1335
MURRAY

EASTY

FIELD BOOK

No. 335 F

Our Leather Bound Engineers Note Books are carried in the following rulings:

No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.

No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.

No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.

No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

We also carry the Note Books listed above, bound in extra strong Fabri-Hide (otherwise the same quality of book), which can be furnished at a somewhat lower price.

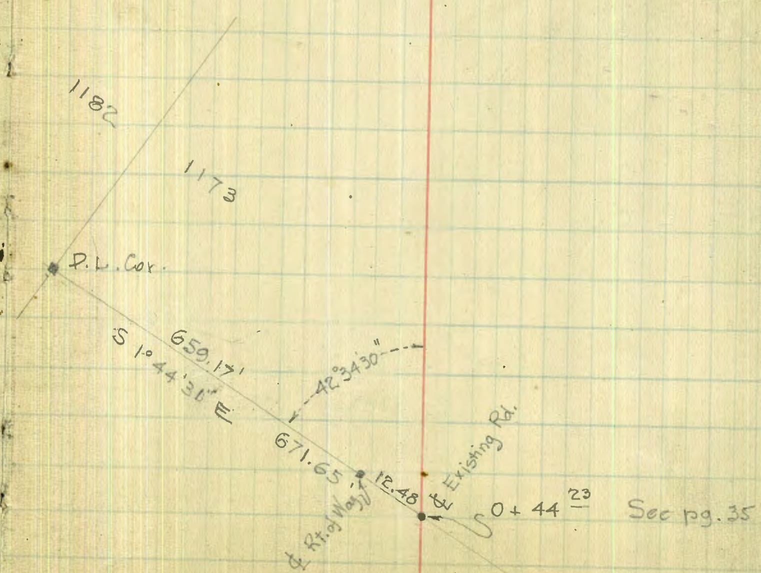
In ordering Fabri-Hide covered books, add the letter *"F"* to catalog number.

℄ Existing Murray Canyon Rd. from Intersection with P.L.L. 1174 & 1173

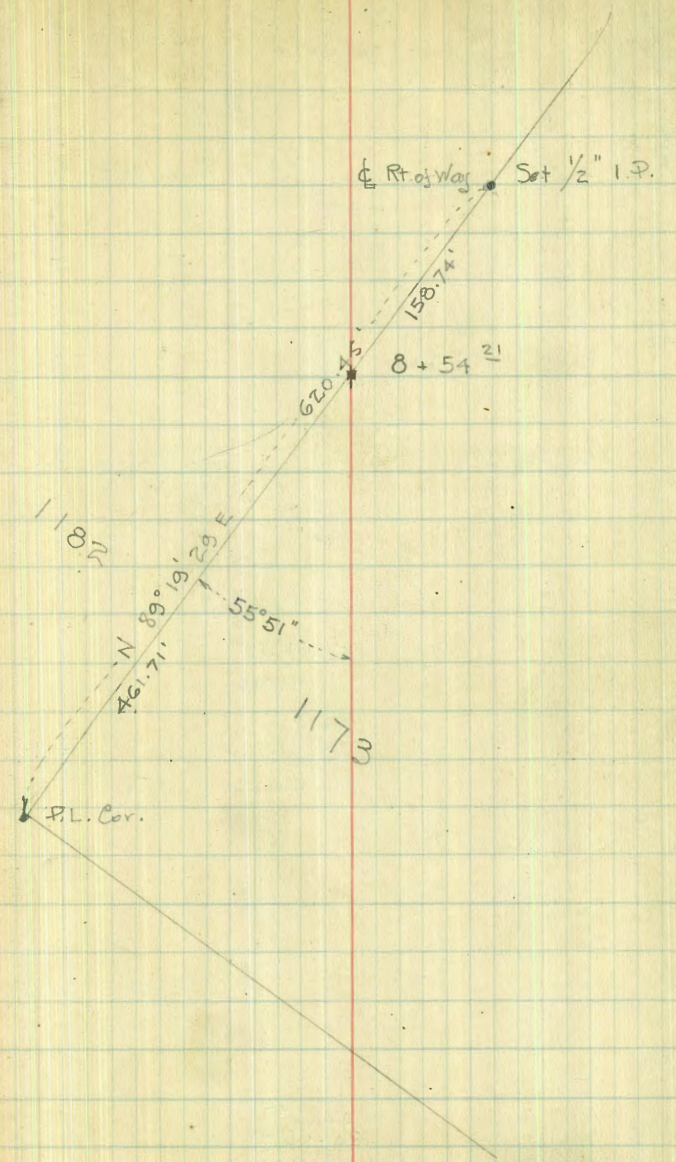
STA	Align.	Defl.∠	Curve Data	True Bearing	Dist. from P.I. - P.I.
4+01.82	B.C.	Rt.			
4+00				N27°09'00"E	273.97
3+53.36	E.C.				
3+00			Δ = 13°43'		
			2Δ = 27°26'		P.I.
			R = 950'		
			T = 114.26		
			L = 227.43 ✓		
2+00					
1+25.93	B.C.	Lt.			
				N40°52'00"E	195.97
1+00					
0+44.23	= 19+51.88	See pg. 35			

JAEGER
Bailey
Brooks
Clavert
} April 8th 1929.

Roll 3597



STA	Align.	Defl. ∠	Curve Data	True Bearing	Dist. from P.I. to P.I.
9+54.55	B.C.	Rt.			
9+00					
8+54.21	P.O.T				
8+00				N 33°31'00" E	500.78
7+00					
6+24.06	E.C.				
6+00					
			Δ = 6°22'		
			2Δ = 12°44'		P.I.
			R = 2000'		
5+00			T = 111.23		
			L = 222.24		



Sta	Align.	Defl. ∠	Curve Data	True Bearing	Dist. from P.I. to P.I.
14+32.52	B.C.	Lt.			
	14.22				
14+18.30	E.C.		Δ = 72°02'30"	N 63°15'30" E	90.92
			2Δ = 144°05'		
			R = 50'		
14+00			T = 36.35 ✓		P.I.
			L = 62.87 ✓		
13+55.43	B.C.	Lt.			
	86.75			S 44°42'00" E	191.68
13+00					
12+68.68	E.C.				
			Δ = 68°53'		
			2Δ = 137°46'		
			R = 100'		
12+00			T = 68.58 ✓		P.I.
			L = 120.22 ✓		
11+48.46	B.C.	Rt.			
11+00				N 66°25'00" E	206.70
10+69.39	E.C.				
			Δ = 32°54'		
			2Δ = 65°48'		
			R = 200'		
			T = 59.05 ✓		
10+00			L = 114.84 ✓		
					P.I.

36.35
14.22
40.35
90.92

STA	Align.	Defl. ∠	Curve Data	True Bearing	Dist. from P.I. to P.I.
19+00					
	359.76				
18+00				N19°18'30"E	720.31
17+18.09	P.O.T.				
17+00					
	208.77				
16+00					
15+09.23	E.C.		Δ = 43°57'		
15+00			ΣΔ = 87°54'		
			R = 100'		
			T = 40.35 ✓		
			L = 76.71 ✓		P.I.

208.77
40.35
249.12

Sta	Align.	Defl. ∠	Curve Data	True Bearing	Dist. from P.I. To P.I.
24+01.73	B.C.	Lt.			
24+00					
				N32°01'30"E	291.57
	102.02				
23+00					
22+99.71	E.C.				
			Δ = 12°43'		
			2Δ = 25°26'		
22+00	21+89.19		R = 1000'		~~P.I.~~
			T = 111.43 ✓		
			L = 221.95 ✓		
21+00					
20+77.76	B.C.	Rt.			
20+00					

24+01.73
78.12
24+79.85

Sta	Align.	Defl. ∠	Curve Data	True Bearing	Dist from P.I. To P.I.
29+00					
28+00					583.50'
	453.49				
27+00					
26+00					
25+57.65	E.C.				
			Δ = 8°56'		
			2Δ = 17°52'		
			R = 1000'		
			T = 78.12' ✓		
25+00	24+79.85		L = 155.92' ✓		P.I.

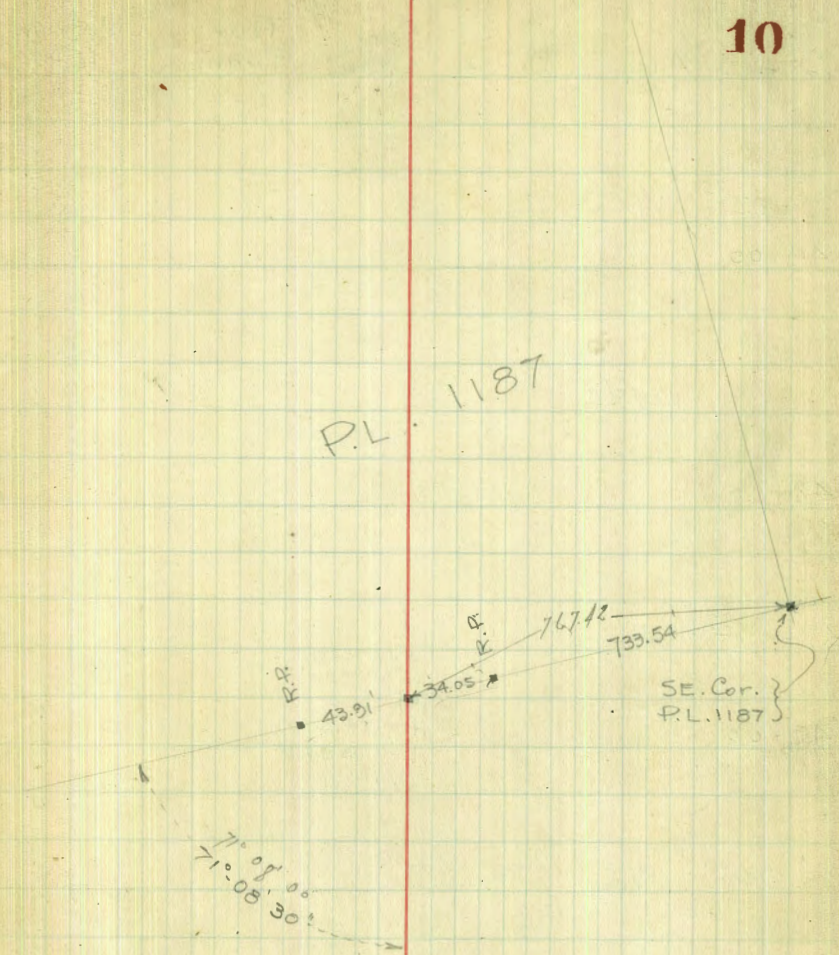
STA	Align.	Defl. ∠	Curve Data	True Bearing	Dist. from P.I. to P.I.
			Δ = 20°40' 2Δ = 41°20' R = 200' T = 36.47' ✓ L = 72.14' ✓		P.I.
34+24 41	B.C.	Lt.			
34+00					148.48
	84.92				
33+39 49	E.C.				
			Δ = 30°19' 2Δ = 60°38' R = 100' T = 27.09' ✓ L = 52.91' ✓		P.I.
33+00					
32+86 58	B.C.	Lt.			
	172.23'				251.21
32+00					
31+14 35	E.C.				
			Δ = 14°47' 2Δ = 29°34' R = 400' T = 51.89' ✓ L = 103.21' ✓		
31+00					
	30+63 03				P.I.
30+11 14	B.C.	Rt.			
30+00					

30+11.14
- 51.89
30+63.03

179-60
14-47
2) 165-13
82-34-30

Sta	Align.	Defl.	Curve Data	True Bearing	Dist. from P.I. to P.I.
39+73.02	E.C.		$\Delta = 31^\circ 18' 15''$		
			$\Delta = 31^\circ 18'$		
			$2\Delta = 62^\circ 36' 30''$		
			$R = 300'$		
			$T = 84.05'$ ✓		
39+00			$L = 163.89'$ ✓		P.I.
			91		
38+09.12	B.C.	Rt.			
38+00					
					301.13'
	183.30				
37+00					
36+25.83	E.C.				
			$\Delta = 12^\circ 51'$		
			$2\Delta = 25^\circ 42'$		
36+00			$R = 300'$		P.I.
			$T = 33.78'$ ✓		
			$L = 67.28'$ ✓		
35+58.55	B.C.	Rt.			
	62.00'				132.25'
35+00					
34+96.55	E.C.				

Sta.	Align.	Defl. ∠	Curve Data	True Bearing	Dist. from P.I. to P.I.
	308.88'				
44+00					
43+25.81	E.C.		Δ = 16°13'30"		
43+00			Δ = 16°13' 2D = 32°27' R = 300' T = 42.76' L = 84.95'		P.I.
42+40.86	B.C.	Lt.			
42+19.03	P.O.T.	Intersection with S.L. of P.L. 1187			
42+00					210.12'
	130.19'				
41+10.67	E.C.		Δ = 12°07'30"		
41+00			Δ = 12°07' 2D = 24°15' R = 350' T = 37.17' L = 74.07'		P.I.
40+36.66	B.C.	Lt.			
40+00					184.80'
	63.58'				



Sta	Align.	Defl.	Curve Data	True Bearing	Dist. from P.I. to P.I.
49+23.75	B.C.	Lt.			
49+00					
					320.98'
	180.22'				
48+00					
47+43.53	E.C.		Δ = 17°49' 2Δ = 35°38' R = 350' T = 54.86' ✓ L = 108.84' ✓		
47+00					P.I.
46+34.69	B.C.	Rt.			
46+00					
45+00					406.50'

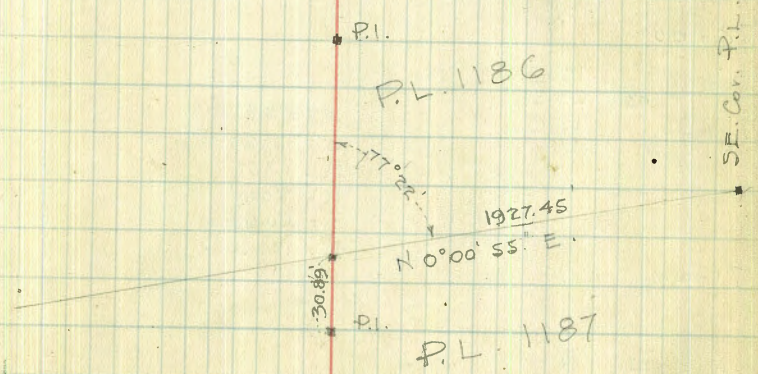
Sta	Align	Deft. x	Curve Data	True Bearing	Dist. from P.I. to P.I.
	43.73				
54+44.21	E.C.				138.01
			Δ = 18°06'		
			2Δ = 36°12'		
			R = 300'		
			T = 47.78' ✓		
54+00			L = 94.77' ✓		P.I.
53+49.44	B.C.	Rt.			123.40'
	36.74'				
53+12.70	E.C.		Δ = 42°29'-30"		
			Δ = 42°30'		
53+00			2Δ = 84°59'		
			R = 100'		
			T = 38.88' ✓		P.I.
			L = 74.16' ✓		
52+38.54	B.C.	Lt.			
					120.25'
	44.91'				
52+00					
51+93.63	E.C.				
			Δ = 27°18'30"		
			2Δ = 54°37'		P.I.
			R = 150'		
			T = 36.46' ✓		
			L = 71.49' ✓		
51+22.14	B.C.	Rt.			
51+00	27.45'				149.81'
50+94.69	E.C.				
			~~Δ = 13°59'-30"~~		
			Δ = 14°00'		
			2Δ = 27°59'		
			R = 700'		
			T = 85.90 ✓		P.I.
			L = 170.94' ✓		
50+00					

STA	Align.	Defl. ∠	Curve Data	True Bearing	Dist. from P.I. to P.I.
			Δ = 10°05'		
			2Δ = 20°10'		
			R = 500'		P.I.
			T = 44.11 ✓		
59+02 45	B.C.	Lt.	L = 87.99' ✓		
59+00	14.02				78.73'
			Δ = 23-16'30"		
58+88 43	E.C.		Δ = 23°16'		
			2Δ = 46°33'		P.I.
			R = 100'		
			T = 20.60 ✓		
58+47 81	B.C.	Rt.	L = 40.62' ✓		
	50.31'				105.57'
58+00			Δ = 49°36'30"		
			Δ = 49°37'		
57+97 58	E.C.		2Δ = 99°13'		
			R = 75'		P.I.
57+32 56	B.C.	Lt.	T = 34.66 ✓		
	27.33'		L = 64.94 ✓		
57+05 23	E.C.				104.94'
			Δ = 24°14'30"		
57+00			2Δ = 48°29'		
			R = 200'		P.I.
			T = 42.95 ✓		
			L = 84.62' ✓		
56+20 61	B.C.	Rt.			
56+00	37.73				127.18'
55+82 88	E.C.		Δ = 5°19'30"		
55+80 00 =			Δ = 5°19'		
			2Δ = 10°39'		
			R = 1000'		
			T = 46.50 ✓		P.I.
			L = ~~94.94~~ 92.94'	2' error C.B.K.	
55+00					
54+87 24	B.C.	Rt.			

STA	Align.	Defl. ∠	Curve Data	True Bearing	Dist. from P.I. to P.I.
64+77.68	E.C.				157.43'
			Δ = 5°36'		
			2Δ = 11°12'		
			R = 1500'		
			T = 73.37' ✓		P.I.
64+00			L = 146.71' ✓		
63+30.97	B.C.	Lt.			
	28.91'				143.70'
63+02.06	E.C.				
63+00			Δ = 45°00'		
			R = 100'		
			T = 41.42' ✓		P.I.
			L = 78.54' ✓		
					83.33
62+23.52	P.C.C.	Rt.			
			Δ = 38°30'		
62+00			R = 120'		
			T = 41.91' ✓		
			L = 80.63' ✓		P.I.
61+42.89	B.C.	Rt.			
61+00	87.14'				161.78'
60+55.75	E.C.				
			Δ = 9°26'		
			2Δ = 18°52'		
			R = 396.69'		P.I.
			T = 32.73' ✓		
60+00			L = 65.31' ✓		
59+90.44	P.R.C.	Rt.			76.84'

Sta	Align.	Defl. ∠	Curve Data	True Bearing	Dist. from P.I. to P.I.
			$\Delta = 6°10'15"$		
			$\Delta = 6°10'$		
			$2\Delta = 12°20'30"$		P.I.
			$R = 1000'$		
			$T = 53.91'$ ✓		
			$L = 107.70'$ ✓		
69+00					
68+97.94	B.C.	Lt.			
	148.97'				257.04'
68+00					
67+48.97	E.C.				
			$\Delta = 6°12'$		
			$2\Delta = 12°24'$		
			$R = 1000'$		
67+00			$T = 54.16'$ ✓		P.I.
			$L = 108.21'$ ✓		
66+40.76	B.C.	Lt.			133.78
	6.95'				
66+33.81	E.C.				
			$\Delta = 12°45'30"$		
			$\Delta = 12°46'$		
66+00			$2\Delta = 25°31'$		
			$R = 650'$		
			$T = 72.67'$ ✓		P.I.
			$L = 144.74'$ ✓		
65+00					
64+89.07	B.C.	Rt.			
	11.39'				

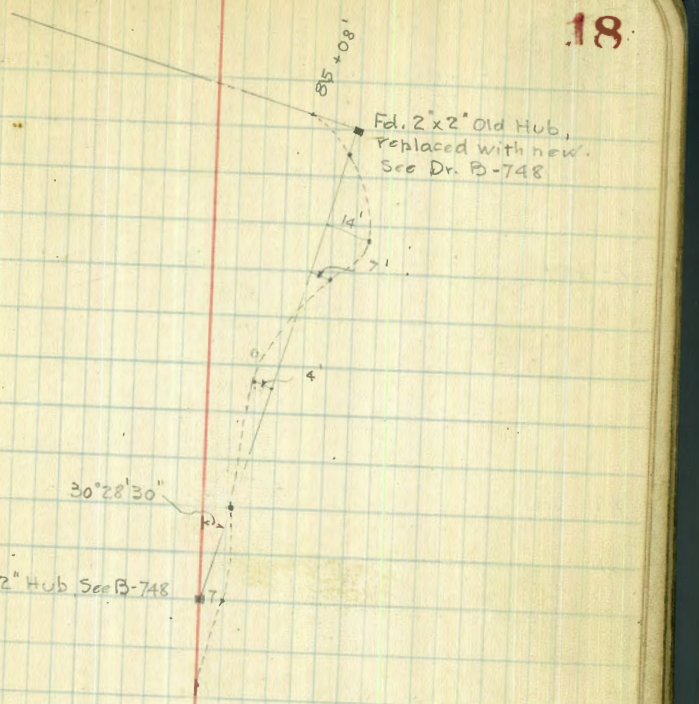
77 - 22
154 - 44



Sta	Align.	Defl. ∠	Curve Data	True Bearing	Dist. from P.I. to P.I.
	193.47'				
74+00					283.66'
73+04.81	E.C.				
73+00					
			Δ = 3°37'		
			2Δ = 7°14'		
			R = 2000'		
			T = 63.16'		P.I.
			L = 126.25' ✓		
72+00					147.37'
71+78.56	B.C.	Rt.			
71+55.03	23.53' E.C.				
			Δ = 3°28'30"		
			Δ = 3°29'		
			2Δ = 6°57'		
			R = 2000'		
			T = 60.68' ✓		P.I.
			L = 121.30' ✓		
71+00					
70+33.73	B.C.	Rt.			
	28.09'				
70+05.64	E.C.				142.68'
70+00					

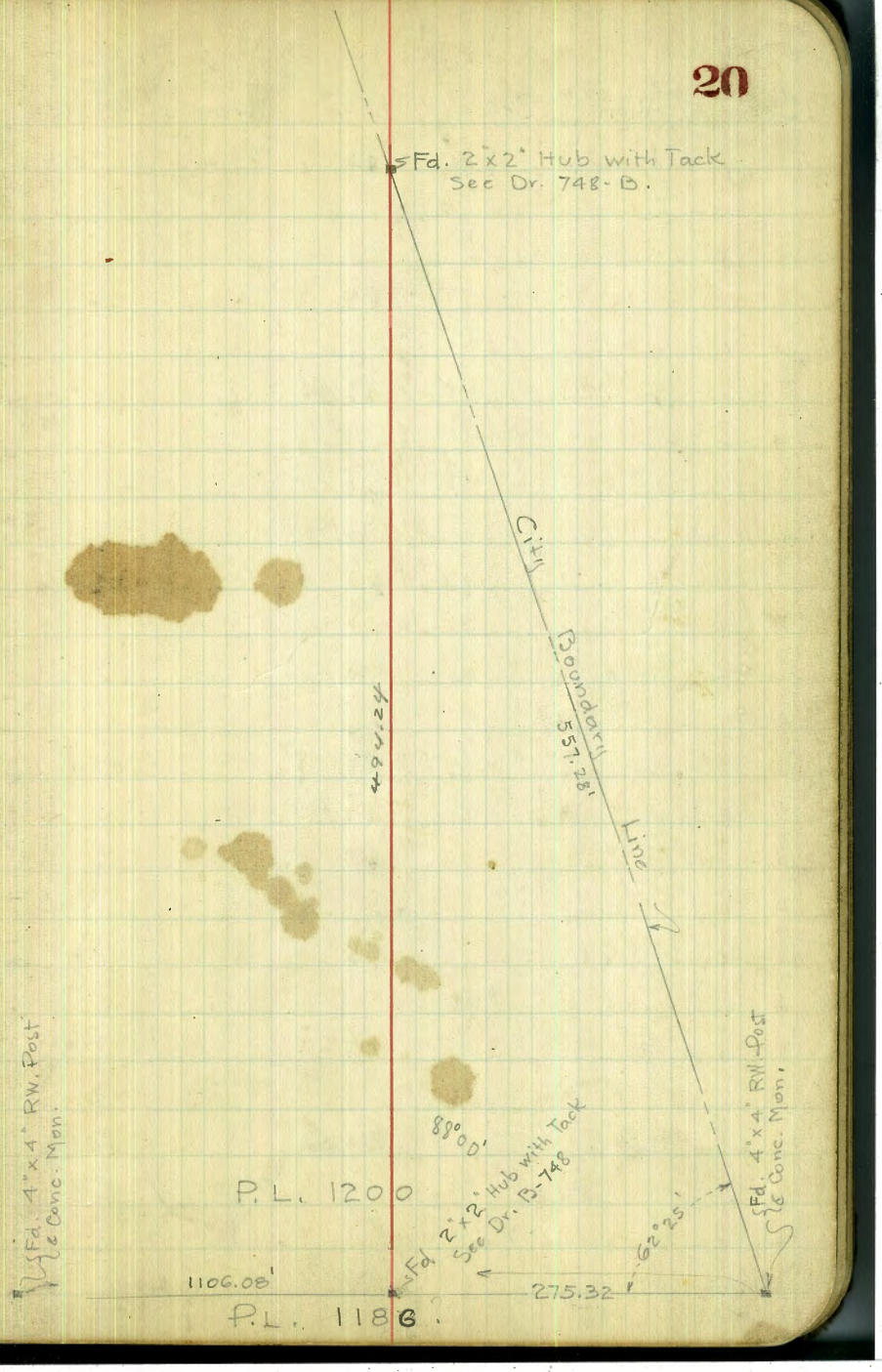
Sta	Align.	Defl. ±	Curve Data	True Bearing	Dist. from P.I. To P.I.
79+37.88	B.C.	Lt.			
	41.32'				101.20
79+00			Δ=15°28'30"		
78+96.56	E.C.		Δ = 15°29'		
			2Δ = 30°57'		
			R = 200'		P.I.
			T = 27.18' ✓		
78+42.59	B.C.	Rt.	L = 54.02' ✓		
78+00					
	170.97'				259.73'
77+00					
76+71.57	E.C.				
			Δ = 14°33'		
			2Δ = 29°06'		P.I.
			R = 482.38'		
			T = 61.58' ✓		
			L = 122.50' ✓		
76+00					
					88.61'
75+49.07	P.R.C.	Rt.			
			Δ = 48°30'		
			2Δ = 97°00'		
			R = 60'		P.I.
			T = 27.03' ✓		
			L = 50.79' ✓		
75+00					
74+98.28	B.C.	Lt.			

Sta	Alingn.	Defl. ∠	Curve Data	True Bearing	Dist. from P.I. to P.I.
84+96.24		Lt.	Δ = 90°		P.I.
84+00					
					220.0'
83+00					
			Δ=30°28'30"		
82+76.24	P.I.	Rt.	Δ = 30°29'		P.I.
			2Δ = 60°57'		
82+00					
	199.04'				216.24
81+00					
80+77.20	E.C.		Δ = 15°05'		
80+42.95	B.C.	Rt.	2Δ = 26°10'		P.I.
			R = 150'		
	41.27'		T = 17.20'		
			L = 34.25'		
80+01.72	E.C.				91.17'
80+00			Δ = 30°29'		
			2Δ = 60°58'		
			R = 120'		
			T = 32.70'		P.I.
			L = 63.84'		



Sta	Align.	Defl. ∠	Curve Data	True Bearing	Dist. from P.I. To P.I.
89+00					
88+00					
					500.00'
87+00					
86+00					
85+00					
84+96.24					P.I.

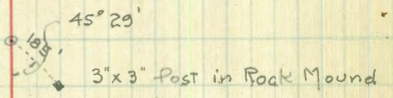
Sta	Align.	Defl. ∠	Curve Data	True Bearing	Dist. from P.I. to P.I.
94+90.48					P.I.
94+00					
93+00					
					494.24'
92+00					
91+00					
90+00					
89+96.24	P.O.T.				P.I.



STA	Align.	Defl.'s	Curve Data	True Bearing	Dist. from P.I. to P.I.

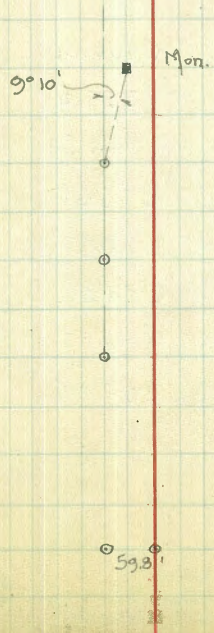
Pueblo Random Line from S.E. Cor. P.L. 1200 West

STA	Slope Dist	V.A.	Hor. Dist.	Defl. ∠	Bearing
△ 11					
	212.89	5°25'	211.94		West
△ 10					
	54.77'	26°40'	48.94'		West
△ 9					
	500.0'	13°24'	486.39'		West
△ 8					
	500.0'	15°40'	481.43'		West
△ 7					
	440.00'	9°15'	434.28'		West
△ 6					
			67.00'		West
△ 5					
			96.43'		West
△ 4					
			500'		West
△ 3					
	500'	1°02'	499.92		West
△ 2					
			275.32'		West
△ 1	Concrete Mon. on City Boundary Line				



Gregory's Hub in ℄ Highway. See Dr # 748-B.
Bearing from Dr. # 748-B.

STA	Slope Dist.	VA.	Hor. Dist.	Deff. ∡	Bearing
□ 17	Granite	Mon.	N.W. Cor. P.L. 1187		
	176.46'	2°05'	176.34		N 81°14' W
△ 16				9°10'-R	
	129.70'	8°18'	128.34'		S 89°36' W
△ 15					
	500.0'	2°30'	499.53'		S 89°36' W
△ 14					
	336.0'	1°17'	335.92'		S 89°36' W
△ 13				89°36'-R	
			59.80'		South
△ 12				90°00'-L	
			504.89		West



			6.73		0.82	79162
cos	89-36	=	7.84	39338		
log	963.79	=	2.98	39824		
dm	89-36	=	9.99	99894		
	963.77		2.98	39718		
	26.88		1.42	93668		
cos	81°14'	=	9.18	30160		
log	176.34	=	2.24	63508		
dm	81°14	=	9.99	48964		
	174.28		2.24	12472		

	N	E
	5000.00 ①	5000.00
	4960.35 (17)	255.41
	39.65	4744.59
	4743.91'	3.67 61361
- dm	0°28.44	= 7.92 21071
log	39.65	= 1.59 82432
- "	4744.59	= 3.67 61987
dy	0°28'44"	7.92 20445
	89-59-60	
	0-28-44	
S	89-31-16 W	

STA	Bearing	Dist	N	S	E	W
Δ 1			5000.00		5000.00	Conc. Mon.
	West	3606.54				3606.54
Δ 12			5000.00		1393.46	
	South	59.80		59.80		
Δ 13			4940.20		1393.46	
	S 89°36' W	963.79		6.73		963.77
Δ 16			4933.47		429.69	
	N 81°14' W	176.34	26.88			174.28
Δ 17			4960.35		255.41	
						Gran. Mon.

Δ 1		
	S 89° 31' 16" W	4743.91'
Δ 17		

0 1000 2000 3000 4000 5000

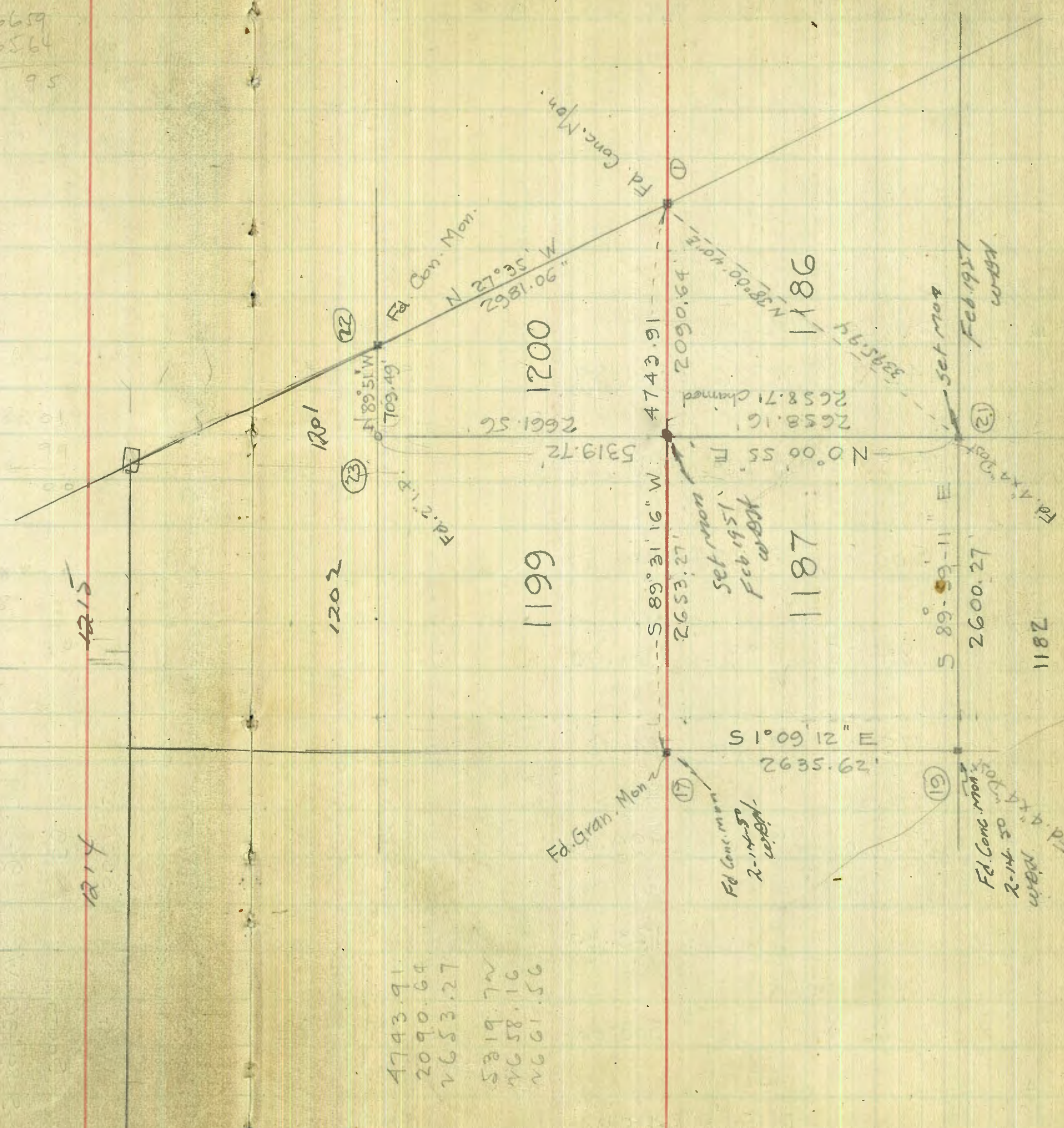
5000

4500

	2509.96	= 3.39 96659	6659 / 6564 / 95
Cos	0°18'16"	= 9.99 99939	
log	2509.99	= 3.39 96720	
sin	0°18'16"	= 7.72 53834	
	13.34	= 1.12 50554	
	125.40	= 2.09 83067	
cos	27°53'44"	= 9.94 63549	
log	141.89	= 2.15 19518	
sin	27°53'44"	= 9.67 01171	
	66.39	1.82 20688	

N		E
4960.35	(17)	255.41
2324.99	(19)	308.46
2635.36		53.05

	2635.62	3.42 08825
- sin	1°09'12"	= 8.30 38029
log	53.05	= 1.72 46854
- "	2635.36	= 3.42 08400
	1°09'12"	8.30 38454



Random Line on W.L. of P.L. 1187 from NW. Cor. P.L. 1187 to SW. Cor. 1187

Sta	Slope Dist	V.A.	Hor. Dist.	Dgl.'s	Bearing
■ 17					
	416.0'	0°58'	415.94'		
△	NW. Cor. P.L. 1187				S 0°18'16" W
△			128.30'		
△	500.0'	1°22'	499.86'		
△	75.12'	7°30'	74.48'		
△	184.05'	0°36'	184.03'		
△	500.0'	2°23'	499.57'		
△	208.10'	3°00'	207.81'		
△ 18				28°12'-L	
	145.30'	12°26'	141.89		S 27°53'44" E
■ 19	SW. Cor. P.L. 1187				

Sta	Bearing	Dist.	N	S	E	W
△ 17			4960.35		255.41	
	S 0°18'16" W	2509.99		2509.96		13.34
△ 18			2450.39		242.07	
	S 27°53'44" E	141.89		125.40	66.39	
△ 19			2324.99		308.46	
△ 17						
	S 1°09'12" E	2635.62				
△ 19						

Random Line on S.L. P.L. 1187
from SW. Cor. P.L. 1187 to SE. Cor. 1187

STA	Slope Dist.	V.A.	Hor. Dist.	Defl. ∠	Bearing
■ 21	SE. Cor. P.L. 1187				
			37.94'		
	500.00'	0°48'	499.95'		S85°31'E
△ 20				5°38'-R	
	279.78'	27°12'	248.84'		
△					
	500.00'	16°06'	480.39'		
△					
	93.12'	6°43'	92.48		
△					
			66.0'		
△					
	110.00	29°55'	95.34'		
△					
	500.00'	8°41'	494.27'		
△					
	119.00'	9°30'	117.37'		
△					
			21.62'		
△					
	450.00'	5°13'	448.14'		N88°51'E
■ 19	SW. Cor. P.L. 1187				

STA	BEARING	Dist	N	S	E	W
△ 19			2324.99		308.46	
△ 20	N 88° 51' E	2064.45'	41.43		2064.03	
△ 21	S 85° 31' E	537.89'	2366.42	42.05	2372.49	
△ 19			2324.37		2908.73	
△ 21	S 89° 59' 11" E	2600.27	2324.99	0.64W	308.46	
			2324.37		2600.27	
					2908.73	

✓	41.43	= 1.61	73504	
cos	88-51	= 8.30	25460	✓
log	2064.45	= 3.31	48044	✓
tan	88-51	= 9.99	99125	✓
✓	2064.03	= 3.31	47169	
✓	42.05	= 1.62	37286	
cos	85-31	= 8.89	30351	✓
log	537.89	= 2.73	06935	✓
tan	85-31	= 9.99	86691	✓
✓	536.24	= 2.72	93626	
	N		E	
	2324.99	(19)	308.46	
	2324.37	(21)	2908.73	
	0.62		2600.27	
	2600.27	3.41	50185	
- cos	89°59'11"	= 6.37	73732	
log	0.62	= 9.79	23917	
- log	2600.27	= 3.41	50185	
cot	89°59'11"	= 6.37	73732	
	89-59-60			
	0-00-49			
∴	89-59-11 E			

.7939
105
8044

7169
7097
72

/

0068
33
0101

From SE. Cor. P.L. 1200 along City's Boundary Line to NE. Cor. P.L. 1200, thence West to NW. Cor. PL. 1200

STA	Slope Dist.	V.A.	Hor. Dist.	Defl. ∠	Bearing
○ 23	Fd. 2" I.P.				
	450.00'	5°28'	447.95		
△					
	264.0'	7°50'	261.54'		N 89°51' W
■ 22	Fd. Conc. Mon. & 4"x4" Post.			62°16'-L	
	88.0'	25°40'	79.32'		
△					
	54.00	2°55'	53.93'		
△					
			430.00'		
△					
	183.65'	2°24'	183.20'		
□	Fd. Conc. Mon. & 4"x4" Post.				
	196.00'	2°58'	195.74		
△					
			500.00'		
△					
	500.00	1°26'	499.87'		
■	Fd. Conc. Mon. & 4"x4" Post.				
			1039.00		N27°35' W
■ ①	SE. Cor. P.L. 1200				

NW. Cor. P.L. 1200

NE. Cor. P.L. 1200

	2642.23	3.42197 02	
Cos	27-35	= 9.94 75995	3620 / 87 / 3707
log	2981.06	= 3.47 43707	
sin	27-35	= 9.66 56168	
	1380.35	3.13 99875	
	1.86	0.26 89144	
Cos	89-51	= 7.41 79681	
log	709.49	= 2.85 09463	
sin	89-51	= 9.99 99985	
	709.49	2.85 09448	
	N		E
	7644.09	(23)	2910.16
	2324.37	(21)	2908.73
	5319.72		143
	5319.72'	3.72 58887	
- sin	0°00'55"	= 6.42 94473	
log	1.43	= 0.15 53360	
- =	5319.72	= 3.72 58887	
to N	0°00'55"	E 6.42 94473	

STA	BEARING	Dist.	N	E	S	W
1			5000.00	5000.00		
22	N 27°35' W	2981.06	2642.23	3619.65		1380.35
23	N 89-51 W	709.49	7642.23 / 1.86 / 7644.09	2910.16		709.49
21	N 0°00'55" E	5319.72				
23			5000.00	5000.00		
1			2675.63	2091.27		2881 / 134 / 3015
21	N 51-22-18 E	3723.36	2324.37	2908.73		

3956 / 145 / 4101

4212 / 49 / 4261

9549 / 9603 / 54

5946 / 100 / 6046

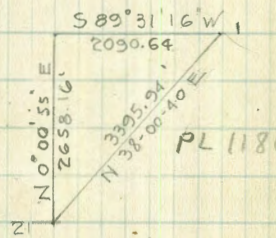
3395.94 = 3.5309603

+ sin 38-00-40 = 9.7894498

log 2091.27 = 3.3204101

- = 2675.63 = 3.4274261

N 38-00-40 E = 9.8929840



log 3395.94 = 3.5309603

- Cos 0°29'39" = 9.9999838

3.5309765

+ sin 51°30'36" = 9.8936046

2658.16 3.4245811

3.5309765

+ sin 37°59'45" = 9.7893015

2090.64 3.3202780

9704 / 9657 / 45

9875 / 9735 / 140

8871 / 16 / 8887

True Line from SE. Cor. P.L. 1187 N 0-05-27 E
to set NE. Cor. P.L. 1187

Sta	Slope Dist.	V.A.	Hor. Dist.	Defl. &	Bearing
□					
			5.85		
△					
	100.0'	24°30'	91.00		
△					
	124.0'	10°43'	121.84		
△					
	217.0	0°10'	217.00		
△ X					
	366.90'	1°42'	366.74'		
△					
	93.00	4°22'	92.73'		=
△					
	475.00	0°13'	474.99'		
△					
	500.00	0°38'	499.97'		
△					N 0°00'55" E.
	186.00'	6°00'	184.98'		
△					
	242.00'	4°26'	241.28'		
△					
	366.00'	8°09'	362.30		
■	SE. Cor. P.L.		1187.	90°00'06"	

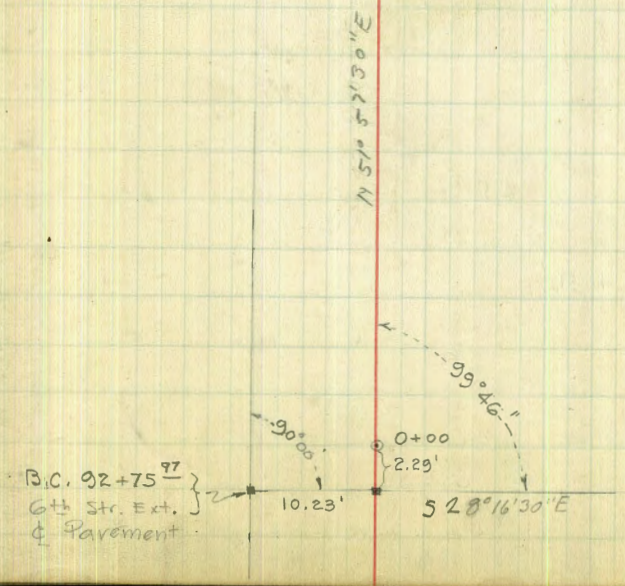
Set by Intersection.

■ Set Granite Mon. with L & T. an 4"x4" Post

2658.71 chained
2658.16 computed

℄ Existing Murray Canyon Rd. from B.C. 92+60.36 of 6th Street Extension Alignment to 0+00 (See pg. 2)

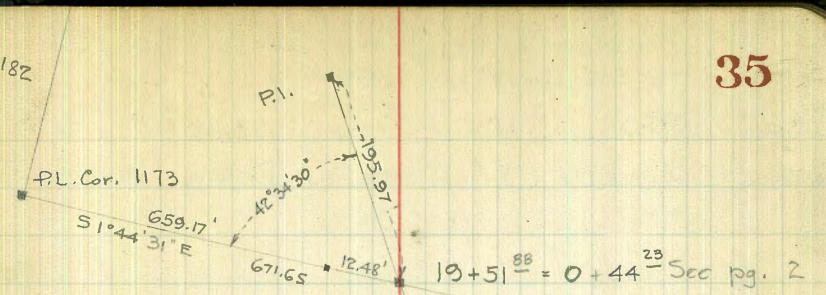
Sta	Align.	Defl. Δ	Curve Data	True Bearing	Dist. from P.I. to P.I.
4+17.54	E.C.				
4+00					
			Δ = 22° 59'		
			Δ = 22°59'30"		
			2A = 45°58"		
			R = 500'		
			T = 101.65'	101.50	P.I.
			L = 200.57'	✓	
3+00					
2+16.97	B.C.	Lt.			
2+00					
					318.62'
	216.97'				
1+00					
0+00					
	2.29'				
Δ					



STA	Align.	Defl. ∡	Curve Data	True Bearing	Dist. by P.I. to P.I.
9+44.56	E.C.				
			Δ = 9°18'30"		
9+00			Δ = 9°19'		
			½Δ = 18°37'		
			R = 1000'		
			T = 81.41' ✓		P.I.
			L = 162.46 ✓		
8+00					
7+82.10	B.C.	R+.			
7+00					
					547.62'
6+00					
	364.56'				
5+00					

Sta	Align.	Defl. Δ	Curve Data	True Bearing	Dist. fr. P.I. to P.I.
14+00					
13+00					
12+33 18	E.C.				
			Δ = 4°01'		
12+00			ΣΔ = 8°02'		P.I.
			R = 1750'		
			T = 61.37' ✓		
			L = 122.68' ✓		
11+10 50	B.C.	Rt.			
11+00					
					308.72'
	165.94'				
10+00					

STA	Align.	Defl. ∠	Curve Data	True Bearing	Dist. betw. P.I. to P.I.
19+51.88	= 0+44.23	Δ = 1°26' 2Δ = 2°52'	} Left.	P.I.	
19+00					
18+00					
17+00					
					780.07'
16+00					
15+00					



Random Line from SW. Cor. P.L. 1187 to SW. Cor. P.L. 1182

STA	Slope Dist.	V.A.	Hor. Dist.	Defl. &	Bearing
■ 25	Fd. 4"x4" Post		SW. Cor. P.L. 1182		
	210.0'	11°03'	206.11		S 0°37' E
△ 24				1°23' - L	
	495.20'	5°26'	493.98'		
△					
			111.75'		
△					
	382.0'	0°19'	381.99'		
△					
	494.75'	1°40'	494.54		
△					
	228.0'	2°35'	227.77		
△					
	247.05'	3°24'	246.62		
△					
	500.0'	3°11'	499.23'		S 0°46' W
■ 19	SW. Cor. P.L. 1187				

STA	BEARING	DIST.	N	S	E	W
△ 19			2324.99		308.46	
△ 24	S 0°46' W	2455.88		2455.66		32.86
△ 25	S 0°37' E	206.11		130.67	275.60	
△ 19	N 0°39'34" E	2662.21		206.10	2.22	
				336.77	277.82	

36

2455.66 = 3.3901683
Cos 0°46' = 9.9999611
log 2455.88 = 3.3902072
tan 0°46' = 8.1264710
32.86 = 1.5166782

206.10 = 2.3140739
Cos 0°37' = 9.9999748
log 206.11' = 2.3140991
tan 0°37 = 8.0319195
2.22 = 0.3460186

N		E
2324.99	(19)	308.46
- 336.77	(25)	277.82
2661.76		30.64

2662.21 = 3.4252428
- tan 0°39'34" = 8.0610460
log 30.64 = 1.4862888
- = 2661.76 = 3.4251689
S 0°39'34" W 8.0611199

Random Line from S.E. Cor P.L. 1187
To SE. Cor P.L. 1182

STA	Slope Dist.	V.A.	Hor. Dist.	Defl. ∠	Bearing
PL 1182					
■ 27	Fd. 3"x3" Hub with		Tack	SE. Cor. P.L. 1182	
	365.33'	18°41'	346.08'		S 10°42' E
△ 26				10°42' -	L
	272.0'	12°12'	265.86		
△					
	124.00'	5°38'	123.40'		
△					
	457.40'	1°00'	457.33		
△					
	452.94	1°35'	452.77		
△					
	492.85	3°14'	492.07		
△					
	500.0'	5°17'	497.88'		South
■ 21	SE. Cor. P.L. 1187				

STA	BEARING	DIST	N	S	E	W
△ 21	South	2289.31'	2324.37	2289.31	2908.73	
△ 26	S 10°42' E	346.08'	35.06	340.07	2908.73	
△ 27	N 1°24'00" W	2629.95'		305.01	64.26	
△ 21	N 89°19'29" E	2694.83'			2972.99	
△ 25						
△ 27						

340.07 = 2.5315589
cos 10°42' = 9.9923824
log 346.08 = 2.5391765
tan 10°42' = 9.2687338
64.26 = 1.8079103

N	E
2324.37 (21)	2908.73
-305.01 (27)	2972.99
2629.38	64.26

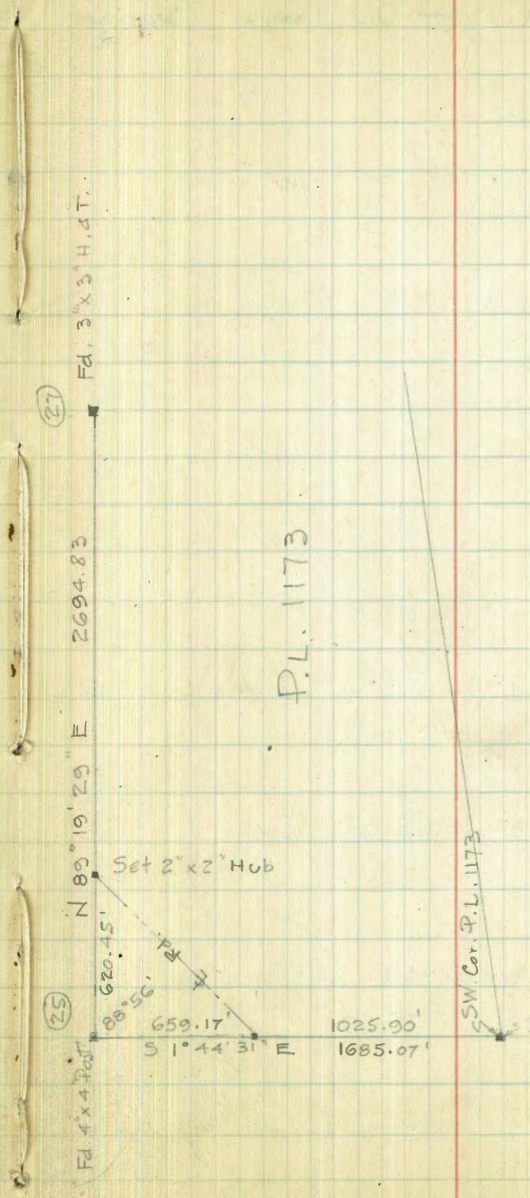
2629.95 = 3.4199481
- sin 1°24'00" = 8.3879622
log 64.26 = 1.8079103
- " 2629.38 = 3.4198534
S 1°24'00"E 8.3880569

N	E
-305.01 (27)	2972.99
-336.77 (25)	277.82
31.76	2695.17

2694.83 = 3.4305307
- cos 89°19'29" = 8.0713498
log 31.76 = 1.5018805
- " 2695.17 = 3.4305862
N 89°19'29"E 8.0712943

From NW. Cor P.L. 1173 S 1°44'31" E To
set ℄ of Rd. & SW. Cor P.L. 1183

STA	Slope Dist.	V.A.	Hor Dist.	Defl.&	Bearing
△	Set 2"x2" Hub for ℄ Road (Right of Way)		4.66'		
△	368.0'	9°42'	362.74'		
△-1	296.0'	9°42'	291.77'		S1°44'31" E
■ (25)	NW. Cor. P.L. 1173				



From NW. Cor P.L. 1173 N 89°19'29"E
to set ℄ of Rd.

STA	Slope Dist	V.A.	Hor. Dist.	Defl. ∡	Bearing
Δ - 4	Set 2"x 2" on ℄ Road (Right of Way)				
			- 0.20'		
Δ - 3					
	450.0'	8°29'	445.08		
Δ - 1					
Δ - 2	West'ly Stradler on Ex. Rd.				
	286.0'	15°29'	275.62'		
Δ - 1					
	176.80	6°45'	175.57'		
■ (25)	NW. Cor. P.L. 1173				

New Location of Murray Canyon Rd. from Sta. 0+44 23 (see pg. 2) to P.I. 21+89 19
see pg. 6

Jaeger, Bailey, Clarey, Morgan } Sept. 27-1929

Sta	Align.	Defl. ∠	Curve Data	True Bearing	Dist. from P.I. to P.I.
22+02 89	E.C.	9°40.7'			
22+00		9°37.4'			
+50		8°40.1'			
21+00		7°42.9'			
+50		6°45.6'			
20+00		5°48.3'	Δ = 19°22' ; 2Δ = 38°43' } = 19°21'30" ✓		
+50		4°51.0'	T = 255.84 ✓ ; R = 1500. ; L = 506.80 ✓	P.I.	
19+00		3°53.7'			
+50		2°56.4'		N42°20'50"E	
				(N42°18'E)	
18+00		1°59.1'			
+50		1°01.8'			
17+00		0°-4.5'			
16+96 04	B.C.	Lt.			

P.I. 19+51 88 see pg 35
= 0+44 23 " " 2

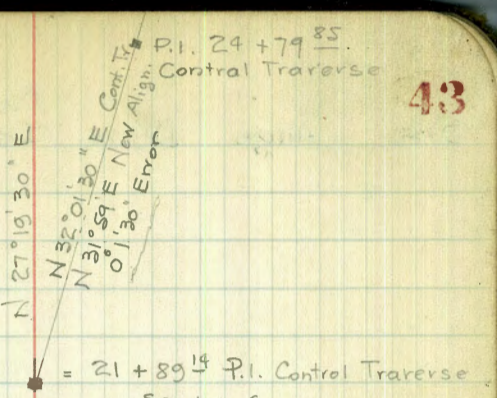
N 42°18' E

16+96 04 B.C.

Sta	Align.	Defl. ∢	Curve Data	True Bearing	Dist. from P.I. to P.I.
28 + 00					
+ 50					
+ 46.05	E.C.	7°04'			
27 + 00		6°11.29'			
+ 50		5°13.99'			
26 + 00		4°16.70'	P.C.		
			Δ = 14°08' ✓		
+ 50		3°19.40'	2Δ = 28°16'		P.I.
			R = 1500'		
			T = 185.96' ✓		
25 + 00		2°22.11'	L = 370.01' ✓		
+ 50		1°24.81'			
24 + 00		0°27.52'			
+ 76.04	B.C.	Rt.			
+ 50					
				N 22°59'20" E	
23 + 00				(N 22°56'30" E.)	615.00'
	173.20'				
+ 50					

Sta	Align.	Defl. ¢	Curve Data	True Bearing	Dist. from P.I. to P.I.
34 + 00		6°18.59'	Δ = 21°33'		P.I.
			2Δ = 43°06'		
+ 50		5°21.29'	R = 1500'		
			T = 285.47' ✓		
33 + 00		4°24.00'	L = 564.18 ✓		
+ 50		3°26.70'			
32 + 00		2°29.41'			
+ 50		1°32.11'			
31 + 00		0°34.82'			
30 + 69.62	B.C.	Rt.			
+ 50					
30 + 00					
+ 50					
	323.57'			N37°07'20"E	
29 + 00				(N37°04'30"E)	795.00'
+ 50					

Sta	Align.	Defl. ¢	Curve Data	True Bearing	Dist. from P.I. to P.I.
40 + 00		14°54.11'			
+ 50		12°02.22'	Δ = 31°18'		
			2Δ = 62°36'		P.I.
			R = 500'		
39 + 00		9°10.33'	T = 140.08 ✓		
			L = 273.14 ✓		
+ 50		6°18.44'			
38 + 00		3°26.55'			
+ 50		0°34.66'			
37 + 39.92	P.C.	Lt.			
37 + 00					
	106.12' ✓			N58°40'20"E	
+ 50				(N58°37'30"E)	531.67
36 + 33.80	E.C.	10°46.50'			
36 + 00		10°07.77'			
+ 50		9°10.47'			
35 + 00		8°13.18'			
+ 50		7°15.88'			



STA	Align.	Deft. ¢	Curve Data	True Bearing	Dist. P.I.-P.I.
46 + 00					
+ 50					
45 + 00					
+ 50					
44 + 00	705.21				
				N 27° 22' 20" E	
+ 50				(N 27° 19' 30" E)	871.24'
43 + 00					
+ 50					
42 + 00					
+ 50					
41 + 00					
+ 50					
40 + 13.06	E.C.	15° 39'			

Sta	Align.	Deft. &	Curve Data	True Bearing	Dist. P.I. - P.I.
52 + 00					
+ 50					
51 + 00					
+ 50					
50 + 00					
49 + 93.60					P.I.
+ 50					
49 + 00				N33°18'50"E	
				(N33°16'00"E)	249.43
+ 50					
			Δ=5°56'30"		
48 + 00			Δ = 5°57'		
47 + 70.12	E.C.		2Δ = 11°53'		
			R = 500'		
+ 50			T = 25.95' ✓		P.I.
47 + 18.27	B.C.	Rt.	L = 51.85' ✓		
47 + 00					
+ 50					

P.I. 30 + 63.03 Control Traverse, See Pg. 8

N 33°18'50"E Computed
N 33°16'00"E

249.37' Chained
249.43' Computed

20'

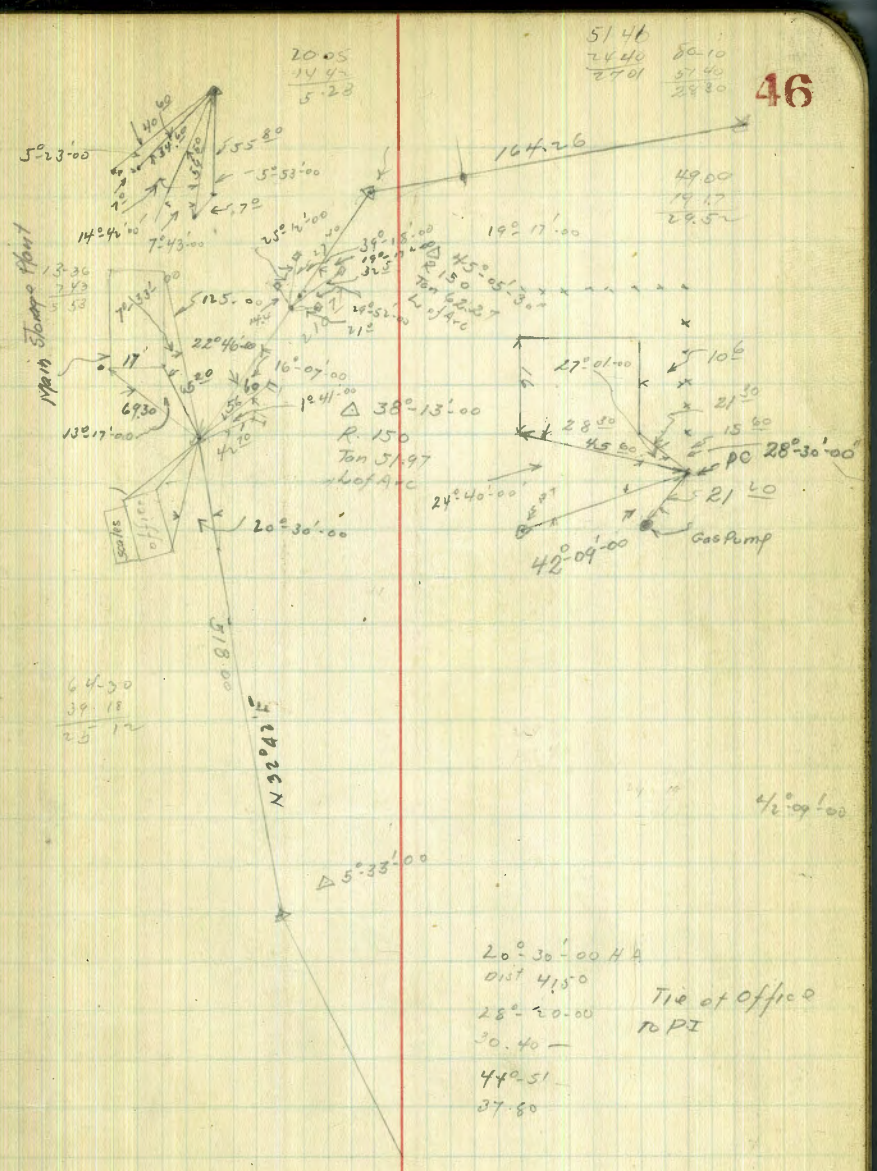
New P.I.

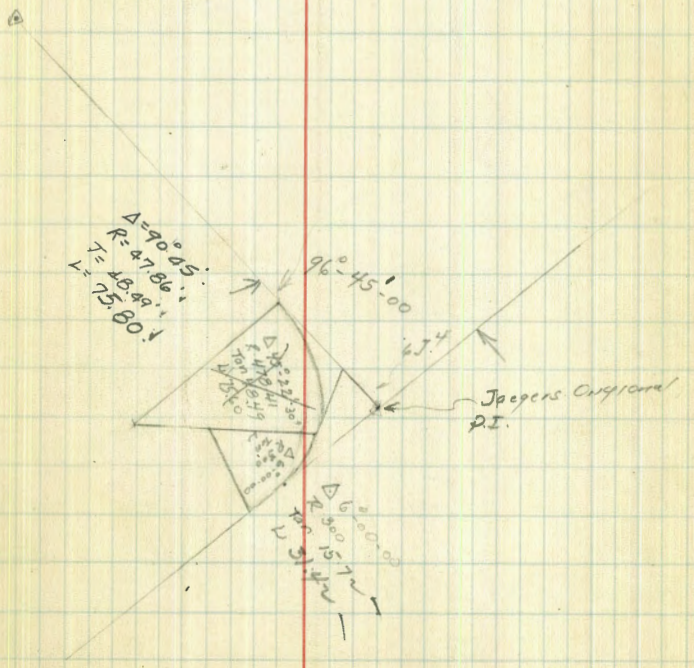
49 + 93.60 = 33 + 13.67 P.I. Control

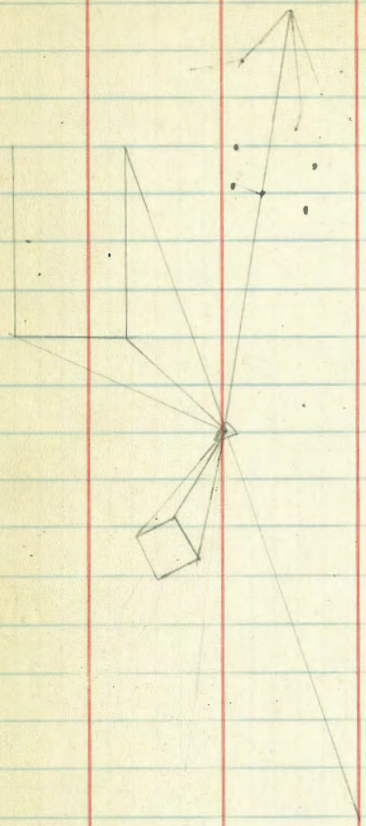
B. Bliss
J. Duermit
J. Roobaszoon
Nov. 29, 1929

Realignment Murray Canyon Road from PI Sta

Sta	Align	Def Δs	Curve Data	True Bearing	Dist PI to PI
	L		Δ 45°-22-30 R 478.41 Tan 198.49 L		
			See page #47		
	L		Δ 6°-00'-00 R 300 Tan 15.72 ✓ L 31.42 ✓		
	R		Δ 45°-05' 30" R 150 Tan 62.27 ✓ 62.27 ✓ L = 118.05 ✓		
					210.77
	R		38°-13-00 R 150 Tan 51.97 ✓ L 100.05 ✓		
					518
	R		Δ 5°-33'-00 R = 2000 ✓ Tan = 96.94 ✓ L = 193.73		

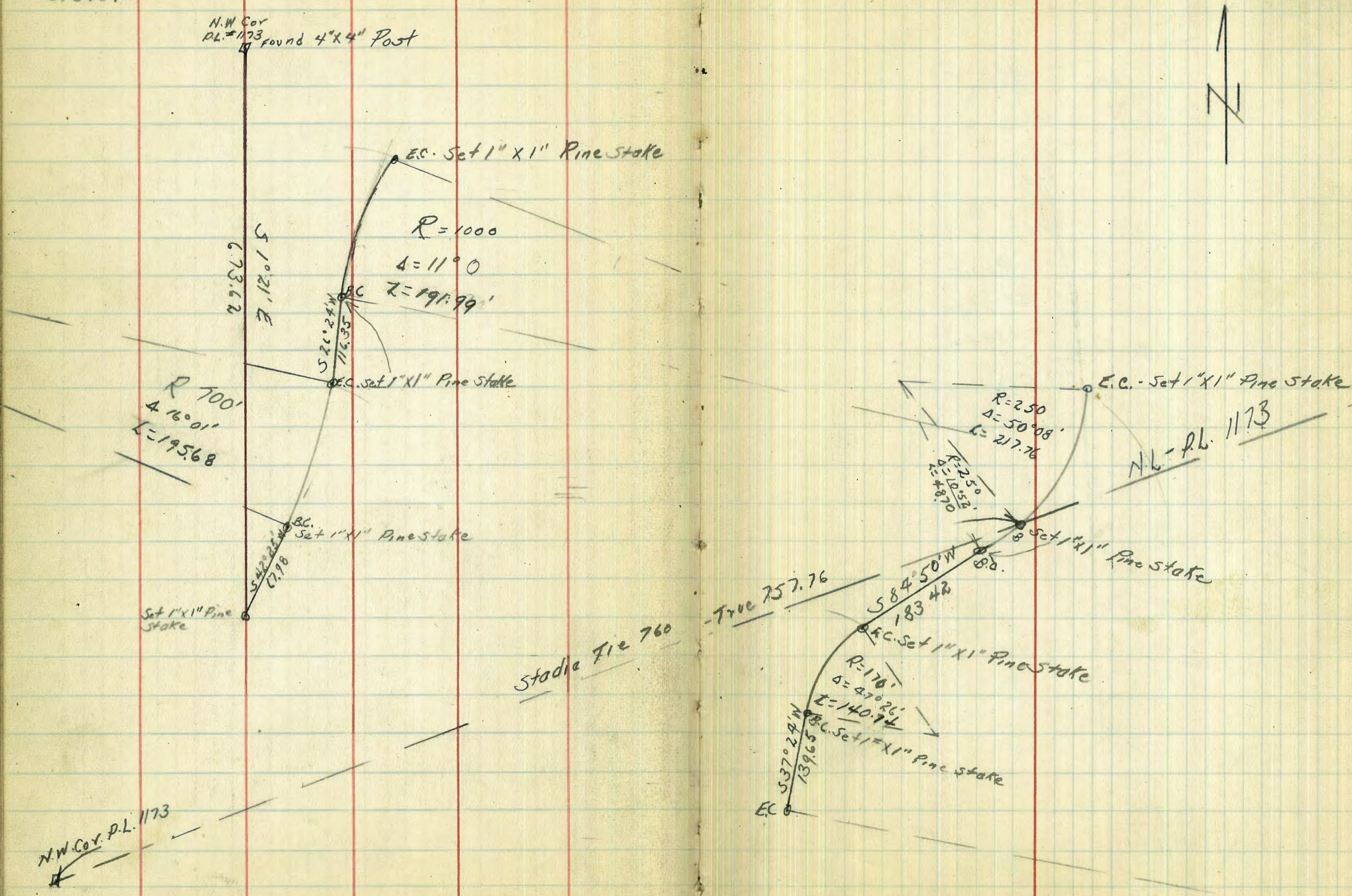


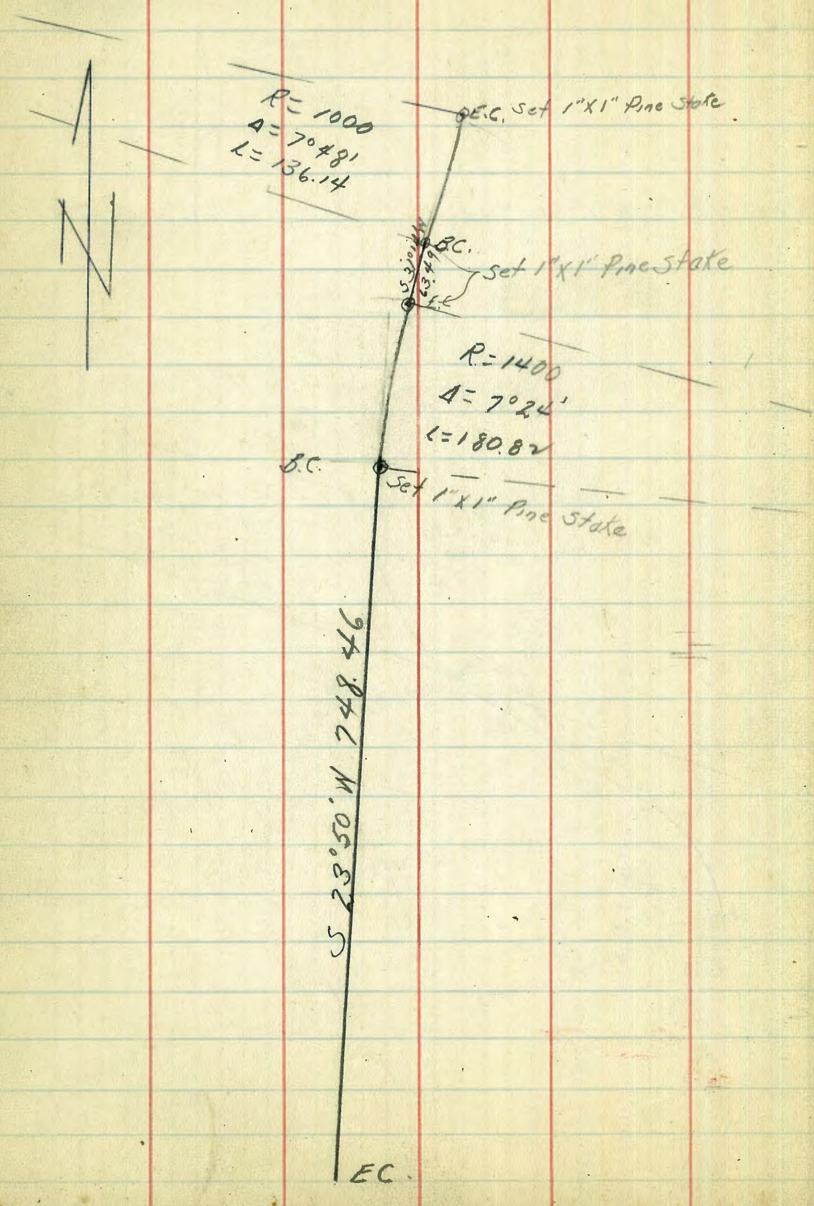

Δ=90°45'
R=47.86'
T=48.49'
L=75.80'
96°-45-00
43.4
Jaegers Original P.I.

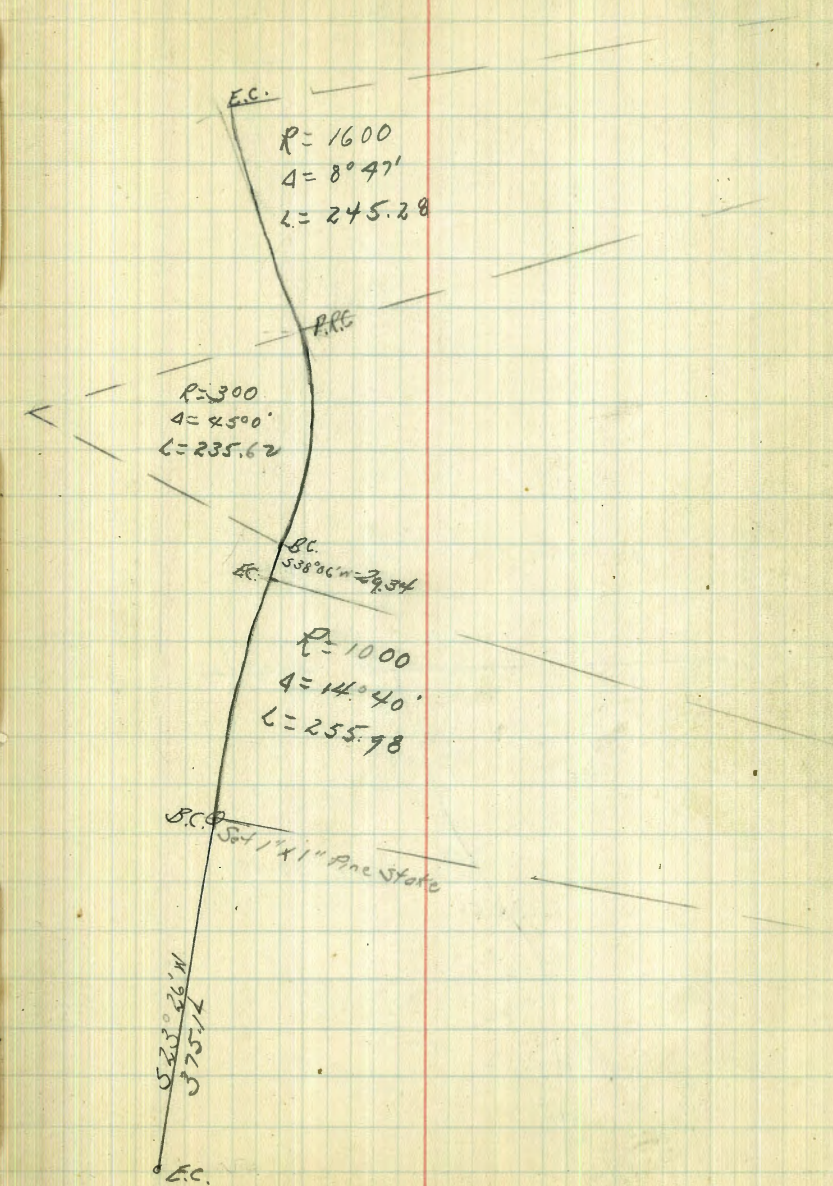


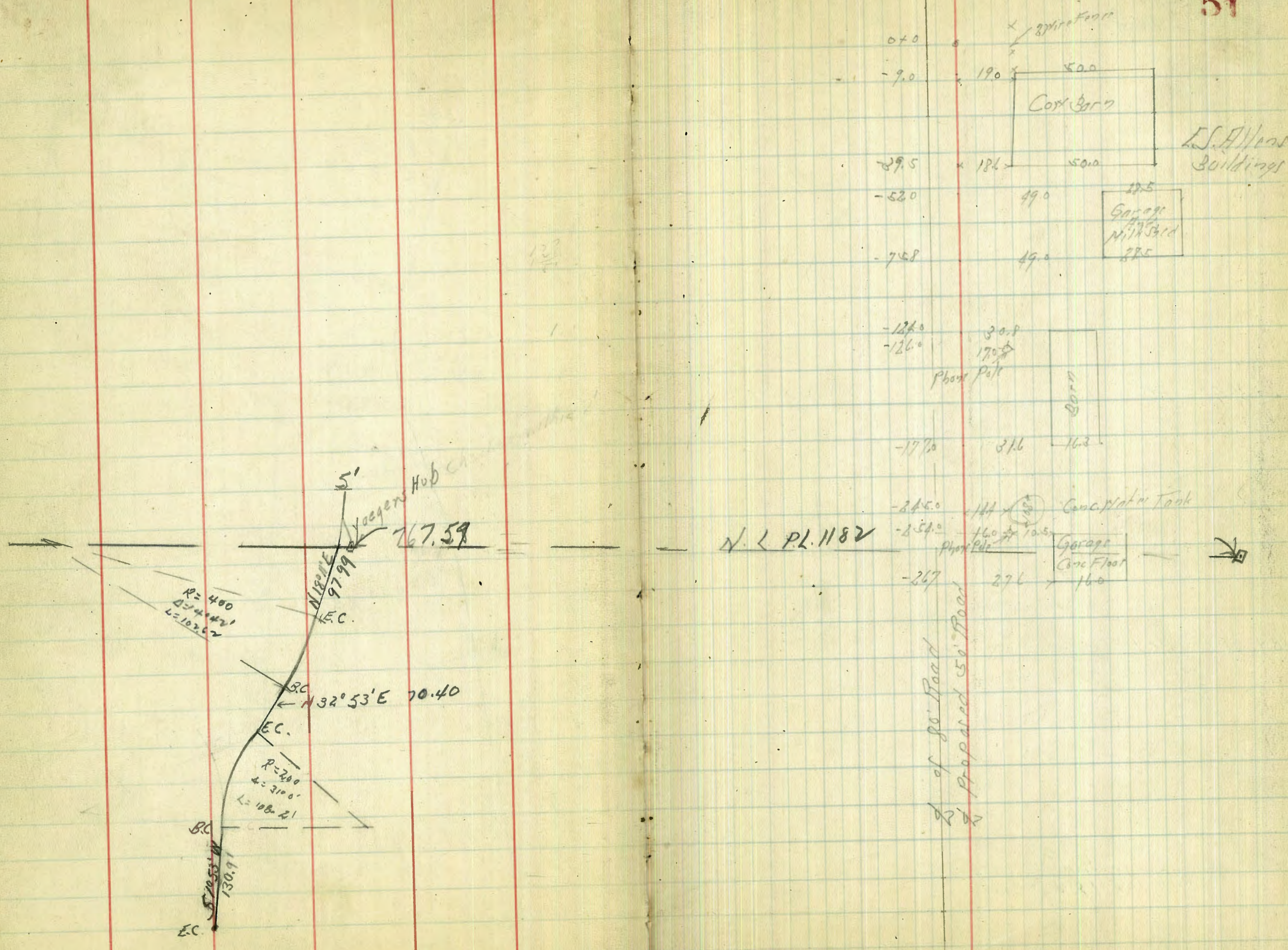
1-21-30
J.C. Bliss
Drebert
Ravner
Clavert

Survey of Murray Canyon
Right of way according to 525-L




N
R= 1000
Δ= 7°48'
L= 136.14
E.C. Set 1"x1" Pine Stake
B.C.
Set 1"x1" Pine Stake
E.C.
R=1400
Δ= 7°24'
L=180.82
B.C.
Set 1"x1" Pine Stake
S 23°50' W 748.46
EC.


E.C.
R= 1600
Δ= 8°47'
L= 245.28
P.R.C.
R=300
Δ=45°00'
L=235.62
B.C.
E.C.
R= 1000
Δ= 14°40'
L= 255.98
B.C.
Set 1"x1" Pine Stake
S 23°26' W
E.C.


5'
Yaegers Hub
767.59
N18°E
97.99
R= 400
E.C.
B.C
N 32°53'E 70.40
E.C.
R=200
Δ=31°00'
L=108.21
B.C
130.91
E.C.
N. ∠ P.L. 1182
0+0
2 wire Fence
-9.0
19.0
50.0
Cow Barn
29.5
18.6
50.0
L.S. Allens
Buildings
-52.0
49.0
27.5
Garage
Milk Shed
27.5
-74.8
49.0
-126.0
30.8
17.0
Phone Pole
Barn
-177.0
31.6
16.3
-245.0
Conc. Water Tank
-254.0
16.0
10.5
Phone Pole
Garage
Conc Floor
-267
27.6
16.0
℄ of 80' Road
Proposed 50' Road

Murray Canon Road

Through H.G. Fenton's Material Plant

P.L. 1173 And P.L. 1182

2+39.90 E.C.

Δ = 12° 04'

R = 700.0'

L = 147.42

T = 73.98

0+92.48 P.C.L.

0+0 = Intersection P.L. 1174 - 1173 Into 10' E of ℄ of 80' Road

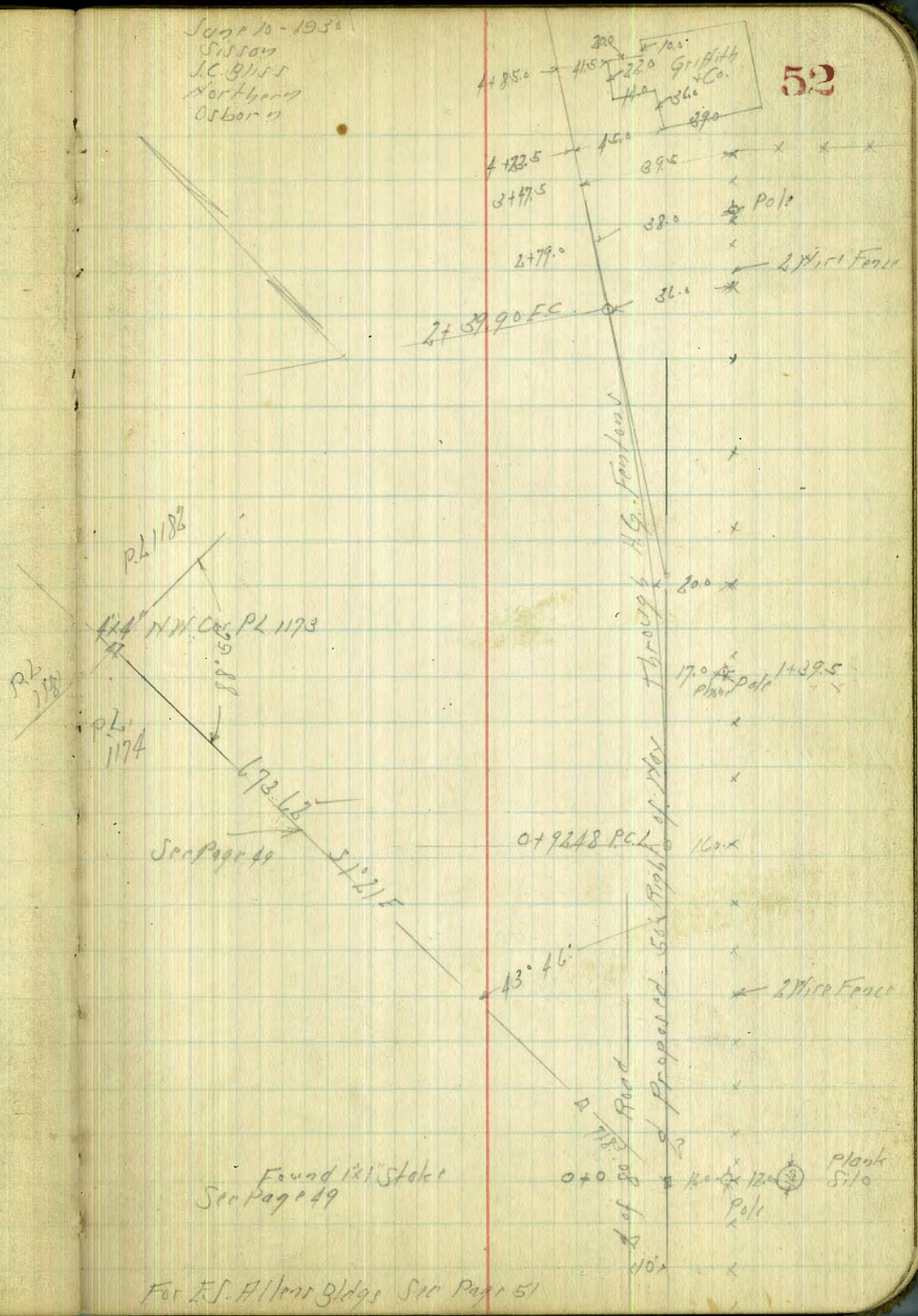
June 10 - 1950

Sisson

J.C. Bliss

Northern

Osborn

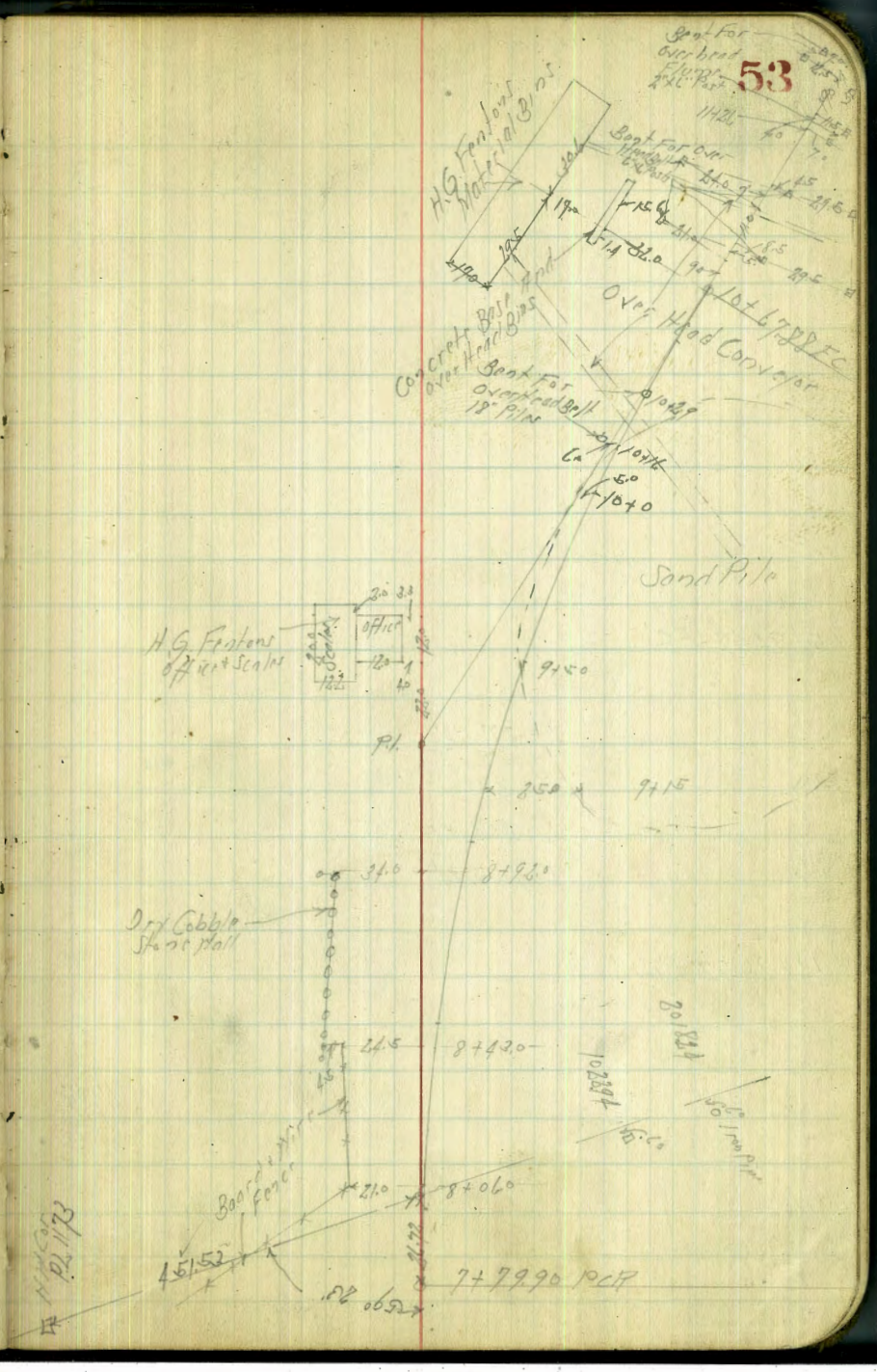


Murray Canon Road
Through H.G. Fentons Material Plant
P.L. 1173 And 1182

10+67.88 E.C.

Δ 33° 00'
R = 500.0
L = 287.98
T = 148.10

7+79.90 P.C.R.



Murray Canon Road

15+94.47 E.C.

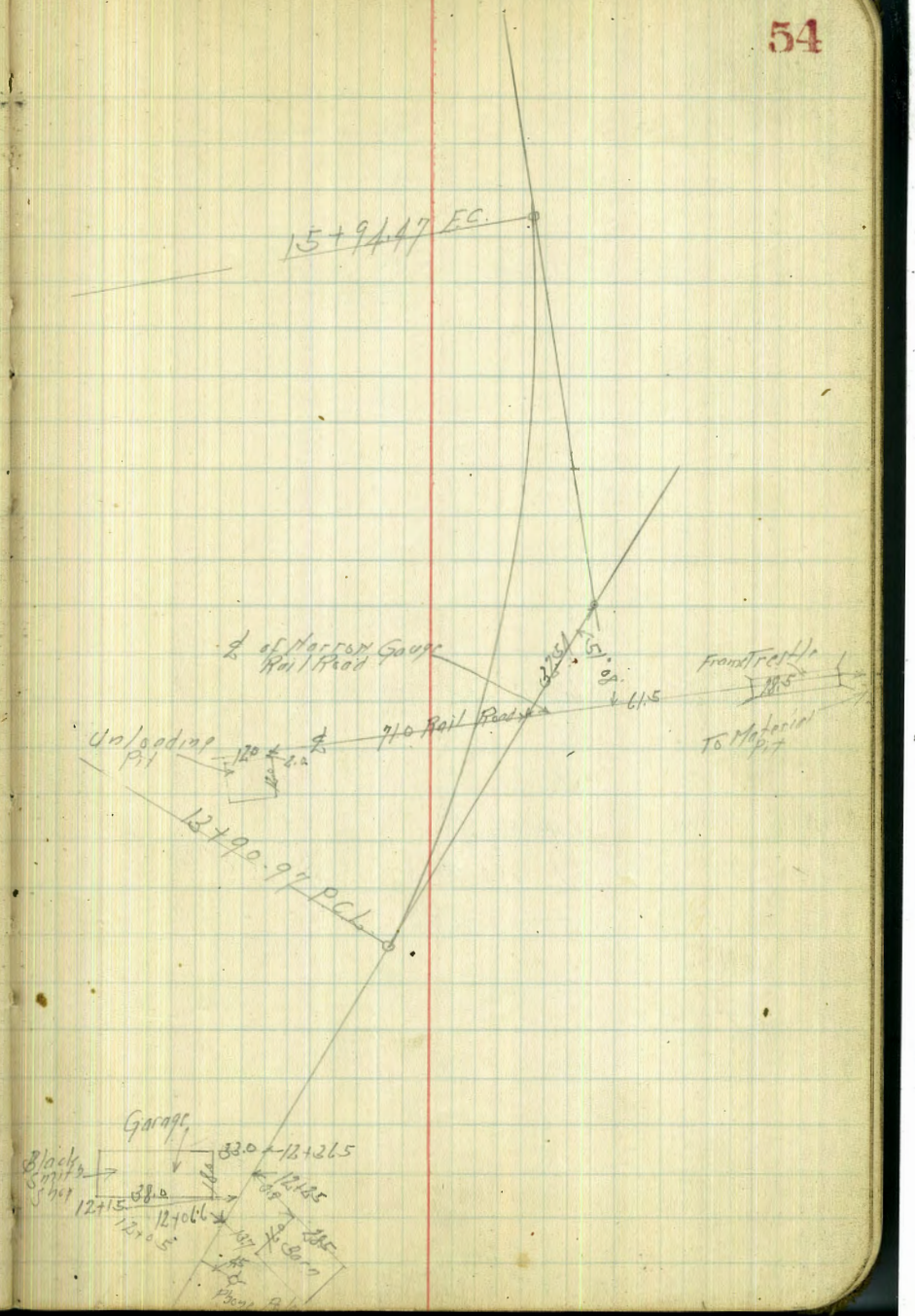
Δ = 38° 52'

R = 300'

L = 203.50

T = 105.84

13+90.97 P.C.L.



Murray Canon Road.

29+99.81 EC = Old EC.

Δ = 13°22'
R = 806.4C
L = 188.14
T = 94.50

28+11.67 P.C.R.C.

R = 200'
Δ = 45°00'
T = 82.84
L = 157.08

See Page 50 →

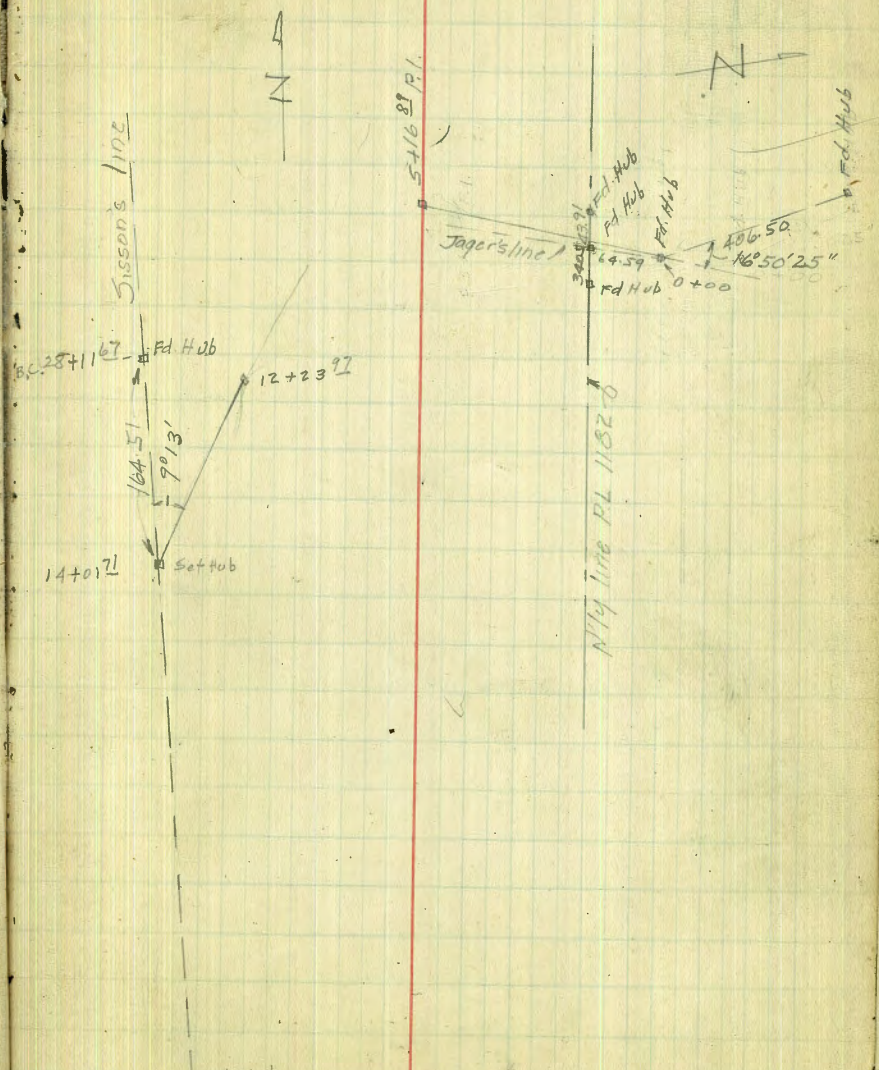
29+99.81 EC = Old EC
See Page 50

28+11.67 P.C.R.

7/7/30
London.

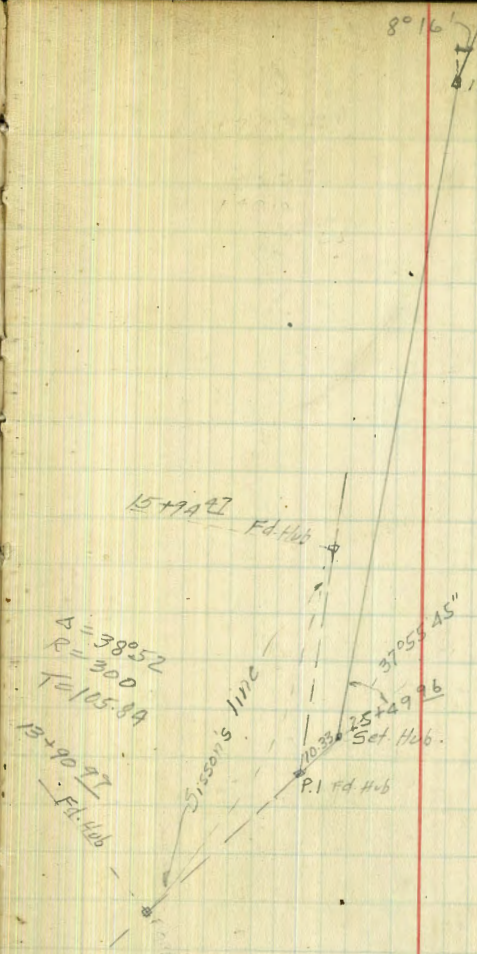
Change alignment Murray Canyon
From N.L. P.L. 1182 Southerly.

0+00	B.S. on P.I. North	Δ = 16°50'25" R.	
1+00			
2+00			
3+00			
3+76 78	B.C.		Set Hub
5+16 89	P.I	Δ = 26° 17'20" L	Set Hub
		R = 600	
		T = 140.11	
6+57	E.C.		Set Hub
7+00			
8+00			
8+20 15	B.C.		Set Hub
9+29 54	P.I.	Δ = 40°04' R	Set Hub
		R = 300	
		T = 109.39	
10+38 93	E.C.		Set Hub
11+00			
11+87 84	B.C.		Set Hub
12+23 97	P.I		Set Hub
13+21 88		Δ = 9°13' L.	
14+01 71	Intersection with Sissop's Line		Set Hub



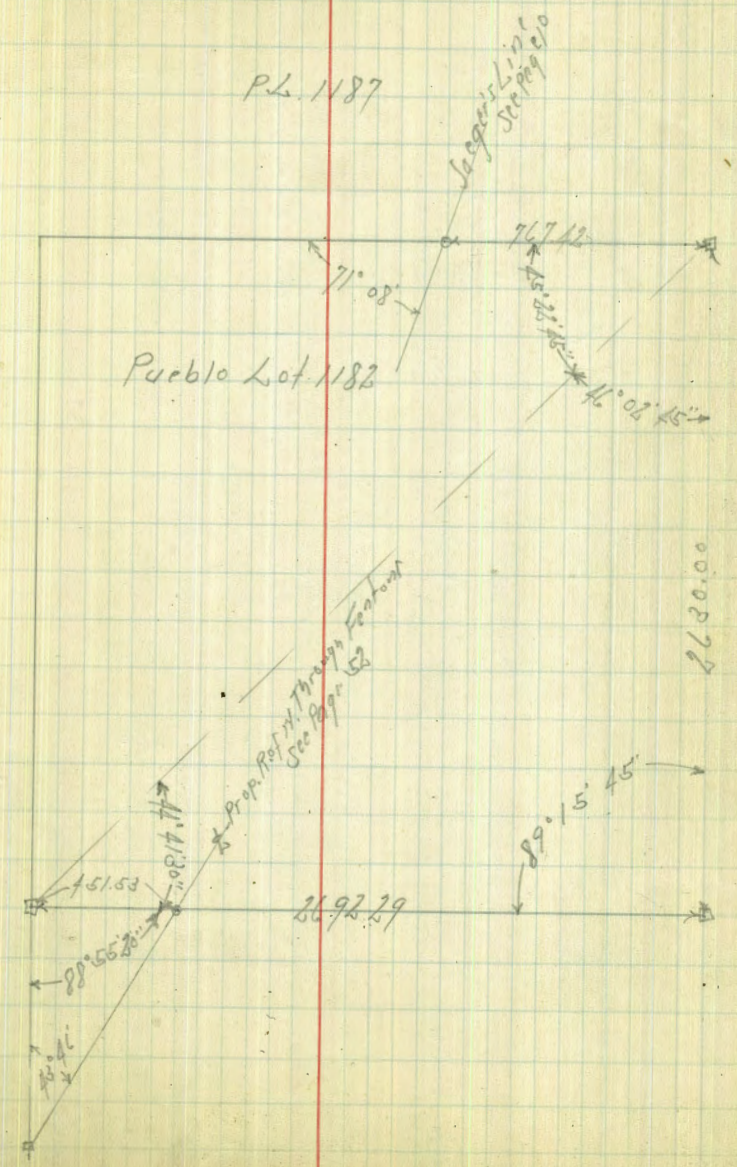
Change Alignment From 12+23.97 P.1
(P 56)

12+23.97	P.1	Δ = 8°16'L
13+22.75		
14+00		
15+00		
16+00		
17+00		
18+00		
19+00		
+80.12	P.O.T. Nail	
20+32.00	P.O.T. Nail	
21+28.78		
22+00		
23+00		
24+00		
25+00		
25+49.96	Intersection with Sisson's N 62°59'30" E.	



Pueblo Lot 1182
Proposed Right of Way Through
H.G. Fentons Murray Canyon

Sept 29-30
1905
McHugh
Northern

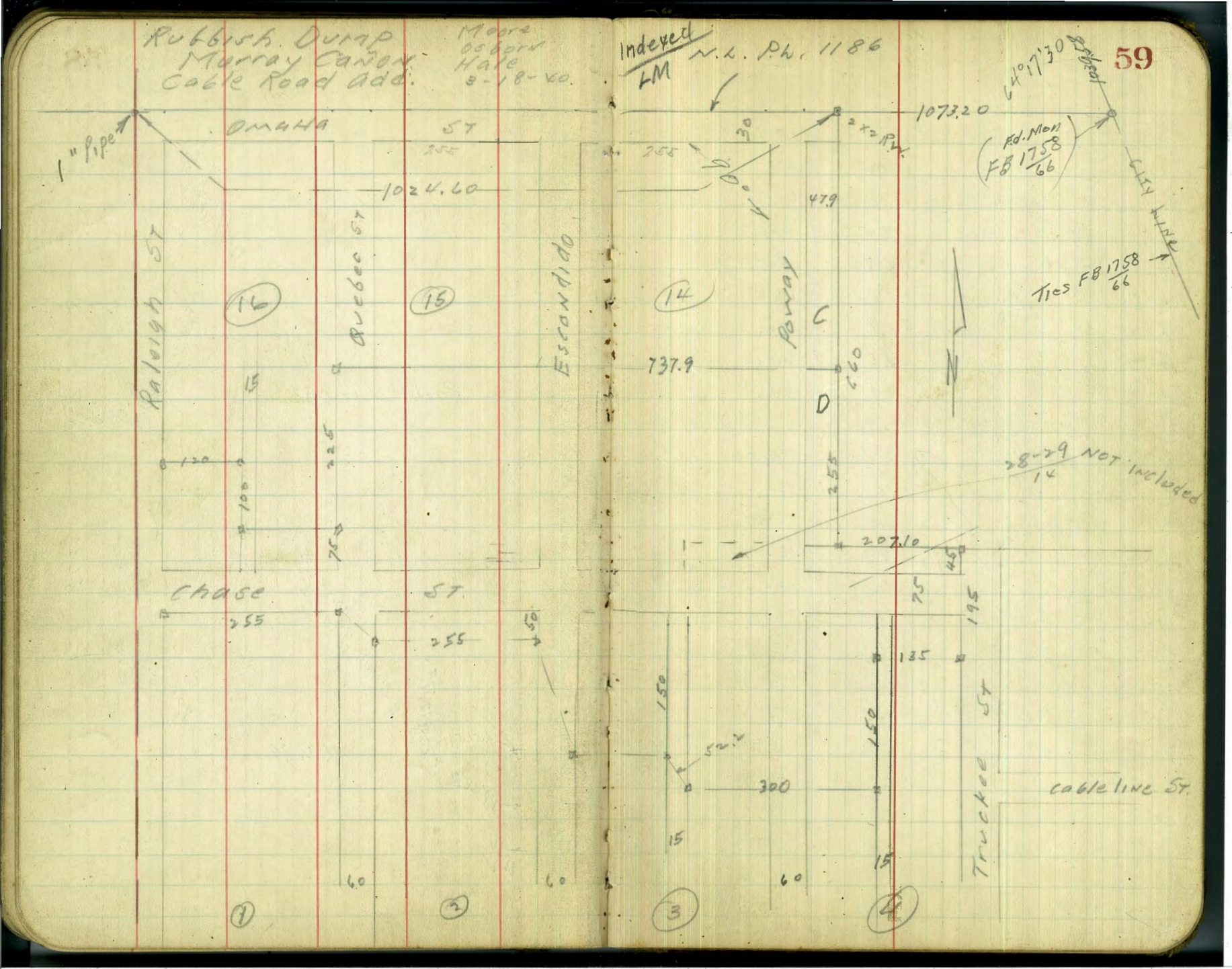


Rubbish Dump
Murray Canon
Cable Road add.

Moore
Osborn
Hale
3-18-60.

Indexed
LM

N.L. Ph. 11186



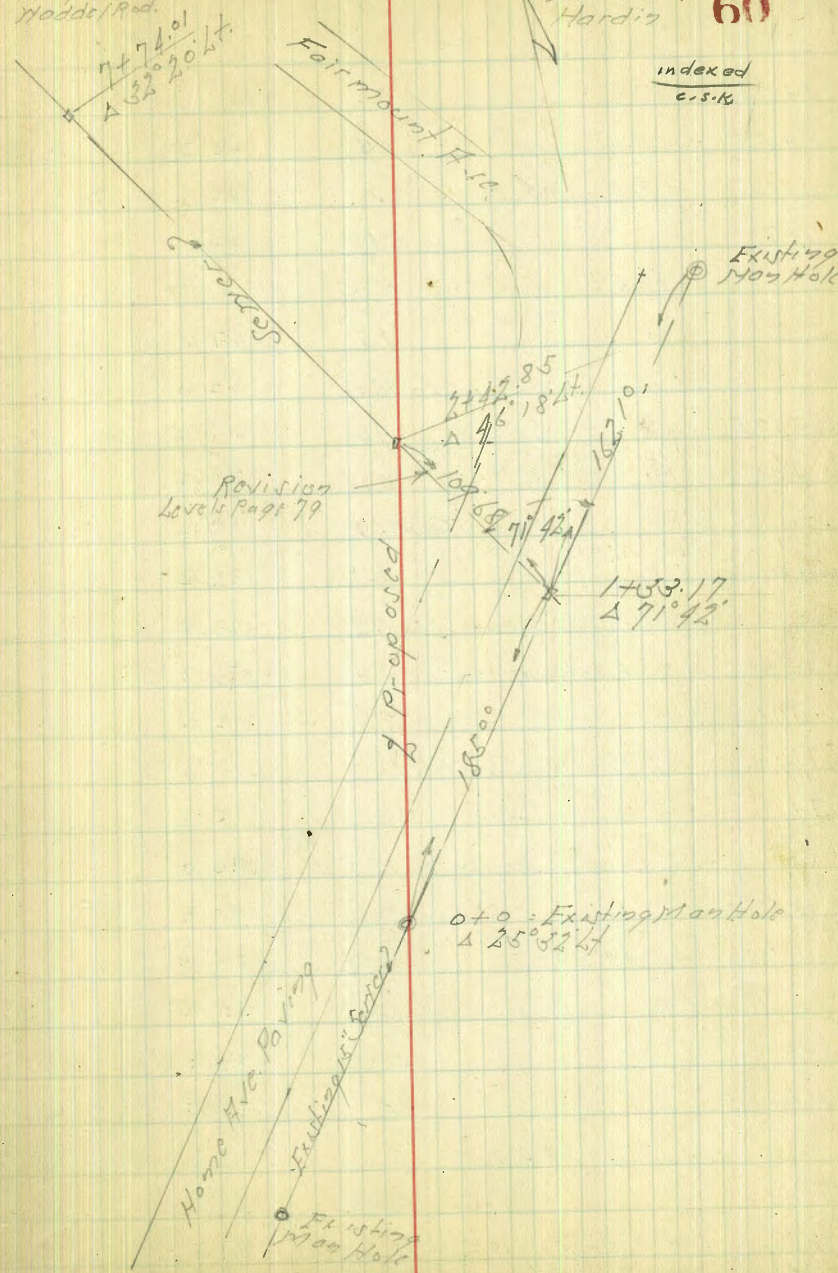
Proposed Sewer West of Fairmount - Home Ave to Laurel St.

BM		5.09	153.14		148.05	B.P. E'ly Cor. Box Culv. Fairmount & Home Av
0+0	= Exist MH			10.41	142.73	on Rim
"	" " "			20.49	132.65	Flow Line
+41	= S.E'ly Paving			8.57	144.57	
+71	= on "			6.85	146.29	
1+02	= N.W'ly Paving			6.24	146.90	
+20				6.2	146.9	
+50				4.5	148.6	
2+0				1.3	151.8	
TP		11.98	164.79	0.33	152.81	
+42.85	= Δ 46°18' Lt			11.79	153.00	on Stake
+77				10.4	154.4	
+80	= Bottom Wash			13.8	151.0	
+85				9.8	155.0	
3+0				8.5	156.3	
+06	= Bottom Wash			10.4	154.4	
+10				8.1	156.7	
+50				6.9	157.9	
"	5 Lt of ℄ = Bot. Wash			7.4	157.4	
+56				5.0	159.8	
+85				3.7	161.1	
+88				4.9	159.9	
4+0	= W'ly & Wash Bot.			5.5	159.3	
+12				3.8	161.0	
+22	= Bottom Wash			4.8	160.0	

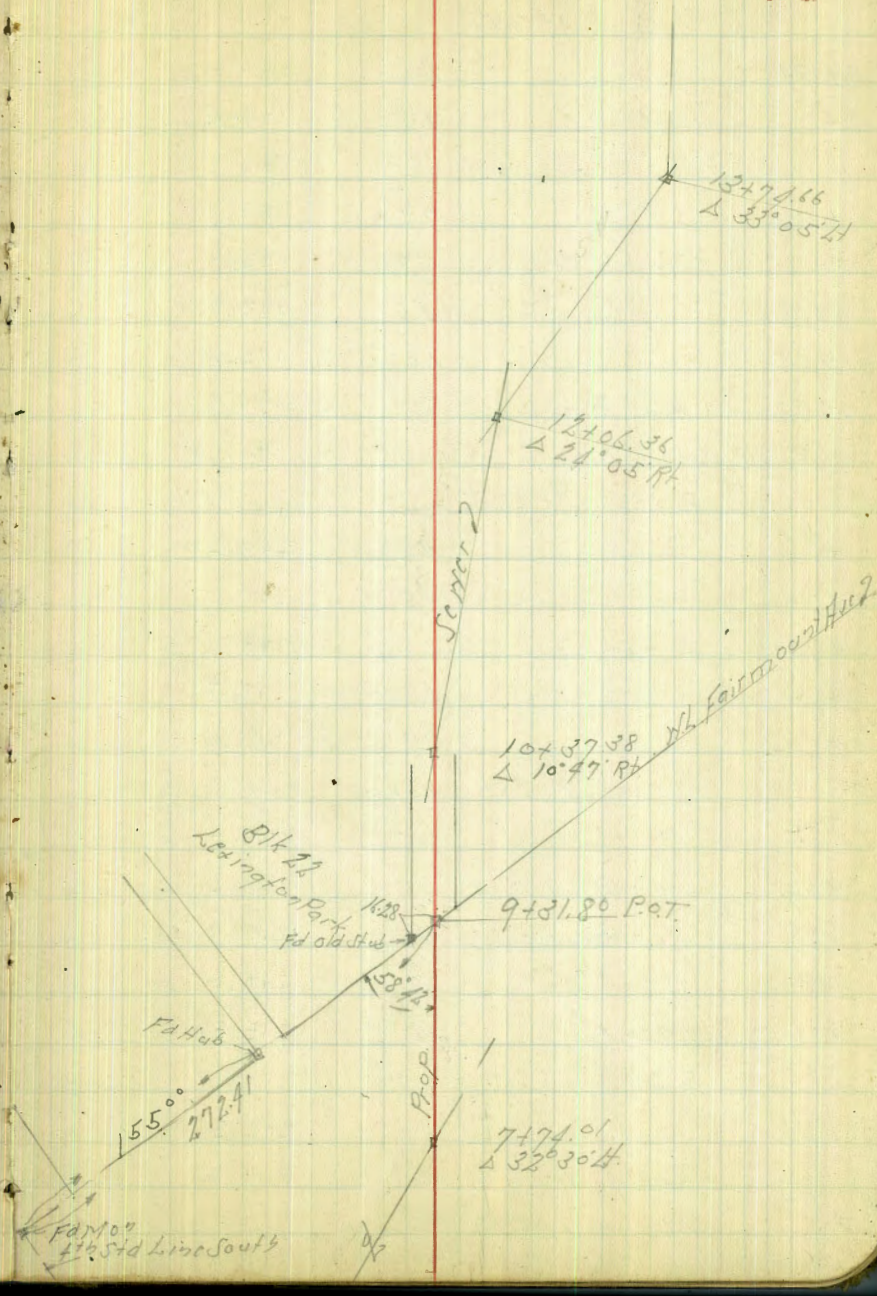
Levels April 4-46
Sisson
Wright T.
Waddel Rod.

March 14-46
Sisson
Waddel
Hardin

indexed
C.S.K.



		164.79			
4+34			2.6	162.2	
+55			1.5	163.3	
+61	= Bottom Wash =		3.0	161.8	
+70			0.8	164.0	
TP	12.55	177.09	0.35	164.54	
5+0			9.5	167.6	
"	16' Rt of ℄ = Bot. Wash		13.5	163.6	
+47.5	44 Rt of ℄ = S.W. Cor Conc. Piers Under Const.	Water Wash	9.6	167.5	on Conc
+50			6.7	170.4	
+58.6	48 Lt of ℄ = N.E. Cor Conc Pier Not Finished		6.9	170.2	on Conc
6+0			4.9	172.2	
"	7' Rt of ℄ = Bottom Wash		7.2	169.9	
+50	= ℄ + Bottom Wash		3.4	173.7	
+70	= " " "		2.7	174.4	
TP	12.82	188.30	1.61	175.48	
7+0			10.1	178.2	
"	13' Lt of ℄ = Bot. Wash		12.3	176.0	
+50			8.0	180.3	
+74.01	= Δ 32° 30' Lt		4.51	183.79	on Stub
"	12 Lt of ℄ = Bot Wash		8.1	180.2	
8+0			4.8	183.5	
+50			2.3	186.0	
"	4' Lt of ℄ = Bot Wash		4.8	183.5	
TP	10.16	197.58	0.88	187.42	
+89	= Bot Wash to N.E.		10.5	187.1	



		197.58			
8+94			8.6	189.0	
9+0			9.0	188.6	
" "	5' Lt of ℄ Bot. Wash		10.9	186.7	
+50			7.7	189.9	
10+0	= ℄ + Bot. of Wash		5.2	192.4	
+12			4.6	193.0	
+25			1.0	196.6	
+33	= Bot. Wash		2.7	194.9	
+37.38	Δ 10°47' Rt.		1.42	196.16	on Stub
TP	8.36	204.52	1.42	196.16	
+62			4.0	200.5	
+70			4.5	200.0	
+73	= Bottom Wash		6.4	198.1	
11+0			4.8	199.8	
+20			2.9	201.6	
TP	12.70	215.61	1.61	202.91	
+25			10.2	205.4	
+60	= Fl. + Bot. of Wash		7.0	208.6	
+86	= Bottom Wash		5.4	210.2	
12+0			1.8	213.4	
+06.36	Δ 24° 05' Rt		0.08	215.53	on Stub
TP	7.38	222.91	0.08	215.53	
+50			4.4	218.5	
+61	= Bottom Wash		5.7	217.2	
TP	12.96	235.14	0.73	222.18	

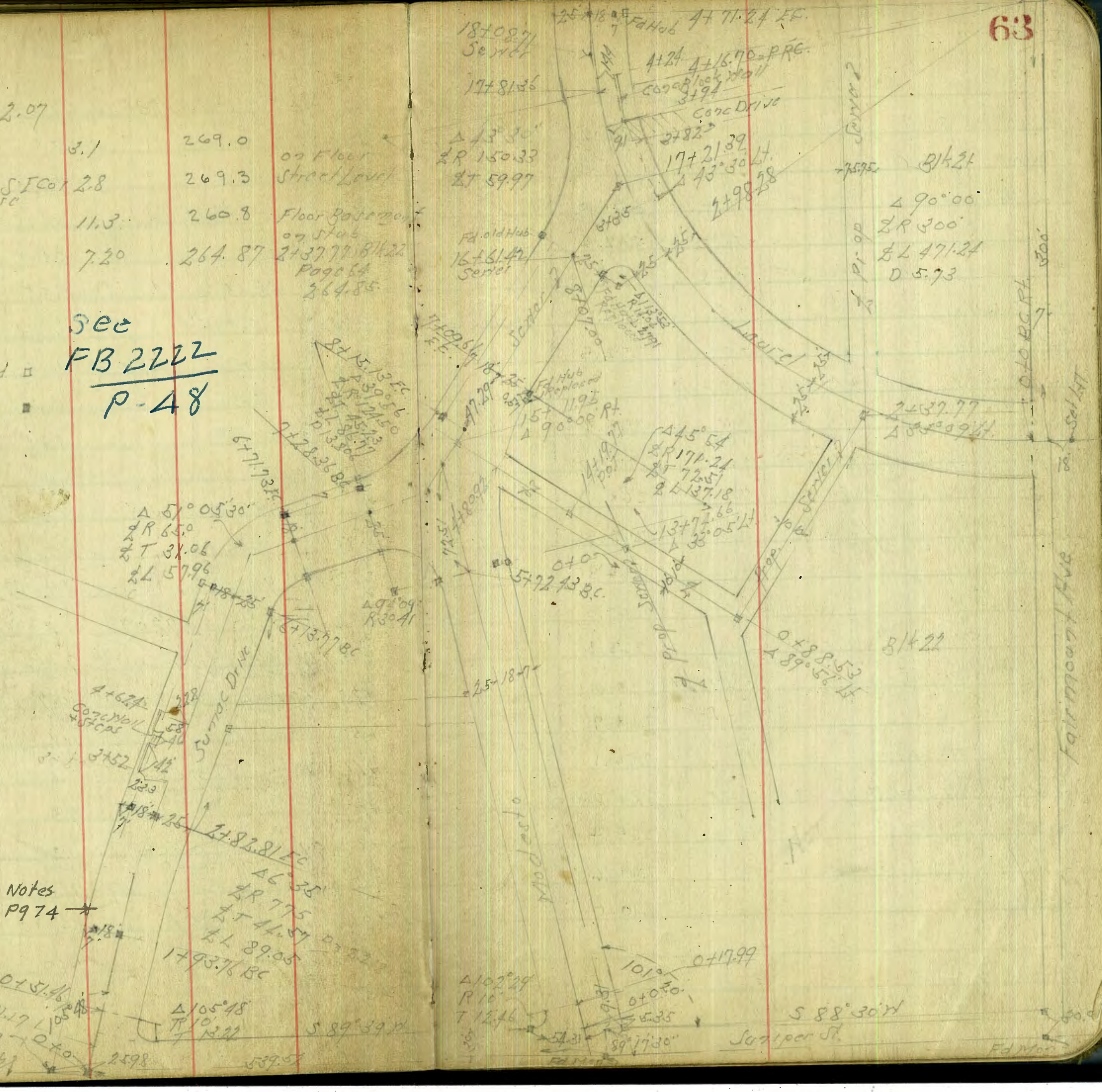
		235.14			
13+0			9.5	225.6	
+15			7.5	227.6	
+40			7.9	227.2	
+50			5.5	229.6	
TP	12.15	246.74	0.55	234.59	on lat b rt 13+65
+74.66 Δ 33°05' Lt.			11.23	235.51	on Stub
TP	12.40	258.04	1.10	245.64	
14+0			10.4	247.6	
+19.77 P.O.T.			3.94	254.10	on Stub
+50			2.4	255.6	
TP	7.97	265.81	0.20	257.84	
+91			5.7	260.1	
15+11.95 Δ 90°00' Rt.			4.96	260.85	on Stub
BM	10.14	272.07	3.88	261.93	S.E. Cor Meter Box opp. E. Conn
+11.95 46' W of ℄ = N.E. Cor Stucco House			9.6	262.5	on Floor
+25 60' W of ℄ = S.E. Cor Frame House			10.7	261.4	on Floor
+50			11.1	261.0	
+66 80' W of ℄ = S.E. Cor Frame House			11.6	260.5	on Floor
16+0			9.9	262.2	
+10 79' W of ℄ = S.E. Cor Frame House			11.2	260.9	on Floor
+50			8.1	264.0	
17+0			5.4	266.7	
+21.39 Δ 43°30' Lt.			4.40	267.67	on Stub
+50			3.9	268.2	
18+0			3.4	268.7	

		272.07		
18+08.71		3.1	269.0	on Floor
"	46 W of SE Cor Frame House	2.8	269.3	Street Level
"		11.3	260.8	Floor Basement on Stat
For Check		7.20	264.87	2+37.77 Blk 22 Page 54 264.85

Hubs Found □

Hubs Set ■

See FB 2222 / P-48

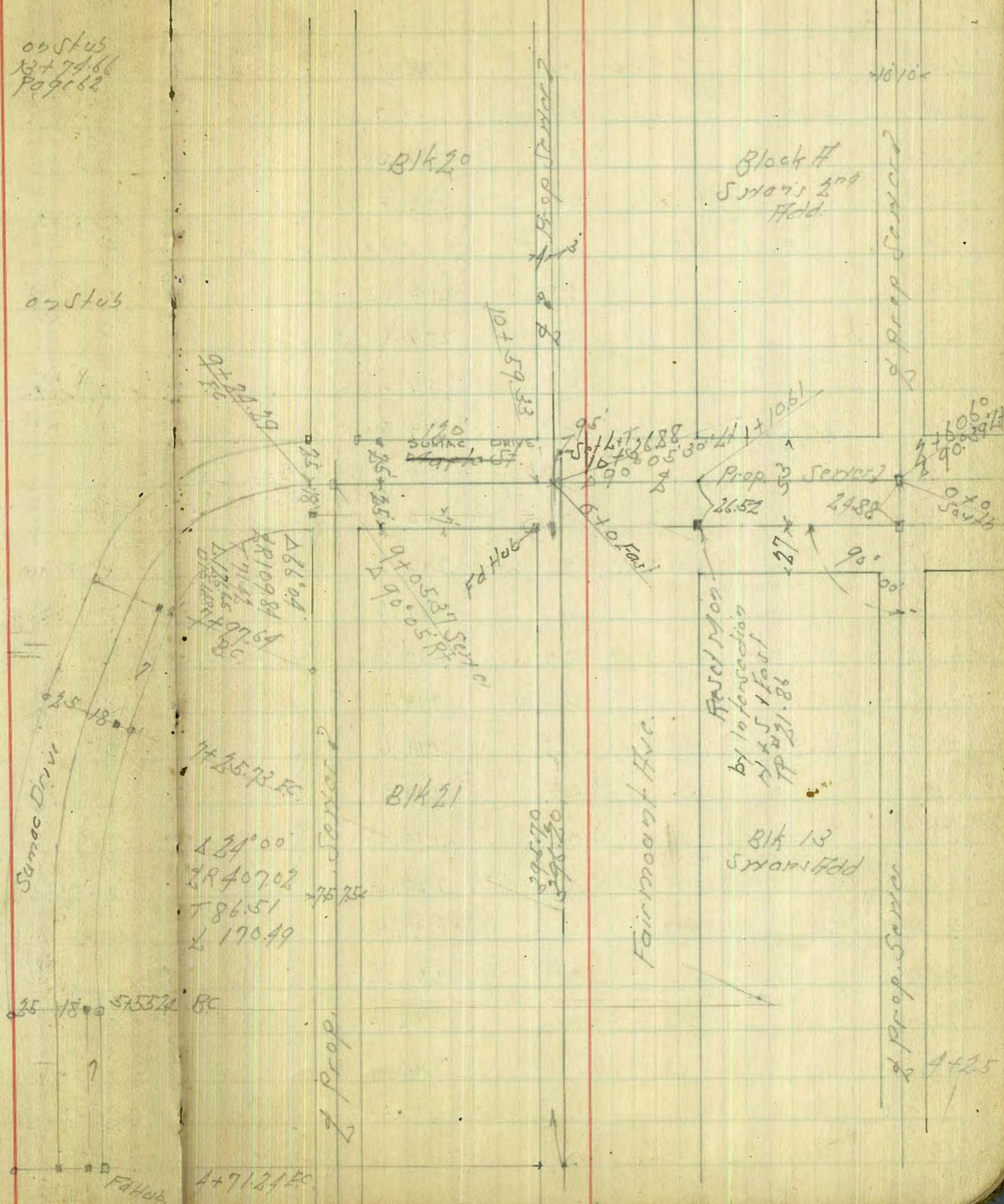


Levels Proposed Sewer Alleys Block 22-21-19-18
+ Fairmount Ave Lexington Park

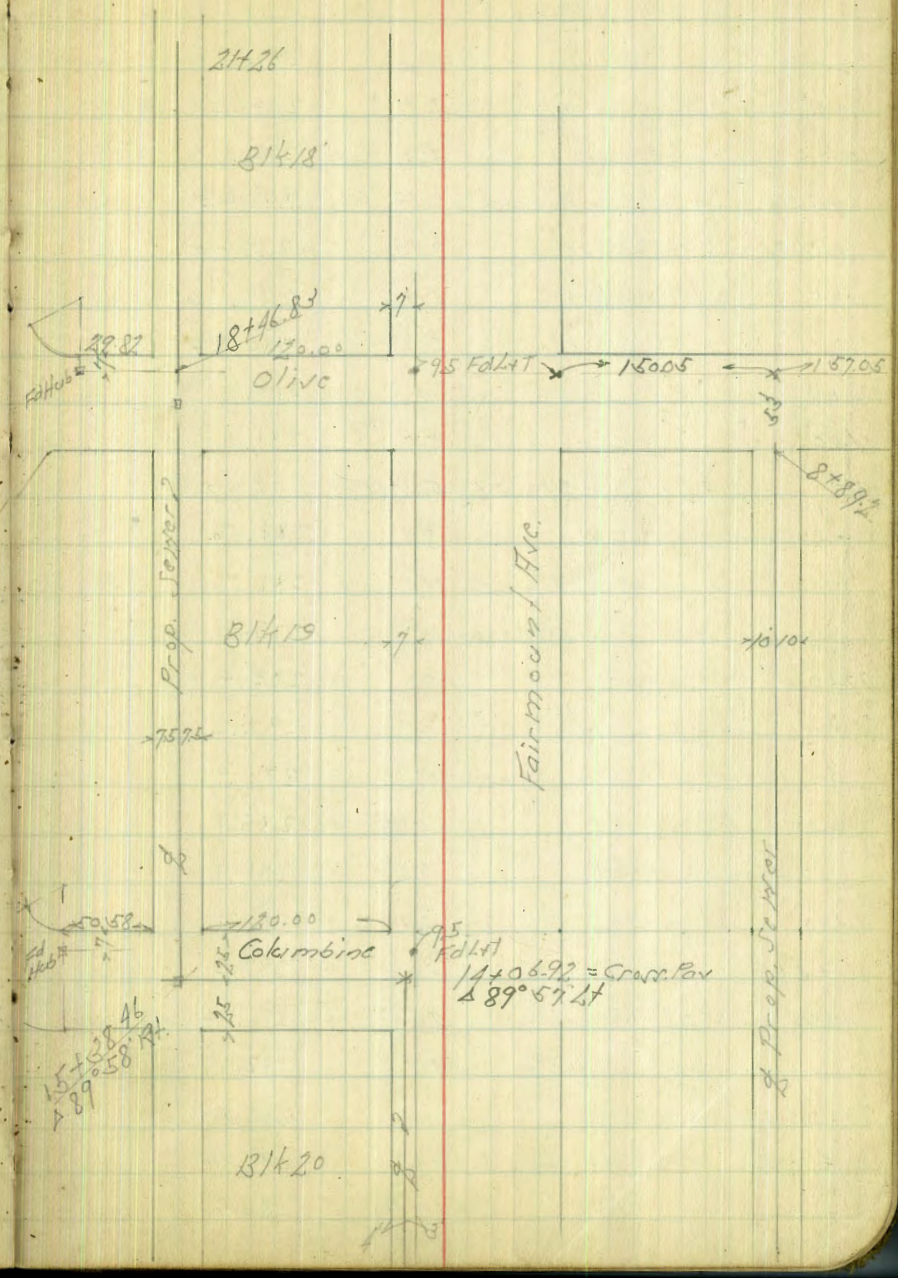
BM	9.49	245.00		235.51	on Stus 13+74.66 Page 62
0+0	= 13+74.66 E+W Alley Block 22				
+16			14.0	231.0	
+50			2.5	242.5	
TP	12.25	256.37	0.88	244.12	
+88.52	∠ 89°56' Lt		7.22	249.15	on Stus
+95			3.9	252.5	
+98	4' Lt of ℄ = Fly Post + Tel Pole				
1+0			2.7	253.7	
TP	12.72	268.43	0.66	255.71	
+50			7.7	260.7	
+56	76 Rt of ℄ = S.W. Cor Stucco House on Floor		0.9	267.5	
+80			3.6	264.8	
2+0			1.4	267.0	
"	94 Lt of ℄ = N.E. Cor. Frame House on Floor		4.6	263.8	
TP	7.30	275.20	0.53	267.90	
+25			6.3	268.9	
+27			9.1	266.1	
+37.77	∠ 33°09' Lt on Stus		10.35	264.85	
+75			9.8	265.4	
3+0			7.6	267.6	
+25			5.2	270.0	
+50			5.2	270.0	
+57	16' Rt of ℄ = N.W. Cor Frame House on Floor		3.8	271.4	
4+0			4.0	271.2	

April 10-46
Sisson
Waddel
Wright

Indexed
C.S.K.



		276.20			
1+16	18' Lt of ℄ Frame House	SE Cor	5.1	272.1	on Floor
"	51' Lt of ℄	Garage	4.5	270.7	" "
+50			2.6	272.6	
+64	9' Lt of ℄ Frame House	℄ + Ely	1.8	273.4	on Floor
TP	9.56	283.78	0.98	274.22	
5+0			9.7	274.1	
+16	10' Lt of ℄ Cobble House	NE Cor	8.0	275.8	on Floor
+50			8.3	275.5	"
+98	74' Rt of ℄ Frame House	NW Cor	4.0	279.8	on Floor
6+0			7.2	276.6	
+10	57' Rt of ℄ Frame House	SW Cor	3.3	280.5	
+21	10' Lt of ℄ Frame House	℄ + Ely	7.1	276.7	on Floor
+50			6.3	277.5	
+80	26' Rt of ℄ Frame House	SW Cor	3.0	280.8	on Floor
7+0			5.1	278.7	
+04	32' Lt of ℄ Frame House	SE Cor	4.2	279.6	on Floor
+50			3.9	279.9	
+83	51' Lt of ℄ Stucco House	℄ + Ely	4.2	279.6	on Floor
8+0			3.2	280.6	
+04	12' Rt of ℄ Shingle House	SW Cor	0.9	282.9	on Floor
+50			2.6	281.2	
+93			1.3	282.5	
9+0			1.9	281.9	
+05.37	∠ 90° 08' Rt.		1.94	281.84	on Stake
TP	1.80	286.64	1.94	281.84	



		286.64			
9+50			3.9	282.7	
+77	27' Rt of ℄ = N W Cor Frame House		2.4	284.2	on Floor
10+0			5.9	280.7	
+32.9	= Wly Conc Paving		7.19	279.45	
+36.88	Δ 90°05' 20" Lt		7.18	279.46	
+51.9	= Gutter on Pav.		6.94	279.70	
"	= N. Cb Maple St		6.41	280.23	
BM			6.41	280.23	N W B P Maple & Fairmount 280.17
11+0			5.5	281.1	
TP	9.22	290.35	5.51	281.13	
+50			8.8	281.6	
"	6' Lt of ℄ = Top Fill		9.2	281.2	
"	11' Lt " " on Slope		15.4	275.0	
12+0			7.0	283.4	
"	6' Lt of ℄ = Top Fill		8.2	282.2	
"	20' Lt " " on Slope		18.5	271.9	
+50			5.3	285.1	
"	34' Lt of ℄		8.5	281.9	
13+0			4.3	286.1	
+50			3.1	287.3	
+92.2	= S Cb Columbine		2.61	287.74	Top
"	Gutter on Paving		3.10	287.25	
14+06.92	= Δ 89°55' Lt		2.55	287.80	
+10.9	= Wly Conc Pav		2.55	287.80	
+50			3.8	286.6	

		290.35			
15+0			4.7	285.7	
+38.46	= Δ 89°58' Rt		5.14	285.21	on Stub
TP	6.10	291.31	5.14	285.21	
+38.46	15' Rt + 45' South of ℄ Columbine = N.E. Cor House		6.0	284.4	on Floor
"	89' Rt + 39' South of ℄ Columbine = N.E. Cor House		6.1	284.3	on Floor
+50			5.7	284.7	
16+0			4.0	286.4	
+01	15' Lt of ℄ = N.E. Cor Calif. House		2.9	287.5	on Floor
+50			2.5	287.9	
TP	7.09	295.99	2.41	288.90	
+55	75' Rt of ℄ = S.W. Cor Stucco House		0.4	295.6	on Floor
17+0			5.4	290.6	
+19	75' Rt of ℄ = N W Cor Stucco House		+1.0	297.0	on Floor
+50			5.2	290.8	
+66	10' Lt of ℄ = S E Cor House Frame		3.7	292.3	on Floor
18+0			5.0	291.0	
TP	8.18	298.82	5.35	290.64	
18+0	62' Rt of ℄ = N W Cor Frame House		1.4	297.4	on Floor
+28.82	= ℄ Olive		8.2	290.6	
+50			7.4	291.4	
+98	68' Rt of ℄ = N W Cor Stucco House		1.1	297.7	on Floor
19+0			6.8	292.0	
"	50' Lt of ℄		8.7	290.1	
+50			7.0	291.8	
20+0			7.1	291.7	

		298.82			
20+0	4 of 4		8.9	289.9	
+50			6.3	292.5	
21+0			3.8	295.0	
+26	= Approx D.E.		3.0	295.8	
TP	6.03	301.53	3.32	295.50	
BM			4.21	297.32	SE&P Quince & Fairmount 29719

Proposed Sewer Alley Block 5
Snapps 2nd Add. Maple to Olive

Sketch Page 65-66

BM	11.28	291.45		280.17	N.W. B.P. Maple + Fairmount
0+0	= 10+36.88 North		12.05	279.40	
+16	on Conc Paving		12.25	279.2	
+36	" "	"	11.60	279.85	
+56	" "	"	12.20	279.25	
+65.9	= Ely Conc Paving		11.79	279.66	
+75			9.8	281.7	
1+0			8.1	283.4	
+50			5.6	285.9	
2+0			5.6	285.9	
+50			5.1	286.4	
+60.60	= Δ 90°59' Lt		4.78	286.67	on Stake
3+0			3.9	287.6	
+25	28 Rt of ℄ = S.W. Cor Frame House		0.9	290.6	on Floor
+50			2.4	289.1	
+60	54 Lt of ℄ = ℄ + Ely Frame House		1.2	290.3	on Floor
TP	8.32	296.82	2.95	288.50	
+60	13' Rt of ℄ = N.W. Cor House		5.5	291.3	on Floor
+73	11 Lt of ℄ = S.E. Cor Bldg.		5.8	291.0	" "
4+0			6.6	290.2	
+50			5.9	290.9	
5+0			5.2	291.6	
+36	12' Rt of ℄ = S.W. Cor House		3.9	292.9	on Floor
+50			4.8	292.0	
6+0			4.2	292.6	

indexed
C.S.K.

April 17-46
Sisson
Wright
Waddel

		296.82			
6+35	63 Lt of ℄ = N.E. Cor Frame House		2.3	294.5	on Floor
+50			3.9	292.9	
7+0			3.5	293.3	
+50			3.3	293.5	
TP	7.65	301.47	3.00	293.82	
+84	50 Lt of ℄ = N.E. Cor Frame House		4.8	296.7	on Floor
8+0			7.5	294.0	
+03	90 Rt of ℄ = N.W. Cor Stucco House		3.8	297.7	on Floor
+50			7.0	294.5	
+54	14 Lt of ℄ = S.E. Cor Frame House		4.1	297.4	on Floor
+89.2	= S.L. Olive		6.5	295.0	
TP	5.66	301.16	5.97	295.50	
BM			3.94	297.22	S.E. B.P. Quince + Fairmount 297.19

Proposed Sewer Alley Block 13
Swan's Add. South of Maple St.

Sketch Page 64

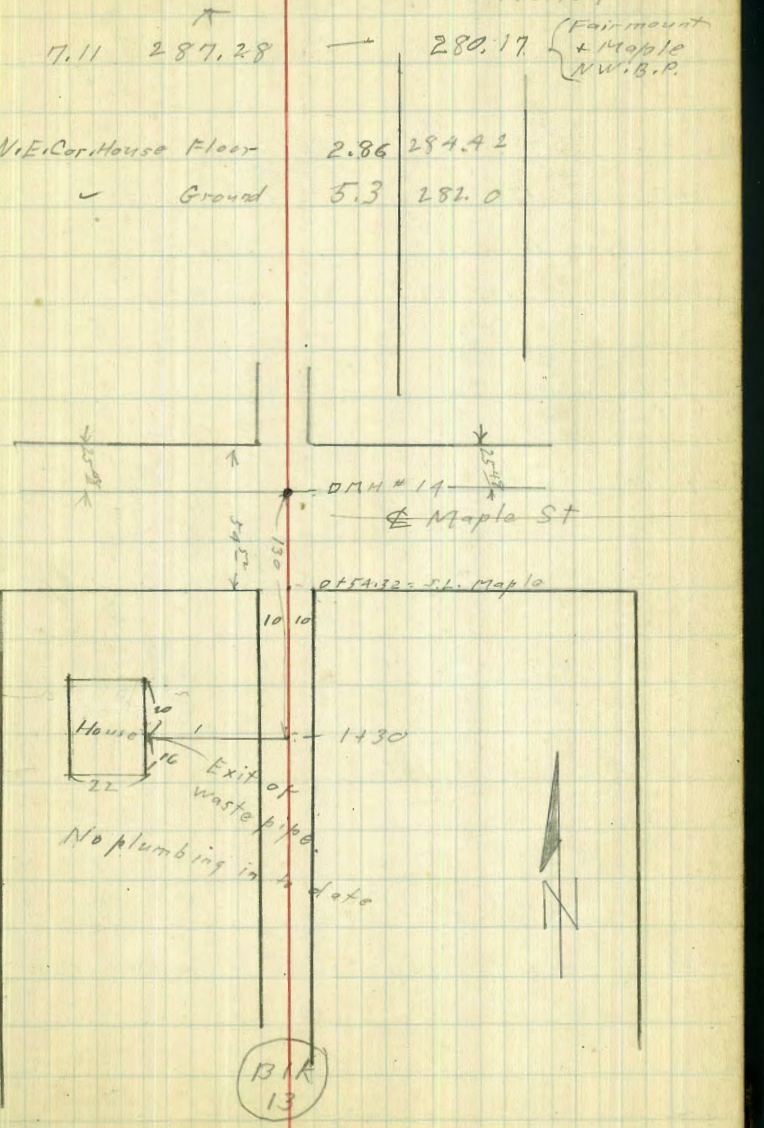
BM	2.74	289.41		286.67	on Stub 2+60.60 Rt.
0+0	= 2+60.60 North				
+50			5.0	286.4	
1+0			3.9	285.5	
"	100' Rt of ℄		6.6	282.8	
+26	42' Lt of ℄ = SW Cor Frame House		0.1	289.3	on Floor
+50			4.5	284.9	
2+0			5.6	283.8	
"	100' Rt of ℄		9.3	280.1	
+50			6.4	283.0	
3+0			7.7	281.7	
"	100' Rt of ℄		12.4	277.0	
+50			9.1	280.3	
4+0			11.9	277.5	
+25	= Rim of Canyon		14.6	274.8	

Additional Levels Blk 13 69

4-3-47
Sommermeyer-
W Moore
Melton

7.11 287.28 — 280.17 (Fairmount + Maple N.W.B.P.

20'S. of N.E. Cor. House Floor 2.86 284.42
" " " Ground 5.3 281.0



Cross Section Modesto St.
Juniper St to Laurel St.

Indexed C.S.K.

Sketch Page 63

May 2 46
Sunny
Waddel
Allen

Station	Remarks	Lt: W				℄				Rt: E
1+50			262.1 2.5/25	261.6 3.0/17	260.3 4.3/12	260.6 4.0	260.6 4.0/8	260.1 4.5/15	259.9 4.7/25	259.3 5.3/35
1+30	17.6 Rt of ℄ = Ely Power Pole		262.2 2.4/25	261.6 3.0/17	260.1 4.5/15	260.5 4.1	260.6 4.0/15	260.2 4.4/25		
1+0			261.3 3.3/25	260.9 3.7/17	259.3 5.3/14	259.9 4.7	259.9 4.7/5	260.2 4.4/7	260.1 4.5/15	260.0 4.6/25
0+50			259.1 5.5/25	258.9 5.7/17	257.3 7.3/14	257.9 6.7	258.0 6.6/5	258.4 6.2/6	258.0 6.6/15	257.9 6.7/25
0+17.99	= B.C. on Lt.		257.3 7.3/25	256.8 7.8/18	255.9 8.7/15	256.4 8.2	256.3 8.3/9	256.6 8.0/10	256.4 8.2/15	256.5 8.1/25
0+0	= ℄ Juniper St Taken on Diagonal	256.9 7.7/38' E.C.	256.4 8.2/29	255.4 9.2/25.6	255.7 8.9/15	255.6 9.0	255.2 9.4/9	256.0 8.6/13	256.0 8.6/15	255.3 9.3/25.6
BM	11.90 264.55 252.65 on Mon Juniper & Modesto #1702.8					264.55				

Notes Reduced
10-15-47

Modesto St.

TP	9.34	268.98	8.60	259.64
4+50				
4+0				
3+50				
3+0				
2+52	18.2 Rt c/℄ = Elec. Power Pole			
TP	8.01	268.24	4.32	260.23
2+0				
		264.55		

Sta.	Lt			℄			Rt		
4+50	261.8	261.1	259.6	259.6	259.6	258.2	257.0	255.0	253.0
	6.4 / 25	7.1 / 19	8.6 / 13	8.6	8.6 / 3	10.0 / 8	11.2 / 15	13.2 / 25	15.2 / 35
4+0	262.1	260.8	259.5	259.6	259.6	258.4	257.2	255.2	253.6
	6.1 / 25	7.4 / 17	8.7 / 15	8.6	8.6 / 2	9.8 / 6	11.0 / 15	13.0 / 25	14.6 / 35
3+50	262.1	261.5	259.6	259.5	259.5	258.5	257.1	255.5	253.8
	6.1 / 25	6.7 / 18	8.6 / 15	8.7	8.7 / 2	9.7 / 6	11.1 / 15	12.7 / 25	14.4 / 35
3+0	262.1	261.1	259.9	259.8	260.0	257.8	256.9	255.4	254.2
	6.1 / 25	7.1 / 18	8.3 / 14	8.4	8.2 / 4	10.4 / 9	11.3 / 15	12.8 / 25	14.0 / 35
2+52	261.3	260.9	259.8	260.0	260.0	258.2	257.4	256.6	255.5
	6.9 / 25	7.3 / 20	8.4 / 13	8.2	8.2 / 3	10.0 / 9	10.8 / 15	11.6 / 25	12.7 / 35
TP				268.24					

Sta.	Lt			℄			Rt	
2+0	262.1	261.4	260.0	260.4	260.4	259.0	258.1	257.7
	2.5 / 25	3.5 / 19	4.6 / 14	4.2	4.2 / 6	5.6 / 15	6.5 / 25	6.9 / 35
				264.55				

	Lt			Rt
6+50	261.5 7.5 25	261.2 7.8 15	260.6 8.4	259.1 9.9 15	258.5 10.5 25	257.6 11.4 35
6+25	262.0 7.0 25	261.6 7.4 15	260.6 8.4	260.3 8.7	259.7 9.3 12	259.4 9.6 15	258.6 10.4 25	257.8 11.2 35
6+0	262.1 6.9 25	261.6 7.4 15	260.7 8.3	260.6 8.4 15	260.2 8.8 9	259.6 9.4 15	258.6 10.4 25	257.8 11.2 35
5+72.43 B.C. Rt.	262.9 6.1 25	262.3 6.7 18	260.8 8.2 15	260.5 8.5	260.4 8.6 15	259.6 9.4 8	259.0 10.0 15	257.9 11.1 25	257.2 11.8 35	257.0 12.0 35
5+50	262.5 6.5 25	261.6 7.4 17	260.3 8.7 15	260.2 8.8	260.2 8.8 4	259.3 9.7 7	258.5 10.5 15	257.2 11.8 35	256.4 12.6 35	256.2 12.8 35
5+0	262.1 6.9 25	261.4 7.6 18	259.8 9.2 25	259.8 9.2	259.0 9.2 5	258.4 10.6 8	257.3 11.7 15	255.9 13.1 25	254.3 14.7 35	

268.98

268.98

Modesto St.

8+07.00 = BC Rt+Lt.				
7+75				
+52	15.4 Lt of ℄ = Wly Power Pole			
7+50				
B.M.		7.15	261.83	on Meter Box Sewer Survey Page 67 261.93
7+09.61 = E.C.				
6+75				
	268.98			

Lt = W				℄	Rt = E			
264.4 4.6/25	264.4 4.6/15	264.0 5.0/12		264.6 / 4.4	264.2 4.8/15	265.2 3.8/18	264.9 4.1/25	264.4 4.6/35
	262.8 6.2/25	263.1 5.9/15		263.0 / 6.0	262.6 6.4/15	262.4 6.6/25	262.3 6.7/35	
	262.1 6.9/25	262.4 6.6/15		262.2 / 6.8	261.6 7.4/15	261.3 7.7/20	261.0 8.0/25	260.5 8.5/35
	261.7 7.3/25	261.6 7.4/15		261.2 / 7.8	260.6 8.4/15	260.3 8.7/25	259.2 9.8/35	
261.6 7.4/25	261.6 7.4/18	260.9 8.1/13		260.6 / 8.4	260.2 8.8/15	259.3 9.7/21	259.0 10.0/25	258.1 10.9/35
				268.98				

Cross Section Sumac Drive
Juniper St to Laurel St.

May 3-46
Sisson
Waddel
Allen

Sketch Page 63

1+64

1+50 — 21.5 Rt of ℄ = Fence

1+0

0+51.46 = E.C. on Rt — 24' Rt of ℄ = Fence Line

0+31.17 = N.L. Juniper Taken on Diag

0+0 = 1st Std Line South Taken on Diag

TP	7.66	260.50	12.45	252.84	on Mon S.L. Juniper N.L. Sumac
BM	12.64	265.29		252.65	on Mon Juniper + Modesto #1702-8

Indexed E.S.K.

250.85
9.65
31' Lt Fl. House or Fdn.

Station	Lt - 1/4				℄		Rt - E		
1+50	249.4 / 11.1 / 35	250.6 / 9.9 / 25	251.7 / 8.8 / 15	252.2 / 8.3 / 10	252.5 / 8.0	252.5 / 8.0 / 12	254.9 / 5.6 / 15	256.3 / 4.2 / 25	
1+0	249.6 / 10.9 / 35	251.2 / 9.3 / 25	252.4 / 8.1 / 15	253.2 / 7.3 / 10	253.9 / 6.6	254.0 / 6.5 / 15	256.0 / 4.0 / 18	257.7 / 2.8 / 25	
0+51.46	250.5 / 10.0 / 35	252.1 / 8.4 / 25	253.3 / 7.2 / 15	254.7 / 5.8 / 7	254.9 / 5.6	255.1 / 5.4 / 15	257.4 / 3.1 / 19	258.2 / 2.3	
0+31.17	248.8 / 11.7 / 50	252.1 / 8.4 / 26	253.9 / 6.6 / 15	254.9 / 5.6 / 11	255.8 / 4.7	255.7 / 4.8 / 15	256.1 / 4.4 / 21	258.1 / 2.4 / 26	258.8 / 1.7 / 40
0+0	248.1 / 12.4 / 50	252.8 / 7.7 / 26	254.5 / 6.0 / 15		256.9 / 3.6	258.2 / 2.3 / 15	258.9 / 1.6 / 26	259.2 / 1.3 / 50	

260.50

Sumac Drive

Station	Remarks				Lt = W				℄		Rt = E	
3+11	17.5 Rt of ℄ = Ely Power Pole											
3+0					249.9 / 16.3 / 35	251.0 / 15.2 / 25	252.4 / 13.8 / 15	254.3 / 11.9 / 5	254.5 / 11.7	254.5 / 11.7 / 15	256.9 / 9.3 / 21	257.8 / 8.4 / 25
TP	10.97	266.17	5.80	255.20					266.17			
2+82.81 = E.C.	24.5 Rt of ℄ = Fence				249.2 / 11.3 / 35	250.2 / 10.3 / 25	252.0 / 8.5 / 15	253.2 / 6.8 / 5	253.9 / 6.6	253.6 / 6.9 / 15	256.1 / 4.4 / 20	257.4 / 3.1 / 25
2+50					249.1 / 11.4 / 35	250.3 / 10.2 / 25	251.5 / 9.0 / 15	252.8 / 7.7 / 5	252.9 / 7.6	252.9 / 7.6 / 15	254.6 / 5.9 / 19	255.4 / 5.1 / 25
2+25	24 Rt of ℄ = Fence				248.6 / 11.9 / 35	249.9 / 10.6 / 25	251.2 / 9.3 / 15	252.3 / 8.2 / 7	252.4 / 8.1	252.6 / 7.9 / 15	254.5 / 6.0 / 20	254.8 / 5.7 / 25
1+93.76 = B.C. Rt.					248.5 / 12.0 / 35	248.5 / 12.0 / 25	250.8 / 9.7 / 15	251.9 / 8.6 / 10	252.05 / 8.45 / 57.5 Sta.	252.7 / 7.8 / 15	254.2 / 6.3 / 25	
1+87							248.9 / 11.6 / 32' Lt Ely Garage Dirt Floor					
1+65	20' Rt of ℄ = Ely Power Pole 260.50								260.50			

Sumac Drive

TP	7.02	270.52	2.67	263.50
6+0				
5+50				
+14	14.7 Rt of ℄ - Ely Power Pole			
5+0				
4+50				
4+0	16.1' Rt of ℄ - Ely Power Pole			
3+52				
		266.17		

Lt ℄ Rt

Sta.		Lt					℄	Rt		
6+0		257.1 (9.1 / 35)	258.6 (7.6 / 25)	260.2 (6.0 / 15)	261.2 (5.0 / 10)	263.2 (3.0 / 5)	263.0 (3.2)	262.6 (3.6 / 13)	265.3 (0.9 / 18)	266.4 (+0.2 / 25)
5+50		255.6 (10.6 / 35)	257.2 (9.0 / 25)	259.4 (6.8 / 15)	260.6 (5.6 / 7)	262.1 (4.1 / 4)	261.9 (4.3)	261.5 (4.7 / 14)	265.3 (0.9 / 19)	266.6 (+0.4 / 25)
5+0	253.7 (12.5 / 35)	254.1 (12.1 / 25)	254.2 (12.0 / 21)	258.0 (8.2 / 16)	258.8 (7.4 / 6)	260.4 (5.8 / 4)	260.4 (5.8)	260.1 (6.1 / 13)	263.6 (2.6 / 19)	264.7 (1.5 / 25)
4+50	253.0 (13.2 / 35)	253.2 (13.0 / 25)	255.67 (10.50 / 22.5 = Top of Wall)	256.8 (9.4 / 18)	257.2 (9.0 / 8)	259.3 (6.9 / 5)	259.2 (7.0)	258.8 (7.4 / 13)	261.9 (4.3 / 18)	263.1 (3.1 / 25)
4+0	253.8 (12.4 / 40 = Ely House on Floor)	252.5 (13.7 / 25)	255.30 (10.87 / 23 = Top of Wall)	256.0 (10.2 / 15)	257.6 (8.6 / 5)		257.6 (8.6)	257.4 (8.8 / 12)	260.9 (5.3 / 26)	261.8 (4.4 / 35)
3+52	251.1 (15.1 / 35)	252.3 (13.9 / 26)	254.02 (12.15 / 33.3 = Sly Garage 10" Wall)	253. (12.3 / 15)	255.8 (10.4 / 5)		256.0 (10.2)	256.0 (10.2 / 13)	259.2 (7.0 / 19)	260.2 (6.0 / 25)

266.17

Sumac Drive

51.2
25.6
26.12

Station	Remarks	Lt					℄			Rt
7+57.28		260.80 (9.72 / 51.2)	261.78 (8.74 / 25±)	262.1 (8.4 / 15)	261.8 (8.7 / 7)		262.0 (8.5)	262.2 (8.3 / 15)	262.1 (8.4 / 25)	
7+28.36	B.C. Lt.		261.8 (8.7 / 35)	262.1 (8.4 / 25)	262.7 (7.8 / 15)	262.7 (7.8 / 10)	262.9 (7.6)	262.7 (7.8 / 15)	264.2 (6.3 / 20)	264.3 (6.2 / 25)
7+0			261.3 (9.2 / 35)	262.1 (8.4 / 25)	262.8 (7.7 / 15)	263.3 (7.2 / 9)	263.4 (7.1)	262.9 (7.6 / 14)	265.0 (5.5 / 19)	265.2 (5.3 / 25)
+92	15' Lt of ℄ = N'ly Tel + Pow Pole									
6+71.73	= E.C.	260.2 (10.2 / 35)	261.3 (9.2 / 25)	262.2 (8.3 / 15)	262.7 (7.8 / 11)	263.5 (7.0 / 7)	263.5 (7.0)	263.1 (7.4 / 13)	265.3 (5.2 / 18)	265.6 (4.9 / 25)
6+42.75		258.7 (11.8 / 35)	259.8 (10.7 / 25)	261.1 (9.4 / 15)	261.7 (8.8 / 9)	263.7 (6.8 / 5)	263.4 (7.1)	262.8 (7.7 / 15)	264.9 (5.6 / 19)	265.4 (5.1 / 25)
6+18.77	B.C. Rt.	257.5 (13.0 / 35)	258.8 (11.7 / 25)	260.3 (10.2 / 15)	260.8 (9.7 / 11)	263.3 (7.2 / 5)	263.1 (7.4)	262.7 (7.8 / 15)	265.2 (5.3 / 19)	265.7 (4.8 / 25)

S'ely Garage Conc Flr.
25± S'Ely Conc Drive to Apt Bldg

270.52

270.52

Sumac Drive

		Lt.	℄	Rt.
BM		8.70	261.82	07 Meter Box Senior Survey: Page 62 261.99
8+15.13	EC 07 Lt.			
8+12	13' Lt of ℄ = NW ly Tel + Power Pole			
7+86.30				
	270.52			

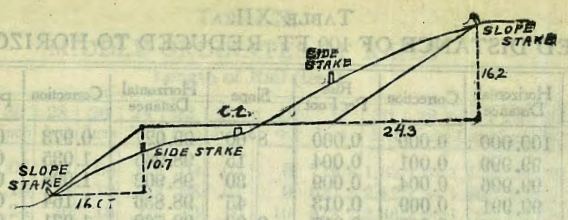
261.4	261.5	261.7	261.3	261.4	261.6	261.0	260.5		
9.1	9.0	8.8	9.2	9.1	8.9	9.5	10.0		
15	25	15	11		6	15	25		
				270.52					
	261.5	261.6	260.6	260.7	260.2	259.9	259.2		
	9.0	8.9	9.7	9.8	10.3	10.5	11.3		
	25	15	9		15	21	25		

Revision of Proposed Sewer
Fairmount & Home Ave.

Sketch Page 60

				153.00	on Stob 2+42.85 & Page 60
BM	4.48	157.48			
1+33.17	162.10 ME = Exist Man Hole		7.39	150.09	on Rim
"			20.16	137.32	Flow Line
"	"		8.09	149.39	on Stob
+38			7.5	150,0	
+41			6.1	151.4	
+51.5	Ely Paving Home Ave		5.80	151.68	
+66	on "		5.10	152.08	
+89	Ely " " "		6.10	151.38	
2+0			6.3	151.2	
+18			4.9	152.6	
+42.85	POT		4.48	153.00	on Stob

May 7-46
Sisson
Waddell
Allen



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1 65	1 80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3 45	3.60	3 75	3.90	4.05	4.20	4 35	2
3	4.50	4 65	4.80	4.95	5 10	5 25	5 40	5.55	5.70	5.85	3
4	6.00	6 15	6.30	6.45	6.60	6 75	6.90	7.05	7.20	7.35	4
5	7 50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9 00	9 15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10 35	6
7	10.50	10 65	10.80	10.95	11.10	11.25	11.40	11.55	11 70	11.85	7
8	12.00	12 15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13 50	13 65	13 80	13 95	14.10	14.25	14.40	14 55	14.70	14.85	9
10	15.00	15 15	15 30	15 45	15.60	15.75	15.90	16.05	16.20	16 35	10
11	16 50	16 65	16 80	16.95	17 10	17.25	17.40	17.55	17.70	17.85	11
12	18 00	18 15	18.30	18 45	18.60	18 75	18.90	19.05	19.20	19 35	12
13	19 50	19 65	19.80	19.95	20.10	20.25	20 40	20.55	20.70	20.85	13
14	21.00	21 15	21.30	21,45	21 60	21.75	21.90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23.10	23,25	23.40	23.55	23.70	23.85	15
16	24.00	24 15	24 30	24 45	24.60	24.75	24 90	25 05	25.20	25.35	16
17	25.50	25 65	25.80	25 95	26.10	26 25	26 40	26.55	26.70	26.85	17
18	27.00	27 15	27.30	27 45	27.60	27.75	27.90	28.05	28 20	28.35	18
19	28 50	28 65	28 80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30 00	30 15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31 50	31 65	31.80	31.95	32 10	32 25	32.40	32.55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33.60	33 75	33.90	34.05	34.20	34.35	22
23	34 50	34 65	34.80	34.95	35.10	35 25	35 40	35.55	35.70	35 85	23
24	36.00	36 15	36.30	36 45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37 80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39 00	39 15	39.30	39 45	39 60	39.75	39.90	40.05	40.20	40.35	26
27	40 50	40 65	40 80	40.95	41.10	41.25	41 40	41.55	41.70	41.85	27
28	42 00	42 15	42.30	42.45	42.60	42 75	42.90	43.05	43.20	43.35	28
29	43 50	43 65	43.80	43 95	44.10	44 25	44 40	44.55	44.70	44 85	29
30	45 00	45 15	45.30	45 45	45.60	45.75	45.90	46.05	46 20	46.35	30
31	46.50	46.65	46.80	46 95	47.10	47 25	47.40	47.55	47.70	47.85	31
32	48 00	48.15	48.30	48 45	48.60	48 75	48.90	49.05	49 20	49.35	32
33	49 50	49 65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51 00	51.15	51.30	51.45	51.60	51 75	51.90	52.05	52.20	52.35	34
35	52 50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54 00	54 15	54.30	54 45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55 50	55 65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57 00	57.15	57.30	57 45	57.60	57 75	57.90	58.05	58.20	58 35	38
39	58 50	58.65	58 80	58.95	59.10	59 25	59.40	59 55	59.70	59.85	39
40	60 00	60 15	60 30	60 45	60 60	60.75	60 90	61.05	61 20	61.35	40
41	61.50	61 65	61.80	61 95	62 10	62 25	62.40	62 55	62 70	62.85	41
42	63 00	63.15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64.35	42
43	64.50	64 65	64 80	64.95	65.10	65 25	65 40	65.55	65.70	65.85	43
44	66 00	66 15	66 30	66.45	66.60	66 75	66.90	67.05	67.20	67.35	44
45	67 50	67 65	67 80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69 00	69 15	69 30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70 50	70 65	70 80	70 95	71.10	71.25	71 40	71.55	71.70	71.85	47
48	72.00	72 15	72.30	72.45	72.60	72.75	72.90	73 05	73.20	73 35	48
49	73 50	73 65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.

South End Bor. 24.45 74+55 93
in Pale

Pale right 24.99 82+35

11+87 84
12+23-97
36 13

2032
96.78
2128.78

97711
82
195422
78.1688
80.12302

63+02

216.97
101.65
318.62

40°-09'
80-19

255
3
765
120
885

1.51
800
500
3000
2400
8000

500
316
184.05

5° 33' 00

430
183
196
2039
2758

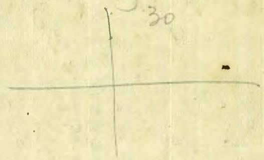
99.39
98.21
1.18

42-35
2 | 85-09
42-34-30

929.54
516.89
412.65

80-11
160-22-30
80-11-15
179-59-60
99-48-45

4 | 125-10 = 31-17-30
4 | 70 =
30



N 89-19-29 E
88-56
178-15-29
179-59-60
01-44-31

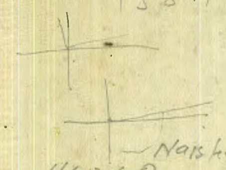
42 18
N 40-52
1° 26

N 88-51 E
91-55
180-46

620.45
461.71
158.74

90.77
75.00
43.00
208.77
1509.23
1718.00

N 88-51
S 27-53-44 E
116-44-44
179-59-60
S 89-59-11 E
90-00-49



4634 Orange

471.19

500
287
213

549.62

2077.76
111.43
21.89.19

308.72

1-23
.46
S 0-37 E
S 1-44-31 E
1-07-31 -L

659.17
12.48
671.65

240.20
44.23
195.97