

1334

FIRST

LEVEL BOOK

NO. 350 F

MICROFILMED
DEC 23 1964

The index is totally of paper A.H.

ENGINEERING DEPARTMENT,
CITY OF SAN DIEGO,
CALIFORNIA.

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79 $\frac{1}{2}$ of Alley Not Main from Rigel to
32nd St outfall.

001

8, 11 Bliss
 Joe Duermit
 J. Jacobsen
 P. Kiernan
 4.8.19

X
 A Sections of 34th Street "E" to

HZ
 69.79
 -
 Elev

002

BM	1.46	100.72	99.26	NE Mon 39 th + Broadway	+4 +5	6.8 6.2	63.0 63.6
T.P.	0.52	88.95	12.29	88.93	E	5.8	64.0
T.P.	1.05	77.78	12.22	76.73		0+05	
T.P.	3.49	69.79	11.48	66.30	E	5.4	64.4
Set BM			8.17	61.62	NE BP Lemon Grove Blvd. or E St 60st 10.65 10.41	+5	5.5 64.3
		0+00 N line of		Lemon Grove Blvd	+6	6.3	63.5
E	"on paving"	7.4	62.4		cb	6.8	63.0
E Top cb		7.62	62.17	✓	+5	7.3	62.5
G		8.32	61.47		1/4	7.3	62.5
1/4		7.68	62.11		ϕ	7.1	62.7
ϕ		7.29	62.50	✓	1/4	6.9	62.9
1/4		7.26	62.53		+5	6.6	63.2
G		7.39	62.40		cb	5.7	64.1
W Top cb		6.70	63.09	✓	+3	4.3	65.5
W		5.7	64.1		W	3.4	66.4
		0+02				0+30	
W		5.5	64.3		W	2.8	67.0
+5		5.7	64.1		cb	3.3	66.5
cb		6.5	63.3		+5	4.1	65.7
+3		7.1	62.7		1/4	4.2	65.6
1/4		7.2	62.6		ϕ	4.1	65.7
ϕ		7.2	62.6		1/4	4.2	65.6
1/4		7.6	62.2		+5	4.7	65.1
+8		7.9	61.8		cb	4.6	65.2
cb		7.5	62.3		E	4.5	65.3

Plotted 4-16-89 C.B.H.
 Reduced by Britten

	+	HZ. 81.04	-	E		+	HZ 81.04	-	E/er
cb			4.3	76.7	1/4			4.3	76.7
ts			4.4	76.6	ϕ			3.7	77.3
1/4			4.9	76.1	ϕ Rim Dr. Hole			3.23	77.81 ✓
ϕ			5.4	75.6	Flow Line			9.84	71.20 ✓
1/4			5.9	75.1	1/4			3.3	77.7
cb			6.3	74.7	cb			2.9	78.1
E			6.4	74.6	W			2.6	78.4
			S. cb					N. 1/4	
E			6.2	74.8	W			1.6	79.4
cb			5.8	75.2	cb			1.8	79.2
1/4			5.3	75.7	ts			1.9	79.1
ϕ			4.8	76.2	1/4			2.2	78.8
1/4			4.2	76.8	ϕ			3.0	78.0
cb			3.5	77.5	1/4			3.4	77.6
W			3.4	77.6	cb			3.9	77.1
			S. 1/4		E			4.4	76.6
W			2.9	78.1				N. cb.	
cb			3.1	77.9	E			3.7	77.3
1/4			3.6	77.4	cb			3.1	77.9
ϕ			4.2	76.8	ts			2.9	78.1
1/4			4.8	76.2	1/4			2.8	78.2
cb			5.3	75.7	ϕ			2.4	78.6
E			5.7	75.3	1/4			1.8	79.2
			ϕ		cb			1.3	79.7
E			5.4	75.6	W			1.0	80.0
cb			4.8	76.2	T.P.	12.73	92.53	1.24	79.80

9253N line of				9253			
+	HZ	Elev		+	HZ	Elev	
	9253N	Line of	= 00		9253		
W	11.3	81.2	1/4		10.2	82.35	
cb	11.6	80.9	+8		10.6	81.9	
1/4	11.8	80.7	cb		11.4	81.1	
+5	13.0	79.5	+7		11.1	81.4	
ϕ	13.0	79.5	N ?		13.0	79.5	
1/4	13.3	79.2	+2		12.9	79.6	
cb	14.0	78.5	+4		11.7	80.8	
E	14.8	77.7	+10		12.0	80.5	
+10	15.2	77.3					
	0725		-10		0767		
70	13.5	79.0	E		10.4	82.1	
E	12.9	80.1	+3		9.7	82.8	
cb	12.0	80.5	+5		12.1	80.4	
+7	11.7	80.8	cb		10.3	82.2	
1/4	11.7	80.8	+3		10.3	82.2	
ϕ	10.7	81.8	1/4		9.5	83.0	
+5	10.7	81.8	ϕ		9.3	83.2	
1/4	9.9	82.6	+5		8.8	83.7	
cb	9.5	83.0	1/4		8.2	84.3	
W	9.0	83.5	cb		7.7	84.8	
	0750		N		6.8	85.7	
W	7.1	85.4			6.1	86.4	
cb	7.8	84.7	W				
1/4	8.4	84.1	cb		11.00		
+6	9.3	83.2	1/4		9.5	88.0	
ϕ	9.6	82.9	+5		5.1	87.4	
					5.7	86.8	
					6.1	86.4	

	HZ 92.53	Elev	
2	6.8	85.7	+3
t3	6.5	86.0	t7
1/4	6.9	85.6	cb
t5	7.2	85.3	E
cb	7.7	84.8	t10
t5	8.3	84.2	
E	8.6	83.9	-10
t10	8.7	83.8	E
	11.0		cb
-10	6.7	85.8	t3
E	6.1	86.4	t7
cb	5.4	87.1	1/4
1/4	5.1	87.4	2
t7	4.6	87.9	1/4
2	4.8	87.7	cb
1/4	4.3	88.2	T.P
t2	3.9	88.6	t8
cb	2.9	89.6	N.
N	2.4	90.1	
	11.50		N
N	1.4	91.1	cb
cb	2.0	90.5	1/4
1/4	2.4	90.1	2
2	3.0	89.5	t6
t3	3.0	89.5	1/4
1/4	3.8	88.7	t5

	HZ 92.53	Elev	
	3.5	89.0	6
	3.8	88.7	
	3.5	89.0	
	3.9	88.6	
	4.4	88.1	
	11.75		
	2.7	89.8	
	2.2	90.3	
	1.8	90.7	
	2.0	90.5	
	1.8	90.7	
	1.9	90.6	
	1.6	90.9	
	1.5	91.0	
	1.1	91.4	
12.26	104.14	0.65	91.88
	12.0	92.14	
	11.3	92.8	
	11.95		
	10.3	93.8	
	11.0	93.1	
	11.5	92.6	
	12.2	91.9	
	12.1	92.0	
	12.6	91.5	
	12.7	91.4	

HI
109.14

cb	12.4	91.7
E	12.9	91.2
+10	13.4	90.7
	2103 ⁵⁰ <i>Sline of Broadway</i> ^{80'51} _{4'62} _{131'95}	
-10	13.1	91.0
E	12.6	91.5
cb	11.9	92.2
+4	11.8	92.3
+5	12.2	91.9
1/4	12.0	92.1
+3	11.4	92.7
ϕ	11.2	92.9
+5	10.7	93.4
1/4	10.2	93.9
+5	9.5	94.6
cb	9.3	94.8
W	9.4	94.7
	<i>Sline +1</i>	
W	8.8	95.3
cb	8.6	95.5
1/4	9.2	94.9
ϕ	9.6	94.5
+2	9.6	94.5
+4	10.6	93.5
+7	10.3	93.8
1/4	10.9	93.2

HI
109.14

+5	11.2	92.97
cb	10.8	93.3
E	11.8	92.3
	5 cb	
E	10.5	93.6
cb	9.8	94.3
+5	10.1	94.0
1/4	10.3	93.8
+2	10.3	93.8
+4	9.6	94.5
ϕ	9.0	95.1
1/4	8.7	95.4
cb	8.2	95.9
W	8.1	96.0
	5 1/4	
W	7.2	96.9
cb	7.7	96.4
1/4	7.9	96.2
ϕ	8.3	95.8
+5	8.3	95.8
1/4	8.6	95.5
+5	8.2	95.9
cb	8.5	95.6
E	8.7	95.4
	ϕ	
E	7.6	96.5

HI
109.14

cb	7.6	96.5
1/4	7.5	96.6
Φ on Ground	7.6	96.5
Φ on Rim Marked	7.19	96.95 ✓
Flowline	14.19	99.95 ✓
+4	7.6	96.5
+5	7.1	97.0
1/4	6.8	97.3
cb	6.5	97.6
W	6.4	97.7
	N 1/4	
W	6.4	97.7
cb	6.6	97.5
1/4	6.7	97.4
Φ	6.6	97.5
1/4	6.8	97.3
+5	6.7	97.4
+7	6.3	97.8
cb	6.2	97.9
E	6.4	97.7
	N cb	
E	6.7	97.4
+6	6.2	97.9
cb	6.1	98.0
1/4	6.0	98.1
Φ	5.9	98.2

104.14

1/4	5.9	98.2 ⁸
cb	5.6	98.5
W	5.7	98.4
	N line of Broadway = 0.0	
W	4.6	99.5
+5	4.5	99.6
+7	5.1	99.0
cb	4.8	99.3
1/4	4.6	99.5
Φ	5.1	99.0
1/4	5.3	98.8
cb	5.3	98.8
+8	5.6	98.5
E	5.1	99.0
	check on starting 8M	4.86
		99.28
		<u>98.26</u>
	0.25	
E	3.5	100.6
+8	4.1	100.0
cb	4.6	99.5
1/4	4.3	99.8
Φ	4.1	100.0
1/4	3.9	100.2
+8	3.4	100.7
cb	3.4	100.7
W	3.2	100.9

42
10414

0750

N	2.4	101.7
cb	2.6	101.5
1/4	2.8	101.3
+3	3.4	100.7
+6	3.4	100.7
+8	3.0	101.1
⊕	3.1	101.0
1/4	3.4	100.7
cb	3.4	100.7
E	2.7	101.4

T.P.	12.32	115.87	0.59	103.55
------	-------	--------	------	--------

075

E	12.8	103.1
cb	13.2	102.7
+5	13.0	102.9
1/4	13.4	102.5
⊕	13.3	102.6
+4	14.0	101.1
+7	14.2	101.7
+8	13.4	102.5
1/4	13.4	102.5
+4	13.1	102.8
cb	13.0	102.9
N	11.6	104.3

11587

1700

N	10.5	105.4
cb	10.7	105.2
+8	11.4	104.5
1/4	11.7	104.2
+6	11.7	104.2
17	13.2	102.7
+9	13.0	102.9
⊕	11.7	104.2
1/4	11.6	104.3
+3	12.1	103.8
+8	12.0	103.9
cb	11.2	104.7
+4	11.0	104.9
E	11.0	104.9

1735

E	8.4	107.5
cb	8.8	107.1
1/4	8.7	107.2
⊕	8.5	107.4
1/4	8.0	107.9
cb	6.9	109.0
+5	6.4	109.5
N	5.9	110.0
N	5.8	110.1
cb	6.8	109.1

1740 S. Line of Alley

115.87

1/4	7.5	108.4
ϕ	8.3	107.6
1/4	8.3	107.6
cb	8.3	107.6
E	8.2	107.7
1150 ϕ Alley		
E	7.7	108.2
cb	7.9	108.0
1/4	8.0	107.9
+3	7.5	108.4
ϕ	7.5	108.4
ϕ on Rim	7.08	108.1 ✓
Flow Line	12.00	103.87 ✓
1/4	6.5	109.4
+4	6.0	109.9
cb	5.7	110.2
W	4.7	111.2
1160 N. Line of Alley		
W	3.8	112.1
cb	5.1	110.8
1/4	5.7	110.2
ϕ	6.0	109.9
+5	7.5	108.4
1/4	7.6	108.3
+7	7.4	108.5
cb	7.1	108.8

HZ
115.87

+5	6.8	109.1	10
E	6.9	109.0	
1180			
E	5.0	110.9	
+7	5.9	110.5	
cb	5.7	110.2	
+3	6.0	109.9	
+5	6.6	109.3	
+7	6.6	109.3	
+8	5.9	110.0	
1/4	6.0	109.9	
+9	6.1	109.8	
+5	5.6	110.3	
+9	5.4	110.5	
ϕ	4.9	111.0	
+5	4.9	111.5	
+8	4.1	111.8	
1/4	4.1	111.8	
+7	3.8	112.1	
cb	3.5	112.4	
W	2.4	113.5	
1188			
W	2.1	113.8	
cb	3.1	112.8	
1/4	3.7	112.2	
+3	4.7	111.2	

H.Z.
115.87

111.47

H.Z.
127.49

Φ		5.1	110.8	+7	
1/4		5.3	110.6	+9	
+5		5.5	110.4	1/4	
06		4.9	111.0	+6	
+3		4.4	111.5	06	
E		3.9	112.0	+3	
	2100			E	
E		2.5	113.4		
+6		2.8	113.1	E	
06		3.8	113.1	+6	
+5		4.4	111.5	06	
1/4		4.3	111.6	+3	
Φ		4.2	111.7	1/4	
+8		4.0	111.9	+7	
+9		3.0	112.9	Φ	
1/4		3.0	112.9	+2	
06		2.1	113.8	+3	
W		1.5	114.4	1/4	
J.P.	12.50	127.49	0.88	114.99	06
		2125		+3	
W		1.8	115.7	W	
06		12.9	114.6		
+6		13.4	114.1	W	
1/4		13.3	114.2	+5	
+5		13.0	114.5	06	
Φ		13.2	114.3	+5	

	14.2	113.31
	14.3	113.2
	13.8	113.7
	13.4	114.1
	12.5	115.0
	11.9	115.6
	11.2	116.3
	2150	
	9.1	118.4
	9.5	118.0
	10.0	117.5
	10.5	117.0
	10.5	117.0
	10.8	116.7
	11.5	116.0
	11.2	116.3
	10.5	117.0
	10.3	117.2
	11.6	115.9
	1.4	116.1
	10.1	117.4
	2175	
	9.1	118.4
	9.5	118.0
	9.1	118.4
	8.1	119.4

H.I.
127.49

H.I.
127.49

12

14	8.0	119.5	cb
+5	7.9	119.6	1/4
ϕ	8.8	118.7	+5
+1	7.9	119.6	ϕ
1/4	7.2	120.3	+5
cb	6.6	120.9	+8
+5	5.6	121.9	1/4
E	5.3	122.2	T.P.
	3700 S. Line of 'C'		cb
E	0.8	126.7	+4
+5	1.1	126.4	E
cb	2.1	125.4	
+2	2.5	125.0	E
1/4	2.8	124.7	+6
+4	3.4	124.1	cb
ϕ	4.2	123.3	1/4
1/4	5.0	122.5	ϕ
cb	6.1	121.4	1/4
W	7.7	119.8	cb
+5	7.0	120.5	W
+6	6.3	121.2	+5
+10	5.8	121.7	+16
	5.6	122.43	+15
-10	5.2	122.3	
-5	6.0	121.5	-20
W	5.3	122.2	-10

50' of
14' cb
15' 1/4

	11.46	138.59	0.36	127.13
			11.4	127.2
			10.1	128.5
			9.8	128.8
			5 1/4	
			7.7	130.9
			8.0	130.6
			9.6	129.0
			9.8	128.8
			11.0	127.6
			11.7	126.9
			12.7	125.9
			15.1	123.5
			16.3	122.3
			15.4	123.2
			14.8	123.8
			ϕ	
			12.9	125.7
			14.5	124.1

HZ
13859

W		139	124.7
cb		10.7	127.9
T.P.	6.68	14959	0.73 157.86
1/4		15.3	129.2
+5		15.0	129.5
φ		14.8	129.7
1/4		13.9	130.6
cb		13.1	131.4
+5		12.1	132.4
E		11.9	132.6
		N 1/4	
E		10.2	134.3
+6		10.1	134.4
cb		11.2	133.3
1/4		12.4	132.1
+6		12.6	131.9
φ		13.4	131.1
1/4		13.7	130.8
+7		14.3	130.2
cb		14.8	129.7
W		17.1	127.4
+20 no slope		17.8	126.7
+25		16.3	128.2
		N.C.B.	
-25		15.2	129.3
-20		16.7	127.8

HZ
14959

-5		16.7	127.8
W		15.4	129.1
cb		13.3	131.2
+3		12.8	131.7
1/4		11.9	132.6
+5		11.6	132.9
+6		12.4	132.1
φ		12.0	132.5
+3		11.8	132.7
+4		11.0	133.5
1/4		10.4	134.1
+9		9.5	135.0
cb		8.8	135.7
E		8.8	135.7
		N line of "c" = 00	
E		7.0	137.5
+8		7.2	137.3
cb		7.8	136.7
1/4		8.4	136.1
+5		9.0	135.5
φ		9.8	134.7
+4		10.4	134.1
+5		9.3	135.2
1/4		9.9	134.6
+5		10.4	134.1
cb		11.3	133.2

13

+

HI
14459

-

ERV

+5	12.5	132.0
W	13.6	130.9
+15	15.7	128.8
+25	19.3	130.2
	0+25	
-30	9.8	134.7
-20	12.1	132.4
-10	11.1	133.4
W	9.4	135.1
cb	7.3	138.2
+5	6.6	137.9
1/4	5.9	138.6
+5	5.5	139.0
+6	6.9	137.6
1/2	5.5	139.0
1/4	4.9	139.6
+5	9.5	140.0
cb	4.3	140.2
E	3.8	140.7
	0+38	
E	2.6	141.9
cb	3.0	141.5
1/4	3.4	141.1
+9	4.1	140.4
1/2	4.5	140.0
+5	4.8	139.7

+

HI
14459

14

+7	3.9	140.6
1/4	4.2	140.3
cb	5.1	139.4
W	6.8	137.7
110	9.1	135.4
+20	10.7	133.8
+30	9.3	135.2
	0+50	
-30	8.4	136.1
-20	7.5	137.0
-10	6.8	137.7
W	4.8	139.7
cb	3.7	140.8
1/4	2.9	141.6
+7	2.8	141.7
1/2	3.3	141.2
+3	2.6	141.9
1/4	2.3	142.2
+5	2.0	142.5
cb	1.6	142.9
E	1.1	143.4
T.P.	11.09	155.03
	0.60	143.94
	0+75	
E	8.9	146.1
cb	8.7	146.3

H.I.
155.03

+3	9.5	145.5
+7	9.6	145.4
1/4	10.1	144.9
+3	10.3	144.7
+5	11.0	144.0
ϕ	9.9	145.1
+6	9.8	145.2
+7	10.8	144.2
1/4	10.1	144.9
cb	10.3	144.7
N	10.7	144.3
+10	11.8	143.2
+20	13.0	142.0
	11.00	
-20	8.0	147.0
1-10	7.3	147.7
N	6.8	148.2
cb	6.9	148.1
+5	7.0	148.0
+8	6.5	148.5
1/4	6.6	148.4
ϕ	6.9	148.6
+2	6.6	148.4
+5	7.1	147.9
+8	7.7	147.3
1/4	7.6	147.4

H.I.
155.03

+3	7.3	147.15
cb	6.4	148.6
+2	5.9	149.1
5	6.1	148.9
	11.15	
5	4.5	150.5
+7	4.4	150.6
+8	5.7	149.3
cb	5.6	149.4
+8	5.8	149.2
1/4	5.2	149.8
+2	5.1	149.9
+4	4.6	150.4
ϕ	4.3	150.7
1/4	4.1	150.9
cb	4.1	150.9
+2	4.6	150.4
+9	4.4	150.6
N	5.2	149.8
+10	4.5	150.5
	11.25	
-10	2.1	152.9
N	2.5	152.5
+5	3.2	152.8
cb	2.4	152.6
1/4	2.7	152.3

H.I.
155.03

¢	3.0	152.0
+6	3.3	151.7
1/4	4.0	151.0
+2	4.3	150.7
+5	4.7	150.3
+8	4.6	150.4
cb	5.0	150.0
+3	4.7	150.3
+4	4.0	151.0
E	3.9	151.1

1+40 S. Line of Alley

E	3.2	151.8
+5	3.1	151.9
cb	3.2	151.8
+5	2.6	152.4
1/4	1.8	153.2
¢	0.7	154.3
1/4	0.2	154.8
T.P.	12.27	166.88
	0.42	159.61
+6	11.6	155.3
cb	11.7	155.2
W	11.2	155.7

1+60 N. Line of Alley

W	7.6	159.3
cb	8.2	158.7
1/4	8.6	158.3

H.I.
166.88

16

¢	9.5	157.4
+8	10.0	156.9
1/4	10.6	156.3
cb	12.3	154.6
+5	12.7	154.2
+8	13.4	153.5
E	12.9	154.0
+10	13.3	153.6
+20	14.1	152.8
	14.5	

-20	13.1	153.8
-15	11.9	155.0
-10	11.7	155.2
E	11.4	155.5
+5	10.6	156.3
cb	10.0	156.9
1/4	8.9	158.0
¢	7.5	159.4
1/4	6.1	160.8
cb	5.5	161.4
W	5.0	161.9
	14.7	

W	2.9	164.0
cb	3.6	163.3
1/4	4.6	162.3
¢	5.8	161.1

HI
166.88

1/4		71	159.8	
cb		8.9	158.5	
+3		9.2	157.7	
E		10.1	156.8	
+10		10.8	156.1	
+20		11.3	155.6	
		2+100		
-20		10.4	156.5	
-10		9.8	157.1	
-3		8.7	158.2	
E		8.7	158.2	
+5		7.5	159.4	
cb		6.8	160.1	
1/4		5.2	161.7	
¢		4.0	162.9	
1/4		2.7	164.2	
cb		1.4	165.5	
N		0.2	166.7	
TP	12.66	179.03	0.51	166.37
		2+15		
N		9.6	169.4	
cb		10.9	168.1	
1/4		12.8	166.2	
¢		14.2	165.8	
1/4		15.4	163.6	

HI
179.03

cb		16.9	162.1 ¹⁷
E		18.5	160.5
+10		20.0	159.0
+20		21.2	157.8
+30		22.6	156.4
		2+25	
-30		21.4	157.6
-20		19.7	159.3
-10		18.7	160.3
E		17.4	161.6
cb		16.0	163.0
1/4		14.3	164.7
¢		12.8	166.2
1/4		11.0	168.0
cb		9.4	169.6
N		8.5	170.5
		2+50	
N		6.2	172.8
cb		7.2	171.8
1/4		8.2	170.8
¢		9.8	169.2
1/4		11.9	168.1
cb		13.8	165.2
E		15.4	163.6
+10		16.6	162.4
+20		17.7	161.3

HI
179.03

+30	18.9	160.1
	27.75	
-30	16.5	162.5
-20	15.3	163.7
-10	14.4	164.6
E	13.4	165.6
+5	12.5	166.5
cb	11.1	167.9
+5	9.6	169.4
1/4	8.5	170.5
¢	7.0	172.0
1/4	5.8	173.2
cb	4.9	174.1
N	3.6	175.4

3400 Skins of 'B'

80.51
19.065
13.114

W	1.0	178.0
+5	1.5	177.5
cb	2.7	176.3
1/4	4.0	175.0
¢	5.4	173.6
1/4	6.7	172.3
cb	8.8	170.2
+5	10.3	168.7
E	11.2	167.8
+10	12.0	167.0
+20	13.1	165.9

+ HI
179.03

+30	13.8	165.2
	5.26	
E	9.8	169.2
+6	8.7	170.3
+7	7.7	171.3
cb	7.2	171.8
1/4	5.8	173.2
¢	4.6	174.4
1/4	3.1	175.9
cb	1.8	177.2
+5	0.6	178.4
N	0.1	178.9

TP. 11.72 190.01 0.74 178.29

5 1/4

N	10.3	179.7
cb	12.0	178.0
1/4	13.2	176.8
¢	14.3	175.7
1/4	15.3	174.7
cb	17.0	173.0
+5	18.9	171.6
E	19.4	170.6
	¢	
E	18.1	171.9
+3	18.1	171.9

18

H.I.
190.01

t5	17.4	172.6	1/4
t8	17.1	172.9	cb
cb	15.9	174.1	N
1/4	14.7	175.3	
2	13.5	176.5	W
1/4	12.6	177.4	cb
cb	11.6	178.4	1/4
t5	10.5	179.5	2
N	9.9	180.1	1/4
	N 1/4		t5
W	8.9	181.1	cb
cb	10.4	179.6	t3
1/4	12.2	177.8	t8
2	13.2	176.8	E
1/4	14.1	175.9	t10
cb	15.6	174.4	t20
t5	16.7	173.3	
E	16.9	173.1	-20
	N-cb		E
E	15.7	174.3	cb
t5	15.4	174.6	t4
t6	15.8	174.2	1/4
cb	15.0	175.0	t5
t6	13.0	177.0	2
1/4	13.0	177.0	1/4
2	12.1	177.9	cb

H.I.
190.01

19

11.3	178.7
9.7	180.3
8.2	181.8
N line of B = 00	
7.4	182.6
9.1	180.9
10.4	179.6
11.4	178.6
12.2	177.8
12.8	177.2
14.4	175.6
13.9	176.1
14.0	176.0
13.8	176.2
15.3	174.7
15.6	174.4
0+25	
13.2	176.3
11.6	178.4
11.0	179.0
11.4	178.6
11.2	178.8
11.2	178.8
9.9	180.1
8.9	181.1
7.6	182.4

+

4I
19001

W	6.2	183.8	1/4
	0+50		cb
X	4.7	185.3	E
tb	5.3	184.7	+10
cb	6.3	183.7	
1/4	7.4	182.6	-10
ϕ	8.2	181.8	E
1/4	9.0	181.0	cb
cb	9.6	180.4	1/4
+8	10.3	179.7	ϕ
E	9.9	180.1	1/4
+10	9.8	180.2	cb
	0+67		W
-10	8.6	181.4	
E	8.5	181.5	W
cb	8.3	181.7	cb
1/4	7.5	182.5	1/4
ϕ	6.4	183.6	ϕ
1/4	5.4	184.6	1/4
cb	4.6	185.4	cb
W	4.1	185.9	E
	0+75		+10
W	3.2	186.8	
cb	4.0	186.0	-10
1/4	4.9	185.1	E
ϕ	5.7	184.3	cb

+

4I
190.01

20

	6.7	183.3	
	7.5	182.5	
	7.9	182.1	
	8.2	181.8	
	1400		
	7.0	183.0	
	6.4	183.6	
	5.9	184.1	
	5.2	184.8	
	4.6	185.4	
	3.9	186.1	
	3.3	186.7	
	2.7	187.3	
	1425		
	2.8	187.2	
	3.6	186.4	
	4.3	185.7	
	5.0	185.0	
	5.6	184.4	
	6.0	184.0	
	6.7	183.3	
	7.2	182.8	
	1440		
	8.3	181.7	
	7.3	182.7	
	6.5	183.5	

	+	HZ 190.01	Elev
1/4		5.8	184.2
ϕ		5.3	184.7
1/4		4.8	185.2
cb		4.2	185.8
W		3.3	186.7
		1160. N line of Alley	
W		4.6	185.4
cb		5.1	184.9
1/4		5.7	184.3
ϕ		6.4	183.6
1/4		7.5	182.5
cb		8.4	181.6
E		9.3	180.7
+10		10.0	180.0
		1175	
-10		11.3	178.7
E		10.1	180.9
cb		9.8	180.2
1/4		8.9	181.1
ϕ		7.9	182.1
1/4		6.9	183.1
cb		6.0	184.0
W		5.2	184.8
		2100	
W		8.1	181.9
cb		8.9	181.1

	+	HZ 190.01		
1/4		9.8	180.2	21
ϕ		10.4	179.6	
1/4		11.1	178.9	
cb		11.8	178.2	
E		12.7	177.3	
+10		13.3	176.7	
+20		14.2	175.8	
T.P.	3.41	180.25	13.17	176.84
		2135		
-20		9.2	171.1	
-10		8.2	172.1	
E		7.1	173.2	
cb		6.0	174.3	
1/4		5.1	175.2	
ϕ		4.2	176.1	
1/4		3.4	176.9	
cb		2.7	177.6	
W		2.2	178.1	
		2150		
W		3.8	176.5	
cb		4.6	175.7	
1/4		5.3	175.0	
ϕ		6.1	174.2	
1/4		7.2	173.1	
cb		8.0	172.3	
E		9.0	171.3	

	+	HI 18025	-	
t10			10.2	170.1
t20			11.1	169.2
			2175	
-20			14.8	165.5
-10			14.1	166.2
E			13.3	167.0
cb			12.6	167.7
1/4			11.4	168.9
1/2			10.3	170.0
1/4			9.2	171.1
cb			8.3	172.0
N			7.6	172.7
T.P.	4.58	173.15	11.68	168.57
			2190	
N			4.8	168.4
cb			5.2	168.0
1/4			6.2	167.0
1/2			7.0	166.2
1/4			7.7	165.5
cb			8.2	165.0
E			8.6	164.6
t10			9.5	163.7
t20			10.3	162.9
			3101 ⁸⁰	S. Line of A
-20			12.2	161.0
-10			11.4	161.8

	+	HI 173.15	-	E/e	
E			11.0	162.2	22
cb			9.9	163.3	
1/4			9.2	164.0	
1/2			8.7	164.5	
1/4			8.3	164.9	
cb			7.7	165.5	
N			6.9	166.3	
			11.17	161.98	
			Set BM. SE Prop Cor. 39 1/2 A		
T.P.	12.44	184.25	1.34	171.81	
TP	116	183.74	167	182.58	
TP	0.29	171.20	12.83	170.91	
TP	2.18	160.38	13.00	158.20	
TP	0.60	148.04	12.94	147.94	
			10.17	137.87	
				137.89	
				0.02	

B. Bhs S
9/5/29

st.
X Section 35th Lemon Grove Blvd
to the S. line of B³
60' st
10' cbs
10' 1/2"
N.E. B.P.
Lemon Grove
Blvd. 39th

H.I.
56.92

				1/4	4.7	52.2
BM	0.22	61.84	61.62	cb	4.9	52.0
TP	4.42	56.92	52.50	E	5.2	51.7
		0700			0750	
	on paving					
W		4.9	52.0	E	5.8	51.1
W Top cb		5.16	51.76	+5	5.3	51.6
G		5.68	51.24	cb	5.1	51.8
1/4		5.21	51.71	1/4	4.9	52.0
⊥		4.97	51.95	⊥	4.8	52.1
1/4		5.09	51.83	1/4	4.9	52.0
G		5.32	51.60	cb	5.0	51.9
E Top cb		4.69	52.23	W	5.0	51.9
E		4.9	52.0		0790	
		0710		W	5.2	51.7
E		5.0	51.9	cb	5.4	51.5
cb		5.2	51.7	1/4	5.2	51.7
1/4		4.8	52.1	⊥	5.2	51.7
⊥		4.9	52.0	1/4	5.4	51.5
1/4		5.0	51.9	cb	5.3	51.6
cb		5.1	51.8	E	5.5	51.4
W		4.9	52.0		1100	
		0725		E	5.1	51.8
W		4.9	52.0	cb	5.2	51.7
cb		5.0	51.9	1/4	5.3	51.6
1/4		5.0	51.9	⊥	5.1	51.8
⊥		4.7	52.2	1/4	5.3	51.6

Plotted 4/16-29 C.B.H.
Reductions British

H.I.
56.92

cb	5.3	51.6
N	5.1	51.8
	1450	
N	4.3	52.6
cb	4.4	52.5
ts	4.1	52.8
1/4	4.3	52.6
¢	4.6	52.3
1/4	4.9	52.0
cb	4.9	52.0
E	4.6	52.3
	2100	5 line of E.
E	4.6	52.3
cb	4.7	52.2
1/4	4.5	52.4
¢	4.1	52.8
1/4	4.0	52.9
cb	3.6	53.3
N	3.4	53.5
	5cb	
N	3.5	53.4
cb	3.6	53.3
1/4	3.7	53.2
¢	3.9	53.0
1/4	4.5	52.4
cb	4.6	52.3

50/57
10 2/45
25/45

+

H.I.
56.92

E	4.6	52.3
	5/4	
E	4.9	52.0
cb	4.6	52.3
1/4	4.4	52.5
¢	4.0	52.9
1/4	3.9	53.0
cb	3.9	53.5
N	3.4	53.5
	¢	
N	3.2	53.7
cb	3.5	53.4
1/4	3.8	53.1
¢	4.1	52.8
1/4	4.6	52.3
cb	4.8	52.1
E	5.0	51.9
	N/4	
E	4.7	52.2
cb	4.6	52.3
1/4	4.6	52.3
¢	3.9	53.0
1/4	3.7	53.2
cb	3.4	53.5
N	3.2	53.7

Elev

20

+

H.I.
6081

Elev

H.I.
6081

26

cb	5.1	55.7
1/4	4.8	56.0
ϕ	5.0	55.8
1/4	4.8	56.0
cb	4.9	55.9
E	5.2	55.6
	5.06	
E	5.9	54.9
cb	5.5	55.3
76	5.5	55.3
1/4	4.7	56.1
ϕ	4.4	56.4
1/4	4.8	56.0
cb	4.8	56.0
N	4.8	56.0
	5/4	
N	4.4	56.4
cb	4.3	56.5
1/4	4.8	56.0
ϕ	4.8	56.0
1/4	4.9	55.9
74	5.5	55.3
cb	5.4	55.4
E	5.5	55.3
	ϕ	
E	5.4	55.4

cb	5.3	55.5
1/4	5.0	55.8
ϕ	4.8	56.0
ϕ Pin Mo. Hole	4.73	56.08 ✓
1/4	4.4	56.4
cb	4.4	56.4
N	4.5	56.3
	N 1/4	
N	4.4	56.4
cb	4.5	56.3
1/4	4.6	56.2
ϕ	4.4	56.4
1/4	4.6	56.2
cb	4.9	55.9
E	5.0	55.8
	N cb	
E	4.8	56.0
cb	4.8	56.0
1/4	4.5	56.3
ϕ	4.5	56.3
1/4	4.7	56.1
cb	4.5	56.3
N	4.4	56.4
	9.17	56.64
	N Line of Broadway = 00	
N	4.4	56.4
cb	4.5	56.3

	H.I.	-	Elev
	6081		
1/4		4.6	56.2
2		4.5	56.3
1/4		4.3	56.5
cb		4.5	56.3
E		4.6	56.2

0+50

E		4.4	56.4
cb		4.2	56.6
1/4		3.9	56.9
2		3.7	57.1
1/4		4.2	56.6
cb		4.2	56.6
W		4.2	56.6

1+00

W		3.1	57.7
cb		3.3	57.5
1/4		3.5	57.3
2		3.5	57.3
1/4		3.6	57.2
cb		3.4	57.4
E		3.7	57.1

T.P. 7.59 65.68 2.72 58.09

1+40

E		7.9	57.8
cb		7.8	57.9

	H.I.		27
	65.68		
1/4		8.2	57.5
2		7.9	57.8
1/4		7.6	58.1
cb		7.7	58.0
W		7.5	58.2

1+60 N-line Alley

W		6.9	58.8
cb		7.3	58.4
1/4		7.4	58.3
2		7.0	58.7
1/4		7.8	57.9
cb		7.7	58.0
E		7.4	58.3

2+00

E		7.5	58.2
cb		7.0	58.7
1/4		6.9	58.8
2		6.9	58.8
1/4		6.9	58.8
cb		7.0	58.7
E		6.8	58.9
W		6.4	59.3

2+50

W		5.9	59.3
cb		6.1	59.6
1/4		6.2	59.5

+

HI
6568

Elev

+

HI
6568

scb

28

φ	5.9	59.8
1/4	5.8	59.9
+5	7.0	58.7
cb	7.4	58.3
E	7.3	58.4
	2+75	
E	8.8	56.9
cb	8.8	56.9
+5	7.3	58.4
1/4	5.4	60.3
+5	4.1	61.6
φ	5.8	59.9
1/4	5.9	59.8
cb	5.6	60.1
W	5.4	60.3
	3+00.5 line of c	^{50.5} 19'cb 15'1/4
W	5.0	60.7
+5	5.0	60.7
cb	5.5	60.2
1/4	5.8	59.9
φ	6.0	59.7
+5	5.7	60.0
1/4	5.6	60.1
+5	7.2	58.5
cb	8.0	57.7
+5	6.8	58.9
E	8.1	57.6

E

+5

cb

1/4

φ

+7

1/4

cb

W

W

cb

1/4

φ

1/4

cb

E

+10

+20

-20

-10

E

+5

cb

7.2

6.6

7.2

6.6

6.0

5.3

5.4

5.1

5.1

5/4

5.1

4.7

5.0

5.6

6.4

6.6

7.1

7.5

8.3

φ

7.6

7.8

8.0

6.8

6.8

58.5

59.1

58.5

59.1

59.7

60.4

60.3

60.6

60.6

60.6

61.0

60.7

60.1

59.3

59.1

58.6

58.2

57.4

58.1

57.9

57.7

58.9

58.9

H.I.
6568

+7	6.8	58.9	1/4
1/4	5.5	60.2	cb
+3	4.4	61.3	N
ϕ	4.6	61.1	
1/4	4.6	61.1	N
cb	4.5	61.2	cb
N	4.4	61.3	+5
	N 1/4		1/4
N	4.2	61.5	ϕ
cb	4.0	61.7	+4
1/4	4.3	61.4	+5
ϕ	4.4	61.3	1/4
+7	4.2	61.5	cb
1/4	5.8	59.9	+5
+5	6.3	59.4	E
cb	8.1	57.6	+20
E	8.1	57.6	
+20	8.1	57.6	-20
	Ncb		E
-20	7.4	58.3	cb
E	7.3	58.4	+5
cb	8.2	57.5	1/4
1/4	7.8	57.9	+3
+5	7.0	58.7	ϕ
+6	4.2	61.5	+5
ϕ	4.3	61.4	+7
			1/4

H.I.
6568

4.4	61.3	29
3.8	61.9	
3.9	61.8	
N. cb +5		
3.8	61.9	
3.7	62.0	
4.4	61.3	
4.3	61.4	
4.5	61.2	
7.7	61.0	
7.7	58.0	
8.3	57.4	
7.3	58.4	
7.0	58.7	
7.1	58.6	
N. line of "C"		
6.9	58.8	
6.9	58.8	
7.1	58.6	
8.4	57.3	
8.2	57.5	
7.7	58.0	
7.4	58.3	
7.2	58.5	
4.1	61.6	
4.0	61.7	

H.I.
6568

cb	3.9	61.8
N	3.6	62.1
	0+13	
N	3.5	62.2
+7	3.9	61.8
cb	4.4	61.3
+6 Top	4.7	61.0
+6 Bottom	6.8	58.9
1/4	7.3	58.4
2	7.5	58.2
+4	8.4	57.3
+6	7.6	58.1
1/4	7.2	58.5
cb	6.8	58.9
E	6.5	59.2
+20	6.8	58.9
L	0+31	
-20	6.7	59.0
E	6.3	59.4
cb	6.3	59.4
1/4	6.6	59.1
2	7.1	58.6
1/4	7.6	58.1
cb	6.7	59.0
+9	6.8	58.9
N	3.8	61.9

+

H.I.
6568

	0+33	30
N	7.0	58.7
cb	6.8	58.9
1/4	7.5	58.2
2	6.8	58.9
1/4	6.1	59.6
cb	6.3	59.4
E	6.7	59.0
+20	6.7	59.0
	0+50	
-20	7.3	58.4
-10	7.3	58.4
E	6.2	59.5
cb	6.0	59.7
1/4	6.3	59.4
2	6.8	58.9
+9	6.8	58.9
1/4	7.3	58.4
+9	7.0	58.7
+7	6.0	59.7
cb	5.8	59.9
N	6.0	59.7
+8 Bottom	6.6	59.1
+8 Top	3.6	62.1
	0+25	
-14 Top	3.6	62.1

H.Z.
6568

-13 Bottom	6.2	59.5
W	5.5	60.2
cb	5.9	60.3
1/4	6.4	59.3
φ	6.4	59.3
1/4	6.3	59.4
cb	7.0	58.7
E	6.5	59.1
+20	6.1	59.6

1100

-20	6.1	59.6
-15	5.3	60.4
E	5.4	60.3
cb	5.8	59.9
1/4	6.8	58.9
φ	6.6	59.1
1/4	6.1	59.6
+5	5.3	60.4
cb	5.1	60.6
W	5.2	60.5
+12 Bottom	5.7	60.0
+13 Top	3.1	62.6

1125

-9 Top	2.6	63.1
-9 Bottom	4.9	60.8
W	4.9	60.8

H.Z.
6568

31

5.2	60.5
5.7	60.0
5.8	59.9
6.7	59.0
6.4	59.3
6.1	59.6
5.9	60.3
5.4	60.3
4.9	60.8

1140 S. Line of Alley

-20	4.9	60.8
E	4.5	61.2
cb	5.1	60.6
+5	5.5	60.2
+7	6.4	59.3
1/4	6.5	59.2
φ	6.5	59.2
1/4	6.4	59.3
+5	6.1	59.6
+7	5.5	60.2
cb	5.3	60.4
W	5.0	60.7
+13 Bottom	5.0	60.7
+4 Top	2.1	63.6

1153 Mn. Hole

φ on Rib

4.62 61.06 ✓

H.I.
6568

1+60 N. line of Alley

+2 Top	1.7	64.0
-1 Bottom	4.8	60.9
W	4.8	60.9
+5	5.7	60.0
cb	5.8	59.9
1/4	5.2	60.5
+7	4.9	60.8
ϕ	5.3	60.4
+5	5.8	59.9
1/4	6.1	59.6
+5	6.0	59.7
cb	4.3	61.4
E	4.4	61.3
+20	4.5	61.2
	1+15 Tree on West	
-20	9.1	61.6
E	3.8	61.9
cb	4.2	61.5
+1	5.8	59.9
1/4	6.1	59.6
+4	5.8	59.9
+5	5.2	60.5
ϕ	7.7	61.0
1/4	4.5	61.2
+5	4.6	61.1
cb	5.5	60.2

H.I.
6568

32

W	5.3	60.4
+1 Top Bank	1.4	64.3
	2+00	
W. Top Bank	1.6	64.1
W. Bottom Bank	4.2	61.5
+5	5.5	60.2
cb	5.6	60.1
+3	5.0	60.7
1/4	4.9	61.3
ϕ	4.1	61.6
1/4	4.5	61.2
+7	4.6	61.1
cb	5.8	59.9
+7	6.0	59.7
E	5.3	60.4
+2 Bottom Bank	4.9	60.8
+5	3.5	62.2
+20	3.5	62.2
	2+15	
-20	2.8	62.9
-10	5.6	60.1
E	5.6	60.1
+2	4.5	61.2
cb	4.3	61.4
1/4	4.0	61.7
ϕ	4.1	61.6

H.I.
6568

1/4		4.7	61.0
t5		5.3	60.4
cb		5.2	60.5
t4		4.2	61.5
t5		1.3	64.4
W		1.3	64.4
T.P.	560	70 30 098	64.70
		1150	
W		5.1	65.2
cb		5.3	65.0
1/4		5.2	65.1
t7		5.2	65.1
Φ		7.3	63.0
t5		8.9	61.4
1/4		9.2	61.1
t7		9.0	61.3
cb		8.5	61.8
E		8.5	61.8
t20		9.0	61.3
		1175	1733 trees
-20		8.7	61.6
E		9.2	61.1
t5		9.2	61.1
t6		8.2	62.1
t7		5.1	65.2
cb		5.0	65.3

1777 tree H.I.
1787 tree 7030

1/4		4.8	65.5 ³³
Φ		4.5	65.8
1/4		4.8	65.5
cb		4.4	65.9
W		4.4	65.9
		3100. S line of B.	
W		3.8	66.5
cb		3.7	66.6
1/4		3.9	66.4
Φ		4.0	66.3
1/4		4.2	66.1
cb		4.2	66.1
E		4.3	66.0
t21. E dge Bank		4.8	65.5
t22 Bottom of		6.2	64.1
T.P.	4.81	64.35	1076 59.54
check on B.M. NW Mar. 25 th Broadway		7.67	56.98
			56.92
			0.06 error

"B" St

34

"B" St

Street

St.

300'

80'

300'

80'

209.94

35 7/8

50'

200'

BM NW 5187

300'

80'

300'

80'

203.50

50'

200'

BM Mon Elev 137.89

600.10

BM Mon Elev 99.29

STO 220 RW 11/6

PO 1/2" RW 11/6

600.20

BM Mon NW Elev 56.62

D or Broadway

E St

34 1/2

Lemon

Grove

BM NE BP Elev 41.60

Blvd

Bill Bliss
April 6, 1919

X. Section Broadway 34th to 35th

+ HI - Elev
100.86

35

	+	HI	-	Elev	N		Elev
BM	160	100.86		99.26	76	2.6	98.3
					cb	2.6	98.3
			0400. E. line of 34 th		cb	3.6	97.3
N			2.1	98.8	t8	4.2	96.7
t5			2.3	98.6	1/4	4.7	96.2
cb			3.5	97.4	t2	4.4	96.5
t11			3.1	97.8	t4	5.1	95.8
1/4			4.0	96.9	t	5.7	95.2
t			4.6	96.3	1/4	6.9	94.0
1/4			5.6	95.3	t7	7.7	93.2
cb			7.2	93.7	cb	8.7	92.2
S			9.5	91.4	S	10.6	90.3
			0410		t15	11.5	89.4
S			9.8	91.1		0442	
cb			7.6	93.3	-15	12.4	88.5
1/4			6.0	94.9	S	11.2	89.7
t			5.1	95.8	cb	10.0	90.9
t7			4.5	96.4	1/4	8.0	92.9
t10			3.8	97.1	t8	7.0	93.9
1/4			3.5	97.4	t	6.6	94.3
t8			4.0	96.9	t9	6.7	94.2
t11			3.4	97.5	1/4	5.4	95.5
cb			3.2	97.7	t8	4.7	96.2
t7			2.2	98.7	t10	4.3	96.6
N			2.1	98.8	cb	4.0	96.9
			0425		N	3.5	97.4

Plotted 4-16-29 - C.B.H.
Reduced by Britton

NE Corner
Broadway + 34th
80.51
19.065
12.49

	H.I. 10086	Elev
	0+50	
N	40	96.9
cb	4.8	96.1
+4	4.7	96.2
+8	5.8	95.1
1/4	6.3	94.6
+9	6.3	94.4
ϕ	7.1	93.8
+5	7.4	93.8
1/4	8.3	92.6
cb	10.0	90.9
S	11.4	89.5
+15	12.9	88.0
	0+75	
-15	14.4	86.5
S	12.4	88.5
cb	11.3	89.6
+11	9.7	91.2
1/4	9.4	91.5
+10	9.4	91.5
ϕ	9.0	91.9
+8	8.8	92.1
1/4	8.7	92.2
+10	8.0	92.9
cb	7.4	93.5
N	6.5	94.4

	H.I. 10086	Elev
	1+00	36
N	7.5	93.4
cb	8.5	92.4
+10	9.1	91.8
1/4	10.0	90.9
+7	10.1	90.8
ϕ	9.8	91.1
+5	10.6	90.3
1/4	11.0	89.9
cb	12.2	88.7
S	13.2	87.7
+15	14.7	86.2
	1+25	
-15	16.2	84.7
S	14.4	86.5
cb	13.3	87.6
1/4	12.3	88.6
ϕ	11.2	89.7
+6	11.7	89.2
1/4	10.9	90.0
+2	10.5	90.4
+7	10.4	90.5
cb	9.6	91.3
N	8.9	92.0
	1+50	
N	10.4	90.5

	+	H.I. 100.86	-	Elev
cb			110	89.9
1/4			117	89.2
+9			13.0	87.9
T.P.	2.69	90.73	12.82	88.04
8			2.6	88.1
+3			2.3	88.4
1/4			3.4	87.3
cb			4.3	86.4
S			5.2	85.5
+15			6.7	84.0
			11.75	
-15			7.7	83.0
-5			6.2	84.5
S			6.1	84.6
cb			5.8	84.9
+5			5.2	85.5
1/4			4.6	86.1
8			3.9	86.8
+9			3.8	86.9
1/4			3.0	87.7
cb			2.0	88.7
N			0.7	90.0
			24.00	
N			1.9	88.8
cb			2.8	87.9
+5			3.1	87.6

	H.I. 90.73		Elev
			86.8 ³⁷
			86.9
			85.9
			85.8
			85.2
			85.5
			84.9
			84.4
			83.7
			83.1
			81.8
		24.15	
			81.2
			82.9
			83.6
			84.1
			83.6
			84.1
			84.2
			85.4
			85.7
			86.2
			86.8
			87.5
		24.25	
			87.3

+	HI 9073	Elev
cb	48	85.9
1/4	5.2	85.5
+3	5.6	85.1
+5	5.7	85.0
+7	6.3	84.4
8	6.3	84.4
1/4	7.2	83.5
+1	7.3	83.4
+2	8.3	82.4
+3	7.2	83.5
cb	7.4	83.3
S.	8.1	82.6
+15	10.4	80.3
	2150	
-15	11.3	79.4
S	9.8	80.9
+6	9.2	91.5
cb	8.9	81.8
+10	8.1	82.6
+11	8.9	81.8
+12	8.3	82.4
1/4	8.3	82.4
+8	7.5	83.2
8	7.4	83.3
1/4	6.9	84.8
+5	6.0	84.7

+	HI 9073	Elev
cb	51	85.6
N	4.6	86.1
	2+75	
N	5.4	85.3
cb	6.4	84.3
1/4	7.4	83.3
8	8.1	82.6
1/4	9.0	81.7
+7	9.4	81.3
cb	10.3	80.4
S.	11.1	79.6
+15	12.9	77.8
	3+00	
-15	14.0	76.7
S	12.4	78.3
cb	11.2	79.5
1/4	10.1	80.6
8 on ground	9.0	81.7
n Rim Mt. Hole	8.7	81.96
+5	8.5	82.2
1/4	8.7	82.0
+4	8.2	82.5
cb	7.9	82.8
+5	7.3	83.4
N	6.6	84.1

	+	HI. 90.73	-	Elev
			3125	
N			7.5	83.2
+5			8.0	82.7
cb			8.6	82.1
+10			8.8	81.9
14			9.1	81.6
2			9.6	81.1
14			10.7	80.0
+1			11.6	79.1
+9			11.7	79.0
+5			11.0	79.7
cb			11.2	79.5
S			12.8	77.9
+10			14.3	76.4
+17 bottom step			12.79	77.94
+17 floor of Residence			11.05	79.68
T.P.	3.67	82.92	14.8	79.25
			3150	
-15			8.7	74.2
-10			7.2	75.7
S			6.1	76.8
cb			4.3	78.6
+6			4.1	78.8
+7			5.0	77.9
+9			4.7	78.2
14			4.5	78.4

	+	HI. 82.92	-	Elev
			39	
			9.2	78.7
			2.8	80.1
			2.5	80.4
			2.1	80.8
			1.5	81.4
			0.1	82.8
			3175	
			1.6	81.3
			2.5	80.4
			3.3	79.6
			3.3	79.6
			3.8	79.1
			4.6	78.3
			4.8	78.1
			6.6	76.3
			6.6	76.3
			8.9	84.0
			8.8	84.1
			5.8	77.1
			5.7	77.2
			6.4	76.5
			7.7	75.2
			8.8	74.1
			10.5	72.4
			4400	
			10.6	72.3

HZ.
8292

-15	98	73.1
S	93	73.6
+4	88	74.1
cb	88	74.1
+5 Top	9.4	73.5
+5 Bottom	11.7	71.2
1/4	12.0	70.9
+1	11.1	71.8
+5	10.9	72.0
+8	9.4	73.5
ϕ	7.9	75.0
+10	5.3	77.6
1/4	4.9	78.0
cb	4.0	78.9
N	3.2	79.7
	4+06	
N	5.1	77.8
cb	5.6	77.3
+7	5.3	77.6
1/4	6.0	76.9
ϕ	9.1	73.8
+7	12.0	70.9
+11	12.1	70.8
1/4	13.2	69.7
+6	13.1	69.8
+7	10.0	72.9

HZ
8292

40

cb	98	73.1
S	10.0	72.9
+20	11.0	71.9
	9+14	
-20	12.9	70.0
-15	11.7	71.2
S	11.7	71.2
+5	11.1	71.8
+12	11.5	71.4
cb	12.1	70.8
+8 Top	12.5	70.4
+8 Bottom	14.6	68.3
1/4	14.9	68.0
+3	13.9	69.0
+5	14.1	68.8
+11	11.9	71.0
ϕ	11.8	71.1
+5	10.6	72.3
+11	8.8	74.1
1/4	8.9	74.0
cb	9.3	73.6
N	9.0	73.9
TP.	0.75	70.48
	13.19	69.73
	4+25	
N	1.6	68.9
cb	2.2	68.3

	HI 7098	-	Elev
t6		1.8	68.7
1/4		1.7	68.8
t8		2.1	68.4
ϕ		2.9	68.1
t2		2.5	68.0
t5		3.3	68.2
t11		3.5	67.0
1/4		4.3	66.2
t5 Bottom		4.1	66.4
t5 Top		2.8	67.7
cb		2.3	68.2
t5		1.6	68.9
S		1.6	68.9
t10		1.0	69.5
t20		1.6	68.9
	4438		
-20		5.1	65.4
-10		5.0	65.5
S		5.9	64.6
cb		6.2	64.3
t10		5.5	65.5
1/4		5.6	64.9
t3		5.5	65.0
ϕ		6.2	64.3
t2		6.8	63.7
1/4		7.2	63.3

	HI 7098	-	Elev
cb		6.9	63.6
N		6.9	63.6
	4450		
N		9.2	61.3
cb		9.3	61.2
1/4		9.4	61.1
ϕ		8.3	62.2
t3		7.8	62.7
t10		7.3	63.2
1/4		7.2	63.3
cb		8.3	62.2
14		7.8	62.7
t6		8.4	62.1
S		8.9	62.1
	4475		
S		10.3	60.2
cb		10.3	60.2
t7		10.3	60.2
t8		10.1	60.4
1/4		10.4	60.1
t6		10.3	60.2
t8		10.6	59.9
ϕ		10.7	59.8
1/4		11.4	59.1
cb		11.7	58.8
N		11.6	58.9

HI
7098

Elev

5400

N		127	57.8
cb		124	58.1
1/4		124	58.1
¢		11.9	58.6
1/4		11.6	58.9
75		11.2	59.3
cb		11.4	59.1
S		11.2	59.3
7P	2.99	61.75	59.26

5450

S		41	57.7
cb		41	57.7
1/4		4.3	57.5
¢		4.5	57.3
1/4		4.7	57.1
cb		4.8	57.0
N		4.6	57.2

5490

N		5.3	56.5
cb		5.2	56.6
1/4		5.2	56.6
¢		5.1	56.7
1/4		5.1	56.7
cb		5.1	56.7
S		5.4	56.4

HI
6175

42

6400 ²⁰ W line of 35th

S		6.0	55.8
cb		5.8	56.0
1/4		5.4	56.4
¢		5.4	56.4
1/4		5.3	56.5
cb		5.3	56.5
N		5.4	56.4
check out on BM N.W. Corner 35 th + Broadway			
		5.11	56.64
			56.62
			0.02 error

Bill Bliss
 Joe Guernit
 J. Jacobsen
 P. Kiernan
 of 8/1922

X Section "C" Street 34th to 35th

+ HZ
 139.93

- Elev

43

BM.	204	139.93	137.89	N&M on 39 th St			Elev
					+5	8.3	131.6
					1/4	9.4	130.5
						11.5	128.4
N			2.3	137.6	+4	12.2	127.7
cb			4.1	135.8	+9	14.6	125.3
1/4			5.5	134.4	S	15.2	124.7
ϕ			7.4	132.5	+20	16.2	123.7
1/4			9.0	130.9		0150	
cb			11.1	128.8	-20	15.9	124.0
S			13.1	126.8	S	15.6	124.3
					+5	15.3	124.6
-20			16.6	123.3	+10	12.7	127.2
-5			14.7	125.2	cb	12.9	127.5
S			13.0	126.9	1/4	10.4	129.5
cb			10.5	129.4	ϕ	8.4	131.5
+5			9.7	130.2	1/4	6.3	133.6
1/4			8.5	131.4	cb	4.7	135.2
ϕ			6.8	133.1	N	2.8	137.1
1/4			4.6	135.3		0175	
cb			3.3	136.6	N	6.6	133.3
1/4			1.6	138.3	cb	8.6	131.3
					1/4	10.3	129.6
N			2.3	137.6	ϕ	12.3	127.6
cb			3.7	136.2	1/4	14.2	125.7
1/4			5.5	134.4	cb	15.3	124.6
ϕ			7.5	132.4	S	16.5	123.4

Plotted 4-16-29- CBH
 Reduced by Bathin

H.Z.
139.93

		17.8	122.1	
t20		1400		-30
-30		25.2	114.7	S
-3		22.3	117.6	cb
S		21.6	118.3	1/4
cb		20.2	119.7	¢
1/4		18.5	121.4	1/4
¢		16.6	123.3	cb
1/4		14.7	125.2	N
cb		13.0	126.9	t10
N		11.0	128.9	t20
t10		9.6	130.3	
TP	2.00	129.56	127.56	-20
S		1125		-10
-15		9.3	125.3	N
N		6.1	123.5	cb
cb		8.0	121.6	1/4
1/4		9.2	120.4	¢
¢		10.7	118.9	1/4
1/4		12.8	116.8	cb
cb		14.5	115.1	t8
t7		15.0		S
N t9		14.4		t30
S		15.5	115.1	
t30		17.3	112.3	-30
¢				S

H.Z.
129.56

Elex

44

		1435	
		19.2	110.4
		16.8	112.8
		15.3	115.3
		14.7	114.9
		13.4	116.2
		12.2	117.4
		11.2	118.4
		9.4	120.2
		8.2	121.4
		7.3	122.3
		1145	
		8.6	121.0
		9.4	120.2
		10.3	119.3
		11.2	118.4
		12.3	117.3
		13.7	115.9
		15.1	114.5
		15.4	114.2
		15.6	114.0
		16.6	113.0
		18.4	111.2
		1154	
		17.2	112.4
		15.3	114.3

HZ
12956

+4	19.4	115.2
cb	14.4	115.2
1/4	13.3	116.3
φ	12.1	117.5
1/4	11.2	118.4
cb	10.5	119.1
+11	10.8	118.8
N	10.8	118.8
+10	10.0	119.6
+20	9.2	120.4
	1170	
-15	3.6	126.0
N	4.8	124.8
cb	6.4	123.2
1/4	8.3	121.3
φ	9.2	120.4
1/4	9.4	120.2
cb	10.0	119.6
S.	11.0	118.6
+20	12.5	117.6
	1185	
-20	8.3	121.3
S	7.8	121.8
+5	8.1	121.5
cb	7.7	121.9
1/4	7.0	122.6

+ HZ
12956

φ	5.9	124.245
1/4	4.5	125.1
cb	3.4	126.2
N	2.2	127.4
+10	1.3	128.3
	2100	
N	0.2	129.4
cb	1.3	128.3
1/4	2.1	127.5
φ	2.9	126.7
1/4	3.8	125.8
cb	4.9	124.7
S.	6.3	123.3
+2	7.4	122.2
+20	9.6	120.0
	2125	
-20	10.5	119.1
-7	9.0	120.6
-5	8.3	121.3
-4	7.0	122.6
S.	4.8	124.8
+3	4.4	125.2
cb	2.6	127.0
1/4	1.4	128.2
φ	0.3	129.3
T.P.	9.05	133.12
	0.49	139.07

+	HI. 13312	-	Elev
1/4		2.9	130.2
cb		1.8	131.3
N		0.7	132.4
	2450		
N		0.5	132.6
cb		2.2	130.9
1/4		3.7	129.4
¢		5.9	127.7
1/4		6.9	126.2
cb		8.1	125.0
S.		10.3	122.8
t5		11.3	121.8
t20		12.9	120.2
t30		14.9	118.2
	2475		
-30		20.7	112.4
-3		15.7	117.4
S.		14.5	118.6
cb		11.7	121.4
1/4		9.6	123.5
¢		7.8	125.3
1/4		6.5	126.6
cb		5.0	128.1
N		3.2	129.9
	2488		
N		4.2	128.9

+	HI. 13312	-	Elev
		4.9	128.2
		6.2	126.9
		8.5	124.6
		10.5	122.6
		12.2	120.9
		14.8	118.3
		17.3	115.8
		18.5	114.6
		23.0	110.1
	3400		
		25.3	107.8
		20.3	112.8
		17.6	115.5
		15.1	118.0
		13.2	119.9
		11.6	121.5
		10.7	122.4
		8.2	124.9
		6.1	127.0
	3425		
		12.3	120.8
	0.71	121.27	120.56
		2.4	118.9
		4.6	116.7
		6.7	114.6
		8.6	112.7

46

	+	HI 121.27	-	Elev
cb			11.1	110.2
S			13.3	108.0
+20			15.8	105.5
+30			17.2	104.1
			3+40	<i>beginning of the forest</i>
-30			19.2	102.1
S			15.6	105.7
cb			13.9	107.4
1/4			12.4	109.9
ϕ			10.4	110.9
1/4			8.4	112.9
cb			6.3	115.0
+4			5.5	115.8
N			4.6	116.7
			3+50	
N			9.3	112.0
cb			10.2	111.1
1/4			11.5	109.8
ϕ			13.0	108.3
TP	1.53	109.60	13.20	108.07
1/4			2.8	106.8
cb			4.4	105.2
S			5.5	104.1
+30			8.9	100.7
			3+65	
-30			11.3	98.3

	+	HI 109.60	-	Elev	47
			8.6	101.0	
			7.3	102.3	
			6.0	103.6	
			5.2	104.4	
			5.4	104.2	
			5.4	104.2	
			4.3	105.3	
			3.4	106.2	
			3+75		
			8.0	101.6	
			9.1	100.5	
			10.5	99.1	
			10.4	99.2	
			9.3	100.3	
			9.1	100.5	
			9.7	99.9	
			10.5	99.1	
			12.0	97.6	
			3+85		
			13.9	95.7	
			13.4	96.2	
			12.5	97.1	
			11.8	97.8	
			12.9	96.7	
			I.P	96.90	
	0.37	97.27	12.70	96.90	
			1.6	95.7	

	H.I. 97.27	-	Elev
cb		1.8	95.5
+5		0.9	96.4
N		0.8	96.5
		3+90	
N		2.7	94.6
cb		3.4	93.9
1/4		3.4	93.9
¢		2.9	94.4
1/4		1.8	95.5
cb		1.8	95.5
S		2.9	94.4
		4+00	
S		8.4	88.9
cb		7.8	89.5
1/4		7.9	89.4
¢		8.7	88.6
1/4		7.9	89.4
+10		6.7	90.6
cb		6.9	90.4
+4		7.1	90.2
N		8.2	89.1
		4+10	
N		12.7	84.6
+4		12.2	85.1
+10		10.7	86.6
cb		10.4	86.9

	H.I. 97.27	-	Elev
+10		10.9	86.4
1/4		12.1	85.2
+7		13.9	83.4
¢		14.0	83.3
1/4		14.1	83.2
cb		13.6	83.7
S		14.1	83.2
TP	0.44	89.60	13.11
		4+15	
S		4.1	80.5
+5		3.4	81.2
cb		2.5	82.1
1/4		2.6	82.0
¢		2.8	81.8
+8		2.4	82.2
1/4		1.2	83.4
+7		0.7	84.5
TP	3.00	87.56	0.04
cb		2.3	85.3
+5		3.1	84.5
TP	0.04	84.60	3.00
+11		2.1	82.5
N		2.3	82.3
		4+30	
N		7.8	76.8
+5		8.2	76.4

48

	+	#I. 8460	-	Elev
			7.7	769
tg			7.6	770
cb			8.2	764
1/4			9.8	748
ϕ			10.1	745
1/4			10.7	739
cb			11.5	731
S				
TP	1.93	74.05	12.48	72.12
			4+90	
S			5.0	69.1
cb			9.5	69.6
1/4			3.9	70.2
ϕ			2.7	71.4
1/4			2.1	72.0
cb			1.1	73.0
N			0.5	73.6
			4+50	
N			2.3	71.8
cb			2.7	71.4
1/4			3.7	70.4
ϕ			4.7	69.4
1/4			5.5	68.6
cb			6.6	67.5
S			7.0	67.1
			4+75	
S			10.~	63.9

	+	#I. 7405	-	Elev
			9.9	64.2
			9.5	64.6
			8.7	65.4
			7.9	66.2
			7.3	66.8
			7.6	66.5
			5+00	
			10.7	63.4
			10.4	63.7
			10.6	63.5
			11.0	63.1
			11.3	62.8
			11.4	62.7
			11.7	62.4
			5+25	
			12.3	61.8
			12.4	61.7
			12.5	61.6
			12.9	61.7
			12.4	61.7
			12.9	61.7
			12.0	62.1
			TP	9.31
			66.29	12.12
			5+50	
			9.3	61.9
			4.4	61.8

4/25/29

Landon

SE 7th Rock Locust
B.M. Wilbur

X section Soledad Road.
See Back 1324 P 11 for Alignment.

				186.06
T.P.	12.79	198.85	0.00	198.85
0+00				
40L		2.6		207.9
36L		3.5		207.0
20L	top e b	3.65		206.87
✓	cut	4.26		206.26
±	Raw	3.81		206.71
20R	cut	4.26		206.26
20R	top e b	3.60		206.92
40R		3.2		207.3
0+30				
50R		0.7		209.8
25R		1.4		209.1
±		2.0		208.5
32L		1.2		209.3
100L		1.7		208.8
0+65L				
T.P.	12.89	221.91	1.50	209.02
100L			10.8	211.1
35L			10.0	211.9
±			10.3	211.6
100R			8.1	213.8

1+00	221.71
90R	8.0 213.9
19R	Road 7.0 214.9
±	5.8 216.1
T.P.	12.24 233.46 0.69 221.22
100L	11.0 222.5
1+42 ⁶³ B.C.	
110L	5.5 228.0
19L	12.3 221.2
11L	11.7 221.8
±	Road 13.2 220.3
13R	14.3 219.2
19R	12.3 221.2
60R	12.2 221.3
2+00	
40R	+4.0 237.5
15R	2.3 231.2
±	4.4 229.1
34L	Road 5.7 227.8
15L	5.8 227.7
49L	6.7 226.8

2+50		233.46	
75L		3.2	230.3
70L		0.9	232.6
62L	Road	1.9	231.6
50L		2.8	230.7
45L		0.7	232.8
T.P.	12.89	246.29	0.06
10L		10.6	235.7
±		8.8	237.5
40R		1.7	244.6
3+00			
40R		+10.7	257.0
±		+3.6	249.9
61L		9.0	237.3
64L		12.7	233.6
76L	Road	12.8	233.5
82L		11.6	234.7
88L		13.4	232.1
3+50			
94L		12.0	234.3
90L		10.0	236.3
83L	Road	10.5	235.8
72L		11.3	235.0
67L		7.2	239.1
T.P.	11.90	257.84	0.35

3+50		257.84	
20L		7.2	250.6
±		1.0	256.8
40R		+8.2	266.0
4+00			
50R		+11.4	269.2
40R		+9.9	267.7
±		+0.3	258.1
34L		8.1	249.7
49L		12.7	245.1
63L		16.5	241.3
69L		21.5	236.3
79L	Road	21.0	236.8
87L		20.1	237.7
90L		22.0	235.8
A+50			
135L		34.8	223.0
76L		22.1	235.7
70L		18.7	239.1
60L	Road	19.3	238.5
53L		19.8	238.0
52L		18.3	239.5
40L		13.0	244.8
15L		5.2	252.6
±		1.4	256.4
40R		+6.6	264.4

		257.84		
5+00				
40R		+4.9	262.7	
±		4.6	253.2	
26L		13.8	244.0	
34L		19.2	238.6	
40L	Road.	19.0	238.8	
47L		19.0	238.8	
56L		23.7	234.1	
100L		32.0	225.8	
5+50				
100L		34.0	223.8	
65L		30.8	227.0	
43L		23.4	234.4	
32L		17.1	240.7	
24L	Road.	17.4	240.4	
18L		17.3	240.5	
15L		13.6	244.2	
±		8.0	249.8	
T.P	11.31	265.44	3.71	254.13
40L			5.0	260.4

		6+00	265.44	
40R			5.4	260.0
22R			10.1	255.3
±			17.6	247.8
4L			23.0	242.4
12L	Road		22.6	242.8
18L			22.3	243.1
24L			26.3	239.1
39L			31.4	234.0
59L			38.0	227.4
6+50				
60L			36.0	229.4
36L			27.5	237.7
15L			20.6	244.8
10L			17.2	248.2
5L	Road		17.8	247.6
±			18.0	247.4
4R			18.0	247.4
8R			14.1	251.3
33R			7.2	258.2
40R			5.8	259.6

7+00		26544	
40R		5.5	259.9
20R		9.0	256.4
12R		11.6	253.8
10R		15.7	249.7
±	Road	15.1	250.3
5L		15.0	250.4
8L		17.6	247.8
40L		27.0	238.4

7+51 ² B.C.			
40L		26.0	239.4
5L		16.2	249.2
±		13.6	251.8
7R	Road	13.8	251.6
14R		13.8	251.6
17R		11.0	254.4
40R		6.0	259.4

8+00			
40R		5.6	259.8
18R		9.6	255.8
16R		12.3	253.1
7R	Road	12.5	252.9
±		12.1	253.3
5L		14.9	250.5
30L		22.4	243.0
45L		24.7	241.3

8+50		26544	
50L		21.2	244.2
24L		15.4	250.0
5L		12.5	252.9
±		9.9	255.5
8R	Road	10.1	255.3
16R		9.8	255.6
21R		6.7	258.7
40R		4.4	261.0
TP	13.05	275.37	3.12

9+00			
40R		10.8	269.6
20R		12.8	262.6
16R		16.2	259.2
6R	Road	16.7	258.7
±		16.0	259.4
1L		17.0	258.4
22L		20.1	255.3
40L		24.0	251.4

9+50			
40L		23.0	252.4
35L		20.6	254.8
9L		14.6	260.8
3L		13.0	262.4
±		12.0	263.4

9+50		275.37	
9R	Road	12.4	263.0
18R		12.4	263.0
20R		10.6	264.8
30R		9.9	265.5
10+00			
30R		7.6	267.8
17R		8.6	266.8
15R		9.8	265.6
6R	Road	9.8	265.6
±		9.5	265.9
4L		9.5	265.9
6L		10.5	264.9
30L		12.9	262.5
10+51 ²³ P.C.C.			
30L		7.2	268.2
±	Road	6.4	269.0
11R		6.6	268.8
13R		5.4	270.0
30R		5.0	270.4
11+00			
30R		4.8	270.6
±	Road	4.3	271.1
15L		4.4	271.0
17L		3.4	272.0
30L		3.0	272.4

11+50		275.37	
30L		2.0	273.4
±		3.4	272.0
7R	Road	3.4	272.0
17R		4.4	271.0
19R		3.5	271.9
30R		4.0	271.4
12+04 ⁶⁴ E.C.			
30R		4.2	271.2
9R	Road	3.6	271.8
±		3.1	272.3
30L		2.6	272.8
12+39 ⁸⁸ B.C.			
30L		2.5	272.9
15L		2.9	272.5
13L		2.2	273.2
±		2.8	272.6
9R	Road	3.3	272.1
30R		3.9	271.5
13+00			
30R		2.8	272.6
20R	Road	2.5	272.9
5R		2.1	273.3
3R		1.3	274.1
±		1.0	274.4
TP-	12.86	286.12	2.11 273.26

13+00	286.12		
30L		10.5	275.6
13+50			
30L		8.8	277.3
±		10.2	275.9
30R		11.8	274.3
14+00			
30R		10.3	275.8
±		7.9	278.2
30L		5.8	280.3
14+50			
40L		2.0	284.1
30L		2.6	283.5
±		5.5	280.6
30R		7.7	278.4
15+00			
61R Road		7.6	278.5
51R		7.5	278.6
30R		3.9	282.2
±		1.8	284.3
T.P.	11.21	295.80	1.53 284.59
B.M	Hub + BC	5+11.2	10.99 284.81
30L		8.8	287.0
50L		8.0	287.8

15+11 ²⁷ EC	295.80		
50L		5.3	290.5
35L		8.3	287.5
30L		8.5	287.3
±		11.0	284.8
30R		14.4	281.4
47R		16.2	279.6
57R Road		17.4	278.4
15+50			
50R		18.3	277.5
43R Road		18.4	277.4
31R		17.0	278.8
30R		16.8	279.0
±		10.9	284.9
30L		5.6	290.2
50L		3.5	292.3
15+75			
50L		3.1	
30L		6.6	289.2
±		13.0	282.8
15R		17.8	278.0
17R		17.2	276.6
25R Road		19.8	276.0
30R		19.8	276.0
36R		19.4	276.4
50R		21.6	274.2

16+00		295.80		
50R			28.0	267.8
30R			22.0	273.8
20R			19.8	276.0
10R	Road		19.7	276.1
±			19.7	276.1
3L			17.8	278.0
30L			9.6	286.2
50L			4.7	291.1

16+38				
50L			11.2	
TP	1.49	284.60	12.69	283.11
30L			5.4	279.2
20L			8.2	276.4
14L	forks Roads		9.7	275.9
±			9.0	275.6
6R			13.0	271.6
30R			10.4	264.2
50R			23.6	261.0
55R			21.0	263.6

16+75				
50R			14.4	270.2
30R			23.0	261.6
8R			13.9	270.7
±			12.7	271.9
5L			10.8	273.8

16+75				57
15L	Road		10.8	273.8
30L			9.0	275.6
47L	Road		7.6	277.0
55L			6.9	277.7

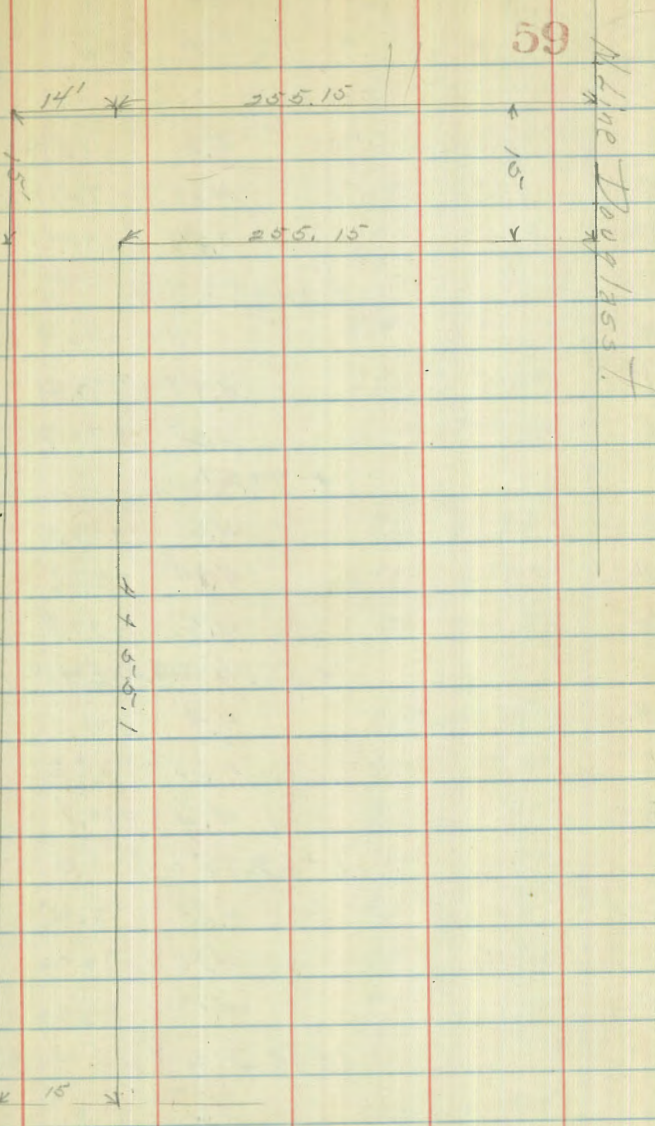
17+00				
50L			8.4	276.2
37L			10.3	274.3
30L			12.1	272.5
24L			13.3	271.3
21L			11.8	272.8
14L	Road		12.0	272.6
5L			12.2	272.4
±			14.6	270.0
10R			21.0	263.6
30R			15.0	269.6
41R			13.0	271.6
50R			13.3	271.3

17+25				
50R			11.7	272.9
30R			12.6	272.0
±			12.6	272.0
3L			11.6	273.0
9L	Road		11.7	272.9
19L			11.4	273.2
23L			16.0	268.6
27L			16.4	268.2

Re Xsec Alley 1 Palm Hghts
To Check finish grade

B.M. S.M.B.P.	+	π	-	ELEV	Douglas Albatross grades set for Construction
	5.90	276.43		270.53	
T.P.	4.46	277.40	3.49	272.94	
0+00 = N.A. Douglas on Print					
W			6.17	271.23	271.22
Φ			6.11	71.29	
E			5.76	271.64	271.64
0+10					
E			5.2	272.2	
Φ			5.7	71.70	
W			5.7	271.7	271.6
0+20					
W.			5.4	272.0	272.0
Φ			5.45	71.95	
E			5.15	272.25	272.2
0+40					
E			4.6	272.8	272.8
Φ			5.0	72.40	
W.			4.85	272.55	272.6
0+60					
W			4.6	272.8	273.0
Φ			4.69	72.71	
E			4.25	273.15	273.2

Nine changed to meet discrepancy
 in lines of the contiguous
 sub divisions.



	+	277.40 π	-	Elev	grades Set	
		0+80				
E			4.2	273.2	273.3	N
Φ			4.69	72.71		Φ
W.			4.50	272.85	273.1	S.
		1+00				
W			4.50	272.9	273.0	S
Φ			4.49	72.91		Φ
E			4.2	273.2	273.2	N
		1+27.57				
E			4.6	272.8	273.0	N.
Φ			4.74	72.66		Φ.
W			4.60	272.8	272.8	S.
		1+55.15 = S.L. E & W. Alley				
W.			4.9	272.5	272.6	S.
Φ			4.85	72.55		Φ
E			4.6	272.8	272.8	N.
		1+62.15 = Φ E & W. Alley				
E			4.75	72.65		N.
Φ Both alleys			4.80	72.60		Φ.
W.			5.17	72.20		S.
		1+69.15 = N.L. E & W Alley				
W.			5.0	272.4	272.6	S
Φ			4.8	72.60		Φ
E			4.6	272.8	272.8	N

	+	277.40 π	-	Elev	60 grades Set	
		0+00 = S.L. N & S Alley				
			5.0	272.4	272.6	
			5.19	72.21		
			4.9	272.5	272.6	
		0+22.5				
			5.9	271.5		
			4.2	71.20		
			6.2	271.2		
		0+45				
			7.6	269.8	269.8	
			7.67	69.77		
			7.6	269.8	269.8	
		0+65				
			8.65	268.75	268.7	
			9.0	68.40		
			8.8	268.60	268.7	
		0+85				
			9.6	267.8	267.8	
			9.9	67.50		
			9.6	267.8	267.8	
		1+05				
			10.25	267.15	267.15	
			10.46	66.94		
			10.2	267.2	267.15	

Grades changed
From this point to
to total basin by
Bissell 8/8/29
to fit new
location of
drain

	+	Σ	-	Elev	grades set
		277.40			
	1+25				
N.			10.8	266.6	266.9
+1			10.4	67.0	
±			10.69		66.6
S.			10.5	266.9	266.9
	1+45				
S.			10.7	266.7	266.85
±			10.86	66.54	
N.			10.6	266.8	266.85
	1+65				
N.			11.15	266.75	266.8
+1			10.65	66.85	
±			10.78	66.62	
S.			10.65	266.75	266.8
	1+85				
S.			10.6	266.8	
±			10.93	66.47	
N.			10.8	266.6	
	2+06.00				
N.			10.8	266.6	266.65
±			11.12	66.28	
S.			10.8	266.6	266.65
	2+21 = Catch Basin				
S.			10.96	266.44	266.6
± on grating			11.11	266.29	266.3

	+	Σ	-	Elev	grades set
		277.40			
	2+47.88				
			10.85	266.55	266.6
			10.8	266.6	266.66
			11.05	66.35	
			10.83	266.57	266.66
	2+68.60				
			9.80	267.6	
			10.65		
			10.77	67.43	
			10.77		
			10.4	267.0	
	2+89.32				
			10.53	266.87	266.79
			10.73	66.67	
			10.49	266.91	266.79
	3+10.04				
			10.45	266.95	
			10.66	66.74	
			10.35	267.05	
	3+30.76				
			10.38	267.02	266.92
			10.59	66.81	
			10.40	267.	266.92

1-8-30
J.C. Bliss
D. Prebert
Rouner

X-section Rigel Street - Acacia
to Main - 60' wide - 10' cbs - 10' 1/4s

B.M. S.E. Prop Hub 35th & Boston 31.46
+0.54

T 32.00

S.L. Acacia = 0+00

W	4.2	27.8
cb	4.0	28.0
1/4	4.5	27.5
1/4	4.6	27.4
1/4	4.1	27.9
1/4	4.1	27.9
cb	4.8	27.2
E	5.0	27.0
0+25		
E	4.8	27.2
cb	4.7	27.3
1/4	4.5	27.5
1/4	4.8	27.2
1/4	4.9	27.1
+7	4.8	27.2
+8	4.0	28.0
cb	4.2	27.8
W	4.4	27.6

Plotted 1-15-30 - C.B.H.

T 32.00

63

0+50

W	5.4	26.6
cb	5.2	26.8
+3	5.0	27.0
+4	5.5	26.5
1/4	5.5	26.5
R	5.5	26.5
1/4	5.3	26.7
cb	5.1	26.9
E	4.9	27.1
0+75		
E	5.7	26.3
cb	5.6	26.4
1/4	6.0	26.0
R	6.0	26.0
1/4	6.1	25.9
+5	6.1	25.9
+6	5.7	26.3
cb	5.7	26.3
W	6.0	26.0
1+00		
W	6.4	25.6
cb	6.1	25.9
+3	6.1	25.9
+5	7.1	24.9
1/4	6.8	25.2

π 32.00

£	68	252
1/4	67	253
cb	66	254
E	66	254

1+25

E	76	24.4
cb	77	24.3
1/4	77	24.3
£	76	24.4
1/4	77	24.3
+5	78	24.2
+8	69	25.1
cb	70	25.0
W	71	24.9

1+50

W	82	23.8
cb	83	23.7
1/4	86	23.4
£	83	23.7
1/4	85	23.5
cb	85	23.5
E	9.0	23.0

π 32.00

1475

64

E	9.2	22.8
cb	9.5	22.5
1/4	9.5	22.5
£	9.7	22.3
1/4	9.7	22.3
+5	9.0	23.0
cb	8.9	23.1
W	8.8	23.2

2400

W	9.7	22.3
cb	10.2	21.8
+3	10.1	21.9
1/4	10.8	21.2
£	10.6	21.4
1/4	10.6	21.4
cb	10.5	21.5
E	10.4	21.6

2+25

E	11.0	21.0
+2	11.4	20.6
cb	11.3	20.7
1/4	11.6	20.4
£	11.6	20.4
1/4	11.8	20.2
cb	11.8	20.2

T 32.00

W	11.7	20.8
2+50		
W	11.0	21.0
cb	11.8	20.2
1/4	12.6	19.4
♀	12.4	19.6
1/4	12.4	19.6
cb	12.4	19.6
+7	12.4	19.6
E	11.8	20.2

2+75

E	12.6	19.4
+v	13.3	18.7
cb	13.3	18.7
1/4	13.0	19.0
♀	12.9	19.1
1/4	13.0	19.0
+5	12.7	19.3
+7	11.6	20.4
cb	11.7	20.3
W	11.4	20.6

T 32.00

65

3400 = N L Birch - 80' wide - 14' cbs 13 1/4 S

W	12.0	20.0
cb	12.0	20.0
+4	12.1	19.9
+6	13.0	19.0
1/4	13.4	18.6
♀	13.4	18.6
1/4	13.3	18.7
cb	13.7	18.3
E	13.2	18.8

11.95 20.05

+536

T 25.41

N cb Birch

E	8.1	17.3
cb	7.6	17.8
1/4	7.0	18.4
♀	6.9	18.5
1/4	6.9	18.5
+6	6.6	18.8
+8	5.4	20.0
cb	5.4	20.0
W	5.4	20.0

2541

N 1/4 Birch

w	6.1	19.3
cb	6.8	18.6
1/4	7.2	18.2
♀	7.2	18.2
1/4	7.3	18.1
cb	7.8	17.6
E	8.4	17.0

♀ Birch

F	8.4	17.0
cb	7.8	17.6
1/4	7.4	18.0
♀	7.4	18.0
1/4	7.1	18.3
cb	6.7	18.7
w	6.4	19.0

S 1/4 Birch

w	6.4	19.0
cb	7.0	18.4
1/4	7.2	18.2
♀	7.5	17.9
1/4	7.8	17.6
cb	8.0	17.4
E	8.2	17.2

2541

S cb Birch

E	8.5	16.9
cb	7.7	17.7
1/4	7.5	17.9
♀	7.5	17.9
1/4	7.3	18.1
cb	6.9	18.5
w	6.2	19.2

S-L Birch = 0400

w	5.2	20.2
cb	6.0	19.4
1/4	7.2	18.2
♀	7.6	17.8
1/4	7.5	17.9
cb	8.0	17.4
E	8.5	16.9

0425

E	8.0	17.4
cb	7.7	17.7
1/4	7.2	18.2
♀	7.2	18.2
1/4	7.2	18.2
+5	7.0	18.4
+6	5.6	19.8
cb	5.4	20.0
w	5.4	20.0

66

T 25.41

0+50

W	4.9	20.5
cb	5.4	20.0
+2	5.5	19.9
+5	6.4	19.0
1/4	6.7	18.7
£	6.8	18.6
1/4	6.8	18.6
cb	7.4	18.0
E	7.7	17.7

0+75

E	7.2	18.2
cb	6.8	18.6
1/4	6.4	19.0
£	6.3	19.1
1/4	6.2	19.2
+4	6.2	19.2
+7	5.0	20.4
cb	4.7	20.7
W	4.5	20.9

1+00

W	4.9	20.5
cb	5.2	20.2
1/4	5.4	20.0
£	5.5	19.9
1/4	5.7	19.7

T 25.41

67

cb	6.0	19.4
E	6.5	18.9

1+25

E	5.8	19.6
cb	5.4	20.0
1/4	5.2	20.2
£	5.0	20.4
1/4	5.0	20.4
cb	4.5	20.9
W	4.4	21.0

1+50

W	4.3	21.1
cb	4.4	21.0
1/4	4.9	20.5
£	4.9	20.5
1/4	4.9	20.5
cb	5.1	20.3
£	5.3	20.1

1+75

E	5.2	20.2
cb	5.2	20.2
1/4	5.2	20.2
£	5.0	20.4
1/4	4.9	20.5
+5	4.8	20.6

T 25.41

+6	4.3	21.1
cb	4.5	20.9
w	4.5	20.9

2400

w	4.6	20.8
cb	4.5	20.9
+3	4.6	20.8
+5	5.2	20.2
1/4	5.2	20.2
¢	5.2	20.2
1/4	5.4	20.0
cb	5.3	20.1
E	5.5	19.9

2425

E	5.5	19.9
cb	5.5	19.9
1/4	5.8	19.6
¢	5.6	19.8
1/4	5.6	19.8
+5	5.6	19.8
+6	5.2	20.2
cb	5.1	20.3
w	5.1	20.3

T 25.41

68

2450

w	5.9	19.5
cb	5.6	19.8
+4	5.7	19.7
+5	6.5	18.9
1/4	6.5	18.9
¢	6.3	19.1
1/4	6.4	18.0
¢	5.8	19.6
cb	5.7	19.7
E	5.9	19.5

2475

E	6.6	18.8
cb	6.3	19.1
+4	6.5	18.9
1/4	7.3	18.1
¢	7.1	18.3
1/4	7.4	18.0
+4	7.4	18.0
+5	6.7	18.7
cb	6.8	18.6
w	7.0	18.4

π 25.41

3+00 = N.L. Cottonwood

80' wide
14' cbs
13' 1/2

w	8.3	17.1
cb	8.1	17.3
+5	8.2	17.2
+6	8.6	16.8
1/4	8.6	16.8
♀	8.2	17.2
1/4	8.2	17.2
gb	7.1	18.3
E	7.1	18.3
N cb		
E	7.6	17.8
cb	7.7	17.7
+4	7.8	17.6
1/4	8.8	16.6
♀	8.8	16.6
1/4	9.1	16.3
+4	9.4	16.0
+6	9.0	16.4
cb	8.8	16.6
w	9.1	16.3
N 1/4		
w	10.6	14.8
cb	10.2	15.2
1/4	9.5	15.9
♀	9.3	16.1

π 25.41

69

1/4	9.2	16.2
+6	8.6	16.8
cb	8.4	17.0
E	8.1	17.3
♀ Cottonwood		
E	8.6	16.8
cb	8.8	16.6
1/4	9.7	15.7
♀	9.8	15.6
1/4	10.0	15.4
cb	10.2	15.2
w	10.7	14.7
S 1/4		
w	7.2	18.2
cb	10.6	14.8
1/4	10.4	15.0
♀	10.1	15.3
1/4	10.2	15.2
cb	9.1	16.3
E	9.0	16.4
S cb		
E	9.4	16.0
cb	9.9	15.5
1/4	10.7	14.7
♀	10.9	14.5

T 2541

1/4	11.0	14.4
cb	11.4	14.0
W	11.7	13.7

S.L. Cottonwood = 0+00

W	12.3	13.1
cb	11.6	13.8
1/4	11.7	13.7
♀	11.4	14.0
1/4	11.4	14.0
cb	10.2	15.2
E	9.7	15.7

B.M. 13 Men Rigol x Cottonwood 10.41 15.00
+0.21

T 15.21

0+25

E	0.9	14.3
cb	1.3	13.9
+5	1.5	13.7
+7	2.3	12.9
1/4	2.6	12.6
♀	2.6	12.6
1/4	2.8	12.4
+3	2.8	12.4
+5	2.5	12.7
cb	2.8	12.4

T 15.21

70

W	3.3	11.9
0+50		
W	5.1	10.1
cb	4.2	11.0
+5	3.8	11.4
1/4	4.1	11.1
♀	3.8	11.4
1/4	3.7	11.5
+2	3.6	11.6
+6	2.2	13.0
cb	2.1	13.1
E	1.6	13.6

0+75

E	2.7	12.5
cb	3.2	12.0
+4	3.6	11.6
+5	4.7	10.5
1/4	5.2	10.0
♀	5.2	10.0
1/4	5.5	9.7
+4	5.2	10.0
cb	6.6	8.6
W	7.0	8.2

1521

1400

W	8.3	69
cb	8.0	72
+3	7.7	75
+6	7.0	82
14	6.9	83
¢	6.8	84
14	6.6	86
+4	6.3	89
+6	5.2	100
cb	5.0	102
E	4.2	110

1425

E	6.3	89
cb	6.0	84
+4	7.0	82
+5	7.9	73
14	8.1	71
¢	8.1	71
14	8.3	69
cb	8.9	63
W	9.0	62

1450

W	9.8	54
cb	9.7	55
14	9.4	58

1521

71

¢	9.2	60
14	9.4	58
+5	9.1	61
cb	8.3	69
E	7.7	75

1475

E	9.3	59
cb	9.8	54
14	10.4	48
¢	10.4	48
14	10.4	48
cb	10.6	46
W	10.6	46

2400

W	11.0	42
cb	11.2	40
14	11.4	38
¢	11.2	40
14	11.4	38
cb	11.6	36
+8	11.4	38
+9	10.7	45
E	10.7	45

π 15.21

2+25

E	11.8	3.4
+5	12.7	2.5
cb	12.7	2.5
1/4	12.4	2.8
♀	12.1	3.1
1/4	12.0	3.2
+7	12.0	3.2
cb	11.5	3.7
W	11.6	3.6

2+50

W	12.3	2.9
cb	12.3	2.9
+2	13.0	2.2
1/4	12.9	2.3
♀	13.0	2.2
1/4	13.3	1.9
cb	13.6	1.6
E	13.4	1.8

T.P. Nail in Pole at Dalbergia 11.45 3.76

+248

π 6.24

π 6.24

2+75

72

E	5.7	0.5
cb	5.5	0.7
1/4	5.1	1.1
♀	5.0	1.2
1/4	4.8	1.4
+9	4.5	1.7
cb	3.9	2.3
W	3.8	2.4

3+00 = N.L. Dalbergia E 0+00

100" wide

W	4.5	1.7
cb	4.6	1.6
1/4	5.5	0.7
♀	5.5	0.7
1/4	5.5	0.7
cb	5.5	0.7
E	6.1	0.1

0+10

E	6.5	-0.3
cb	6.1	0.1
1/4	5.7	0.5
♀	5.7	0.5
1/4	5.7	0.5
cb	4.5	1.7
W	4.9	1.3

T6.24

0+20

w	5.2	1.0
cb	4.9	1.3
+7	5.3	0.9
+8	7.3	-1.1
1/4	7.6	-1.4
+5	7.9	-1.7
+6	6.1	0.1
q	5.8	0.4
1/4	5.8	0.4
cb	5.9	0.3
E	6.5	-0.3

0+30

out7	7.9	-1.7
out2	5.6	0.6
E	5.5	0.7
cb	5.4	0.8
1/4	5.6	0.6
+6	6.0	0.2
+7	7.8	-1.6
q	8.8	-2.6
+7	7.8	-1.6
+8	6.0	0.2
1/4	5.4	0.8
cb	5.1	1.1
w	5.4	0.8

T6.24

0+40

w	5.6	0.6
cb	5.8	0.4
1/4	5.7	0.5
+5	5.7	0.5
+8	8.8	-2.6
q	9.1	-2.9
+8	8.0	-1.8
1/4	6.3	-0.1
+7	5.2	1.0
cb	4.9	1.3
E	5.1	1.1
out6	7.9	-1.7

0+50 = q Dalbergia

out4	8.2	-2.0
E	4.2	2.0
cb	4.3	1.9
+5	4.4	1.8
1/4	7.4	-1.2
+1	8.1	-1.9
q	8.9	-2.7
+8	7.7	-1.5
1/4	7.2	-1.0
cb	7.2	-1.0
+7	7.2	-1.0
+5	5.9	0.3

73

T 6.24

W	5.6	0.6
	0+60	
W	7.8	-1.6
cb	8.6	-2.4
1/4	8.8	-2.6
ϕ	9.5	-3.3
1/4 - Approximate slowline	9.8	-3.6
+5	9.4	-3.2
+7	4.4	1.8
cb	3.9	2.3
E	3.5	2.7
	0+70 = Base Railway fill on West	
E	3.3	2.9
cb	3.7	2.5
1/4	4.0	2.2
+3 = Top fill	3.9	2.3
ϕ	5.9	0.3
+6	8.6	-2.4
1/4 = Base fill	8.9	-2.7
cb	8.9	-2.7
W	9.6	-3.4

T 6.24

74

0+80

W = Base Railway fill	8.2	-2.0
+7	4.4	1.8
cb	4.5	1.7
1/4	3.6	2.6
ϕ	4.0	2.2
1/4	3.7	2.5
cb	3.5	2.7
E	5.4	2.8
↳ Top Rail	3.40	2.8

0+90

E	4.2	2.0
cb	4.3	1.9
1/4	4.3	1.9
ϕ	4.0	2.2
1/4	3.5	2.7
cb	3.5	2.7
W	4.0	2.2
↳ Top Rail	3.20	3.04

1400 = St. Dalbergia = 0+00

W	4.0	2.2
cb	4.3	1.9
1/4	5.4	0.8
ϕ	6.1	0.1
1/4	6.6	-0.4
cb	6.1	0.1

7 6.24

+7	5.4	0.8
E	4.8	1.4
out 20	4.7	1.5
	0+25	
out 20	4.9	1.3
out 6	5.0	1.2
E	5.8	0.4
cb	6.7	-0.5
1/4	7.0	-0.8
£	7.0	-0.8
1/4	7.0	-0.8
cb	7.1	-0.9
w	7.1	-0.9
out 8	5.2	1.0
out 20	5.2	1.0
	0+50	
out 20	5.1	1.1
w	5.4	0.8
+3	6.4	-0.2
cb	6.5	-0.3
1/4	6.4	-0.2
£	6.6	-0.4
1/4	6.8	-0.6
cb	6.2	0.0
E	6.3	-0.1

7 6.24

75

out 20	5.0	1.2
	0+75	
out 20	4.9	1.3
E	4.9	1.3
cb	6.4	-0.2
1/4	6.8	-0.6
£	7.0	-0.8
1/4	6.4	-0.2
cb	6.5	-0.3
£	6.5	-0.3
w	5.2	1.0
out 20	5.0	1.2
	1+00	
out 20	4.8	1.4
w	4.8	1.4
+5	6.0	0.2
cb	6.0	0.2
1/4	6.3	-0.1
£	6.0	0.2
1/4	6.1	0.1
cb	6.2	0.0
E	5.5	0.7
out 20	4.8	1.4

76.24

1+25

Out 20	4.7	15
E	5.7	05
cb	6.2	00
1/4	6.2	00
¢	6.1	01
1/4	6.0	02
cb	6.2	00
+4	6.0	02
w	5.1	11
Out 20	4.5	17

1+50

Out 20	4.7	1.5
w	4.5	1.7
+5	5.8	0.4
cb	5.9	0.3
1/4	5.8	0.4
¢	5.9	0.3
1/4	6.0	0.2
cb	6.3	-0.1
+8	6.0	0.2
E	5.2	1.0
Out 20	4.5	1.7

76.24

1+75

Out 20	4.3	19
E	5.1	11
cb	5.5	07
1/4	5.5	07
¢	5.4	08
1/4	5.4	08
cb	5.4	08
+8	5.4	08
w	4.9	13
Out 20	4.6	16

2+00

Out 20	4.6	16
Out 4	4.3	19
w	5.1	11
+2	5.7	05
cb	5.6	06
1/4	5.6	06
¢	5.6	06
1/4	5.6	06
cb	5.6	06
+5	5.8	04
E	4.5	17
Out 20	4.4	18

76

T 6.24

2+25

Out 20	4.4	1.8
E	4.6	1.6
+8	5.9	0.3
cb	6.1	0.1
1/4	5.7	0.5
♀	5.7	0.5
1/4	5.8	0.4
cb	5.8	0.4
+8	5.7	0.5
W	5.2	0.5
Out 4	4.4	1.8
Out 20	4.7	1.5

2+50

Out 20	4.6	1.6
Out 3	4.6	1.6
W	5.1	1.1
+4	5.9	0.3
cb	6.0	0.2
1/4	6.0	0.2
♀	6.2	0.0
1/4	6.4	-0.2
+7	6.0	0.2
cb	5.0	1.2
E	4.5	1.7
Out 20	4.4	1.8

T 6.24

2+75

Out 20	4.6	1.6
E	4.6	1.6
cb	5.4	0.8
+6	6.5	-0.3
1/4	6.7	-0.5
♀	6.9	-0.7
1/4	6.9	-0.7
cb	6.5	-0.3
+7	6.3	-0.1
W	5.3	0.9
Out 20	4.6	1.6

(2400 = N.L. Main

80' wide 13' 1/2 S
14' cbs

Out 20	4.8	1.4
Out 5	4.8	1.4
W	6.8	-0.6
cb	7.1	-0.9
1/4	6.7	-0.5
♀	6.5	-0.3
1/4	6.7	-0.5
cb	6.4	-0.2
+6	5.0	1.2
E	4.9	1.3
Out 20	4.7	1.5

76.24

N. cb Main

Out 20	4.6	1.6	
E	4.8	1.4	S
cb	6.1	0.1	R
1/4	6.2	0.0	N
R	6.2	0.0	
1/4	6.4	-0.2	N
cb	6.4	-0.2	R
W	6.5	-0.3	S
Out 5	5.1	1.1	
Out 20	4.6	1.6	S
N. cb + 5			R
Out 20	4.4	1.8	N
W	4.9	1.3	
cb	4.6	1.6	N
+ 8 ft. gas & Electric M.H. on top	4.40	1.84	R
1/4	4.5	1.7	S
R	4.5	1.7	
1/4	4.5	1.7	S
cb	4.7	1.5	R
E	4.6	1.6	N
Out 20	4.7	1.5	

76.24

Levels on Main St Parking 36' Strip
100' West of W.L. Main Rig? 78

4.90	1.34
4.30	1.94
4.50	1.74

50' West

4.62	1.62
4.48	1.76
5.10	1.14

W.L. Main Rig?

5.42	0.82
4.65	1.59
4.94	1.30

W. Main Rig?

4.92	1.32
4.72	1.52
5.47	0.67

E.L. Main Rig

5.39	0.85
4.70	1.54
4.97	1.27

50' East

4.75	1.49
4.52	1.72
5.16	1.08

120
130
140
150
160

π 6.24

100' East

S	4.92	1.32
φ	4.34	1.90
N	4.64	1.60

Levels in φ Alley North of Main

E.L. Rigel = 0+00	5.3	0.9
+25	4.5	1.7
+50	4.6	1.6
+75	4.9	1.3
+100	5.0	1.2
+25	4.9	1.3
+50	5.1	1.1
+75	5.0	1.2
+200	4.7	1.5

BM. N.W. Spike in Pole Main & Rigel 3.31 - 2.93

Correct = 2.90

+3.78

W?

π 6.68

E.L. Rigel = 0+00	5.1	1.6
+25	5.2	1.5
+50	4.9	1.8
+75	5.7	1.0
+82	4.4	2.3
+100	4.6	2.1
+25	5.0	1.7
+50	5.1	1.6

π 6.68

79

+75	7.2	-0.5	5+75	8.9	-2.2
+200	7.3	-0.6	+82	8.6	-1.9
+25	7.7	-1.0	+87	7.7	-1.0
+50	8.3	-1.2	+98	8.1	-1.4
+62	8.7	-2.0	6+00 = E.L. Photo	60' wide	
+75	8.0	-1.3	↳	9.1	-2.4
3+00	7.6	-0.9	+8	11.8	-5.1
+15	8.2	-1.5	+18	12.2	-5.5
+25	7.4	-0.7	+20	13.3	-6.6
+50	8.0	-1.3	↳	13.3	-6.6
+75	8.2	-1.5	+3	12.7	-6.0
+81	8.5	-1.8	+20	13.2	-6.5
+86	10.5	-3.8	+25	12.5	-6.8
+90	10.8	-4.1	W.L. Photo ⁵⁰⁰⁰	13.0	-6.3
+100	10.5	-3.8	+07	7.8	-1.1
+109	8.8	-2.1	+25	6.6	+0.1
+25	9.3	-2.6	+33	8.3	-1.6
+32	8.1	-1.4	+50	8.7	-2.0
+41	11.0	-4.3	+75	8.6	-1.9
+50	11.3	-4.6	+100	8.9	-2.2
+68	11.1	-4.4	+07	8.0	-1.3
+75	9.4	-2.7	+30 = Approximate		
5+00	8.3	-1.6	Intersection with Chillas		
+25	8.4	-1.7	Trunk line sewer		
+50	8.4	-1.7	↳ +4.0		

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

$$\begin{array}{r} 1227.3 \\ 60 \overline{) 7362} \\ \underline{6000} \\ 362 \\ \underline{360} \\ 2 \end{array}$$

$$\begin{array}{r} 22.8 \\ 2 \overline{) 45.6} \\ \underline{45.6} \\ 0 \end{array}$$

$$\begin{array}{r} 60 \\ 17.7 \overline{) 1062} \\ \underline{1062} \\ 0 \end{array}$$

290

35

17-30

315.30

48.53

ENGINEERING DEPARTMENT,
CITY OF SAN DIEGO,
CALIFORNIA.

221
222.2
543.4
271.2

140
35
105
72

34 ^m	NE MON	99.26
35 ^m	NW 11	56.62
36 ^B	SE 8P	195.08
33 ^d	WNW	106.50

283.2
206.7
76.5

200