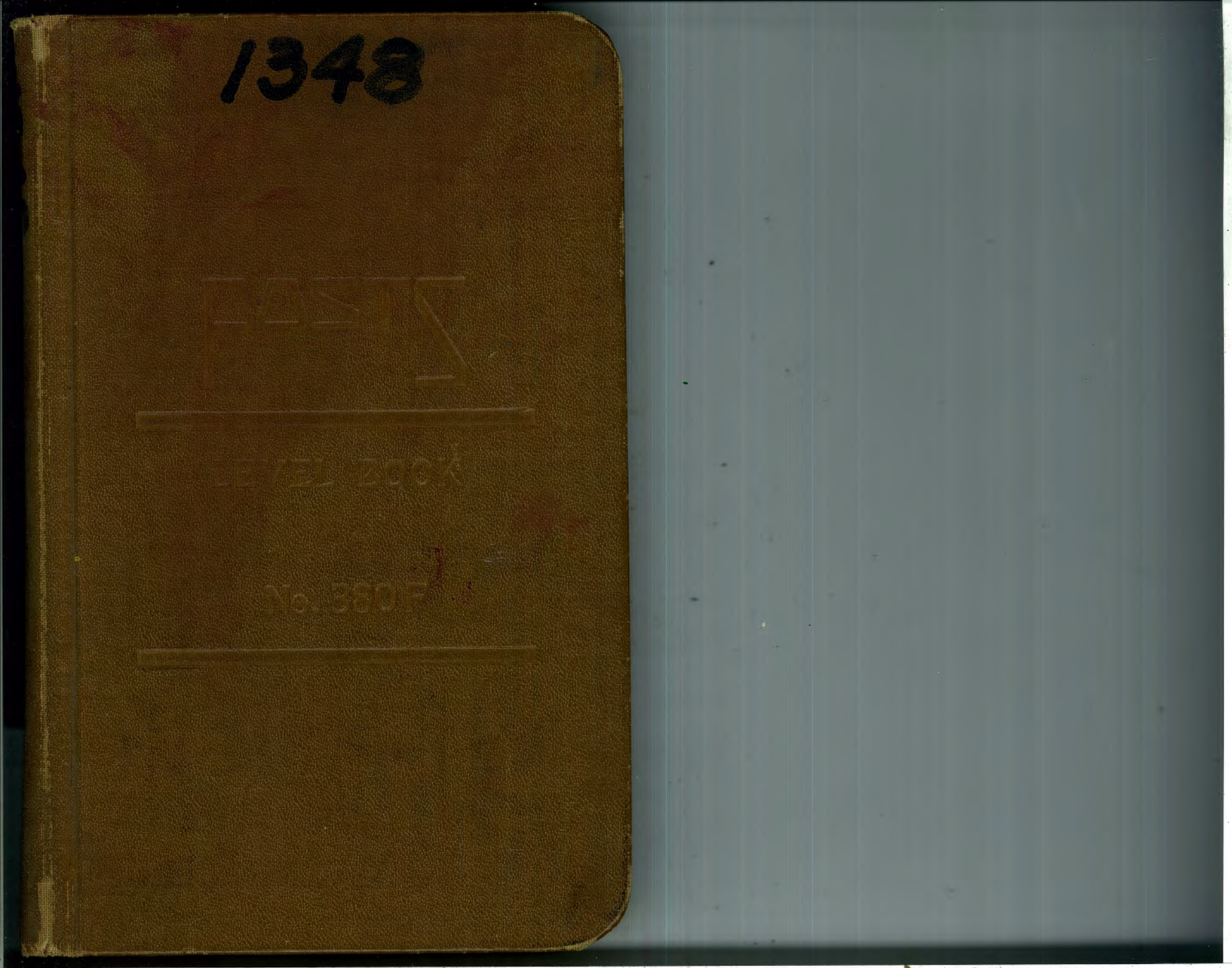

1348

Our Leather Bound Engineers Note Books are carried in the following rulings:

No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.

No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.

No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.

No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

We also carry the Note Books listed above, bound in extra strong Fabri-Hide (otherwise the same quality of book), which can be furnished at a somewhat lower price.

In ordering Fabri-Hide covered books, add the letter *"F"* to catalog number.

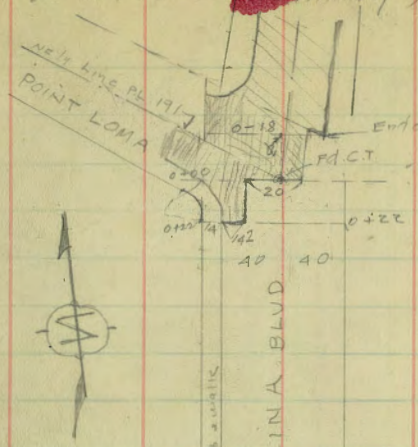
X Sec.	Catalina Blvd. to Military Res.	1
" "	Aztec. Catalina Blvd & Cortez	57
X Sec of	Road Bet. Pts 143 and 104	59
cb	levels. 32nd " Elm.	63
Landis,	Marlborough to 42nd "	65
Alleys	34th Washington Hts	67-71
"	173 University Heights	72
Reset SW cor	Lot 5 Blk 2 Roseorans Park	79

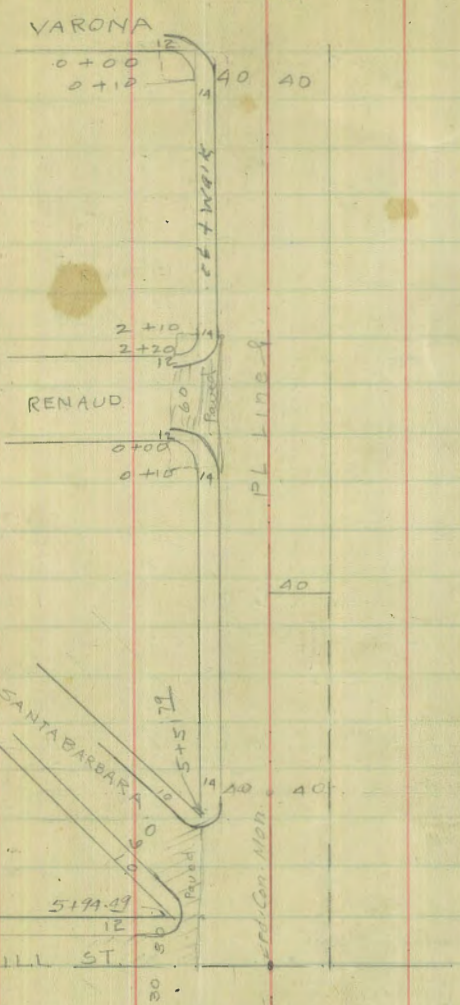
Incumbent 6/30/70 MH

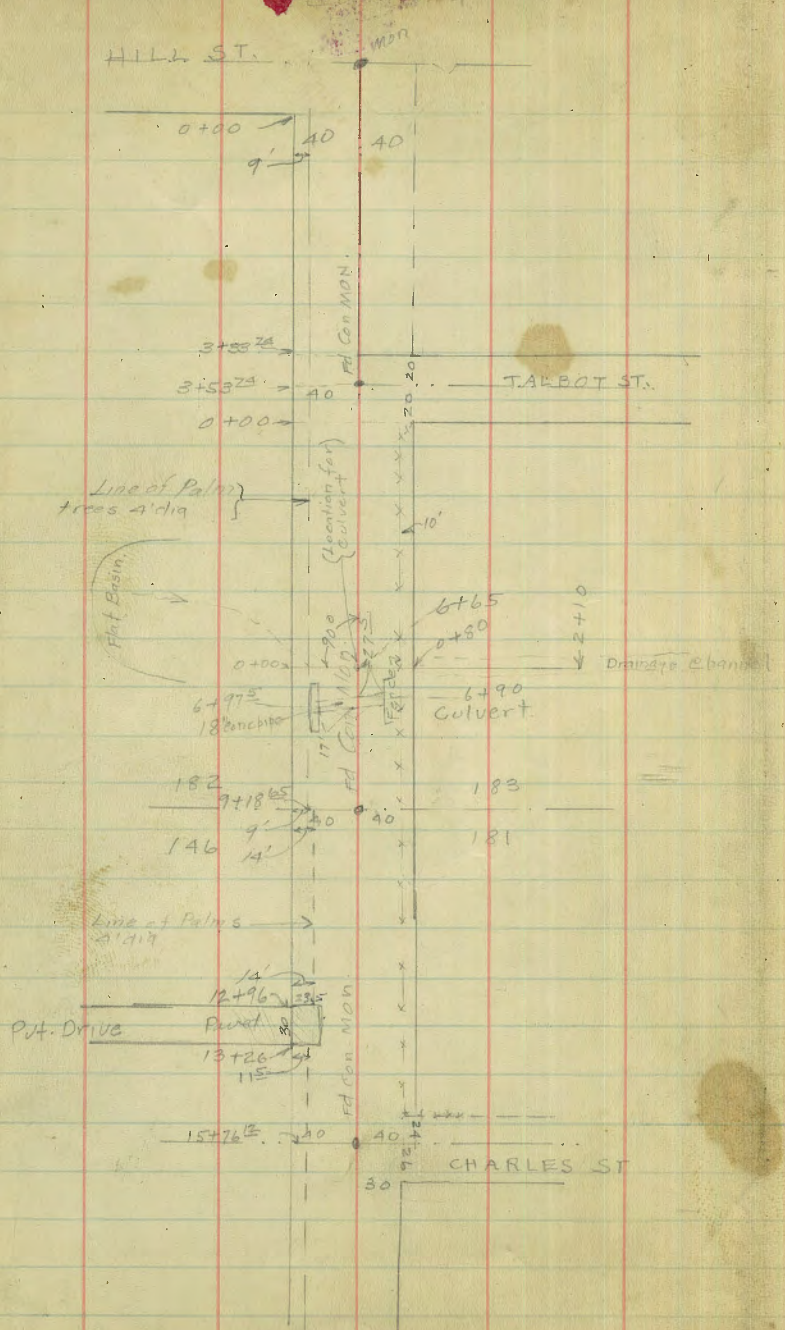
X Section Catalina Blvd from Pt Loma Ave to Military Reservation.

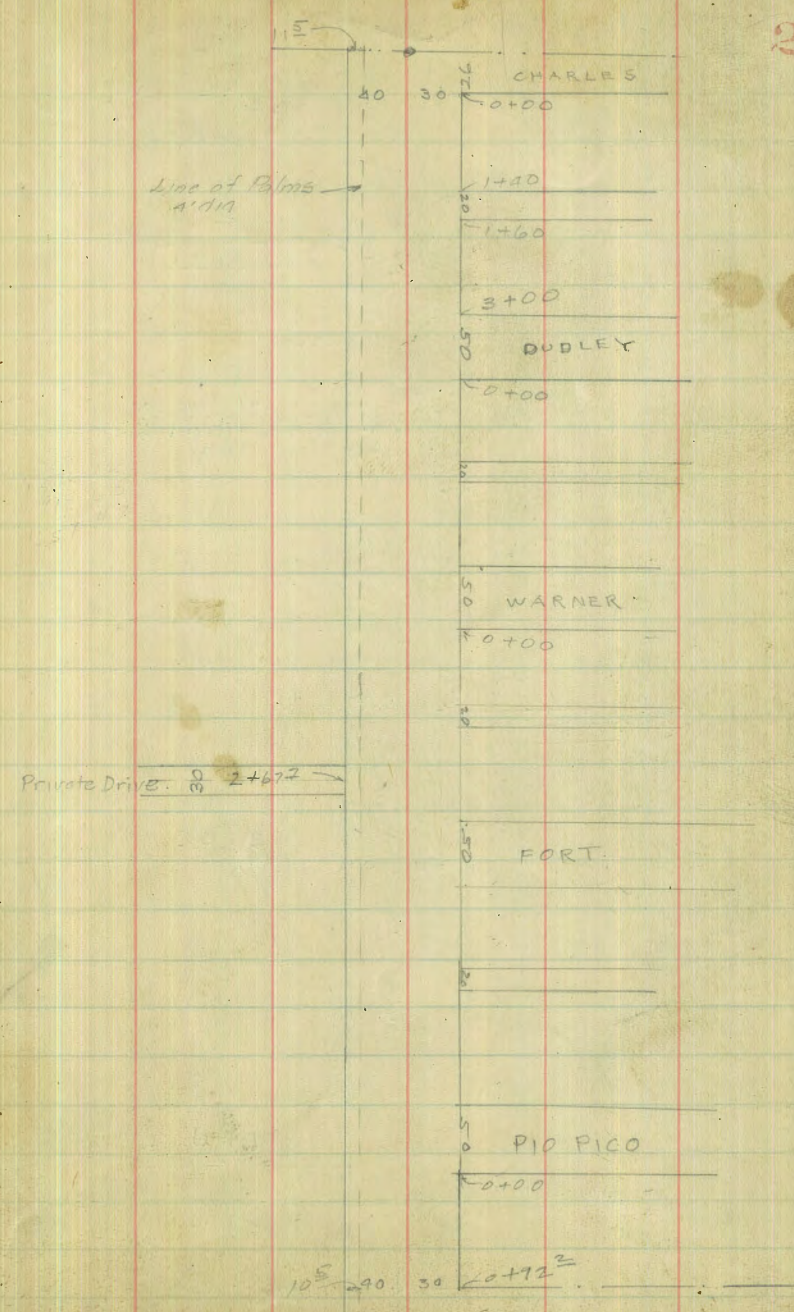
5/21/29
Loudon

1

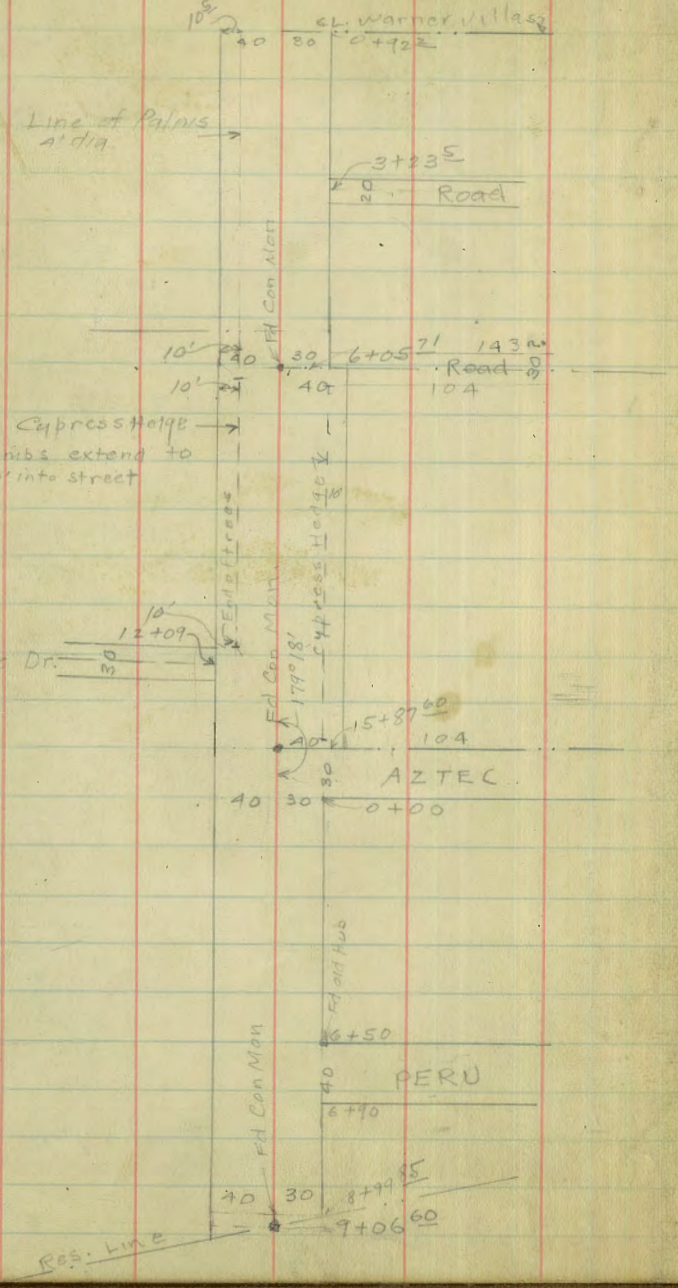





HILL ST.
Mon
0+00
40
9'
40
Fd Con MON
3+53
TALBOT ST.
0+00
Line of Palm trees 4' dia
(Location for Culvert)
10'
Flat Basin
6+65
0+80
2+10
Drainage Channel
0+00
6+97.5
18" conc pipe
6+90
Culvert
182
183
181
146
9'
14'
Line of Palms 4' dia
14'
12+96
Pvt. Drive
Paved
13+26
Fd Con Mon
40
CHARLES ST
30


40
30
CHARLES
0+00
Line of Palms 4' dia
1+40
1+60
3+00
DUDLEY
0+00
WARNER
0+00
Private Drive
2+67.7
FORT
PIO PICO
0+00
0+92.2

Ca. 11/29.



X Sec Catalina Blvd.
70' St 14' cbs 42' Rdway from
40' West of P.L. Line.

BP N.W. La Mirada & Catalina

B.M.	0.87	235.49		234.62
T.P.	5.98	231.15	10.32	225.17
0-18				
10E			12 4	218.7
E.L.			12 2	218.9
+2	+cb Existeb		12 23	218.92
+2	gut Pav		12 87	218.28
cb			12.7	218.4
+45	Pav		12 58	218.57
1/4	Pav		12 31	218.81
E	Pav		12 21	218.94
+4	Pav		12 16	218.99
1/4	Pav		11.80	219.35
cb	Pav		10 91	220.24
+7	Pav.		10 42	220.73
W.L	Pav		9.45	221.70
0+00				
W.L.	Pav		9.46	221.69
cb	Pav		10 29	220.86
1/4	Pav		10 85	220.30
+5	Pav		11.12	220.03
E	Pav		11.70	219.95
1/4	Pav		11.30	219.85
+5	Pav		11.45	219.70
cb			11 7	219.4
+8			11.6	219.5

PLOTTED
JUNE 11, '29
DAVIES

0+00						0+50			
E.L				11.3	219.8	10E		8.4	222.7
10E	true E.L.			11.3	219.8	1+00			
0+02	on scb Pt Loma Ave.					10E		6.9	224.2
W.L	Paw			9.44	221.71	E.L.		6.3	224.8
W.L	to b cb			8.75	222.40	+7		6.3	224.8
0+22 = B.C. S.W. ret.						cb		7.1	224.0
10E	True E.L.			9.9	221.2	¼		6.7	224.4
E.L.				9.9	221.2	℄		6.4	224.7
cb				10.5	220.6	¼		6.9	224.2
¼				10.4	220.7	+5		7.2	223.9
℄				10.0	221.1	g.t		6.2	224.9
+6.5	Paw			9.91	221.24	w.cb		5.70	225.45
¼	Paw			9.89	221.26	1+50			
g.t	Paw			9.79	221.36	w.cb		3.79	227.36
w.cb	to b cb			9.05	222.10	g.t.		4.4	226.7
0+50						+6		5.7	225.4
w.cb		7.80			223.35	¼		5.4	225.7
g.t		8.5			222.6	+5		4.9	226.2
+6		9.2			221.9	℄		4.9	226.2
¼		8.8			222.3	¼		5.1	226.0
+5		8.5			222.6	cb		5.6	225.5
℄		8.6			222.5	+9		5.8	225.3
¼		8.9			222.2	E.L		5.2	225.9
cb		9.2			221.9	10E		4.9	226.2
+7		8.7			222.4				
E.L		8.6			222.5				

2+00					3+00	231.15			
IDE			4.2	226.9	IDE			2.7	228.4
EL			4.3	226.8	EL			2.3	228.8
cb			4.1	227.0	cb			1.8	229.3
¼			3.9	227.2	¼			1.6	229.5
℄			3.5	227.6	℄			1.2	229.9
+6			3.5	227.6	¼			1.3	229.8
¼			3.8	227.3	+6			1.4	229.7
+7			4.0	227.1	gut			0.7	230.4
gut			3.1	228.0	Wcb			0.33	230.82
Wcb			2.34	228.81	TP	7.54	23.9.97	0.72	230.43
2+50					3+50				
Wcb			1.36	229.79	Wcb			6.06	231.91
gut			1.9	229.2	gut			6.1	231.9
+8			2.6	228.5	+5			6.7	231.3
¼			2.6	228.5	¼			7.0	231.0
℄			2.4	228.7	℄			6.9	231.1
¼			2.9	228.2	¼			7.3	230.7
cb			3.2	227.9	cb			7.6	230.4
+8			3.6	227.5	EL			8.1	229.9
EL			3.2	227.9	IDE			8.5	229.5
IDE			3.8	227.3					

4+00	237.97		
10E		7.7	230.3
E.L		7.3	230.7
cb		6.6	231.4
¼		6.3	231.7
℄		5.9	232.1
¼		6.0	232.0
+7		5.8	232.2
gut		5.3	232.7
Wcb		5.06	232.91
4+50			
Wcb		4.30	233.67
gut		4.4	233.6
+7		5.5	232.5
¼		5.3	232.7
℄		5.4	232.6
¼		5.8	232.2
+8		6.1	231.9
cb		5.8	232.2
E.L		6.2	231.8
10E		6.7	231.3

5+00			
10E		5.8	232.2
E.L.		5.5	232.5
cb		5.3	232.7
¼		5.3	232.7
℄		5.0	233.0
¼		4.7	233.3
gut		4.1	233.9
Wcb		3.66	234.31
5+29.37 = B.C. N.W. rat.			
Wcb		3.37	234.60
gut		4.0	234.0
¼		4.5	233.5
℄		4.6	233.4
¼		5.0	233.0
+8		5.2	232.8
cb		5.0	233.0
EL		4.8	233.2
10E		4.7	233.3

5 +39 36 =		237.97			
NL La Paloma					
10E			4.7	233.3	
EL			4.3	233.7	
eb			4.8	233.2	
¼			5.0	233.0	
℄			4.5	233.5	
¼			4.1	233.9	
+5			4.8	233.7	
W eb	Paw		3.95	234.02	
+2	gut		3.89	234.08	
+2	robeb on ret.		3.19	234.78	
BM			3.36	235.45	235.46
N eb La Paloma					
10W	top eb Ec ret.		2.07	235.90	
10W qrt	Paw		2.69	235.28	
WL	Paw		3.21	234.76	
eb	Paw		3.62	234.35	
¼			4.0	234.0	
℄			4.5	233.5	
¼			4.9	233.1	
+8			4.9	233.1	
eb			4.6	233.4	
+5			4.5	233.5	
+9			3.6	234.4	
EL			4.6	233.4	
10E			6.2	231.8	

N ¼ La Paloma				
10E			8.0	230.0
2E			6.8	231.2
EL			5.3	232.7
+1			4.7	233.3
+5			3.5	234.5
eb			4.3	233.7
+3			4.8	233.2
¼			4.9	233.1
℄			4.5	233.5
¼			3.8	234.2
eb	Paw		3.50	234.47
WL	Paw		2.79	235.18
℄ La Paloma				
NL	Paw		2.44	235.53
eb	Paw		3.30	234.67
¼			3.6	234.4
℄			4.5	233.5
¼			4.9	233.1
+9			4.8	233.2
eb			4.5	233.5
+3 5			4.4	233.6
+5			3.1	234.9
+12			4.6	233.4
EL			5.8	232.2
10E			7.5	230.5

S'4 La Palonia 231.97

10E		11.0	227.0
E.L.		10.1	227.9
+3		5.9	232.1
+10		3.8	234.2
+11		4.7	233.3
cb		4.7	233.3
'4		4.9	233.1
℄		4.5	233.5
'4		3.5	234.5
cb		2.5	235.5
w.L.		1.1	236.9
Scb La Palonia			
w.L.		1.0	237.0
cb		2.5	235.5
'4		3.5	234.5
℄		4.5	233.5
'4		4.9	233.1
cb		4.9	233.1
+6		3.7	234.3
E.L.		4.9	233.1
10E		6.9	231.0

237.97

S.L La Palonia = 0+00

10E			5.9	232.1
EL			3.6	234.4
+6			3.2	234.8
+13			4.9	233.1
cb			4.9	233.1
'4			4.8	233.2
℄			4.3	233.7
'4			3.5	234.5
+45			3.7	234.3
+45	+ob Exist cb		2.50	235.47
cb			2.2	235.8
+4	true w.L.		2.1	235.9
w.L.			1.2	236.8
TP	11.97	247.65	2.29	235.68
0+50				
w.L.			8.5	239.1
+8			9.6	238.0
+10	true w.L.		10.4	237.2
+12			11.6	236.0
cb			11.7	235.9
+6	+ob cb		11.88	235.77
+6			12.8	234.8
'4			12.3	235.3
℄			13.0	234.6
'4			13.6	234.0
cb			14.0	233.6

0+50			
+5		13.8	233,8
+6		12.8	234,8
+10		11.8	235,8
E.L		12.4	235,2
10 E		15.6	232,0
1+00			
10E		15.3	232.3
E.L		13.1	234,5
+8		11.7	235,9
+9		11.5	236,1
+9		12.8	234.8
cb		13.0	234.6
¼		12.7	234,9
½		12.2	235,4
¼		11.4	236,2
+45		11.8	235,8
+45	top cb	10.88	236.77
cb		10.8	236,8
+8		10.8	236,8
+4	true w.L.	10.0	237.6
+6		8.4	239,2
w.L.		7.9	239.7

1+50			
w.L		6.8	240.8
+10	true w.L	7.8	239,8
+12		9.8	237,8
cb		9.9	237,7
+6	top cb	9.96	237.69
+6		10.8	236,8
¼		10.7	236,9
½		11.4	236,2
¼		11.8	235,8
cb		11.8	235.8
+8		11.8	235.8
+4		10.5	237,1
+6		10.0	237,6
+13		10.3	237,3
E.L		10.8	236,8
10E		15.0	232,6
2+00			
10E		13.8	233,8
E.L		10.1	237,5
+10		10.4	237,2
cb		10.9	236,7
¼		10.8	236,8
½		10.4	237,2
¼		9.6	238,0
+45		9.9	237,7
+45	top cb	8.65	239.00

2+00			
eb		8.6	239.0
+3		8.4	239,2
+4	true w.L.	7.1	240,5
+6		6.4	241.2
w.L.		5.7	241.9
2+50			
w.L		4.6	243.0
+9		5.6	242.0
+10	true w.L.	7.1	240,5
+11		7.7	239.9
eb		7.9	239,7
+6	top eb	7.88	239.77
+6		8.8	238,8
¼		8.4	239,2
±		9.4	238,2
¼		9.7	237,9
+8		9.8	237,8
eb		8.8	238,8
+10		7.7	239,9
EL		8.8	239,3
16E		9.6	238,0
10E	true E.L.	11.3	236.3

3+00			
10E	true E.L.	9.4	238,2
E.L.		7.7	239,9
+3		6.8	240,8
eb.		8.0	239,6
+n		8.6	239,0
¼		8.4	239,2
±		8.0	239,6
¼		7.3	240,3
+45		7.7	239,9
+45	top eb	6.85	240.80
eb		6.6	241.0
+4	true w.L.	5.9	241,7
+5		4.3	243,3
w.L.		3.4	244.2
3+50			
w.L.		2.0	245,6
+9		2.6	245,0
+10	true w.L.	3.6	244.0
+11		5.0	242,6
eb		5.2	242,4
+6	top eb	5.35	242,30
+6		6.4	241,2
¼		5.9	241.7
±		6.5	241,1
¼		6.9	240,7
+9		7.1	240,5

3+50	247.65			
cb			6.3	241,3
+5			6.5	241.1
+8			5.6	242,0
E.L.			5.5	242,1
10E			6.8	240,8
4+00				
10E			5.4	242,2
E.L.			4.7	242,9
+8			5.3	242,3
+8			7.7	239,9
+10			6.0	241,6
cb			5.7	241,9
1/4			5.3	242,3
E			5.0	242,6
1/4			4.6	243,0
+45			5.0	242,6
+45	top cb		3.89	243.76
cb			3.8	243,8
T.P.	9.59	257.19	0.25	247.60
+2			13.2	244,0
+4	true w.L.		11.9	245,3
+7			10.6	246,6
w.L.			10.1	247.1

4+50	257.19			
w.L.			8.5	248,7
+8			9.0	248,2
+10	true w.L.		10.4	246,8
+12			11.9	245,3
cb			12.0	245,2
+6	top cb		11.87	245,32
+6			12.9	244,3
1/4			12.8	244,4
E			13.1	244,1
1/4			13.4	243,8
cb			13.6	243.6
+8			13.6	243,6
+4			15.3	241,9
+5			13.4	243,8
E.L.			13.3	243,9
10E			13.4	243,8
5+00				
10E			12.0	245,2
EL			11.8	245,4
+8			12.2	245,0
+8			13.4	243,8
+10			12.2	245.0
cb			12.2	245,0
1/4			11.9	245,3
E			11.6	245,6
1/4			11.2	246.0

5+00			
+45		11.4	245,8
+45 top eb		10.20	246,99
eb		10.4	246,8
+3		10.4	246,8
+4 true w.L.		9.0	248,2
+5		7.6	249,6
w.L.		7.1	250,1
5+50			
w.L		5.4	251,8
+9		6.1	251,1
+10 true w.L.		7.0	250,2
+11		8.6	248,6
eb		8.8	248,4
+6 top eb		8.59	248.60
+6		9.9	247,3
1/4		9.7	247,5
E		10.2	247.0
1/4		10.5	246,7
eb		11.0	246,2
+6		11.6	245,6
+7		10.2	247.0
E.L.		10.1	247,1
5 E		10.0	247,2
7 E		9.4	247,8
10 E		10.0	247.2

6+00 31 = N.L. Varona.			
10E		9.8	247,4
E.L.		8.7	248.5
+11		9.2	248,0
+12		10.0	247.2
eb		9.7	247,5
1/4		9.2	248,0
E		8.7	248,5
1/4		8.2	249,0
+45		8.1	249,1
+45 top eb		7.11	250.08
eb		6.8	250,4
+4 true w.L.		6.5	250,7
w.L.		3.9	253,3
N.L. Varona +10			
w.L. top Exist eb		6.05	251,14
+10 true w.L. top Exist eb		6.91	250,28
N eb Varona			
w.L.		6.0	251,2
+10		6.8	250,4
eb		7.2	250,0
1/4		7.7	249,5
E		8.4	248,8
1/4		8.9	248,3
eb		9.4	247.8
+3		9.5	247,7
+4		8.7	248.5

Xcb Varona			
E.L.		8.3	248,9
10E		9.5	247,7
N ¼ Varona			
10E		9.0	248.2
EC.		8.0	249.2
+10		8.5	248,7
+10		9.2	248.0
cb		9.1	248.1
¼		8.8	248.4
±		8.2	249.0
¼		7.5	249.7
cb		7.0	250,2
W.L.		5.9	251,3
± Varona			
W.L.	Paw	5.90	251,29
cb	Paw	7.33	249.86
¼		7.5	249,7
±		8.0	249,2
¼		8.4	248.8
cb.		8.7	248.5
+8		8.8	248.4
+4		8.2	249.0
E.L.		7.9	249.3
10E		9.2	248.0

S ¼ Varona			
10E		9.8	247.4
E.L.		8.2	249,0
+10		7.9	249.3
+11		8.5	248,7
cb		8.5	248,7
¼		8.2	249,0
±		7.9	249.3
¼		7.4	249,8
cb	Paw	7.19	250.00
W.L.	Paw	6.09	251.10
S cb Varona			
12W	EC. SW ret gut	5.05	252.14
12W	+ob cb	4.44	252,75
W.L.	Paw	6.22	250,97
cb	Paw	7.25	249.94
¼		7.1	250,1
±		7.7	249,5
¼		7.8	249,4
cb		8.2	249,0
+8		8.2	249,0
E.L.		7.7	249,5
1E		8.5	248.7
5E		8.5	248,7
10E		9.9	247.3

S.L Varona = 0+00			
10 E	9.8	247,4	
5 E	8.2	249.0	
E.L.	8.1	249,1	
+1	7.3	249,9	
+10	7.4	249,8	
cb	7.8	249,4	
¼	7.5	249,7	
±	7.3	249,9	
¼	6.9	250,3	
cb Pav	7.20	249,99	
+25 gut	7.15	250,04	
+25 top cb on ret	6.65	250.54	
WL wall c	5.68	251,51	
0+10 = B.C. sw. ret			
wcb	6.45	250.74	
gut Pav	7.03	250.16	
¼	6.7	250,5	
±	7.0	250,2	
¼	7.2	250,0	
cb	7.6	249,6	
+4	7.3	249,9	
+11	7.3	249,9	
E.L.	7.7	249.3	
10 E	9.6	247,6	

0+60	257.19		
10 E	7.7	249,3	
E.L.	6.6	250,6	
+10	5.8	251,4	
cb	6.5	250,7	
¼	6.1	251,1	
±	5.7	251,5	
¼	6.1	251,1	
gut	5.6	251.6	
wcb	5.15	252,04	
B.M. sw catalina & Varona			
B.M. 10.09 260.91	6.40	250.79	(250.82)
1+10			
wcb	7.64	253,27	
gut	8.3	252,6	
¼	8.4	252,5	
±	8.3	252,6	
¼	8.5	252,4	
cb	8.7	252,2	
+1	8.5	252,4	
E.L.	8.5	252,4	
10 E	9.5	251,4	

1+60			
10E		7.7	253.2
E.L.		7.1	253,8
cb		7.7	253,2
¼		7.6	253,3
±		7.3	253,6
¼		7.5	253.4
qvt		7.5	253,4
wcb		6 3/4	254,57
2+10			
wcb		5.18	255.73
qvt	Paw	5.86	255.05
¼		6.5	2544
±		6 3	254,6
¼		6.6	254,3
cb		6.9	254,0
+6		6.6	254,3
E.L.		5.8	255,1
10E		6.7	254.2

2+20 = N.L. Renaud.			
10E		6.1	254,8
E.L.		5.7	255,2
+6		6.4	254,5
cb		6.8	254,1
¼		6.5	254,4
±		6.1	254,8
¼		6 2	254,7
cb	Paw	5.56	255.35
+2⁴	qvt	5.37	255,54
+2⁴	top cb on ret.	4.72	256,19
Scb Renaud.			
8W	top cb EC. NW ret.	2.84	258,07
8W	qvt	3.42	257,49
Int of W.L. & N.W. ret.	qvt	4.17	256.74
	top cb on ret	3.51	257.40
W.L.	Paw	4.13	256.78
cb	Paw	5.24	255.67
¼		5.7	255.2
±		5.9	255.0
¼		6.3	254,6
cb		6.6	254,3
+5		6.3	254,6
+12		5.2	255,7
E.L.		5.4	255.5
10E		6.1	254,8

X¼ Renaud

10E		5.9	255.0
EL		5.5	255.4
+7		5.5	255.4
+10		6.4	254.5
cb		6.4	254.5
¼		6.2	254.7
℄		5.8	255.1
¼		5.5	255.4
cb	Pav	5.01	255.90
W.L.	Pav.	3.85	257.06

℄ Renaud.

W.L.	Pav	3.62	257.29
cb	Pav	4.89	256.02
¼		5.4	255.5
℄		5.7	255.2
¼		6.1	254.8
cb		6.3	254.6
+5		5.9	255.0
+7		5.6	255.9
E.L.		4.9	256.0
10E		5.8	255.1

S¼ Renaud.

10E		5.6	255.3
E.L.		5.7	255.2
cb		6.2	254.7
¼		6.0	254.9
℄		5.6	255.3
¼		5.3	255.6
cb	Pav	4.83	256.08
W.L.	Pav.	3.62	257.29

Sch Renaud.

8'W	+ob cb EC sw ret	2.31	258.60
8W	gut	2.95	257.96
W.L.		3.72	257.19
Int. of W.L. &	gut	3.71	257.20
S.W. ret	+ob cb	3.08	257.83
cb	Pav	4.81	256.10
¼		5.1	255.8
℄		5.4	255.5
¼		5.7	255.2
cb		5.9	255.0
E.L.		5.1	255.8
10E		5.6	255.3

S.L. Renaud = 0+00

10E		5.5	255,4
E.L.		5.1	255,8
+6		5.0	255,9
+8		5.5	255,4
cb		5.7	255,2
¼		5.5	255,4
℄		5.2	255,7
¼		5.1	255.8
cb	Paw	4.80	256.11
+23	gut	4.75	256.16
+23	top cb on sw. ret.	4.16	256.75
0+10 = B.C. sw ret.			
wcb		4.10	256,81
gut	Paw	4.74	256.17
¼		5.0	255,9
℄		5.0	255,9
¼		5.3	255,6
+9		5.5	255,4
cb		5.1	255.8
+5		5.5	255,4
E.L.		4.8	256,1
10E		4.9	256.0

0+50

10E		4.2	256,7
5E		4.7	256,2
E.L.		4.0	256,9
+10		4.6	256,3
cb		4.5	256,4
+1		4.8	256,1
¼		4.6	256,3
℄		4.3	256,6
¼		4.3	256,6
+6		4.7	256,2
gut		4.6	256,3
Wcb		3.52	257,39
1+00			
Wcb		2.71	258,20
gut		3.4	257,5
¼		3.5	257,4
℄		3.5	257.4
¼		3.8	257.1
+8		3.9	257,0
cb		3.4	257,5
+5		3.7	257.2
E.L.		3.1	257.8
10E		3.5	257.4

1+50	260.91			
10E			2.8	258,1
E.L			2.4	258,5
+5			2.7	258.2
+10			3.4	257,5
cb			2.8	258,1
+2			3.3	257,6
¼			3.0	257.9
℄			2.8	258,1
¼			2.8	258,1
gut			2.4	258,5
web			1.93	258,98
2+00				
web			1.17	259,74
gut			1.9	259,0
¼			2.2	258,7
℄			2.2	258.7
¼			2.4	258,5
+8			2.6	258.3
cb			2.3	258,6
E.L			2.3	258,6
10E			2.3	258,6
T.P.	2.78	263.52	0.17	260.74

2+50	263.57			
web			3.32	260,20
gut			3.4	260,1
+3			4.8	258,7
¼			4.5	259,0
℄			4.4	259,1
¼			4.6	258,9
+8			4.7	258,8
cb			4.1	259,4
+4			4.6	258,9
E.L			4.0	259,5
10E			4.3	259,2
3+00				
10E			3.7	259,8
E.L			3.3	260,2
+10			4.2	259,3
cb			3.8	259,7
+2			4.5	259,0
¼			4.5	259,0
℄			4.3	259,2
+5			4.3	259,2
¼			4.6	258,9
+5			5.0	258,5
+1			4.3	259,2
gut			3.6	259,9
web			3.39	260.13

3+50			
web	3.72	259.80	
gut	3.7	259,8	
+2	4.7	258,8	
+4	5.0	258,5	
¼	4.6	258,9	
¢	4.5	259.0	
¼	4.7	258,8	
+8	4.8	258,7	
eb	4.2	259.3	
+4	4.8	258,7	
+9	3.9	259,6	
E.L.	4.2	259,3	
10E	4.0	259.5	
4+00			
10E	3.9	259,6	
7E	4.6	258,9	
E.L.	4.5	259,0	
+5	4.5	259.0	
+11	5.0	258,5	
eb	4.4	259,1	
+2	5.2	258,3	
¼	5.1	258,4	
¢	4.8	258.7	
¼	49	258.6	
+7	5.2	258,3	
+9	5.1	258.4	

4+00		
gut	4.5	259.0
Web	4.05	259.47
4+50		
Web	4.36	259.16
gut	4.7	258.8
+2	5.3	258.2
¼	5.2	258,3
¢	5.2	258,3
¼	5.4	258,1
+9	5.5	258,0
eb	4.6	258,9
+3	5.4	258,1
+9	4.6	258.9
E.L.	4.6	258,9
10E	4.7	258.8
5+00		
10E	5.3	258,2
E.L.	4.6	258,9
+5	4.7	258,8
+11	5.5	258,0
eb	5.1	258,4
+15	5.7	257,8
¼	5.6	257,9
¢	5.5	258,0
¼	5.3	258,2

5+00			
+6		5.1	258,4
+8		5.4	258,1
gut		5.2	258,3
web		4.66	258.86
5+51.2I = N'/4 line		Santa Barbara	
W.L. + B	top eb on ret.	4.50	259.07
	gut	4.5	259.0
		4.4	259,1
eb		5.1	258,4
1/4		5.4	258,1
℄		5.7	257,8
1/4		5.8	257.7
+9		5.1	258,4
eb		5.6	257,9
+1		5.7	257,8
+10		5.1	258,4
EL		6.3	257,2
10E			
5+60.2 = Int w.L. =		N.W. ret to Santa Bar.	
10E		6.4	257,1
4E		6.3	257,2
E.L.		5.4	258,1
+5		5.1	258,4
+13		5.7	257.8
eb		5.2	258,3
+2		5.8	257.7

5+60.2			
1/4		5.8	257,7
℄		5.2	258,1
1/4		5.0	258.5
eb		4.6	258,9
W.L.	Pav	4.17	259,35
W.L.	top eb	3.62	259,90
5+94.9 = N.L. - Hill 5+			
W.L.	Pav	4.51	259,01
eb		4.3	259,2
1/4		4.7	258,8
℄		5.3	258,2
1/4		5.8	257,7
eb		6.0	257.5
+5		5.4	258,1
EL		5.5	258,0
10E		6.4	257,1
Neb Hill			
10E		6.6	256,9
EL		5.5	258.0
+9		5.4	258,1
+11		6.1	257,4
eb		6.0	257,5
1/4		5.9	257,6
℄		5.3	258,2
1/4		4.8	258,7
+5		4.6	258,9

Neb Hill.			
eb		4.8	258,7
W.L	Paw	4.78	258.74
N ¼ Hill			
W.L	Paw	5.17	258.35
eb		5.2	258,3
¼		4.9	258,6
℄		5.3	258,2
¼		5.9	257,6
eb		6.0	257,5
+4		6.1	257,4
+5		5.3	258,2
EL		5.5	258,0
10.E		6.1	257,4
℄ Hill.			
10E		5.9	257,6
E.L.		5.5	258,0
+9		5.4	258,1
+10		6.2	257,3
eb		6.1	257.4
¼		5.9	257,6
℄		5.4	258,1
+6		5.3	258.2
¼		5.8	258,2
eb		5.4	258,1
+10		5.2	258,3
W.L.	Paw	5.45	258.07

S ¼ Hill			
W.L		5.1	258,4
+7		5.2	258,3
eb		5.6	257,9
¼		5.6	257,9
℄		5.5	258,0
+5		5.5	258,0
¼		5.9	257,6
eb		6.1	257,4
+3		6.3	257,2
+4		5.8	257,7
+6		5.4	258,1
EL		5.5	258,0
7E		5.7	257,8
10E		6.5	257,0
S eb Hill			
10E		5.2	258,3
4E		7.1	256,4
EL		5.5	258,0
+10		5.6	257,9
+11		6.4	257,1
eb		6.2	257,3
¼		5.9	257.6
+5		5.6	257,9
℄		5.6	257,9
¼		5.6	257,9
eb		5.5	258.0

Sch Hill			
+4	5.3	258,2	
WL	5.0	258,5	
SL Hill = 0+00			
WL	5.4	258,1	
ch	5.4	258,1	
1/4	5.9	257,6	
±	5.8	257,7	
1/4	5.9	257,6	
ch	6.3	257,2	
+2	6.3	257,2	
+4	5.5	258.0	
EL	5.5	258,0	
10E	6.1	257.4	
0+50			
10E	5.9	257,6	
EL	5.5	258,0	
+12	5.6	257.9	
+13	6.3	257.2	
ch	6.3	257.2	
1/4	6.2	257,3	
±	6.1	257.4	
1/4	5.7	257,8	
+5	5.9	257,6	
ch	5.7	257,8	
WL	5.4	258,1	

1+00	263.52				
WL			5.5	258.0	
ch			5.6	257.9	
1/4			5.9	257,6	
±			6.1	257.4	
1/4			6.2	257,3	
ch			6.3	257,2	
+2			6.3	257,2	
+5			5.3	258,2	
EL			4.8	258,7	
10E			5.6	257,9	
1+50					
10E			5.3	258,2	
3E			5.2	258,3	
EL			4.4	259,1	
+5			4.6	258,9	
+11			5.4	258,1	
+13			6.1	257.4	
ch			6.1	257.4	
1/4			6.0	257.5	
±			5.9	257,6	
1/4			5.8	257,7	
ch			5.4	258,1	
WL			5.2	258,3	
BP NW Corp line Santa Barbara					
BM			2.86	260.66	(260.68)
	263.54				
TP	8.67	266.07	6.14	257.40	

2+00	266.07		
W.L.		7.3	258.8
eb		7.6	258,5
¼		7.9	258,2
℄		8.1	258,0
¼		8.2	257,9
eb		8.1	258,0
+2		8.1	258,0
+3		7.5	258,6
EL		6.7	259,4
10E		6.8	259,3
2+50			
10E		6.5	259,6
EL		6.1	260,0
+6		5.8	260,3
+9		7.6	258,5
eb		7.6	258,5
¼		7.2	258,9
℄		7.0	259,1
¼		6.9	259,2
eb		7.2	258,9
W.L.		7.2	258,9

3+00			
W.L.		5.8	260.3
eb		5.9	260,2
¼		5.7	260,4
℄		5.9	260,2
¼		5.9	260,2
eb		5.8	260,3
EL		5.9	260,2
10E		6.1	260,0
3+33.74 = NL Talbot.			55+46.32
10E		5.2	260,9
EL		5.1	261.0
eb		4.9	261,2
¼		5.0	261.1
℄		5.0	261.1
¼		4.9	261,2
eb		5.1	261.0
W.L.		5.0	261.1
3+53.74 = ℄ Talbot.			55+46.32
W.L.		4.5	261,6
eb		4.7	261.4
¼		4.6	261,5
℄		4.8	261,3
¼		4.7	261.4
eb		4.7	261.4
EL		4.8	261,3
10E		5.1	261.0

3+73 24 = 0+00 = S.L. Talbot. 55+26.3 32		
10E	5.6	260.5
E.L.	5.2	260.9
cb	4.8	261.3
¼	4.9	261.2
℄	5.0	261.1
¼	5.2	260.9
+6	4.5	261.6
cb	4.4	261.7
W.L.	4.0	262.1
0+50	54+76 32	
W.L.	4.1	262.0
cb	4.5	261.6
¼	5.8	260.3
℄	6.2	259.9
¼	6.1	260.0
cb	6.5	259.6
+11	7.0	259.1
E.L.	6.2	259.9
10E	6.3	259.8

1+00		
10E	8.1	258.0
E.L.	7.8	258.3
+3	8.6	257.5
+8	7.8	258.3
+10	8.4	257.7
cb	8.2	257.9
¼	7.9	258.2
℄	7.9	258.2
¼	7.7	258.4
Cb	6.1	260.0
W.L.	5.4	260.7
1+50	53+76 32	
W.L.	7.7	258.4
cb	8.0	258.1
¼	9.6	256.5
℄	9.9	256.2
¼	9.8	256.3
cb	10.0	256.1
+4	10.1	256.0
+5	9.5	256.6
+11	10.6	255
E.L.	9.9	256.2
10E	10.0	256.1

24
54+26 32

2+00				53+26 32	2+50	266.07			52+76 32
10E			12.8	253,3	10E			14.1	252.0
EL			12.1	254,0	T.P.	0.40	258.52	12.95	253.12
+5			12.1	254.0	3+00				52+26 32
+10			11.1	255,0	10E			2.5	251.0
+11			12.0	254,1	EL			2.2	251.3
cb			11.9	254,2	+4			2.6	250.9
¼			11.7	254,4	+11			1.4	252,1
℄			11.8	254,3	+12			2.3	251.2
+5			11.9	254,2	cb			2.3	251,2
¼			11.6	254,5	¼			2.2	251,3
cb			10.9	255,2	℄			2.4	251,1
w.L.			10.3	255,8	+6			2.5	251.0
2+50				52+76 32	+7			2.1	251,4
w.L			12.8	253,3	¼			2.2	251.3
+10			12.6	253,5	cb			2.4	251,1
cb			13.1	253,0	w.L			2.3	251,2
¼			13.2	252,9	3+50				51+76 32
+8			13.1	253,0	w.L.			3.5	250.0
+5			13.7	252,4	cb			3.7	249,8
℄			13.5	252,6	+8			3.8	249,7
¼			13.4	252,7	¼			3.5	250,0
cb			13.6	252,5	+3			3.2	250.3
+2			13.6	252.5	+5			3.8	249.7
+4			12.7	253,4	℄			3.7	249.8
+9			13.6	253,5	¼			3.4	250.1
EL			13.6	253,5	cb			3.5	250.0

3+50	25352			51476 32
+15		3.4	250,1	
+25		2.8	250,7	
+7		3.1	250.4	
+10		3.7	249,8	
E.L.		3.3	250,2	
10E		3.3	250,2	
4+00				51+26 32
10E		3.6	249,9	
EL		3.6	249,9	
+4		4.7	248,8	
+8		4.2	249.3	
+13		4.1	249,4	
cb		4.7	248,8	
1/4		4.6	248,9	
℄		4.8	248.7	
+1		4.9	248.6	
+8		4.4	249.1	
1/4		4.5	249,0	
+3		4.6	248,9	
cb		4.0	249.5	
W.L.		4.2	249.3	

4+50			50+76 32
W.L.	4.4	249.1	
cb	4.6	248,9	
1/4	5.7	247.8	
+3	5.6	247,9	
+4	6.1	247,4	
℄	5.8	247.7	
1/4	5.6	247,9	
cb	5.8	247,7	
+2	5.8	247,7	
+3	5.1	248,4	
+11	5.5	248,0	
EL	4.0	249,5	
10E	3.7	249,8	
5+00			50+26 32
10E	4.4	249,1	
EL	5.5	248,0	
+3	6.6	246,9	
+12	6.1	247,4	
+13	6.8	246.7	
cb	6.8	246.7	
1/4	6.8	246.7	
℄	7.0	246.5	
+7	7.1	246,4	
+8	6.6	246,9	
1/4	6.8	246,7	
cb	5.5	248.0	

5+00			50+26 32
+4	5.0	248.5	
W.L.	5.0	248.5	
5+50			49+76 32
W.L.	6.5	247.0	
+10	6.6	246.9	
e b	7.0	246.5	
1/4	7.9	245.6	
+2	7.9	245.6	
+3	8.3	245.2	
E	8.2	245.3	
1/4	7.9	245.6	
c b	7.9	245.6	
+1	7.9	245.6	
+2	7.2	246.3	
+5	7.3	246.2	
+11	8.0	245.5	
E L	7.0	246.5	
10 E	7.0	246.5	

6+00			27
			49+26 32
10E	8.9	244.6	
EL	8.9	244.6	
+4	9.0	244.5	
+7	8.2	245.3	
c b	8.0	245.5	
+1	9.0	244.5	
1/4	9.1	244.4	
E	9.3	244.2	
+7	9.3	244.2	
+8	8.9	244.6	
1/4	9.1	244.4	
+7	8.9	244.6	
e b	9.1	244.4	
W L	9.1	244.4	
6+50			49+76 32
W L	8.6	244.9	
e b	9.2	244.3	
1/4	9.7	243.8	
+3	9.6	243.9	
+4	10.0	243.5	
E	9.9	243.6	
1/4	10.0	243.5	
+9.5	9.8	243.7	
c b	9.2	244.3	
+1	9.1	244.4	

	6+50	253.52			48+76 32
E.L			10.0	243,5	
10E			11.0	242,5	
	7+00				48+26 32
10E			10.9	242,6	
E.L			10.9	242,6	
+11			9.3	2447	
cb			9.3	244,2	
+1			10.0	243,5	
¼			9.8	243,7	
℄			9.8	243,7	
¼			10.0	243,5	
cb			9.5	244,0	
W.L			9.2	244,3	
XTP.	6.82	250.57	9.77	243.75	
	7+50				47+76 32
W.L			5.7	244,9	
cb			6.0	244,6	
¼			6.6	244.0	
℄			6.7	243,9	
¼			6.7	243,9	
+9			6.9	243.7	
+10			6.1	244,5	
cb			6.1	244.5	
+2			6.8	243.8	
+7			6.8	243.8	
E.L			6.4	244,2	

	7+50	250.57			47+76 32
10E			7.3	243.3	
	8+00				47+26 32
10E			6.4	244,2	
EL			6.0	244,6	
+9			6.0	244,6	
cb			5.5	245,1	
+2			5.0	245,6	
+8			6.1	244,5	
¼			6.1	244,5	
℄			6.3	244,3	
+4			6.4	244,2	
¼			6.0	244,6	
cb			5.5	245,1	
WL			5.2	245,4	
	8+50				46+76 32
W.L			4.2	246,4	
cb			4.6	246,0	
¼			4.9	245,7	
+6			5.4	245,2	
℄			5.3	245,3	
¼			5.1	245,5	
+7			5.0	245,6	
+8			4.1	246,5	
cb			4.2	246,4	
+5			4.5	246,1	
+10			5.2	245,4	

8+50				46+76 32			250.57			
E.L		4.7	245.9		T.R	12.82	263.10	0.30	250.27	
10E		4.7	245.9		10+00					45+26 32
9+00				46+26 32	10E			11.4	251.7	
10E		3.7	246.9		E.L			12.1	251.0	
E.L.		3.7	246.9		+10			12.5	250.6	
+5		4.1	246.5		+12			12.1	251.0	
+9		3.3	247.3		+13			12.8	250.3	
cb		3.1	247.5		cb			12.8	250.3	
+½		2.9	247.7		¼			12.8	250.3	
+3		2.9	246.7		±			13.0	250.1	
¼		3.8	246.8		+8			13.2	249.9	
±		3.8	246.8		¼			12.9	250.2	
+6		3.9	246.7		cb			11.6	251.5	
¼		3.4	247.2		W.L			11.8	251.3	
cb		2.9	247.7		10+50					44+76 32
W.L.		3.2	247.4		W.L			10.9	252.2	
9+50				45+76 32	cb			10.4	252.7	
W.L		0.2	250.4		¼			11.2	251.9	
cb		+0.4	251.0		±			11.1	252.0	
¼		2.0	248.6		¼			11.0	252.1	
±		2.0	248.6		Cb			11.1	252.0	
¼		2.1	248.5		+½			11.1	252.0	
+9E		2.9	247.7		+3			10.4	252.7	
cb		1.4	249.2		+11			11.5	251.6	
E.L		1.4	249.2		E.L			9.8	253.3	
10E		0.9	249.7		10E			9.8	253.3	

11+00	263.10			44+26 32
10E		8.0	255.1	
E.L.		8.0	255.1	
+4		9.6	253,5	
+8		8.6	254,5	
+10		8.4	254.7	
+11		9.1	254.0	
cb		9.1	254.0	
1/4		8.9	254,2	
℄		9.0	254,1	
1/4		9.1	254.0	
+5		8.3	254.8	
cb		8.4	254.7	
W.L.		8.8	254.3	
11+50				43+76 32
W.L		6.9	256,2	
cb		6.5	256.6	
1/4		7.2	255.9	
℄		7.1	256,0	
1/4		7.0	256.1	
cb		7.0	256.1	
+8		6.7	256,4	
+10		7.5	255.6	
E.L		5.8	257.3	
10E		5.6	257,5	

12+00			43+26 32
10E		4.2	258,9
E.L		4.2	258.9
+8		5.5	257.6
cb		5.5	257,6
1/4		5.4	257,7
℄		5.6	257,5
1/4		5.9	257.2
cb		5.7	257,4
W.L.		6.3	256,8
12+50			42+76 32
W.L		5.3	257,8
cb		4.9	258.2
1/4		4.5	258,6
℄		4.4	258,7
1/4		4.1	259,0
cb		4.1	259,0
+8		4.0	259.1
+11		4.5	258,6
E.L		2.7	260,4
10E		2.1	261.0

12+96 = 263.10 XL Put. Drive to Theosophical 42+30. 32

10E			1.2	261.9
EL			2.0	261.1
+5			3.0	260.1
cb			2.9	260.2
1/4			2.9	260.2
±			3.1	260.0
1/4			3.3	259.8
+1	Paw		3.39	259.71
cb	Paw		3.55	259.55
WL	Paw		3.77	259.33

13+11 = ± Put Drive. 42+15 32

WL	Paw		3.58	259.52
cb	✓		3.28	259.82
+9 5	Paw		3.03	260.07
1/4			3.0	260.1
±			2.8	260.3
1/4			2.5	260.6
cb			2.6	260.5
+9			2.3	260.8
EL			1.9	261.2
10E			1.4	261.7

13+26 = ± Put Drive 42+00 32

10E			1.1	262.0
EL			1.6	261.5
+5			2.2	260.9
+9			2.0	261.1
cb			2.4	260.7
1/4			2.3	260.8
±			2.5	260.6
1/4			2.7	260.4
+1	Paw		2.81	260.29
cb	Paw		3.13	259.97
WL	Paw		3.68	259.42

13+50 41+76 32

WL			2.6	260.5
cb			2.6	260.5
1/4			2.5	260.6
±			2.2	260.9
1/4			2.0	261.1
cb			1.8	261.3
+5			1.5	261.6
+10			2.0	261.1
EL			1.0	262.1
10E			0.5	262.6

14+00	263.10			41+26.32	
10E			+0.2	263.3	
EL			+0.2	263.3	
+3			1.4	261.7	
+9			0.6	262.5	
+11			1.0	262.1	
cb			1.0	262.1	
1/4			1.1	262.0	
℄			1.4	261.7	
1/4			1.8	261.3	
cb			1.7	261.4	
w.L.			2.0	261.1	
14+50				40+76.32	
w.L.			1.3	261.8	
cb			1.0	262.1	
1/4			0.8	262.3	
℄			0.5	262.6	
1/4			0.3	262.8	
cb			0.1	263.0	
+2			0.0	263.1	
+4			+0.4	263.5	
+9			0.2	262.9	
+13			0.1	263.0	
EL			+1.1	264.2	
10E			+1.1	264.2	
T.P.	8.28	271.20	0.18	262.92	

15+00	271.20			40+26.32	
10E			6.6	264.6	
EL			6.6	264.6	
+3			7.7	263.5	
+8			7.6	263.6	
+10			7.1	264.1	
+12			7.1	264.1	
cb			7.5	263.7	
1/4			7.7	263.5	
℄			7.9	263.3	
1/4			8.2	263.0	
+4			8.0	263.2	
cb			8.6	262.6	
+10			9.3	261.9	
w.L.			8.9	262.3	
15+52.12 = N.L. Charles				39+74.20	
w.L.			8.0	263.2	
+5			8.3	262.9	
cb			7.8	263.4	
+6			7.2	264.0	
1/4			7.6	263.6	
℄			7.0	264.2	
+5			6.7	264.5	
1/4			6.8	264.4	
cb			6.6	264.6	
+9			6.6	264.6	
+11			5.8	265.4	

15+52 12		39+74 20
E.L.	5.8	265.4
10E	5.3	265.9
15+77 12 = ℄ Charles		39+49 20
10E	5.2	266.0
E.L.	5.5	265.7
+11	5.8	265.4
cb	6.0	265.2
1/4	6.5	264.7
+6	6.5	264.7
℄	6.7	264.5
1/4	7.3	263.9
+4	6.9	264.3
cb	7.5	263.7
+5	8.3	262.9
w.L.	7.9	263.3
16+02 12 = 0+00 = S.L. Charles		39+29 20
w.L.	7.8	263.4
+10	7.8	263.4
cb	7.2	264.0
1/4	7.0	264.2
℄	6.6	264.6
+5	6.4	264.8
1/4	6.4	264.8
cb	6.0	265.2
E.L.	5.5	265.7

0+50		38+74 20
E.L.	5.3	265.9
+4	6.0	265.2
+10	5.4	265.8
+12	5.5	265.7
cb	6.0	265.2
1/4	6.3	264.9
℄	6.2	265.0
1/4	6.8	264.4
cb	7.1	264.1
w.L.	7.3	263.9
1+00		38+24 20
w.L.	6.7	264.5
+4	6.9	264.3
cb	6.3	264.9
1/4	6.0	265.2
℄	5.5	265.7
1/4	5.5	265.7
+5	5.5	265.7
cb	4.9	266.3
+3	4.3	266.9
E.L.	4.9	266.3

1+40 = N.L. Alley			37+84 20
E.L.	4.5	266.7	
+10	3.8	267.4	
cb	4.3	266.9	
+1	4.8	266.4	
¼	4.8	266.4	
℄	4.8	266.4	
¼	5.3	265.9	
cb	5.6	265.6	
W.L.	5.8	265.4	
1+60 = S.L. Alley			37+64 20
W.L.	5.5	265.7	
+9	5.7	265.5	
cb	5.4	265.8	
¼	4.8	266.4	
℄	4.3	266.9	
¼	4.4	266.8	
cb	4.3	266.9	
+4	3.5	267.7	
E.L.	3.7	267.5	

2+00	271.20		37+24 20
E.L.		2.7	268.5
+10		2.5	268.7
cb		3.4	267.8
+1		3.6	267.6
¼		3.5	267.7
℄		3.5	267.7
¼		4.0	267.2
+5		4.0	267.2
cb		4.8	266.4
W.L.		5.1	266.1
2+50			36+74 20
W.L.		3.8	267.4
+3		4.4	266.8
cb		3.2	268.0
+6		2.8	268.4
¼		2.7	268.5
℄		2.3	268.9
¼		2.3	268.9
cb		2.0	269.2
+1		1.6	269.6
+4		1.4	269.8
E.L.		1.3	269.9
T.P.	12.14	282.69	0.65 270.55

3+00 = N.L 282.69 Dudley

E.L		11.9	270.8
+10		11.6	271.1
cb		12.0	270.7
¼		12.2	270.5
℄		12.3	270.4
¼		12.7	270.0
cb		12.6	270.1
+12		14.0	268.7
W.L		13.2	269.5

℄ Dudley 35+99 22

W.L		12.8	269.9
+10		11.6	271.1
cb		11.5	271.2
¼		11.7	271.0
℄		11.4	271.3
¼		11.4	271.3
cb		11.3	271.4
+4		10.8	271.9
E.L.		10.9	271.8

36+24 20

SL. Dudley = 0+00

35+74 20

E.L		10.4	272.3
+11		10.3	272.4
+12		10.6	272.1
cb		10.6	272.1
¼		10.6	272.1
℄		10.6	272.1
¼		11.0	271.7
+3		11.0	271.7
+5		10.7	272.0
cb		11.0	271.7
+9		11.7	271.0
W.L.		12.3	270.4

0+50 35+24 20

W.L		10.5	272.2
cb		9.3	273.4
¼		9.0	273.7
℄		8.8	273.9
¼		8.8	273.9
cb		8.6	274.1
+2		8.3	274.4
+9		8.1	274.6
E.L.		8.4	274.3

1+00			34+74 20
E.L.	7.3	275.4	
+2	8.0	274.7	
+3	7.0	275.7	
cb	7.0	275.7	
1/4	7.1	275.6	
℄	7.2	275.5	
1/4	7.5	275.2	
cb	7.6	275.1	
W.L.	9.0	273.7	
1+40 = N.L. Alley			34+34 20
W.L.	7.4	275.3	
+2	8.2	274.5	
cb	6.6	276.1	
+6	5.8	276.9	
+7	6.2	276.5	
1/4	6.1	276.6	
℄	5.8	276.9	
+5	5.6	277.1	
1/4	5.7	277.0	
cb	5.6	277.1	
+4	5.3	277.4	
+5	5.8	276.9	
E.L.	5.1	277.6	

282.69

36

1+60 = S.L. Alley			34+14 20
E.L.	5.3	277.4	
+4	4.8	277.9	
+7	5.2	277.5	
+10	4.9	277.8	
cb	5.0	277.7	
1/4	5.1	277.6	
+6	4.9	277.8	
℄	5.1	277.6	
1/4	5.2	277.5	
+4	5.1	277.6	
cb	5.7	277.0	
+12	7.4	275.3	
W.L.	6.7	276.0	
+ob Post SE Dudley = Catalina. BM 12.93 290.26	5.36	277.33	
2+00			33+74 20
W.L.	13.2	277.1	
+3	13.6	276.7	
cb	12.3	278.0	
+6	11.5	278.8	
1/4	11.5	278.8	
℄	11.1	279.2	
1/4	11.1	279.2	
cb	11.1	279.2	
+4	11.0	279.3	
+10	11.4	278.9	
+12	12.0	278.3	

2+00	290.26			33+74 20
E.L.		11.3	279,0	
2+50				33+24 20
E.L.		9.5	280.8	
cb		9.2	281.1	
¼		9.3	281,0	
+6		9.2	281,1	
℄		9.3	281,0	
¼		9.5	280,8	
+5		9.7	280,6	
cb		10.2	280,1	
+1		10.3	280,0	
+10		12.2	278,1	
+13		12.5	277,8	
W.L.		11.7	278,6	
3+00 = NL Warner				32+74 20
W.L.		9.4	280,9	
+3		10.3	280.0	
+6		9.2	281,1	
cb		8.2	282,1	
+5		7.4	282,9	
¼		7.3	283,0	
℄		7.1	283,2	
+5		7.0	283.3	
¼		7.2	283.1	
cb		7.2	283.1	
+6		7.5	2828	

3+00			32+74 20
EL	7.0	283,3	
℄ Warner			32+49 20
EL	6.1	284,2	
+7	6.5	283,8	
+10	6.2	284,1	
cb	6.2	284,1	
¼	6.1	284.2	
+5	59	284.4	
℄	6.0	284.3	
¼	6.2	284,1	
+4	6.3	284.0	
cb	7.4	282,9	
W.L.	8.2	282,1	
S.L. Warner = 0+00			32+24 20
W.L.	6.8	283.5	
+10	6.6	283,7	
cb	6.3	284,0	
+6	5.0	285,3	
¼	5.1	285,2	
℄	4.9	285.4	
+5	4.8	285.5	
¼	5.0	285,3	
cb	5.1	285,2	
+9	5.1	285,2	
+10	5.5	284,8	
E.L.	5.5	284,8	

0+50	290.26				31+74 20	1+40 N.L Alley	802.95		30+84 20
E.L			3.2	287.1		E.L		12.0	290.9
+4			2.7	287.6		cb		11.7	291.2
cb			2.9	287.4		¼		11.6	291.3
¼			2.7	287.6		℄		11.5	291.4
+5			2.6	287.7		¼		11.5	291.4
℄			2.7	287.6		+4		11.4	291.5
¼			2.9	287.4		+6		12.1	290.8
+4			2.9	287.4		cb		11.5	291.4
cb			3.2	287.1		W.L.		12.0	290.9
W.L			3.7	286.6		1+60 = S.L Alley			30+64 20
1+00					31+24 20	W.L		11.6	291.3
W.L			1.1	289.2		cb		10.7	292.2
cb			0.3	290.0		+7		11.2	291.7
¼			0.5	289.8		+9		11.0	291.9
℄			0.5	289.8		¼		10.9	292.0
+6			0.3	290.0		℄		10.9	292.0
¼			0.5	289.8		+7		10.7	292.2
cb			0.7	289.6		¼		10.8	292.1
+9			0.5	289.8		cb		11.0	291.9
+11			1.7	288.6		+12		10.8	292.1
E.L.			1.7	288.6		E.L.		9.7	293.2
T.P.	12.72	302.95	0.03	290.23					

2+00			30+24.20
E.L.		7.6	295,3
+2		9.3	293,6
cb		9.6	293,3
¼		9.5	293,4
+3		9.3	293,6
℄		9.5	293,4
¼		9.6	293,3
cb		9.5	293,4
W.L.		99	293,0
2+67.1 = ℄ Put Drive on West			29+56.50
W.L.		7.5	295,4
cb		7.3	295,6
¼		7.4	295,5
℄		7.4	295,5
+7		7.3	295,6
¼		7.4	295,5
cb		7.5	295,4
+8		7.4	295,5
E.L.		5.5	297,4

3+00 = N.L. Fort.			29+24.20
E.L.		6.5	296,4
cb		6.8	296,1
¼		6.7	296,2
℄		6.7	296,2
¼		6.8	296,1
+7		6.8	296,1
cb		6.5	296,4
W.L.		6.6	296,3
℄ Fort.			28+99.20
W.L.		6.0	296,9
cb		6.4	296,5
¼		6.4	296,5
℄		6.4	296,5
¼		6.3	296,6
cb		6.4	296,5
E.L.		6.3	296,6
S.L. Fort. = 0+00			28+74.20
E.L.		4.1	298,8
+2		6.1	296,8
cb		6.2	296,7
¼		6.0	296,9
℄		6.1	296,8
¼		6.2	296,7
cb		6.0	296,9
W.L.		5.7	297,2

0+50			28+24.20
W.L	5.3	297.6	
cb	5.4	297.5	
1/4	5.7	297.2	
℄	5.7	297.2	
1/4	5.6	297.3	
cb	5.7	297.2	
E.L.	5.6	297.3	
1+00			27+74.20
E.L	3.7	299.2	
+1	5.2	297.7	
cb	5.6	297.3	
1/4	5.5	297.4	
℄	5.5	297.4	
1/4	5.3	297.6	
+2	5.1	297.8	
cb	5.3	297.6	
W.L.	5.4	297.5	
1+40 = N.L. Alley			27+34.20
W.L.	5.2	297.7	
cb	5.2	297.7	
1/4	5.3	297.6	
℄	5.4	297.5	
1/4	5.3	297.6	
cb	5.3	297.6	
+13	5.3	297.6	
E.L.	4.3	298.6	

1+60 = S.L. Alley			27+14.20
E.L.	3.6	299.3	
+2	5.1	297.8	
cb	5.3	297.6	
1/4	5.3	297.6	
℄	5.3	297.6	
1/4	5.3	297.6	
cb	5.2	297.7	
W.L.	5.2	297.7	
2+00			26+74.20
W.L.	5.2	297.7	
cb	5.2	297.7	
1/4	5.2	297.7	
℄	5.3	297.6	
1/4	5.2	297.7	
cb	5.3	297.6	
+5	5.3	297.6	
+12	5.0	297.9	
E.L.	3.5	299.4	

2+50			26+24 20
E.L.	3.7	299,2	
+1	5.0	297,9	
+8	4.7	298,2	
cb	5.1	297,8	
¼	5.1	297,8	
℄	5.2	297,7	
¼	5.2	297,7	
+1	4.9	298,0	
cb	5.1	297,8	
W.L	5.2	297,7	
3+00 = N.L. Pio Pico			25+74 20
W.L.	5.3	297.6	
cb	5.1	297,8	
¼	4.8	298,1	
+1	5.1	297,8	
℄	5.1	297,8	
¼	4.9	298,0	
cb	4.9	298,0	
+11	4.8	298,1	
E.L	4.1	298.8	

℄ Pio Pico			25+49 20
E.L	4.6	298,3	
cb	4.8	298,1	
¼	4.9	298,0	
℄	5.1	297,8	
¼	4.7	298,2	
cb	5.1	297,8	
W.L	5.1	297,8	
S.L. Pio Pico = 0+00			25+24 20
W.L.	5.2	297.7	
cb	5.0	297,9	
¼	4.6	298,3	
+1	5.0	297,9	
℄	5.1	297.8	
¼	4.9	298.0	
cb	4.7	298,2	
E.L.	4.5	298,4	
0+50			24+74 20
E.L.	3.3	299.6	
+1	4.5	298,4	
cb	4.5	298,4	
¼	4.8	298,1	
℄	5.0	297.9	
+9	4.9	298.0	
¼	4.3	298.6	
cb	4.7	298,2	
W.L	4.6	298,3	

1+00			23+24 20
W.L.	4.4	298.5	
cb	4.3	298.6	
+7	4.5	298.4	
1/4	4.1	298.8	
+1	4.8	298.1	
℄	4.9	298.0	
1/4	4.7	298.2	
cb	4.2	298.7	
+5	4.8	298.1	
E.L.	4.2	298.7	
1+50			23+74 20
E.L.	2.8	300.1	
+3	4.7	298.2	
+6	4.1	298.8	
cb	4.3	298.6	
1/4	4.5	298.4	
℄	4.6	298.3	
+9	4.5	298.4	
1/4	4.0	298.9	
cb	4.1	298.8	
W.L.	4.0	298.9	

2+00	302.95			23+24 20
W.L.		3.8	299.1	
cb		3.7	299.2	
1/4		3.9	299.0	
+1		4.2	298.7	
℄		4.3	298.6	
1/4		4.2	298.7	
cb		4.1	298.8	
+3		3.4	299.5	
+5		3.7	299.2	
+8		4.2	298.7	
E.L.		2.7	300.2	
T.P.	9.19	4.28	298.67	
2+50				22+74 20
E.L.		7.8	300.1	
+2		8.7	299.2	
+8		8.3	299.6	
+9		8.2	299.7	
cb		8.8	299.1	
1/4		8.8	299.1	
℄		8.8	299.1	
+7		8.7	299.2	
+8		8.0	299.9	
1/4		8.0	299.9	
cb		8.2	299.7	
W.L.		7.9	300.0	

3+23.5 = ℄ Road on East				22700.70
	307.86			
W.L.		7.0	300,9	
+6		6.9	301.0	
cb		7.2	300.7	
¼		7.2	300.7	
+3		7.8	300,1	
℄		7.9	300,0	
¼		7.9	300.0	
cb		7.8	300,1	
E.L.		7.8	300,1	
3+50				21+74.20
E.L.		7.7	300,2	
+6		6.6	301,3	
+10		7.4	300.5	
cb		7.3	300,6	
¼		7.4	300.5	
℄		7.5	300,4	
+8		7.4	300,5	
¼		6.8	301.1	
cb		6.6	301.3	
+5		6.3	301.6	
W.L.		6.6	301,3	

A+00			21+24.20
W.L.	5.4	302,5	
cb	5.7	302,2	
+8	6.2	301,7	
¼	5.9	302,0	
+2	6.5	301,4	
℄	6.5	301,4	
¼	6.4	301,5	
cb	6.4	301,5	
+1	5.7	302,2	
+8	5.6	302,3	
E.L.	6.5	301,4	
A+50			20+74.20
E.L.	5.4	302,5	
+8	4.6	303,3	
cb	5.6	302,3	
¼	5.5	302,4	
℄	5.6	302,3	
+9	5.6	302,3	
¼	5.1	302,8	
cb	5.0	302,9	
W.L.	5.0	302,9	

5+00	307.86			20+24 NO	
W.L.			3.6	304.3	
+10			3.4	304.5	
cb			3.8	304.1	
1/4			4.6	303.3	
℄			4.6	303.3	
1/4			4.5	303.4	
cb			4.6	303.3	
+1			3.9	304.0	
+6			3.4	304.5	
+11			4.3	303.6	
E.L.			3.9	304.0	
5+50					19+74 NO
E.L.			2.8	305.1	
+12			2.9	305.0	
+13			3.6	304.3	
cb			3.6	304.3	
1/4			3.6	304.3	
℄			3.4	304.5	
1/4			3.3	304.6	
+8			3.0	304.9	
cb			2.5	305.4	
W.L.			1.6	306.3	
⊙ T.P	12.95	E 319.77	1.04	306.82	

6+05 11 - ℄ Road on East.

	319.77				19+18 49
W.L.			12.8	307.0	
+10			12.8	307.0	
cb			13.7	306.1	
1/4			14.0	305.8	
℄			14.0	305.8	
1/4			14.0	305.8	
cb			13.9	305.9	
E.L.			13.5	306.3	
6+50					18+74 NO
10E			12.9	306.9	
E.L.			12.3	307.5	
cb			12.7	307.1	
1/4			12.9	306.9	
℄			12.8	307.0	
1/4			12.5	307.3	
+5			11.3	308.5	
cb			11.4	308.4	
+4			10.6	309.2	
W.L.			10.6	309.2	

7+00			18+24 20
w.L.	10.2	309.6	
+10	9.9	309.9	
eb	10.7	309.1	
+6	10.5	309.3	
+7	10.8	309.0	
1/4	10.9	308.9	
℄	11.3	308.5	
1/4	11.2	308.6	
eb	10.8	309.0	
EL	10.6	309.2	
10E	11.2	308.6	
7+45			17+79 20
10E	10.0	309.8	
E.L	9.2	310.6	
+10	9.5	310.3	
eb	9.5	310.3	
1/4	9.5	310.3	
℄	9.7	310.1	
1/4	9.4	310.4	
eb	9.2	310.6	
+4	8.7	311.1	
W.L	8.9	310.9	

8+05			17+19 20
w.L.	6.2	313.6	
+10	5.9	313.9	
eb	6.6	313.2	
1/4	7.0	312.8	
℄	7.0	312.8	
1/4	7.1	312.7	
eb	6.9	312.9	
+4	6.3	313.5	
E.L.	6.2	313.6	
10E	7.0	312.8	
8+50			16+74 20
10E	5.3	314.5	
E.L	4.8	315.0	
eb	4.8	315.0	
1/4	5.0	314.8	
℄	5.0	314.8	
1/4	5.1	314.7	
eb	5.0	314.8	
+4	4.0	315.8	
W.L	4.3	315.5	

8+93	319.77			16+31.20	
w.L.			2.0	317.8	
+10			2.0	317.8	
cb			3.0	316.8	
1/4			3.3	316.5	
+2			3.0	316.8	
℄			2.9	316.9	
1/4			2.9	316.9	
cb			2.7	317.1	
+7			2.6	317.2	
49			3.0	316.8	
+10			2.5	317.3	
E.L			2.5	317.3	
10E			3.5	316.3	
9+50				15+74.20	
10E			1.2	318.6	
EL			0.2	319.6	
+5			0.4	319.4	
+6			0.1	319.7	
cb			0.0	319.8	
T.P.	12.90	332.48	0.19	319.58	
1/4			12.6	319.9	
℄			12.7	319.8	
1/4			12.5	320.0	
+3			12.4	320.1	
+5			18.0	319.5	
cb			12.5	320.0	

9+50	332.48			15+74.20
+4		11.9	320.6	
w.L.		12.2	320.3	
10+00				15+24.00
w.L		9.5	323.0	
+10		9.5	323.0	
cb		9.8	322.7	
+5		9.9	322.6	
+7		9.5	323.0	
1/4		9.4	323.1	
℄		9.6	322.9	
+5		9.5	323.0	
1/4		9.7	322.8	
cb		9.8	322.7	
+3		9.7	322.8	
EL		10.9	321.6	
10E		11.4	321.1	
10+50				14+74.20
10E		8.1	324.4	
E.L.		7.7	324.8	
+5		7.9	324.6	
+10		6.6	325.9	
cb		6.7	325.8	
1/4		6.6	325.9	
℄		6.5	326.0	
1/4		6.6	325.9	

10+50					14+74 20						
+7			6.8	325.7							
+9			7.4	325.1							
cb			7.1	325.4							
WL			7.1	325.4							
11+00					14+24 20						
10E			5.0	327.5							
EL			4.4	328.1							
+10			3.5	329.0							
cb			3.8	328.7							
¼			3.7	328.8							
℄			3.6	328.9							
¼			3.6	328.9							
+7			3.5	329.0							
cb			4.2	328.3							
+4			4.0	328.5							
WL			4.4	328.1							
12+50					13+74 20						
WL			1.2	331.3							
+10			0.6	331.9							
cb			0.9	331.6							
¼			0.6	331.9							
℄			0.6	331.9							
¼			0.5	332.0							
cb			0.5	332.0							
EL			0.9	331.6							
10E			1.7	330.8							

℄ Put Drive on West

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12+09			332.48							13+15 20	
T.P.	12.84		345.24		0.08	332.40					
10E					10.2	335.0					
E.L.					10.1	335.1					
cb					9.7	335.5					
¼					9.8	335.4					
℄					9.8	335.4					
¼					9.6	335.6					
cb					9.6	335.6					
WL					9.6	335.6					
12+50										12+74 20	
WL					6.3	338.9					
+11					6.1	339.1					
+12					7.2	338.0					
cb					7.2	338.0					
+7					7.0	338.2					
+8					7.8	337.4					
+9					6.9	338.3					
¼					7.0	338.2					
℄					7.2	338.0					
¼					7.1	338.1					
cb					7.1	338.1					
+7					7.1	338.1					
+8					6.8	338.4					
EL					6.4	338.8					
10E					7.4	337.8					

13+00	345 24			12+24 20
10E		3.0	342.2	
EL		2.5	342.7	
+7		2.7	342.5	
+8		4.2	341.0	
+11		4.5	340.7	
cb		4.1	341.1	
1/4		4.0	341.2	
℄		4.1	341.1	
1/4		4.0	341.2	
+1		5.2	340.0	
+7		4.3	340.9	
cb		4.4	340.8	
+3		2.7	342.5	
W.L.		2.4	342.8	
13+50				11+74 20
W.L.		+0.7	345.9	
+11		+1.0	346.2	
+11		+0.1	345.3	
cb		1.1	344.1	
+3		2.2	343.0	
+7		0.6	344.6	
+8		0.7	344.5	
+9		2.3	342.9	
1/4		2.3	342.9	
+1		1.0	344.2	

13+50	34524			11+74 20
℄		1.1	344.1	
1/4		0.9	344.3	
cb		1.3	343.9	
+5		1.1	344.1	
+6		+0.4	345.6	
E.L.		+0.6	345.8	
10E		1.4	343.8	
T.S.	12.51	357.65	0.10	345.14
14+00			8.7	11+24 20
10E		8.7	348.9	
EL		8.2	349.4	
+9		9.0	348.6	
+11		10.6	347.0	
cb		10.8	346.8	
1/4		10.5	347.1	
℄		10.5	347.1	
+9		10.7	346.9	
1/4		12.3	345.3	
+1		10.4	347.2	
cb		11.0	346.6	
+2		8.9	348.7	
W.L.		9.2	348.4	

14+50	35765			10+74 20
W.L		6.8	350.8	
+12		6.4	351.2	
cb		8.1	349.5	
+2		9.1	348.5	
+4		7.7	349.9	
+9		7.4	350.2	
+9 5		9.8	347.8	
'4		7.6	350.0	
℄		7.6	350.0	
'4		7.8	349.8	
cb		7.8	349.8	
+3		7.7	349.9	
+6		6.3	351.3	
E.L		6.0	351.6	
10E		6.6	351.0	
15+00				10+24 20
10E		3.2	354.4	
E.L		3.5	354.1	
+7		3.1	354.5	
+10		5.2	352.4	
+12		4.1	353.5	
cb		4.4	353.2	
'4		4.7	352.9	
℄		4.5	353.1	
+9		4.7	352.9	
'4		5.4	352.2	

15+00	35765			10+24 20
+1		4.4	353.2	
+5		4.4	353.2	
cb		5.0	352.6	
+5		4.2	353.4	
W.L.		4.4	353.2	
15+50				9+74 20
W.L		1.7	355.9	
+9		1.6	356.0	
cb		1.0	356.6	
+1		0.7	356.9	
+9		1.7	355.9	
'4		2.5	355.1	
+2		2.2	355.4	
℄		1.9	355.7	
'4		2.0	355.6	
cb		1.9	355.7	
+3		1.8	355.8	
+4		2.2	355.4	
+6		1.2	356.4	
E.L		1.2	356.4	
10E		2.0	355.6	
Mon N.L. Aztec. B.M	12.73	370.32	0.06	357.59

15+87.60 = N.L Aztec.				9+36.60
10E		11.9	358,4	
EL		11.9	358.4	
+7		12.1	358,2	
+8		13.3	357.0	
+11		12.8	357.5	
cb		13.0	357.3	
1/4		12.9	357,4	
℄		12.8	357,5	
1/4		13.6	356,7	
+2		12.7	357.6	
cb		12.9	357.4	
+4		13.0	357.3	
+5		12.2	358,1	
W.L		12.4	357,9	
16+17.68 = 0+00 = S.L Aztec				9+06.60
W.L		10.8	359.5	
+9		10.7	359,6	
+10		11.4	358,9	
cb		11.5	358.8	
+9		11.1	359.2	
1/4		12.1	358.2	
+1		11.3	359.0	
℄		11.3	359.0	
1/4		11.3	359.0	
cb		11.1	359.2	
+2		11.0	359.3	

0+00	370.32			9+06.66
EL		11.1	359,2	
0+50				9+56.60
EL		8.3	362.0	
+5		8.3	362.0	
+6		9.3	361,0	
cb		8.2	362,1	
cb		8.8	361.5	
1/4		8.9	361,4	
℄		8.9	361,4	
+8		9.0	361,3	
+9		10.3	360,0	
1/4		10.3	360,0	
+7		8.6	361.7	
cb		8.9	361,4	
+4		7.8	362.5	
W.L.		7.8	362.5	
1+00				8+06.60
W.L		5.4	364.9	
+9		5.2	365,1	
+10		6.9	363,4	
cb		7.0	363.3	
+1		6.5	363,8	
+9		6.4	363,9	
1/4		8.2	362,1	
+2		6.7	363,6	
℄		6.8	363,5	

1+00				8+06.60
¼		6.7	363.6	
eb		6.8	363.5	
+1		6.3	364.0	
+7		7.5	362.8	
+10		5.9	364.4	
E.L.		5.7	364.6	
1+50				7+56.60
E.L.		3.7	366.4	
+4		4.0	366.3	
+5		5.5	364.8	
+13		4.4	365.9	
eb		5.0	365.3	
¼		4.8	365.5	
℄		4.8	365.5	
+9		4.8	365.5	
¼		6.4	363.9	
+1		4.4	365.9	
+9		4.7	365.6	
eb		5.8	364.5	
+2		5.8	364.5	
+4		3.3	367.0	
w.L.		3.3	367.0	

2+00	370.32			7+06.60
w.L.		1.8	368.5	
+9		1.8	368.5	
+12		4.6	365.7	
eb		4.7	365.6	
+1		3.6	366.7	
¼		3.1	367.2	
+1		4.3	366.0	
+2		3.4	366.9	
℄		3.5	366.8	
¼		3.4	366.9	
eb		3.6	366.7	
+1		3.1	367.2	
+9		3.6	366.7	
+11		2.4	367.9	
E.L.		2.4	367.9	
TP	5.68	367.97	0.03	370.29
2+50				6+56.60
E.L.		7.1	368.9	
+5		7.2	368.8	
+11		8.2	367.8	
eb		7.7	368.3	
+2		7.5	368.5	
+3		8.3	367.7	
¼		8.1	367.9	
℄		8.2	367.8	

Catalina

2+50	375.97			6+56.60
¼		8.3	367.7	
+2		8.8	367.2	
+3		7.9	368.1	
cb		7.7	368.3	
+2		7.7	368.3	
+6		7.0	369.0	
W.L.		6.3	369.7	
3+00				6+06.60
W.L.		6.0	370.0	
+5		6.2	369.8	
+11		6.8	369.2	
cb		6.9	369.1	
+7		7.0	369.0	
+8		7.3	368.7	
¼		7.0	369.0	
+1		7.3	368.7	
±		7.2	368.8	
¼		7.2	368.8	
+7		7.2	368.8	
+9		6.5	369.5	
cb		6.7	369.3	
+6		7.5	368.5	
+11		6.6	369.4	
E.L.		6.7	369.3	

3+50				5+56.60
E.L.		6.3	369.7	
+3		6.1	369.9	
+8		6.7	369.3	
cb		5.6	370.4	
+3		5.5	370.5	
+4		6.3	369.7	
¼		6.3	369.7	
±		6.4	369.6	
¼		6.6	369.4	
+1		6.2	369.8	
cb		6.3	369.7	
+5		6.4	369.6	
+9		5.4	370.6	
W.L.		5.5	370.5	
4+00				5+06.60
W.L.		5.1	370.9	
+8		5.1	370.9	
+10		5.6	370.4	
cb		5.6	370.4	
+9		5.1	370.9	
¼		5.6	370.4	
±		5.7	370.3	
¼		5.5	370.5	
+6		5.4	370.6	
+7		4.7	371.3	
cb		5.2	370.8	

A+00				5+06.60
+5		5.8	370.2	
E.L.		5.9	370.1	
4+50				4+56.60
E.L.		5.3	370.7	
+10		4.9	371.1	
c.b		4.3	371.7	
+3		3.8	372.2	
+4		4.7	371.3	
¼		4.7	371.3	
℄		4.8	371.2	
¼		4.5	371.5	
+1		4.1	371.9	
c.b		4.9	371.1	
+3		4.8	371.2	
+6		4.3	371.7	
W.L.		4.3	371.7	
5+00				4+06.60
W.L.		3.6	372.4	
+10		3.7	372.3	
c.b		3.9	372.1	
+9		3.2	372.8	
¼		3.3	372.7	
+1		3.8	372.2	
℄		3.9	372.1	
¼		3.8	372.2	

5+00		375.97		4+06.60
+6.5			3.8	372.2
+7			3.0	373.0
c.b			3.8	372.2
E.L.			4.4	371.6
T.P.	9.56	382.54	2.99	372.98
5+50				3+56.60
E.L.			9.9	372.6
+11			9.8	372.7
c.b			9.0	373.5
+3			8.8	373.7
+4			9.6	372.9
¼			9.5	373.0
℄			9.6	372.9
+9.5			9.4	373.1
¼			9.0	373.5
+1			8.8	373.7
+9			9.4	373.1
c.b			9.2	373.3
+3			8.7	373.8
W.L.			8.7	373.8

6+00	382.54			3+06.60
W.L		7.2	375.3	
eb		7.5	375.0	
+½		8.5	374.0	
+8		8.0	374.5	
¼		8.0	374.5	
+1		8.5	374.0	
℄		8.5	374.0	
¼		8.4	374.1	
eb		8.3	374.2	
EL		8.8	373.7	
Mon NE Catalina 2 Peru B.M		7.54	375.00	Bench Book 375.16
6+50 = NL Peru				2+56.60
EL		7.6	374.9	
eb		7.1	375.4	
¼		7.3	375.2	
℄		7.4	375.1	
¼		7.4	375.1	
+6.5		7.2	375.3	
+9		6.2	376.3	
eb		6.1	376.4	
W.L		5.9	376.6	

6+70 = ℄ Peru				2+36.60
W.L		5.5	377.0	
eb		5.6	376.9	
+1		5.6	376.9	
+5		6.8	375.7	
¼		7.0	375.5	
℄		6.7	375.6	
¼		6.8	375.7	
eb		6.7	375.8	
EL		7.0	375.5	
6+90 = SL Peru				2+16.60
EL		6.3	376.2	
+7		6.6	375.9	
eb		6.2	376.3	
¼		6.3	376.2	
℄		6.5	376.0	
¼		6.6	375.9	
+3		6.2	376.3	
+5		6.2	376.3	
+8		5.4	377.1	
eb		5.4	377.1	
W.L		5.3	377.2	

7+50				1+56.60
W.L.		4.5	378.0	
cb		4.7	377.8	
+5		4.7	377.8	
+7		5.0	377.5	
+9		4.6	377.9	
1/4		5.2	377.3	
℄		5.3	377.2	
1/4		5.1	377.4	
cb		4.9	377.6	
+3		4.6	377.9	
+10		4.9	377.6	
E.L.		4.3	378.2	
8+00				1+06.60
E.L.		2.9	379.6	
cb		3.8	378.7	
1/4		4.1	378.4	
℄		4.2	378.3	
1/4		4.3	378.2	
+1		3.7	378.8	
cb		3.7	378.8	
W.L.		3.8	378.7	

8+50				0+56.60
W.L.		2.8	379.7	
cb		2.7	379.8	
+9		2.8	379.7	
1/4		3.1	379.4	
℄		3.0	379.5	
1/4		3.0	379.5	
cb		2.5	380.0	
+7		1.8	380.7	
E.L.		0.5	382.0	
8+99.85 = Res Line on East				0+06.75
E.L.		+0.1	382.6	
cb		0.7	381.8	
1/4		0.9	381.6	
℄		1.2	381.3	
1/4		1.2	381.3	
cb		1.1	381.4	
W.L.		1.2	381.3	
End Sec. on Res. Line				0+00
W.L.		0.6	381.9	
cb		0.6	381.9	
1/4		0.7	381.8	
℄		0.9	381.6	
1/4		0.6	381.9	
cb		0.4	382.1	
E.L.		+0.1	382.6	

Restationing going north

5/25/29 Loudon to Cortez

X Sec. Peru St. from Catalina Blvd. 40' St + 5' Sidewalk 30' Rdway.

		378.88			
B.M.	3.88	378.88		375.00	NCor NE Catalina & Peru
0+00 = E.L. Catalina Blvd.					
N.L.			3.9	375.0	
cb			3.8	375.1	
¼			3.6	375.3	
℄			3.4	375.5	
¼			3.4	375.5	
cb			2.9	376.0	
S.L.			2.6	376.3	
0+50					
S.L.			2.3	376.6	
℄			3.3	375.6	
cb			3.6	375.3	
¼			4.3	374.6	
℄			4.6	374.3	
¼			4.8	374.1	
cb			4.8	374.1	
N.L.			4.9	374.0	
1+00					
N.L.			5.9	373.0	
cb			5.7	373.2	
¼			5.8	373.1	
℄			5.4	373.5	
¼			5.2	373.7	
cb			4.0	374.9	
S.L.			2.6	376.3	

PLOTTED JUNE 4, '29 DAVIES

		378.88			
T.P.	4.68	377.20	6.36	372.52	
1+60					
S.L.			2.9	374.3	
cb			3.1	374.1	
¼			3.1	374.1	
℄			4.4	372.8	
¼			4.7	372.5	
cb			4.7	372.5	
N.L.			5.0	372.2	
2+00					
N.L.			5.2	372.0	
cb			5.0	372.2	
¼			5.1	372.1	
℄			4.4	372.8	
¼			4.1	373.1	
cb			4.1	373.1	
S.L.			4.2	373.0	
2+50					
S.L.			4.7	372.5	
cb			4.8	372.4	
¼			5.0	372.2	
℄			5.2	372.0	
¼			5.6	371.6	
cb			5.4	371.8	
N.L.			5.6	371.6	

X Sec Aztec st from EL Catalina Blvd. to W.L Cortez st. 30' width taken as half 60' st 12' cbs 9' gutters.

57

3+00								
N.L		6.2	371.0	B.M	7.94	365.53	357.59	Mon. in S Catalina & Aztec
cb		6.1	371.1	0+00 = EL Catalina.				
¼		6.2	371.0	S.L		6.4	359.1	
℄		5.8	371.4	cb		6.7	358.8	
¼		5.6	371.6	¼		6.8	358.7	
cb		5.3	371.9	℄		7.0	358.5	
S.L		5.2	372.0	0+50				
3+50				℄		7.0	358.5	5.9
S.L		6.1	371.1	¼		6.5	359.0	
cb		6.3	370.9	cb		6.5	359.0	
¼		6.4	370.8	+3		5.7	359.8	
℄		6.7	370.5	S.L		6.0	359.5	
¼		7.2	370.0	1+00				
cb		7.4	369.8	S.L		6.3	359.2	
N.L		7.5	369.7	+6		6.2	359.3	
4+00 = W.L Cortez				cb		6.8	358.7	
N.L		9.5	367.7	¼		6.7	358.8	
cb		9.1	368.1	℄		7.6	357.9	
¼		8.9	368.3	1+50				
℄		8.4	368.8	℄		8.0	357.5	
¼		8.1	369.1	¼		7.8	357.7	
cb		7.8	369.4	+3		8.2	357.3	
S.L		7.7	369.5	+6		7.7	357.8	
				cb		7.7	357.8	
				+9		6.9	358.6	
				S.L		7.2	358.3	

PLOTTED JUNE 4, 29 DAVIES

Aztec

2+00		365.53		
S.L.			8.6	356.9
cb			9.5	356.0
+5			10.0	355.5
¼			9.5	356.0
℄			9.7	355.8
2+50				
℄			11.8	353.7
¼			11.9	353.6
+4			12.7	352.8
cb			11.8	353.7
+4			11.2	354.3
S.L.			11.1	354.4
T.P.	1.29	355.22	11.60	353.93
3+00				
S.L.			4.0	351.2
+3			3.7	351.5
cb			4.6	350.6
+6			5.2	350.0
¼			4.7	350.5
℄			5.3	349.9

Aztec

3+50	355.22		
℄		8.5	346.7
¼		8.1	347.1
+3		8.5	346.7
+5		8.2	347.0
cb		7.9	347.3
S.L.		7.2	348.0
4+00 = M.L. Cortez			
S.L.		10.4	344.8
+9		10.2	345.0
cb		10.7	344.5
+6		11.2	344.0
¼		10.9	344.3
℄		11.5	343.7

Profile of Road Between PL 143 & 104 East from Catalina Blvd. 30' wide taken 15' on each side of PL. line (Sta. 6+65 Catalina X Secs) see P3.

(P. 44)

⊙T.P.	4.71	311.53		306.82
0+00 = E.L Catalina (30' E of Mon.)				
N.L.			5.7	305.8
℄			5.5	306.0
S.L.			5.1	306.4
0+50				
S.L.			6.0	305.5
℄			6.2	305.3
N.L.			6.6	304.9
1+00				
N.L.			6.4	305.1
℄			6.3	305.2
S.L.			6.0	305.5
1+50				
S.L			6.0	305.5
℄			6.3	305.2
N.L			6.0	305.5
2+00				
N.L			6.2	305.3
℄			6.1	305.4
S.L			5.8	305.7
2+50				
S.L.			5.7	305.8
℄			5.9	305.6
N.L.			6.8	305.2

PLOTTED P29 JUNE 4, 29 DAVIES

3+00		311.53		
N.L.			4.5	307.0
℄			4.7	306.8
S.L			4.5	307.0
4+00				
S.L			0.7	310.8
℄			1.1	310.4
N.L			0.5	311.0

Profile of Culvert Location shown on Page 2 at 6+65

XT.P.	4.33	248.08		243.75
0+00			3.2	244.9
+20			4.1	244.0
+27			4.6	243.5
+40			4.5	243.6
+55			4.5	243.6
+58			3.9	244.2
+70			5.1	243.0
0+96			7.9	240.2
1+85			9.6	238.5
2+10			10.3	237.8

Profile of Main Drive to Theosophical Institute at 12+96 Catalina x Secs.

(See PZ & 31)

℄ Dr. W.L. Catalina	9 06	268.58		259.52
0+00 = W.L. Catalina				
0+50				
N.L.			10.56	258.02
℄			9.74	258.84
S.L.			9 88	258.70
1+00				
S.L.			10.15	258.43
℄			10 44	258.14
N.L.			11.04	257.54
1+50				
N.L.			10.60	257.94
℄			10.01	258.57
S.L.			10.07	258.51
2+00				
S.L.			8 60	259.98
℄			8 41	260.17
N.L.			8.26	260.32
2+50				
N.L.			6.68	261.90
℄			6.10	262.48
S.L.			6.16	262.42

PLOTTED JUNE 4, '29 DAVIES

5½ & 6" x Sec Talbot Street from 40.00' EL. Catalina to 500' East 40' St. 5' cb 30' Rdway.

B.M.	4.41	265.09		260.68
0+00 = EL. Catalina (40' E of P.L line)				
N.L.			4 2	260.9
cb			4.1	261.0
¼			4.0	261.1
℄			4.1	261.0
¼			4 3	260.8
cb			4.5	260.6
S.L.			4.8	260,3
0+50				
S.L.			5 9	259.2
cb			5 8	259.3
¼			5.6	259.5
℄			5 5	259.6
¼			5.5	259.6
cb			5.4	259,7
N.L.			5 3	259,8
1+00				
N.L.			7.1	258.0
cb			7.1	258.0
¼			7.0	258,1
℄			7.0	258,1
¼			7.1	258.0
cb			7.4	257,7
¼			7.5	257.6
S.L.			7.1	258,0

PLOTTED JUNE 4, '29 DAVIES

B.P. N.W. Catalina & Santa Barbara

1+50			
S.L.		8.7	256,4
+3		9.2	255.9
eb		9.1	256.0
¼		9.0	256.1
℄		8.8	256,3
¼		8.8	256,3
eb		8.5	256.6
NL		8.7	256,4
2+00			
NL		8.8	256.3
+3		10.3	254.8
eb		10.3	254,8
¼		10.7	254,4
℄		10.8	254,3
¼		10.8	254,3
eb		11.0	254.1
+3		11.2	253.9
S.L.		10.6	254.5
2+50			
S.L.		12.5	252.6
+2		13.1	252.0
eb		13.1	252,0
¼		13.0	252.1
℄		13.0	252.1
¼		13.0	252.1
eb		12.7	252,4

2+50	265.09		
+2		12.7	252,4
NL		12.0	253,1
+P	0.38	252.56	12.91	252.18
3+00			
NL		2.3	250.3
+4		3.0	249.6
eb		3.0	249.6
¼		3.1	249.5
℄		3.1	249.5
¼		3.1	249.5
eb		2.8	249,8
+4		2.8	249.8
S.L.		2.2	250,4
3+50			
S.L.		5.4	247.2
+1		5.8	246,8
eb		5.8	246.8
¼		6.2	246.4
℄		6.2	246.4
¼		6.2	246.4
eb		6.2	246.4
+3		5.9	246,7
NL		5.1	247,5

4+00	252.56		
N.L		8.4	244,2
+2		8.4	244.2
℄b		9.5	243,1
¼		9.4	243,2
℄		9.4	243,2
¼		9.4	243,2
eb		9.4	243,2
+4		9.2	243,4
S.L.		8.3	244,3
4+50			
S.L.		11.5	241,1
+05		12.3	240,3
eb		12.7	239,9
¼		12.7	239,9
℄		12.7	239,9
¼		12.8	239,8
eb		13.1	239,5
+3		12.0	240,6
N.L.		12.0	240,6

5+00	252.56		
N.L		14.9	237,7
+4		15.1	237,5
eb		16.1	236,5
¼		15.8	236,8
℄		15.4	237,2
¼		15.6	237,0
eb		15.4	237,2
S.L.		15.6	237,0

8-14-29 Cb levels on returns at 32nd
J.C.Bliss + Elm + cb-gutter + ℄ levels to 175'
Dreibert North of N cb line Elm
Rauser

B.M. N.W. B.P. Bancroft + Elm 226.53
+5.66

ℸ 232.19

N.E. Return 32nd + Elm - 28' Radius - 4 parts 11' each - approx.

East end		8.91	223.28
G		9.55	222.64
+11		8.82	223.37
G		9.43	222.76
+22	G = Gutter	8.41	223.78
G		9.08	223.11
+33		7.70	224.49
G		8.24	223.95
+44 = North end		7.18	225.01
G		7.73	224.46

N.W. Return - 28' Radius

North end		7.54	224.65
G		7.93	224.26
+11		8.45	223.74
G		8.99	223.20
+22		9.22	222.97
G		9.87	222.32
+33		9.89	222.30
G		10.56	221.63
+44 = West end		10.39	221.80
G		10.99	221.20

S.W. Return - 28' Radius

West end		12.19	220.00
+11		12.45	219.74
+22		12.73	219.46
+33		12.90	219.29
+44 = South end		13.21	218.98

S.E. Return - 28' Radius - 4 Parts - 11.75 each - approx.

South end		12.19	220.00
+7.75		11.78	220.41
+15.50		11.38	220.81

Note - 32nd paved to N cb Line Elm

ℸ 232.19

33

+23.25		10.93	221.26
+31 = East end		10.43	221.76

N cb Line Elm = 0+00

℄ Paving N cb Line Elm		9.42	222.77

0+28 = P.C. of N.E. and N.W. Returns

E Tpcb		7.13	225.06
G		7.69	224.50
℄		7.31	224.88
G		7.91	224.28
W Tpcb		7.55	224.64

0+32 - B.K. in East cb. Line

W Tpcb		6.92	225.27
G		7.40	224.79
℄		6.85	225.34
G		7.35	224.84
E Tpcb		6.92	225.27

0+50

E Tpcb		3.89	228.30
G		4.37	227.82
℄		3.82	228.37
G		4.36	227.83
W Tpcb		3.86	228.33
T.P.			-0.37 231.82
	+13.23	245.05	

	T 245.05		
	0+75		
W-Gutter-Driveway	13.10	231.95	
℄	12.51	232.54	
G	13.02	232.03	
E Tp cb	12.53	232.52	
	1+00		
E-Gutter-Driveway	8.88	236.17	
℄	8.27	236.78	
G	8.76	236.29	
W Tp cb	8.22	236.83	
	1+25		
W Tp cb	4.61		
G-Driveway	4.61	240.44	
℄	4.07	240.98	
G	4.59	240.46	
E Tp cb	4.05	241.00	
	1+50		
E-Gutter-Driveway	0.85	244.20	
℄	0.27	244.78	
G	0.73	244.32	
W Tp cb	0.22	244.83	
T.P	-0.65	244.40	
+13.18	T 252.58		
	1+75		
N-Gutter-Driveway	10.84	247.24	
℄	9.74	247.84	
G	10.36	247.22	
E Tp cb	9.77	247.81	
T.P	-0.40	257.18	
+12.01	269.19		
B.M. In East walk about center of Block between Elm & Grape	-1.15	268.04	
+11.18	279.22		
B.M. S.W.B.P 32nd & Grape	-2.35	276.87	
	Correct	276.96	

T 257.58

Landis St Section. 10-28-1929.
Marlborough to 42nd Mill.

B.M. B.P.	2.53	349.62		347.09	N.W. Marlborough & Wightmans
T.P. on B.M. B.P.	4.59	347.67	6.54	343.08	N.W. Landis & Marlborough
		00 = E. Line Marlborough (51.7 Bet Curbs)			
N. emt. cb			4.58	343.09	✓
gutter Parmt.			5.29	342.38	✓
1/4 "			4.97	342.70	
℄ "			5.03	342.64	✓
1/4 "			5.24	342.43	
gutter "			5.48	341.99	✓
S. emt. cb.			5.16	342.51	✓
		10'. E.			
S. emt. cb			5.44	342.53	
gutter			5.6	342.0	
1/4			5.0	342.6	
C			4.7	343.0	
1/4			4.8	342.8	
gutter			5.4	342.2	
N. emt. cb			4.64	343.03	
		50'. E.			
N. emt. cb			4.77	342.90	
gutter			5.4	342.2	
1/4			4.9	342.7	
C			4.8	342.8	
1/4			5.2	342.4	
gutter			5.8	341.8	
S. emt. cb			5.20	342.47	

Plotted Oct. 29-1929 - C.T.H.

347.67

100'. E (51.85 Bet. Cbs)

S. emt. cb		5.24	342.39
gutter		5.8	341.8
1/4		5.4	342.2
C		4.8	342.8
1/4		5.1	342.5
gutter		5.5	342.1
N. emt. cb		4.84	342.83
	140'. E. = W. Line Alley		
N. Line on Alley Ret		4.73	342.94
" " emt		5.0	342.6
N. emt. cb.		4.90	342.77
gutter		5.5	342.1
1/4		5.0	342.6
C		4.8	342.8
1/4		5.3	342.3
gutter		5.8	341.8
S. emt. cb		5.39	342.28
S. Line Alley Return		5.14	342.53
" " emt		5.3	342.3

347.67

160'E = E Line Alley

S Line cmt. Return & dirt	5.06	342	61
S. cmt. eb	5.34	342	33
gutter	5.8	341	8
1/4	5.4	342	2
E	4.9	342	7
1/4	5.1	342	5
gutter	5.5	342	1
N. cmt. eb	5.00	342	67
N Line cmt. Return & dirt	4.81	342	86
From 185'E to 190'E. A. Curb Broken			
200'E.	(5'.9 Bet. Cbs)		
N. cmt. eb	5.11	342	56
gutter	5.5	342	1
1/4	5.2	342	4
E	4.9	342	7
1/4	5.4	342	2
gutter	5.9	341	7
S. cmt. eb	5.38	342	29
250'E.			
S. cmt. eb	5.43	342	24
gutter	6.1	341	5
1/4	5.4	342	2
E	5.1	342	5
1/4	5.3	342	3
gutter	5.6	342	0
N. cmt. eb	5.13	342	54

347.67

285'E.

N. cmt. eb			5.31	342	36
gutter			5.6	342	0
1/4			5.3	342	3
E			5.1	342	5
1/4			5.6	342	0
gutter			6.2	341	4
S. cmt. eb			5.58	342	09
360'E = W. Line. 42[deg] 54'			(5'.75 Bet. cbs.		
S. cmt. eb			5.59	342	08
gutter Pavmt			6.08	341	59
1/4 "			5.84	341	83
E "			5.76	341	91
1/4 "			5.74	341	93
gutter "			5.82	341	85
N. cmt. eb.			5.33	342	34
T. P.	10.17	352.69	5.15	342.52	N.W. 42[deg] 54'
chk on BM. 88.			0.13	352.56 = 352.57	+ Wightman

12-10-29 A-section Alley Block 3
J.C. Bliss Washington Hts. Ft Stockton
Drc bert - to Lewis - Between Ingalls & Jackson
Rauner 15' Wide

B.M. S.E. B.P. Ingalls & Ft. Stockton 272.98 ✓
+467
A 277.65

North Gutter Fort Stockton Facing

W		6.30	271.35
℄		6.45	271.20
E		6.52	271.13

Plotted 12/13/29 T.J.

N.L. Ft. Stockton = 0+00

E Tpcb		5.70	271.95
G		5.84	271.81
℄		6.07	271.58
G		5.68	271.97
W Tpcb		5.58	272.07

Note - Sta 0+00 to 0+76 on East side of alley - ornamental hedge by church extends 2.5' into alley

0+17

℄ 8' Garage Apron 8.5' Back W.L. Concrete		4.47	273.18

0+25

W		4.5	273.2
℄		4.8	272.9
E		4.8	272.9
Out 0.5' Edge concrete walk that started at 0+00		4.89	272.76

A 277.65

0+50

Out 0.5 edge walk		4.79	272.86
E		4.8	272.9
℄		4.6	273.1
W		4.8	272.9

0+71

E Concrete Garage apron 4' Back W.L.		4.70	272.95

0+75

W		4.8	272.9
℄		4.7	273.0
E		4.7	273.0
Out 0.5 edge walk		4.73	272.92

0+95

End concrete walk that started at 0+00 - 95' Back E.L.		4.69	272.96

1+00

E		4.7	273.0
℄		4.6	273.1
W		4.4	273.3

1+21

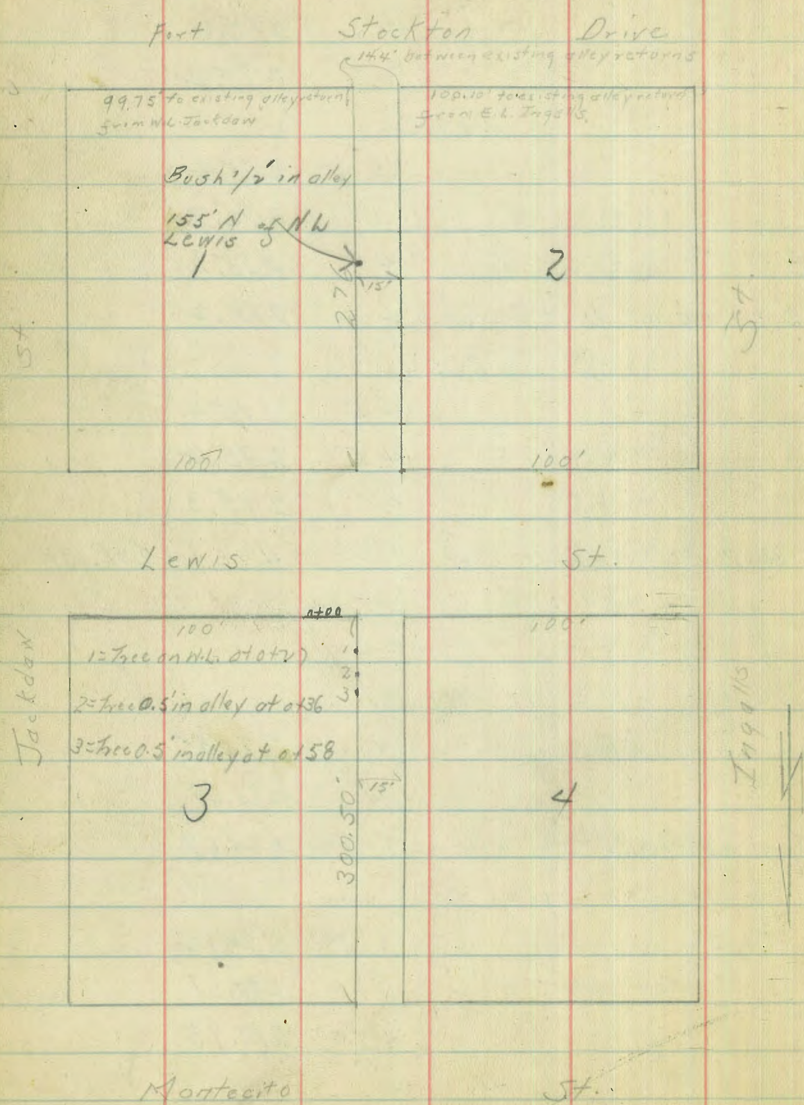
℄ 8' Garage 4' Back W.L. First Floor		4.0	273.7

1+25

W		4.0	273.7
℄		4.1	273.6
E		4.2	273.5

	℄ 277.65		
T.P		-3.79	273.86
	+6.00		
	℄ 279.86		
	1+33		
℄ 14' Garage 1' Back E.L. Concrete Floor			
North end edge floor		5.93	273.93
South " " "		5.96	273.90
	1+48		
℄ 10' Garage 4.5' Back E.L. Concrete Floor		5.65	274.21
	1+50		
E		5.9	274.0
℄		5.5	274.4
W		5.5	274.4
	1+75		
W		5.2	274.7
℄		5.2	274.7
E		5.3	274.6
	1+79		
℄ 8' Concrete Garage Apron 1.5' Back W.L.		5.12	274.74
	1+95		
℄ 14' Double Garage 1' Back W.L. Concrete Floor			
South end edge floor		4.48	275.38
North " " "		4.46	275.40

	℄ 279.86		68
	2+00		
E		5.1	274.8
℄		4.9	275.0
W		4.7	275.2
	2+25		
W		4.5	275.4
℄		4.6	275.3
E		4.8	275.1
Ost 2' ℄ 8' Garage Dirt Floor		4.7	275.2
	2+50		
E		4.5	275.4
℄		4.5	275.4
W		4.6	275.3
T.P		4.98	274.88
	2+59		
	℄ 282.47		
	2+76 = S.L. Lewis		
W Tp c.b. + paving flush		7.62	274.85
℄		8.06	274.41
E Tp c.b. + paving flush		7.80	274.67
	South gutter line Lewis		
E		8.65	273.82
℄		8.60	273.87
W		8.54	273.93



J.C. Bliss

X-section Alley Block 1 Washington Hts - Lewis to Montecito between Jackdaw + Ingalls - 15' wide

⊼ 282.47 (Page 68)

North Gutter Line Lewis

W	8.59	273.88
℄	8.82	273.65
E	8.90	273.57
N L Lewis = 0+00		
E Tp cb + paving flush	8.10	274.37
℄	8.29	274.18
W Tp cb + paving flush	7.85	274.62
0+25		
W	6.4	276.1
℄	6.7	275.8
E	6.3	276.2
0+44		
℄ 8' Garage 6.5 Back E.L. Dirt Floor	6.5	276.0
0+50		
E	6.1	276.4
℄	6.2	276.3
W	6.0	276.5
0+75		
W	5.3	277.2
℄	5.6	276.9
E	5.6	276.9

Plotted 12/12/39 TL

	T 282.47		
	0+93		
℄ 10' Garage 2' Back W.L. Dirt Floor		5.1	277.4
	0+94		
℄ 8' Garage 2' Back E.L. Dirt Floor		5.5	277.0
	1+00		
E		5.4	277.1
℄		5.1	277.4
W		5.1	277.4
	1+07		
℄ 8' Garage 5.5' Back E.L. Concrete Floor		5.26	277.21
	1+16		
℄ 8' Garage 5.5' Back E.L. Dirt Floor		5.4	277.1
	1+25		
℄ 2.5' Concrete walk at W.L.		4.67	277.80
W		4.8	277.7
℄		5.0	277.5
E		5.1	277.4
	1+43		
℄ 8' Concrete Garage Apron 0.5' Back W.L.		4.5V	277.95
	1+50		
E		4.9	277.6
℄		4.9	277.6
W		4.8	277.7
	1+59		
℄ 8' Garage Apron 3' Back E.L. Concrete		5.2V	277.22

	T 282.47		
	1+75		
W		4.8	277.7
℄		4.6	277.9
E		4.8	277.7
	1+94		
℄ 8' Garage 3' Back W.L. Concrete Floor		4.54	277.93
	2+00		
E		4.9	277.6
℄		4.8	277.7
W		4.6	277.9
	2+25		
N		5.0	277.5
℄		5.1	277.1
E		5.2	277.3
7.0		5.4V	277.05
	+0.9V		
	T 277.95		
	2+40		
℄ 10' Garage 4.5' Back E.L. Dirt Floor		0.9	277.1
	2+50		
E		1.3	276.7
℄		1.2V	276.8
W		1.1	276.9
	2+52		
℄ 12' Concrete Apron at E.L. (Level)		1.2V	276.75

27797.

	2+65	
℄ 27' Concrete Garage Apron at		W.L.
South end edge apron	1.21	276.86
North " " "	2.40	275.57
	2+75	
W	2.4	275.6
℄	2.2	275.8
E	2.3	275.7
	2+61	
℄ 2' Concrete walk at E.L.	1.60	276.37
3+00.50 = S.L. Montecito		
E Tpcb	3.60	274.37
G	3.74	274.23
℄	3.80	274.17
W Tpcb & paving flush	3.88	274.09
South Gutter Montecito		
W	4.65	273.32
℄	4.44	273.53
E	4.34	273.63

Note - Paving at alley on Montecito is in poor condition.

B.M. S.W.B.P. Montecito & Jackdaw	2.48	275.49
	Correct	275.50

20' wide — x See Alley Blk 173 U.H. — Lincoln to Polk — Bet Mississippi & Louisiana Sts.

Miller McHugh J.E. Bliss Garage

S.E. Univ & Mississippi

B.M.	10.51	292.50		281.99	
T.P.	7.67	300.05	0.12	292.38	
T.P.	4.49	301.33	5.21	294.84	S.E. Lincoln & Louisiana
Set B.M. B.P.			1.35	299.98	

14' N. of N. el. Line Lincoln = {N. End Pavmt. / N. End emt. el. Returns}

E. on emt. el Alley ret.			9.39	291.94
E. " pavmt.			9.55	291.78
℄ " "			10.33	291.00
W " "			10.68	290.65
W. on emt. el. Alley Ret			10.53	290.80

0+00 = N. Line Lincoln Ave = 20' N. of N. el. of Lincoln

W			10.6	290.7
℄			10.4	290.9
E			9.3	292.0

Plotted 7-23-30 CBH

0+15' N

E			10.5	290.8
℄			10.6	290.7
W.			10.9	290.4
T.P.	11.10	301.86	10.57	290.76

0+41 N = double garage 2.5 W. of W. Line emt. floor ✓

W-2.5 floor garage			11.49	290.37 ✓
W			11.2	290.6
℄			11.1	290.8
E			11.2	290.6

301.86

0+75 N

E		10.8	291.0
℄		11.0	290.9
W		11.1	290.8
+5		11.1	290.8

1+00

W		9.7	292.2
℄		10.2	291.7
E		9.8	292.1

1+40 double garage on E dirt floor 0.4 E. of E. Line ✓

E-0.4 floor		8.3	293.6 ✓
E		8.3	293.6
℄		8.2	293.7
W		7.1	294.8

1+75

W		5.1	296.8
℄		5.9	296.0
E		6.3	295.5

1+87 garage on W emt. floor 0.8 Back ✓

E		5.8	296.1
℄		5.4	296.5
W		5.0	296.9
W+0.8		4.55	297.31 ✓

2+35 garage on W. dirt floor 1.3 Back ✓

W-1.3		3.1	298.8 ✓
W		3.1	298.8
℄		3.9	298.0
E			

301.86

2+13

S. End Shack on E. 1.0 in Alley ✓

From 2+33 To 2+40 projection on above shack 3.0 in Alley ✓

2+50

N. End above shack 1.0 in Alley ✓

2+65

E		3.6	298 3
℄		2.9	299 0
W.		2.2	299.7
	3+00		
W		1.2	300 7
℄ Top M.H.		1.49	300 37 ✓
℄ ground		1.7	300.2
E.		1.8	300.1

3+09 garage on E. dirt floor 0.8 in Alley ✓

E+0.8 floor		1.8	300.1 ✓
	3+25		
E		1.2	300.7
℄		1.1	300 8
W		0.6	301.3
T.P.	9.40 310.96	0.30	301.56

3+55 { garage on W. dirt floor 1.5 Back
" " E. " " 0.2 "

W-1.5 floor		8.8	302 1 ✓
W		8.8	302.1
℄		9.0	301.3
E floor		9.3	301.6 ✓

310.96

3+75

E		8.5	302 4
℄		8.7	302 2
W.		8.2	302.7

4+00 S. End 5 garages on W. 5.2 Back ✓

W.- floor		5.62	305.34
W. on E. Edge cmt. Apron		6.52	304 44 ✓
+1		7.1	303.8
℄		8.2	302.7
E.		8.1	302 8
	4+25		
E		7.7	303 2
℄		7.8	303.1
W on E. Edge cmt. Apron		6.3	304 6

4+41 garage on E cmt. floor 0.5 in Alley ✓

4' W. of E. line on W. edge cmt. Apron		7.47	303 49 ✓
0.5 W. of E line floor		7.40	303 56 ✓

4+50 N. End above garages on W. ✓

W-5.2 floor		5.63	305 33 ✓
W. on E. End cmt. Apron		6.10	304 86 ✓
+1		6.5	304 4
℄		7.2	303 7
E.		7.1	303 8
	4+75		
E		6.6	304 3
℄		6.7	304 2
W		5.8	305.1

3 10.96

4+91 garage on E. dirt floor 0.4 in Alley ✓			
W	5.9	305 0	
℄	6.4	304 5	
E floor	6.6	304 3	✓
5+07 garage on E dirt floor 3.5 Back ✓			
E - 3.5	6.2	304.7	✓
E	6.1	304 8	
℄	5.9	305 0	
W	5.3	305.6	
5+32 garage on W dirt floor 0.5 Back ✓			
W. floor	4.4	306 5	✓
℄	5.2	305.7	
E	5.7	305.2	
+3	6.0	304 9	
5+44 garage on W. dirt floor 0.5 Back ✓			
E - 3	5.2	305.7	
E	5.0	305 9	
℄	4.4	306 4	
W floor	3.8	307 1	✓
5+75			
W	2.6	308 3	
℄	3.2	307 7	
E	3.8	307 1	
+2	3.8	307.1	
6+00 = 5. Line Polk Ave			
E	2.7	308 2	
℄	2.3	308 6	
W	1.8	309 1	

Alley 173 24 H.

3 10.96

T.P.	9.91	313.65	7.22	303.74	
T.P.	12.95	326.47	0.13	313.52	
					S.E. Texas + Polk Ave
chk on BM.			1.52	324.95 = 324.95	

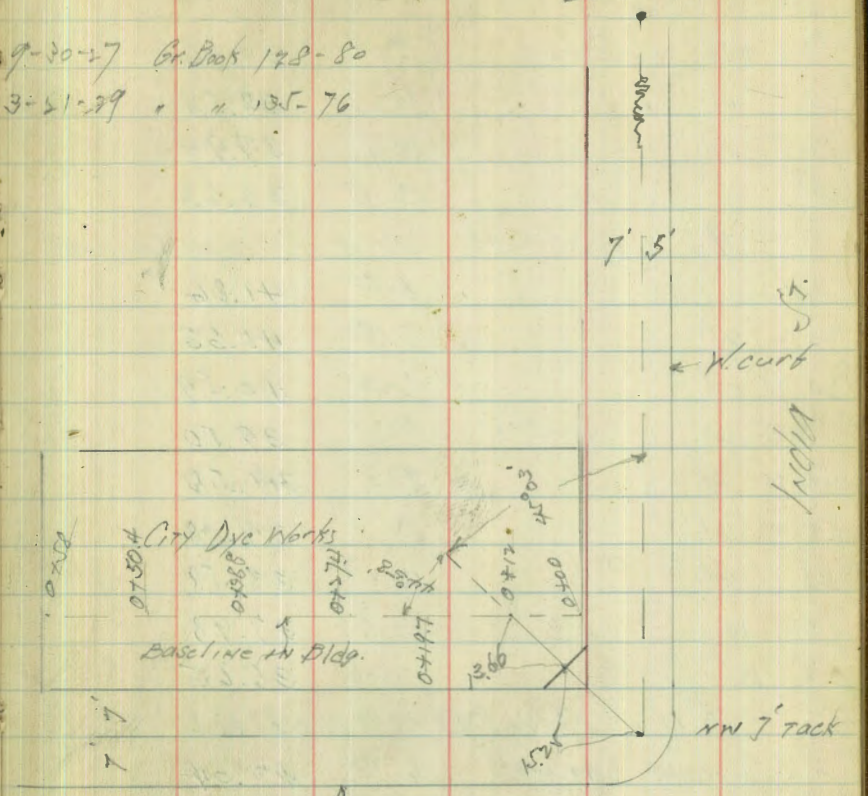
Levels on NW Cor. India & Kalmia and floor of City Dye Works

Moore Sisson Northern 4-5-34

SW 7' rack Laurel & India

75

				BM. used	9-30-27 Gr. Book 128-80
SW BP India Juniper	2.57	49.44	46.87	" "	3-21-29 " " 135-76
T.P.	6.93	48.81	41.88		
	N. cb. of Kalmia				
WL India	Top cb	7.11	41.70	Grade Pt. 3-21-29	
0.8 W	" "	7.17	41.64		
"	Crow ft. Set 3-21-29	7.45	41.36	gutter	
20.6 W of WL	Top cb	8.22	40.59		
" " "	gut	8.68	40.13		
25.2 W of WL	Top cb	8.45	40.36		
" " "	gut.	8.92	39.89	Grade Pt. 3-21-29	
40.5 W of WL	Top cb.	9.26	39.55		
" " "	gut	9.80	39.01		
50.3 W	" Top cb	9.73	39.08		
" "	" Crow foot	10.43	38.38	Set 3-21-29 near line of Drain	
60 W of WL	Top cb	10.32	38.49		
" "	" gut	10.98	37.83		
75.5 "	" Top cb	10.90	37.91		
" "	" gut	11.56	37.25		
100 "	" Top cb	12.22	36.59		
" "	" gut	12.94	35.87		
	4.5 N of N curb Kalmia = Edge Sidewalk				
WL India		7.00	41.81		
20.6 W		8.13	40.68		
40.5 W		9.19	39.62		



4881

50.3 N of WL India	9.75	39.06
60 " " "	10.27	38.54
72.5 " " "	10.87	37.94
100 " " "	12.18	36.63
9.5 N of N. curb Kalmia = Ledge Sidewalk		
WL India	6.95	41.86
30.6 W	8.18	40.63
30.7 W	8.22	40.59
40.5 W Sunken	9.31	39.50
40.6 W	9.23	39.58
50.3 W	9.73	39.08
60 W	10.23	38.58
72.5 W	10.83	37.98
100 W	12.16	36.65
14' N of N curb Kalmia = NL X.		
WL India Cem. walk	6.77	42.04
30.6 W " Col. Base	7.82	40.99
40.5 W " " "	8.95	39.86
50.3 W Cem. walk	9.46	39.35
60 W Conc. Col. Base	9.93	38.88
72.5 W Conc. Dr.	10.16	38.65
100 W Conc. Dr.	11.09	37.72
NL Kalmia & WL India	7.05	41.76 Top cb El. 41.80 = 9-30-77 Gr. Bk. 128-80

4881

20' N of N cb Line Kalmia

WL India	6.61	47.70
W cb " Top cb	6.91	41.90
" gut	7.27	41.54

30' N of N cb Kalmia

WL India	6.27	47.54
W cb Top	6.51	47.30
" gut	6.85	41.96

48' N of N cb Kalmia

WL India	5.62	43.19
W cb " Top	5.78	43.07
" gut	6.18	47.67

64' N of N cb Kalmia

WL India	5.00	43.81
W cb Top	5.43	43.38
" gut	5.78	43.03
T.P.	6.93	41.88

Levels on floor Bldg. p 98

Levels on Cert. Floor of City Dye Work Bldg

T.P.	4.98	46.81 ✓		41.88
0+00 Baseline				
Baseline			4.52	47.29
20 N			4.49	47.32
7 S			4.53	47.28
0+12				
Baseline			4.55	47.26
12 S			4.58	47.23
20 N			4.52	47.29
0+19.7				
Baseline			4.73	47.08
6 S			4.72	47.09
5 N			4.72	47.09
12 N			4.76	47.05
20 N			4.52	47.29
0+27.4				
Baseline			4.92	41.89
12 S			4.65	47.16
5 N			4.88	41.93
12 N			4.68	47.13
20 N	Could not See			
0+38.8				
Baseline			4.86	41.95
8 S			4.79	47.02
5 N			4.87	41.94

46.81

12 N			4.81	47.00
20 N			4.63	47.18
T.P.	4.97	47.05 ✓	4.72	47.08 +
0+50.4				
Baseline			4.98	47.07
12 S			4.87	47.18
5 N			4.95	47.10
20 N			4.85	47.20
0+58 - W end Bldg.				
20 N			4.77	47.28
5 N			4.82	47.23
Baseline			4.83	47.22
12 S			4.86	47.19
T.P.	5.04	47.12 ✓	4.97	47.08 +
T.P.	7.59	49.47 ✓	5.24	41.88 +
ch. to BM			2.60	46.87 ✓ 46.87

Swap Indian Juniper

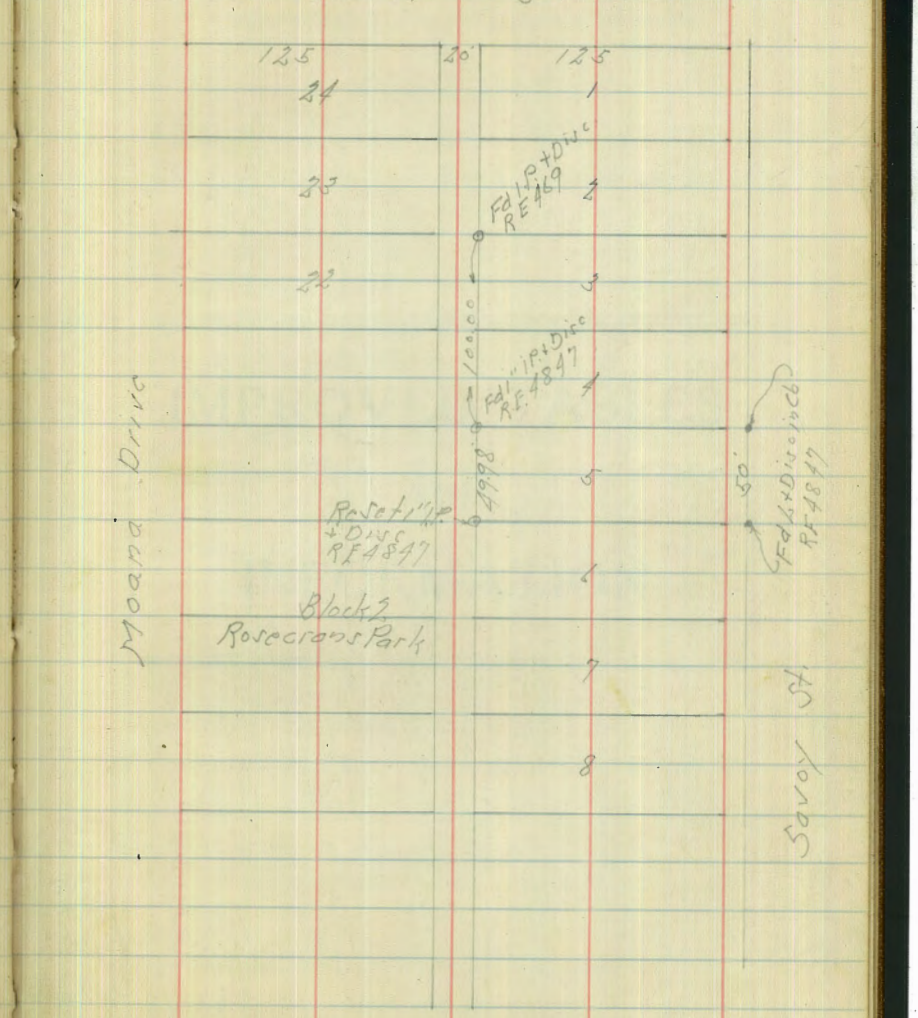
ReSet South West Corner Lot 5
Block 2 Tract 1878 Rosecrans Park

June 13-47
S. Nan
McCoy
Hilen
Williams

W.O. 21018

This Corner Destroyed by
City Blade

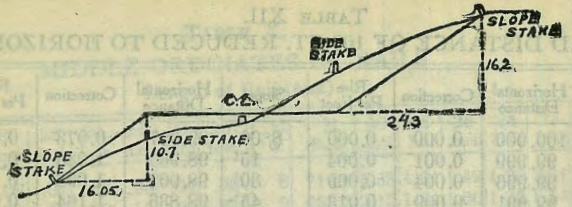
Indexed
C.S.N.



IMPROVED TABLES

AND

INFORMATION



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1 65	1 80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3 45	3.60	3 75	3.90	4.05	4.20	4 35	2
3	4.50	4 65	4.80	4.95	5 10	5 25	5 40	5.55	5.70	5.85	3
4	6.00	6 15	6.30	6.45	6.60	6 75	6.90	7.05	7.20	7.35	4
5	7 50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9 00	9 15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10 65	10.80	10.95	11.10	11.25	11.40	11.55	11 70	11.85	7
8	12.00	12 15	12.30	12.45	12.60	12.75	12.90	13 05	13.20	13.35	8
9	13 50	13 65	13 80	13 95	14.10	14.25	14.40	14 55	14.70	14.85	9
10	15.00	15 15	15 30	15 45	15.60	15.75	15.90	16.05	16.20	16 35	10
11	16 50	16 65	16 80	16.95	17 10	17.25	17.40	17.55	17.70	17.85	11
12	18 00	18 15	18.30	18 45	18.60	18 75	18.90	19.05	19.20	19 35	12
13	19 50	19 65	19.80	19.95	20.10	20.25	20 40	20.55	20.70	20.85	13
14	21.00	21 15	21.30	21.45	21 60	21.75	21.90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24 15	24 30	24 45	24.60	24.75	24 90	25 05	25.20	25.35	16
17	25.50	25 65	25.80	25 95	26.10	26 25	26 40	26.55	26.70	26.85	17
18	27.00	27 15	27.30	27 45	27.60	27.75	27.90	28.05	28 20	28.35	18
19	28 50	28 65	28 80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30 00	30 15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31 50	31 65	31.80	31.95	32 10	32 25	32.40	32.55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33.60	33 75	33.90	34.05	34.20	34.35	22
23	34 50	34 65	34.80	34.95	35.10	35 25	35 40	35.55	35.70	35 85	23
24	36.00	36 15	36.30	36 45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37 80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39 00	39 15	39.30	39 45	39 60	39.75	39.90	40.05	40.20	40.35	26
27	40 50	40 65	40 80	40.95	41.10	41.25	41 40	41.55	41.70	41.85	27
28	42 00	42 15	42.30	42.45	42.60	42 75	42.90	43.05	43.20	43.35	28
29	43 50	43 65	43.80	43 95	44.10	44 25	44 40	44.55	44.70	44 85	29
30	45 00	45 15	45.30	45 45	45.60	45.75	45.90	46.05	46 20	46.35	30
31	46.50	46.65	46.80	46 95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48 00	48.15	48.30	48 45	48.60	48 75	48.90	49.05	49 20	49.35	32
33	49 50	49 65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51 00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52 50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54 00	54 15	54.30	54 45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55 50	55 65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57 00	57.15	57.30	57 45	57.60	57 75	57.90	58.05	58.20	58 35	38
39	58 50	58.65	58 80	58.95	59.10	59 25	59.40	59 55	59.70	59.85	39
40	60 00	60 15	60 30	60 45	60 60	60.75	60 90	61.05	61 20	61.35	40
41	61.50	61 65	61 80	61 95	62 10	62 25	62.40	62 55	62 70	62.85	41
42	63 00	63.15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64.35	42
43	64.50	64 65	64 80	64.95	65.10	65 25	65 40	65.55	65.70	65.85	43
44	66 00	66 15	66.30	66.45	66.60	66 75	66.90	67.05	67.20	67.35	44
45	67 50	67 65	67 80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69 00	69 15	69 30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70 50	70 65	70 80	70 95	71.10	71.25	71 40	71.55	71.70	71.85	47
48	72.00	72 15	72.30	72.45	72.60	72.75	72.90	73 05	73.20	73 35	48
49	73 50	73 65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

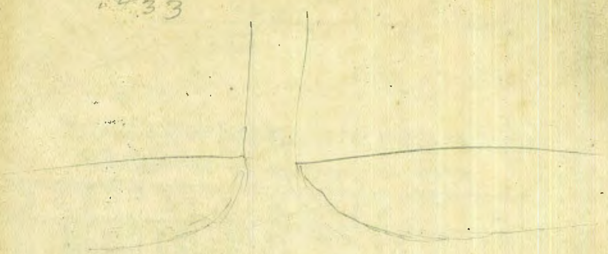
Computed by L. Leland Locke.

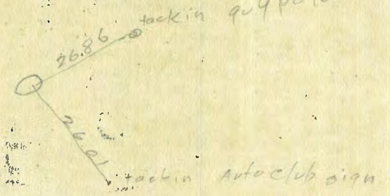
291.94
4.20
296.14

E Gutter & W Gutter

5.25 5.64 6.03
290.89 290.50 290.13 on East 8' back 4.90
291.24

343.75
4.33





5 39.34
600.31
90.33
1229.67

144
99.75
100.1
214.25
107.12

107.12
99.75
7.37

Catalina & Peru 100' N of Tank
N.E. Mon. 375.16

94.49
5.51.79
42.70
3
72.10