on Footing on West	4.5	326.3 on line ✓

6+25 = E Door to Basement on West.

-0.2' Bottom of Door	4.87	325.93	✓
W on Natl. Ground.	5.4	325.4	
E	7.0	322.8	
E	8.4	322.4	
+2	9.6	321.2	
+7	10.0	320.8	
+15'	13.0	317.8	
6+36.17 = Pat. Hub.	6.77	324.03	✓
-0.4' at Wall on Footing	8.0	322.8	
6+40			
-15'	15.8	315.0	
E	11.7	319.1	
E	8.4	322.4	
W on Natl. Ground.	6.9	323.9	
6+42 = Bottom Footing of B	8.8	322.0 on West.	
#8 3.18 321.08			
T.P. 2.18 320.08	12.90	317.90	
6+44.01 = S.W. Univ. Hts			
W on Walk at C	5.87	315.21	
E " "	7.66	313.42	
E " "	9.46	311.62	
(6+41 = Gas. Main on 9" Pipe)	0.76	320.32	✓
T.P. 12.84	333.49	0.43	320.65
top of Wall at C	0.94	332.55	
T.P. 8.12	341.47	0.14	333.35
chk. on S.W. Univ. & Georgia	4.96	336.51	
		336.41 = BM.	

Alley Blk. 256-Univ. Hts.

75

Check Levels

BM. P. 68

163	313.62	311.99	
T.P. 083	302.18/2.27	301.35	
chk. T.P. #1 - Page 68	1.77	300.41	✓
Flow Line Sewer M.H. S. Robinson No	16.77		
Rim " " " "	8.87		
T.P. 12.22	314.20 0.90	301.28	
chk. T.P. #2 - P. 68	10.80	303.40	✓
T.P. 12.89	327.02 0.07	314.13	
chk. T.P. #3 - P. 70	11.02	316.00	✓
chk. T.P. #4 - P. 70	7.66	327.68	✓
T.P. 12.60	340.28 + 0.66	327.68	
chk. T.P. #5 - P. 71	1.17	339.11 = 0.2 level.	
T.P. 4.28	343.39 1.17	339.11	
T.P. 0.86	331.20 13.05	330.34	
chk. Pat. Hub 6+36.17 opp. Page	7.21	323.99	0.4 level chk. T.P. #8
T.P. 12.87	330.73 13.34	317.86	= 0.4 level.
T.P. 11.14	341.52 0.35	330.38	
chk. S.W. Univ. & Georgia	5.05	336.47	
		336.41 = BM.	
		0.06 = diff.	
	Blk. 256- Univ. Hts.		
	LEVELS ON TOP EXISTING 6" Sewer. in Alley		
1191	335.94	324.03	BM. on Hole 6+36.17
Sta. 5+88 on top of Pipe	8.15	327.79	

Johnson
Cota
Greer
Crawford
8-14-50
W.O. 20006

Reset Point "A"
Int. West Prop. Line Tennyson
East Prop. Line Wabaska
(SEE MAP 1523)

All 4's d' Radii are from
Point Lema Hts. Resub.
Map #1523

INDEXED
SWK.
AUG 18 1950

$R = 538.28$
 $\Delta = 24^{\circ}44'40''$

$R = 556.2$
 $\Delta = 28^{\circ}08'04''$

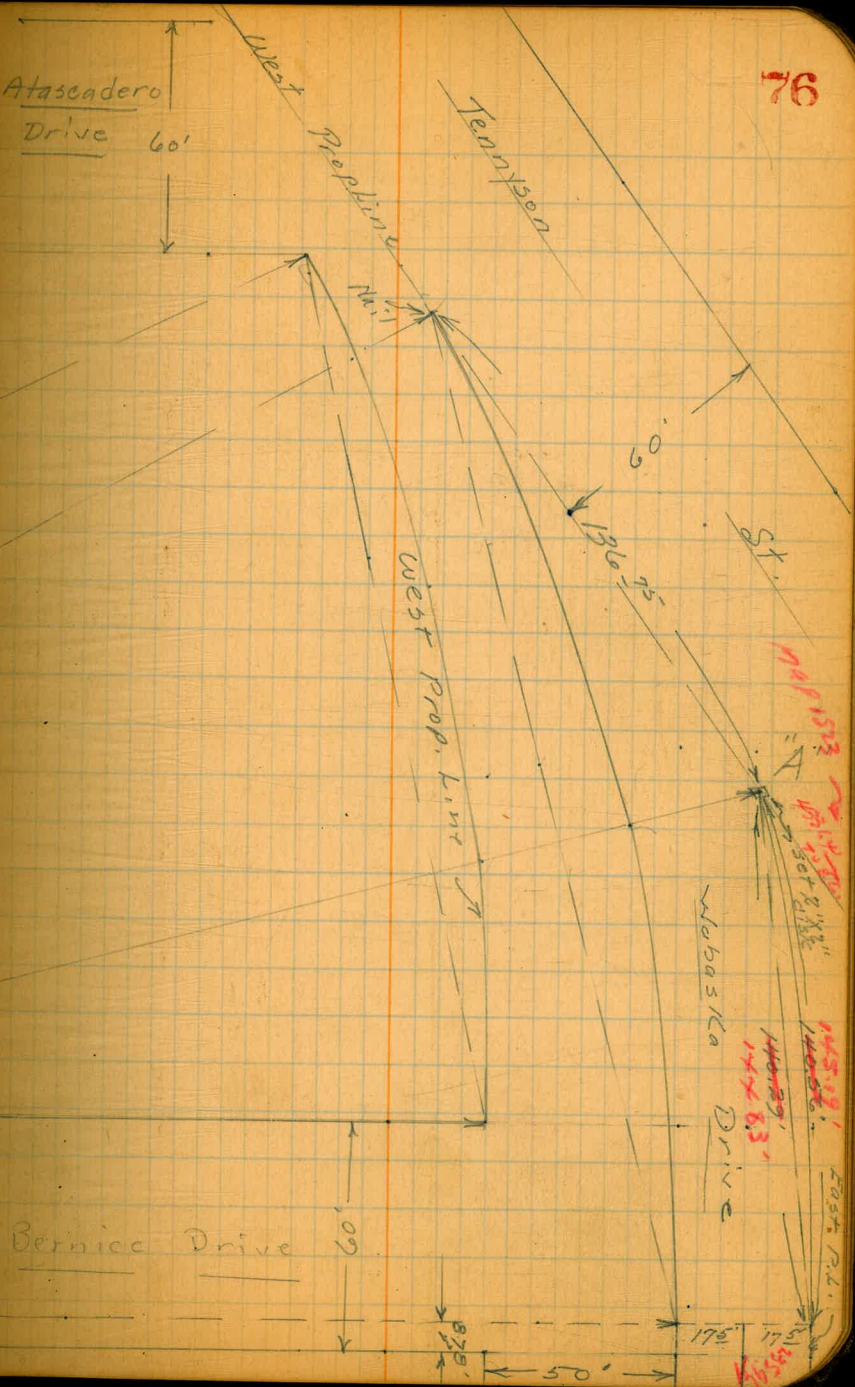
$N 45^{\circ}15'56'' E$

~~$N 61^{\circ}35'24'' E$~~
 $N 59^{\circ}19'43'' E$

$R = 591.2'$
 $\Delta = 11^{\circ}48'36''$

$R = 538.28'$
 $N 73^{\circ}24' E$

$R = 556.2$
 $N 73^{\circ}24' E$



DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1/2 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table is same row and column cross distance.

IMPROVED TABLES
AND
INFORMATION

To find Tangent and External for curve of any other degree divide by degree of curve and add correction found in column of corrections. Degree of curve with a given L may be found by dividing tangent (or external) opposite L by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

TABLE II—Continued
TRIGONOMETRIC FORMULAE (continued)

In any triangle:

Given a, b, C; to find c, B, A.

Use Law of Lines.

Given A, B, c; to find a, b, C.

Use Law of Lines.

Given a, b, c; to find A, B, C.

$$\text{Let } \frac{a+b+c}{2} = s, \sqrt{\frac{(s-a)(s-b)(s-c)}{s}} = r$$

$$\cos \frac{1}{2} A = \sqrt{\frac{s(s-a)}{bc}}$$

$$\tan \frac{1}{2} A = \frac{r}{s-a}$$

$$\tan \frac{1}{2} B = \frac{r}{s-b}$$

$$\tan \frac{1}{2} C = \frac{r}{s-c}$$

Area of a triangle:

$$\text{Area} = \frac{1}{2} ab \sin C$$

$$\text{Area} = \sqrt{s(s-a)(s-b)(s-c)}$$

PRISMOIDAL FORMULA.

$$\text{Vol.} = \frac{h}{6} (B+b+4M)$$

h = altitude; b, B = bases; M = midsection

TABLE III
INCHES AND FRACTIONS OF AN INCH IN DECIMALS OF A FOOT

	0	1	2	3	4	5	6	7	8	9	10	11
$\frac{1}{16}$.0052	.0885	.1719	.2552	.3385	.4219	.5052	.5885	.6719	.7552	.8385	.9219
$\frac{1}{8}$.0104	.0938	.1771	.2604	.3438	.4271	.5104	.5938	.6771	.7604	.8438	.9271
$\frac{3}{16}$.0156	.0990	.1823	.2656	.3490	.4323	.5156	.5990	.6823	.7656	.8490	.9323
$\frac{1}{4}$.0208	.1042	.1875	.2708	.3542	.4375	.5208	.6042	.6875	.7708	.8542	.9375
$\frac{5}{16}$.0260	.1094	.1927	.2760	.3594	.4427	.5260	.6094	.6927	.7760	.8594	.9427
$\frac{3}{8}$.0313	.1146	.1979	.2813	.3646	.4479	.5313	.6146	.6979	.7813	.8646	.9479
$\frac{7}{16}$.0365	.1198	.2031	.2865	.3698	.4531	.5365	.6198	.7031	.7865	.8698	.9531
$\frac{1}{2}$.0417	.1250	.2083	.2917	.3750	.4583	.5417	.6250	.7083	.7917	.8750	.9583
$\frac{9}{16}$.0469	.1302	.2135	.2969	.3803	.4635	.5469	.6302	.7135	.7969	.8802	.9635
$\frac{5}{8}$.0521	.1354	.2188	.3021	.3854	.4688	.5521	.6354	.7188	.8021	.8854	.9688
$\frac{11}{16}$.0573	.1406	.2240	.3073	.3906	.4740	.5573	.6406	.7240	.8073	.8906	.9740
$\frac{3}{4}$.0625	.1458	.2292	.3125	.3958	.4792	.5625	.6458	.7292	.8125	.8958	.9792
$\frac{13}{16}$.0677	.1510	.2344	.3177	.4010	.4844	.5677	.6510	.7344	.8177	.9010	.9844
$\frac{7}{8}$.0729	.1563	.2396	.3229	.4063	.4896	.5729	.6563	.7396	.8229	.9063	.9896
$\frac{15}{16}$.0781	.1615	.2448	.3281	.4115	.4948	.5781	.6615	.7448	.8281	.9115	.9948
1	.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167	1.0000
	0	1	2	3	4	5	6	7	8	9	10	11

TABLE IV
USEFUL RELATIONS.

Lineal feet	×.00019	= miles
Lineal yards	×.0006	= miles
Square inches	×.007	= square feet
Square feet	×.111	= square yards
Square yards	×.0002067	= acres
Acres	×4840	= square yards
Cubic inches	×.00058	= cubic feet
Cubic feet	×.03704	= cubic yards
Links	×.22	= yards
Links	×.66	= feet
Feet	×1.5	= links
360° = 21600' = 1296000"		
Radius = arc of 57.2957790°		
Arc of 1° (radius = 1) = .017453292		
Arc of 1' (radius = 1) = .000290888		
Arc of 1" (radius = 1) = .000004848		

$$\pi = 3.141592654 \quad \sqrt{\frac{1}{4}} = 0.564190$$

$$\frac{\pi}{4} = 0.785398163 \quad \sqrt[3]{\frac{6}{\pi}} = 1.240700982$$

$$\frac{\pi}{6} = 0.523598776 \quad \pi^3 = 9.869604401$$

$$\sqrt{\frac{4}{\pi}} = 1.128379167 \quad \frac{1}{\pi^2} = 0.101321184$$

$$\frac{\pi}{6} = 0.523598776 \quad \sqrt{\pi} = 1.772453851$$

$$\frac{4\pi}{3} = 4.188790205 \quad \frac{1}{\pi} = 0.3183099$$

Curvature of Earth's surface = about 0.7 feet in 1 mile

Curvature in feet = 0.667 (Dist. in miles)²

Difference between arc and chord length, 0.05 feet in 11½ miles

$$\text{Probable error of a single observation} = 0.6754 \sqrt{\frac{\sum v^2}{n-1}}$$

Error in chaining of 0.01 feet in 100 feet:

Due to—

1. Length of tape error of 0.01 feet
2. Alignment. One end 1.4 feet out of line
3. Sag of tape at centre of 0.61 feet.
4. Temperature difference of 15°
5. Difference of pull of 15 lbs.

STADIA REDUCTION FORMULAE.

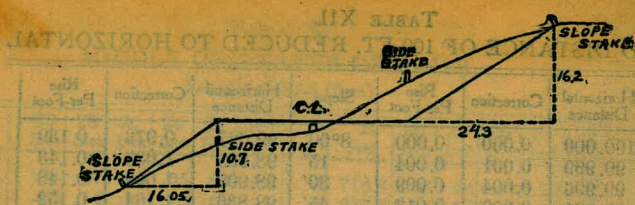
Horizontal Distance = R - R sin² a + C cos a

Vertical Distance = R ½ sin 2 a + C sin a

R = Reading × $\frac{\text{distance from Object glass to cross hairs}}{\text{distance between cross hairs}}$

C = distance from Object glass to cross hairs + distance from Object glass to center of instrument.

a = angle of elevation for mid Reading



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING

SLOPE 1 1/4 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

2.29
 5.87
 7/3.58
 1.79

587
 171
 7.66
 9.45

0
 0-1
 0-2
 1-0
 1-1
 1-2
 2-0
 2-1
 2-2
 2-3
 3-0
 3-1
 3-2
 3-3
 3-4
 4-0
 4-1
 4-2
 4-3
 4-4
 5
 6
 7

To find

