

1340

SOLICITAD NO



EVERY BOOK

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Sta	+	Hl.	-	El.
B.W.	9.00	403.99		394.99
T.P.	6.60	409.17	1.42	402.57
T.P.	10.49	419.52	0.14	409.03
T.P.	12.76	428.59	3.69	415.83
T.P.	7.24	435.69	0.14	428.45
B.M.			5.67	430.02
T.P.	12.96	445.29	3.36	432.33
T.P.	0.46	437.79	7.96	437.33
T.P.	0.73	425.85	12.67	425.12
T.P.	2.22	423.58	4.49	421.36
B.M.			6.67	416.91

0+00

**INDEXED**

WK  
**FEB 15 1949**

1.14 418.05

		6.28	417.30
		2.77	420.81
		4.44	419.14
		7.10	416.48
		5.48	418.10
		6.67	416.91
1		5.7	412.3
2		11.8	406.2
	2.29	12.07	405.98
3		1.5	403.8
4		6.5	401.8
5		9.2	399.1
	0.79	11.41	396.86

## PROFILE AND TOPOGRAPHY

Bolt in Culvert H.W., Eastly side  
Biological Road at Italian Villa

Apr. 29, 1929 { Osborne &  
Hilbourne Rod  
Remmen "

Stob on West side of paving opposite blazed tree. top of Second  
rise north of Service Station

**INDEXED**

WK

**FEB 15 1949**

Nail in Gum tree 20' left of sta. 0+45

Edge of Pavement.

" " 200' South  
" " 100' "  
" " 100' North  
" " 200' "

± Profile

SOLEDA VALLEY ROAD  
Government Canyon Line

On ± Hub Sta. 5+56.25

Sta	+	HI	-	E.L.
		397.65		
6			2.5	395.1
7			7.3	390.3
8			11.3	386.3
	2.05	386.75	12.95	384.70
9			4.0	382.7
10			8.1	378.6
BM			10.72	376.03
	0.26	376.29		
11			17	374.6
12			6.7	369.6
13			11.2	365.1
	1.33	365.55	12.07	364.22
14 ±			4.1	361.4
2L			2.4	363.1
2R			5.9	359.6
15			8.0	357.5
16			10.6	354.9
17			12.9	352.6

± Profile

Nail in Gum Tree 20' Rt. Sta. 10+50

Note:

All distances Lt. or Rt. are from ±.  
 At P.I. X-Sec taken on bisection of angle -  
 Alignment Notes in Book #1339, Pg. 13

Sta	+	HI	-	El.					
						351.70			
		365.55			30' L.		9.7	342.0	3
					30' R.		12.0	339.7	
			12.63	352.92	T.P.	0.99	340.61	12.02	339.62 ✓
	5.72	358.64							
18			7.1	351.5	25+50		11.3	329.3	
A.L			5.0	353.6	T.P.	0.14	328.50	12.25	328.36
A.R			10.4	348.2	T.P.	0.77	316.82	12.45	316.05 ✓
19			7.5	351.1	26		3.1	313.7	
30 L			5.4	353.2	30' L		3.2	313.6	
40 R			11.5	347.1	30' R		+2.2	319.0	
					T.P.	0.60	304.24	12.58	304.24 ✓
20			3.5	355.1	27		20.0	284.8	
T.P.	7.64	363.68	2.60	356.04	30' L.		6.9	297.9	Same Slope 40' further
21			5.0	358.7	30' R.		6.4	298.4	SS 40' further
22			4.6	359.1	T.P.	0.17	292.48	12.53	292.31
P.L. 22+26			4.42	359.26	B.M.				
23			6.7	357.0	28		17.5	275.0	
24			11.5	352.2	30' L.		4.0	288.5	SS 40'
T.P.	0.71	351.70	12.69	350.99	11' R.		24.7	267.8	
24+56 <sup>36</sup>			4.6	347.1	40' R.		7.3	285.2	SS 40'
					T.P.		12.60	279.98	
25			1.16	340.1		1.69	281.57		

Sta	+	H.I.	-	E.L.		Sta.	+	H.I.	-	E.L.
29		281.57	18.4	263.2		T.P.	0.64	257.26	12.60	244.66
20' L			7.7	273.9						
30 "			2.2	279.4	Same Slope 40' further	31+10			5.6	239.7
12' R			21.4	260.2		30' R			+11.0	256.3
33 "			22.8	258.8	Level 20' then up	22' L			31.0	214.3
	0.39	269.47	12.49	269.08		34' L			10.0	235.3
	0.42	257.26	12.63	256.84		65' L			4.0	241.3
+66			9.4	247.9		85' L			+2.5	247.8
20' L			0.0	257.3	SS 30' further					SS 40'
10' R			8.7	248.6		32			18.0	227.3
40' R			+3.2	260.5	SS 30'	10' R			33.9	211.4
						18' R			20.6	224.7
30			19.9	237.4		40' "			13.4	231.9
2' L			11.4	245.9		60' "			5.0	240.3
15' L			11.0	246.3		30' Lt.			11.8	233.5
50' "			+2.0	259.3	SS to top of 20' Knoll	50' "			5.0	240.3
18' R			7.2	250.1		T.P.	0.87	233.41	12.76	2325.4
40' "			+5.1	262.3	SS 30'	32+65			36	229.8
						20' R			11.3	222.1
30+65			14.4	242.9		35' R			25.0	208.4
30' R			+3.1	260.4	SS 40'	50' R			13.3	220.1
17' L			28.0	229.3		65' "			11.0	222.4
72' L			26.5	230.8		85' "			2.0	231.4
79' "			14.0	243.3		30' Lt.			+13.0	246.4
100' L			10.5	246.8						SS 30'

Sta	+	H.I.	-	El.		Sta	+	H.I.	-	El.	
		233.41						215.53			5
33 ✓			6.1	226.8		35+76.45 ✓			10.3	205.2	
26' R.			15.8	217.6		10' Lt.			6.6	208.9	
37 "			29.8	203.6		25 "			+1.6	217.1	SS. 50.
51' R			17.0	216.4		24' R.			19.0	196.5	
70 "			14.1	219.3	then up steep slope	18 "			24.7	190.8	
30' Lt.			+7.0	240.4	SS. 70.	BM			10.29	205.24	On Pl. Hub 35476.45
T.P. /	0.26	220.99	12.69	220.73		37+00 ✓	1.95	207.19			
34			+3.5	224.5		17' R.			4.1	203.1	
20' Lt.			+14.3	235.3	SS. 70.	67 "			14.0	193.2	
23' R.			9.0	212.0		20' Lt.			25.0	182.2	
36' R			23.0	198.0					+9.2	216.4	SS. 70' more
45 R.			14.0	207.0					12.38	194.81	
70' R.			8.1	212.9			2.29	197.10			
	0.37	215.53	5.83	215.16		38 ✓			3A	193.7	
35 ±			1.0	214.5		16' Lt.			+4.1	201.2	
18' R.			8.3	207.2		11 "			+18.0	215.1	SS. 70.
14 "			16.2	199.3		20' R.			9.5	187.6	
26' Lt.			+12.0	227.5	SS. 70.	70 "			23.8	173.3	Level 50.
+42 ✓			5.6	209.9		+80 ✓			+2.8	199.9	
20' Lt.			+6.5	222.0	SS. 70.	20' Lt.			+18.7	215.8	SS. 50.
16' R.			12.7	202.8		36' R.			2.1	176.0	
51 "			21.2	194.3		57 "			29.6	167.5	Level 50' more



Sta.	+	H.I.	-	El.
		197.10		
39+47 <sup>45</sup>			+ 0.4	197.5
25' Lt.			+ 15.7	212.8
50 "			+ 28.5	225.6
60 "			+ 31.8	228.9
55 Rt.			33.0	164.1
			12.56	184.54
	0.15	184.69		
40			5.6	179.1
60 Lt.			4.0	180.7
27 Rt.			12.9	171.8
57 "			26.7	158.0
			12.51	172.18
	0.15	172.33		
BM			12.55	159.78
	0.80	160.58		
40+73			7.0	153.6
81 Lt.			2.0	158.6
100 "			0.8	159.8
55 Rt.			5.1	155.5
95 "			10.2	150.4

S.S.  
40'  
Level  
30'

S.S.  
50'

Level  
30'

On Hub 35 Rt.  
Sta 40+55

Level  
30' more

Sta.	+	H.I.	-	El.
		160.58		
Alt 03			10.3	150.3
100 Lt.			13.0	147.6
94 Rt.			12.8	147.8
				Level 30'
+ 20			22.3	138.3
43 Lt.			4.3	156.3
73 "			1.6	156.0
86 "			0.0	160.6
100 Rt.			31.5	129.1
				S.S. 30'
				S.S. 50'
+ 48			+ 1.6	162.2
25 Lt.			+ 7.0	167.6
100 "			+ 15.5	176.1
55 Rt.			10.9	149.7
90 "			17.7	142.9
			5.18	155.40
	8.65	164.05		
42+00			+ 14.2	178.2
40 Lt.			34.3	129.7
70 "			13.8	120.2
28 Rt.			1.0	163.0
41 "			14.8	149.2
95 "			19.3	144.7

Sta	+	H.I.	-	ΣI.	
		164.05			
42+42			+12.1	176.1	
30' Lt.			+29.3	193.3	
55"			+12.8	206.8	$\frac{S.S.}{40}$
20' Rt.			0.0	164.0	
50"			8.5	155.5	
94"			19.7	144.3	
43+13			14.1	149.9	
57' Lt.			7.9	156.1	$\frac{S.S.}{50}$
100' Rt.			21.0	143.0	
+73			5.2	158.8	
84' Lt.			0.2	163.8	
54' Rt.			12.6	151.4	
92"			25.4	138.6	
			4.47	159.58	
	1.97	161.55			
43+90			+0.6	162.1	
65' Lt.			+13.0	174.5	
70' Rt.			11.5	150.0	

Sta	+	H.I.	-	ΣI.	
		161.55			
44+23 <sup>27</sup>			+8.7	170.2	
25' Lt.			+23.5	185.0	$\frac{S.S.}{20}$
230' Rt.			4.1	157.4	
93"			16.4	145.1	
45			6.1	155.4	
20' Lt.			0.0	161.5	
43"			+13.0	174.5	$\frac{S.S.}{40}$
60' Rt.			17.3	144.2	
			9.94	151.61	
	1.43	153.04			
46			5.6	147.4	
30' Lt.			+9.6	162.6	
50"			+23.1	176.1	$\frac{S.S.}{40}$
60' Rt.			17.0	136.0	
47			12.3	140.7	
50' Lt.			3.2	149.8	$\frac{S.S.}{30}$
60' Rt.			21.4	131.6	
+40			8.8	144.2	
30' Lt.			+39	156.9	$\frac{S.S.}{30}$
50' Rt.			20.7	132.3	

Sta.	+	H.I.	-	El.	
		153.04			
48			10.0	143.0	SS. 30
30' Lt.			+8.4	161.4	
50' Rt.			75.0	128.0	
+90°			17.0	136.0	
30' Lt.			+2.0	155.0	SS. 50
35' Rt.			34.9	118.1	
63' "			38.8	114.2	Edge Wash
T.P.			12.41	140.63	Hub on E 48+60
	1.06	141.69			
			12.59	129.10	
	1.04	130.14			
50			16.4	113.7	
21' Lt.			9.4	120.7	
57' "			+10.4	140.5	SS. 20
10' Rt.			18.8	111.3	
50' "			21.0	109.1	SS. 100
			12.52	117.62	
	0.45	118.07			
51			12.5	105.6	
30' Lt.			10.6	107.5	
55' "			0.0	118.1	
50' Rt.			13.8	104.3	SS. 30

Sta.	+	H.I.	-	El.	
		118.07			
52			16.0	102.1	
50' Lt.			9.4	108.7	
50' Rt.			19.0	99.1	SS. 50
			12.47	105.60	
	0.48	106.08			
53			11.0	95.1	
18' Lt.			8.8	97.3	
47' "			+6.8	112.9	
69' "			+16.9	123.0	
50' Rt.			12.1	94.0	SS. 50
			12.52	93.56	
	0.18	93.74			
54			4.1	89.6	
30' Lt.			0.5	93.2	
55' "			+13.0	106.7	SS. 20
50' Rt.			4.7	89.0	
55			6.3	87.4	
55' Lt.			0.5	93.2	
50' Rt.			8.3	85.4	SS. 50 more
56			10.2	83.5	
18' Lt.			7.0	86.7	
70' "			+6.3	100.0	
50' Rt.			11.6	82.1	SS. 50

Sta.	+	H.I.	-	ΣI.	
		93.74			
	0.50	88.12	6.12	87.62	
56+52			2.5	85.6	
32' Lt.			+15.2	103.3	<u>SS</u> 30
20' R.			8.0	80.1	
26 "			16.0	72.1	
32 "			8.0	80.1	
50 "			8.4	79.7	<u>SS</u> 30
57+50			+2.2	90.3	
22' Lt.			+16.3	104.4	<u>SS</u> 30
23' R.			11.0	77.1	
49 "			15.5	72.6	
58 "			31.8	56.3	Wash
67 "			14.5	73.6	<u>Level</u> 100'
58+10			8.0	80.1	
28' Lt.			0.0	88.1	
60 "			+13.0	101.1	
34' R.			16.6	71.5	
A6 "			32.2	55.9	Wash
69 "			16.6	71.5	<u>Level</u> 150'

Sta.	+	H.I.	-	ΣI.	
		88.12			
58+75			7.8	80.3	
22' Lt.			+7.8	95.9	
39' "			+17.7	105.8	<u>SS</u> 30
4' R.			8.6	79.5	
25' "			33.0	55.1	
35' "			33.0	55.1	
A8			20.2	67.9	<u>Level</u> 200'
			7.76	80.36	
	1.61	81.97			
59+37			9.5	72.5	
28' Lt.			+3.9	85.9	
55 "			+18.6	100.6	<u>SS</u> 30
32' R.			15.0	67.0	
47 "			28.5	53.5	
62 "			15.1	66.9	<u>Level</u> 150'
BM			0.69	81.28	On P.I. Hub Sta 60+04.72
60+04.72			0.7	81.3	
34' Lt.			+13.0	95.0	<u>SS</u> 100'
40' R.			17.3	64.7	
88 "			19.2	62.8	Edge Wash

Sta	+	HI	-	El.
		81.97		
61			5.0	77.0
35 Lt.			+14.0	96.0
40 Rt.			22.4	59.6
140 "			27.0	55.0
			12.03	69.94
	2.32	72.26		
+67 <sup>20</sup>			+5.5	77.8
20 Lt.			+17.0	89.3
59 Rt.			16.6	55.7
160 "			22.1	50.2
62+50			+28	75.1
30 Lt.			+16.0	88.3
63 Rt.			22.1	50.2
113 "			26.0	46.3
BM			2.54	69.72
	1.42	71.14		
+80			+1.7	72.8
37 Lt.			+14.8	85.9
66 Rt.			21.1	50.0
116 "			25.9	45.2

On Pt. Hub  
Sta 63+57.3

Level  
stop  
5.0

Sta	+	HI	-	El.
		71.14		
63+26			0.9	70.2
60 Lt.			+10.6	81.7
47 Rt.			7.2	63.9
84 "			16.5	54.6
103 "			25.7	45.4
+57 <sup>30</sup>			1.4	69.7
45 Rt.			3.9	67.2
83 "			9.3	61.8
102 "			13.0	58.1
64			8.0	63.1
18 Lt.			6.8	64.3
60 "			+4.4	75.5
86 "			+13.7	84.8
116 "			+26.0	97.1
18 Rt.			10.6	60.5
76 "			26.0	45.1
			12.28	58.86
	0.34	59.20		
	0.19	46.95		
			12.44	46.76

SS  
30

Sta	+	H.I.	-	El.		+	H.I.	-	El.
		46.95					24.86		
64+83			17.3	29.6		11.35	34.76	1.45	23.41
40 Lt.			29	44.0		11.37	45.96	0.17	34.59
68 "			+10.0	56.9	$\frac{SS}{60}$	11.90	57.18	0.68	45.28
26 Rt.			19.2	27.7		12.57	68.95	0.80	56.38
75 "			18.5	28.4	$\frac{SS}{100}$	4.80	72.99	0.76	68.19
			12.57	34.38				3.25	69.74
	0.75	35.13							69.72
65+50			10.5	24.6		12.99	85.50	0.48	72.51
45 Lt.			10.8	24.3				4.20	81.30
78 "			+2.0	37.1		6.50	87.78		81.28
40 Rt.			10.3	24.8	$\frac{SS}{100}$	12.21	96.73	3.26	84.52
						12.09	108.48	0.34	96.39
66			12.3	22.8		11.17	119.25	0.40	108.08
			11.02	24.11		12.12	131.14	0.23	119.02
	0.75	24.86				11.98	142.88	0.24	130.90
67			5.5	19.4				2.24	140.64
									140.63
68			7.7	17.2		11.31	153.64	0.55	142.33
40 Lt.			7.6	17.3		10.90	164.03	0.51	153.13
40 Rt.			7.9	17.0	$\frac{SS}{100}$ $\frac{SS}{100}$			4.24	159.79
									159.78
69			8.3	16.6		12.37	172.16		
						11.60	183.58	0.18	171.98
70			8.3	16.6		12.96	196.43	0.11	183.47
						12.66	208.89	0.20	196.23
								3.64	205.25
									205.24

B.M. - Sec Pg 10

B.M. - Pg 9

Old T.P. - Pg 8

B.M. - Pg 6

B.M. - Pg 5

	+	Hl.	-	E.l.	
		208.89			
	12.90	221.48	0.31	208.58	
	12.85	234.33	0.00	221.48	
	12.36	246.48	0.21	234.12	
	12.73	258.87	0.34	246.14	
	12.64	271.21	0.30	258.57	
	12.53	283.14	0.60	270.61	
	11.68	294.64	0.18	282.96	
	12.86	307.30	0.20	294.44	
	12.34	319.18	0.16	306.84	
	12.19	331.14	0.23	318.95	
	12.85	343.80	0.19	330.95	
	12.55	355.69	0.66	343.14	
	8.40	363.37	0.72	354.97	
BM-Pg. 3			4.07	359.30	359.26
	3.14	359.51	7.00	356.37	
	7.20	359.49	7.22	352.29	
	10.74	368.69	1.54	357.95	
	9.73	378.17	0.25	368.44	
BM-Pg. 2	12.07	388.10	2.01	376.11	376.03
	11.75	398.29	1.56	386.54	
	12.28	408.13	2.44	395.85	
	11.87	417.97	2.03	406.10	
BM-Pg. 1			1.01	416.96	416.91

INDEXED

WK  
FEB 15 1949

SOLEDAD VALLEY ROAD-

Profile and Topography

"B" LINE

(Sorrento Canyon)

Marine Camp to Sorrento School-

May 1929

Coote

Osborne

Wilbourne

Pammen

Alignment notes in F.B.# 1339



	+	HI.	-	El.					
B.M.	7.21	402.20		394.99	See Pg. 1	↖ 13R			
	5.40	404.44	3.16	399.04		40'			
	0.64	393.63	12.45	392.99	Error - 1' too high		114	368.89	9.37
	0.59	383.67	10.55	383.08					
B.M.			10.24	373.43	On Base of El Camino Real Sign at SW Corner of intersection -	3			
						13' Lt			5.9
						26 "			6.8
						40 "			3.0
	1.69	378.12				70 Rt			2.4
0+00			5.0	369.1		23 "			6.4
8' Lt			5.2	368.9		40 "			5.2
10 "			4.0	370.1					4.9
40 "			2.2	371.9					9.8
40 Rt			7.1	367.0		4			5.7
						23 Lt			1.3
0+60 ±			4.3	369.8		40 "			11.0
0-200 "			2.8	371.3		8' Rt			16.6
0-300 "			2.2	371.9		18 "			17.8
						52 "			12.68
			6.0	368.1			189	356.10	3
									1.4
↖			8.8	365.3					14
24 Lt			9.2	364.9		20 Lt			+0.1
30 "			8.0	366.1		40 "			+0.9
40 "			8.0	366.1		20 Rt			3A
10' Rt			9.9	364.2		40 "			5.6

INDEXED  
WK

FEB 15 1949

S.S.  
40

Same Slope  
40

S.S.  
40

S.S.  
50

S.S.  
20

Sta	+	HI. 346.10	-	El.		Sta.	+	HI. 347.79	-	El.	
5+70 ±			7.1	349.0		732, 19' R. 56.			10.7	336.1	
6			13.2	341.9					15.9	330.9	-90° to R.
15' Lt.			10.5	344.6			0.30	<sup>4</sup> 337.75	12.34	<sup>4</sup> 337.45	
40 "			7.5	347.6	$\frac{SS.}{100}$						
41' Rt.			19.7	335.4	$\frac{SS.}{50}$	475			14.4	320.4	
+12			8.9	346.2		8			16.3	318.5	
BM			9.29	346.81	on P.I. # 103 6+52.7	47' Lt. 18' Rt.			11.0	323.8	$\frac{SS.}{40}$
+52.70			9.3	345.8		+50			12.7	322.1	
30' Lt.			10.8	344.3		61' Lt.			3.0	331.8	
50 "			13.3	341.8	then up ss.	31' Rt.			17.7	317.1	
35' Rt.			12.2	342.9		43 "			20.4	314.4	
62 "			22.8	332.3		66 "			25.6	309.2	
	0.98	<sup>6</sup> 347.79	9.29	346.81		9			+0.8	335.6	
+90			3.8	343.0		15' Lt.			+5.4	340.2	
732			10.8	336.0		49 "			+9.0	333.8	Level $\frac{50}{20}$
30' Lt.			14.1	332.7		21' Rt.			6.5	328.3	
55 "			18.0	328.8	Level $\frac{25}{25}$	41 "			15.8	319.0	$\frac{SS.}{20}$

Sta.	+	H.I.	-	El.		Sta.	+	H.I.	-	El.	
		332.75						319.31			
9+13 <sup>28</sup>			12	333.6		11+13			21.7	296.6	
44' Lt			+3.1	337.9	$\frac{S.S.}{100}$	30' Lt			10.6	307.7	$\frac{S.S.}{50}$
20' Rt			5.0	329.8		31' Rt			28.0	290.3	$\frac{S.S.}{20}$
31' "			8.4	326.4							
52' "			17.7	317.1	$\frac{S.S.}{20}$	BM	0.48	318.53	6.26	312.05	on PI + 0.5 Sta. 11+81.25
	0.92	332.71	4.96	330.79		11+60			2.9	309.6	
						+81 <sup>25</sup>			0.5	312.0	
10+16			4.9	325.8		29' Lt			+6.4	318.9	$\frac{S.S.}{100}$
22' Lt			5.8	324.9	$\frac{S.S.}{100}$	24' Rt			6.7	305.8	
17' Rt			6.6	324.1		54' "			17.4	295.1	$\frac{S.S.}{20}$
34' "			12.0	318.7	$\frac{S.S.}{25}$						
	0.47	319.31	12.87	318.84		12+17			7.8	304.7	
+75			15.6	302.7		+6A			22.2	290.3	
30' Lt			15.3	303.0	#Draw	41' Lt			13.0	299.5	
72' "			7.8	310.5		66' "			6.6	305.9	$\frac{S.S.}{50}$
94' "			1.3	317.0		53' Rt			31.0	281.5	$\frac{S.S.}{15}$
108' Rt			16.0	302.3							
60' "			21.3	297.0		13			10.3	302.2	
						57' Lt			8.3	304.2	
11			22.0	296.3	#Draw	BM	0.38	309.67	4.24	309.29	on PI + 0.5 Sta. 13+46.22

Sta	+	H <sub>2</sub>	-	El.		Sta	+	H <sub>1</sub>	-	El.	
		309.67						302.15			
13+46.22			0.4	308.3		15			+5.1	306.3	
26 Lt.			+6.3	315.0		41 Lt.			11.5	289.7	Level 30
54 "			+10.8	319.5	SS 30						
28 Rt.			7.9	300.8		+23.13			+6.6	307.8	
55 "			18.4	290.3	SS 30	14 Lt.			+10.4	311.6	
						48 "			+15.8	317.0	SS 30
+84			7.3	301.4		34 Rt.			4.2	297.0	
33 Lt.			1.3	307.4		49 "			12.3	288.9	SS 20
34 Rt.			15.6	293.1							
	5.10	302.15	12.62	297.05		+81			1.1	300.1	
						23 Rt.			13.0	288.2	SS 30
14			6.4	294.8		16+27			11.2	290.0	
						18 Lt.			3.0	298.2	
+36			13.3	287.9		45 "			+10.0	311.2	SS 20
44 Lt.			5.8	295.4							
61 "			0.0	301.2	SS 30						
10 Rt.			15.5	285.7		3.12	302.83		12.44	289.71	
56 "			22.0	279.2	SS 30						
						17+21			7.3	284.5	
+78 ±			1.0	300.2		35 Lt.			+10.1	301.9	
32 Rt. ✓			5.6	295.6		65 "			+18.4	310.2	
43 "			8.0	293.2		19 Rt.			18.0	273.8	SS 25
66 "			11.3	284.9	SS 25						

Sta.	+	HI	-	ΣI.		Sta.	+	HI	-	ΣI	18
		297.83						288.13			
17+79			13.9	277.9		19+41.37			1.9	285.2	
5' Lt.			5.2	286.6	$\frac{S.S.}{100}$	35' Lt.			+8.0	295.1	$\frac{S.S.}{100}$
18 Rt.			18.4	273.4		23' Rt.			10.5	276.6	
46.			32.5	259.3	At Fence	49'.			26.3	260.8	$\frac{S.S.}{20}$
18+15			28.1	263.7		20			12.1	275.0	
70' Lt.			26.0	265.8		21' Lt.			0.0	287.1	
44 Rt.			38.8	253.0		55.			+13.0	300.1	$\frac{S.S.}{50}$
50			43.7	248.1	$\frac{Level Road}{15}$	31' Rt.			26.0	261.1	$\frac{S.S.}{20}$
139			34.4	257.4		BM	2.01	288.27	1.87	286.26	on P.I. Hub Sta 19+41.37
55' Lt.			27.0	264.8	$\frac{S.S.}{30}$	+23			13.4	273.9	
45' Rt.			39.3	252.5							
+74			28.3	263.5		0.46		276.42	12.31	274.96	
	7.89	288.13	12.59	280.24		+50			6.0	269.4	
19+15			6.5	280.6		37' L			+9.0	284.4	
55' Lt.			+3.2	290.3	$\frac{S.S.}{100}$	70' L			+21.0	296.4	$\frac{S.S.}{20}$
13' Rt.			11.2	275.9		12' R.			11.7	264.7	
						36' R			25.2	250.2	$\frac{S.S.}{70}$
						+88			19.3	256.1	
						42' L			0.0	275.4	

Sta.	+	H.I.	-	El.		Sta.	+	H.I.	-	El.	
		<sup>5</sup> 276.42						<sup>4</sup> 268.01			
64 L			+13	288.4	$\frac{55}{20}$	23+54			12.6	251.4	
31 R			30.2	245.2		22 L			+3.6	267.6	
51 R			39.0	236.4		47 "			+17.0	281.0	
						82 "			24.0	240.0	
21+19			20.3	250.1		T.P.	0.28	257.72	12.57	237.44	
49 LF			+5.3	280.7		24+15			7.4	244.3	
65 L			+13.0	288.4	$\frac{55}{20}$	32 L			+6.5	258.4	
T.P.	0.86	<sup>4</sup> 268.01	12.27	264.15	$\frac{3}{20}$	50 L			+8.8	260.5	$\frac{35}{40}$
						26 R			21.4	230.3	$\frac{35}{35}$
22+00			7.1	256.9							
34 L			+10.0	274.0		+50			17.0	234.7	
55 "			+18.9	282.9	$\frac{55}{50}$	16 L			13.1	238.6	
29 R			21.4	242.6		47 "			12.2	239.5	$\frac{55}{50}$
57 R			32.0	238.0		43 R			33.0	218.7	
60 "			42.6	216.4	10' Level Road						
						B.M.			10.70	242.02	ON P.O. Hub Sta. 26+05
+62			6.5	257.5		T.P.	0.27	<sup>39</sup> 240.34	12.65	240.07	
26 L			+9.8	273.8							
56 "			+24.0	288.0	$\frac{55}{20}$	25+15			39.0	200.3	
26 R			22.0	247.0		47 LF			32.2	207.1	
50 "			38.3	245.7		108 "			26.0	213.3	+ Draw
60 "			48.3	215.7	15' Level Road	51 R			41.2	198.1	Level to Rd

Sta	+	H	-	El.	
		210.34			
25+62			10.3	229.0	
30' Lt			3.3	236.0	$\frac{SS}{10}$
Rt			17.9	221.4	$\frac{SS}{25}$
26+05			+1.8	241.1	
43' Lt			+13.0	252.3	
63'			+16.0	255.3	$\frac{SS}{40}$
35' Rt			13.0	226.3	$\frac{SS}{35}$
+74			4.4	234.9	
46' Lt			+9.0	248.3	$\frac{SS}{40}$
41' Rt			20.8	218.5	$\frac{SS}{40}$
	0.49	228.45	12.38	227.96	
27+25			12.7	214.8	
37' Lt			+1.4	228.9	
54'			+13.0	240.5	$\frac{SS}{100}$
15' Rt			23.6	203.9	$\frac{SS}{20}$
+50			4.1	223.4	
40' Lt			+12.3	239.8	$\frac{SS}{40}$
26' Rt			13.0	214.5	$\frac{SS}{30}$

Sta	+	H	-	El.	
		228.45			
27+90 <sup>20</sup>			5.5	228.0	
27' Lt			+9.4	236.9	
19'			+2.1	248.6	
82'			+28.4	255.9	
27' Rt			17.3	210.2	$\frac{SS}{40}$
BM			3.74	224.71	3 ew pot Hub Sta. 28+85.78
	0.44	228.15			
28+85.78			0.4	223.8	
27' Lt			+13.0	237.2	$\frac{SS}{50}$
18' Rt			13.0	211.2	
39'			23.6	200.6	$\frac{SS}{20}$
29+43			12.7	214.5	
+75			11.4	212.8	
23' Lt			+2.8	227.0	$\frac{SS}{75}$
20' Rt			23.0	201.2	
46'			33.3	190.9	$\frac{SS \text{ Vert}}{10-15}$
	3.95	216.70	12.40	214.75	

Sta.	+	H <sub>1</sub>	-	ΣI.	
		216.70			
30+27			18.4	197.3	
36' Lt.			11.0	204.7	$\frac{S.S.}{100}$
48' Rt.			31.4	184.3	$\frac{S.S. - 90^\circ \pm Rd.}{8 \quad 28 \quad 15}$
t60			36.0	179.7	
50' Lt.			30.0	185.7	$\frac{S.S.}{100}$
48' Rt.			43.4	172.3	$\frac{Level}{30}$
31			13.1	202.6	
35' Lt.			9.0	206.7	$\frac{S.S.}{100}$
51' Rt.			27.0	188.7	$\frac{S.S. - 90^\circ \pm Rd.}{10 \quad 15}$
BM			1.36	217.31	on Pt. Hub Sta 31+39.90
31+39.90			1.4	214.3	
25' Lt.			+9.0	224.7	
59.			+17.8	243.5	$\frac{S.S.}{30}$
44' Rt.			22.0	193.7	$\frac{S.S.}{15}$
			12.79	208.91	
0.37		<sup>3</sup> 204.28			

Sta.	+	H <sub>2</sub>	-	ΣI.	
		204.28			
32+23			9.0	194.3	
17' Lt.			0.0	203.3	
39 "			+13.0	216.3	$\frac{S.S.}{50}$
11' Rt.			14.0	189.3	
28 "			26.3	177.0	
48 "			36.0	167.3	$\frac{Level}{15} Road$
33			9.5	193.8	
16' Lt.			0.0	203.3	
39 "			+13.0	216.3	$\frac{S.S.}{75}$
22' Rt.			22.7	180.6	
35 "			28.4	174.9	$\frac{-90^\circ Level}{10 \quad 16}$
T.P.	7.81	<sup>8</sup> 199.73	12.36	191.92	on Hub 5' Pt. Sta 33+50
34			11.3	187.4	
23' L			+6.5	205.2	
56 "			+26.0	224.7	$\frac{S.S.}{40}$
28 R			30.0	168.7	
33 "			36.6	167.1	15' Level Road.
34+67			+1.7	200.4	
50' L			+20.0	218.7	



Sta.	+	H.I.	-	EL.
		19 <sup>8</sup> 8.73		
68' L			+26.0	224.7
30' R			9.0	189.7
65' "			25.2	173.5
68' "			38.0	160.7
35+00			9.6	189.1
34' L			0.0	198.7
55' R			26.0	172.7
35+50			+2.3	201.0
40' L			+15.6	214.3
70' "			+26.0	224.7
51' R			16.8	181.9
83' "			26.0	171.7
35+74			+2.2	200.9
T.P.	1.47	19 <sup>8</sup> 2.32	8.88	190.85
36+00			+6.0	197.3
35' L			+21.7	213.0
60' "			+30.7	222.0
40' R			13.0	178.3
36+50			8.4	182.9

Sta.	+	H.I.	-	EL.
		19 <sup>8</sup> 2.32		
T.P.	1.42	18 <sup>8</sup> 8.31	12.43	179.89
37+13			15.1	165.2
25' L			1.7	178.6
50' "			+13.0	193.3
40' R.			32.0	148.3
37+85			7.8	172.5
25' L			+5.6	185.9
55' "			+16.7	197.0
18' R			19.2	161.1
38' "			30.6	149.7
44' "			34.6	145.7
38+45			10.1	170.2
25' L			4.7	165.6
65' "			2.0	178.3
31' R			17.0	163.3
55' "			25.5	154.8
63' "			35.7	144.6
T.P.			12.68	168.63
	0.25	16 <sup>7</sup> 8.88		

Sta	+	III	-	El.		Sta	+	III	-	El.
		168.88						158.53		
39			116	157.3		40+77 <sup>20</sup>			+5.8	163.3
55' Lt.			12.5	155.4	S.S. 50	20' Lt.			+13.0	170.5
26' Rt.			12.6	155.3		43' Rt.			13.7	143.8
69' "			19.1	148.8		65' "			17.4	140.1
72' "			25.4	142.5	Level 20					Level 50
	2.28	158.53	12.63	156.25		41			0.2	157.3
+50			9.0	148.5		+50			6.3	151.2
29' Lt.			11.2	146.3	Level 15	30' Lt.			+0.3	157.8
65' Rt.			11.7	146.8		20' Rt.			9.7	147.8
						39' "			19.6	137.9
40			14.3	143.2		BM			6.18	158.35
14' Lt.			12.8	144.7						In Phone Pole 5' Lt. 41+55
40' "			4.0	153.5		42+36			15.7	141.8
65' Rt.			13.0	144.5		40' Lt.			7.6	149.9
67' "			17.0	140.5	Level 20	8' Rt.			17.2	140.3
+25			10.0	147.5		15' "			20.9	136.6
+63			+5.2	162.7		50' "			21.0	136.5
										Level 20
									12.98	148.55
							3.77	149.32		

Sta	+	HI	-	El.
		148.32		
43			7.0	141.3
33 Lt			+10.5	151.8
55.			+26.0	174.3
7 Rt			9.8	138.5
13.			14.0	134.3
52			12.2	136.1

SS.  
50SS.  
30

44			+1.3	149.6
29 Lt			+13.0	161.3
61.			+26.0	174.3
26 Rt			8.2	140.1
30.			14.8	133.5
58.			15.0	133.3

SS.  
20

+72			9.8	138.5
79 Lt			1.9	136.4
29 Rt			13.7	134.6
33.			15.4	132.9

Level  
151.42  
7  
138.9911.75  
6  
137.57

Sta	+	HI	-	El.
		138.99		
45+37			3.0	135.0
47 Lt			+3.8	141.8
80.			+13.0	151.0
12 Rt			4.7	133.3
14.			7.4	130.6
31.			6.5	131.5

SS.  
20SS.  
50

46+07.50			9.4	128.6
16 Lt			9.8	128.2
19.			6.5	131.5
95.			+12.0	150.0
20 Rt			8.5	129.5

SS.  
30

BM

9.35  
8  
129.64  
on P.I. + 0.6  
Sta 46+07.50

47+16.90			11.0	127.0
18 Lt			12.0	126.0
21.			9.3	128.7
90.			+6.2	144.2
40 Rt			11.0	127.0
50.			9.0	129.0

8.11  
3  
138.52  
12.58  
5  
128.41

Sta	+	H <sub>3</sub> 134.52	-	ΣI.		Sta	+	H <sub>3</sub> 134.52	-	ΣI.	
48			8.4	125.1		50, 5' Rf			12.4	121.1	
8' Lt			8.7	124.8		10' "			18.7	114.8	
10'			6.9	126.6		17' "			13.1	120.4	
25'			4.9	128.6		50'			7.1	126.4	
23' Rf			8.5	125.0	Edge Ditch	76'			0.0	133.5	$\frac{SS.}{50}$
35'			15.0	118.5							
40'			6.3	127.2		51			13.4	120.1	
58'			0.0	133.5		5' Lt			13.4	120.1	
66'			17.5	141.0	$\frac{SS.}{50}$	6' "			9.8	123.7	
						26' "			0.0	133.5	$\frac{SS.}{100}$
49			10.3	123.2		15' Rf			13.3	120.2	
5' Lt			10.5	123.0		24			21.2	112.3	
9' "			7.2	126.3		28' "			14.6	118.9	
51' "			0.0	133.5		69' "			11.7	121.8	
12' Rf			10.0	123.5		100' "			2.7	130.8	$\frac{SS.}{50}$
28' "			16.7	116.8							
35'			8.2	125.3							
60'			0.0	133.5	$\frac{SS.}{50}$				8.20	129.68	
									130.4	121.48	
50			12.5	121.0		52+48'			11.8	116.9	
10' Lt			12.6	120.9		18' Lt			12.5	116.2	
18'			8.8	124.7		20' "			10.6	118.1	
33'			6.4	127.1		42' "			5.6	123.1	
49'			1.7	131.8	$\frac{SS.}{50}$	55' "			0.0	128.7	$\frac{SS.}{50}$
						20' Rf			12.3	116.4	$\frac{SS.}{50}$

Sta	+	HI	-	ΣI		Sta	+	HI	-	ΣI
		129.68						128.85		
54			10.6	118.1		57	19.5	112.91	12.89	109.96
30 Lt.			+3.4	132.1					2.6	108.3
47 "			+13.0	141.7	$\frac{S.S.}{100}$	30 Lt.			+2.4	113.3
11 Rt.			13.3	115.4		60 Rt.			2.6	108.3
15 "			16.3	112.4						
47 "			15.2	113.5	Edge Ditch	58			4.4	106.5
B.M.			9.22	119.46	On P.O.T. Hub Sta. 54+53.55	59			7.0	103.9
	2.39	127.85				60			9.8	102.1
55			3.6	118.3		25 Lt.			7.0	103.9
33 Lt.			+13.0	134.9	$\frac{S.S.}{75}$	46 "			0.0	110.9
14 Rt.			11.4	110.5		30 Rt.			9.8	101.1
54 "			10.9	111.0	$\frac{S.S.}{50}$					$\frac{S.S.}{60}$
56			12.6	109.3		61			10.1	100.8
15 Lt.			10.5	111.4						
39 "			0.0	121.9		3.08	103.88	10.11	100.	101.80
64 "			+13.0	134.9						
21 Rt.			13.4	108.5		62			4.3	99.6
25 "			20.4	101.5	Edge Ditch	63			5.2	98.7
35 "			14.5	107.4		20 Rt.			5.1	98.8
52 "			11.5	110.4		110'			8.7	95.2
71 "			10.0	111.9	$\frac{S.S.}{40}$					

Sta.	+	H	-	EI		Sta.	+	H	-	EI
65+15 <sup>LS</sup>		104.88				72		87.72		
94Rt			+0.2	104.1					4.3	82.4
100 "			4.9	99.0		73			6.6	80.1
150 "			6.5	97.4		6' Lt.			6.9	79.8
			9.6	94.3	20' to ditch	12 "			2.4	84.3
	0.18	97.49	7.57	97.31		44 "			+11.0	97.7
						50 Rt.			7.5	79.2
68			+7.8	89.7		74			8.1	78.6
11' Lt.			+13.0	109.5	SS 40	75			9.5	77.2
17 Rt.			0.3	96.2						
19 "			6.8	89.7						
53 "			7.6	88.9						
58 "			16.5	80.0	+ ditch		0.60	78.56	9.76	77.96
65 "			7.6	88.9		76			2.3	75.3
100 "			8.0	88.5		10' Lt.			2.6	75.0
69			8.8	87.7	In Road	15 "			+1.0	78.6
						74 "			+5.0	82.6
70			10.6	85.9		50 Rt.			2.4	75.2
	0.93	87.72	10.70	86.79		77			5.3	74.3
						78			7.6	70.0
71			2.7	84.0		14' Lt.			2.1	75.5
						40 "			+13.0	90.6
						50 Rt.			8.0	69.6

 $\frac{5.5}{50}$



Sta	+	H	-	El		Sta	+	H	-	El	
		<sup>69</sup> 70.06						<sup>3</sup> 84.97			
92			8.3	60.8		96			5.7	78.3	
	3.85	<sup>4</sup> 68.66	8.25	61.81		40' Lt.			0.0	84.0	
						101'			+13.0	97.0	
						52' R			12.1	71.9	<u>SS.</u> 60
93			8.5	56.1							
75' Lt.			4.5	60.2	feet of hill.	+54.20			3.5	80.5	
74' R.			13.7	51.0	<u>SS.</u> 100	(+19)			0.0	84.0	
						33' Lt.			+9.3	93.3	<u>SS.</u> 50
+75			11.0	53.7		100'			10.3	73.7	
34' Lt.			5.7	59.0		56' R.			16.0	8.0	<u>SS.</u> 80
61'			0.0	64.7	<u>SS.</u> 100	86'					
76' R.			16.0	48.7	<u>SS.</u> 50	B.M.			3.52	0	at P.I. Hub
							1.04	<sup>1</sup> 84.49		84.45	96+84.30 (+19)
94			8.5	56.2							
	12.59	<sup>6</sup> 77.78	0.47	68.19		#18			5.5	76.0	
						100' Lt.			+5.1	86.6	
95			9.0	67.8		51' R.			11.7	69.8	
45' Lt.			0.0	76.8							
87'			+11.0	88.8							
80' R.			20.8	56.0	<u>SS.</u> 100		0.55	<sup>69</sup> 70.05	12.99	8	69.50
	7.43	<sup>3</sup> 84.97	0.24	77.54		#18 + 120			5.4	63.7	
						69' Lt.			0.0	69.1	
						41' R.			9.1	60.0	<u>SS.</u> 20



Sta	+	HI	-	ΣI.	
		<sup>69.</sup> <del>70.05</del>			
#18+200	0.74	58.22	12.57	57.49 ✓	
			10.5	46.7	
	0.15	<sup>4</sup> 47.67	12.70	47.52 ✓	
+300'			13.3	31.4	
80' Lt			5.7	39.0	
64' R.			20.5	24.2	$\frac{SS}{30}$
	0.99	<sup>2</sup> 37.64	13.02	37.65 ✓	BM
+400'			10.6	22.0	
+500'			12.1	20.5	
40' Lt.			11.1	21.5	$\frac{SS}{50}$
40' R.			12.4	20.2	$\frac{SS}{100}$
+600'			12.7	19.9	
	Profile slope continues same for 500' more.				
	11.96	<sup>8</sup> 39.85	5.75	27.89 ✓	
			2.76	37.09 ✓	

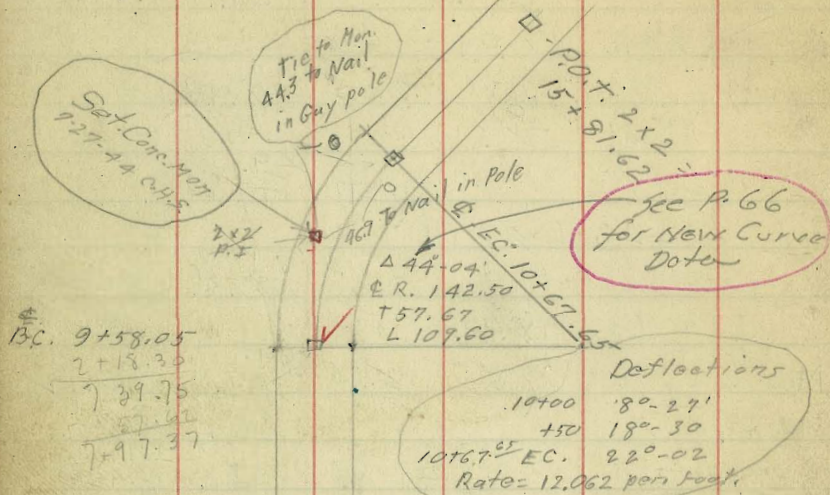
+	HI	-	ΣI.
			<sup>6</sup> 37.09 ✓
4.83	<sup>0</sup> 47.92		
		3.02	9
12.91	<sup>0</sup> 57.81		37.90 ✓
		1.27	49.
12.43	<sup>1</sup> 67.97		50.54 ✓
		0.61	67.36
10.63	<sup>1</sup> 77.99		
		2.14	<sup>69.</sup> 70.85

69.72  
Sta 63+57.32  
X-Line  
B. 10

Completed 5/18/29

Semmermeter  
Osborne  
W Moore  
Beqq

X-sec.  
Seminole Drive Ely.



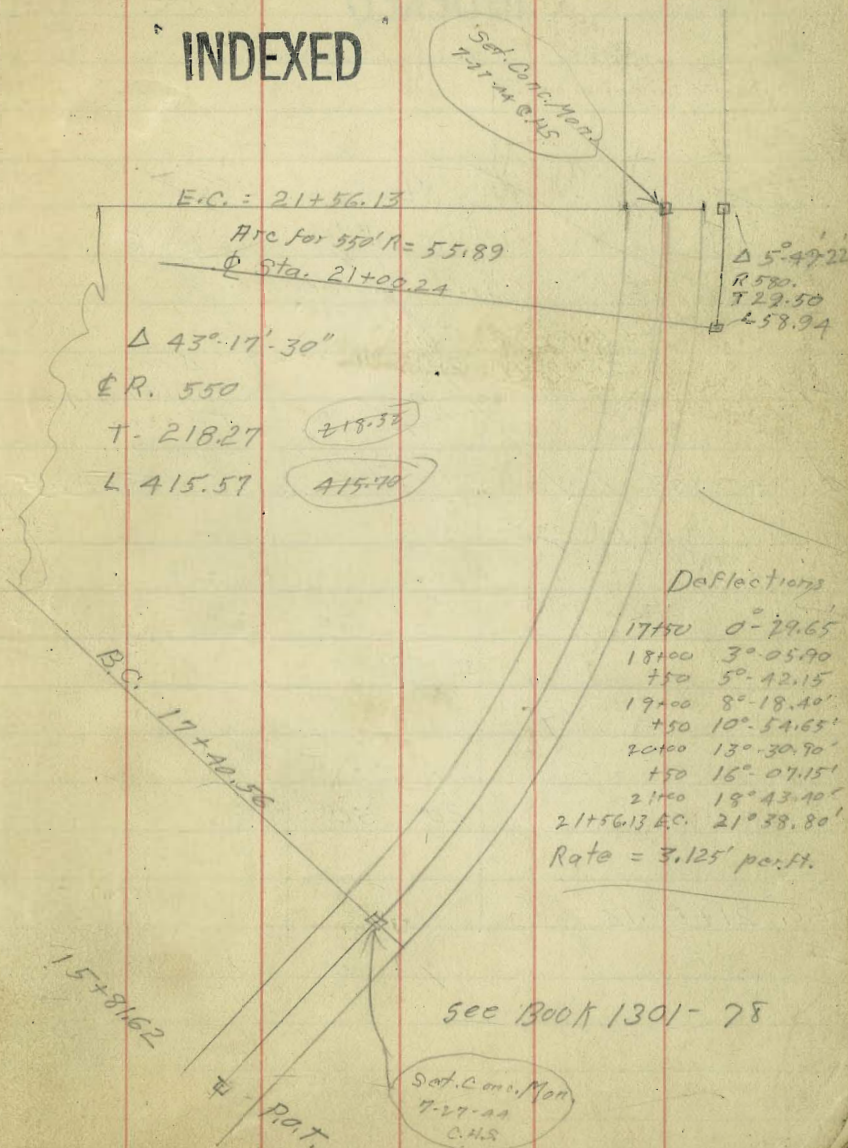
INDEXED

Reset Conc.  
Monument

This  
Alignment  
Void  
see P.66

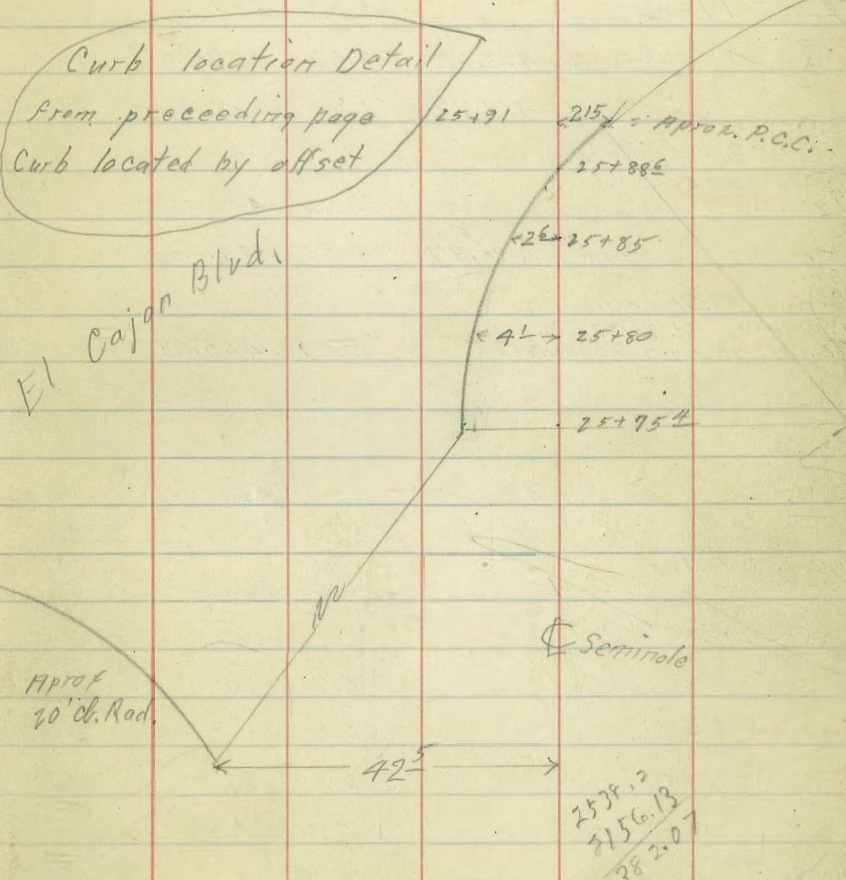
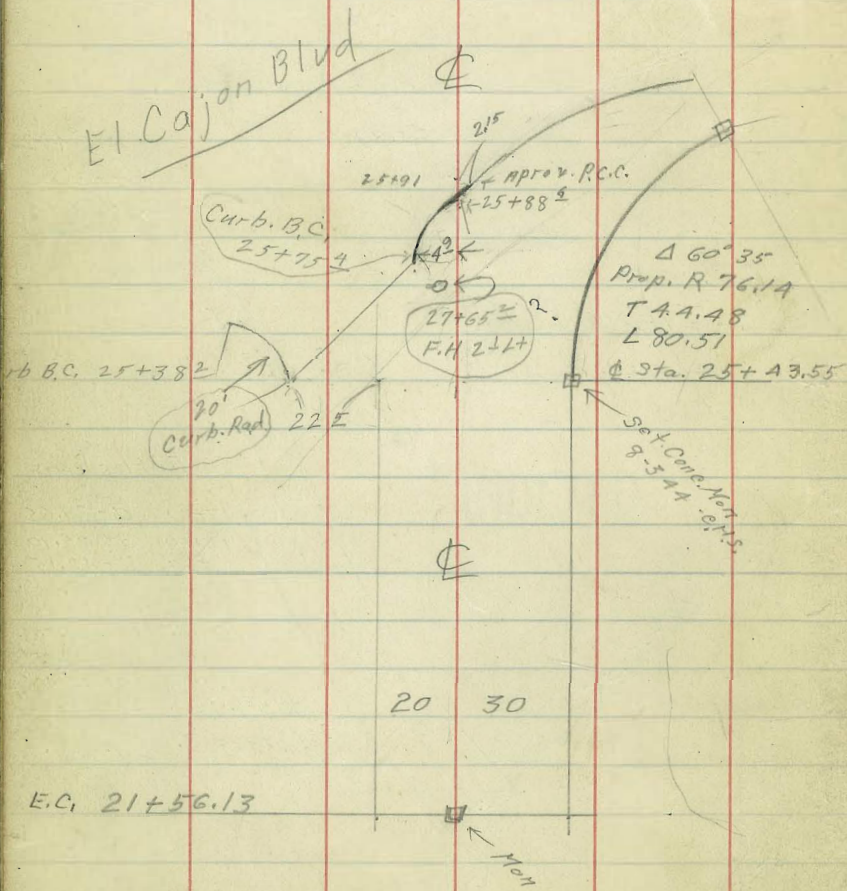
7-24-44 <sup>indexed</sup> c.s.k. 31  
End to El Cajon Blvd. Plotted TPS  
Council order Doc# 349235 2785  
2794  
2795  
4309

INDEXED



TPS-4309

INDEXED



X-Sec. Seminole Dr.  
 Ely End to El Cajon Blvd INDEXED

Sammermeyer  
 Osborne  
 W Moore  
 Beeg

4-27-44  
 33

470.79

B.M. = S.W. B.M. Rolando + El Cajon	5.63	458.09	-	452.46	✓
r.p.	7.64	464.95	0.78	457.31	✓
Set. B.M. #1 1" pipe	3.57	462.10	6.42	458.53	✓
22' RT 17+00			4.03	458.07	✓
	5.43	463.02	4.51	457.59	✓
	7.77	469.78	1.01	462.01	✓
Set. B.M. #2 spike in P. Pole P175666 18' RT 7+92			3.76	466.02	✓
	5.34	470.77	4.35	465.43	✓
Set. B.M. #3 - Spike in P. Pole 19' RT 2+183 S.E. Cor. Moore + Seminole			5.09	465.68	✓
B.M. #3 500 Moore	5.11	470.77	-	465.68	
Sly End. Seminole Dr. 0+00			6.6	464.2	
20 - Lt			6.1	464.7	
20 - Rt			6.7	464.1	
0+50 &			6.5	464.3	
20 Lt			6.3	464.5	
20 Rt			7.0	463.8	
1+00			6.5	464.3	
20 Lt			5.9	464.9	
15 Rt			7.1	463.7	
20 Rt			7.6	463.2	

Reduced A.E.B.  
Profile C.P.R.A.

1+50	6.6	464.2	
20 Lt	5.8	465.0	
20 Rt	6.8	465.6	464.0
2+00	6.1	464.7	
20 Lt	5.7	465.1	
20 Rt	6.1	464.7	
2+183 S. Line Moore	5.7	465.1	
18 Rt P. pole			
20 Rt	5.8	465.0	
18 Lt. Guy pole			
20 Lt	5.4	465.4	
2+383 & Moore	5.3	465.5	
20 Rt	5.4	465.4	
120 Rt	5.6	465.2	
2+583 N. Line Moore	5.2	465.6	
20 Lt	5.1	465.7	
20 Rt	5.3	465.5	
3+00	5.2	465.6	
20 Lt	4.9	465.9	
20 Rt	5.8	465.0	
+50	5.1	465.7	
20 Lt	4.9	465.9	
20 Rt	5.4	465.4	
3+91 - 18 Rt. - P. Pole			

## Seminole Dr.

 $\bar{x}$   
470.79

4+00	5.1	465.7
20LT	4.8	466.1
20RT	4.9	465.9
4+50	5.5	465.3
20LT	5.0	465.8
20RT	4.9	465.9
5+00	5.4	465.7
20LT	5.2	465.6
20RT	5.3	465.5
5+41 18RT P. Pole		
+50	5.3	465.5
20LT	5.6	465.2
20RT	5.4	465.4
6+00	5.5	465.3
20LT	5.6	465.2
20RT	5.0	465.8
6+50	5.5	465.3
20LT	5.8	465.1
20RT	5.0	465.8
	$\bar{x}$ 470.79	
T.P.	2.37	467.68
7+00	5.48	465.31
20LT	2.3	465.4
20RT	2.7	465.0
	1.8	465.9

 $\bar{x}$   
467.68

34

7+50	2.4	465.3
20LT	3.0	464.7
20RT	2.2	465.5
7+92- 18 <sup>2</sup> RT = P. Pole		
8+00	3.1	464.6
20LT	3.0	464.7
20RT	2.6	465.1
8+50	3.6	464.1
20LT	3.7	464.0
20RT	3.3	464.4
9+00	4.7	463.0
20LT	4.3	463.4
20RT	4.2	463.5
9+58.05 B.C.	5.9	461.8
12LT	5.9	461.8
20LT	5.1	462.6
20RT	5.5	462.2
9+73- 19 <sup>2</sup> LT = T. pole		
10+00	5.9	461.8
20LT	5.3	462.4
20RT	5.6	462.1
+50	6.5	461.2
20LT	6.3	461.4
20RT	6.3	461.4
+51- 7 <sup>2</sup> RT = P. pole		
21 <sup>2</sup> LT = Guy pole		

π  
467.68

Seminole Drive

EC.			
10+67.65		6.8	460.9
20LT		6.5	461.2
20RT		6.4	461.3
11+00		7.0	460.7
20LT		7.0	460.7
20RT		6.7	461.0
+50		7.8	459.9
20LT		8.1	459.6
20RT	467.68	7.2	460.50
T.P	1.49	461.00	8.17 459.51
12+00		2.2	458.8
20LT	W. Edge Road	2.1	458.9
30LT		0.5	460.5
20RT		1.6	458.4
+50		3.2	457.8
18LT	Edge Road	3.1	457.9
23LT		1.7	457.3
20RT		3.0	458.0
13+00		4.1	456.9
17LT		4.0	457.0
18LT		2.5	458.5
20LT		2.5	458.5
30LT		2.1	458.9
20RT		5.4	455.6
30RT		5.3	455.7

π  
461.00

35

13+06 - 20RT = P. pla		
13+50	5.4	455.6
18LT	5.1	455.6
20LT	5.0	456.0
30LT	3.2	457.8
20RT	6.6	454.4
40RT	7.1	453.9
14+00	5.3	455.7
15LT	5.2	455.8
20LT	4.8	456.2
20RT	5.9	455.1
40RT	6.4	454.6
+50	4.3	456.7
16LT	4.3	456.7
20LT	3.6	457.4
20RT	3.7	457.3
15+00	2.5	458.5
20LT	2.0	459.0
20RT	1.9	459.1
+50	1.6	459.4
20LT	1.1	459.9
20RT	1.7	459.3
15+92 - 22LT 9 trunk Eucalyptus tree 4" diam		
16+00	2.4	458.6
10LT	2.5	458.5

## Seminole Drive

π  
461.00

16100 - 20 Lt		1.4	459.6	
20 Rt		2.8	458.2	
+06 19 <sup>th</sup> Rt = Power pole				
+34 - 21 Lt = 4' Diam Euc. tree - 10 trunk clump				
16150		2.9	458.1	
10 Lt		3.2	457.8	
20 Lt		1.7	459.3	
20 R	461.00	3.0	458.0	
T.P.	5.13 463.01	3.12	457.98	
16184 - 19 Lt = 3' Eucalyptus tree				
17100		5.5	457.5	
9 Lt		5.7	457.3	
20 Lt		4.4	458.6	
20 Rt		5.5	457.5	
+A0.56 BC		6.1	456.9	
10 Lt		6.3	456.7	
20 Lt		5.2	457.8	
20 Rt		6.2	457.8	456.8
+30		6.1	457.9	456.6
10 Lt		6.4	457.6	456.6
Lt.		5.3	457.7	
Rt		6.0	457.0	
18100		6.3	456.7	
10 Lt		6.4	456.6	
20 Lt.		5.7	457.3	
20 Rt		5.9	457.1	

36

π  
463.01

18144 - 14 <sup>th</sup> Lt = P. pole				
18150	463.01	6.0	457.0	
10 Lt		6.1	456.9	
20 Lt		5.6	457.4	
20 Rt		5.4	457.6	
+96 16 Lt = 3 <sup>rd</sup> Euc. Tree				
19100		5.6	457.4	
9 Lt.		5.8	457.2	
20 Lt		4.9	457.1	
20 Rt		5.3	457.7	
+12 - 14 Lt = 2 <sup>nd</sup> Euc. Tree				
+30 - 15 Lt = 2 <sup>nd</sup> " "				
+50		4.8	458.2	
20 Lt		4.6	458.4	
20 Rt.		4.8	458.2	
+78 - 19 Lt = 3 <sup>rd</sup> Euc. tree				
+86 28 Rt = 2.0 Ribbons	π Ribbon Drive	4.1	458.9	
+87 - 15 <sup>th</sup> Lt = P. Pole				
+92 - 15 Lt = 8" Euc. Tree				
20100		1.5	458.5	
20 Lt		4.4	458.6	
20 Rt		4.3	458.7	
+44 - 18 <sup>th</sup> Lt = T. pole				
" 19 <sup>th</sup> Rt = start 3' High picket Fence				
+51		3.7	459.3	
20 Lt		3.8	459.2	

463.01

Seminole Drive

Conc.

4 Ribbon Drive

20+51	19RT	20 <sup>o</sup> Ribbons	3.23	459.78
	20RT		3.2	459.8
	+177-18 <sup>1</sup> RT	4 <sup>o</sup> Conc. Walk	2.85	460.16
21+00.24	(5C)	P.O.C	3.3	459.7
	13 <sup>1</sup> LT		3.8	459.2
	14 <sup>1</sup> LT		2.8	460.2
	20 <sup>1</sup> LT		2.8	460.2
	18 <sup>3</sup> RT	End 3' picket fence		
	30RT		2.8	460.2
	+20-19 <sup>3</sup> RT	4 3 <sup>o</sup> Conc. Walk	2.78	460.23
	+36-13 <sup>1</sup> LT	ctr. P. Pole		
	+50-18 <sup>1</sup> RT	" Guy pole		
	- 20RT	Start post + wire fence		
	" "	End Hedge on lot line		
21+56.13	EC		2.9	460.1
	20 <sup>1</sup> LT		2.7	460.3
	20RT		2.6	460.4
	30RT	463.01	2.5	460.5
	T.R	402	2.91	460.10
22+00			4.2	461.9 459.9
	20 <sup>1</sup> LT		3.6	460.5
	20RT		4.3	459.8
	30RT		4.1	460.0
+09	20 <sup>5</sup> LT	20" Luc. Tree		
+09	20 <sup>3</sup> RT	T. Pole		

464.12

37

22+28	21 <sup>3</sup> RT	End Post + Wire fence		
	+47-14 <sup>5</sup> LT	P. Pole		
	+47-20 <sup>3</sup> LT	Start 3' High Board fence		
	+50		4.2	459.9
	20 <sup>1</sup> LT		3.8	460.3
	20RT		4.4	459.7
	30RT		4.4	459.7
	+60-19 <sup>3</sup> LT	2 <sup>5</sup> Ribbons 4 <sup>o</sup> Conc. Ribbon Dr.	3.78	460.34
	+68-19 <sup>1</sup> LT	ctr. 1' ? tree		
	+80	" " 8" "		
	+85-19 <sup>5</sup> LT	4 <sup>o</sup> Conc. Walk	3.74	460.38
	+90-19 <sup>1</sup> LT	ctr. 8" ? tree		
23+00			3.8	460.3
	20 <sup>1</sup> LT		3.8	460.3
	20RT		4.0	460.1
	30RT		4.7	459.4
	+01-19 <sup>1</sup> LT	ctr 8" ? tree		
	+135-20 <sup>2</sup> LT	End board Fence		
	+137-18 <sup>2</sup> RT	T. pole		
	+50		4.1	460.0
	20 <sup>1</sup> LT		3.8	460.3
	20RT		4.4	459.7
	30RT		4.8	459.3
	+180-20 <sup>2</sup> LT	P. Pole		
	+81-29 <sup>2</sup> RT	ctr. 5 <sup>o</sup> Tile Flag Walk	4.65	459.47



Seminole Drive

464.12

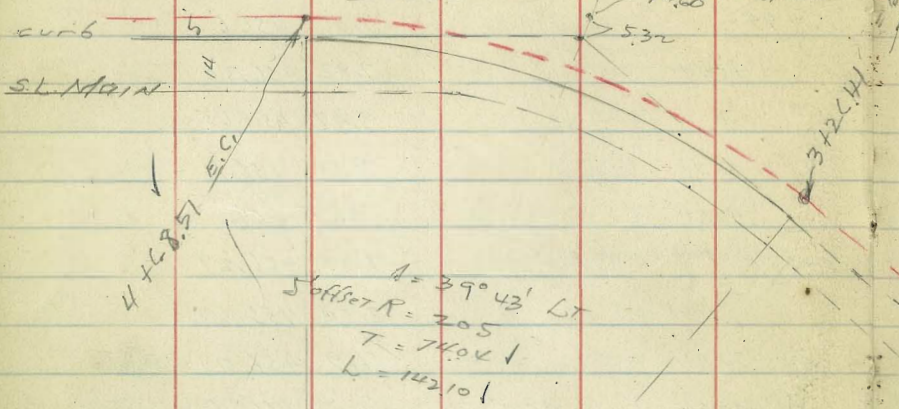
464.12

24+00	4.5	459.6
18 Lt	3.9	460.2
20 Lt	3.1	461.0
20 Rt	5.5	458.6
30 Rt	4.8	459.3
+50	5.7	458.4
20 Lt	4.9	459.2
20 Rt	6.1	458.0
30 Rt	5.7	458.4
+84 - 30 <sup>th</sup> Lt = P. Pole		
+97 - 5 <sup>th</sup> Rt = 16" Pepper tree		
25+00	6.5	459.6
20 Lt	5.9	458.2
20 Rt	7.2	456.9
30 Rt	7.5	456.6
+13 5 <sup>th</sup> Rt = T. Pole		
+38 <sup>th</sup>	7.0	457.1
20 Lt	6.7	457.4
12 <sup>th</sup> Lt = Gutter	6.8	457.3
" <sup>top</sup> Curb - Ret end.	6.21	457.91
20 Rt	8.2	457.9
30 Rt	8.4	455.7
25+43.55	7.0	457.1
20 Rt	8.0	456.1
30 Rt = Prop. B.C.	8.4	455.7

25+65 <sup>th</sup>	2 <sup>nd</sup> Lt = Ctr. Fire plug	
+75 <sup>th</sup>		7.5 456.6
	4 <sup>th</sup> Lt = End Return top curb	7.82 456.30
	Gutter	8.17 455.65
	20 Rt	8.0 456.1
	40 Rt	9.2 454.9
25+88.6	top curb Ft. Cajon	7.88 456.29
	Gutter	8.50 455.62
	20 Rt	7.9 456.2
	40 Rt	9.5 454.6
	464.12	
T.P.	5.71 458.20	11.63 452.49
original B.M.		
See page 33	at hook, etc.	5.74 452.96

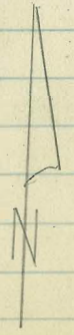
Align. and levels on  
32nd & Main St. C38C A-L

Main St. - SW. Cor.



$A = 39^{\circ} 43' LT$   
 Offset  $R = 205$   
 $T = 740.61$   
 $L = 142101$

INDEXED



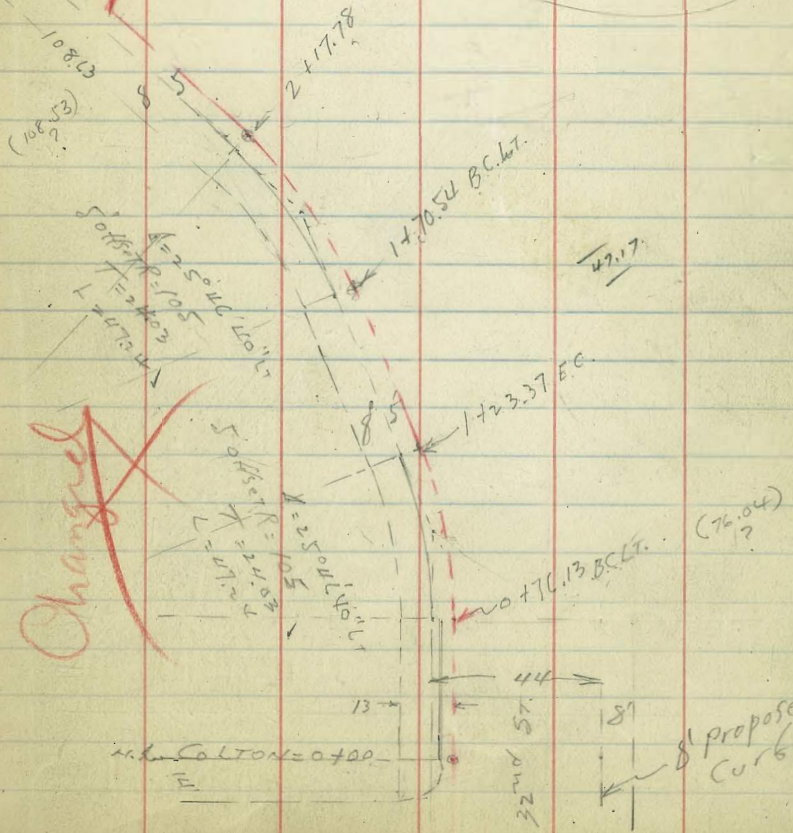
Indexed  
C.S.N.

C. Moore  
 S. Moore  
 W. Moore  
 10-13-44  
**39**

INDEXED

Proposed Curb  
 5' Offset Baseline  
 5' Offset Levels

No Levels  
 on THIS  
 under Contract



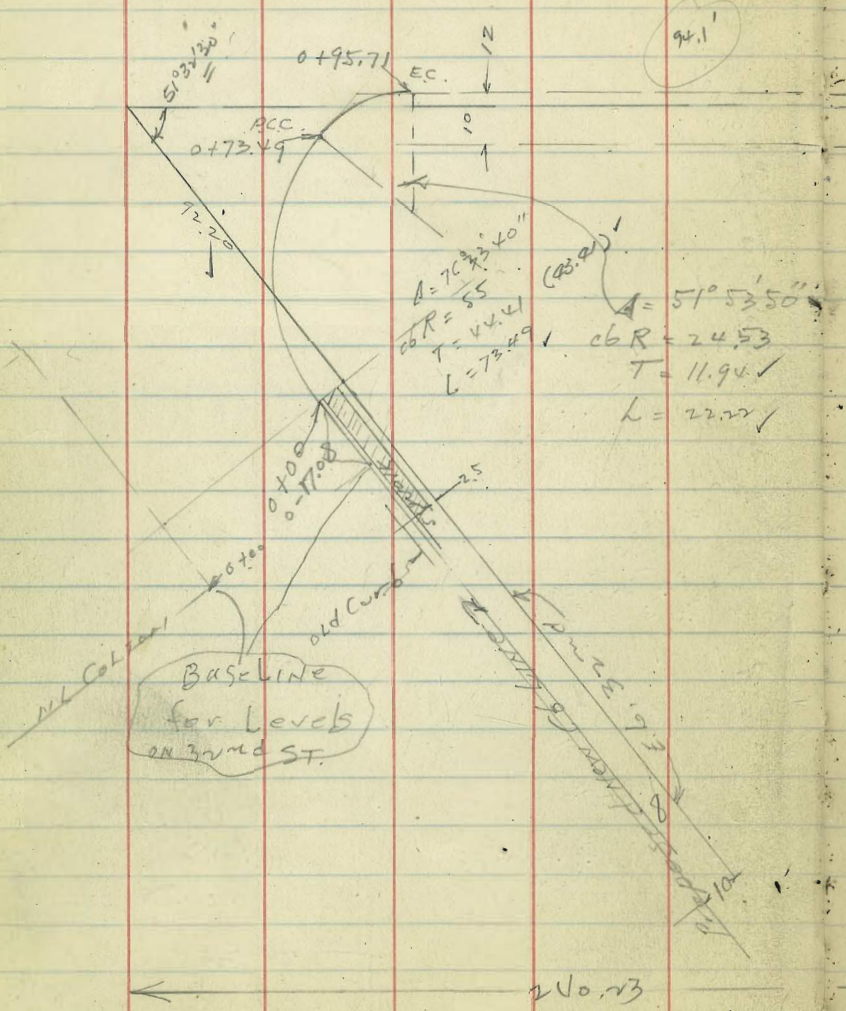
~~Change~~

Colton = 0+00

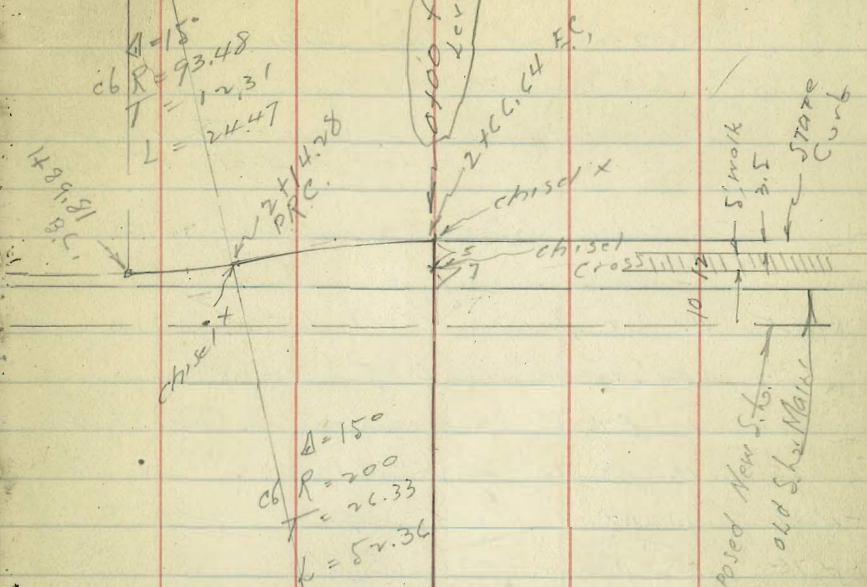
INDEXED

Proposed Curb Cutback  
S.E. Cor. 3rd + Main ST.

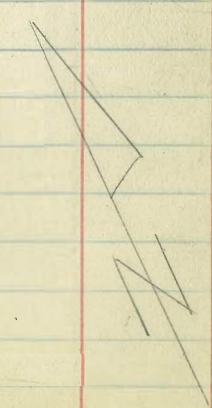
No Levels, under Contract



Indexed  
c.s.k.



INDEXED



Location of P. Poles, Signals etc

Sw Con 3rd + Main

Sketch p. 39. Location at 90° on T. and Radial on Curves.

Baseline = 5' out from proposed Curb

- 0 + 35 47 LT to CTC 16" P.P. (Transformer P.)
- 0 + 72 48 LT " " D.M. (Power Co.)
- 1 + 32 10' RT. 8" Cap over Gas Co. Elec. Control
- 1 + 35.5 11.5 RT. to CTC 16" P.P.
- 1 + 38 13 RT to Traf. Sig.
- 1 + 75 15.5 RT " CTC 16" P.P.
- 1 + 89 11.2 RT " " F. Hyd.
- 2 + 68.7 7.2 RT " " 16" P.P. (Transformer P.)
- 3 + 68 7 RT " " " "

- 00 - 13
- 0 + 49.6
- 0 + 54.9
- 0 + 66.2
- 0 + 66.6
- 0 + 67
- 1 + 89.81 B.C.

SE. Con. Location PP etc

Baseline = prop. cb Line

Location at 90° + Radial

- 1' LT to 12" Tel. Pole
- 33.5 LT Tel. Co. D.M.
- 47 LT CTC 16" Tel. Pole
- 50.8 LT 2" Iron Pipe 7' High <sup>VENT. of</sup> <sub>SAME KIND</sub>
- 50 LT CTC Traf. Sig.
- 47 LT CTC 16" P.P.
- 85 LT " " " (Transformer pole)

Levels for 3<sup>rd</sup> ST. Ex. 40' Rd. way  
 10' 1/2" Sec. at 90°

4201

SW. Cor. Main 3.42

Transfer B.M. to Ret. N.E. Co. Brass Plug Co.

38.59 2<sup>nd</sup> and Main

38.45 " "

W 9T

1/4

C

1/4

9T

E cb

5.60

5.53

5.53

5.87

6.21

5.56

36.41

36.48

36.48

36.19

35.80

36.45

0+72.13. Cb. B.C. on West

0+00 = N.L. GELTON

W cb

9T

1/4

C

1/4

9T

E cb

5.56

6.23

6.27

6.37

6.75

7.14

6.46

36.45

35.78

35.79

35.69

35.26

34.87

35.55

E cb

9T

1/4

C

1/4

9T

W cb

5.10

5.73

5.40

5.12

5.15

5.29

4.62

36.91

36.28

36.61

36.89

36.86

36.72

37.37

5.00  
4.60  
37.37

1+29.28 opp. old S.E. Cor

0+170.8 = Curb B.C. on EAST

E cb

9T

1/4

C

1/4

9T

W cb

0+50

W cb

4.16

6.85

6.41

6.06

6.02

6.01

5.37

35.85

35.16

35.60

35.95

35.99

36.00

36.64

W cb

9T

1/4

C

1/4

9T

E cb

4.23

6.85

4.63

4.54

4.81

5.13

2.47

37.78

37.16

37.38

37.59

37.20

36.88

37.54

37.49

Sec. on S.L. Main St. Cor To SW. Cor. diag.

E.L. 000

+9.8 cb

4.7

4.41

37.3

37.60

43.01

EL. + 95	9T	5.07	36.99	✓
E 1/4	25.54	4.57	37.02	✓
C	39.31	4.15	37.86	✓
W 1/4	51.08	4.12	37.89	✓
9T	25.54	4.32	37.69	✓
W c6	16.63	3.76	38.25	✓
W.L.	PIPE PIPE	3.6	38.9	

T.P. 359 3271 12.89 29.12

T.P. nail in pipe  
 8.5 Lt. of 1 + 89.81

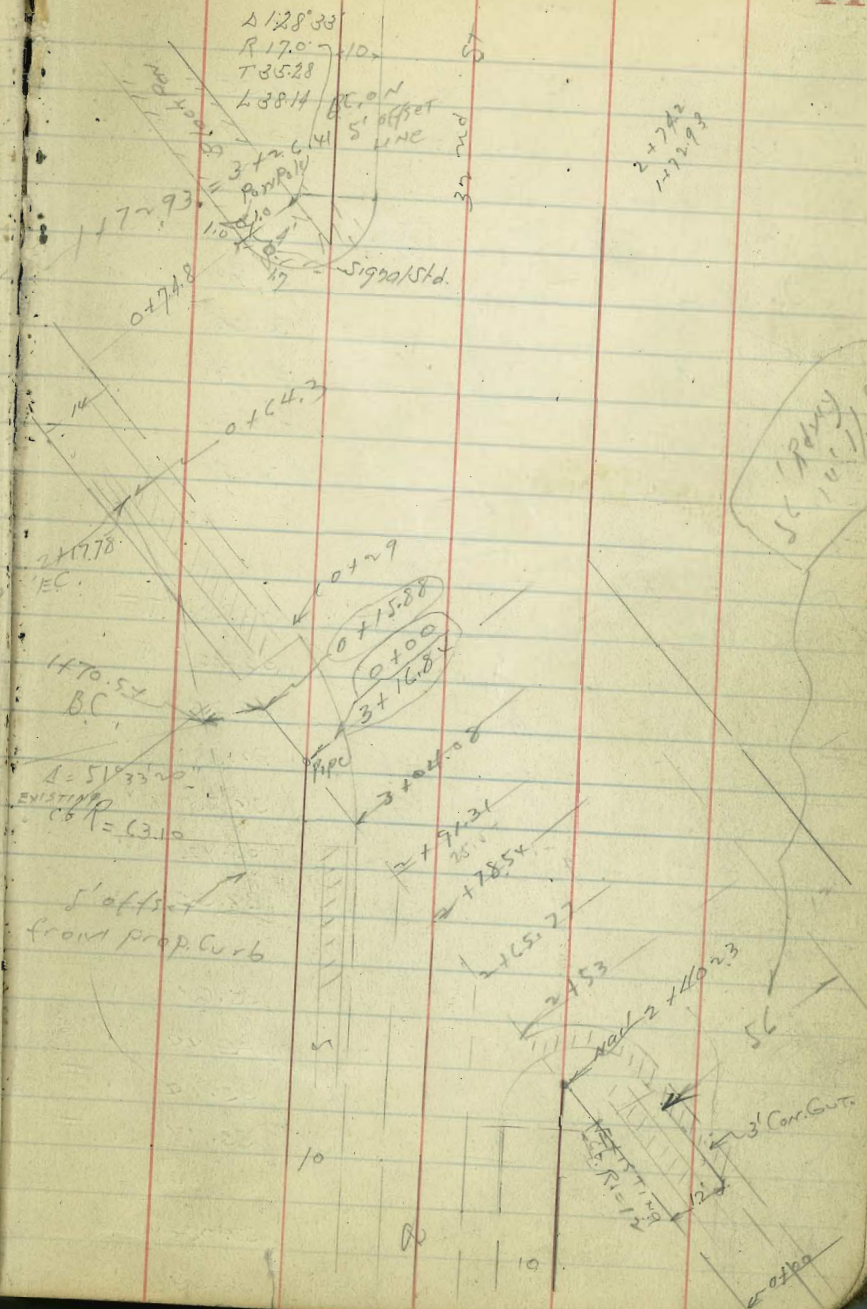
*[Faint handwritten notes and bleed-through from the reverse side of the page]*

Levels on S 1/2 of Main St.

240.03 Fly from old S.E. Cor.,  
3rd & Main = 0+00

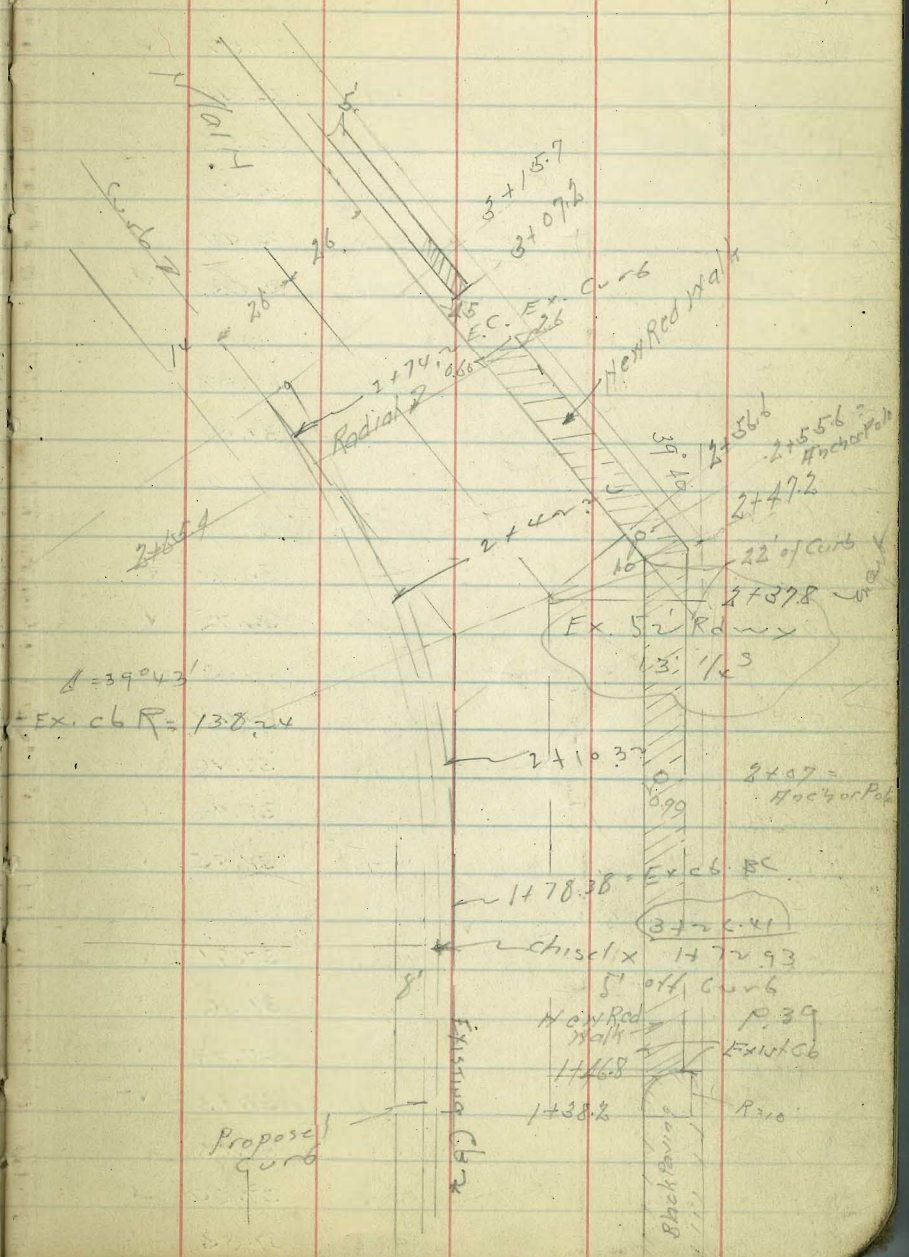
Sections at 90° with Mains

TP. P. 43	5.94	33.81	27.87	
	0+00			
S cb		11.51	22.30	✓
PT		12.12	21.69	✓
1/4		11.39	22.92	✓
1/4		11.20	22.61	✓
1/4		11.41	22.80	✓
PT		11.79	22.02	✓
N cb		11.15	22.65	✓
	0+50			
S 1/4		8.60	25.21	✓
S 1/4		8.74	25.07	✓
PT		9.19	24.62	✓
S cb		8.51	25.30	✓
	1+00			
S cb		5.65	28.16	✓
PT		6.28	27.53	✓
1/4		5.90	27.91	✓
1/4		5.66	28.15	✓
1/4		5.84	27.97	✓



3381 ✓

	1+00				
97		6.26	27.55	✓	
N cb		5.64	28.17	✓	
	1+50				
♀		2.57	31.24	✓	
S 1/4		2.83	30.98	✓	
97		3.23	30.58	✓	
S cb		2.63	31.18	✓	
T.P.	8.53	<u>42.21</u>	0.13	33.68	✓
	2+00				
S cb		7.83	34.38	✓	
97		8.45	33.76	✓	
1/4		7.98	34.23	✓	
♀		7.83	34.38	✓	
1/4		7.73	34.28	✓	
97		8.29	33.92	✓	
N cb		7.66	34.55	✓	
	2+20				
♀		6.00	35.61	✓	
S 1/4		6.77	35.22	✓	
97		7.07	35.14	✓	
S cb		6.44	35.77	✓	
	2+37.7				
S cb	PC: Ex. Ret.	5.19	37.02	✓	
S 97		5.83	36.38	✓	





4221

✓

2+40.23

S cb	5.12	37.09	✓
qt.	5.72	36.49	✓✓
1/4	5.68	36.53	✓
2	5.62	36.59	✓
1/2	5.74	36.47	✓
qt. in drive in	5.98	36.23	✓
2+53			
S to Main pay	5.12	37.07	✓
cb line "	5.12	37.09	✓
1/4	5.10	37.11	✓
2	5.12	37.09	✓
1/2	5.20	36.95	✓
qt in drive "	5.49	36.72	✓
2+65.77			
2	4.70	37.27	✓
S 1/2	4.75	37.46	✓
S cb line Main	4.75	37.46	✓
SL "	4.74	37.25	✓
2+78.54			
S to Main	4.30	37.91	✓
S cb line "	4.35	37.86	✓
1/4	4.43	37.78	✓
2	4.38	37.83	✓
1/2	4.56	37.65	✓
qt	4.97	37.24	✓
N cb	4.38	37.83	✓

4221

Main

46

2+91.31

2 Main	4.20	38.01	✓
S 1/4	4.27	37.94	✓
S cb line "	4.20	37.95	✓
SL "	4.30	37.91	✓
3+04.08			
SL Main pay	4.51	37.70	✓
S cb " "	4.31	37.90	✓
1/4	4.12	38.09	✓
"	4.05	38.16	✓
1/4	4.20	38.01	✓
N cb line Main pay	4.32	37.89	✓
+ 1.3 qt	4.30	37.85	✓
+ 1.3 cb	3.80	38.35	✓
3+16.84 = 0+00	See p. 44		
N cb line Main pay	3.95	38.26	✓
N 1/4	3.97	38.29	✓
2	3.88	38.33	✓
S 1/4	4.02	38.19	✓
S cb " " "	4.32	37.89	✓
+ 6.8 qt.	4.38	37.83	✓
+ 6.8 cb	3.80	38.21	✓
SL Top Pipe Cor.	3.75	38.46	✓
0+15.88			
SL dirt	3.3	38.9	
+ 12.7 cb	3.57	38.62	
" qt.	4.22	37.99	

Req. of  
52 Roddy.  
and 13 1/2  
Sketch  
p. xv

SW Cor  
3rd  
Main

4271

S.c.	pay	4.23	37.98	
S 1/4		3.84	38.37	
£		3.60	38.61	
	0 + 29			
S.c.	dist	3.1	39.1	
S.c.		3.41	38.80	
9T		4.07	38.19	
S 1/4		3.70	38.51	
£		3.43	38.78	
	0 + 643			
S.c.		2.97	39.29	✓
9T		3.63	38.58	✓
1/4		3.13	39.08	✓
£		2.96	39.25	
1/4		3.16	39.05	
Mobline pay		3.36	38.85	
+ 1 9T		3.40	38.81	
+ 1 6 Ret.		2.49	39.52	
T.P.	6.74	46.76	21.7	40.05
	1 + 00			
S.c.		6.97	39.79	
9T		7.62	39.19	✓
1/4		7.10	39.66	

4676 ✓

47

£		6.95	39.81	
1/4		7.15	39.61	
9T		7.59	39.17	
1 6		6.99	39.77	
	1 + 18			
£		6.64	40.12	
S 1/4		6.81	39.95	✓
9T	in old alley	7.30	39.25	39.46
	1 + 397			
S.c.	line in 9T.	6.98	39.78	✓ sid alley
S 1/4		6.48	40.28	
£		6.32	40.99	
	1 + 72.93 = 3 + 26.41 B.C. Lt. P. 39			
S.c.		5.89	40.87	
9T		6.46	40.30	✓
S 1/4		5.97	40.79	
£		5.75	41.01	
	1 + 78.38 B.C. FISTING curb			Sketch P 45
S.c.		5.81	40.95	
9T		6.37	40.39	✓
1/4		5.87	40.89	
£		5.65	41.11	
	2 + 10.32			
S.c.		5.06	41.70	
9T		5.91	40.85	✓
1/4		5.55	41.21	
£		5.15	41.61	

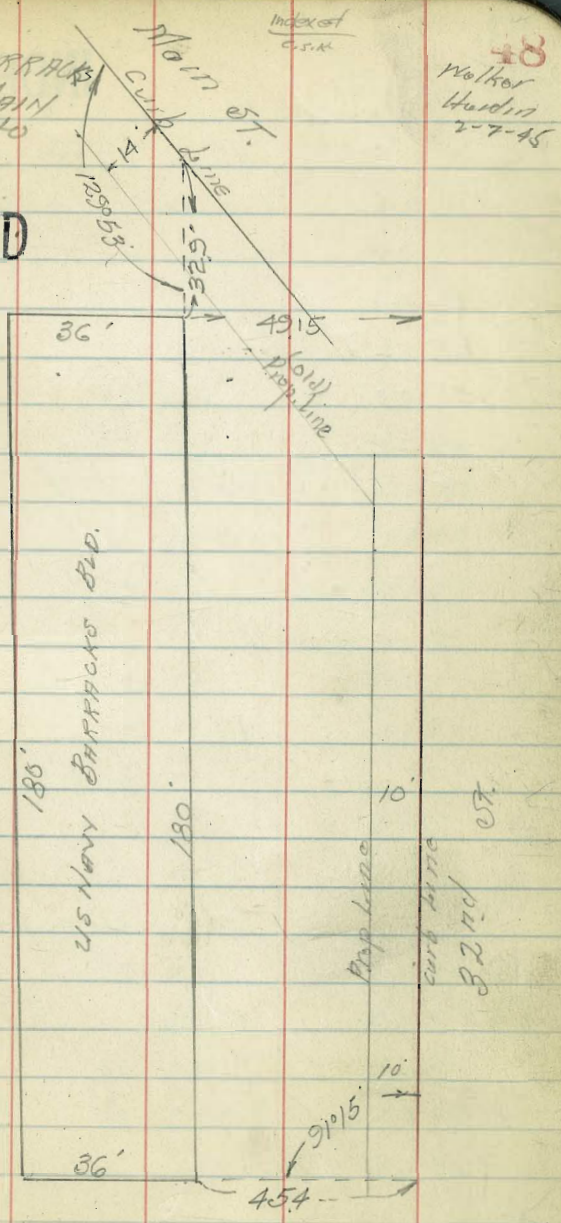
4070 ✓

2 + 42.26			
506	4.55	42.21	
97	5.28	41.98	✓
5 1/2	4.88	41.88	
8	4.43	42.33	✓
2 + 74.2 E.C. EXISTING CURB			
506	4.11	42.65	
97	4.66	42.10	✓
5 1/2	3.95	42.81	✓
9	3.59	43.17	✓
3 + 18.5 - 4 + 8.51 = E.C. on 5' offset line			
506	CUT CURB HERE	3.70	43.06 ✓
97		4.70	42.56 ✓
check to orig. B.M. Main.			
	8.16	38.50	38.59 0.01 p. 42

Notes Reduced. 10.17.22

Location  
US NAVY BARRACKS  
- BLD. 3202 + MAIN  
With reference to  
Curb lines.

INDEXED



Additional Levels South Side Main St.  
West of 3200 ft  
See sketch page 44-45

**INDEXED**

BM 8.57 47.16 FEB 15 1899  
 0+0 feet = 4+16.84 ft. East  
 S.L. 8.8 38.4  
 20'S of S.L. 8.7 38.5  
 0+15.88  
 S.L. 8.4 38.8  
 20'S of S.L. 8.2 39.0  
 0+29  
 S.L. 8.2 39.0  
 20'S 8.1 39.1  
 0+64.3  
 S.L. 7.8 39.4  
 15'S 8.4 39.4  
 20'S 8.1 39.1  
 1+0  
 S.L. 7.8 39.7  
 5'S 8.0 39.2  
 20'S 8.1 39.1  
 1+18  
 S.L. 7.0 40.2 ✓  
 20'S 8.1 39.1  
 1+39.7  
 S.L. 6.5 40.7  
 5'S 7.8 39.4  
 20'S 7.7 39.5

S.W. Mon  
Main 33rd

-20  
 S.L.  
 S.C.B.  
 Gutter  
 1/4  
 1/2  
 1/4  
 Gutter  
 H.C.B.  
 1/2  
 S.L.  
 20'S  
 S.L.  
 20'S  
 -20  
 S.L.  
 S.C.B.  
 Gutter  
 1/4  
 1/2  
 Gutter  
 H.C.B.

47.16  
 1+72.92

2+10.32

2+42.26

2+74.2

6.7  
 6.1  
 6.32  
 6.88  
 6.36  
 6.16  
 6.27  
 6.32  
 5.81  
 6.31  
 6.2  
 5.1  
 5.8  
 4.8  
 5.4  
 5.2  
 4.5  
 4.55  
 5.09  
 4.37  
 4.01  
 3.99  
 4.31  
 3.58

March 24 45  
 Simon  
 8111  
 O.S. 21  
 8299

40.5  
 41.1  
 40.84 ✓  
 40.28 ✓  
 40.30  
 41.00  
 40.89  
 40.84  
 41.35  
 40.85  
 40.8  
 42.1  
 41.3  
 42.3  
 41.8  
 42.0  
 42.7  
 42.61 ✓  
 42.07 ✓  
 42.79  
 43.15  
 43.17  
 42.85  
 43.61

4716

34185

S-L

42

430

✓

20'S

52

420

Levels South Side of Main St  
East of 32<sup>nd</sup> St. Proposed Curb

INDEXED

Stationing	Prop Cb	8' S	8' S	8' S	Prop Cb	8' S	8' S	8' S	8' S
BM 1.88	39.97	38.59	41.03	38.59	1+67.47 = B.C. Lt				
TP 4.02	31.23	27.21	27.21	Prop Cb	8.7	32.3			
	0+0 = 240.23 East of Old S.E. Cor. 32 <sup>nd</sup> St.			8' S	8.4	32.6			
5' Cb	8.93	22.30			1+80.59				
12' S	9.0	23.2		Prop Cb	8.0	33.0			
	0+26.18			8' S	7.9	33.1			
Prop Cb	7.6	23.6			1+93.71 = P.C.C.				
8' South	7.1	24.1		Prop Cb	7.0	34.0			
	0+52.36 = P.R.C.			8' S	7.3	33.7			
Prop Cb	5.8	25.4			2+08.41				
8' S	5.4	25.8		Prop Cb	5.8	35.2			
	0+64.6			8' S	6.3	34.7			
Prop Cb	5.1	26.1			2+23.11				
8' S	4.5	26.7		Prop Cb	4.9	36.1			
	0+76.84 = E.C.			8' S	5.4	35.6			
Prop Cb	4.3	26.9			2+37.81				
8' S	3.7	27.5		Prop Cb	4.8	36.2			
	1+0			8' S	5.0	36.0			
Prop Cb	2.9	28.3			2+52.51				
8' S	2.4	28.8		Prop Cb	4.9	36.1			
TP 16.97	41.03	30.06	30.06	8' S	5.0	36.0			
	1+50				2+67.20 = E.C.				
Prop Cb	9.9	31.1		2' H = Exint Cb	5.8	35.85			
8' S	9.4	31.6		Prop Cb	5.1	35.9			
				8' S	5.2	35.8			
				BM	24.5	38.58			

SW Mon  
Main 432<sup>nd</sup>

Additional Level North Side Main St  
West of 32nd St.

14' Cbs  
13 1/4

April 7-45

5.0007  
81.00  
Outborer  
8099

52

Sketch Page - 44-45

H. Cb Line Stationing

44.67

BM	6.08	44.67	38.59	5 1/2 Mon Main St	2	5.26	39.41
	0+0 to W = 3+16.84 to East					1.70	
		0+15.88			2	4.89	39.78
					1/4	5.05	39.62
2		6.09	38.58		Gutter	5.51	39.16
H 1/4		6.23	38.44		Cb	4.93	39.74
H Cb Line		6.19	38.48		H	4.68	39.99
H L		6.23	38.44			1.718	
		0+29			H	4.54	40.13
H L		6.03	38.64		Cb	4.65	40.02
Cb Line		6.07	38.60		Gutter	5.20	39.47
1/4		6.08	38.59		1/4	4.78	39.89
2		5.92	38.75		2	4.55	40.12
		0+64.3				1.7397	
2		5.42	39.25		2	4.28	40.39
H 1/4		5.64	39.03		1/4	4.44	40.23
Cb Line		5.83	38.84		Gutter	4.81	39.86
+4.2 = Gutter		5.87	38.80		Cb	4.28	40.39
+4.2 = Top Cb		5.18	39.49		4.9 = 1/4 oil Pav	4.35	40.32
H		5.18	39.49		H	4.3	40.4
		0+74.8 = Cb BC on North				1.7293	Page 49
H		4.91	39.26			2.41032	
Cb		5.26	39.41				
Gutter		5.76	38.91		H	2.7	42.0
1/4		5.45	39.12		1.13	3.0	41.7
					Cb	2.62	42.05

	44.67		
Gutter		3.14	41.53
1/4		3.10	41.57
1/2		3.13	41.54
	2+37.8		
1/2		2.67	42.00
1/4		2.76	41.91
Gutter		3.00	41.67
Cb		2.50	42.17
H		2.7	42.0
	2+47.2 = 4 in Cb. taken on split		
H		2.5	42.2
Cb		2.42	42.25
Gutter		3.00	41.67
1/4		2.69	41.98
1/2		2.67	42.00
	2+56.6		
1/2		2.67	42.00
1/4		2.62	42.05
Gutter		2.89	41.80
Cb		2.22	42.47
H		1.9	42.97
	2+80		
H		1.8	42.9
Cb		1.90	42.97
Gutter		2.43	42.24

	44.67		
1/4		2.15	42.52
1/2		2.30	42.37
	2+15.7 = 2+74.2 on South		
1/2		1.50	43.17
1/4		1.48	43.19
TP	4.82	47.07	2.42
Gutter		4.20	42.87
Cb		3.43	43.64
H		3.3	43.8
	2+50		
H		2.7	44.4
Cb		3.08	43.99
Gutter		3.84	43.23
1/4		3.55	43.52
1/2		3.48	43.59



Cross Section Main St.  
West of 32nd St

INDEXED

New South Carb Sta. Sketch Page 14+45

1796.04 Def 3°18'35" Taken Radial

1772.93 = New C6 B.C. Lt.

1739.7

1718

sections extended Page 61

170

0+74.8 = C6 E.C. on N

B.M. 8.44 47.03

28.59

5.11 1107  
17074+822

New  
to Carb 2

May 1-45  
5.5507  
81.11  
05604  
8099

N

54

41.3	41.4	41.39	40.63	41.25	41.43	41.42	41.47	41.99	41.5	41.7
57	52	564 74-cb	640 142-5ul	578 29	560 40	561 55	556 677-5ul	509 677-5ul	555 88	528 81

40.8	41.0	40.86	40.28	40.82	41.01	40.93	40.86	41.35	40.83	40.8
62	60	617 14-cb	675 14-5ul	621 28	602 40	610 55	617 86-5ul	568 86-cb	620 87	620 80

40.2	40.6	39.76	40.27	40.40	40.31	39.86	40.39	40.2
68	64	727 15	676 28	663 40	672 50	717 86-5ul	664 86-cb	680

39.8	40.1	39.43	39.80	40.11	39.83	39.45	40.03	40.15
72	69	760 15	723 25	822 40	720 50	758 86-5ul	790 86-cb	688 80

39.5	39.7	39.77	39.13	39.57	39.80	39.68	39.14	39.75	40.00
75	78	745 14-cb	790 14-5ul	746 25	723 40	745 50	789 86-5ul	788 86-cb	780 80

39.4	39.4	39.38	38.78	39.23	39.42	39.29	38.92	39.41	39.76
26	76	765 14-cb	825 14-5ul	780 25	761 40-8	774 50	811 86-5ul	762 86-cb	727 80

47.03

3750

2+11.63 Def 19° 51' 30" Cb EC - Exnting Cb

2+88.51 Def 16° 32' 50" Taken Radial

2+65.40 Def 13° 14' 20" Taken Radial

2+42.28 Def 9° 55' 45" Taken Radial

2+19.16 Def 6° 37' 10" Taken Radial

47.03

New  
50 Cb

42.9	43.17	42.66	43.38	43.72	43.81	43.42	44.13	44.4
4/14	3.86 Cb	4.27 100-Gul	5.65 13	5.21 26	5.22 38	5.61 52-G	2.90 52-G	2.6 86
42.8	43.04	42.58	43.33	43.41	43.53	43.31	44.04	44.4
4/14	3.98 Cb	4.45 100-Gul	3.70 13	3.42 26	3.50 38	3.72 52-Gul	2.99 52-G	2.6 86
42.8	42.9	42.97	42.46	43.09	43.45	43.42	43.15	43.91
4/13	41	4.06 15-Cb	4.57 15-Gul	3.94 13	3.55 38	3.91 46	3.88 53-Gul	3.14 53-G
42.6	42.7	42.68	41.99	42.70	42.96	42.92	42.58	42.26
4/8	43	4.35 56-Cb	5.04 56-Gul	4.33 20	4.07 33	4.11 45	4.45 59-Gul	3.77 59-Cb
42.3	42.8	42.23	41.49	42.05	42.37	42.35	42.07	42.70
4/8	42	4.80 99-Cb	5.54 99-Gul	4.88 25	4.26 38	4.68 50	4.96 69-Gul	4.33 69-Cb
41.8	42.0	41.91	41.08	41.47	41.75	41.82	41.71	42.20
5/28	5/0	5.12 127-Cb	5.95 127-Gul	5.56 38	5.28 40	5.21 55	5.32 73-Gul	4.89 73-Cb

17.03

S

New Sec

7

47.50

47.0

47.03

43.1	43.53	43.03	43.62	43.97	44.00	43.75	45.0	
3.9 14	3.50 56	4.00 100-94	3.41 13	3.06 28	3.02 38	3.38 84-94	2.8 86	
43.1	43.33	42.85	43.57	43.86	43.79	43.56	44.30	44.5
3.9 14	3.70 56	4.18 100-94	3.46 13	3.7 26	3.14 38	3.47 84-94	2.73 86	2.5 86
			47.03					

Cross Section Lincoln Ave  
At Cleveland  
Levels next Page

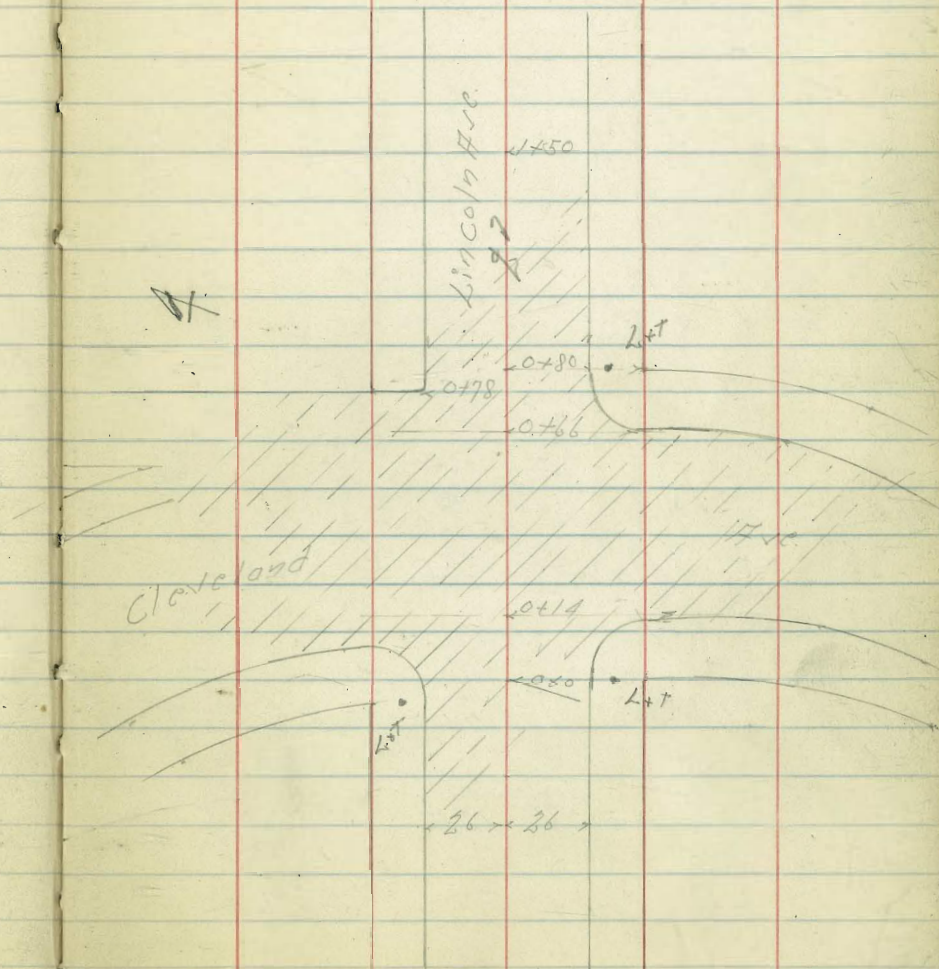
INDEXED

indexed  
c.s.K.

INDEXED

Sept. 1-45  
Sisson  
Bliss  
Osborn  
Begg

57



Cross Section Lincoln Ave.  
At Cleveland

Lt=11

S

Rt=5

58

**INDEXED**

+40 = 1/2 Cleveland

6.08 75	6.61 40	6.82 26	6.89 26	7.04 10	7.17	7.32 10	7.45 20	7.53 26	7.67 10	7.93 75
------------	------------	------------	------------	------------	------	------------	------------	------------	------------	------------

6.04 75	6.67 40	6.90 26	6.96 26	7.08 10	7.23	7.40 10	7.58 20	7.69 26	7.91 10	8.10 75
------------	------------	------------	------------	------------	------	------------	------------	------------	------------	------------

+25

+14 = W CB

6.34 75	7.12 40	7.21 26	7.29 26	7.17 10	7.27	7.57 10	7.87 20	8.10 26	8.35 40	7.93 75
------------	------------	------------	------------	------------	------	------------	------------	------------	------------	------------

0+0 = W 1/2 Cleveland South side of Lincoln

6.77 26-CB	7.48 26-Gut	7.29 26	7.38 26	7.38 10	7.38	7.65 10	8.08 20	8.34 26	7.77 26-CB
---------------	----------------	------------	------------	------------	------	------------	------------	------------	---------------

BM

7.53 305.09

S.W. 1/4  
Lincoln  
Cleveland

TP 0.73 312.62 12.42 311.89

312.62

TP 0.21 324.81 11.13 324.10

BM 6.03 335.23 332.20

N.E. 1/4  
Lincoln  
Park 8th

1+25

1+0

+80 = FL Cleveland

+78 = Alley Return on Lt.

+66 = F.Cb of Cleveland = Valley Gutter

0+52

312.62

	LT=N	△	R1=N	59
	08.94	08.27	08.32	08.39
	368 26.05	438 26.51	430 20	442 10
	07.40	06.71	06.82	06.94
	522 26.26	591 26.91	580 20	568 10
	06.06	05.41	05.58	05.62
	656 26.23	721 26.61	724 20	700 10
	06.20	05.30	05.43	05.47
	641 40.05	668 40.51	719 20	715 10
	05.97	06.05	05.43	05.43
	639 40.05	689 26.26	738 26.51	719
	06.23	05.27	05.08	04.84
	700 40	735 26	754 20	767 10
	05.62	05.49	05.08	04.95
	713 26	720 20	732 10	745
	06.01	05.17	05.13	04.74
	711 40	745	749	788
	05.44	04.72	04.54	04.56
	758 10	808	813	806
	05.00	04.66	04.74	04.56
	771 26	813 4.08	813	806
	04.91	04.49	04.85	04.93
	813 40	827 40.51	769 26.51	769
	04.70	05.02	04.85	04.93
	778 40	827 40.51	769 26.51	769
	04.40	04.40	04.40	04.40
	827 15	827	827	827

312.62

1-30

2/262

10.52  
2.10  
26-cb

09.84  
2.78  
26-9d

09.83  
2.79  
20

09.80  
2.82  
70

09.54  
2.88

09.07  
3.58  
70

08.34  
4.18  
26

08.03  
4.59  
26-9d

08.91  
4.21  
26-cb

LT=11

2

AT=5

60

2/262

Levels on New Walk North Side Main St  
West of 32nd St.

INDEXED

New South Carb Stationing Sketch Page 45

BM	4.92	46.51	38.59	5477.00 Main St 32nd
		1+46.8 = Fly New Red Walk		
66.7H = HCB		6.00	40.51	
66.8" = Sly Walk		6.07	40.44	
76.6" = Hly "		5.99	40.52	
		1+59.4 = Fly Island		
66.7H = HCB		5.56	40.95	
66.8 = Sly Walk		5.86	40.65	
68.7 = Hly Island		5.89	40.62	
76.6 = Hly Walk		5.76	40.75	
		1+62		
66.7H = HCB		5.96	41.05	
68.7 = Hly Island		5.93	41.08	
68.7 on Walk		5.81	40.67	
76.6 = Hly Walk		5.72	40.79	
		1+72.93 = BC on S		
66.7H = HCB		5.14	41.37	
68.7 = Hly Island		5.13	41.38	
" on Walk		5.58	40.93	
76.6 = Hly Walk		5.41	41.07	
		1+96.04 = Island Ext. 9 W on HCB		
67.7 = HCB		4.50	42.01	
70.4 = Hly Island		4.47	42.04	
" on Walk		4.86	41.65	
78.5 = Hly Walk		4.83	41.68	

Nov. 6-75  
Sisson  
Bliss  
Beeg.

61

46.51

2+49.16 Taken Radial

72.7H = H Gutter in Drive 4.72 41.79

82.7H = Hly Walk 4.36 42.25

2+42.28 Taken Radial

67.9H = H Gutter in Drive 4.33 42.18

78.1H = Hly Walk 3.65 42.86

2+65.40 Taken Radial

59.7H = HCB 3.23 43.28

68.7H = Hly Walk 2.00 43.51



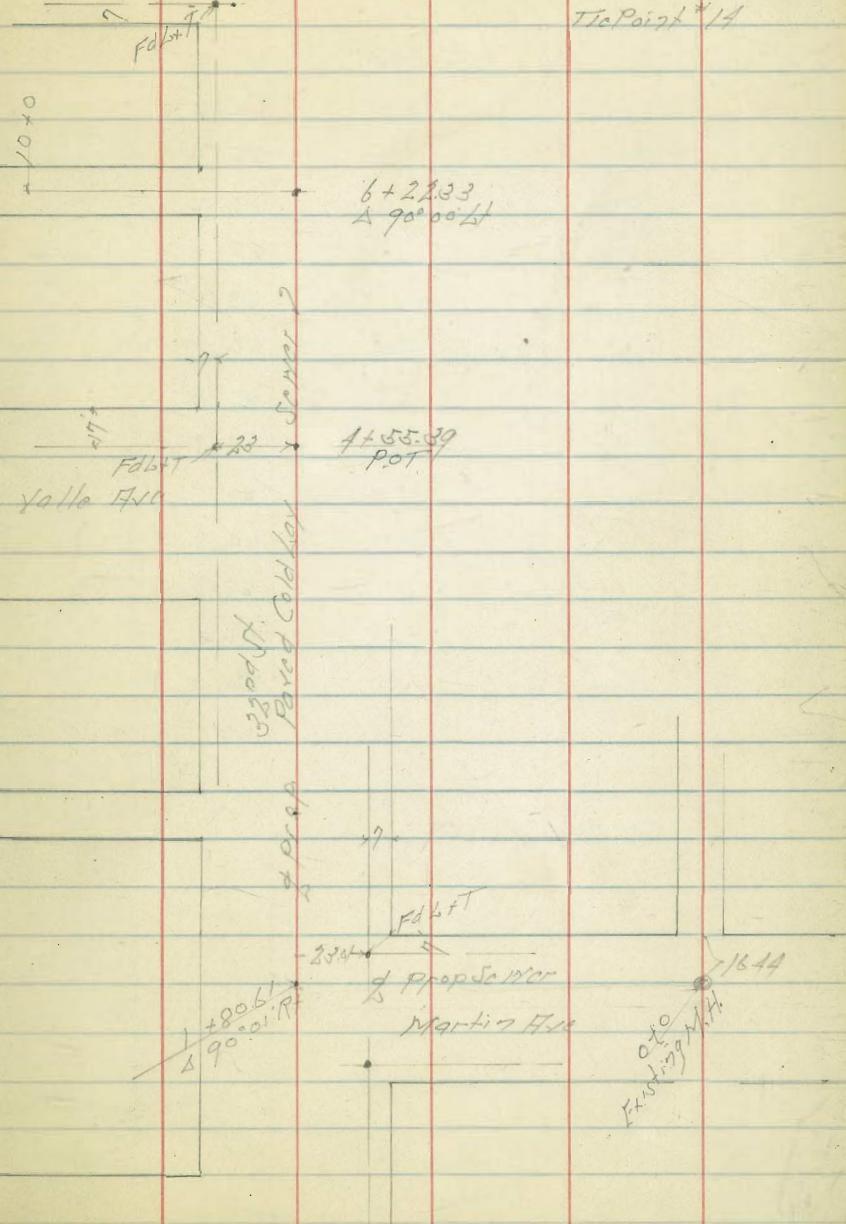
Proposed Sewer Martin Ave 32nd St to Alley East. 32nd St Martin Ave to Alley Between Valle Ave & Ocean View Blvd.

Ocean View Blvd

June 19-46  
Sisson  
Haddel  
Ellen  
Tie Point #14

62

BM	0.39	60.79		60.40	S on Top of Hd Ocean View Blvd 432nd St
TP	0.04	47.90	12.93	47.86	
TP	0.81	36.00	12.71	35.19	
0+0 =	Fast M.H.		12.68	23.32	on Rins
"	<b>INDEXED</b>		17.76	18.24	Flanline
+50	<b>WK</b>		8.3	27.7	
1+0	<b>FEB 15 1949</b>		1.8	34.2	
TP	11.44	16.63	0.81	35.19	
+50			9.0	37.6	
+60	Fly Cobble Pav		8.10	38.53	
+80.61 =	$\Delta 90^\circ$ on R = 32nd St		6.94	39.69	on Road/ail
2+0			6.42	40.21	
+50			4.05	42.58	
3+0			0.99	45.64	
TP	13.12	38.41	0.34	46.29	
+50			9.59	48.82	
4+0			6.68	51.73	
+55.39 =	N 17 1/2' line of Valle		4.81	53.60	
5+0			3.96	54.45	
+50			3.23	55.18	
6+0			2.58	55.83	
+22.38 =	$\Delta 90^\circ$ on Lt.		2.34	56.07	
+42			2.2	56.2	on Pav
+50			1.5	56.9	on Ground over Paving
TP	11.26	68.75	0.92	57.49	



	68.75			
6781		7.5	61.3	
740		61	62.6	
"	17' Rt of 2	12.4	56.4	Ground
"	10' 10" Pl. " " 5' W Cor Conc Block Bldg Under Coat.	10.6	58.2	07 Floor
719	4' of 7 - 2 + 1/4 House	3.6	65.2	07 Floor
750		3.7	65.1	
840		2.4	66.4	
"	11.5' Rt of 2	1.5	67.3	07 Ground
"	19' Rt "	13.9	54.9	" "
750		2.7	66.1	
940		3.9	64.9	
"	14' 1/2 of 2 + 1/4 H6600	11.1	67.7	07 Floor
750		7.6	61.2	
1040		12.8	56.0	
B.M.		8.35	60.40	S.M. Top of Hill Occas. Vert + 3.20 60.40

Montezuma Road + College Ave.  
Transfer of Bench Mark

Sept. 29-49  
H. Sisson  
Garber

Seminole Drive Bench Levels  
South Easterly of El Capon Blvd.

64

B.M. 1.903 454.43

452.51

SE Top of Hill  
Montezuma  
College Ave

B.M.

5.25

457.71

452.46

Six BP  
El Capon +  
Re lands

10.07

464.22

3.56

454.15

B.M. set

INDEXED

W.K.

DFG 19 1949

4.583

449.83

NE B.P.H.  
Re lands  
Montezuma  
+ College

2.32

462.27

4.27

459.95

B.M. #1

4.30

462.36

4.21

458.66

1" P.I.P.  
22 ft 17+0  
Fugate  
458.87

8.46

466.81

4.01

458.35

B.M. #2

0.81

466.00

Six P.I.P.  
#176866  
15 ft 7+25  
189.87  
466.02

B.M.

5.62

461.19

07 1/2 P.I. May  
+ 2ood plug  
# R 14256  
+ 57.67

B.M.

3.21

462.60

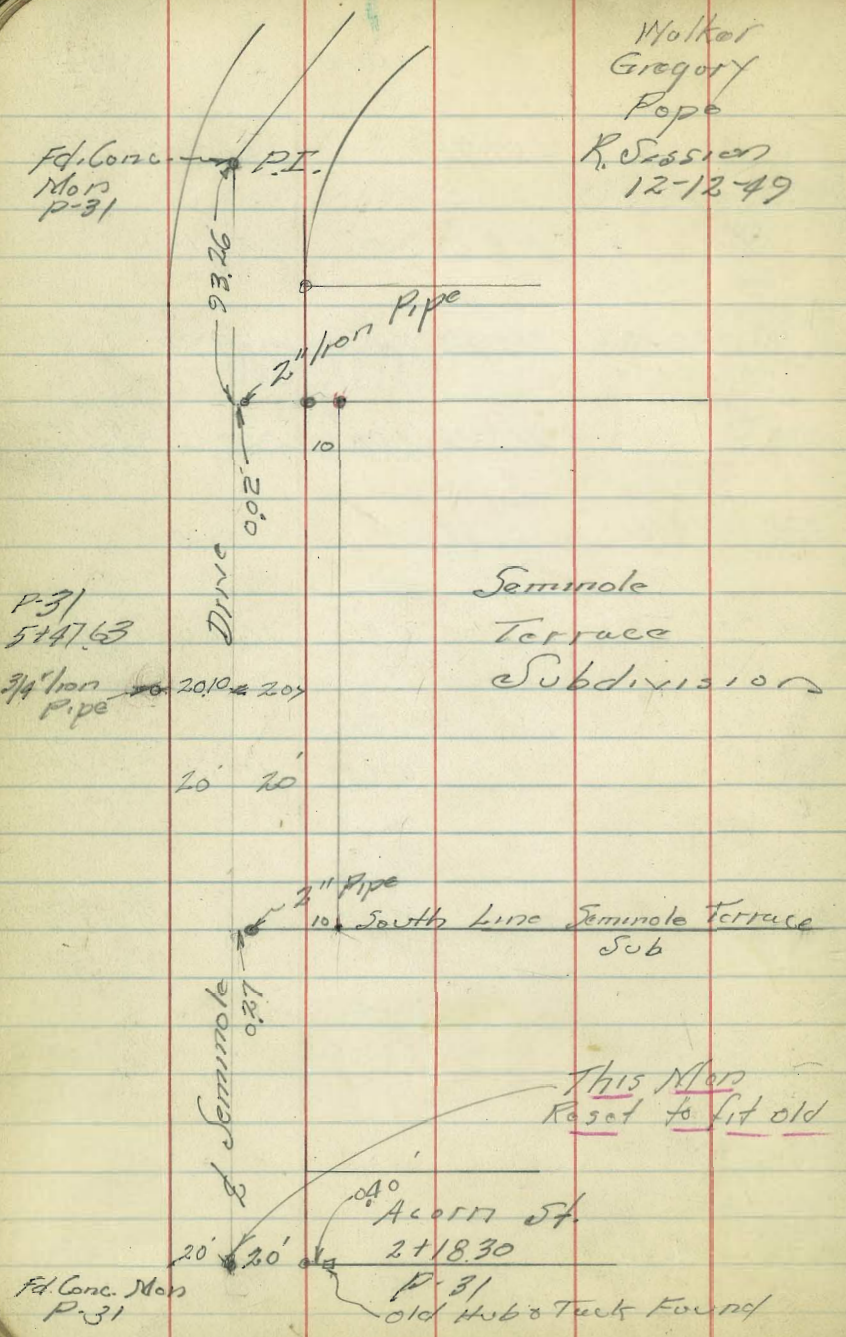
07 1/2 P.I. 1953  
85.07 West  
9 + 52.05

Paving on Montezuma East of College Ave  
is H.C. and 5" thick

Tested new 2 opposite N.E. Curb EC.  
Also Ely Paving East of College Ave

Walker  
Gregory  
Pope  
R. Session  
12-13-49

Ties To Seminole Terrace  
Subdivision  
Supplementary Notes to EP 2037

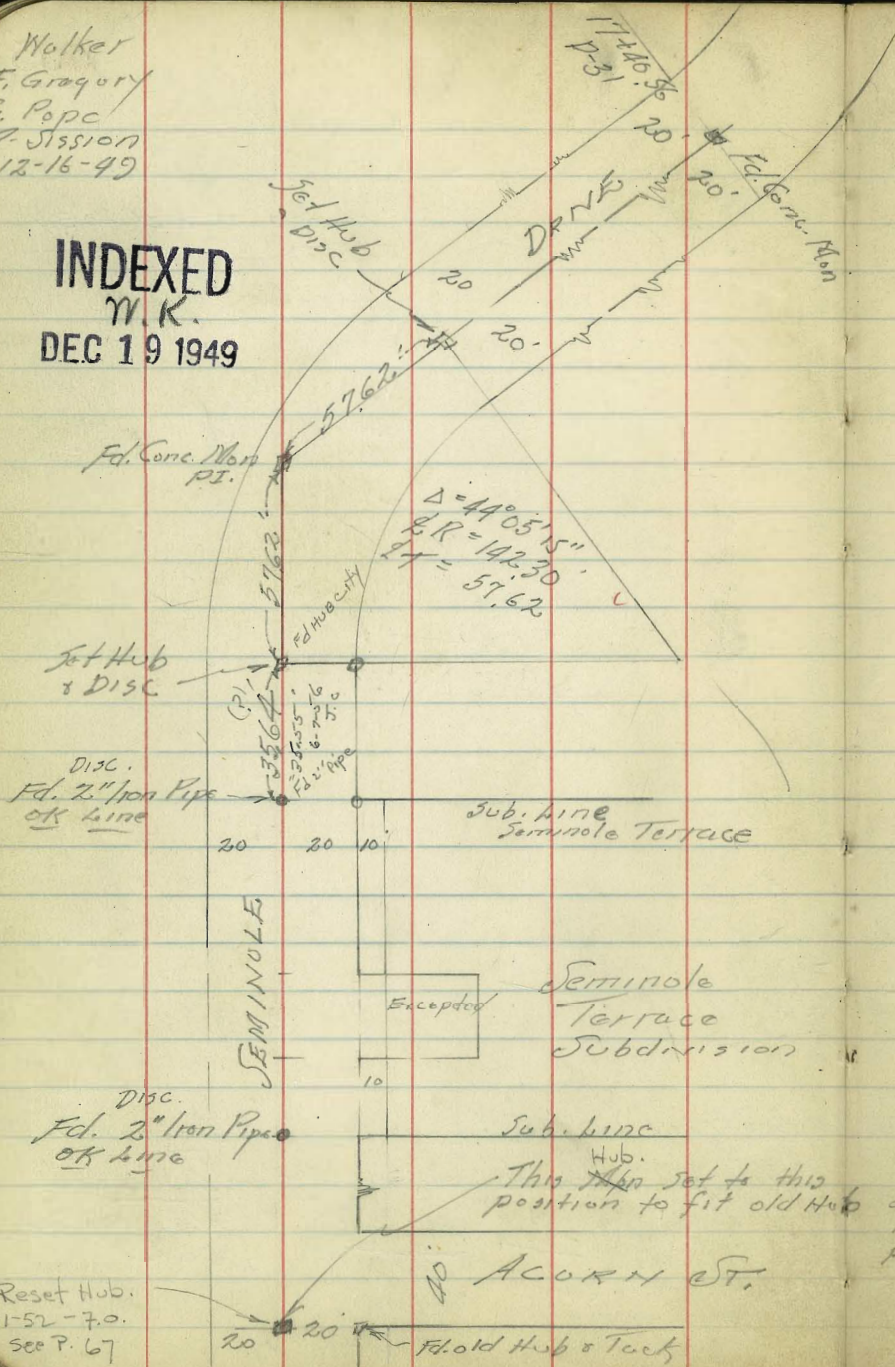


See Page 66

This Mon  
Reset to fit old Hub & Tack at S.E. Cor Acorn & Seminole Dr.  
as per instruction E.F. Gabrielson  
See P-66 for New Curve Data

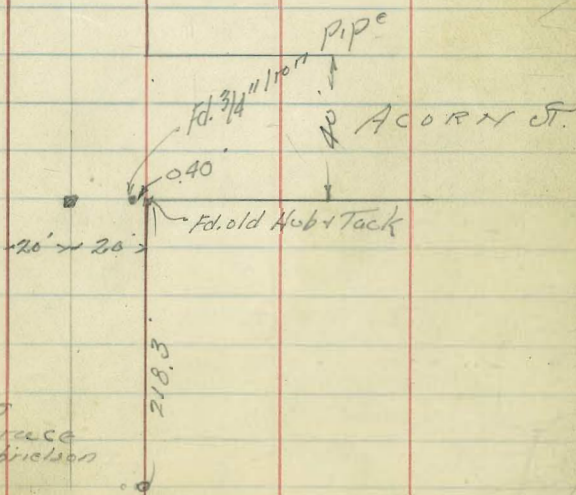
Walker  
 F. Gregory  
 G. Pope  
 R. Sisson  
 12-16-49

INDEXED  
 M.K.  
 DEC 19 1949

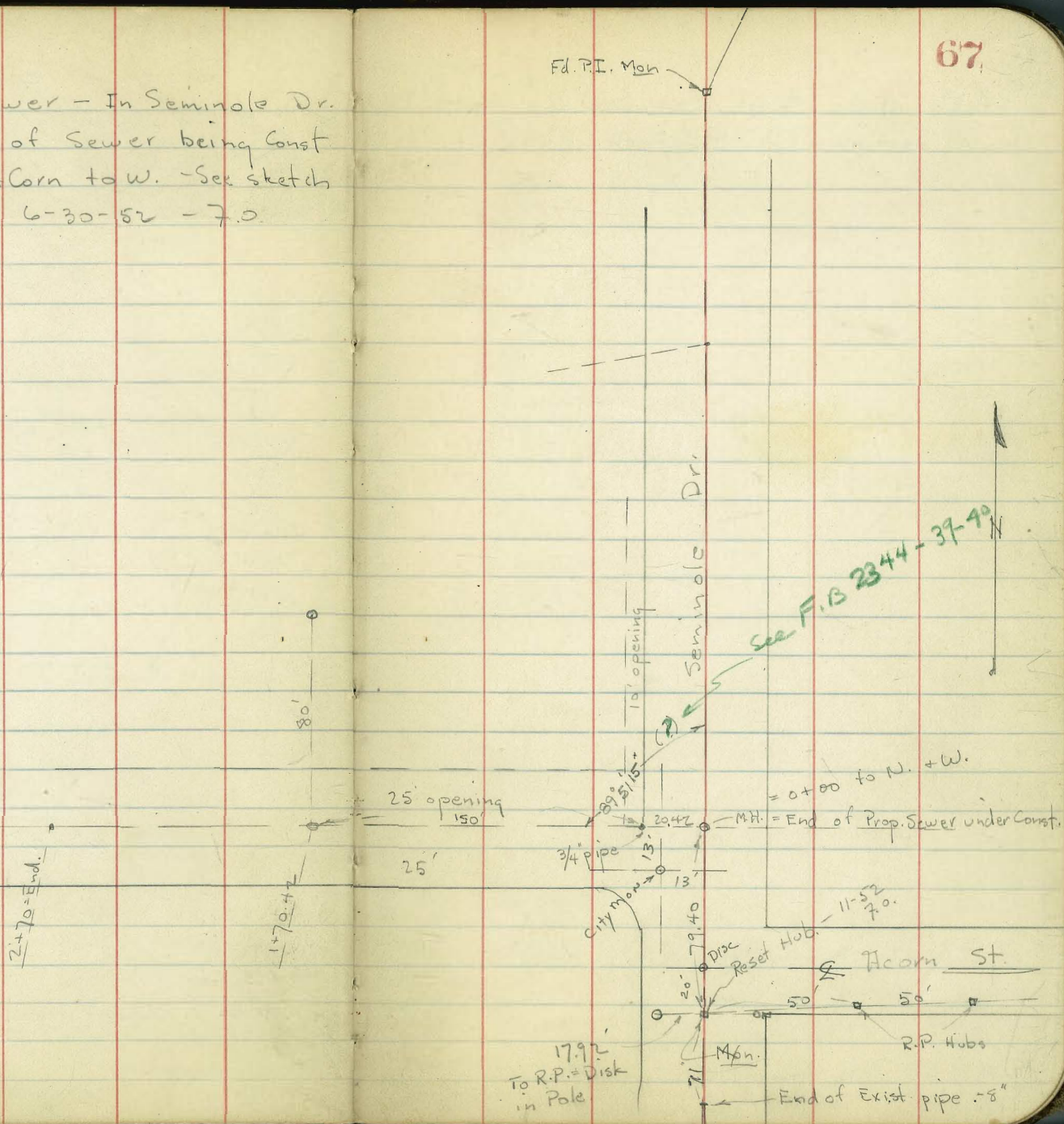


Ties on  
 Seminole Terrace  
 & Seminole Drive

66



Survey for Prop. Sewer - In Seminole Dr.  
 + Acorn St. - Ext. of Sewer being Const  
 By City to ± of Acorn to W. - See sketches  
 W.O. 20009 - 6-30-52 - 7.0



Levels along  $\pm$  of Prop. Sewer - Acorn St.  
w. of Seminole Pr. - Sketch - P. 67

3+00

2+00

1+00

Ground Both sides level

0+00 = M.H. - to be Const.

B.M. = S.E. Pole - Seminole  
+ Acorn

465.68

Lt.

$\pm$

Rt.

68

65.2

65.3

65.88

65.6

4<sup>th</sup> Elev. Not Noted.

Actual Elev. Shown

Levels along  $\pm$  of Prop Sewer - in  $\pm$   
of Seminole Dr. - Acorn to N.

3+80 = End. = Lot Line S. of Stanley St.

65.4

3+00

65.6

2+00

65.7

1+00

65.9

0+00 = M.H.

65.6







72



74

Sta.	+	H1	-	E1							
0				300.00	Arbitrary out 70'	11	169.9		5.9	164.0	75 Grade
	0.9	300.9				12			11.9	158.0	
	-0.2	288.7	12.5	288.4		25	160.5				
1			4.1	284.5		13			8.5	152.0	
	0.1	275.3	13.0	275.2		0.0	148.0	12.5		148.0	
	0.2	262.5	13.0	262.3		14			2.0	146.0	
2			8.1	254.4		15			8.0	140.0	
	0.4	250.2	12.7	249.8		0.3	135.2	13.1		134.9	Final out 70'
	0.2	237.4	13.0	237.2		0.9	123.2	12.9		122.3	
3			7.2	230.2		16			4.8		
	1.2	225.7	12.9	224.5		12	111.4	13.0		110.2	
4			2.3	223.4		+75			10.2		
	0.4	213.0	13.1	212.6		17				87.0	
5			6.2	206.8		+25			2.6	108.8	
	1.7	201.8	12.9	200.1		12.2	123.4	0.2		111.2	
6			8.1	193.7	Grade	18				122.0	Grade
	0.8	194.5				19					
7			10.2	184.3		20				110.0	
	0.7	182.1	13.1	181.4		0.7	110.7	13.4		110.0	
8			0.1	182.0	Grade	21			6.7	104.0	
9			6.1			22	0.6	98.6	12.7	98.0	
10			12.1	170.0	Grade	23			6.6	92.0	
	0.6	169.9	12.8	169.3		24	0.0	86.0	12.6	86.0	
						25			6.0	80.0	
						26	0.6	74.6	12.0	74.0	
						27			6.6		
						28			12.6		

Sta	+	HI	-	El.		%					
0	09	300.9		300.0	Q50			229.1			
1			11.9	289.0	Grade		3.9	220.0	13.0	216.1	
	04	289.4				16			6.0	214.0	$\frac{12.9}{F7.9}$
2			5.4		"	17			11.0		Gr. ✓
3			10.4	279.0	$\frac{12.6}{Q22}$		2.7	209.7	13.0	207.0	
	2.2	284.8	6.8	282.6		18			5.7	204.0	Co. S
4			10.8	274.0	$\frac{7.1}{C3.7}$	19			10.7		Gr. C10
	1.6	273.4	13.0	271.8			3.0	199.7	13.0	196.7	
5			4.4	269.0	$\frac{14.1}{F10.2}$	20			5.7	194.0	C15
6			9.4	64.0		21			10.7		C20
7			14.4	259.0	$\frac{6.9}{C7.2}$	+50			13.2		$\frac{15.4 C0.3}{F2.2}$
	0.3	260.7	13.0	260.4			-0.7	183.6	15.4	184.3	
	1.4	249.1	13.0	247.7		22				184.0	
8			+4.9	254.0	$\frac{7.0}{F11.9}$	23			7.6	179.0	Gr. ✓
9			0.1	249.0	Gr	24			13.1		$\frac{7.2}{C5.9}$
10			5.1		$\frac{12.5}{F7.4}$		2.2	172.8	13.0	170.6	
	11.3	247.9	12.5	236.6		25			7.8	165.0	
11			8.9	239.0		26			13.3		Gr
12			13.9		$\frac{9.1}{C4.8}$		4.8	164.3	13.3	159.5	
	3.5	238.4	13.0	234.9		27			10.3	154.0	"
13			9.4	229.0	Gr		2.1	153.4	13.0	151.3	
	3.7	229.1	13.0	225.4		28+50			7.6	145.8	"
14			5.1	224.0		29			10.4	143.0	
15			10.1				1.0	141.4	13.0	140.4	

		141.4			
30			3.9	137.5	Gr
31			9.4	132.0	"
	0.9	129.3	13.0	128.4	
32			2.3	127.0	$\frac{0.0}{C 2.3}$
33			7.3		Gr
	2.4	124.4	7.3	122.0	
34			7.4	117.0	"
35			12.4		"
	0.6	112.6	12.4	112.0	
36			5.6	107.0	"
	0.7	100.3	13.0	99.6	
37			+2.3	102.0	$\frac{10.6}{F 12.9}$
38			—	97.0	
+50			5.8	94.5	Gr
39				92.0	"
40			13.3	87.0	"
	3.6	90.6	13.3	87.0	
41			8.6	82.0	$\frac{2.7}{P 1.7}$
42			13.6		$\frac{10.3}{C 3.3}$



Proposed Sewer Alley Between  
Valle St + Martin Ave. From 31st St to 32nd St.

**INDEXED**

BM	0.66	49.27	48.61	N.M.B.P. Occasy 10w Blvd. + 31st St
TP	1.51	39.39	11.39	37.88
0+0	-	FL 31st St	5.9	33.3
+35			4.6	34.8
+44	103' H of 1/2" SFH	10.1	29.3	on Basement Floor
+55.10	- EXIST MH	13.05	26.34	on Floor
"	"	20.15	19.24	Floor Line
+63	52' RT of 1/2" SFH 30' Conc Pipe Culvert	14.04	25.35	Floor Line
+70		12.3	27.1	
+70		12.3	27.1	
+50		7.8	32.1	
TP	11.85	50.77	0.47	38.92
+70		10.4	40.4	
"	50' RT of 1/2"	14.5	36.3	
+37		3.1	47.7	
+50		2.8	48.0	
3+0		1.3	49.5	
"	100' RT of 1/2"	7.3	43.5	
TP	10.96	61.58	0.15	50.62
3+27		10.0	51.6	
"	89' H of 1/2" SFH Frame House	17	59.9	on Floor
2+57		7.3	44.3	
"	94' H of 1/2" SFH Frame House	2	61.4	on Floor
+95.61	POT	3.66	57.92	on Stub

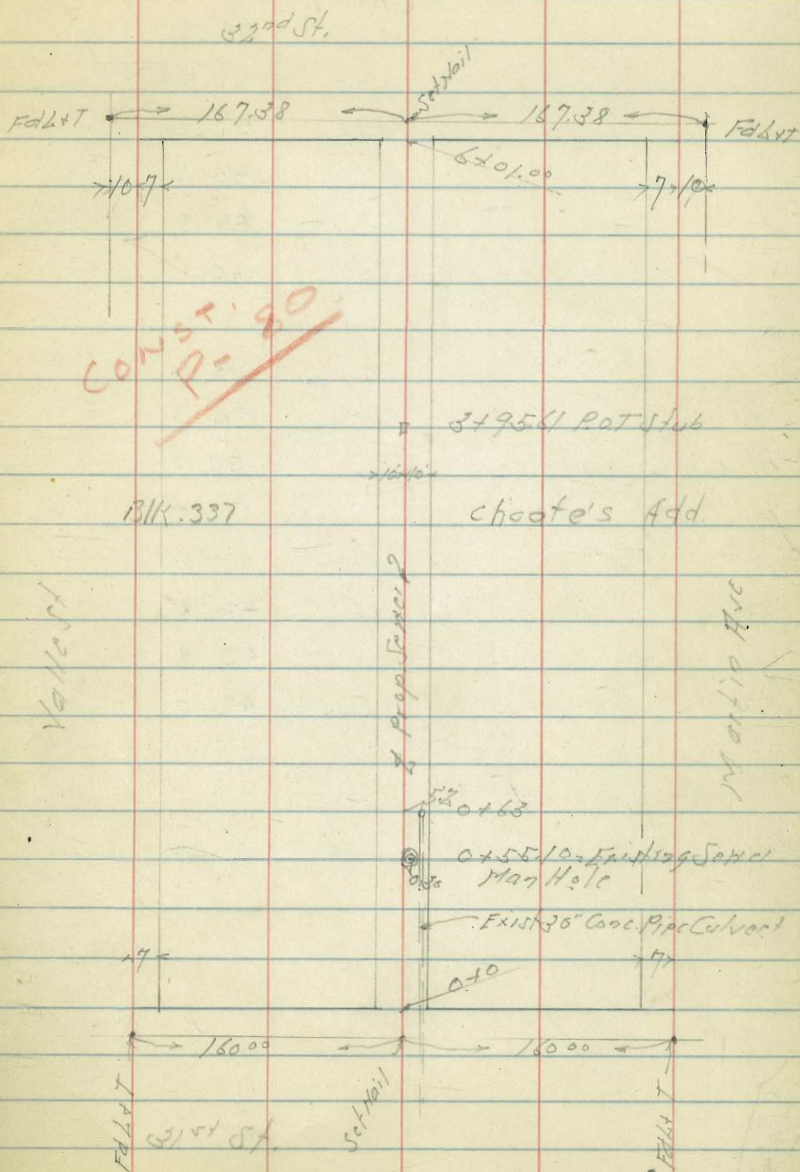
INDEXED  
C.S.K.

T.P. #14

**INDEXED**

March 11-16  
S. 5507  
Osborne  
8999  
Haddel

78



	61.58			
+27		3.4	58.2	
"	73' H of 2nd S.F.H. Frame House	0.00	61.58	07 Floor
+50		4.4	57.2	
"	100' R to 1/2	11.4	50.2	
+77		5.8	55.8	
"	94' H of 1st = 1/2 x 5 1/2' St 60' House	1.5	60.1	07 Floor
+50		8.0	53.6	
+50		11.3	50.3	
+57	15' R to 1st = 1/2 x Frame House	11.6	50.0	07 Floor
TP	5.83	55.41	12.00	49.58
+85		8.6	46.8	
6+01.00	W.L. 32nd St	11.6	43.8	Ground
+11	W.C. 1st x 32nd	13.4	42.0	07 Pav 129
TP	7.00	61.98	0.43	54.98
BM		1.45	60.53	5' H Top Finishes Occupied + 32' 0.5' x 60.50

# INDEXED

80

150' Sewer grades

Blk 337 Choates add

Moore  
Boyer  
Greer  
Roberts  
11-4-47.

W/O, 602.05

Sketch P. 78  
~~XXXXXXXXXX~~  
Stakes set at 25 intervals  
and 41 S. on Rt.

24649 M.H. #1

3383  
11.17  
45.00

45.00

1+50 end

33.83

7.47

2.16

C 7.31

1+25

31.40

7.06

1.96

C 5.10

1+00

28.96

9.50

6.04

C 3.46

0+75

26.53

11.93

9.34

C 2.59

check to orig BM 019 4862 4861

0+50

24.10

14.36

11.57

C 2.79

T.P. 915 4881 364 39.66

0+25

21.67

16.79

10.68

C 6.11

T.P. 680 4330 1.96 36.50

T.P. 131 3846 11.84 37.15

N.W. B.P. 038 4899 4861

0+00 = Ex. M.H.

19.24

17.22

3.27

C 15.95

Ocean View Blvd  
and 31st

on P.M.

175' Sower in  
BIK 337 Cheates Add.

Sommermeier  
McCoy  
Jones  
2-14-49

81

N.W. 8. B. Ocean View. + 31<sup>st</sup> = → B.M. Page 90

Stakes - 5' so of ♀

48.61  
8.59  
57.20  
10.04  
47.16  
4.65  
51.81  
1.20  
50.61  
11.77  
62.40

2+64<sup>l</sup> ↓ M.H. #1  
↑

51.81X

45.00

6.81

1.20

C 5.61

2+50

43.57

8.24

2.18

C 6.06

2+25

41.13

10.68

3.56

C 7.12

2+00

9.724%

38.70

13.11

4.36

C 8.75

Dead end

3+25

.844%

45.50

16.90

5.63

C 11.27

1+75

36.26

15.55

6.39

C 9.16

3+00

45.29

17.11

8.32

C 8.77

1+50 = Exist. D.E.

33.83

17.98

10.84

C 7.14

2+75

62.40X

45.08

17.32

10.84

C 6.50

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope  $\frac{1}{2}$  to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance

**IMPROVED TABLES**

AND

**INFORMATION**

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given  $L$  may be found by dividing tangent (or external), opposite  $L$  by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

At Overhead Xing -

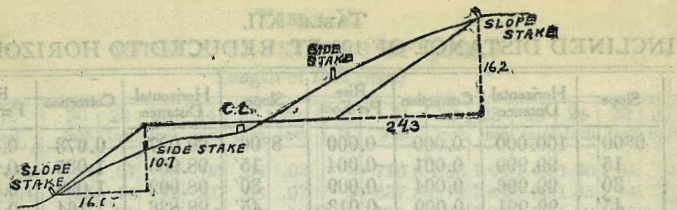
Rail			100.0	Assumed
	7.2	107.2		
		9.4	97.8	Assumed

203 =  $\Sigma$  of Blw at underpass -

16+02.5

N. 14° E

13+23.5    118° 35    237° 04

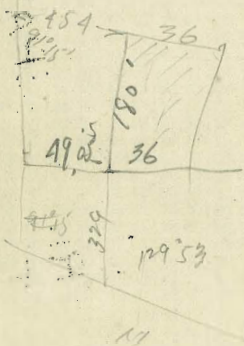


DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/4 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

$$\begin{array}{r}
 237 \\
 .64 \\
 \hline
 948 \\
 1422 \\
 \hline
 15168
 \end{array}$$


$$\begin{array}{r}
 12.81 \\
 5.02 \\
 \hline
 9.79 \\
 4.90 \\
 \hline
 14.69
 \end{array}$$

$$\begin{array}{r}
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 22 \\
 \hline
 565
 \end{array}$$

$$\begin{array}{r}
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 34.0 \\
 \hline
 8.2
 \end{array}$$

$$\begin{array}{r}
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 5.1 \\
 2.5 \\
 \hline
 220.5 \\
 223.5
 \end{array}$$

129.53

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 493.7 \\
 194 \\
 \hline
 36 \\
 230
 \end{array}$$

$$\begin{array}{r}
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 18 \\
 \hline
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 \end{array}$$

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 232.5 \\
 \hline
 11.9
 \end{array}$$

$$\begin{array}{r}
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 11.3 \\
 \hline
 143.5 \\
 137.5 \\
 132.0
 \end{array}$$

$$\begin{array}{r}
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 113 \\
 \hline
 187
 \end{array}$$

$$\begin{array}{r}
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 4.03 \\
 \hline
 11.21 \\
 3.75 \\
 \hline
 14.96
 \end{array}$$

$$\begin{array}{r}
 5.7 \\
 3.2 \\
 \hline
 2.3
 \end{array}$$

$$\begin{array}{r}
 35.0 \\
 14.8 \\
 9.5 \\
 \hline
 132.0
 \end{array}$$

$$\begin{array}{r}
 65 \\
 48 \\
 \hline
 113
 \end{array}$$

$$\begin{array}{r}
 70 \\
 48 \\
 \hline
 22
 \end{array}$$

ENGINEERING DEPARTMENT  
 CITY OF SAN DIEGO,  
 CALIFORNIA.

$$\begin{array}{r}
 150 \\
 16.3 \\
 2.75 \\
 \hline
 145.75
 \end{array}$$