

1331

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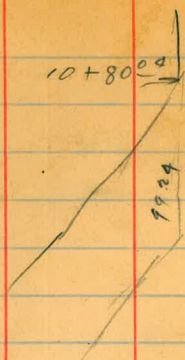
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29
Bliss
1

X. Sec. THORN ST.	42 ND to Fairment	1	
" " Van Dyke	THORN to Lexington	15	
" " LEXINGTON	Van Dyke to Fairment	19	
" " Manzanita	Thorn to Dahlia	29	✓
" " REDWOOD	41 ST to Central	42	✓
" " 41 ST	Redwood to Lexington	46	
" " QUINCE	40 TH to "	54	
" " LEXINGTON	" to Central	61	
QUINCE canon.	Water course crossing	69	✓
REDWOOD "	" " " "	70	✓
Cypress	Indiana to Florida	72	

4/1/29 Loudon
Isbell
Morgan.



BPNE. X Sec Thorn St. from EL
Van Dyke 42nd to W.L. Fairmont.
3 Thorn 80' st 14' cbs 52' Rdway
BM. 145 310.15 308.70

Set by
(w. Bliss)

1

0+00 = E.L. 42nd.

N.L.		9.1	301.1
+5		9.7	300.5
cb	topcb	10.30	299.85 ✓
cut	Par	11.10	299.05 ✓
1/4	Par	10.98	299.17
±	✓	11.11	299.04
1/4	✓	11.40	298.75
cut	✓	11.79	298.36 ✓
cb	topcb	11.16	298.99 ✓
+6		11.0	299.2
S.L.		11.3	298.9
0+25			
S.L.		11.2	299.0
+10		10.7	299.5
cb		11.1	299.1
1/4		10.3	299.9
±		10.2	300.0
1/4		9.7	300.5
cb		9.8	300.4
+6		9.8	300.4
N.L.		8.7	301.5

Plotted 4/17-29 CBH

Thorn

Thorn

3

0+50	310.15		
NL	6.4	303.8	
+7	7.8	302.4	
eb	7.8	302.4	
1/4	9.0	301.2	
+10	9.0	301.2	
+	9.3	300.9	
+10	9.2	301.0	
1/4	9.6	300.6	
eb	10.0	300.2	
+5	10.0	300.2	
SL	10.6	299.6	
0+75			
SL	9.6	300.6	
+10	8.8	301.4	
eb	9.0	301.2	
+8	8.2	302.0	
1/4	8.2	302.0	
+10	8.0	302.2	
+	7.7	302.5	
1/4	7.7	302.5	
eb	7.0	303.2	
+6	7.1	303.1	
N.L.	5.0	305.2	

1+00	310.15		
NL	3.9	306.3	
+10	6.8	303.4	
eb	6.9	303.3	
+6	7.2	303.0	
1/4	7.2	303.0	
+	7.6	302.6	
+6	7.8	302.4	
+10	7.5	302.7	
1/4	7.6	302.6	
eb	8.1	302.1	
+8	7.9	302.3	
SL	7.8	302.4	
1+20			
SL	6.4	303.8	
+3	7.2	303.0	
+9	7.8	302.4	
eb	7.6	302.6	
+3	7.4	302.8	
+9	7.4	302.8	
1/4	7.1	303.1	
+3	6.7	303.5	
+	6.9	303.3	
1/4	6.9	303.3	
eb	6.7	303.5	
+7	6.4	303.8	
NL	2.6	307.6	

Thorn

1+38 ²⁵ = N.L. Alley		
N.L.	2.6	307.6
+7	5.8	304.4
cb	6.3	303.9
1/4	6.4	303.8
+5	6.3	303.9
±	6.6	303.6
1/4	6.7	303.5
cb	6.9	303.3
+7	7.0	303.2
SL	5.5	304.7

1+58 ²⁵ = E.L. Alley		
SL	4.8	305.4
+5	5.8	304.4
cb	6.4	303.8
1/4	6.1	304.1
+4	5.8	304.4
±	5.7	304.5
+8	5.7	304.5
1/4	6.0	304.2
+7	6.0	304.2
+8	5.6	304.6
cb	5.8	304.4
+7	5.3	304.9
N.L.	1.7	308.5

Thorn

1+80 310.15 4		
N.L.	1.5	308.7
+6	5.4	304.8
cb	5.6	304.6
+11	5.5	304.7
1/4	5.1	305.1
+9	4.9	304.3
±	5.3	304.9
+3	5.5	304.7
+7	5.2	305.0
1/4	5.4	304.8
cb	5.8	304.4
+12	5.5	304.7
SL	4.7	305.5
2 + 00		
SL	4.4	305.8
+7	5.3	304.9
cb	5.4	304.8
1/4	4.8	305.4
+4	4.6	305.6
+10	5.1	305.1
±	4.7	305.5
+5	4.4	305.8
1/4	4.9	305.3
cb	5.2	305.0
+8	4.9	305.3
N.L.	1.3	308.9

Thorn

5

2+25	310.15		
NL	0.6	309.6	
+8	4.6	305.6	
cb	4.6	305.6	
1/4	4.2	306.0	
+6	4.3	305.9	
±	4.0	306.2	
+6	4.6	305.6	
1/4	4.3	305.9	
+5	4.7	305.5	
cb	4.9	305.3	
+12	4.8	305.4	
SL	4.0	306.2	
2+50			
SL	3.5	306.7	
+2	4.1	306.1	
cb	4.1	306.1	
+6	4.0	306.2	
1/4	3.7	306.5	
+8	3.9	306.2	
±	3.6	306.6	
1/4	3.7	306.5	
cb	4.0	306.2	
+7	3.9	306.2	
NL	0.8	309.4	

2+75	310.15		
NL	0.2	310.0	
+8	3.4	306.8	
cb	3.7	306.5	
1/4	3.2	307.0	
±	3.2	307.0	
+2	3.1	307.1	
+7	3.5	306.7	
1/4	3.4	306.8	
cb	3.6	306.6	
+3	3.5	306.7	
+12	3.5	306.7	
SL	2.9	307.3	

2+97⁵⁰ = w.L. Van Dyke

SL	3.1	307.1	
+10	2.9	307.2	
cb	3.0	307.2	
1/4	2.9	307.2	
+8	2.7	307.5	
±	2.8	307.4	
1/4	2.5	307.7	
cb	2.4	307.8	
NL	1.3	308.9	

Van Dyke 90' st 14' cbs 52' Rd way

Thorn

West Van Dyke		
N.L. top eb	1.50	308.65 ✓
Ngut Pav	2.08	308.07 ✓
eb	2.6	307.6
1/4	2.9	307.2
+	3.2	307.0
1/4	3.3	306.9
cb	3.5	306.7
SL	3.4	306.8

W 1/4 Van Dyke		
SL	4.0	306.2
eb	3.2	307.0
1/4	2.8	307.4
+	2.4	307.8
1/4	2.1	308.1
cb	1.8	308.4
+8	1.6	308.6
N.L. Pav	1.74	308.41

Thorn

E Van Dyke		
N.L. Pav.	1.72	308.43
+7	1.4	308.8
eb	1.7	308.5
1/4	1.9	308.3
+	2.3	307.9
1/4	2.2	308.0
cb	2.6	307.6
SL	3.0	307.2

E 1/4 Van Dyke		
SL	3.3	306.9
+7	2.2	308.0
cb	1.7	308.5
1/4	2.1	308.1
+	1.9	308.3
1/4	1.7	308.5
cb	1.5	308.7
N.L. Pav.	1.78	308.37

Ecb Van Dyke.		
N.L. top eb	1.47	308.68
N.L. gut Pav	2.07	308.08
eb	2.7	307.5
1/4	1.9	308.3
+	1.9	308.3
1/4	2.0	308.2
cb	2.5	307.7
SL	2.8	307.4

Thorn

E.L. Van Dyke = 0+00

S.L.	3.0	307.2
cb	2.5	307.7
1/4	2.3	307.9
1/2	2.1	308.1
+5	2.0	308.2
1/4	2.2	308.0
+4	2.2	308.0
+7	2.7	307.5
cb	2.3	307.9
N.L.	0.9	309.3

0+03

N.L.	+1.6	311.8
+6	1.3	308.9
cb	2.5	307.7
+6	2.8	307.4
+7	2.2	308.0
1/4	2.3	307.9
+7	1.9	308.3
1/2	2.1	308.1
1/4	2.3	307.9
cb	2.7	307.5
S.L.	3.1	307.1

Thorn.

0+35

S.L.	5.4	304.8
cb	4.3	305.9
1/4	3.6	306.6
+8	3.4	306.8
1/2	3.6	306.6
+5	3.0	307.2
1/4	3.1	307.1
+9	3.2	307.0
cb	3.6	306.6
+4	2.5	307.7
+8	+2.8	313.0
N.L.	+3.0	313.2

0+46

N.L.	1.0	309.2
+6	1.0	309.2
cb	3.5	306.7
+3	4.0	306.2
+10	3.4	306.8
1/4	3.5	306.7
1/2	3.6	306.6
1/4	3.8	306.4
+7	4.4	305.8
+10	5.2	305.0
cb	5.5	304.7
+3	5.7	304.5
+5	12.7	297.5

Thorn

0+46	310.15		
SL	18.1	292.1	
15's	20.4	289.8	
0+63			
15's	22.9	287.3	
SL	21.6	288.6	
cb	13.7	296.5	
+1/2	8.5	301.7	
1/4	6.1	302.1	
+4	6.4	303.8	
±	3.2	307.0	
+6	5.1	305.1	
+7	6.3	303.9	
+11	5.9	304.3	
1/4	4.4	305.8	
cb	4.4	305.8	
+5	3.6	306.6	
N.L.	3.4	306.8	
0+77			
N.L.	6.0	304.2	
cb	6.4	303.8	
+9	7.1	303.1	
+11	8.0	302.2	
1/4	7.3	302.9	
+4	7.1	303.1	
+5	9.0	301.2	
+7	7.8	302.4	

Thorn

0+77			8
±	8.4	301.8	
1/4	10.0	300.2	
+2	10.1	300.1	
+6	23.6	286.6	
cb	25.8	284.4	
+8	28.0	282.2	
SL	28.3	281.9	
7's	27.8	282.4	
20's	28.2	282.0	
1+00			
20's	28.6	281.6	
12's	29.4	280.8	
SL	29.0	281.2	
+11	26.5	283.7	
+12	21.2	289.0	
cb	20.6	289.6	
+8	14.5	295.7	
1/4	14.2	296.0	
+5	14.0	296.2	
+6	14.9	295.3	
+8	13.9	296.3	
±	13.0	297.2	
+7	13.4	297.8	
+8	15.4	294.8	
+10	12.7	297.5	
1/4	12.2	298.0	

Thorn

1+00	310.15		
cb		11.3	298.9
+7		11.0	299.2
N.L.		11.2	299.0
TP. 0.68	299.85	10.98	299.17
1+29			
N.L.		10.7	289.2
+3		10.3	289.6
cb		9.3	290.6
1/4		8.8	291.1
+9		9.1	290.8
+11		10.6	289.3
£		10.7	289.2
+3		9.7	290.2
1/4		10.5	289.4
+4		10.9	289.0
+5		13.5	286.4
+9		13.0	286.9
+11		12.0	287.9
cb		12.5	287.4
+5		12.2	287.7
SL		15.6	284.3
9.5		18.9	281.0
20.5		20.9	279.0

Thorn

9

1+50	299.85		
20.5		19.5	280.4
14.5		19.6	280.3
4.5		17.0	282.9
SL		17.2	282.7
cb		15.5	284.4
+6		15.2	284.7
1/4		13.3	286.6
£		12.0	287.9
TOP M.H. 15 s. of £ sta 1+50		11.91	287.94
FL		17.51	282.34 ✓
1/4		11.0	288.9
cb		13.1	286.8
+12		12.8	287.1
N.L.		12.4	287.5
1+75			
N.L.		6.7	293.2
cb		9.3	290.6
1/4		11.8	288.1
+10		13.4	286.5
£		15.0	284.9
+2		15.7	284.2
1/4		15.7	284.2
cb		17.0	282.9
SL		18.4	281.5
8.5		20.0	279.9
13.5		19.2	280.7

Thorn

2+00	299.85		
155	21.7	278.2	
75	20.3	279.6	
S.L.	17.3	282.6	
cb	16.4	283.5	
+3	19.7	280.2	
1/4	19.5	280.4	
+11	18.2	281.7	
±	17.0	282.9	
+6	10.5	289.4	
1/4	9.5	290.4	
cb	8.2	291.7	
+4	7.8	292.1	
+8	5.9	294.0	
N.L.	4.7	295.2	
2+20			
N.L.	6.8	293.1	
+8	10.0	289.9	
cb	9.8	290.1	
1/4	13.4	286.5	
±	19.4	280.5	
1/4	19.4	280.5	
+5	19.8	280.1	
+10	16.2	283.7	
cb	15.9	284.0	
S.L.	15.8	284.1	
155	17.4	280.5	

Thorn

299.85			
2+45 ^U = w.L. Lexington on south			10
S.L.	20.9	279.0	
cb	18.1	281.8	
1/4	20.1	279.8	
±	21.3	278.6	
1/4	20.7	279.2	
cb	18.3	281.6	
N.L.	13.5	286.4	
T.P. 0.30	287.43	12.72	287.13
2+45 ^U = 2+65			
N.L.	4.8	282.6	
cb	8.6	278.8	
1/4	9.8	277.6	
±	9.7	277.7	
1/4	8.3	279.1	
cb	7.7	279.7	
S.L.	8.7	278.7	
2+45 ^U = 2+80			
S.L.	8.7	278.7	
cb	8.1	279.3	
1/4	7.8	279.6	
+6 on diag.	8.4	279.0	
±	10.2	277.2	
1/4	11.4	276.0	
cb	11.0	276.4	
+10 on diag.	8.1	279.3	
N.L.	1.9	278.5	
10N	11.7	275.7	

Thorn.

287 43
2+45¹¹ = 3+03³⁰ = w.L. Lexington.

NL	10.5	276.9
cb	10.8	276.6
1/4	11.1	276.3
±	11.6	275.8
HD on diag.	9.1	278.3
1/4	7.9	279.5
cb	8.4	279.0
S.L.	8.7	278.7
60' st 10' ebs 40' Rdway.		
0+00 ^{on south} = E.L. Lexington = 0+00 ^{on north}		
S.L.	7.7	279.7
cb	7.5	279.9
1/4	6.0	281.4
±	6.4	281.0
1/4	5.6	281.8
cb	3.0	284.4
NL	1.7	285.7
TP 12.99	300.00	0.41 287.02
0+10		
NL	6.5	293.5
cb	9.5	290.5
1/4	12.8	287.2
±	13.5	286.5
1/4	12.5	287.5
+5	14.1	285.9

Thorn

0+10 300.00 11

cb	13.9	286.1
+5	13.4	286.6
S.L.	15.4	284.6
15's	16.1	283.9
0+20		
15's	10.3	289.7
S.L.	8.9	291.1
cb	8.3	291.7
1/4	6.8	293.2
+8	5.9	294.1
±	7.8	292.2
1/4	6.5	293.5
cb	3.9	296.1
+5	3.7	296.9
TP 12.53	312.49	0.04 299.96
+6	9.5	303.0
NL	8.6	303.9
0+35		
NL	5.1	307.4
cb	6.3	306.2
1/4	8.1	304.4
±	10.9	301.6
1/4	13.1	299.4
cb	14.3	298.2
S.L.	15.4	297.1
10's	16.9	296.6

Thorn

0+50	312.49		
SL		10.8	301.7
cb		8.8	303.7
1/4		7.0	305.5
±		5.4	307.1
1/4		3.8	308.7
cb		3.1	309.4
N.L.		1.9	310.6
T.P. 844	319.74	1.19	311.30

0+75

N.L.		6.6	313.1
cb		7.2	312.5
1/4		7.5	312.2
±		8.3	311.4
1/4		9.6	310.1
cb		10.4	309.3
S.L.		11.5	308.2

1+00

SL		8.6	311.1
cb		7.8	311.9
1/4		7.1	312.6
±		6.3	313.4
1/4		6.1	313.6
cb		5.8	313.9
N.L.		5.5	314.2

Thorn

= w.L. Manganita

1+30 ²²	319.74		
N.L.		4.9	314.8
cb		5.1	314.6
1/4		5.3	314.4
±		5.6	314.1
1/4		5.9	313.8
cb		6.3	313.4
S.L.		6.7	313.0
		6.66	313.08
BM Hub SW Manganita & Thorn			

1+55²⁸ = ± Manganita

S.L.		6.0	313.7
cb		5.6	314.1
1/4		5.4	314.3
±		5.1	314.6
1/4		4.9	314.8
cb		4.6	315.1
N.L.		4.6	315.1

1+80³⁹ = E.L. Manganita

N.L.		4.9	314.8
cb		4.9	314.8
1/4		5.0	314.7
+2		5.4	314.3
±		5.1	314.6
1/4		5.6	314.1
+8		6.1	313.6
cb		5.6	314.1
S.L.		6.0	313.7

12

Thorn

2+00		
SL	6.0	313.7
1/4	6.0	313.7
eb	5.6	314.1
+	5.4	314.3
1/4	5.4	314.3
eb	5.2	314.5
NL	5.2	314.2
2+25		
NL	5.4	314.3
eb	5.4	314.3
1/4	5.4	314.3
+4	5.7	314.0
+	5.6	314.1
1/4	5.8	313.9
+7	6.3	313.4
eb	5.8	313.9
SL	6.1	313.6
2+46 ²⁵ = m.L. Alley		
SL	6.2	313.5
eb	6.2	313.5
+3	6.3	313.4
1/4	6.0	313.7
+5	5.8	313.9
+	5.8	313.9

Thorn

2+46 ²⁵		
+7	6.0	313.7
1/4	5.6	314.1
eb	5.7	314.0
NL	5.8	313.9
2+65 ²⁸		
NL	6.2	313.5
eb	5.9	313.8
1/4	5.9	313.8
+3	6.2	313.5
+	6.1	313.6
1/4	6.2	313.5
+8	6.6	313.1
eb	6.3	313.4
SL	6.2	313.5
3+10 ²⁹ = BC. NW ret.		
SL	7.3	312.4
+3	7.1	312.6
eb	7.3	312.4
1/4	7.2	312.5
+	7.2	312.5
1/4	7.2	312.5
eb	7.2	312.5
NL	6.9	313.8

13

Thorn

3+30 ⁸⁵ = B.C. on south see P2		
8 ⁵ N ^{True N.L.} Int with NW ret.	7.1	312.6
N.L. Not true line.	7.4	312.3
cb	7.5	312.2
1/4	7.7	312.0
±	7.7	312.0
1/4	7.6	312.1
cb	7.6	312.1
S.L.	7.6	312.1
3+75 see P2.		
SL	7.7	312.0
cb	7.6	312.1
1/4	7.7	312.0
±	7.8	311.9
1/4	7.4	312.3
cb	7.4	312.3
N.L. Not true line	7.0	312.7
1 N ^{True N.L.} Int with NW ret	7.0	312.7

Thorn

319.74

3+79 ⁸⁰ see P2 on south = W.L. Fairmont		
30 ¹³ N ^{True N.L.} EC NW ret.	5.4	314.3
N.L.	5.8	313.9
+6 ² top cb endretent	6.00	313.74
+6 ² ext Pav	6.35	313.39
cb Pav.	6.43	313.31
1/4 ✓	6.57	313.17
± ✓	6.84	312.90
1/4 ✓	7.27	312.67
cb ext Pav.	7.87	311.87
cb top c b	7.24	312.50
S.L.	7.4	312.3
Hub w Fairmont sec's of Lexington.		
B.M.	1.27	318.47
B.M. Begin.	11.04	308.70

14

X sec. Van Dyke Ave from SL
 Thorn to N.L. Lexington.
 80' St. 14' cbs 52' Rdway.
 N.E. B.P.
 Van Dyke = Thorn.
 B.M. 0.84 309.54 308.70

4/1/29
 Gordon

Van Dyke.

15

0+00 = SL Thorn. (See Thorn for Section)

0+2.5

EL

cb

+9

1/4

±

+8

1/4

+4

cb

+10

w.L.

0+50

w.L.

cb.

+10

1/4

±

+2

+8

1/4

cb

EL

3.8

3.9

3.3

4.0

4.0

4.5

3.4

2.8

3.1

3.2

3.0

4.7

4.1

3.8

4.4

5.4

5.6

5.3

4.5

5.4

6.3

305.7

306.1

305.5

306.4

306.5

304.8

304.1

303.2

0+75

20'E

EL.

cb

+2

1/4

+10

±

1/4

+3

cb

w.L.

1+00

w.L.

cb

1/4

±

1/4

+4

+5

cb

EL.

20'E

309.54

29.5

27.1

9.4

6.8

6.1

6.9

6.7

5.6

5.3

5.5

6.6

8.9

8.2

8.1

8.0

8.0

8.3

21.0

23.6

28.8

30.0

282.4

302.8

302.9

300.6

301.5

280.7

Plotted 4-18-29 - C.H.

Van Dyke

1+26	309.54		
20E	30.0		
EL	28.1	281.4	
+12	22.6		
cb	15.4		
+3	11.5		
1/4	9.1		
+E	8.8	300.7	
1/4	8.9		
+10	9.5		
cb	9.3		
wL	10.4	299.1	
1+35			
wL	10.6	298.9	
cb	10.2		
+8	10.1		
1/4	9.4		
E	9.4	300.1	
1/4	10.6		
cb	12.3		
E.L	14.5	295.0	

van Dyke

1+50	309.54		
EL	16.6	298.9	16
cb	14.4		
+10	13.7		
1/4	11.6		
E	11.2	298.3	
1/4	11.3		
+7	11.5		
cb	12.8		
wL	12.6	296.9	
T.P. 0.08	296.49	13.13	296.41
1+75			
wL	3.1	293.4	
cb	2.8		
+4	3.2		
1/4	2.6		
E	1.6	294.9	
1/4	2.0		
+2	2.4		
+6	4.4		
cb	5.0		
E.L	6.0	290.5	

Van Dyke

2+00	296.49		
EL	11.3	285.2	
cb	10.1		
1/4	9.4		
±	8.1	288.4	
1/4	7.6		
cb	6.6		
wL	7.1	289.4	
2+25			
wL	8.7	287.8	
cb	9.5		
1/4	9.9		
±	10.5	286.0	
1/4	11.8		
cb	12.8		
EL	13.9	282.6	
2+50			
EL	19.3	277.2	
cb	16.7		
1/4	13.4		
±	12.6	283.9	
1/4	11.3		
cb	10.6		
wL	7.4	287.1	

Van Dyke

2+75	296.49		17
wL	9.8	286.7	
+12	11.4		
cb	11.0		
+7	11.5		
1/4	12.0		
±	14.2	282.3	
1/4	16.6		
cb	20.2		
EL	24.4	272.1	
T.P. 1.84	286.63	11.70	284.79
2+92			
EL	18.0	268.6	
cb	12.5		
1/4	8.2		
±	5.3	281.3	
+6	3.6		
1/4	3.0		
cb	2.2		
wL	0.0	286.6	

Van Dyke
 = WL Lexington on East Sec R2

3+25	286.63	
wL	2.6	284.0
cb	3.7	
1/4	5.9	
1/2	7.6	279.0
1/4	13.5	
cb	21.0	
EL	27.3	259.3

3+25 = 3+50

EL	27.3	259.3
cb	21.8	
1/4	14.4	
+9 on diqq	9.8	
1/2	8.9	277.7
1/4	7.4	
cb	5.3	
wL	3.3	282.7

3+25 = 3+75

wL	6.3	280.3
cb	7.5	
1/2	8.6	
1/2	10.3	276.3
+11 on diqq	11.8	
1/4	14.0	
cb	24.0	
EL	27.3	259.3

Van Dyke

286.63

3+25 = 3+99

EL	27.3	259.3
cb	22.2	
1/4	13.9	
1/2	12.8	273.8
1/4	12.0	
cb	10.3	
wL	10.9	275.7

3+25 = 4+32 = WL Lexington

T.P.	0.40	274.12	12.91	273.72
wL			9.5	264.6
cb			7.0	
1/4			5.5	
1/2			5.2	268.9
1/4			3.3	
+10 on diqq			3.6	
cb			8.9	
EL			14.7	259.4

Xsec Lexington Ave from EG
on E.L. of Van Dyke to Fairmont.
60' st 10' ebs 40' Rdway.

274.12

0+00 = E.L. = E.L. Van Dyke on West.

w.L.	14.7	259.4
+4	15.3	
cb	15.5	
1/4	14.8	
E	14.0	260.1
1/4	12.6	
cb	10.8	
E.L.	8.8	265.3
0+25		
E.L.	5.0	269.1
cb	7.9	
1/4	10.0	
E	12.0	262.1
1/4	14.2	
+8	15.5	259.6
cb	15.3	
w.L.	13.3	260.8
0+50		
w.L.	9.8	264.3
cb	12.4	
1/4	14.7	259.4
+7	14.3	
E	12.0	262.1
1/4	7.7	
cb	5.3	

Plotted 5/14/89 - CBK

A/3/29
London

Lexington

19

0+50	274.12	
E.L.	2.4	271.7
TP 8.25	280.91	1.46 272.66
0+75		
E.L.	7.9	273.0
cb	16.5	
1/4	15.2	
+4	16.7	
+8	20.4	
E	20.4	260.5
+6	20.3	
1/4	19.7	
cb	16.4	
w.L.	13.8	267.1
1+00		
w.L.	12.0	268.9
cb	15.7	
+7	19.2	
1/4	18.7	261.2
+6	19.3	
E	17.0	263.9
+4	15.3	
1/4	13.9	
cb	11.0	
E.L.	8.0	272.9

Lexington

1+25	280.91		
EL	7.6	273.3	
cb	10.0		
1/4	12.3		
±	14.0	266.9	
1/4	18.2		
cb	19.0	261.9	
W.L.	13.5	267.4	

1+50			
W.L.	14.7	266.2	
+7	18.2	262.7	
cb	18.1		
+7	17.4		
1/4	16.0		
+6	13.3		
±	12.5	268.4	
1/4	9.8		
cb	7.3		
EL	3.7	277.2	

1+75			
EL	1.7	279.2	
cb	5.1		
1/4	8.4		
±	11.4	269.5	
1/4	14.5		
+5	16.5		
cb	16.0		

Lexington

1+75	280.91		
+5	16.2	264.7	
W.L.	14.6	266.3	
10W	8.0		
1+84 MH. 16' W. of ±			
{ Top	15.69	265.22	/
{ FL	21.52	259.39	/
2+00			

5W	7.3		
W.L.	10.0	270.9	
cb	15.4	265.1	
1/4	15.2		
+6	11.7		
±	10.6	270.3	
1/4	8.0		
cb	4.3		
EL	0.3	280.6	

2+25			
EL	40.1	281.0	
cb	3.8		
1/4	7.3		
±	10.7	270.2	
+5	13.5		
1/4	14.1	266.8	
cb	13.9		
W.L.	7.7	273.2	

13.05
3.86
9.19
12.33
21.52

20

Lexington

2+50	280.91		
wL	5.5	275.4	
+7	7.6		
cb	9.1		
+4	12.1		
1/4	12.2		
+4	13.3	267.6	
+9	13.0		
1/4	12.0	268.9	
1/4	7.0		
cb	2.7		
EL	+1.5	282.4	
2+65			
EL	+1.6	282.5	
cb	3.0		
1/4	7.4		
+7	10.4		
1/4	12.4	268.5	
1/4	11.4		
+8	6.2		
cb	6.0		
wL	5.3	275.6	
SW	5.2		

Lexington

2+75	280.91		21
10W	5.8		
5W	8.8		
wL	10.1	270.8	
+5	10.7	270.2	
cb	9.1		
1/4	9.0		
1/4	6.3	273.6	
1/4	6.6		
cb	2.6		
EL	+2.0	282.9	
3+00			
EL	+3.5	284.4	
cb	1.2		
1/4	1.1		
1/4	1.2	279.7	
+3	0.7		
1/4	3.3		
cb	3.6		
+7	4.1		
wL	6.3	274.6	
4W	10.2	270.7	
10W	3.9		
T.P.	9.10	288.97	1.04 279.87

Lexington

3+25	288.97		
10W	10.9		
3W	15.0	274.0	
w.L	14.5	274.5	
+7	10.8	278.2	
cb	10.3		
1/4	9.8		
+8	6.7		
⊕	7.2	281.8	
1/4	9.2		
cb	8.1		
E.L	4.1	284.9	

3+50			
EL	3.8	285.2	
cb	7.4		
1/4	11.2		
⊕	11.2	277.8	
1/4	12.9		
cb	12.1		
+2	12.2		
w.L	14.6	274.4	
2W	14.8	274.2	
10W	12.6		

3+75	288.97		
10W	13.3		
w.L	13.6	275.4	
cb	14.2	274.8	
1/4	14.0		
+5	12.0		
⊕	13.2	275.8	
+8	14.6		
1/2	13.1		
cb	7.7		
E.L	3.8	285.2	

4+10 = S.L. Tbox on west.			
EL	8.5	280.5	
cb	11.7		
1/4	15.0		
⊕	15.0	274.0	
1/4	14.1		
+5	13.6		
cb	11.6		
w.L	10.2	278.8	

288.97
 A+98^{el} = sl. Thorn on East

w.L.	10.8	278.2
+5	13.7	
cb	13.4	
1/4	13.6	
±	13.9	275.1
1/4	14.5	
cb	13.6	
E.L.	9.2	279.8

A+72^{el} MH. 12' W of ±

{TOP	12.34	276.63 ✓
{FL	19.09	268.88 ✓

A+78^{el} = ± Thorn on East

EL	8.2	280.8
+6	11.0	
cb	11.4	
1/4	12.3	
±	13.0	276.0
1/4	12.8	
cb	12.8	
w.L.	12.7	276.3

288.97
 5+08^{el} = NL Thorn on East

w.L.	11.8	277.2
cb	11.5	
1/4	12.0	
±	11.7	277.3
1/4	10.4	
cb	7.7	
EL	3.1	285.9
T.P.	11.95	300.80
	0.12	288.85
5+33 ^{el}		
E.L.	4.1	296.7
cb	10.4	
1/4	14.5	
±	16.1	286.7
1/4	18.3	
cb	19.2	
±	22.2	
+8	22.0	
w.L.	20.5	280.3
5W	18.2	
10W	18.1	

5+50		300.80	
10W		12.8	
WL		17.6	283.2
+2		18.0	
+5		21.6	
+8		21.6	
cb		18.3	
+5		16.3	
1/4		15.8	
±		12.2	288.6
1/4		9.3	
cb		5.5	
EL		1.9	298.9
5+75			
EL		0.9	299.9
cb		3.4	
1/4		6.9	
±		11.5	289.3
+4		13.4	
1/4		17.9	
+5		17.8	
+8		20.5	
cb		20.5	
+2		18.5	
WL		17.0	283.8
10W		13.5	

6+00		300.80	24
10W		14.1	
WL		16.0	284.8
+6		17.4	
cb		16.9	
1/4		17.0	
±		12.3	288.5
1/4		8.0	
cb		3.3	
EL		0.5	300.3
6+25			
EL		2.6	298.2
cb		4.9	
1/4		7.7	
±		10.8	290.0
1/4		14.5	
cb		14.3	
WL		15.2	285.6
10W		11.8	

= EL 43^d on West.

6+37¹²

300.80

10W	10.6	
W.L.	13.9	286.9
eb	12.7	
1/4	13.5	
+7	13.8	
±	12.3	288.5
+5	9.9	
1/4	9.7	
eb	7.8	
EL	6.5	294.3

6+44 MH. 9' W of ±

top	11.03	289.73 ✓
FL	19.34	280.46 ✓

6+42

EL	9.3	291.5
eb	10.5	
1/4	11.6	
±	13.2	287.6
1/4	12.0	
eb	12.2	
W.L.	13.0	287.8
10W	10.0	

6+50

300.80

25

10W	8.8	
6W	12.1	
W.L.	11.8	289.0
eb	10.6	
1/4	10.4	
±	9.8	291.0
1/4	9.9	
eb	8.3	
EL	7.6	293.2

6+75

EL	1.5	299.3
eb	2.2	
1/4	2.9	
±	4.0	296.8
1/4	5.5	
eb	6.4	
W.L.	8.0	292.8
10W	9.0	

Lexington

7+00	300.80		
10W	6.9		
w.L.	5.5	295.3	
eb.	4.0		
1/4	2.6		
1/4	0.9	299.9	
TP 12.13	311.74	1.19	299.61
1/4	11.2		
eb	10.2		
EL	9.6	302.1	
7+50			
EL.	5.5	307.2	
eb	6.4		
1/4	7.5		
1/4	8.2	303.5	
1/4	9.5		
+5	9.6		
eb	10.5		
w.L.	12.0	299.7	
10W	14.0		

Lexington

8+00	311.74		26
10W	13.0		
w.L.	11.0	300.7	
eb	8.9		
+5	7.6		
1/4	7.0		
1/4	5.8	305.9	
1/4	4.8		
eb	3.7		
EL	2.7	309.0	
8+42 ⁰³	= w.L. Alley on west.		
EL	0.6	311.1	
eb	2.4		
1/4	3.5		
1/4	5.2	306.5	
1/4	6.6		
eb	7.7		
w.L.	9.4	302.3	
10W	11.0		
8+37 M.H. 12' W of 1/4			
Top	7.30	304.44	✓
F.L.	11.76	299.98	✓

Lexington

311.74

8+75¹¹ = E.L. Alley on West.

10w	7.8	
w.L.	10.5	301.2
cb	8.2	
4	5.8	
4	3.9	307.8
1/4	2.3	
cb	1.0	
E.L.	+0.4	312.1
9+00		
E.L.	+2.3	314.0
cb	40.6	
1/4	1.3	
4	3.1	308.6
1/4	4.5	
cb	7.0	
+4	8.8	
w.L.	7.0	304.7
10w	4.9	

Lexington

9+25

311.74

27

10w		3.6
2w		6.2
w.L.		6.1
+3		4.3
cb		3.4
1/4		2.6
TR.	12.90	321.61
4		3.03
1/4		308.71
cb		11.1
E.L.		310.5
1/4		9.4
cb		7.9
E.L.		6.2
9+50		315.4
E.L.		5.0
cb		316.6
1/4		6.4
4		7.9
1/4		9.2
cb		312.4
+7		10.8
w.L.		11.6
3w		12.4
6w		13.7
10w		307.9
		306.7
		14.9
		12.9
		11.8

Lexington

9+75	321.61	
10W	10.5	
5W	12.9	
W.L.	10.4	311.2
+2	9.5	
cb	9.0	
1/4	8.5	
±	7.6	314.0
1/4	6.4	
cb	4.9	
E.L.	3.5	318.1

10+01⁰⁰ = w.L. Fairmont on East

E.L.	+2.6	324.2
+A	+1.4	
cb	1.0	
1/4	4.2	
±	5.7	315.9
1/4	6.5	
cb	6.8	
W.L.	6.3	315.3
8W	7.8	
10W	7.4	

Lexington

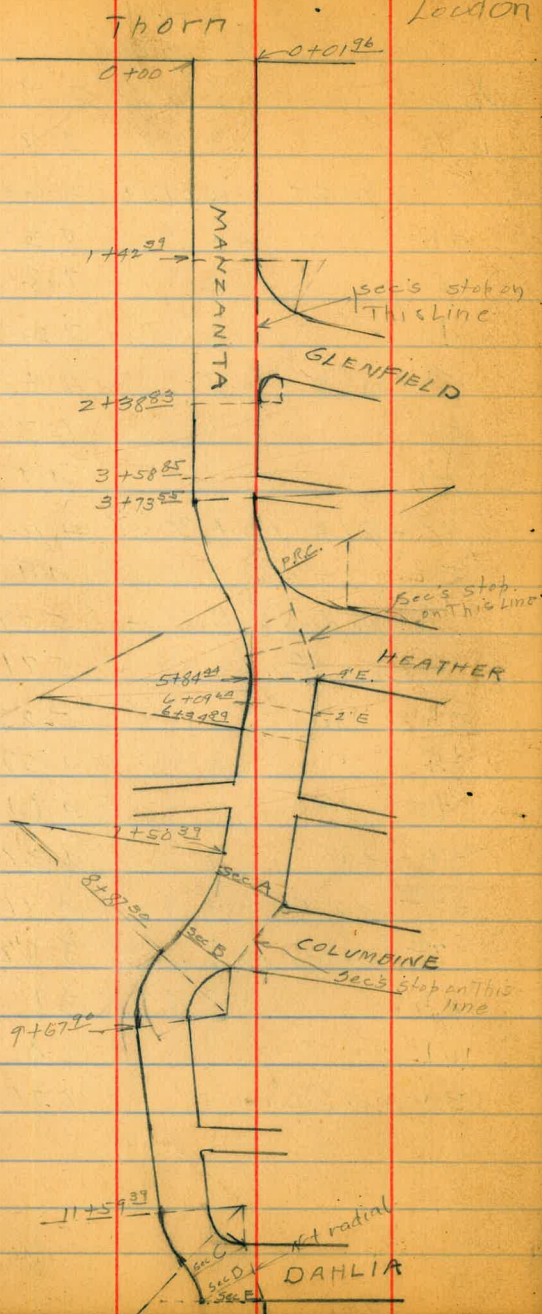
10+01 = 10+50	321.61		28
10W	2.9		
W.L.	2.9	318.7	
T.P. 1025	329.18	2.68	318.93
cb	8.3		
1/4	7.8		
±	7.2	322.0	
1/4	6.4		
cb	6.3		
E.L.	4.9	324.3	
10+01 = 10+80 ⁰⁵ = w.L. Fairmont			
E.L.	4.9	324.3	
+6 ² on diag. end of ret.	5.29	323.89	
+6 ² gut Pav.	5.71	323.47	
cb Pav	5.23		
1/4 ✓	4.57		
± ✓	4.61	324.57	
1/4 ✓	4.30		
+7 ³ gut Pav	4.16	325.02	
+7 ³ top end chcc ret.	3.82	325.36	
cb	3.1		
W.L.	2.4	326.8	
B.M. Hub w Fairmont	10.70	318.48	(319.47)

4/6/29

London

X sec Manganita St From S.L
 Thorn to S.L Dahlia
 50' St 10' c/o 30' Rdway.

29



BM	0.60	313.68	313.08
0+00 west = 0+01.96 East = S.L. Thorn			
EL		+0.3	314.0
cb		0.2	13.5
+3		0.4	13.3
1/4		0.3	13.4
E		0.0	13.7
1/4		0.2	13.5
+4		0.5	13.2
eb		0.2	13.5
W.L		0.6	13.1
0+25			
W.L		1.7	312.0
eb		1.5	12.2
1/4		1.2	12.5
E		0.9	12.8
1/4		1.0	12.7
+4		1.2	12.5
eb		0.9	12.8
EL		0.8	12.9

Plotted
 5/15/29
 J.L.

Heb SW
 Manganita =
 Thorn.

Manzanita.

0+50

EL	1.5	312.2
eb	1.7	12.0
+3	2.2	11.5
1/4	1.9	11.8
+	1.7	12.0
1/4	2.0	11.7
eb	2.4	11.3
wL	2.6	11.1

0+74

conc. Drive 1' in on West. 2.87 310.81

0+75

wL	3.0	310.7
eb	3.0	10.7
+3	3.2	10.5
1/4	2.7	11.0
+	2.5	11.2
1/4	2.6	11.1
+3	2.9	10.8
eb	2.5	11.2
EL	2.3	11.4

0+88

conc. Drive 1' in on West 3.29 310.39

Manzanita.

1+00

EL	3.0	310.7
eb	3.2	10.5
+3	3.5	10.2
1/4	3.3	10.4
+	3.2	10.5
1/4	3.5	10.2
+3	3.8	309.9
eb	3.7	10.0
wL	3.8	09.9

1+25

wL	4.5	309.2
eb	4.4	09.3
+4	4.8	08.9
1/4	4.4	09.3
+	4.0	09.7
1/4	4.1	09.6
+6	4.3	09.4
eb	4.0	09.7
EL	4.0	09.7

30

Margarita

1+42³⁹ = B.C. ret on East.

EL	4.4	309.3
cb	4.6	309.1
+4	4.9	308.8
1/4	4.7	309.0
1/4	4.6	309.1
1/4	5.0	08.7
+4	5.3	08.4
cb	5.2	08.5
wL	5.2	08.5

1+46²wak 3.3' wide
11' in st on East 4.39 309.291+53⁵7' wide
con c'drive 11' in st on West 5.14 308.541+75⁵

wL	6.4	307.3
cb	6.1	07.6
+4	6.4	07.3
1/4	6.1	07.6
1/4	5.8	07.9
1/4	5.6	08.1
cb	5.6	08.1
EL	5.7	08.0

Margarita

2+00

EL	6.2	307.5
cb	6.2	07.5
1/4	6.3	07.4
1/4	6.5	07.2
1/4	6.9	06.8
+4	7.1	06.6
+5	6.6	07.1
cb	6.5	07.2
wL	6.9	06.8

2+38⁸³ = EC ret on East.

wL	8.3	305.4
cb	8.2	05.5
+1	8.1	05.6
+3	8.5	05.2
1/4	8.2	05.5
1/4	7.7	06.0
1/4	8.0	05.7
+3	8.1	05.6
cb	7.7	06.0
EC	7.6	06.1

31

Manzanita

2+75		
E.L.	8.7	305.0
eb	8.9	304.8
+5	9.4	304.3
1/4	9.3	04.4
1/4	8.9	04.8
1/4	9.4	04.3
+5	9.9	03.8
eb	9.6	04.1
w.L.	9.9	03.8

3+00

w.L.	10.6	303.1
eb	10.3	03.4
+2	10.6	03.1
1/4	10.1	03.6
1/4	9.7	04.0
1/4	10.0	03.7
+4	10.2	03.5
eb	9.7	04.0
E.L.	9.4	04.3

Manzanita

32

3+25		
E.L.	10.3	303.4
eb	10.6	303.1
+2	10.9	302.8
1/4	10.7	303.0
1/4	10.4	303.3
1/4	11.0	302.7
+4	11.2	302.5
eb	10.9	302.8
w.L.	11.1	302.6

3+58⁸⁵ - N.L. on East

w.L.	12.0	301.7
eb	11.6	302.1
+5	12.0	301.7
1/4	11.8	301.9
1/4	11.3	302.4
1/4	11.5	302.2
+4	11.7	302.0
eb	11.3	302.4
E.L.	11.1	302.6

Manzanita

9+73⁵⁵ = B.C. on West = S.L. Alleg on East

EL	11.7	302.0
cb	11.8	301.9
+4	12.2	301.5
1/4	12.0	301.7
1/4	11.8	301.9
1/4	12.3	301.4
cb	12.1	301.6
w.L.	12.5	301.2

cv. in 5 parts stationed on West

4+00^{6L} ①

w.L.	12.9	300.8
cb	12.8	300.9
1/4	12.7	301.0
1/4	12.4	301.3
1/4	12.4	301.3
+5	12.8	300.9
cb	12.4	301.3
EL	12.2	301.5

Manzanita

4+27⁶² ② 313.68

EL	12.8	300.9
+8	12.9	300.8
cb	13.3	300.4
+2	13.4	300.3
1/4	13.0	300.7
1/4	13.1	300.6
1/4	13.6	300.1
+L	13.1	300.6
cb	13.3	300.4
w.L.	13.6	300.1

TP 0.53 301.71 12.50 301.18

4+54⁷³ ③

w.L.	2.7	299.0
cb	2.3	299.4
+4	2.2	299.5
1/4	2.3	299.4
1/4	1.6	300.1
1/4	1.6	300.1
+6	1.9	299.8
cb	1.7	300.0
EL	1.2	300.5

Manganitz

4+8129 ④

E.L.	1.8	299.9
cb	2.2	99.5
+2	2.4	99.3
1/4	2.2	99.5
±	2.2	99.5
1/4	3.0	98.7
cb	3.1	98.6
w.L.	3.3	98.4
walk 2' wide 2' in station West	3.18	98.53

5+1139

conc Drivon w.L. 3.40 298.31

5+0884 P.R.C. on West.

w.L.	3.5	298.2
cb	3.4	98.3
1/4	3.2	98.5
±	2.6	99.1
1/4	2.6	99.1
cb	2.5	99.2
E.L.	2.3	99.4

Cain. 5 parts station West.

Manganitz

5+3409 ④

E.L.	2.2	299.5
+2	2.7	99.0
cb	2.6	99.1
1/4	2.6	99.1
±	2.8	98.9
1/4	3.5	98.2
+6	3.6	98.1
cb	3.5	98.2
w.L.	3.6	98.1

5+5929 ②

w.L. 4.1 297.6

cb	3.8	97.9
+5	4.0	97.7
1/4	3.8	97.9
±	3.2	98.5
1/4	2.9	98.8
cb	2.7	99.0
E.L. + 06 int.	2.8	98.9

5+56

6' wide
conc Drive 11' in West 3.85 97.86

34

Manzanita

5+84 ⁹⁴		
9 E secor	3.2	298.5
EL	3.4	98.3
+5	3.7	98.0
cb	3.6	98.1
1/4	3.4	98.3
1/4	3.7	98.0
1/4	4.2	97.5
cb	4.2	97.5
wL	4.2	97.5

5+78

3' wide
on oak 12' in on West

4.04 297.67

6+0964⁹⁴

wL	5.0	296.7
cb	4.7	97.0
+2	4.9	96.8
1/4	4.4	97.3
1/4	4.1	97.6
1/4	4.1	97.6
+6	4.5	97.2
cb	3.9	97.8
EL	3.7	98.0
2'E true EL	3.7	98.0

Manzanita

6+34 ⁸⁴ = E.C. on West		35
E.L	4.2	297.5
cb	4.6	97.1
+5	5.1	96.6
1/4	5.0	96.7
1/4	4.8	96.9
1/4	5.2	96.5
+4	5.5	96.2
+5	5.2	96.5
cb	5.0	96.7
wL	5.6	96.1

6+75

wL	7.3	294.4
cb	6.6	95.1
+1 ⁵	6.5	95.2
+3	7.0	94.7
+5	6.5	95.2
1/4	6.3	95.4
1/4	5.7	96.0
1/4	5.7	95.8
+5	6.2	95.5
+6	5.7	96.0
cb	5.6	96.1
E.L	5.3	96.4

Manzanita

6 + 93⁸¹ = N.L. Alley on West

EL	5.3	296.4
eb	5.8	95.9
+1 ^E	5.8	95.9
+3 ^S	6.5	95.2
4	6.4	95.3
4	6.2	95.5
4	6.8	94.9
+2	6.8	94.9
+4	7.4	94.3
+6	7.1	94.6
eb	7.2	94.5
w.L.	7.8	93.9

6 + 99³ = N.L. Alley on East

w.L.	7.9	293.8
eb	7.3	94.4
+1	7.3	94.4
+3	7.4	94.3
+5	6.9	94.8
4	6.7	94.8
4	6.4	95.3
4	6.5	95.2
+3	6.7	95.0
eb	5.9	95.8
EL	5.3	96.4

Manzanita

7 + 14¹⁵ = 7 + 14³¹ = 21 Alley on East - West. 36

EL	6.0	295.7
eb	6.4	295.3
+4	7.0	94.7
4	6.9	94.8
4	6.8	94.9
4	7.4	94.3
+2 ^E	7.3	94.4
+4	7.9	93.8
+6	7.6	94.1
eb	7.8	93.9
w.L.	8.5	93.2

7 + 50³⁹ BC on West

w.L.	9.1	292.6
eb	8.1	93.6
+1	8.0	93.7
+2	8.5	93.2
4	7.8	93.9
4	7.3	94.4
4	7.7	94.0
+4	7.7	94.0
+6	6.8	94.9
eb	7.1	94.6
EL	6.2	95.5

ev in 5 Parts.

Manganita

7+78 ²⁰ ①		
2 ⁵ E True EL	6.5	295.2
EL	6.7	95.0
ob	7.5	94.2
+1 ⁵	7.4	94.3
+3	7.8	93.9
4	7.7	94.0
4	7.5	94.2
4	8.0	93.7
+5	8.6	93.1
ob	8.5	93.2
wL	9.0	92.7
8+0592②		
wL	7.9	293.8
ob	7.5	294.2
+2	7.9	93.8
4	7.4	94.3
4	6.9	94.8
4	6.8	94.9
ob	7.1	94.6
+5	7.3	94.4
+7	6.4	95.3
EL	6.5	95.2
10 ⁵ E True EL	6.5	95.2

Manganita

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Sec A p29

17 ⁵ E True EL	NE Cor	5.5	296.2
3E		5.8	95.9
EL		6.5	95.2
ob		6.4	95.3
4		6.3	95.4
4		6.5	95.2
4		6.7	95.0
ob		7.2	94.5
+2		6.8	94.9
wL		7.1	94.6
8+3274③			
wL		6.9	294.8
ob		6.6	95.1
+1		6.9	94.8
+3		6.8	94.9
+4		6.4	95.3
4		6.5	95.2
4		6.3	95.4
4		6.1	95.6
ob		6.0	95.7
EL		6.1	95.6
16 ⁵ E int		6.2	95.5

Manzanita.

8 + 60 ^{2L}		
15 ^E int.	5.5	2962
10 ^{SE}	5.9	95.8
8 E	6.6	95.1
EL	6.4	95.3
cb	6.0	95.7
1/4	5.9	95.8
+	6.1	95.6
1/4	6.4	95.3
+6	6.7	95.0
cb	6.9	94.8
w.L.	6.6	95.1
Sec B P 29		
w.L.	6.9	2948
cb	6.5	95.2
+2	6.7	95.0
1/4	6.4	95.3
+	6.1	95.6
1/4	6.0	95.7
cb	6.3	95.4
+6	6.6	95.1
+8	6.1	95.6
EL	5.9	95.8
15 ^E EC SE. ret.	5.9	95.8

Manzanita.

8 + 87 ³⁰ = PRC. on West.		
EL	6.2	295.5
cb	6.3	95.4
+3	7.1	94.6
1/4	6.7	95.0
+	6.4	95.3
1/4	6.7	95.0
+5	6.9	94.8
cb	6.6	95.1
w.L.	6.5	95.2
cv in 3 Parts		
9 + 1/4 ⁶⁰		
w.L.	7.8	2939
cb	7.5	94.2
+2	7.6	94.1
1/4	7.3	94.4
+	6.8	94.9
1/4	7.2	94.5
+4	7.6	94.1
+5 ^E	6.7	94.9
cb	6.7	94.9
EL	6.6	95.1

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Manzanita.

9+41⁰² ②

EL	7.1	294.6
cb	7.3	94.4
+1	7.4	94.3
+3	8.1	93.6
1/4	7.8	93.9
±	7.5	94.2
1/4	8.0	93.7
cb	8.5	93.2
wL	9.2	92.5

9+67⁹⁰ EC on West

wL	10.0	291.7
cb	9.0	92.7
+4	8.9	92.8
1/4	8.4	93.3
±	8.0	93.7
1/4	8.1	93.6
f4	8.4	93.3
cb	7.7	94.0
EL	7.4	94.3

Manzanita.

10+00

301.71

39

EL	8.2	293.5
cb	8.6	293.1
+4	9.1	92.6
1/4	8.8	92.9
±	8.7	93.0
1/4	9.0	92.7
cb	9.9	91.8
wL	10.6	91.1
TR	1.00	293.60
	9.11	292.60

10+25

wL	3.0	290.6
cb	2.1	91.5
+3	1.6	92.0
1/4	1.3	92.3
±	1.1	92.5
1/4	1.3	92.3
+5	1.4	92.2
cb	0.9	92.7
EL	0.5	93.1

Manzanita
= N.L. Alley on East

10 + 50⁸⁴

293.60

E.L.	06	293.0
cb	08	92.8
+2	07	92.9
1/4	1.6	92.0
1/4	1.5	92.1
1/4	1.7	91.9
+3 ^S	1.9	91.7
+5 ^S	1.6	92.0
cb	1.7	91.9
w.L.	3.0	90.6

10 + 66²⁹ = S.L. Alley on East.

w.L.	3.3	290.3
cb	2.2	91.4
+2	2.0	91.6
1/4	2.0	91.6
1/4	1.9	91.7
1/4	2.0	91.6
+4	2.3	91.3
+5 ^S	1.2	92.4
cb	1.1	92.5
E.L.	0.9	92.7

Manzanita

40

11 + 00

E.L.	2.0	291.6
cb	2.4	91.2
+4	3.2	90.4
1/4	3.2	90.4
1/4	3.2	90.4
1/4	3.5	90.1
+5	3.3	90.3
cb	3.6	90.6
w.L.	4.4	289.2

11 + 25

w.L.	5.5	288.1
cb	4.9	88.7
+5	4.3	89.3
1/4	4.2	89.4
1/4	4.1	89.5
1/4	4.1	89.5
+5	4.1	89.5
cb	3.2	90.4
E.L.	2.8	90.8

Manzanita 9.

11+59³⁹ = B.C. on West

EL	3.7	289.9
cb	4.4	89.2
+3	5.5	88.1
1/4	5.0	88.6
+3	4.8	88.8
±	5.0	88.6
1/4	5.1	88.5
cb	5.5	88.1
w.L.	6.3	87.3

11+92²⁹ C of CV on West.

w.L.	6.0	287.6
cb	5.0	88.6
+6	4.9	88.7
1/4	5.3	88.3
+3	5.5	88.1
±	5.4	88.2
+5	5.3	88.3
1/4	5.5	88.1
+4	5.9	87.7
cb	4.3	89.3
EL	4.0	89.6

Manzanita 9.

41

12+25²⁹ = P.R.C. on West

EL	4.1	289.5
cb	4.4	89.2
+1	4.4	89.2
+4	6.3	87.3
1/4	6.3	87.3
±	6.1	87.5
1/4	6.5	87.1
+5	6.6	87.0
cb	6.3	87.3
w.L.	7.3	86.3

SECC P 29

w.L.	8.7	84.9
+9	7.6	86.0
cb	8.3	85.3
+2	8.0	85.6
+4	7.6	86.0
1/4	7.3	86.3
±	6.8	86.8
1/4	6.3	87.3
+4	6.0	87.6
cb	6.0	87.6
+6	6.2	87.4
EL	4.6	89.0
ISE EC NE ret Dablia	4.2	89.4

Manzanita

293.60

Sec D P 29

11 ^E E	int.	5.8	287.8	
E.L.		6.4	87.2	
cb		7.5	86.1	
1/4		7.5	86.1	
±		8.1	85.5	
1/4		8.4	85.2	
+5 ^S		8.6	85.0	
+6		9.7	83.9	
cb		7.8	83.8	
+0 ^S		8.9	84.7	
w.L.		9.7	83.9	
Sec E = SL Dahlia Prod.				
w.L.		9.8	283.8	
+8.		9.6	84.0	
+11.		11.3	82.3	
+13		9.3	84.3	
+20		7.3	84.3	
+30		9.1	84.5	
+40		8.7	84.9	
+49		8.4	85.2	
+55		8.9	84.7	
+58		8.2	85.4	
+67 = E.L.		8.0	85.6	
T.P.	8.07	301.57	0.10	293.50
T.P.	12.50	313.95	0.12	301.45
B.M.	Beginning	0.83	313.12	313.08

B.P.N.E
Van Dyke
& Thorn.
B.M.

X sec Retwood St from w.L
41st to E.L. Central.
80st 17' 6" to 52' Retway

4/9/29
London.

42

B.M.	1.75	310.45		308.70
T.P.	0.99	310.72	0.72	309.73
T.P.	0.40	298.51	12.61	298.11
B.M.	Nails Pole Retwood & 41 st			
			10.11	288.40 (corrected 288.42)
T.P.	13.02	311.96	0.07	298.44
T.P.	0.74	310.86	1.34	310.12
B.M.	Beginning		2.20	308.66
B.M.	12.65	301.07		288.42
	0+00 = E.L. Central.			

N.L.			2.6	298.5
cb			1.4	299.7
1/4			0.1	301.0
±			+0.6	301.7
1/4			+1.3	302.4
cb			+1.6	302.7
SL			+2.0	303.1
	0+25			
SL			0.3	300.8
+3			1.0	300.1
cb			1.1	300.0
1/4			2.5	298.6
±			3.8	297.3
1/4			5.2	295.9
cb			6.1	295.0
N.L.			8.3	292.8

Plotted 5-22-29 E.A.B.

Redwood

0+50	301.07		
NL	12.6	288.5	
cb	10.8	290.3	
1/4	9.0	292.1	
1/2	7.3	293.8	
3/4	5.8	295.3	
cb:	4.4	296.7	
+10	4.1	297.0	
SL	3.1	298.0	

0+75

SL	6.9	294.2	
cb	7.9	293.2	
1/4	9.9	291.2	
+8	11.2	289.9	
1/2	12.3	288.8	
3/4	14.3	286.8	
cb	16.0	285.1	
NL	18.2	282.9	
10'N	19.8	281.3	

Redwood.

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0+75	301.07		
10'N	26.4	274.7	
NL	24.0	277.1	
cb	21.6	279.5	
1/4	18.4	282.7	
1/2	15.4	285.7	
+4	14.8	286.3	
3/4	13.5	287.6	
cb	11.1	290.0	
SL	9.2	291.9	
+10			
SL	11.8	289.3	
T.P.	0.58	288.71	12.94 288.13
cb	2.1	286.6	
1/4	4.8	283.9	
1/2	7.7	281.0	
3/4	11.5	277.2	
cb	14.6	274.1	
NL	17.4	271.3	
15'N	18.5	270.2	

Redwood

	1+30	288.7'		
20'N			24.2	264.5
N.L.			22.8	265.9
cb			19.6	269.1
'A			15.7	273.0
+			11.8	276.9
'A			7.4	281.3
cb			4.8	283.9
S.L.			2.5	286.2
1+40 = wL Alley				
S.L.			4.1	284.6
+9			4.6	284.1
cb			6.6	282.1
'A			10.4	278.3
+			14.5	274.2
'A			18.3	270.4
cb			22.7	266.0
N.L.			26.0	262.7
3N			27.2	261.5
18N			26.4	262.3
MH. at 1+51 3' se of NL (sealed)				
top			26.3	262.4

Redwood

= E.L. Alley.

	1+60	288.7'		
10'N			21.0	267.7
N.L.			24.0	264.7
+8			27.1	261.6
cb			27.4	261.3
+3			27.6	261.1
'A			22.7	266.0
+			18.4	270.3
'A			13.5	275.2
cb			10.8	277.9
S.L.			7.2	281.5
1+80				
S.L.			10.1	278.6
cb			13.3	275.4
J.P.	0.47	276.25	12.93	275.78
'A			5.2	271.1
+			10.4	265.9
'A			17.4	258.9
+9			16.8	259.5
N.L.			11.0	265.3
10'N			6.4	269.9

Red wood

	2+00	276.25	
10'N		4.4	271.9
N.L.		7.6	268.7
eb		13.3	263.0
1/4		17.5	258.8
1/4		17.8	258.5
+		13.6	262.7
1/4		10.4	265.9
cb		6.2	270.1
+7		2.9	273.4
S.L.		1.4	274.9
	2+15		
S.L.		5.0	271.3
+4		7.7	268.6
cb		12.6	263.7
1/4		16.9	259.4
+6		19.0	257.3
+		18.9	257.4
1/4		16.5	259.8
cb		9.7	266.6
N.L.		3.6	272.7

Redwood

45

	2+50	276.25	
N.L.		+0.9	277.2
eb		4.6	271.7
1/4		10.3	276.0
+		14.4	261.9
1/4		18.3	258.0
+4		19.4	256.9
cb		19.5	256.8
+6		19.7	256.6
S.L.		14.7	261.6
15's		11.6	264.7
	2+70		
20's		15.9	260.4
10's		17.5	258.8
5's		21.7	254.6
S.L.		20.0	256.3
cb		19.3	257.0
1/4		15.7	260.6
+		11.6	264.7
1/4		6.0	270.3
cb		0.7	275.6
N.L.		+6.7	283.0

Redwood			
		276.25	
3 + 0097 =	WL	41 st	
NL		+10.8	287.1
cb		+4.4	280.7
1/4		0.3	276.0
±		8.6	267.7
1/4		13.6	262.7
cb		17.7	258.6
SL		20.9	255.4
TP	12.73	288.84	0.14 276.11
BM	Beq.	0.43	288.41 288.42

X sec. 41st St. from NL
 Redwood to N.L. Lexington.
 80' st. 14' cbs 52' Rwy.

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NL Redwood		288.84	
WL		1.9	286.9
cb	to be b	1.94	286.90
cb	put	2.8	286.0
1/4		1.7	287.1
±		1.4	287.4
1/4		1.2	287.6
cb	put	1.4	287.4
cb	to be b	1.78	287.06
EL		1.2	287.6
Ncb Redwood			
EL		+2.0	290.8
+5		0.7	288.1
cb		1.6	287.2
1/4		1.3	287.5
±		1.6	287.2
1/4		2.5	286.3
cb		3.7	285.1
+6		3.3	285.5
WL		8.4	280.4

Plotted 5-12-29
 CBH

41st

288.84

N 1/4 Redwood.

wL	12.7	276.1
+7	9.3	279.5
eb	11.0	277.8
+7	5.8	283.0
1/4	4.8	284.0
±	2.0	286.8
1/4	1.2	287.6
+9	1.1	287.7
+10	3.5	285.3
eb	3.3	285.5
+12	3.3	285.5
+6	1.6	287.2
EL	0.5	288.3
± Redwood.		
EL	3.7	285.1
+7	3.7	285.1
eb	6.7	282.1
+8	3.9	284.9
1/4	4.2	284.6
±	6.0	282.8
+10	6.9	281.9
1/4	8.3	280.5
eb	13.3	275.5
+9	17.4	271.4
+10	21.1	267.7
wL	21.2	277.6

41st

288.84

S 1/4 Redwood.

wL	25.8	263.0
eb	17.9	270.9
1/4	12.0	276.8
+5	9.0	279.8
±	9.0	279.8
1/4	7.3	281.5
+7	7.2	281.6
eb	8.9	279.9
+4	7.0	281.8
EL	6.6	282.2
Sub Redwood.		
EL	9.5	279.3
+10	11.5	277.3
eb	13.4	275.4
+8	12.6	276.2
1/4	13.1	275.7
±	14.7	274.1
1/4	18.2	270.6
eb	24.3	264.5
wL	30.8	258.0

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41st

288-84

S.L. Redwood = 0+00

wL		34.0	254.8
+10		31.7	257.1
cb		29.3	259.5
1/4		24.0	264.8
±		20.7	268.1
+11		18.6	260.2
1/4		20.5	268.3
+3		17.5	271.3
cb		15.5	273.3
E.L.		12.6	276.2
T.P.	0.29	276.15	12.98 275.86
T.P.	0.12	263.28	12.99 263.16
		0+25	
E.L.		1.5	261.8
cb		3.4	259.9
+8		5.6	257.7
+10		9.0	254.3
1/4		9.0	254.3
+3		3.2	260.1
±		3.5	259.8
1/4		4.4	258.9
cb		7.9	255.4
+5		10.1	253.2
w.L.		10.3	253.0
6W		9.6	253.7
7W		8.5	254.8
20W		5.0	258.3

41st

0+50

263.28

48

10W		0.0	263.3
wL		3.6	259.7
cb		7.7	255.6
1/4		11.6	251.7
±		14.2	249.1
+11		14.0	249.3
1/4		15.6	247.7
+10		16.8	246.5
cb		13.6	249.7
E.L.		15.2	248.1
	MH at 0+60 10' W of E.L. Scaled ✓		
Top		13.88	249.40
13'E		13.6	249.7
26'E		5.0	258.3
	0+65		
25'E		7.4	255.9
9'E		15.7	247.6
E.L.		15.9	247.4
+3		15.9	247.4
+5		19.3	244.0
+9		14.9	249.4
cb		13.1	250.2
1/4		11.2	252.1
±		9.3	254.0
1/4		5.6	257.7
cb		1.3	262.0

41st41st

0+65	263.28		
WL	+2.7	266.0	
0+80			
WL	+7.2	270.5	
cb	+3.7	267.0	
1/4	2.0	261.3	
±	6.3	257.0	
1/4	9.9	253.4	
cb	12.3	251.0	
+8	13.5	249.8	
EL	15.4	247.9	
2E	20.9	242.4	
5E	20.8	242.5	
6E	18.4	244.9	
25E	10.4	252.9	
1+00			
25E	18.3	245.0	
20E	21.6	241.7	
15E	21.6	241.7	
14E	18.3	245.0	
EL	12.0	251.3	
cb	9.1	254.2	
1/4	6.2	257.1	
±	3.3	260.3	
1/4	+1.3	264.6	
cb	+6.5	269.8	
WL	+12.9	276.2	

	263.28		
T.P.*	12.67	274.62	1.33
TP	12.75	287.33	0.04
1+25			
WL		4.2	283.1
+7		5.2	282.1
cb		6.7	280.6
1/4		11.7	275.6
±		16.0	271.3
1/4		19.8	267.5
cb		24.3	263.0
EL		30.2	257.1
20'E		37.0	250.3
1+45			
20E		34.2	253.1
EL		26.3	261.0
cb		20.2	267.1
1/4		14.9	272.4
±		10.5	276.8
1/4		5.8	281.5
cb		3.7	283.6
WL		1.0	286.3

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41st

1+75	287.33		
w.L.	+4.0	291.3	
cb	+0.9	288.2	
1/4	2.2	285.1	
⊕	4.7	282.6	
1/4	8.7	276.6	
cb	13.3	274.0	
E.L.	17.8	269.5	
20'E	25.0	262.3	
2+00			
20E	19.0	268.3	
E.L.	12.7	274.6	
cb	8.2	279.1	
1/4	4.0	283.3	
⊕	1.2	286.1	
1/4	+2.5	289.8	
+8	+5.8	293.1	
cb	+6.2	293.5	
w.L.	+8.3	295.6	

41st

50

2+25	287.33		
w.L.	+8.1	295.4	
cb	+5.3	292.6	
1/4	+2.7	290.0	
⊕	0.2	287.1	
1/4	2.9	284.4	
cb	5.6	281.7	
E.L.	10.3	277.0	
20'E	15.9	271.4	
2+50			
10E	8.1	279.2	
E.L.	7.6	279.7	
cb	4.9	282.4	
TP 634	288.43	5.24	282.09
1/4	2.9	285.5	
⊕	0.9	287.5	
1/4	+1.4	289.8	
cb	+4.1	292.5	
w.L.	+6.4	294.8	
2+75			
w.L.	+3.5	291.9	
cb	+1.9	290.3	
1/4	0.4	288.0	
⊕	2.0	286.4	
1/4	6.8	281.6	
cb	7.4	281.0	
E.L.	8.5	279.9	

41st41st

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3+00	28843		
FL		9.3	279.1
cb		6.8	281.6
1/4		5.6	282.8
+7		5.1	283.3
±		7.8	280.6
1/4		7.3	281.1
+5		6.5	281.9
cb		1.3	287.1
wL		0.8	287.6
3+11			
wL		1.8	286.6
+11		7.5	280.9
cb		7.8	280.6
1/4		7.9	280.5
+6		4.9	283.5
±		4.6	283.8
1/4		6.0	282.4
cb		7.8	280.6
EL		8.9	279.5
10E		11.0	277.4

3+22	28843		
10E		12.0	276.4
EL		11.0	277.4
cb		8.9	279.5
1/4		7.3	281.1
±		5.8	282.6
1/4		4.9	283.5
+6		4.8	283.6
cb		8.4	280.0
wL		8.3	280.1
3+33			
wL		9.1	279.3
+8		5.5	282.9
cb		5.6	282.8
1/4		6.7	281.7
±		7.7	280.7
1/4		8.7	279.7
cb		10.1	278.3
EL		11.9	276.5
10E		13.1	275.3

41st

3+40	288.43		
10E		13.8	274.6
EL		12.5	275.9
cb		10.7	277.7
1/4		9.6	278.8
1/4		8.7	279.7
1/4		7.7	280.7
cb		6.8	281.6
wL		5.8	282.6

3+70

wL		10.9	277.5
cb		11.4	277.0
1/4		12.2	276.2
1/4		13.2	275.2
1/4		14.4	274.0
cb		15.6	272.8
EL		16.2	272.2
10E		17.5	270.9

4+00

T.P.	0.95	276.43	12.95	275.48
10E			9.6	266.8
EL			8.6	267.8
cb			6.8	269.6
1/4			6.4	270.0
1/4			5.9	270.5
1/4			5.1	271.3

41st

4+00	276.43		
cb		4.1	272.3
wL		3.5	272.9
4+25			
wL		7.9	268.5
cb		8.8	267.6
1/4		9.7	266.7
1/4		10.1	266.3
1/4		10.8	265.6

cb		11.8	264.6
EL		12.7	263.7
10E		13.4	263.0
4+50			
10E		17.7	258.7
EL		16.7	259.7
cb		15.7	260.7
1/4		14.8	261.6
1/4		13.8	262.6

1/4		13.7	262.7	
cb		13.6	262.8	
wL		12.9	263.5	
T.P.	1.64	265.73	12.34	264.09

		41st			
4+70		265.73			
w.L		6.6	259.1		
cb		7.7	258.0		
1/4		7.9	257.8		
±		9.1	256.6		
1/4		10.7	255.0		
cb		12.1	253.6		
EL		13.3	252.4		
T.P.	0.32	253.16	12.89	252.84	
4+95					
E.L.		12.1	241.1		
cb		10.8	242.4		
1/4		9.1	244.1		
±		7.1	246.1		
1/4		5.8	247.4		
cb		4.3	248.9		
w.L		3.6	249.6		
5+25					
w.L		14.1	239.1		
T.P.	0.61	241.07	12.70	240.46	
+7		2.1	239.0		
cb		3.0	238.1		
1/4		5.9	235.2		
±		7.8	233.3		
1/4		9.4	231.7		
cb		10.9	230.2		
E.L.		11.7	229.4		

		41st			
5+40		244.07			
EL		18.0	223.1		
cb		17.0	224.1		
1/4		15.8	225.3		
±		13.6	227.5		
+8		10.5	230.6		
1/4		9.9	231.2		
cb		7.9	233.2		
+2		7.6	233.5		
w.L.		9.7	231.4		
T.P.	0.31	228.37	13.01	228.06	
5+60					
w.L		8.4	220.0		
cb		5.6	222.8		
+8		3.7	224.7		
1/4		4.1	224.3		
±		6.4	222.0		
1/4		8.7	219.7		
cb		9.3	219.1		
EL		9.9	218.5		

41st

5+75	228.37		
EL		15.0	213.4
eb		14.6	213.8
1/4		13.1	215.3
±		12.2	216.2
±		13.9	214.5
TR 5.90	221.42	12.85	215.52
cb		7.9	213.5
wL		9.7	211.7
10W		9.3	212.1
5+98 ⁶ = N.L. Quince on West			
wL		12.1	209.3
cb		12.3	209.1
1/4		12.2	209.2
±		11.7	209.7
1/4		11.1	210.3
cb		10.6	210.8
EL		10.5	210.9
5+98 ⁶ = 6+11I From N.L. Quince on West to N.L. Lexington on East			
EL		10.8	210.6
cb		11.0	210.4
1/4		11.3	210.1
±		11.7	209.7
1/4		12.2	209.2
cb		12.3	209.1
wL		12.1	209.3
Hub B.C. N.L. Lexington		10.77	210.65
B.M. 3' west EL 41 st			

221.42

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X sec Quince St. From N.L. Lexington
London to EL 40th 80' st 14' cbs 52' Rdway

2+66 on South = N.L. Lexington = 3+00 on North = W.L. 41st

N.L.	12.1	209.3
cb	12.7	208.7
1/4	13.5	207.9
±	14.5	206.9
1/4	15.5	205.9
eb	16.6	204.8
S.L.	17.0	204.4
2+66		
S.L.	17.0	204.4
cb	16.5	204.9
+9	14.1	207.3
1/4	14.8	206.6
±	15.9	205.5
1/4	13.2	208.2
cb	12.0	209.4
N.L.	10.8	210.6
2+50		
N.L.	10.4	211.0
cb	11.1	210.3
1/4	13.1	208.3
±	14.2	207.2
+8	16.3	205.1
±	15.8	205.6
1/4	15.1	206.3
cb	15.3	206.1

Plotted 5-23-29 C.B.H.

Quince

2+50	221.42		
S.L.	16.0	205.4	
2+25			
20.5	17.3	204.1	
S.L.	17.1	204.3	
eb	16.9	204.5	
1/4	16.5	204.9	
+10	16.3	205.1	
±	12.7	208.7	
+5	10.2	211.2	
1/4	10.1	211.3	
eb	8.3	213.1	
+3	9.4	212.0	
+7	6.5	214.9	
N.L.	4.3	217.1	
2+14			
N.L.	2.2	219.2	
+9	7.2	214.2	
+12	5.5	215.9	
eb	5.5	215.9	
1/4	7.5	213.9	
±	7.0	214.4	
1/4	7.9	213.5	
+8	11.7	209.7	
+10	16.5	204.9	
eb	16.5	204.9	
S.L.	17.3	204.1	
20.5	16.6	204.8	

Quince

55

2+00	221.42		
20.5	16.3	205.1	
S.L.	11.5	209.9	
eb	5.8	215.6	
1/4	2.8	218.1	
±	1.1	220.3	
1/4	1.6	219.8	
eb	3.0	218.4	
N.L.	2.6	218.8	
T.P.	12.85	234.17	0.10
1+80			221.32
N.L.	5.9	228.3	
eb	7.1	227.1	
1/4	7.4	226.8	
±	9.4	224.8	
1/4	9.8	224.4	
eb	13.8	220.4	
S.L.	20.7	213.5	
15.5	29.0	205.2	
1+60 = E.L. Alley			
20.5	24.0	210.2	
S.L.	14.6	219.6	
eb	9.9	224.3	
1/4	7.6	226.6	
±	5.0	229.2	
1/4	3.0	231.2	
eb	1.0	233.2	

Quince

1+60	234.17		
N.L.	+0.8	235.0	
1+40 = w.L. Alley			
N.L.	+5.7	239.9	
+2	+4.7	238.9	
cb	+3.0	237.2	
1/4	+1.0	235.2	
±	1.0	233.2	
1/4	3.1	231.1	
cb	6.5	227.7	
S.L.	11.6	222.6	
20's	20.4	213.8	
1+00			
20's	8.1	226.1	
S.L.	0.9	233.3	
T.P.	12.10	246.21	0.06
cb			234.11
1/4			235.5
±			237.5
1/4			240.1
1/4			241.8
cb			244.0
N.L.			246.6

Quince

56

0+75	246.21		
N.L.	+5.4	251.6	
+3	+3.8	250.0	
cb	+1.6	247.8	
1/4	0.0	246.2	
+8	1.6	244.6	
±	3.2	243.0	
1/4	5.6	240.6	
cb	8.0	238.2	
S.L.	10.0	236.2	
20's	14.5	231.7	
0+50			
20's	16.0	230.2	
S.L.	11.1	235.1	
cb	6.9	239.3	
7/11	3.9	242.3	
1/4	2.8	243.4	
±	+0.1	246.3	
+7	+2.2	248.4	
1/4	+2.4	248.6	
+11	+3.6	249.8	
cb	+5.0	251.2	
+9	+7.2	253.4	
N.L.	+9.6	255.8	

Quince

0+25	246.21		
N.L.	+8.9	255.1	
cb	+7.4	253.6	
1/4	+3.2	249.4	
⊕	0.4	245.8	
1/4	5.6	240.6	
cb	11.4	234.8	
S.L.	17.0	229.2	
20'S	22.0	224.2	

0+00 = E.L. Central.

20'S	30.0	216.2	
S.L.	21.8	224.4	
cb	16.0	230.2	
1/4	10.3	235.9	
⊕	4.9	241.3	
1/4	+2.4	248.6	
cb	+5.5	251.7	
N.L.	+10.0	256.2	
TP	11.49	246.44	11.26 234.95

Quince

246.44

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Ecb Central.

N.L.	+6.8	253.2	
cb	+0.2	246.6	
1/4	3.7	242.7	
⊕	8.2	238.2	
1/4	13.6	232.8	
cb	20.0	226.4	
S.L.	25.1	221.3	
20'S	33.2	213.2	

E 1/4 Central.

20'S	34.8	211.6	
S.L.	30.6	215.8	
cb	22.3	224.1	
1/4	18.7	227.7	
⊕	14.2	232.2	
1/4	9.3	237.1	
cb	4.1	242.3	
N.L.	+2.2	248.6	

⊕ Central.

N.L.	2.0	244.4	
cb	8.5	237.9	
1/4	14.7	231.7	
⊕	17.6	228.8	
1/4	23.1	223.3	
cb	28.6	217.8	
S.L.	34.4	212.0	
20'S	35.3	211.1	

Quince

246.44

w 1/4 Central.

20's	32.5	2139
SL	34.0	2124
+8	34.8	211.6
eb	32.0	2144
1/4	26.8	2196
+	21.4	225.0
1/4	15.8	230.6
eb	11.4	235.0
NL	4.0	242.4

w eb Central.

NL	4.6	241.8
eb	13.0	233.4
1/4	17.7	228.7
+	23.4	223.0
1/4	27.3	219.1
eb	32.4	214.0
+4	33.8	212.6
SL	31.4	215.0
15's	28.5	217.9

Quince

246.44

w 1/4 Central = 2+98⁰⁹

58

15's	23.7	212.7
SL	25.7	220.7
+5	30.0	216.4
eb	32.0	214.4
1/4	29.5	216.9
+	25.7	220.7
1/4	21.0	225.4
eb	15.8	230.6
NL	9.9	236.5

2+7.5

NL	17.0	229.4
eb	23.0	223.4
+7	26.5	219.9
1/4	29.8	216.6
+5	29.8	216.6
+9	28.9	217.5
+	29.0	217.4
+8	30.3	216.1
1/4	27.9	218.5
+2	26.3	220.1
eb	23.6	222.8
SL	18.7	227.7

Quince

2+65	246.44		
SL		16.1	230.3
cb		20.3	226.1
1/4		23.4	223.0
+5		24.2	222.2
±		26.6	219.8
+5		27.9	218.5
1/4		27.3	219.1
+7		27.6	218.8
+10		29.4	217.0
cb		29.4	217.0
+5		26.3	220.1
NL		26.0	220.4
15N		22.0	224.4
20N		21.0	225.4
T.P.	12.41	251.67	7.18 239.26
2+25			
20N		28.0	223.7
9N		28.5	223.2
8N		30.0	221.7
NL		30.4	221.3
+3		30.7	221.0
cb		28.6	228.1
1/4		20.0	231.7
±		15.7	236.0
1/4		12.0	239.7
cb		9.3	242.4

Quince

59

2+25	251.67		
SL		4.7	247.0
2+00			
SL		+6.2	257.9
cb		+1.4	253.1
1/4		3.1	248.6
±		7.0	244.7
1/4		11.2	240.5
cb		14.0	237.7
NL		17.4	234.3
20N		21.7	230.0
T.P.	12.70	264.09	0.28 251.39
1+58 ⁶	= EL Alloy		
NL		14.6	249.5
cb		9.3	254.8
1/4		6.5	257.6
±		3.5	260.6
1/4		0.6	263.5
cb		+2.0	266.1
SL		+5.0	269.1
1+38 ⁶	= WL Alloy		
SL		+9.3	273.4
+6		+7.6	271.7
cb		+6.7	270.8
1/4		+4.7	268.8

		Quince			
1+38 ⁶	264.09				
±		+2.0	266.1		
A		0.3	263.8		
cb		3.6	260.5		
N.L.		7.5	256.6		
TP 12.86	276.92	0.03	264.06		
1+00					
N.L.		9.1	267.8		
cb		6.2	270.7		
1/4		4.0	272.9		
±		2.4	274.5		
1/4		1.4	275.5		
cb		0.5	276.4		
S.L.		+0.2	277.1		
TP 12.42	289.00	0.34	276.58		
0+75					
S.L.		8.3	280.7		
cb		9.3	279.7		
1/4		9.9	279.1		
±		10.7	278.3		
1/4		11.9	277.1		
cb		13.2	275.8		
N.L.		14.8	274.2		

		Quince			
0+50	289.00				60
N.L.		11.0	278.0		
cb		9.5	279.5		
1/4		8.3	280.7		
±		6.8	282.2		
1/4		5.7	283.3		
cb		5.3	283.7		
S.L.		5.2	283.8		
0+25					
S.L.		1.2	287.8		
cb		2.1	286.9		
1/4		3.2	285.8		
±		3.8	285.2		
1/4		4.8	284.2		
cb		5.6	283.4		
N.L.		6.9	282.1		
0+00 = F.L. 40 th					
N.L.		2.3	286.7		
cb		1.4	287.6		
1/4		0.5	288.5		
±		+0.1	289.1		
1/4		+1.1	290.1		
cb		+2.0	291.0		
S.L.		+2.8	291.8		
T.P. 7.14	294.94	1.20	287.80		
BM Beginning		6.46	288.48	288.42	

X Sec Lexington Ave from WL Central
 to EL 40th 60'st 10' obs 40' Rhway 4/11/29
 North = Rt. South = Lt. Loudon.

Lexington

61

0+26 ²⁸				204.77	
B.M.	198	212.63	210.65	14N	11.2 193.6
T.P.	5.05	20.477	12.91 199.72	16N	8.2 196.6
0+00 = EC = EL Central on North				25N	7.9 196.9
25N		7.6	197.2	0+52 ⁵⁶ = EL Central on North	
14N		10.7	194.1	30N	8.9 196.0
11N		10.5	194.3	15N	9.9 194.9
8N		8.7	196.1	14N	11.9 192.9
NL		8.1	196.7	6N	11.8 193.0
cb		8.0	196.8	NL	8.8 196.0
1/4		7.6	197.2	+8	10.8 194.0
+3		6.7	198.1	cb	11.0 193.8
±		5.9	198.9	+8	11.0 193.8
1/4		4.7	200.1	1/4	9.4 195.4
cb		4.1	200.7	±	7.8 197.0
S.L.		3.1	201.7	1/4	7.4 197.4
0+26 ²⁸				cb	6.5 198.3
S.L.		4.4	200.4	S.L.	5.7 199.1
cb		5.1	199.7	0+78 ⁸⁴	
1/4		5.8	199.0	S.L.	7.2 197.6
±		6.6	198.2	cb	7.9 196.9
1/4		7.4	197.4	1/4	8.5 196.3
cb		9.1	195.7	±	9.1 195.7
+5		8.1	196.7	+2	9.2 195.6
NL		8.4	196.4	+3	12.5 192.3
5N		10.7	194.1	1/4	11.4 193.4
10N		11.5	193.3	cb	10.5 194.3

Lexington

	20477		
0+7884			
N.L.	10.1	194.7	
2N	11.8	193.0	
7N	11.9	192.9	
14N	12.9	191.9	
15N	10.9	193.9	
27N	9.5	195.3	
1+05 ¹³	= w.L. Central on North		
30N	10.3	194.5	
25N	12.7	192.1	
10N	11.8	193.0	
9N	13.5	191.3	
1N	13.0	191.8	
N.L.	12.0	192.8	
cb	10.8	194.0	
1/4	11.2	193.6	
+	10.6	194.2	
1/4	10.1	194.7	
cb	9.2	195.6	
S.L.	8.4	196.4	

Lexington

62

	20477		
1+25			
SL	9.5	195.3	
cb	10.0	194.8	
+5	11.2	193.6	
1/4	11.7	193.1	
+	12.3	192.5	
+2	13.5	191.3	
1/4	13.1	191.7	
+7	11.0	193.8	
cb	11.1	193.7	
N.L.	14.1	190.7	
7N	13.3	191.5	
10N	11.3	193.5	
20N	10.3	194.5	
1+50			
20N	8.1	196.7	
1N	12.2	192.6	
T.P.	8.63	200.33	13.07 191.70
N.L.	10.1	190.2	
+6	10.1	190.2	
cb	7.7	192.6	
+3	6.8	193.5	
1/4	8.5	191.8	
+	9.9	190.4	
+4	10.3	190.0	
1/4	10.5	190.8	
+4	10.6	189.7	

Lexington

	1+50	20033	
+5		6.4	193.9
cb		5.8	194.5
S.L.		5.0	195.3
205		4.0	196.3
	1+75		
205		2.8	197.5
S.L.		4.8	195.5
cb		6.2	194.1
+3		6.6	193.7
+5		11.1	189.2
1/4		11.6	188.7
⊖		9.8	190.5
1/4		7.8	192.5
+4		7.7	192.6
cb		10.8	189.5
+5		10.5	189.8
+7		7.4	192.9
NL		7.5	192.8
20N		4.2	196.1

Lexington

	2+00	20033	
20N		4.3	196.0
15N		5.8	194.5
NL		7.6	192.7
+7		8.5	191.8
+8		11.1	189.2
cb		11.1	189.2
+4		11.0	189.3
+5		8.9	191.4
1/4		8.7	191.6
⊖		10.4	189.9
+5		11.9	188.4
1/4		12.0	188.3
+1		12.0	188.3
+2		10.3	190.0
cb		7.1	193.2
S.L.		6.5	193.8
205		4.5	195.8
	2+25		
205		5.8	194.5
S.L.		7.3	193.0
cb		7.9	192.4
+7		8.8	191.5
1/4		12.1	188.2
⊖		11.8	188.5
+2		10.8	189.5

63

Lexington

2+25	200.33		
1/4		10.1	190.2
+3		9.4	190.9
+6		11.4	188.9
+9		11.5	188.8
cb		9.4	190.9
NL		8.1	192.2
20N		5.0	195.3
2+5052	= E.L. Mangonita Way on South		
20N		6.3	194.0
NL		9.2	191.1
cb		11.3	189.0
1/4		11.8	188.5
+5		11.1	189.2
±		11.8	188.5
+3		11.8	188.5
+5		10.6	189.7
1/4		9.8	190.5
cb		8.4	191.9
SL		7.5	192.8
20s		6.1	194.2

Lexington

2+82 ³⁵	= W.L. Mangonita Way on South		64
205		4.9	195.4
SL		7.0	193.3
cb		8.2	192.1
1/4		10.1	190.2
±		11.7	188.6
+7		12.3	188.0
1/4		11.6	188.7
cb		12.5	187.8
NL		12.4	187.9
6N		12.4	187.9
8N		8.6	191.7
18NE		5.0	195.3
2+87 ⁸⁵	= E.L. Alley on North		
18N		6.0	194.3
8NE		8.8	191.5
6N		12.9	187.4
NL		12.6	187.7
cb		12.4	187.9
1/4		12.0	188.3
±		11.7	188.6
+7		11.5	188.8
1/4		10.0	190.3
cb		8.0	192.3
SL		6.8	193.5
20s		4.5	195.8

Lexington.

200.33

3+14¹³ = v.l. Alley on North.

20S	4.0	196.3
SL	6.7	193.6
cb	8.8	191.5
1/4	10.3	190.0
+7	13.1	187.2
±	13.0	187.3
+8	13.2	187.1
1/4	12.6	187.7
cb	12.9	187.4
NL	14.0	186.3
2N	14.0	186.3
2N	11.0	189.3
15N	6.3	194.0
3+25		
15N	5.0	195.3
NL	11.2	189.1
+2	14.1	186.2
cb	13.5	186.8
1/4	13.0	187.3
+5	14.0	186.3
±	13.5	187.8
+2	13.5	187.8
1/4	10.0	190.3
cb	8.2	192.1
SL	6.8	193.5
20S	4.8	195.5

Lexington.

200.33

65

T.P. 1.20	193.89	7.6d	192.69
3+50			
20S	1.81	0.4	193.5
SL	0.0	2.1	191.8
cb	1.51	3.1	190.8
+3		3.7	190.2
+6	0.31	7.2	186.7
1/4		7.3	186.6
±		8.3	185.6
+4		8.1	185.8
1/4		6.9	187.0
cb		6.5	187.4
NL		5.7	188.2
5N		5.2	188.7
20N	2.91	+2.8	196.7
3+75			
20N	1.81	2.6	191.3
10N	2.91	6.1	187.8
NL	1.81	7.3	186.6
cb		7.8	186.1
+6		7.8	186.1
+7		9.5	184.4
1/4		9.2	184.7
+3		8.0	185.9
±		7.5	186.4
1/4		7.8	186.1

Lexington

	3+75	193.89	
eb		8.5	185.4
+4		8.0	185.9
+6		3.7	190.2
S.L.		3.5	190.4
20s		2.2	191.7
A+00			
20s		4.0	189.9
S.L.		4.8	189.1
+2		5.0	188.9
+3		8.7	185.2
eb		8.6	185.3
1/4		8.0	185.9
£		8.1	185.8
1/4		8.4	185.5
+5		8.5	185.4
+9		10.0	183.9
eb		9.6	184.3
+2		8.7	185.2
NL		8.1	185.8
1/4 N		6.1	187.8
20N		4.3	189.6

Lexington

66

	4+25	193.89	
23N		7.1	186.8
5N		8.2	185.7
NL		9.9	184.0
+3		10.2	183.7
eb		9.0	184.9
1/4		9.1	184.8
£		9.1	184.8
1/4		9.2	184.7
+7		9.5	184.4
eb		9.2	184.7
+3		8.9	185.0
+5		6.6	187.3
S.L.		6.3	187.6
20s		5.3	188.6
A+50			
20s		5.4	188.5
S.L.		7.1	186.8
eb		7.5	186.4
1/4		8.0	185.9
£		8.3	185.6
1/4		9.2	184.7
eb		10.0	183.9
N.L.		10.3	183.6
6N		10.7	183.2
7N		10.1	183.8
11N		8.0	185.9

Lexington

4+50	19389		
25N		7.0	186.9
4+96 ⁸⁵	= EL. 40 ^H on North.		
25N		6.2	187.7
10N		7.7	186.2
8N		11.1	182.8
N.L.		11.7	182.2
cb		12.1	181.8
+8		12.0	181.9
1/4		10.4	183.5
±		10.5	183.4
1/4		9.9	184.0
cb		8.6	185.3
S.L.		6.9	187.0
205		4.7	189.2

5+23¹³

205		5.6	188.3
S.L.		7.9	186.0
+8		8.8	185.1
cb		9.9	184.0
1/4		11.1	182.8
+6		11.7	182.2
±		13.7	180.2
+5		12.7	181.2
1/4		12.0	181.9
+8		12.0	181.9
cb		11.0	182.9

Lexington

67

5+23 ¹³			
N.L.		9.0	184.9
25N		7.0	186.9
5+49 ⁴	= ± 40 ^H on North.		
25N		9.0	184.9
N.L.		10.3	183.6
cb		10.7	183.2
1/4		11.2	182.7
±		12.3	181.6
1/4		13.7	180.2
+5		13.4	180.5
+6		11.8	182.1
cb		9.6	184.3
S.L.		8.6	185.3
155		6.1	187.8

5+69

155		4.5	189.4
S.L.		8.5	185.4
+5		13.9	180.0
cb		14.1	179.8
+6		13.8	180.1
+7		12.9	181.0
1/4		12.5	181.4
±		11.9	182.0
1/4		11.7	182.2
cb		11.2	182.7
N.L.		11.1	182.8

Lexington.

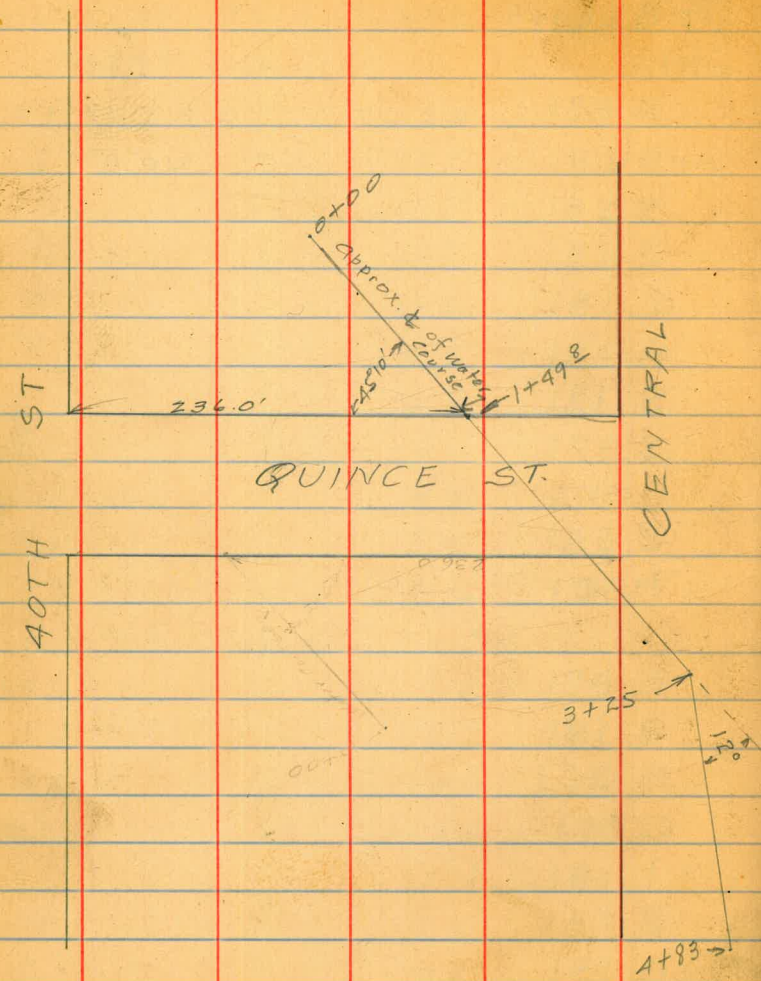
Lexington

68

	5+69	193.89		
25N			10.1	183.8
	5+80			
25N			10.5	183.4
N.L.			11.7	182.2
cb			11.7	182.2
1/4			11.7	182.2
+			12.2	181.7
1/4			12.3	181.6
cb			12.7	181.2
+2			14.6	179.3
5L			14.2	179.7
3s			8.0	185.9
15S			3.5	190.4
67018° = W.L. 40 th on North.				
15S			9.0	184.9
5S			12.3	181.6
4S			14.6	179.3
5L			15.0	178.9
cb			12.8	181.1
1/4			12.6	181.3
+			12.9	181.0
1/4			12.4	181.5
cb			12.3	181.6
N.L.			11.7	182.0
25N			11.3	182.6

		193.89		
T.P.	12.03	205.57	0.33	193.56
-B.M.-			5.96	199.63
T.P.	11.21	216.38	0.42	205.17
B.M. Beginning.			5.71	210.67

Abilene London Profile of Water course in Cañon crossing Quince Near Central.

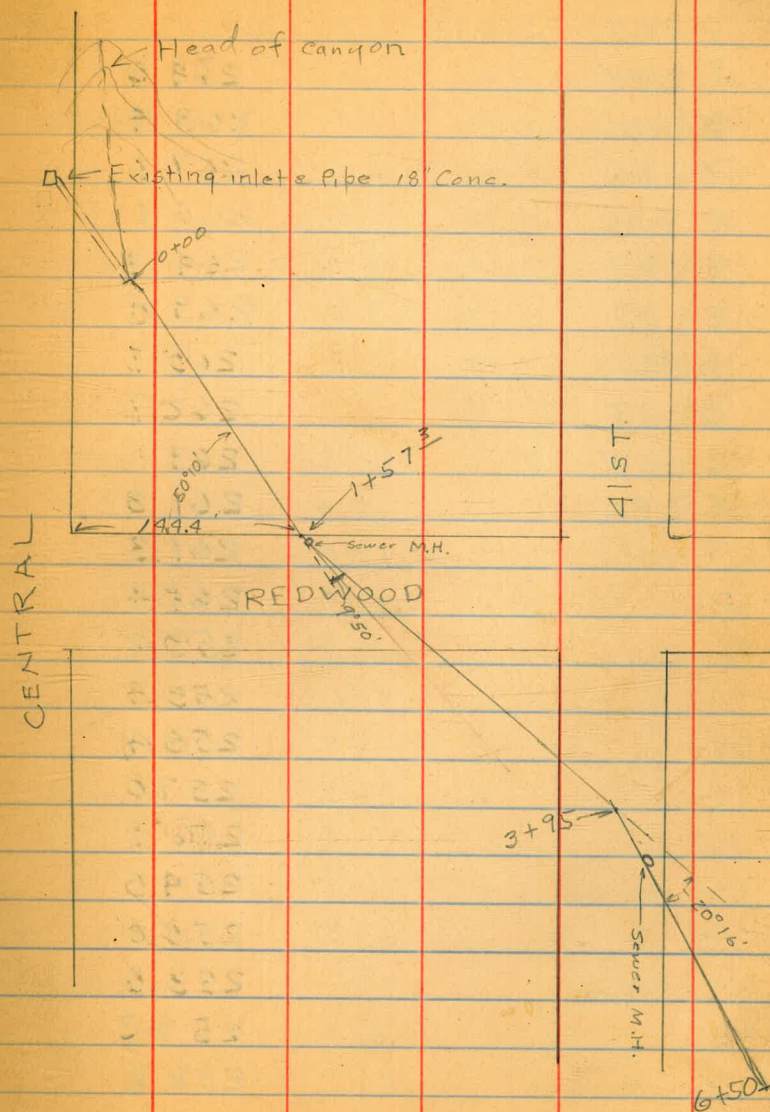


Station	Notes	Distance	Height	Profile
-BM-		1046	210.09	199.63
4+83			10.8	199.3
4+75			10.6	199.5
4+60			12.3	197.8
4+50			13.8	196.3
4+45			10.5	199.6
8' RT	Stream bed.		13.6	197.5
4+40			12.3	198.8
4+25	Stream bed.		11.5	198.6
4+05	stream bed		10.2	199.9
3+94			4.8	205.3
18' RT			9.2	200.7
3+58			4.8	205.3
10' RT	Stream bed.		8.2	201.9
3+48	Stream bed.		7.0	203.1
3+25	L		0.2	209.9
17' LT	stream.		5.0	205.1
T.P.		1221	221.65	0.65 209.44
3+15	Stream		14.9	206.8
3+00	✓		12.9	208.8
2+92			10.2	211.5
12' LT	Stream		15.7	210.0
2+75			8.2	213.5
11' LT	Stream		10.7	210.8
2+55			6.5	215.2
7' LT	Stream		9.1	212.6

		221.65		
2+48	stream	8.6	213.1	
2+25		5.9	215.8	
5' Lt.	stream	7.1	214.6	
2+00		3.2	218.5	
7' Lt.	stream	5.2	216.5	
T.P.	11.91	232.34	1.22	220.43
1+75		12.0	220.3	
9' Lt.	stream	14.7	217.6	
1+60	stream	12.8	219.5	
1+49 ⁸	stream	11.4	220.9	
1+31	✓	10.4	221.9	
1+20		7.9	224.4	
7' Lt.	stream	9.8	222.5	
1+13		6.9	225.4	
7' Lt.	stream	9.2	223.1	
1+00	✓	6.9	225.4	
0+75	✓	5.7	226.6	
0+62	✓	5.7	226.6	
0+50		2.2	230.1	
10' Rt.	stream	4.3	228.0	
0+25		1.5	230.8	
5' Rt.	stream	2.8	229.5	
0+00	✓	1.1	231.2	

Profile of Water Course
in Canon crossing Redwood between
Central & 41st

70



P. 49

T.P.#	1438	273.33	261.95
0+00 FL Pipe	4.4	268.9	
+25 stream	4.9	268.4	
+50 ✓	6.2	267.1	
+75 ✓	7.2	266.1	
1+00 ✓	8.4	264.9	
+15 ✓	9.5	263.8	
+25 ✓	7.6	265.7	
7' Lt stream	10.6	262.7	
1+42	10.2	263.1	
+45	12.0	261.3	
1+57 ³ L	12.0	261.3	
1+75	11.9	261.4	
+85	13.4	259.9	
2+00	14.0	259.3	
+25	14.9	258.4	
+75	16.3	257.0	
3+00	16.8	256.5	
6' Rt stream	18.8	254.5	
3+25	18.3	255.0	
7' Rt stream	19.7	253.6	
3+50	20.0	253.3	
9' Rt stream	20.7	252.6	

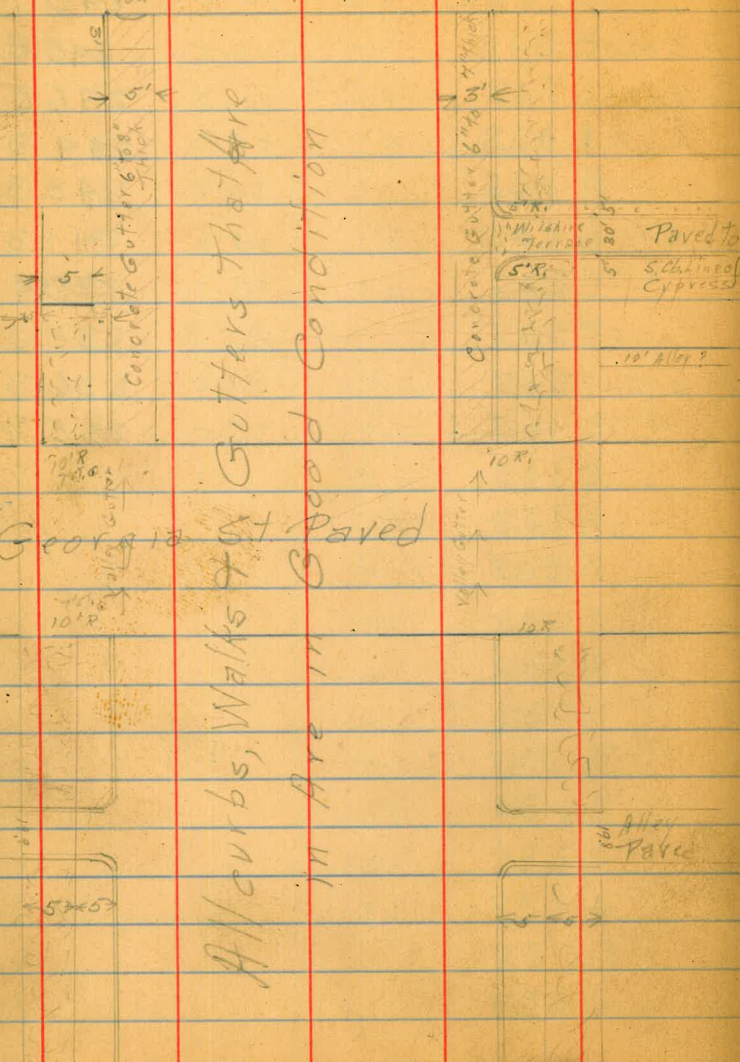
273.33

71

3+75	18.4	254.9
8' Rt stream	23.6	249.7
3+95 L	24.5	248.8
4+25	26.8	246.5
4' Lt stream	29.0	244.3
4+50 stream	30.0	243.3
5+00 ✓	32.0	241.3
+50 ✓	33.9	239.4
6+00 ✓	35.3	238.0
6+50	37.0	236.3
9' Rt stream	38.0	235.3

9/24/27
Floor
level
commence

Section Cypress St.
Indiana to Florida
60' St
10' Cbk
10' 6"



All curbs, Walks & Gutters That Are in Are in Good Condition

Georgia St Paved

Indiana St Paved

	+	-	Elev	72
BM SET	1.31	305.15	300.84	Cypress + P.B.L.D.
T.P.	5.09	306.36	301.27	
0 + 00 = E.L. Indiana				
SB6 top		5.87	300.49	
5' Gut		6.04	300.32	
1/4		5.86	300.50	
⊘		5.57	300.79	
1/4		5.66	300.70	
N Gut		5.80	300.56	
NC6 top		5.35	301.01	
0 + 26'				
NC6 top		4.30	302.06	
Gut		5.2	301.1	
1/4		4.7	301.6	
⊘		4.7	301.6	
1/4		5.0	301.4	
Gut		5.5	300.8	
SB6 top		4.83	301.53	
0 + 30'				
SB6 top		3.74	302.62	
Gut		4.6	301.7	
1/4		3.9	302.4	
⊘		3.5	302.8	
1/4		3.6	302.7	
Gut		4.1	302.2	
NC6 top		3.21	303.15	

cbs Plotted 9/26-29 - CBS

306.36

	+	T	-	Elev
			0 + 75	
N.Cb Top			2.15	304.21
Gut			2.9	303.4
1/4			2.5	303.8
1/4			2.5	303.8
1/4			2.8	303.5
Gut			3.5	302.8
SCb Top			2.74	303.62
			1 + 00 = P.V.C.	
SCb Top			1.65	304.71
Gut			2.3	304.0
1/4			1.7	304.4
¢			1.5	304.8
1/4			1.6	304.7
Gut			1.7	304.6
curb in driveway			1.66	304.70
curb at 097			1.17	305.19
			1 + 25	
N.Cb Top			0.60	305.16
Gut			1.4	305.0
1/4			1.0	305.3
¢			1.0	305.3
1/4			1.3	305.0
Gut			1.6	304.7
SCb in driveway			1.87	304.49
Cb at 7+37			1.10	305.26

306.86

73.

	+	T	-	Elev
			1 + 40 = W.L. Alley	
St. Top Ret.			1.06	305.30
St. paving			1.48	304.88
Cb Top			1.17	305.19
Gut			1.7	304.6
1/4			1.5	304.8
¢			1.1	305.2
1/4			1.3	305.0
Gut			1.6	304.7
Cb Top			0.93	305.43
N.L. Paving			1.27	305.09
N.L. Top Ret.			0.65	305.71
			1 + 50 = ¢ Alley	
N.L. on Ret. Paving			1.76	304.60
Cb Line			1.7	304.6
1/4			1.5	304.8
¢			1.6	304.7
1/4			1.8	304.5
Cb Line			2.0	304.3
St. on Paving			1.90	304.46
			1 + 60 = E.L. Alley	
St. Top Ret.			2.03	304.33
St. on paving			1.98	304.38
Cb Line Top Cb			2.34	304.02
Gut			2.4	303.9

306.36

	+	x	-	Elev
1/4			2.4	303.9
¢			2.1	304.2
1/4			2.2	304.1
Gut			2.2	304.1
Scb Top			1.95	304.41
N.L. paving			1.56	304.80
N.L. Top Ret			1.55	304.81
		17	75	
N.Cb Top			3.13	303.23
Gut			3.9	302.4
1/4			3.6	302.7
¢			3.5	302.8
1/4			3.9	302.4
Gut			4.1	302.2
Scb Top			3.49	302.87
		2400	= E.V.C.?	
Scb Top			6.45	299.91
Gut			7.0	299.3
1/4			7.2	299.1
¢			6.8	299.5
1/4			6.8	299.5
Gut			6.8	299.5
N.Cb Top			6.72	300.14
		27	10 (E.V.C.?)	
N.Cb Top			7.71	298.65

306.36

74.

	+	x	-	Elev
Gut			8.2	298.1
1/4			8.2	298.1
¢			8.2	298.1
1/4			8.5	297.8
Gut			8.3	298.0
Scb Top			7.88	298.48
T.P.	1.20	295.76	11.80	294.56
		24	35	
Scb Top			0.76	295.00
Gut			1.2	294.5
1/4			1.4	294.3
¢			1.0	294.7
1/4			1.3	294.4
Gut			1.4	294.3
N.Cb Top			0.99	294.97
		2460		
N.Cb Top			4.11	291.35
Gut			4.8	290.9
1/4			4.9	290.8
¢			4.7	291.0
1/4			4.8	290.9
Gut			4.7	291.0
Scb Top			4.30	291.46
		2485		
Scb Top			7.90	287.86

	+	7	-	FLY
Gut			8.5	287.2
1/4			8.6	287.1
♀			8.5	287.2
1/4			8.8	286.9
Gut			8.4	287.3
N.Cb. Top			8.19	287.57
	34.10	(10' Closing on Georgia) = W.L. Georgia		
N.Cb. Top			11.74	284.02
Gut on Paring			12.91	283.35
1/4 " "			11.58	283.18
♀ " "			11.14	284.62
1/4 " "			11.28	284.48
Gut " "			12.02	283.74
S.Cb. Top			11.23	284.53
T.P. NW. BP	0.59	284.61	11.74	284.02 ^{Express +} 284.00 GA
	0.400	F.L. Georgia		
S.Cb. Top			1.18	283.43
Gut			2.19	282.42
+ 3 Edge Gut			1.98	282.63 ✓
1/4 on brmt			1.93	282.68
♀ " "			1.92	282.69
1/4 " "			2.22	282.29
+ 5 edge Gut			2.12	282.19 ✓
Gut			2.63	281.98
N.Cb. Top			1.66	282.95

	+	7	-	FLY	75
	0.415	C6 + Gut tier on N. Sunken abt. 3			
N.Cb. Top			1.06	280.55	
Gut			3.06	279.55	
+ 5 Edge			4.71	279.70 ✓	
1/4			1.3	280.3	
♀			3.9	280.7	
1/4			3.8	280.8	
+ 7 edge			4.14	280.47 ✓	
Gut			4.39	280.22	
S.Cb. Top			3.12	281.19	
	0.440				
S.Cb. Top			7.14	277.47	
Gut			8.13	276.48	
1.3			7.85	276.76 ✓	
1/4			7.5	277.1	
♀			7.5	277.1	
1/4			7.6	277.0	
+ 5			8.21	276.40 ✓	
Gut			8.48	276.13	
N.Cb. Top			7.51	277.10	
	0.465	= W.L. of 14' Alley on S.			
N.Cb. Top			11.06	273.55	
Gut			12.07	272.57	
+ 5			11.80	272.81 ✓	
1/4			11.3	273.9	

284.61				272.77			
	+	x	-		+	x	-
							Elev
	4		11.1	273.5		0 + 90	
	1/4		11.2	273.4	N.L. - 35		16.9 255.8
	+ 7		11.69	272.92 ✓	- 35		15.3 257.4
	+ 8.53	edge of drive without intact	11.79	272.82	N.L.		3.6 269.1
	+ 8.86		11.60	273.01	+ 2		1.7 270.0
	Cb Line on drive		11.29	273.32	Cb Top		2.84 269.93
	+ 7.5	endo edge of walk	10.75	273.86	Gut		3.81 268.96
	S.L. in cut		11.0	273.6	+ 5		3.56 269.21 ✓
T.P.	0.17	272.77	12.01	272.60	1/4		3.0 269.7
			0 + 7.5 = E.L. 1.18	Allegon S.	⊕		2.8 269.9
S.L.			0.11	272.6	1/4		3.0 269.7
+ 2.5			0.35	272.42	+ 7		3.19 268.28 ✓
Cb Line on drive			0.91	271.86	Gut		3.71 269.06
+ 1.4			1.25	271.52	Continue in driveway		3.58 269.19
+ 1.5			1.45	271.32	Cb Top @ 21 94		3.34 269.43
+ 3			1.32	271.45 ✓		1 + 15	
1/4			0.7	272.0	5 Cb top		6.45 266.32
⊕			0.7	272.0	Gut		7.46 265.31
1/4			1.0	271.7	+ 3		7.23 265.54 ✓
+ 5			1.39	271.39 ✓	1/4		6.9 265.8
Gut			1.63	271.14	⊕		6.6 266.1
N.Cb Top			0.65	272.12	1/4		6.5 266.2
			0 + 8.0 = end of S. Walk on N.		+ 5		7.22 265.55 ✓
N.L. on edge of fill			1.2	271.4	Gut		7.46 265.31
+ 7.5 on end of S. walk			1.21	271.56	N.Cb Top		6.47 266.30

	+	-	Elev
	272.77		
+ 9		6.2	266.5
N.L.		6.6	266.1
+ 28		29.2	243.5
+ 40		21.4	251.3
	1 + 40 = E.L. Wilshire Terrace		
N.L. - 30		23.8	248.9
- 20		22.2	250.5
N.L.		9.8	262.9
Cb Top		10.13	262.64
Gut		11.12	261.65
+ 5		10.88	261.89 ✓
1/4		10.2	262.4
¢		10.2	262.5
1/4		10.1	261.8
+ 7		10.98	261.79 ✓
Gut		11.22	261.55
Cb Top		10.22	262.55
T.P.	205 260.38	12.44	260.33
	1 + 60 = E.L. Wilshire Terrace on S.		
St. on paving		1.71	258.67
Ob line on paving		1.79	258.59
+ 3 on edge of Cement gutter		1.51	258.87 ✓
1/4		0.8	259.5
¢ on M.H. Rim		0.44	259.94
1/4		0.8	259.5

	+	-	Elev
	260.38		
+ 5		1.35	259.03 ✓
Gut		1.62	258.76
Ncb Top		0.64	259.74
N.L.		0.5	259.9
+ 34		13.5	246.8
+ 30		14.6	245.7
	1 + 90 = E.L. Wilshire Terrace on S.		
N.L. - 30		17.3	243.0
- 20		16.1	244.3
N.L.		3.5	256.8
Ncb Top		3.56	256.82
Gut		4.51	255.87
+ 5		4.76	256.22 ✓
1/4		3.7	256.6
¢		3.6	256.7
1/4		4.0	256.3
+ 7		4.48	255.90 ✓
Gut		4.68	255.70
Cb Top		3.71	256.67
	1 + 95		
5 Cb Top		5.94	254.44
Gut		6.71	253.47
+ 3		6.67	253.71 ✓
1/4		6.3	254.0
¢		5.9	254.4

	+	π	-	Elev
1/4			6.0	254.3
+5			6.31	254.07 ✓
Gut			6.71	253.67
N.C. Top			5.76	254.62
+9			5.9	254.4
N.L.			6.2	254.1
+22			18.0	242.3
+30			19.1	241.2
		2+20		
N.L. -30			21.8	238.5
-20			20.7	239.6
N.L.			9.5	250.8
+1			9.0	251.4
N.C. Top			9.22	251.06
Gut			10.28	250.10
+5			9.73	250.45 ✓
1/4			9.6	250.7
Φ			9.7	250.6
1/4			10.1	250.2
+7			10.44	249.94 ✓
Gutter			10.65	249.73
SC. Top			9.68	250.70
T.P.	0.05	248.06	12.37	248.01
		2+15		
SC. ind. driveway			1.85	246.21

	+	π	-	Elev
Gutter			1.75	246.11
+3			1.82	246.24 ✓
1/4			1.3	246.7
Φ			1.0	247.0
1/4			0.8	247.2
+5			1.08	246.98 ✓
Gut			1.46	246.60
N.C. Top			0.49	247.57
+9			0.3	247.7
N.L.			0.9	247.1
+18			10.7	237.1
+25			12.4	235.6
		2+70		
N.L. -25			14.5	233.5
-15			13.0	235.0
N.L.			1.4	243.6
+1			3.8	244.2
N.C. Top			4.09	243.97
Gut			5.06	243.00
+5			4.63	243.43 ✓
1/4			4.4	243.6
Φ			4.6	243.4
1/4			4.9	243.1
+7			5.48	242.58 ✓
Gut			5.69	242.37
cb line in driveway			5.60	242.41
CB @ 2+72			5.02	243.04

248.06

	+	-	Elev.
			249.5
SC6 Top		8.37	239.67
Gut		9.37	238.69
+3		9.10	238.96 ✓
		8.6	239.4
Φ		8.2	239.8
14		8.0	240.0
+5		8.30	239.76 ✓
Gut		8.59	239.47
NC6 Top		7.60	240.46
18.5		7.4	240.6
N.L.		7.9	240.1
+13		15.0	233.0
+20		15.3	232.7
		3 + 17	
N.L. -10		11.2	236.8
-5		10.1	237.9
N.L.		10.0	238.0
NC6 Top		10.72	237.34
Gut		11.74	236.34
+5		11.47	236.59 ✓
14		10.9	237.3
Φ		10.5	237.5
14		11.1	236.9
+7		12.32	235.74

248.06

79

	+	-	Elev.
Gut		12.60	235.46
SC6 Top		11.61	236.45
		34.20 = W.L. Floor	251.5
SC6 top		12.06	236.00
Gut. End		12.05	235.01
+3 - edge of gutter-end		12.76	235.30 ✓
14		11.30	236.76
2		10.6	237.4
14		10.9	237.1
+5 on dirt		11.2	236.8
+5 edge of Gut gut. end		11.97	236.09 ✓
+8 on Gutter		12.12	235.94
+9 = flow line ^{6002"} 25" iron pipe		13.60	234.46
NC6 Top		11.11	236.95
N.L. on S. Walk (10' x 14' solid)		10.97	237.07
T. R. B. P. W.		3.30	244.76 = 244.77

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 N to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body

from side stake to slope stake. If ground is not

**IMPROVED TABLES
AND
INFORMATION**

necessary.

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given I may be found by dividing tangent (or external), opposite I by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

+ T - Elev

ENGINEERING DEPARTMENT
CITY OF CALIFORNIA, SAN DIEGO.

$$\begin{array}{r} 55 \\ 75 \overline{) 380} \\ \underline{375} \\ 5 \end{array}$$

$$\begin{array}{r} 09 \\ 8 \overline{) 70} \\ \underline{64} \\ 6 \end{array}$$

$$\begin{array}{r} 24 \\ 96 \\ 20 \\ \hline 236 \end{array}$$

$$\begin{array}{r} .16 \\ 8 \overline{) 1.3} \\ \underline{.80} \\ .50 \end{array}$$

$$\begin{array}{r} 16 \\ 14 \\ \hline 2.24 \end{array}$$

$$\begin{array}{r} 1680 \\ 8 \overline{) 1280} \\ \underline{1280} \\ 0 \end{array}$$

$$\begin{array}{r} .34 \\ 14 \\ \hline 136 \\ 39 \\ \hline 4.76 \end{array}$$

$$\begin{array}{r} 34 \\ 13 \\ \hline 102 \\ 34 \\ \hline 4.22 \end{array}$$

$$\begin{array}{r} 7 \\ 8 \overline{) 56} \\ \underline{56} \\ 0 \end{array}$$

$$\begin{array}{r} 14 \\ 7 \\ \hline 9.8 \end{array}$$

$$\begin{array}{r} 13 \\ 7 \\ \hline 9.1 \end{array}$$

$$\begin{array}{r} 90 \\ 49-33 \\ \hline 40-27 \end{array}$$

$$\begin{array}{r} 1.31411 \\ 29809 \\ \hline 1182699 \end{array}$$

$$\begin{array}{r} 1.31411 \\ 80 \\ \hline 10572880 \end{array}$$

$$\begin{array}{r} 1051288 \\ 1182699 \\ 262822 \\ \hline 23917230499 \end{array}$$

$$\begin{array}{r} 180.86 \\ 13.14 \\ \hline 167.72 \end{array}$$

$$\begin{array}{r} 40-27 \\ 28-18 \\ \hline 12-09 \end{array}$$

$$\begin{array}{r} 239172 \\ 195.86 \\ 13.14 \\ \hline 182.72 \end{array}$$

$$\begin{array}{r} 61-42 \\ 49-33 \\ \hline 12-09 \\ 6-04-30 \end{array}$$

$$\begin{array}{r} 182.72 \\ 105.13 \\ \hline 287.85 \\ 26.28 \\ \hline 314.13 \\ 182.72 \\ \hline 496.85 \end{array}$$