

1349

MS

FIELD BOOK

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1.0 index to pg 75 of volume 44.

S'ly. Prod. of Dora St. from Ramona	2
Helen	5
Lois	7
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" " Isabelle " " "	22
X-Sec. - La Mesa to La Mesa Colony	31
Alley Blk 9 1/2 City Hts. Nightmare Landis	37
Edgewood C to Beech	47

1.0 reduced to 75 6/1000000 4/11.

1

	H.I.	-	Elev
	483.15		
E		10.2	473.0
		2+00	
E		11.7	471.5
Φ		11.4	471.8
W		9.8	473.4
		2+50	
W		10.6	472.6
Φ		12.9	470.3
E		14.5	468.7
T.P.	2.01	472.56	12.60 470.55
		3+00	
E		6.4	466.2
Φ		3.4	469.2
W		0.6	472.0
		3+50	
W		1.6	471.0
Φ		4.2	468.4
E		7.0	465.6
		3+82	
E		8.3	464.3
Φ		5.0	467.6
W		2.7	469.9
		4+00	
W		3.7	468.9
Φ		6.5	466.1
E		9.7	462.9

	H.I.	-	Elev
	472.56		
	4+90		
E		12.3	460.3
Φ		9.4	463.2
W		6.8	465.8
	4+70		
W		9.6	463.0
Φ		12.1	460.5
E		14.6	458.0
	5+00		
E		16.3	456.3
Φ		14.9	457.7
W		12.3	460.3
T.P.	0.96	460.37	13.15 459.41
		5+50	
W		4.2	456.2 ✓
Φ		5.8	454.6 ✓
E		6.9	453.5 ✓
	5+83		
E		8.9	451.5
Φ		7.7	452.7
W		6.5	453.9
	5+88		
W		8.3	452.1
Φ		9.3	451.1
E		10.2	450.2
	6+00		
E		9.7	450.7

	HZ	-	Elev
	460.37		
Φ		8.8	451.6
W		7.8	452.6
		6.50	
W		9.9	450.5
Φ		10.8	449.6
E		11.9	448.5
		6.60	
E		12.4	448.0
Φ		11.6	448.8
W		10.6	449.8
		7.00	
W		11.9	448.5
Φ		12.5	447.9
E		13.2	447.2
		7.35	
E		13.2	447.2
Φ		12.2	448.2
W		10.9	449.5
T.P.	5.68	956.02	10.03 450.34
		7.50	
W		5.7	450.3
Φ		7.0	449.0
E		8.3	447.7
		7.80	
E		8.4	447.6
Φ		6.7	449.3

	HZ	-	Harkin
	456.02		554
		7.80	
		5.1	450.9
		8.50	
W		9.8	451.2
Φ		6.5	449.5
E		8.1	447.9
		9.00	
E		8.7	447.3
Φ		6.9	449.1
W		5.4	450.6
		9.50	
W		4.5	451.5
Φ		7.0	449.0
E		8.6	447.4
		10.00	
E		8.9	447.1
Φ		6.3	449.7
W		9.1	451.9
T.P.	9.27	960.05	5.24 450.78
T.P.	11.83	471.13	0.75 459.30
T.P.	13.06	483.14	1.05 470.08
		0.59	482.55
			482.53
			0.02

4

Bill Glass
May 22, 1919

Prop and ϕ Levels on Helen Street
South of Ramona St to Mesa Colony

		42		42
		+	-	+
		467.31		459.02
B.M.	8.29	475.49		467.20
		475.45		466.49
T.P.	896	483.63	0.82	474.67

Set on X-Section of this See Page 7 Spc & Ramona Levels

E. Canyon

Bld

Plotted 28
6-1-29

		0100	
W		7.5	468.0
ϕ		7.9	467.6
E		7.1	468.4

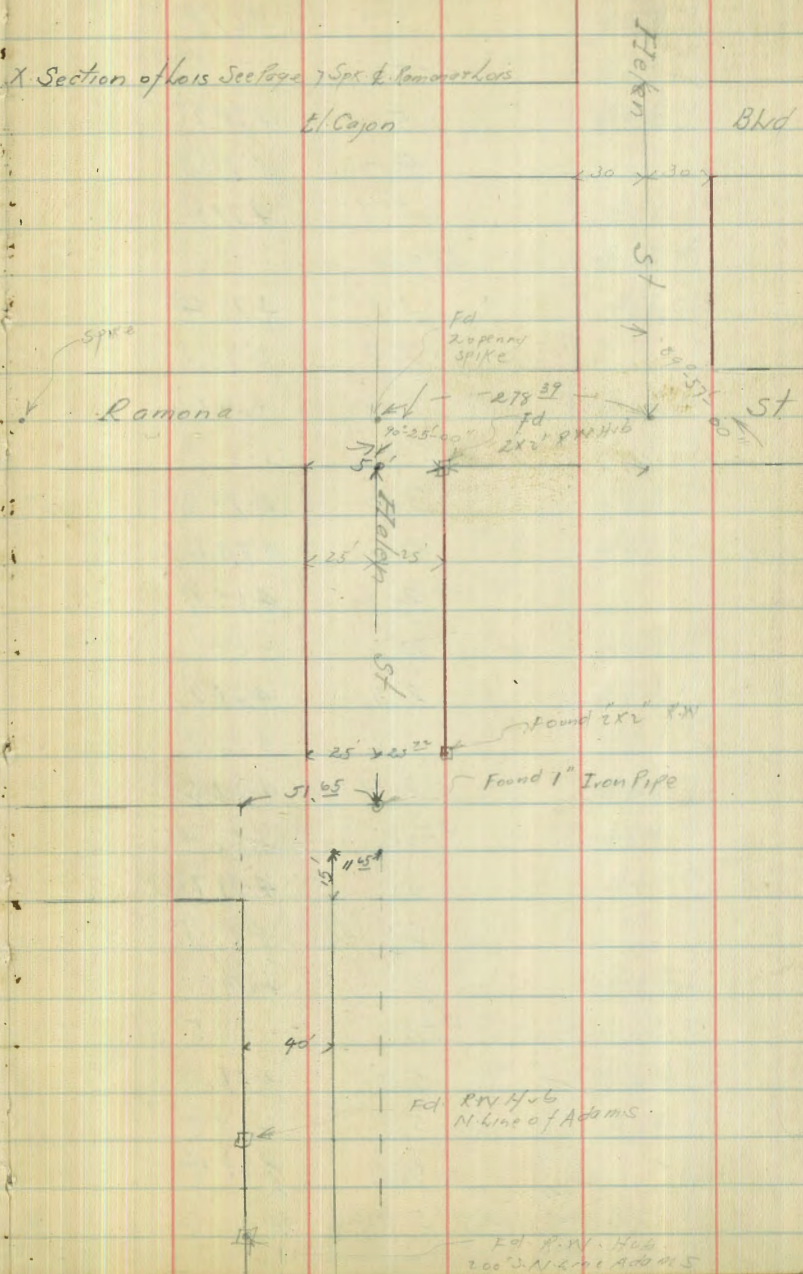
		0112	
E		6.0	469.5
ϕ		7.2	468.3
W		7.1	468.4

		0150	
W		7.2	468.3
ϕ		6.2	469.3
E		5.7	469.8

		1400	
E		5.3	470.2
ϕ		5.6	469.9
W		5.9	469.6

		1450	
W		5.7	469.8
ϕ		5.0	470.5
E		4.7	470.8

		2700	
E		4.4	471.1
ϕ		4.7	470.8



H.I. - Elev
~~483.63~~
475.95

	H.I.	-	Elev
W		5.7	469.8
		2150	
W		5.0	470.5
☺		4.2	471.3
E		3.7	471.8
		3100	
E		3.1	472.4
☺		3.4	472.1
W		4.0	471.5
		3150	
W		3.2	472.3
☺		2.5	473.0
E		2.6	472.9
		3175	
E		2.5	473.0
☺		2.8	472.7
W		2.9	472.6
		4100	
W		3.8	471.7
☺		3.4	472.1
E		3.5	472.0
		4150	
E		5.5	470.0
☺		5.8	469.7
W		6.1	469.4
T.P.	0.71	470.17 478.35	469.46 477.64

H.I. - Elev
~~478.35~~
470.17
5100

	H.I.	-	Elev
W		2.5	467.7
☺		2.4	467.8
E		1.9	468.3
		5142 ³⁰	
E		3.6	466.6
☺		3.8	466.4
W		4.0	466.2
		5167.30	
E		4.2	466.0
☺		4.7	465.5
W		4.5	465.7
+26 ²⁵		4.3	465.9
		5192 ³⁰	
-26 ²⁵		5.7	464.5
-06 ²⁵ ☺ County		5.7	464.5
W		5.7	464.5
☺ E Line Contour		5.5	464.7
☺		5.3	464.9
E		5.3	464.9
		6100	
E		5.6	464.6
+5		6.0	464.2
☺		5.7	464.5
W		6.2	464.0
		6107 ³⁰ N. Line Contour ^{See Sp. 76}	
W		6.3	463.9

(continued on Page 131)

X Section Lois Street South of
Ramona H.I. - Elev

Sta	H.I.	Elev
2.15	467.47	465.32
T.P.	8.18	467.20
	8.45	459.02
	0+00	
W	7.7	459.5
+7	7.9	459.3
+13	7.4	459.8
+20	7.2	460.0
+33	7.0	460.2
+90.5	7.1	460.1
	0+36	
-40.5	6.2	461.0
-32	6.1	461.1
-30	7.1	460.1
-24	6.8	460.4
-20	6.7	460.5
-8	7.2	460.0
-6	6.8	460.4
W	6.9	460.3
	0+50	
W	6.8	460.4
+5	6.7	460.5
17	7.0	460.2
+16	6.6	460.6
120	6.6	460.6
+23	6.6	460.6

Plotted
6-21-29

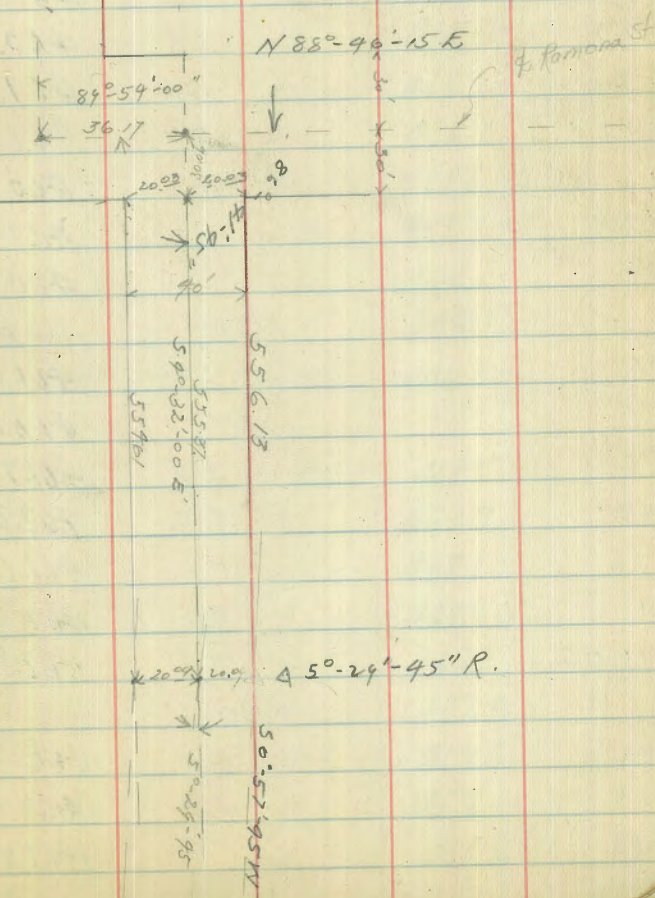
on sv. Nails
in pole 2100 ft
5/10/15

THIS P. USED
AS B.M. IN 1820
of H.C.H.

El Cajon Blvd

S. line of El Cajon Blvd.

This sketch taken from County
Highway Survey



	+	H.Z. 467.20	-	Elev
+30			7.0	460.2
+32			6.3	460.9
+38			6.3	460.9
+40 E line			6.1	461.1
		1100		
-40 E line			5.7	461.5
-38			6.0	461.2
-30			6.3	460.9
-25			6.3	460.9
-20			5.8	461.4
-15			5.9	461.3
-9			6.5	460.7
-7			6.2	461.0
W			6.6	460.6
		1150		
W			5.7	461.5
+7			5.1	462.1
+9			5.5	461.7
+20			5.0	462.2
+28			5.6	461.6
+37			4.8	462.4
+40 E line			4.4	462.8
		2100		
-40			2.9	464.3
-39			3.5	463.7
-32			3.4	463.8

	+	H.Z. 467.20	-	Elev
-23			3.3	463.9
-20			3.2	464.0
-9			3.9	463.3
-7			3.5	463.7
W			3.9	463.3
		2150		
W			1.6	465.6
+6			1.5	465.7
+7			1.8	465.4
+16			1.0	466.2
+20 E			1.1	466.1
+28			1.6	465.6
+30			1.9	465.3
+31			1.1	466.1
+40 E			0.7	466.5
T.P.	5.39	471.89	0.70	466.50
		3100		
-40			3.9	468.5
-39			4.0	467.9
-31			3.8	468.1
-30			4.6	467.3
-23			4.1	467.8
-20			4.0	467.9
-15			4.3	467.6
-10			4.8	467.1
W			5.3	466.6

	HE 471.89	-	Elev
+35		7.5	464.4
+40 E		7.1	464.8
		51.67	
-40 E		7.8	464.1
-35		7.9	464.0
-30		8.3	463.6
-27		8.1	463.8
-24		7.7	464.2
-20 E		7.6	464.3
-17		7.5	464.4
-14		7.8	464.1
-9		8.1	463.8
W		8.2	463.7
		61.00	
W		9.2	462.7
+5		9.1	462.7
+8		9.5	462.4
+20 E		8.7	463.2
+25		8.8	463.1
+30		7.3	462.6
+40		8.7	463.2
		Star Walk on East	
	1 st back & walk	9.01	462.88
-40 E		9.3	462.6
-30		9.9	462.0
-26		9.5	462.4

	HI 471.89	-	Elev
-20		9.3	462.6
-10		10.0	461.9
W		9.7	462.2
		61.50	
W		10.2	461.7
+4		10.1	461.8
+6		10.5	461.4
+20 E		10.0	461.9
+30		10.5	461.4
+36		10.2	461.7
+40 E		9.7	462.2
		61.80	
-40 E		10.2	461.7
-30		10.8	461.1
-20 E		10.7	461.2
-5		11.1	460.8
W		10.7	461.2
		71.30	
W		11.3	460.6
+5		11.4	460.5
+20		11.3	460.6
+26		11.4	460.5
+31		11.3	460.6
+40 E		10.2	461.7
TP	2.87	463.30	460.93

	HI 463.30 8100	-	Elev
-90 E		2.9	460.4
-32		2.9	460.4
-30		3.5	459.8
-20		3.0	460.3
-14		3.3	460.0
-8		3.7	459.6
W		3.5	459.8
	8150		
W		3.7	459.6
+5		3.8	459.5
+20 ϕ		3.7	459.6
+22		3.7	459.6
+29		4.3	459.0
+40 E		3.7	459.6
	8153 Walk on West on line		
09/14/12	ϕ	3.98	459.82
	9100		
-90 E		4.4	458.9
-32		4.5	458.8
-30		5.4	452.9
-27		5.4	457.9
-21		4.5	459.8
-20 ϕ		4.5	458.8
-15		4.7	458.6
-11		4.7	458.6
W		4.9	458.4

	HI 463.30	-	Elev
	9150		
W		5.6	457.7
+5		5.4	457.9
+7		6.0	457.3
+20 ϕ		5.7	457.6
+30		6.2	457.1
+40 E		5.3	458.0
	10100		
-40 E		6.0	457.3
-35		6.5	456.8
-27		6.7	456.6
-20 ϕ		6.4	456.9
W		6.5	456.8
	11100		
W		7.1	456.2
+20 ϕ		6.6	456.7
+26		6.8	456.5
+37 - line		6.8	456.5
+40 E		6.0	457.3
	11170		
-40 E		5.2	458.1
-37		5.9	457.4
-27		6.2	457.1
-20 ϕ		6.0	457.3
-13		6.4	456.9
-8		6.8	456.5

+	H.I.	-	Elev
	463.30		

W		6.9	
	11+95 N Line of Adams Ave		

KV		6.1	457.2
----	--	-----	-------

t10		5.6	457.7
-----	--	-----	-------

t20		5.1	458.2
-----	--	-----	-------

t25		5.6	457.7
-----	--	-----	-------

t35		4.5	458.8
-----	--	-----	-------

t40E		4.1	459.2
------	--	-----	-------

12+35 S Line of Adams			
-----------------------	--	--	--

-40E		3.3	460.0
------	--	-----	-------

-35		3.9	459.4
-----	--	-----	-------

-30		4.7	458.6
-----	--	-----	-------

-20φ		4.5	458.8
------	--	-----	-------

KV		5.5	457.8
----	--	-----	-------

TP	1247	473.46	2.31	460.99
----	------	--------	------	--------

TR	377	466.49	1079	462.67
----	-----	--------	------	--------

check on starting BM 3 Nails in pole SW. El Capn. Ho's		1.13	465.31	
---	--	------	--------	--

H.I.
478.35
470.17

Continued from Pg 6

		5/6x	
35		6.3	466.9
2		5.7	464.5
75		6.3	463.9
E		5.8	464.4
	6+50		
E		6.5	463.7
+5		6.7	463.5
+7		7.3	462.9
+11		6.6	463.6
2		6.3	463.9
126		6.5	463.7
132		7.1	463.1
140		6.7	463.5
	7+00		
40 W		7.5	462.7
-30		8.1	462.1
-25		7.7	462.5
-20 2		7.5	462.7
-6		8.2	462.0
5		7.6	462.6
E		7.6	463.6
T.P	4.38	7.55	462.62 470.80
		7+50	
E		4.3	462.7
+5		4.4	462.6
+6		5.2	461.8

H.I.
~~475.18~~
467.00

5/6x

13

		+20 2	4.8 462.2
		+25	4.9 462.1
		+30	5.4 461.6
		+40 W	5.5 461.5
	8+25		
		-40 W	5.3 461.7
		-30	5.3 461.7
		-20	4.5 462.5
		-6	4.8 462.2
		-5	4.4 462.6
		E	4.3 462.7
	8+88		
		E	5.3 461.7
		+6	5.5 461.5
		+7	6.0 461.0
		+12	5.6 461.4
		+20 2	5.6 461.4
		+25	5.9 461.1
		+30	6.1 460.9
		+40 W	6.0 461.0
	9+50		
		-40 W	5.4 461.6
		-30	5.5 461.5
		-26	4.8 462.2
		-20	4.7 462.3
		-9	4.8 462.2
		-7	5.9 461.1

	H.I.	-	Elev
	467.00		
	467.00		
-6		4.5	462.5
E		4.5	462.5
		10+00	
E		4.5	462.5
16		4.7	462.3
+7		5.7	461.3
+14		4.9	462.1
+20 E		4.9	462.1
+30		5.8	461.2
+40 W		5.9	461.1
		10+25	
-40		5.4	461.6
-30		5.4	461.6
-20		4.8	462.2
-13		4.8	462.2
-7		5.3	461.7
-6		4.8	462.2
E		4.4	462.6
		10+50	
E		3.9	463.1
+6		4.2	462.8
+7		4.7	462.3
+14		3.9	463.1
+20		4.0	463.0
+30		4.6	462.6
+40 W		4.5	462.5

	H.I.	-	Elev
	467.00		
	467.00		
		11+00	
		2.2	
-40		2.3	464.7
-35		2.1	464.9
-26		1.8	465.2
-20		1.8	465.2
-14		2.8	464.2
-7		2.1	464.9
-6		1.7	465.3
E		0.91	466.59
TP.	8.60		474.77
		11+50	
		8.1	467.1
+6		8.1	467.1
+7		8.6	466.6
+14		7.8	467.4
+20 E		7.6	467.6
+26		7.9	467.3
+35		7.8	468.4
+40 W		7.5	468.7
		12+07	N. line of Harris Ave
-40 W		5.0	470.2
-35		5.6	469.6
-26		5.8	469.4
-20 E		5.6	469.6
-14		5.8	469.4
-8		6.0	468.4
-5		5.9	469.3

+	41.	-	5/6x
	483.37		
	475.19	5.8	

E			
		12+47	S. Line of Adams Ave
E		5.1	470.1
+6		4.6	470.6
+10		5.1	470.1
+14		4.5	470.7
+20 S		4.2	471.0
+27		4.1	471.1
+40 W		4.0	471.2
I.P.	0.41	464.27 471.45	463.86 472.04
I.P.	8.13	469.78 476.97	456.66 464.89

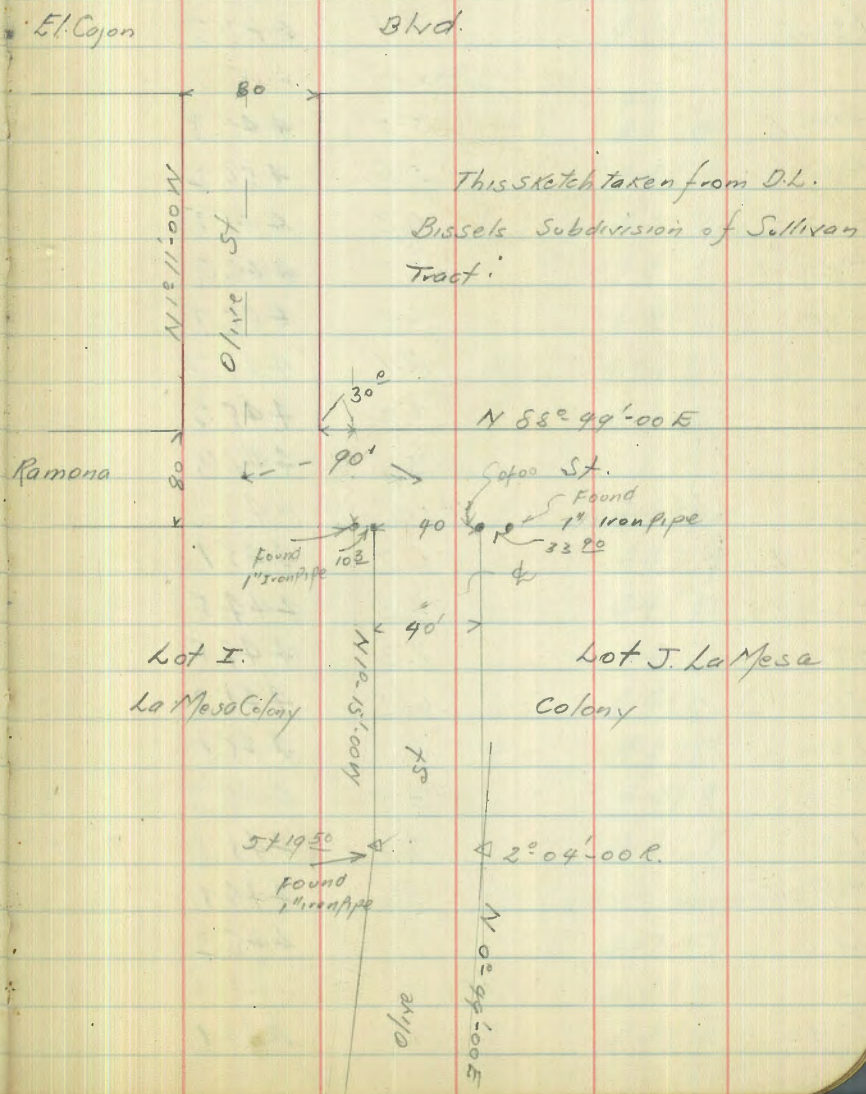
check out on
I.P. used on Sec. off's

Bill Bliss
 Joe Duermit
 J. Jacobszoon
 P. Kierman
 5/27/29

X-Section Olive Street La Mesa Colony
 from the South line of Ramona 1000' South
 + H.I. - Elev.

B.M.	2.95	460.99	958.04	SW. Nail in Pole El Cajon + Olive
I.P.	0.42	951.78	9.63	951.36
			0700	
N		2.0		449.8
+5		2.4		449.4
+10		2.0		449.8
+20 ϕ		1.2		450.6
+25		1.3		450.5
+31		2.1		449.7
+40 E		1.8		450.0
		0750		
-40		3.1		448.7
-31		3.5		448.3
-23		2.6		449.2
-20 ϕ		2.6		449.2
-10		3.4		448.4
-5		4.0		447.8
-9		3.1		448.7
N		2.6		449.2
		1700		
N		5.0		446.8
+2		5.2		446.6
+5		5.6		446.2
+10		5.2		446.6
+15		4.9		446.9

Plotted
 6-3-29



This sketch taken from D.L.
 Bissels Subdivision of Sullivan
 Tract.

Lot I. La Mesa Colony
 Lot J. La Mesa Colony

Found 1" iron pipe
 102
 33 20
 Found 1" iron pipe

5719.50
 found 1" iron pipe

N 0° 49' 00\"/>

	H.I. 95:78	Elev
-3		80
W.		7.6 444.2
+5		7.3 444.5
+12		9.1 442.7
+16		9.5 442.3
+17		6.7 445.1
+20		6.6 445.2
+90 E		6.6 445.2
E110		6.9 444.9
E115		8.6 443.2
E120		8.3 443.5
	2120	
E-15		7.8 444.0
-12		7.7 444.1
-8		6.6 445.2
E40 E		6.6 445.2
1-20 f		6.7 445.1
-10		7.1 444.7
W		10.6 441.2
+15		10.1 441.7
	2135	
W-15		10.5 441.3
W-2		10.7 441.1
W		8.9 442.9
+2		7.9 444.4
+20 f		6.8 445.2

	H.I. 95:78	Elev
+40 E		6.3 445.5
+50		6.7 445.1
	2150	
-50		6.9 444.9
-90 E		6.4 445.4
-20 E		6.4 445.4
W		7.4 444.4
+3		9.6 442.2
+15		10.2 441.6
	2182	
W-10		7.7 444.1
W		7.8 444.0
+4		6.6 445.2
+20 f		6.9 445.4
+40 E		6.5 445.3
+95		6.5 445.3
+50		7.5 444.3
	3100	
-50		7.2 444.6
-40 E		6.3 445.5
-20		6.2 445.6
-5		6.2 445.6
W		6.9 444.9
	3122	
W		5.0 446.8
+3		6.1 445.7

	H.I.	-	Elev
	451.78		
+10		5.8	446.0
+20 ϕ		5.6	446.2
+25		5.4	446.4
+33		5.8	446.0
+40 E		5.8	446.0
		3+50	
-40 E		3.8	448.0
-35		3.9	447.9
-32		4.7	447.1
-23		4.3	447.5
-20 ϕ		4.5	447.2
-4		4.7	447.1
W		2.9	448.9
		3+65	
W		1.7	450.1
+7		3.8	448.0
+20		3.6	448.2
+32		3.6	448.2
+33		2.6	449.2
+40		2.8	449.0
+50		3.8	448.0
		4+00	
79.	10.93	460.89	1.87, 449.91
		4+00	
-50		11.1	449.7
-40		10.3	450.5

	H.I.	-	Elev
	460.84		
		9.8	451.0
		11.3	449.5
		10.8	450.0
		11.3	449.5
		10.7	450.1
		9.3	451.5
		4+50	
		8.4	452.4
		8.8	452.0
		9.2	451.6
		9.4	451.4
		9.0	451.8
		9.7	451.1
		8.8	452.0
		8.9	451.9
		4+75	
		7.7	453.1
		8.0	452.8
		8.7	452.1
		7.9	452.9
		7.9	452.9
		7.6	453.2
		7.9	452.9
		5+00	
		6.7	454.1
		6.8	454.0

+

HI.
46084

-

Elev

+

HI.
46054

-

Elev

20

+10 7.3 453.5

+20 6.9 453.9

+28 7.4 453.4

+30 6.3 454.5

+40 E 6.1 454.7

5+19⁵⁰ Δ 2°-04'00 R.

-40 E 5.1 455.7

-30 5.5 455.3

-27 6.6 454.2

-20 E 6.4 454.4

-9 6.8 454.0

-6 6.5 454.3

W 5.7 455.1

5+35

W 6.5 454.3

+10 6.5 456.3

+20 E 5.8 455.0

+26 6.1 454.7

+30 5.0 455.8

+40 E 4.4 456.4

5+50

-40 E 4.2 456.6

-30 4.9 455.9

-27 5.9 454.9

-20 E 5.4 455.4

-12 5.8 455.0

-10

W

6+00

W

+12

+20

+29

+40 E

-40 E

-30

-28

-20 E

-12

W

W

+12

+20 E

+28

+30

+40 E

-40 E

-30

-28

6.1 454.7

6.3 454.5

6+00

5.5 455.3

5.8 455.0

4.9 455.9

5.2 455.6

4.4 456.4

6+50

3.9 456.9

4.0 456.8

4.4 456.4

4.1 456.7

5.0 455.8

5.0 455.8

7+00

4.1 456.7

4.2 456.6

3.2 457.6

3.6 457.2

3.0 457.8

2.8 458.0

7+50

2.5 458.3

2.6 458.2

3.1 457.7

	HZ	-	Elev
	460.84		
-20 E		2.8	458.0
-12		3.4	457.4
-10		3.2	457.6
W		3.5	457.3
		8+00	
W		1.8	459.0
+10		1.9	458.9
+14		2.2	458.6
+20 E		1.5	459.3
+30		2.1	458.7
+40 E		1.9	458.9
T.P.	5.57	465.06	135 959.49
		8+50	
W		4.6	460.5
-30		9.8	460.3
-20 E		4.5	460.6
-13		5.3	459.8
W		4.9	460.2
		9+00	
W		4.5	460.6
+10		4.7	460.4
+14		4.8	460.3
+20 E		4.2	460.9
+30		4.9	460.2
+40 E		4.7	460.4

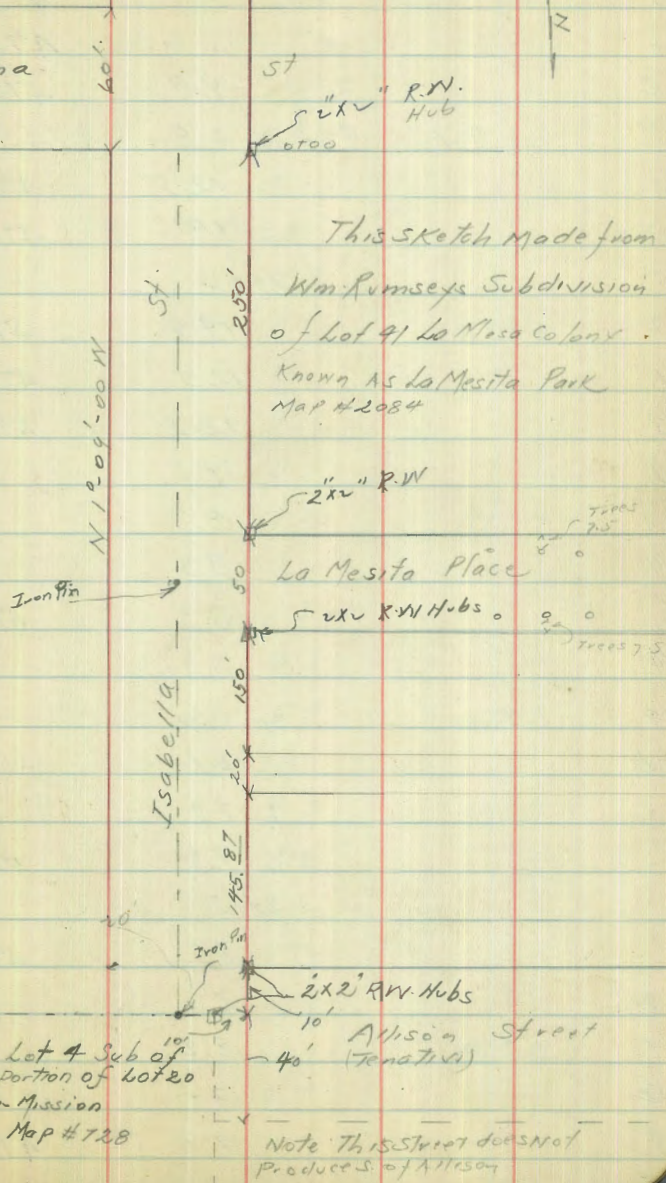
	HZ	-	Elev
	465.06		
		9+50	
-40 E		5.4	459.7
-30		5.5	459.6
-23		4.9	460.2
-20 E		4.9	460.2
-12		5.8	459.3
-8		5.0	460.1
W		5.3	459.8
		10+00	
W		5.8	459.3
+8		5.8	460.3
+12		6.9	458.3
+16		6.1	459.0
+20		5.9	459.2
+30		6.5	458.6
+40 E		6.6	458.5
TP	1.95	459.83	7.18 457.88
TP	3.63	451.78	11.68 998.15
TP	9.17	460.53	0.42 951.36
check on		2.49	958.09

Bill Bliss
 Joe Duermil
 J Jacobszoon
 P Kiernan
 June 5th 1929

Section Isabella. St. La Mesa
 Colony from the S. line of Isabella to the
 S line of Allison

BM.	1.01	482.37	481.36
		0700 = S. Line Ramona	
E	3.5	478.9	
+9	3.9	478.4	
c6	4.8	477.6	
1/4	4.5	477.9	
1/4	4.4	478.0	
1/4	4.8	477.6	
c6	5.4	476.0	
W	5.3	477.1	
	0750		
-20	70.0	472.4	
75	8.1	473.3	
W	6.9	475.5	
c6	6.8	475.6	
1/4	6.3	476.1	
1/4	5.9	476.5	
1/4	5.9	476.5	
+9	6.0	476.4	
c6	5.7	476.7	
+2	5.2	477.2	
E	5.0	477.4	
	0769		
	12" Armitage		
	Call Reddowson		
	0775		
E	5.9	476.5	
c6	6.4	476.0	
1/4	6.2	476.2	
1/4	6.3	476.1	

Ramona



0782 H. End
 on 6/8/30 22

	+	H.I.	-	Elev
		982.37		
1/4			6.4	476.0
+8			6.9	475.5
cb			7.6	474.8
+5			9.9	472.5
TP.	8.74	984.70	6.41	475.96
W			12.5	472.2
+20			14.6	470.1
		1100		
-20			14.4	470.3
W			12.5	472.2
+5			12.2	472.5
cb			9.8	
+3			8.7	
1/4			8.5	
⊘			8.3	476.4
1/4			8.3	
+9			8.6	
cb			8.1	
+2			7.7	
E			7.9	476.8
		1115		
E			7.5	477.2
cb			8.0	
+1			8.2	
1/4			8.0	
⊘			7.8	476.9

	+	H.I.	-	Elev
		984.70		
			8.1	
			8.8	
			9.2	
			10.5	
			11.1	473.6
			12.8	
		1135		
			9.8	
			8.8	475.9
			8.0	
			7.6	
			7.5	
			7.0	477.7
			7.2	
			7.3	
			6.3	
			5.9	478.8
		1150		
			4.7	480.0
			5.2	
			5.9	
			6.7	
			6.2	
			6.2	478.5
			6.9	
			7.2	

HI
984.70

t2	6.9	
W	7.9	477.3
	1725	
W	5.5	479.2
t8	5.3	
cb	5.7	
1/4	5.5	
ϕ	9.9	479.8
t5	9.9	
1/4	5.1	
t9	5.5	
cb	4.5	
t1	3.8	
E	3.4	481.3
	1794	WALK on East
ϕ concrete work	2.50	482.30
	2400	
E	2.3	482.4
t9	2.8	
cb	3.9	
t1	4.4	
1/4	3.9	
t5	3.8	
ϕ	3.9	480.8
1/4	4.5	
cb	4.7	

HI
984.70

24

t2	4.4	
W	4.6	480.1
	2450	N line of La Mesita Place
W	3.9	480.8 ^{50'57} _{10'65} 7.5 1/4
t8	3.4	
cb	3.7	
1/4	3.2	
ϕ	2.5	482.2
t5	2.4	
1/4	2.5	
cb	2.6	
t1	1.2	
E	1.1	483.6
	N cb	
E	1.6	483.1
cb	2.3	
1/4	2.1	
t5	2.2	
ϕ	2.6	482.1
1/4	3.2	
cb	3.9	
W	4.6	480.1
	N 1/4	
W	4.8	479.9
cb	3.8	
1/4	3.4	

HZ
48470

HZ
48470

25

2	2.8	481.9
1/4	2.1	
15	1.8	
cb	1.7	
E	1.4	483.3
	2	
E	1.2	483.5
15	1.5	
cb	1.8	
1/4	2.5	
2	3.0	481.7
1/4	3.5	
cb	3.9	
W	5.3	479.4
10	5.9	
	5 1/4	
-10	6.3	
W	5.4	479.3
cb	4.3	
1/4	3.5	
2	3.1	481.6
1/4	2.9	
cb	2.4	
E	1.7	483.0
	Scb	
E	2.3	482.4

cb	3.0	
1/4	3.1	
2	3.3	481.4
1/4	3.8	
cb	4.2	
W	5.3	479.4
10	6.4	
	5 Line of Merita Place = 00	
-10	6.6	
W	5.9	478.8
cb	4.6	
1/4	4.0	
2	3.5	481.2
1/4	3.4	
cb	3.8	
11	2.3	
E	1.9	482.8
	0 + 25	
E	2.3	482.4
12	3.0	
19	3.3	
cb	3.6	
11	4.6	
1/4	4.1	
2	4.3	480.4
1/4	4.8	

	+	H.I. 984.81	-	Elev	
2			9.9	474.9	cb
1/4			10.1		W
cb			10.7		+10
W			11.3	473.5	T.P.
+10			12.4		
			11.50 N Line of Alley on East		-10
-10			13.0		W
W			12.2	472.6	+5
cb			11.8		cb
1/4			11.3		1/4
2			11.0	473.8	2
1/4			11.0		+5
+4			11.0		1/4
+9			11.6		+4
cb			10.9		+9
+1			10.0		cb
E.			9.6	475.2	+1
			11.70 S Line of Alley on East		E
E			11.1	473.7	
+9			11.6		E
cb			12.2		+9
+1			13.0		cb
+6			12.5		+6
1/4			12.4		1/4
2			12.4	472.4	2
1/4			12.8		1/4

	+	H.I. 484.81	-	Elev	
					13.4
					14.3
					14.5
					12.86
					471.95
					2100
					5.8
					5.2
					468.4
					5.0
					4.9
					4.2
					3.6
					470.0
					3.3
					3.5
					3.7
					4.5
					3.6
					2.9
					2.3
					471.3
					2125
					4.8
					468.8
					5.0
					6.5
					5.7
					5.5
					5.6
					468.0
					6.4

H.I.
473.56

cb	7.3	
t5	7.4	
W	7.9	465.7
t10	8.5	
	21.50	
-10	10.1	
W	9.5	464.1
cb	8.6	
t1	8.8	
1/4	8.3	
ϕ	7.7	465.9
1/4	7.8	
t4	8.1	
cb	8.8	
t1	7.1	
E	7.5	466.0
	21.75	
E	9.6	464.0
t9	9.6	
cb	10.9	
t6	10.1	
1/4	10.0	
ϕ	10.1	463.5
1/4	10.4	
t9	11.2	
cb	10.9	

H.I.
473.56

28

W	11.4	462.1
t10	12.0	
	31.00	
-10	13.5	
W	13.2	460.3
cb	12.7	
t3	13.2	
1/4	12.6	
ϕ	12.0	461.6
1/4	12.0	
t4	12.1	
cb	13.0	
t1	11.8	
E	11.4	462.2
	2.67	
TP.	464.10	12.13. 461.93
	31.15.87	N. Line of Allison
		50.5t 10.0cb 75.19s
E	2.8	461.3
t8	3.0	
t9	4.5	
cb	4.5	
t5	3.8	
1/4	3.6	
ϕ	3.9	460.2
1/4	4.0	
t5	4.3	

HI
46410

16	38	
cb	39	
N	4.5	459.6
	N 4 1/4	
N	49	459.2
cb	4.2	
15	4.2	
16	49	
1/4	4.2	
ϕ	4.2	459.9
1/4	40	
19	45	
cb	45	
14	43	
E	39	460.2
	N:cb	
E	4.7	459.4
cb	48	
16	43	
1/4	4.7	
ϕ	51	459.0
17	54	
1/4	5.1	
14	52	
16	48	
cb	49	

HI
46410

29

	5.7	458.4
	N 1/4	
	6.4	457.7
	6.2	
	6.0	
	6.3	
	6.2	
	5.8	
	5.8	458.3
	5.5	
	5.1	
	5.3	458.8
	ϕ	
	5.8	458.3
	5.8	
	6.2	
	6.1	458.0
	6.1	
	6.5	
	6.7	
	7.0	457.1
	5 1/4	
	7.4	456.7
	6.9	
	6.7	
	6.6	457.5

H.I.
46410

30

1/4	66	
cb	6.4	
E	6.4	457.7

S. CB

E	6.7	457.4
---	-----	-------

cb	6.8	
----	-----	--

1/4	6.9	
-----	-----	--

E	7.3	456.8
---	-----	-------

1/4	7.7	
-----	-----	--

cb	8.0	
----	-----	--

N	8.1	456.0
---	-----	-------

Note Street
Does Not extend South of here (See sketch) Page 22

N	8.5	455.6
---	-----	-------

cb	8.4	
----	-----	--

1/4	8.3	
-----	-----	--

E	7.9	456.2
---	-----	-------

1/4	7.4	
-----	-----	--

cb	7.4	
----	-----	--

E	7.2	456.9
---	-----	-------

Set BM	11.55	472.84	2.87	461.29	NE Prop Hub Allison + Isabella
--------	-------	--------	------	--------	-----------------------------------

TP	13.16	485.11	0.89	471.95	
----	-------	--------	------	--------	--

TP	5.10	483.54	6.67	478.44	
----	------	--------	------	--------	--

check out		2.19	481.35	BM NW Nails in Pole Isabella + El Cajon
-----------	--	------	--------	---

481.36
481.01

Bill Bliss

X Section La Masita Place from the
E line of Isabella 250' East

492.25

31

50' st
10' cb
75' 1/4 s
SE R.W.
Hub La Masita
v Isabella 1/4

BM.	951	492.25	482.74	cb	7.3	
					7.0	
		0+00 = E line of Isabella		¢	6.8	485.4
S	95	482.7		1/4	7.2	
18	9~			cb	7.6	
9	9.9			+1	7.3	
cb	9.8			N	7.3	485.0
1/4	9.3					1+00
¢	8.8	483.4		N	5.8	486.4
1/4	9.0			+9	5.8	
cb	9~			cb	6.1	
+1	8.8			1/4	5.6	
N	8.6	483.6		¢	5.3	487.0
		0+25		1/4	5.3	
N	8.0	484.2		cb	5.7	
+9	8.0			+3	5.2	
cb	8.4			S	5.2	487.0
1/4	7.9					1+50
¢	7.6	484.6		S	3.7	488.5
1/4	7.8			+8	4.0	
cb	8.4			cb	4.3	
+1	8.1			1/4	3.9	
S	8~	484.0		¢	3.8	488.4
		0+50		1/4	3.8	
S	7.0	485.2		cb	4.4	
18	6.9			+1	4.1	

492.25

t3	3.8	
BN	3.8	488.4
	1784 WALK on South	
S	8° in street	489.38
	2400	
N	2.3	490.0
cb	2.7	
t3	3.0	
1/4	2.6	
⊘	2.3	490.0
1/4	2.6	
cb	3.1	
t2	3.0	
t3	2.6	
S	2.4	489.9
	2722 WALK on North	
	9° in street	490.53
	2450	
S	1.8	490.4
t7	1.6	
cb	2.1	
1/4	1.7	
⊘	1.4	490.8
1/4	1.6	
t6	1.9	
cb	1.8	

492.25

32

N	1.4	490.8
	2460 WALK on South	
on line	⊘ 1.51	490.74
	2490 WALK on North	
9° in street	⊘ 0.78	491.47
	3400	
N	0.5	491.7
t8	0.7	
cb	1.0	
1/4	1.0	
⊘	1.0	492.2
1/4	1.5	
cb	2.0	
t2	1.6	
S	1.7	490.5
	9.51	482.74
	check back to BM	

7-11-29
 J. C. Bliss
 Ranner
 Osborn

X-section Scott St - Lowell to
 Keats - 70' Wide - 18' cbs - 34' Roadway

B.M. Nails in Pole Lowell & Scott

+2.35

π 4.24

S.L. Lowell = 0+00

E	4.1	01
cb	3.9	03
♀	3.2	10
cb	3.0	12.1
W	3.1	11

0+50

W	2.9	13
cb	3.3	09
♀	3.5	07
cb	4.0	02
E	4.3	-01

1+00

E	4.2	00
cb	4.0	02
♀	3.3	09
cb	3.5	07
W	2.8	14

1+50

W	3.1	11
cb	3.5	07
♀	3.3	09

Plotted 7-19-29 G.M.I.

π 4.24

33

cb	3.8	04
E	4.0	02

2+00 = N.L. Keats - 70' Wide

E	4.4	-02
cb	4.2	00
♀	4.0	02
cb	4.0	02
W	3.5	07

♀ Keats

W	3.6	06
cb	4.0	02
E	4.4	-02
cb	4.7	-05
E	4.8	-06

S.L. Keats

E	4.7	-05
cb	4.7	-05
♀	4.3	-01
cb	4.2	00
W	3.9	+03

7-14-29 X-section Keats St Scott to
 J.C. Bliss Shafter - 70' wide 18' cbs - 34' Roadway
 Panner
 Oster

$\pi 4.24$

E.L. Scott # = 0100

S	4.7	-0.5
cb	4.6	-0.4
¢	4.8	-0.6
cb	4.9	-0.7
N	4.4	-0.2

0450

N	5.0	-0.8
cb	5.4	-1.0
¢	5.0	-0.8
cb	5.4	-1.2
S	5.2	-1.0

1400

S	5.7	-1.5
cb	5.7	-1.5
¢	5.3	-1.1
cb	5.5	-1.3
N	5.4	-1.2

1450

N	5.8	-1.6
cb	6.0	-1.8
¢	5.3	-1.1
cb	5.5	-1.3
S	5.1	-0.9

Plotted 7-19-29-G.M.I.

$\pi 4.24$

2400

S	6.6	-2.4
cb	6.0	-1.8
¢	5.6	-1.4
cb	6.3	-2.1
N	6.0	-1.8

2450

N	5.9	-1.7
cb	6.3	-2.1
¢	5.8	-1.6
cb	6.3	-2.1
S	6.4	-2.2

3400 = W.L. Shafter

S	5.5	-1.3
cb	6.3	-2.1
¢	5.6	-1.4
cb	6.0	-1.8
N	5.8	-1.6

T.P.

+5.30

$\pi 3.83$

w.l. + 7

N	5.2	-1.4
cb	5.6	-1.8
¢	5.0	-1.2
cb	5.2	-1.4
S	4.7	-0.9

34

-5.71 -1.47

7-3-83

⊥ Shafter

S	7.3	-35
cb	6.5	-27
⊥	6.2	-24
cb	5.5	-17
N	4.8	-10

E.L. Shafter - Wet bay sand - 10' from water

N	7.3	-035
cb	7.8	-901
⊥	8.0	-92
cb	8.1	-93
S	8.2	-94

J.C. Bliss

7-3-83

X-section Shafter - Keats to lower 11
70' wide - 18 obs - 34' Roadway

35

Nike Keats = 0+00

W	5.5	-17
cb	5.2	-14
⊥	4.9	-11
cb	6.0	-22
E	7.3	-35
-	0+50	
E	4.5	-07
cb	4.6	-08
⊥	4.9	-11
cb	4.9	-11
N	4.3	-05

Plotted 7-19-89-G.M.L.

0+50 to 1+00 - Small Wall &

drive ways 11' in st. from Nike

Drive way at South end wall 4.24 -041

North end wall 385 -002

Two drives & walk come out to wall and are flush
with top of it.

1+00

W	3.8	00
cb	4.0	-02
⊥	4.7	-09
cb	4.6	-08
E	3.8	-00

3.83

1450

E	3.9	-01
cb	4.4	-06
f	4.6	-08
cb	4.5	-07
w	3.7	+01

2+00 = S.L. Lowell

w	4.4	-06
cb	4.5	-07
f	4.5	-07
cb	4.6	-08
E	3.9	-01

B.M.S.W. Prop Hub - Lowell & Stager - 4.34 (-0.51)

Correct (-0.55)

7-13-29 X-section Alley Block 9 1/2

J.C. Bliss City Hts Annex - 20' Wide

Drebert
Rauver

Wightman

Street

37

B.M. N.W. B.P. 45th + Wightman 34737

+4.90 34737

SL. Wightman = 0100

West - Top existing return 4.74 34753

G 4.8 3475

4 5.0 3473

G 4.9 3474

E - Top existing return 4.76 34751

E 5.6 3467

4 5.3 3470

W - Base cobble wall 4.6 3471

W - Top 2.68 34959

W 4.8 3475

4 5.6 3467

4 5.6 3467

E 5.8 3465

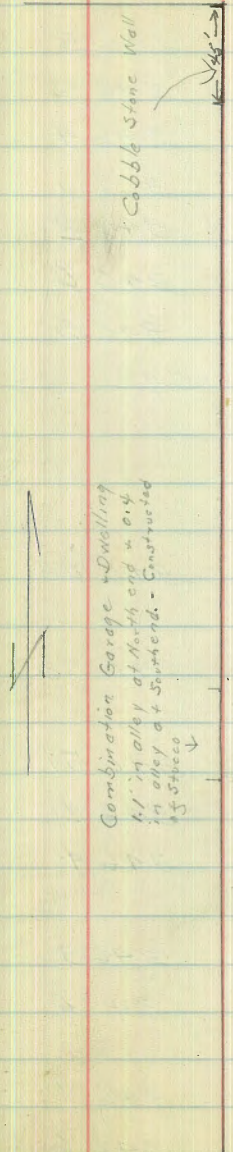
E 5.7 3466

4 5.7 3466

W 5.5 3468

4 8' Garage with concrete apron 5.36 34691

Plotted 7-19-29 G.M.J.



Landis

Street

T 352.27

1400

W	5.8	3465
E	5.8	3465
E	5.9	3464

1425

E	6.1	3462
E	5.7	3466
N	5.8	3465

T.P. -5.94 346.33

+5.38

T 351.71

1442

10' Garage 5' Back W.L. Concrete Floor 5.03 34668

1445

8' Garage 1.5' in alley from E.L. Concrete Floor 5.33 34638

1450

W 5.2 34651

E 5.5 3462

E 5.3 3464

1455

8' Garage 1.5' in alley from E.L. Dirt Floor 5.4 3463

8' Garage 5' Back W.L. Dirt Floor 4.7 3470

1475

E 5.6 3461

E 5.1 3466

W 4.8 3469

351.71

38

2400

W	4.9	3468
E	5.1	3466
E	5.2	3465

2410

8' Garage 13' Back E.L. Concrete Floor 4.80 34691

2425

E 4.9 3468

E 5.1 3466

N 5.1 3466

2439

8' Garage 13' Back E.L. Concrete Floor 4.80 34691

2450

W 5.2 3465

E 5.1 3466

E 5.2 3465

2456

8' Garage 3' Back W.L. Dirt Floor 5.2 3465

2475

E 5.3 3464

E 5.3 3464

W 4.8 3469

3400

W 5.4 3463

E 5.4 3463

E 5.3 3464

7351.71

3406

8' Garage 3' Back W.h. Dirt Floor 5.3 3464

8' Garage 7' Back E.L. Dirt Floor 5.5 3462

3425

E 5.3 3464

8 5.4 3463

W 5.3 3464

3450

W 6.0 3457

8 6.2 3455

E 6.3 3454

3454

8' Garage 0.5' Back E.L. Dirt Floor 6.3 3454

3472 = 8' 20' Double Garage in Storage Bldg see sketch 1937

North end dirt Floor 6.3 3454

South " " " 6.3 3454

3475

E 6.3 3454

8 6.6 3451

W 6.3 3454

4400

W 6.5 3452

8 6.6 3451

E 6.5 3452

T.P. 6.74 344.97

+1.83 346.80

7346.80

4425

E 1.8 3450

8 1.8 3450

W 1.8 3450

4450

W 1.8 3450

8 1.8 3450

E 2.0 3448

4468

8' Garage 4' Back W.h. Concrete Floor 2.30 34450

4475

E 2.4 3444

8 2.8 3440

W 2.1 3439

4488

15' Double Garage 1.3' Back E.L. Dirt Floor 2.7 3441

4493

8' Garage 5' Back W.h. Concrete Floor 3.50 34330

5400

W 4.0 34280

8 4.3 3425

E 3.6 3432

5425

T 346.80

40

5725

E	4.4	3424
φ	4.5	3423
W	4.5	3423

5739

φ 8' Garage 5' Back W. Dist Floor	4.4	3424
-----------------------------------	-----	------

5750

W	4.8	3420
E	4.5	3423
E	4.6	3422

5775

E	4.5	3423
φ	4.6	3422
W	4.8	3420

5796 = M.L. Landis

W - Top existing return	4.78	342 00
G	5.1	341 7
φ	4.9	341 9
G	4.9	341 9
E Top existing return	4.84	341 96

B.M. N.W. B.P. Chemoune + Landis	5.77	341.03
Correct		341.00

Ravine Storm Drains

	57.10		
25.5		11.3	39.8
	37+30		
34.5 - Bottom Gulch		21.0	30.1
24.5		-1.1	38.7
11.5		-2.6	48.5
2		+1.2	52.3
20.4		+7.6	58.7
	37+50		
25.4		-1.0	50.1
2		-5.7	45.4
22.5		10.4	40.7
45.5 - Bottom Gulch		20.6	30.5
	37+70		
43.5		19.2	31.9
2 - Bottom		21.0	30.1
20.4		17.6	33.5
30.4		10.2	40.9
	38+0 ✓		
35.4		10.1	40.0
23.4 - Bottom		23.2	27.9
18.4		19.6	31.5
2		18.4	32.7
6.5		13.8	37.3
25.5		8.2	42.9
TP	194	43.05	41.41
	38+10		

43.05

42

30.5		2.8	40.8
11.4		6.6	36.5
2		11.6	31.5
20.4 - Bottom Gulch		11.2	26.9
30.4		8.4	34.7
	38+25		
25.4		1.1	41.7
16.4		12.5	30.6
2 - Bottom		17.0	26.1
15.5		11.6	31.5
25.5		5.6	37.5
	38+65		
22.4		3.6	39.5
20.5 - Bottom		15.8	27.3
5.5 - "		15.8	27.3
2		10.1	32.7
15.4		1.2	41.9
	38+65		
15.4		2.1	41.0
8.4		6.6	36.5
2		11.5	26.6
5.5 - Bottom		17.5	25.6
13.5		17.3	25.8
23.5		11.6	31.5
30.5		4.8	36.9

Paving Stone Drains
10.25

3920

17.5	48	38.3
4.5	168	27.3
2	163	26.8
14.1 = Bottom	19.5	23.6
20.1	127	30.4
27.1	70	36.1
	39470 ✓	
37.1	120	31.1
28.1	170	26.1
21.1 = Bottom	19.8	23.3
8.1	162	26.9
2	80	35.1
5.5	5.5	37.6
20.5	21	41.0

39425 ✓

18.5	23	39.8
2	74	35.7
18.1	163	26.8
25.1	20.0	23.6
10.1	15.6	27.5
TP	10.20	10.36
	39460 ✓	12.89
10.1	127	27.7
12.1 = Bottom	17.0	23.4
15.1	163	24.1

10.36

2	9.2	31.2
20.5	10	39.4
	39475 ✓	
21.5	23	38.1
2	121	28.3
9.1	163	29.1
18.1 = Bottom	17.0	23.4
30.1	14.3	26.1
	40410 ✓	
25.1 = Base Conc. Slab	15.0	25.4
2.1 = Bottom	18.3	22.1
2	18.2	22.1
7.3	168	23.6
25.5	35	36.9
	40450 ✓	
25.5	73	33.1
12.5	135	26.9
2 = Bottom	188	21.6
11.1	166	23.8
23.1 = Base Conc. Slab	157	25.7
? Station ←		
23.1	175	22.9
2.1	180	22.4
2 = Bottom	193	21.1
20.5	113	24.1
25.5	128	27.6

Proving Storms Drains
40.36

44

TP 3.47 3717 666 33.70
1104.05 - East End Fuel 20 545 Hrs. Q/W

305 41 33.1

CS 17.3 19.9

2 - Flow Line 17.38 19.79

LD 16.2 21.0

3011 48 32.4

TP 12.74 19.07 0.84 36.33

BM 10.70 38.37

TP 1.87 54.43 1.51 17.51

BM 5.20 19.23

SEBR
Proving +
Cliveter
Car 3843
NEBR
Proving
Cliveter
1939

44+37

20 H 67

2 77

6 S 86

20 S 141

11+48

11 S = E+H Ledge House 140

2 110

15 H 139

11+55

15 H 86

2 98

10 S = N.H. House 97

11+72

5.5 S on Conc Walk 692

2 79

15 H 85

45+09 = Stucco Fence

9 H 80

2 71

15 S 18

15+10

10 S 48

2 59

9 H = Conc Walk S Edge 802

IP 316 1967 495 1121

1967

45+50

15 H 74

2 48

15 S 14

45+80

20 S 45

2 81

9 H 81

13 H 147

25 H = Bottom Gully 172

46+0

25 H 170

2 126

25 S 100

11+14 = Mean High Tide

25 S 125

2 133

26 H 164

210.61
100' N

E. emb. ch	5.40	205.21
gutter	5.9	204.7
"	5.9	204.7
♀	5.8	204.8
"	6.3	204.3
gutter	6.9	203.7
W. emb. ch	6.53	204.08

125' N

W. emb. ch	5.44	205.17
gutter	5.7	204.9
"	5.2	205.4
♀	4.8	205.8
"	5.0	205.6
gutter	5.0	205.6
E. emb. ch	4.53	206.08

150' N

E. emb. ch	3.56	207.05
gutter	4.2	206.4
"	4.2	206.9
♀	4.1	206.5
"	4.2	206.4
gutter	4.6	206.0
W. emb. ch	4.18	206.43

210.61
175' N

W. emb. ch	3.41	207.20
gutter	3.8	206.8
"	3.6	207.0
♀	3.3	207.3
"	3.4	207.2
gutter	3.5	207.1
E. emb. ch	2.91	207.70

200' N

E. emb. ch	2.16	208.45
gutter	2.8	207.8
"	2.8	207.8
♀	2.7	207.9
"	2.9	207.7
gutter	3.1	207.5
W. emb. ch	2.59	208.02

250' N

W. emb. ch	1.20	209.41
gutter	1.3	209.3
"	1.3	209.3
♀	1.2	209.4
"	1.3	209.3
gutter	1.2	209.4
E. emb. ch	0.63	209.98

T.P. 11.98 222.01 0.58 210.03

Edgement.

19

222.01

300' N. of C. St. = S. line B. St. (40' Roadway)
B. St. Pav. ed.

E. emb. ch	10.55	211.46
gutter Pavmt.	11.20	210.81
1/4 "	11.16	210.85
1/2 "	11.14	210.87
1/4 "	11.50	210.51
gutter "	12.12	209.89
W. emb. ch	11.57	210.44
00 = N. line B. St. (40' Roadway)		
W. emb. ch.	9.71	212.90
gutter pavmt	10.16	211.85
1/4 "	9.68	212.33
1/2 "	9.27	212.74
1/4 "	9.18	212.83
gutter "	9.09	212.92
E. emb. ch.	8.44	213.57
3' N.		
E. emb. ch	8.26	213.75
gutter	8.7	213.3
1/4 "	8.6	213.4
1/2 "	8.9	213.1
1/4 "	9.3	212.7
gutter	9.7	212.3
W. emb. ch.	9.47	212.54
25' N.		
W. emb. ch	7.72	214.29
gutter	8.1	213.9

222.01

Edgemont.

49

1/4 "	7.2	214.8
1/2 "	4.9	215.1
1/4 "	6.9	215.1
gutter	7.4	214.6
E. emb. ch	6.68	215.33
50' N (39' Roadway)		
E. emb. ch	4.88	217.13
gutter	5.4	216.6
1/4 "	5.4	216.6
1/2 "	5.3	216.7
1/4 "	5.5	216.5
gutter	6.1	215.9
W. emb. ch	5.67	216.34
100' N (40' Rdw.)		
W. emb. ch	2.97	219.04
gutter	3.5	218.5
1/4 "	3.3	218.7
1/2 "	2.7	219.3
1/4 "	2.8	219.2
gutter	2.7	219.3
E. emb. ch	2.26	219.75
T.P.	10.06	231.49
150' N (40' Rdw.)		
E. emb. ch	9.25	222.24
gutter	9.9	221.6
1/4 "	10.2	221.3

231.49

150' N. (con)

⊕	10.0	221.5
1/4	10.3	221.2
gutter	10.4	221.1
W. emb. cl.	9.80	221.69

190' N. (40' Rdw.)

W. emb. cl.	8.28	223.21
gutter	8.8	222.7
1/4	8.5	223.0
⊕	8.6	223.4
1/4	8.4	223.1
gutter	8.2	223.3
E. emb. cl.	7.72	223.77

W. emb. cl. 200' N. (39.80 Rdw.)

E. emb. cl.	7.29	224.20
gutter	8.0	223.5
1/4	8.0	223.5
⊕	7.7	223.8
1/4	8.1	223.4
gutter	8.4	223.1
W. emb. cl.	7.87	223.62

220' N. 40' Rdw.

W. emb. cl.	7.14	224.35
gutter	7.5	224.0
1/4	7.2	224.3
⊕	7.1	224.4
1/4	7.5	224.0

231.49

Edgemont.

50

gutter	7.3	224.2
E. emb. cl.	6.59	224.90

250' N. (39.80 Rdw.)

E. emb. cl.	5.48	226.01
gutter	6.0	225.5
1/4	6.2	225.3
⊕	6.0	225.5
1/4	6.1	225.4
gutter	6.3	225.2
W. emb. cl.	6.00	225.49

300' N. = 3. line A. St. (39.80 Rdw.)

W. emb. cl.	4.10	227.39
gutter	4.7	226.8
1/4	4.9	226.6
⊕	4.5	227.0
1/4	4.8	226.7
gutter	4.5	227.0
E. emb. cl.	3.57	227.92

chk 13 M.

4.11 227.38 = 227.39 + Edgemont

S. W. H. St

A. St 80' wide - 14' ds 13' 1/4s

5. ch. line

E. line emb. cl.	3.52	227.97
" " gutter	4.4	227.1
E. gutter line	4.4	227.1
1/4	4.4	227.1
⊕	4.6	226.9
1/4	4.7	226.8

231.49

N. 1/4 (con)

1/4		3.5	2280
E. gutter line		3.5	2280
E. line		3.4	2281
	N. E. Line H. St.		
E. Line ent. el		2.70	22879
" " gutter		3.3	2282
E. gutter line		3.3	2282
1/4		3.2	2283
⊕		3.3	2282
1/4		3.4	2281
W. gutter line		3.7	2278
W. line ent. el		3.12	22837
" " gutter		3.9	2276
	00-N. Line H. St		
W. ent. el		3.19	22830
gutter		3.7	2278
1/4		3.4	2281
⊕		3.2	2283
1/4		3.1	2284
gutter		3.2	2283
E. ent. el		2.71	22878
T.P. BM	12.23	239.62	4.10 22739
	50' N.		
E. ent. el		9.66	22996
gutter		10.6	2290
1/4		10.3	2293

239.62.

Edgemont.

⊕		10.1	2295
1/4		10.5	2291
gutter		11.0	2286
W. ent. el.		10.11	22951
	100' N.		
W. ent. el		8.92	23070
gutter		9.6	2300
1/4		9.3	2303
⊕		9.0	2306
1/4		9.1	2305
gutter		9.3	2303
E. ent. el.		8.51	23111
	150' N.		
E. ent. el		7.34	23128
gutter		8.0	2316
1/4		8.0	2316
⊕		7.9	2317
1/4		8.0	2316
gutter		8.3	2313
W. ent. el		7.70	23192
	200' N.		
W. ent. el		6.49	23213
gutter		7.4	2322
1/4		6.9	2327
⊕		6.6	2330
1/4		6.7	2329

59

Paused to Put out Fire in W.D. Starks House, 1324 Edgemont.

239.62

200' N. (con)

gutter	6.8	232 8
E. emb. cl.	6.20	233 42
250' N.		
E. emb. cl.	5.07	234 55
gutter	5.7	233 9
"	5.5	234 1
♀	5.4	234 2
"	5.7	233 9
gutter	6.1	233 5
W. emb. cl.	5.32	234.30

300' N.

W. emb. cl.	4.06	235.56
gutter	4.8	234.8
"	4.4	235 2
♀	4.1	235 5
"	4.2	235 4
gutter	4.5	235 1
E. emb. cl.	3.80	235 82

349' N = P.C. 20' Radius Return on E.

E. emb. cl.	2.64	236.98
gutter	3.3	236 3
"	3.2	236 4
♀	3.2	236 4
"	3.4	236 2
gutter	3.7	235.9
W. emb. cl.	2.96	236 66

239.62

00 = 355' N. = S. line Ash ST 80' wide

Edgement. ST.

53

W. emb. cl. P.C.	2.79	236 83
gutter	3.6	236 0
"	3.4	236 2
♀	3.1	236 5
"	3.1	236 5
gutter at E. ch. line	3.2	236 4
+ 0.9 = E. emb. cl. on Return	2.48	237.14

5' N. of old S. line Ash - P.C. 20' Radius Return on W.

3'E. of E. ch. line = emb. cl. Return	2.42	237.20
gutter	3.1	236 5
E. ch. line	3.1	236 5
"	3.1	236 5
♀	3.1	236 5
"	3.3	236 3
gutter	3.5	236 1
W. emb.	2.64	236 98

14' N. = S. ch. line on East

2' N. of W. ch. line = W. emb. cl. on Return	2.52	237 10
gutter	3.3	236 3
W. ch. line	3.1	236 5
"	3.0	236 6
♀	3.0	236 6
"	3.0	236 6
E. ch. line	3.0	236 6
+ 17.5 = E. line st	2.9	236 7
E. ch. + 20 = E. End 20' curb Return gutter	2.8	236 8
" " " " " " " " on emb. cl.	2.42	237.00

239.62

25 N. of 00 = S. ch. line Ash to West.

2.5 E. of E. line	3.0	236.6
E. line 60' st	3.0	236.6
+17.5 = E. ch. line	3.0	236.6
"	2.9	236.7
♀	3.0	236.6
"	2.9	236.7
W. ch. line	3.2	236.4

T.P. 1.37 237.87 3.12 236.50

+12.5 = W. line 60' st.	1.6	236.2
W. line +7.5 = W. End 20' Radius Return	0.87	237.00
" " " " " " " " " gutter	1.6	236.2

40' N of 00 = ♀ Ash St.

7.5 W of W. line	1.3	236.5
W line 60' st.	1.3	236.5
+12.5 = W. ch. line	1.2	236.6
"	1.2	236.6
♀	1.2	236.6
"	1.2	236.6
E. ch. line	1.3	236.5
+17.5 = E. line	1.6	236.2
E. ch. 120	1.7	236.1

55 N. of 00 = N. ch. line Ash to West.

2.5 E. of E. line	2.0	235.8
E. line 60' st.	2.0	235.8
E. ch. line	1.6	236.2
"	1.4	236.4

237.87

Edgement.

54

♀	1.3	236.5
"	1.2	236.6
W. ch. line	1.4	236.4
W. line 60' st	1.6	236.2
7.5 W. of W. line = W. End 20' Radius Return on cent. P.C.		236.95
" " " " " " " " gutter 1.8'		236.0

60' N of 00 = N. ch. line Ash St. to East.

2.1' N. of W. ch. line = cent. ch. Return 0.78 237.09

gutter	1.7	236.1
W. ch. line	1.7	236.1
"	1.4	236.4
♀	1.4	236.4

"	1.4	236.4
E. ch. line	2.2	235.6
E. line 60' st	2.5	235.3
+2.5 gutter	2.2	235.6
2.5 E. of E. line = E. End 20' Radius Cent. Return	1.92	235.95

75' N. of 00 = P.C. 20' Radius Return on W.

3.2 E. of E. ch. line = cent. ch. Return	1.88	235.99
gutter	2.5	235.3
E. ch. line	2.5	235.3
"	2.1	235.7
♀	1.7	236.1
"	1.7	236.1
gutter	1.9	235.9
W. cent. ch. at P.C.	0.95	236.92

237.87

80' N. of 00 = N. Line + Ash St. 80' wide = 00

W. emb. cl	1.19	236.68
gutter	2.1	235.7
"	2.0	235.8
⊕	1.8	236.0
"	2.1	235.7
E. cl. line	2.6	235.2
tag = gutter	2.6	235.2
tag = E. emb. cl. Return	2.00	235.87

6' N. of N. Line Ash. S.P.C. 20' Radino Return on East

E. emb. cl at P.C.	2.20	235.67
gutter	2.9	234.9
"	2.4	235.4
⊕	2.0	235.8
"	2.1	235.7
gutter	2.3	235.5
W. emb. cl	1.47	236.40

50' N. of 00

W. emb. cl	3.74	234.13
gutter	4.3	233.5
"	4.2	233.6
⊕	4.3	233.5
"	4.8	233.0
gutter	5.3	232.5
E. emb. cl	4.80	233.07

237.87

100' N.

Edgemont St

55

E. emb. cl	7.66	230.21
gutter	8.3	229.5
"	7.6	230.2
⊕	7.1	230.7
"	7.0	230.8
gutter	6.8	231.0
W. emb. cl	6.34	231.54

150' N.

W. emb. cl	8.89	228.98
gutter	9.5	228.3
"	9.8	228.0
⊕	10.1	227.7
"	10.8	227.0
gutter	11.3	226.5
E. emb. cl	10.73	227.14

170' N.

E. emb. cl	12.13	225.74
gutter	13.0	224.8
"	12.4	225.4
⊕	11.6	226.2
"	11.2	226.7
gutter	10.8	227.0
W. emb. cl	10.14	227.73

T.P. 1.51 226.89 12.49 225.38

226.89

185' W

W. emb. cl.	0.37	226.52
gutter	1.1	225.8
"	1.5	225.4
♀	1.8	225.1
"	2.7	224.2
gutter	3.6	223.3
E. emb. cl.	2.71	224.18

200' N

E. emb. cl.	4.38	222.51
gutter	5.0	221.9
"	4.3	222.6
♀	3.8	223.1
"	3.2	223.7
gutter	3.0	223.9
W. emb. cl.	1.90	224.99

230' N

W. emb. cl.	4.90	221.99
gutter	5.5	221.4
"	6.2	220.7
♀	6.5	220.4
"	7.4	219.5
gutter	7.8	219.1
E. emb. cl.	7.72	219.17

226.89

Edgemont, ST

(250' 25" N + E = N. End cmt. Walk + curb.

56

10' S. of E. cl.	9.3	217.6
E. emb. cl.	10.04	216.85
E. curb and dirt	9.1	217.8
"	9.0	217.9
♀	8.2	218.7
"	7.8	219.1
gutter	7.5	219.4
W. emb. cl.	6.79	220.10
T.P.	7.39	224.03
	8.25	218.64

255' N = P.C. 70.67 Radius curve on W. curb.

W. emb. cl.	6.56	219.47
gutter	6.9	219.1
"	7.4	218.6
♀	7.8	218.2
"	8.4	217.6
E. cl. line	8.5	217.5
10' E.	8.0	218.0

 $\Delta 12^\circ - 10^\circ - 40^\circ = S. End cl. inlet on W.$

19' E. of E. cl.	9.2	216.8
10' W. of W. cl.	8.7	217.3
E. cl. line	8.8	217.2
"	8.4	217.6
♀	8.2	217.8
"	8.0	218.0
W. gutter. Lip of cl. inlet	8.36	217.67
W. emb. cl.	7.38	218.65

RR6.03

RR6.03

$\Delta 14^{\circ}-33'$ S. End el. inlet on E. Face of
Curb on this curb inlet is 0.30 m street
Leaving R9.70 Roadway

57

			el + 48	39.6	186.4
Top emb. el. at S. End el. inlet.	7.39	218.64	el + 65	44.3	181.7
Gutter lip of " " " "	8.34	217.69	el + 90	54.6	171.4
$\Delta 21^{\circ}-03'$ N. End el. inlet on E.					
Face of curb 0.30 m street			SW. emb. el.	4.48	221.55
N. End el. inlet top curb	7.36	218.67	gutter	4.9	221.1
EN " " " gutter lip.	8.30	217.73	"4	4.7	221.3
$\Delta 21^{\circ}-54'-40''$ N. End el. inlet on W.			ϕ	4.7	221.3
E N. emb. el.	7.35	218.68	+3	4.6	221.4
Gutter lip el. inlet	8.28	217.75	"4	7.0	219.0
"4	7.8	218.2	N.E. el. line	12.8	213.2
ϕ	8.0	218.0	el + 10	20.2	205.8
"4	8.1	217.9	el + 30	32.8	193.2
S. el. line	8.5	217.5	el + 51.5	41.6	184.4
W + 7	9.6	216.4	11' N.W. of above line = E. End 10" cur. T. Culvert	41.5	184.5 Flow. line
+ 10	11.0	215.0	el + 70	44.8	181.2
W + 40	32.8	193.2			
2 d. + 6 R	41.0	185.0			
$\Delta 38^{\circ}-10'-40''$			SW. emb. el.	2.25	223.78
			gutter	2.6	223.4
W. emb. el.	6.29	219.74	"4	2.7	223.3
gutter	6.6	219.4	ϕ	2.5	223.5
"4	6.6	219.4	"4	2.4	223.6
E ϕ	6.7	219.3	N.E. el. line	8.8	217.2
"4	6.7	219.3	el + 10	15.4	210.6
S. el. line	10.1	215.9	el + 40	31.6	194.4
el + 10	16.6	209.4	el + 60	41.0	185.0

 $\Delta 70^{\circ}-42'-40''$

226.03
 $\Delta 78^{\circ} 00' - 40'' = E. \text{ End Pavmt on S.}$

*S.W. cnt. ch	1.67	224.36
gutter pavmt.	2.12	223.91
"	1.9	224.1
4	1.8	224.2
4	1.5	224.5
+3	1.6	224.4
N.E. ch. line	3.7	222.3
ch + 10.	11.0	215.0
ch + 40	27.5	198.5
ch + 56	31.5	194.5

(Not on Radial line) E. End Beech St Pavmt. (see Plat)

14.3 E. of E.C. 70.67 Radius curve on N & South

S. cnt. ch	1.67	224.36
Gutter Pavmt	2.12	223.91
+7.6' 4	1.86	224.17
+15.2' 4	1.64	224.35
+22.8' 4	1.82	224.21
+28.8' S.E. cor. catch Basin on pavmt	2.31	223.72
" " " " " on grating	1.85	224.18
31.8' N. of S. ch. = N. ch to W. = Catch Basin N.E. cor.	1.85	224.18 on grating
10' N. of N. ch. line to West.	8.6	217.4
35' " " " " " " "	21.9	204.1
44' " " " " " " "	22.1	203.9

226.03

Edgemont St.

E.C. 70.67 Radius curb on S

58

N. gutter	1.30	224.73
N. cnt. ch.	0.82	225.21
5' N. of N. ch. line	1.1	224.9
10' " " " " "	3.0	223.0
25' " " " " "	12.3	213.7
35' " " " " "	16.0	210.0
10' W. of E.C.		
N. cnt. ch.	0.10	225.93
10' N. of N. ch.	0.0	226.0
T.P.	9.42	237.78
chk on B.M.	4.23	225.36
		230.55 = 230.57 + Beech St.

Same Point

12-13-29
 J.C. Bliss
 Diebert to Louisiana - 52' Roadway
 13' 1/45
 Runner

B.M. N.W. B.P. Park Blvd & Meade 342.01
 + 6.23

Σ 348.24

Gutter South end of S.E. Return 8.97

Having flush with top curb
 around S.E. Return

E.L. Pk. Blvd = +100 - Park Blvd Paving

5 Tr pb	7.72	340.52
G	8.70	339.54
1/4	7.37	340.87
1/4	7.00	341.24
1/4	6.62	341.62
cb	6.32	341.92
N = Intersection with South paving	6.06	342.18

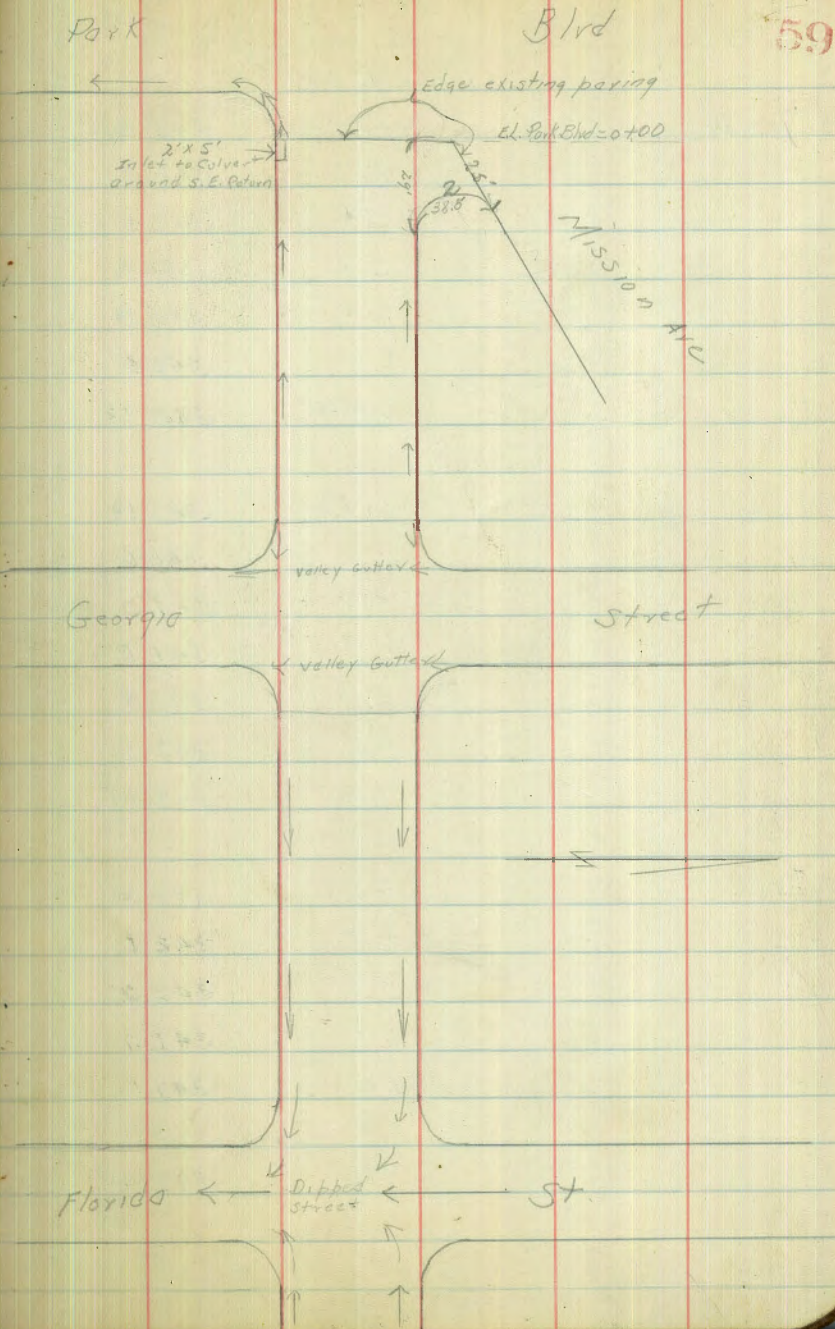
Line of Mission Ave

N.W. B.P. Park Blvd & Meade = 342.01
 5.24

Σ 347.25

Shots on N.E. Return - See sketch

1 - Top cb	4.57	342.68
Gutter - Mission Ave Paving	5.02	342.23
2 - Top cb & Return	4.47	342.78
G	5.1	342.1



347.25

0+29 = E.G. N.E. Return

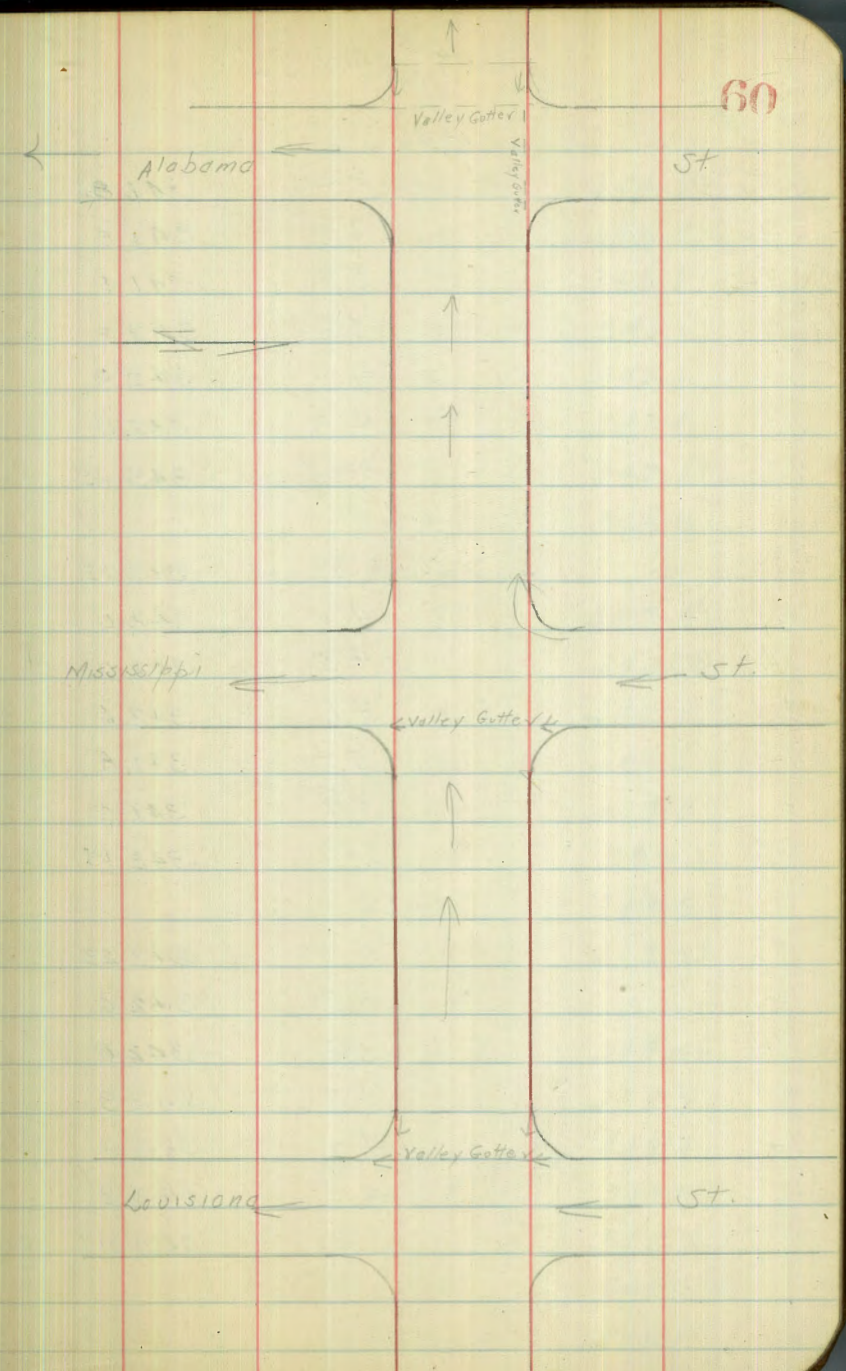
N Tpcb	4.40	342.85
G	5.2	342.0
1/4	5.7	341.5
¢	5.8	341.4
1/4	6.4	340.8
G	6.8	340.4
S Tpcb	6.42	340.83

0+50

S Tpcb	6.12	341.13
G	6.6	340.6
1/4	6.2	341.0
¢	5.7	341.5
1/4	5.4	341.8
G	4.9	342.3
N Tpcb	4.20	343.05

0+75

N Tpcb	4.02	342.23
G	4.7	342.5
1/4	5.2	342.0
¢	5.3	341.9
1/4	6.0	341.2
G	6.3	340.9
S Tpcb	5.80	341.45



π 347.25

1400

S Tr cb	5.44	341.81
G	6.0	341.2
1/4	5.8	341.4
¢	5.0	342.2
1/4	4.9	342.3
G	4.3	342.9
N Tr cb	3.76	343.49

1425

N Tr cb	3.53	343.72
G	4.2	343.0
1/4	4.5	342.7
¢	4.6	342.6
1/4	5.4	341.8
G	5.7	341.5
S Tr cb	5.10	342.15

1450

S Tr cb	4.72	342.53
G	5.2	342.0
1/4	5.2	342.0
¢	4.3	342.9
1/4	4.7	343.0
G	3.9	343.3
N Tr cb	3.28	343.97

π 347.25

61

1470 = W.L. Alley

N Tr cb	3.03	344.22
G	3.7	343.5
1/4	4.1	343.1
¢	4.1	343.1
1/4	4.8	342.4
G	4.8	342.4
Tr cb - No return at alley	4.45	342.80
S	4.0	343.2

1480 = E.L. Alley

S	3.7	343.5
Tr cb - No return at alley	4.35	342.90
G	4.5	342.7
1/4	4.6	342.6
¢	4.0	343.2
1/4	4.0	343.2
G	3.6	343.6
Tr cb - in driveway	3.42	343.83

2400

N Tr cb	2.79	344.46
G	3.5	343.7
1/4	3.8	343.4
¢	3.8	343.4
1/4	4.5	342.7
G	4.6	342.6
S Tr cb	4.14	343.11

T 347.25

2+25

STpcb	3.83	343.42
G	4.4	342.8
1/4	4.3	342.9
¢	3.6	343.6
1/4	3.5	343.7
G	3.0	344.2
N Tpcb	2.55	344.70

2+50

N Tpcb	2.26	344.99
G	3.1	344.1
1/4	3.2	344.0
¢	3.3	343.9
1/4	4.0	343.2
G	4.0	343.2
STpcb	3.43	343.82

2+75

STpcb	3.15	344.10
G	3.7	343.5
1/4	3.6	343.6
¢	2.9	344.3
1/4	2.8	344.4
G	2.7	344.5
N Tpcb	2.18	345.07

2.29 344.96

0.71 345.67

T 345.67

3400=W.L. Georgia - Intersection Paved

 80' wide
 20' - 65'
 10' roadway

62

N Tpcb	0.17	345.50
G	0.74	344.83
1/4	0.53	345.14
¢	0.55	345.12
1/4	0.92	344.75
G	1.73	343.94
STpcb	1.17	344.50

W cb Georgia

SL Tpcb	1.19	344.48
G	1.87	343.80
cb	1.76	343.91
1/4	1.40	344.27
¢	1.25	344.42
1/4	1.05	344.62
cb	0.87	344.80
G	0.87	344.80
N Tpcb	0.17	345.50

¢ Georgia

N	0.68	344.99
cb	0.84	344.83
1/4	0.98	344.69
¢	1.17	344.50
1/4	1.30	344.37
cb	1.50	344.17

T 345.67

5		1.68	343.99
	F cb	Georgia	
S.L. Tp cb		2.17	343.50
G		2.66	343.01
cb		2.49	342.18
1/4		2.22	343.45
¢		2.07	343.60
1/4		1.96	343.71
cb		1.82	343.85
N.L. Gutter		1.70	343.97
N.L. Tp cb		1.06	344.61
	E.L. Georgia	20+00	
N Tp cb		1.15	344.52
G		1.66	344.01
1/4		1.59	344.08
¢		1.70	343.97
1/4		2.05	343.62
G.		2.81	342.86
STp cb		2.16	343.51
	0440 = P.V.O.		
STp cb		4.21	341.46
G		4.7	341.0
1/4		4.3	341.3
¢		3.8	341.8
1/4		3.9	341.7

T 345.67

63

G		4.0	341.6
N Tp cb		3.17	342.50
	0460		
N Tp cb		4.37	341.30
G		5.3	340.3
1/4		5.1	340.5
¢		5.0	340.6
1/4		5.4	340.2
G		6.0	339.6
STp cb		5.36	340.31
	0480		
STp cb		6.81	338.86
G		7.5	338.1
1/4		7.1	338.5
¢		6.6	339.0
1/4		6.4	339.2
G		6.5	339.1
N Tp cb		5.75	339.92
	1400		
N Tp cb		7.49	338.18
G		8.2	337.4
1/4		8.2	337.4
¢		8.2	337.4
1/4		8.8	336.8
G		9.1	336.5

T 34567

S Tp cb	8.57	337.10
	1+20	
S Tp cb - Drive way	11.02	334.65
G	11.3	334.3
1/4	10.8	334.8
¢	10.2	335.4
1/4	10.4	335.2
G	10.4	335.2
N Tp cb	9.46	336.21
	1+39.20 = N.L. Alley-	
N.L. Tp cb	11.02	334.65
G - existing alley paving	11.65	334.02
Cb - Tp cb	11.50	334.17
G	12.4	333.2
1/4	12.6	333.0
¢	12.3	333.3
1/4	13.1	332.5
G	13.7	332.0
Cb - Tp cb	12.67	333.00
S.L. Tp cb	12.62	333.05
G - Existing alley paving	13.27	332.40
T.B.		12.72 332.95

0.26

T 333.21

T 333.21

64

	1+49.20 = ¢ Alley	
S - Existing alley paving	2.16	331.05
cb	2.0	331.2
1/4	1.8	331.4
¢	1.0	332.2
1/4	1.4	331.8
cb	1.1	332.1
N - Existing alley paving	0.45	332.76
	1+59.20 = Fl Alley - E.V.C	
N - On existing alley paving	1.07	332.14
Tp alley return - N.L.	17.0	331.51
G - N.L.	1.1	332.1
cb - Tp cb	2.00	331.21
G	2.0	331.2
1/4	2.7	330.5
¢	2.5	330.7
1/4	2.9	330.3
G	3.3	329.9
Cb - Tp cb	2.99	330.22
S.L. Tp cb - Alley paving Flush	2.65	330.56
	1+75	
S Tp cb	5.03	328.18
G	5.5	327.7
1/4	4.5	328.7
¢	4.6	328.6
1/4	4.4	328.8

T 333.21

G	44	328.8	
N T p c b	4.00	329.21	
	2400		
N T p c b	7.38	325.83	
G	7.8	325.4	
1/4	8.0	325.2	
Q	7.9	325.3	
1/4	8.5	324.71	
G	9.0	324.2	
S T p c b	8.37	324.84	
	2425		
S T p c b	11.75	321.46	
G	12.3	320.9	
1/4	12.1	321.1	
Q	11.4	321.8	
1/4	11.4	321.8	
G	11.3	321.9	
N T p c b	10.80	322.41	
T. P.		1524	319.97

020

T 320.17

T 320.17

2450

65

N T p c b	120	318.97
Q	16	318.5
1/4	18	318.3
Q	18	318.3
1/4	2.4	317.7
G	2.9	317.2
S T p c b	2.14	318.03
	2475	
S T p c b	5.59	314.58
G	6.2	314.0
1/4	5.8	314.4
Q	5.2	315.0
1/4	5.4	314.7
G	5.1	315.0
N T p c b	4.65	315.52
	3409 = W. h. Florida = Intersection Payed	
N T p c b	9.17	311.00
G	9.7.7	310.40
1/4	9.75	310.42
Q	9.90	310.27
1/4	10.25	309.92
G	10.73	309.44
S T p c b	10.19	309.98

π 320.17

W cb Florida

S.L. Top cb	10.17	310.00
SL Gutter	11.08	309.09
cb	11.03	309.14
1/4	10.79	309.38
¢	10.57	309.60
1/4	10.43	309.74
cb	10.34	309.83
NL Gutter	10.09	310.08
N.L. Top cb.	9.18	310.99

¢ Florida

N	11.00	309.17
cb	11.18	308.99
1/4	11.31	308.86
¢	11.49	308.68
1/4	11.63	308.54
cb	11.80	308.37
S	11.98	308.19

E cb Florida

S.L. Top cb	11.06	309.11
SL Gutter	11.67	308.50
cb	11.60	308.57
1/4	11.40	308.77
¢	11.23	308.94
1/4	11.10	309.07
cb	10.90	309.27

π 320.17

66

N.L. Gutter	10.65	309.52
N.L. Top cb	10.18	309.99
-E.L. Florida = 0.20		
N Top cb	10.23	309.94
¢	10.66	309.51
1/4	10.75	309.42
¢	10.89	309.28
1/4	11.11	309.06
¢	11.60	308.57
S Top cb	11.19	308.98
0.25		
S Top cb	11.04	309.13
¢	11.6	308.5
1/4	10.9	309.2
¢	10.5	309.6
1/4	10.6	309.5
¢	10.6	309.5
N Top cb	10.08	310.09

0.50

N - Driveway + Gutter	10.43	309.74
1/4	10.4	309.7
¢	10.3	309.8
1/4	10.7	309.4
S - Driveway + Gutter	11.27	308.90

π 320.17

0+75

S Tr cb	10.62	309 55
G	11.1	309 0
1/4	10.7	309 4
ϕ	10.2	310 0
1/4	10.2	310 0
G	10.3	309 8
N Tr cb	9.66	310 51
T.P.		10.00 310.17

9.76

π 319.93

1+00

N Tr cb	9.09	310 84
G	9.6	310 3
1/4	9.7	310 2
ϕ	9.7	310 2
1/4	10.2	309.7
G	10.8	309.1
S Tr cb	10.14	309 79

1+25

S Tr cb	9.86	310 07
G	10.4	309 5
1/4	9.9	310 0
ϕ	9.5	310 4
1/4	9.3	310 6
G	9.3	310 6

π 319.93

67

N Tr cb	8.78	311 15
	1+50 = W.L. Alley	
N-L Top alley return	8.20	311 73
G = existing alley paving	8.50	311 43
cb - gutter	9.0	310 9
" = Tr cb	8.58	311 34
1/4	8.9	311 0
ϕ	9.0	310 9
1/4	9.5	310 4
G	10.3	309 6
cb Tr cb	9.65	310 28 -
S-L Tr cb - alley return	9.24	310 69
G	9.7	310 2
	1+59.9 = G Alley	
S	9.4	310 5
cb	9.8	310 1
1/4	9.2	310 7
ϕ	8.7	311 2
1/4	8.7	311 2
cb	8.5	311 4
N = Existing alley paving	8.70	311 23

31993

14698 = E.L. Alley

N.L. Tp alley return	7.46	312.47
Gutter - existing alley paving	8.24	311.69
cb. Tp cb	7.60	312.33
Gutter	8.2	311.7
1/4	8.3	311.6
£	8.4	311.5
1/4	8.9	311.0
cb. Tp cb	8.67	311.26
G	9.5	310.4
S.L. Tp alley return	8.58	311.35
G	9.1	310.8
	2+00	
S Tp cb	7.33	312.60
G	7.9	312.0
1/4	7.4	312.5
£	6.9	313.0
1/4	7.0	312.9
G	7.2	312.7
N Tp cb	6.38	313.55
	2+25	
N Tp cb	5.19	314.74
G	5.9	314.0
1/4	5.7	314.2
£	5.6	314.3
1/4	6.1	313.8

31993

68

G	6.9	313.0
S Tp cb	6.13	313.80
	2+50	
S-Drive way + gutter	5.40	314.53
1/4	4.9	315.0
£	4.5	315.1
1/4	4.4	315.5
G	4.7	315.2
N Tp cb	3.95	315.98
	2+75	
N Tp cb	2.80	317.13
G	3.4	316.5
1/4	3.2	316.7
£	3.2	316.7
1/4	3.6	316.3
G	4.4	315.5
S Tp cb	3.73	316.20
	3+10 =	
	W.L. Alabama-Intersection paved	
	2.00	317.84.93
G	2.48	317.45
1/4	1.98	317.95
£	1.70	318.23
1/4	1.62	318.31
G	1.63	318.30
N Tp cb	1.12	318.81

T 319.93

B.M. SE. S.P. Alabama R. West -113 318.80

Correct 318.87

11.25

T 330.12

W cb Alabama

N.L. Top curb 11.23 318.89

G 11.85 318.27

cb 11.90 318.22

1/4 12.00 318.12

f 12.18 317.94

1/4 12.38 317.74

cb 12.67 317.45

S.L. Gutter 12.85 317.27

S.L. Top curb 12.17 317.95

f Alabama

S 11.97 318.15

cb 11.75 318.37

1/4 11.54 318.58

f 11.37 318.75

1/4 11.33 318.79

cb 11.41 318.71

N 11.04 319.08

T 330.12

69

N.L. Top curb 10.13 319.99

G 10.79 319.33

cb 11.02 319.10

1/4 10.91 319.21

f 10.92 319.20

1/4 11.17 318.95

cb 11.63 318.49

S.L. Gutter 11.95 318.17

S.L. Top curb 11.24 318.88

El. Alabama = 2000

S Top curb 11.05 319.07

G 11.63 318.59

1/4 10.94 319.18

f 10.62 319.50

1/4 10.51 319.61

G 10.67 319.45

N Top curb 10.09 320.03

0+25

N Top curb 8.70 321.42

G 9.2 320.9

1/4 9.1 321.0

f 9.2 320.9

1/4 9.7 320.4

G 10.2 319.9

S Top curb 9.60 320.52

T 330.12

0+50

S Tpcb	8.12	322 00
G	8.8	321 3
1/4	8.2	321 9
♀	7.7	322 4
1/4	7.6	322 5
G		
N-Driveway	7.68	322.44

0+75

N Tpcb	5.80	324 32
e	6.4	323 7
1/4	6.0	324 1
♀	6.1	324 0
1/4	6.7	323 4
G	7.6	322 5
S Tpcb	6.70	323.42

1+00

S-Driveway & Gutter	5.78	324 34
1/4	5.2	324 9
♀	4.8	325 3
1/4	4.8	325 3
G	5.1	325 0
N Tpcb	4.39	325 73

T 330.12

1+25

N Tpcb	2.91	327 21
G	3.7	326 4
1/4	3.6	326 5
♀	3.3	326 8
1/4	3.8	326 3
G	4.6	325 5
S Tpcb	4.06	326 06

1+40.50 = W.L. Alley

Sh Top alley return	26.7	327 45
G	2.9	327 2
Ob line Tpcb	2.96	327 16
G	3.5	326 6
1/4	3.1	327 0
♀	3.5	326 6
1/4	2.8	327 3
Ob line Tpcb	1.98	328.14
G	2.9	327 2
N.L. Top alley return	1.66	328.46
G-Existing alley paving	1.73	328.39

1+50.35 = ♀ Alley

N-existing alley paving	1.82	328 30
cb	2.5	327 6
1/4	2.3	327 8
♀	2.1	328 0
1/4	2.6	327.5

70

π 330.12

cb	33	326 8
S	2.3	327 6
1460.20 = F.L. Alley		
S.L. Tpcb-Alley return	19.2	328 20
G	2.2	327 9
cb line Tpcb	2.02	328 10
G	3.0	327 1
1/4	2.4	327.7
¢	1.8	328 3
1/4	1.9	328 2
cb line Tpcb.	1.15	328 97
G	2.2	327 9
N.L. Top alley return	0.95	329 17
G- Existing alley paving	1.26	328 85
1475		
N Tpcb	0.68	329 44
G	1.6	328 5
1/4	1.3	328 8
¢	1.2	328 9
1/4	1.8	328 3
G	2.5	327 6
S Tpcb	1.50	328.62

π 330.12

21

2400

S Tpcb	0.22	329 40
G	1.6	328 5
1/4	1.0	329.1
¢	0.4	329 7
1/4	0.4	329 7
G	0.8	329 3
Ncb-Driveway	0.40	329 72
T.P.		008 330.04

+2.88

π 337.92

2425

N Tpcb	7.13	330 79
G	7.9	330.0
1/4	7.6	330.3
¢	7.6	330.3
1/4	8.0	329 9
G	8.6	329.3
S Tpcb	7.78	330 14
2450		
S Tpcb	7.15	330.77
G	8.0	329 9
1/4	7.3	330.6
¢	6.8	331.1
1/4	6.9	331.0
G	7.3	330.6
N Tpcb	6.54	331.38 ✓

T 337.92

2475

N Top cb	5.97	331.95
G	6.8	331.1
1/4	6.3	331.6
¢	6.2	331.7
1/4	6.6	331.3
G	7.3	330.6
S Top cb	6.50	331.42

3400 = W.L. Mississippi-Intersection Paved

S Top cb	5.83	332.09
G	6.56	331.36
1/4	6.22	331.70
¢	6.06	331.86
1/4	6.02	331.90
G	6.17	331.75
N Top cb	5.38	332.54

W cb Mississippi

N.L. Top cb	5.35	332.57
G	5.99	331.93
cb	5.93	331.99
1/4	5.81	332.11
¢	5.88	332.04
1/4	5.98	331.94
cb	6.23	330.69
S.L. Top cb	5.83	332.09
G	6.44	331.48

T 337.92

72

¢ Mississippi

S	5.81	332.11
cb	5.73	332.19
1/4	5.63	332.29
¢	5.56	332.36
1/4	5.46	332.46
cb	5.38	332.54
N	5.28	332.64

E cb Mississippi

N.L. Top cb	4.83	333.09
G	5.46	332.46
cb	5.62	332.30
1/4	5.73	332.19
¢	5.79	332.13
1/4	5.87	332.05
cb	5.96	331.96
S.L. Top cb	5.35	332.57
G	6.10	331.82

E.L. Mississippi = 20400

S Top cb	5.32	332.60
G	5.90	332.02
1/4	5.66	332.26
¢	5.50	332.42
1/4	5.49	332.43
G	5.55	332.37
N Top cb	4.90	333.02

π 337.92

0+25

N Tpcb	4.83	333.09
G	5.2	332.7
1/4	5.2	332.7
¢	5.0	332.9
1/4	5.4	332.5
G	5.7	332.2
STpcb	5.24	332.68

0+50

S Tpcb	5.18	332.74
G	5.6	332.3
1/4	5.3	332.6
¢	5.0	332.9
1/4	5.1	332.8
G	5.2	332.7
N Tpcb	4.71	333.21

0+75

N Tpcb	4.63	333.29
G	5.0	332.9
1/4	5.0	332.9
¢	4.9	333.0
1/4	5.3	332.6
G	5.5	332.4
STpcb	5.14	332.78

π 337.92

1+00

STpcb	5.08	332.84
G	5.4	332.5
1/4	5.3	332.6
¢	4.9	333.0
1/4	5.1	332.8
G	5.1	332.8
N. Tpcb	4.58	333.34

1+25

N Tpcb	4.52	333.40
G	5.0	332.9
1/4	4.9	333.0
¢	4.8	333.1
1/4	5.1	332.8
G	5.2	332.7
STpcb	4.95	332.97

T.R.

4.77 333.15

+5.52

π 338.67

1439²⁸ = W.L. Alley

S. Top alley return	5.43	333.24
Gutter	5.4	333.2
cb line Top curb	5.54	333.13
G	6.1	332.5
1/4	5.8	332.8
¢	5.5	333.1

73

T 338.67

1/4	56	333 0
cb line Top curb	517	333 50
G	56	333 0
N.L. Top alley returns	492	333 75
G	51	333 5
1+496 = 6 Alley		
N	51	333 5
cb	56	333 0
1/4	56	333 0
¢	54	333 2
1/4	58	332 8
cb	59	332 7
S	54	333 2
1+59.5 = P.L. Alley		
S.L. Top alley returns	539	333 28
G	54	333 2
cb line Top cb	557	333 10
G	60	332 6
1/4	58	332 8
¢	55	333 1
1/4	57	332 9
G	57	332 9
cb line Top cb	517	333 50
N.L. Top alley returns	502	333 65
G	53	333 3

T 33867

74

2+00

N Top cb	505	333 62
G	58	332 8
1/4	56	333 0
¢	54	333 2
1/4	57	332 9
G	59	332 7
S Top cb	552	333 15
2+25		
S Top cb	548	333 19
G	60	332 6
1/4	56	333 0
¢	53	333 3
1/4	54	333 2
G	57	332 9
N Top cb	495	333 72
2+50		
N Top cb	490	333 77
G	56	333 0
1/4	54	333 2
¢	52	333 4
1/4	57	332 9
G	58	332 8
S Top cb	539	333 28

π 33867

2475

S Tpcb	536	333.31
G	58	332.8
1/4	56	333.0
♀	52	333.4
1/4	53	333.3
G	55	333.1
N Tpcb	486	333.81

24993 = W.L. Louisiana - Paved 1

N Tpcb	470	333.97
G	534	333.33
1/4	514	333.53
♀	515	333.52
1/4	543	333.24
G	576	332.91
S Tpcb	520	333.47

W cb Louisiana

S.L. Tpcb	533	333.34
G	600	332.67
cb	602	332.65
1/4	587	332.80
♀	572	332.95
1/4	560	333.07
cb	550	333.17
N.L. Top cb.	470	333.97
G	537	333.30

π 33867

75

B.M. S.E. Meade + Louisiana	-594	332.73
Correct		332.70

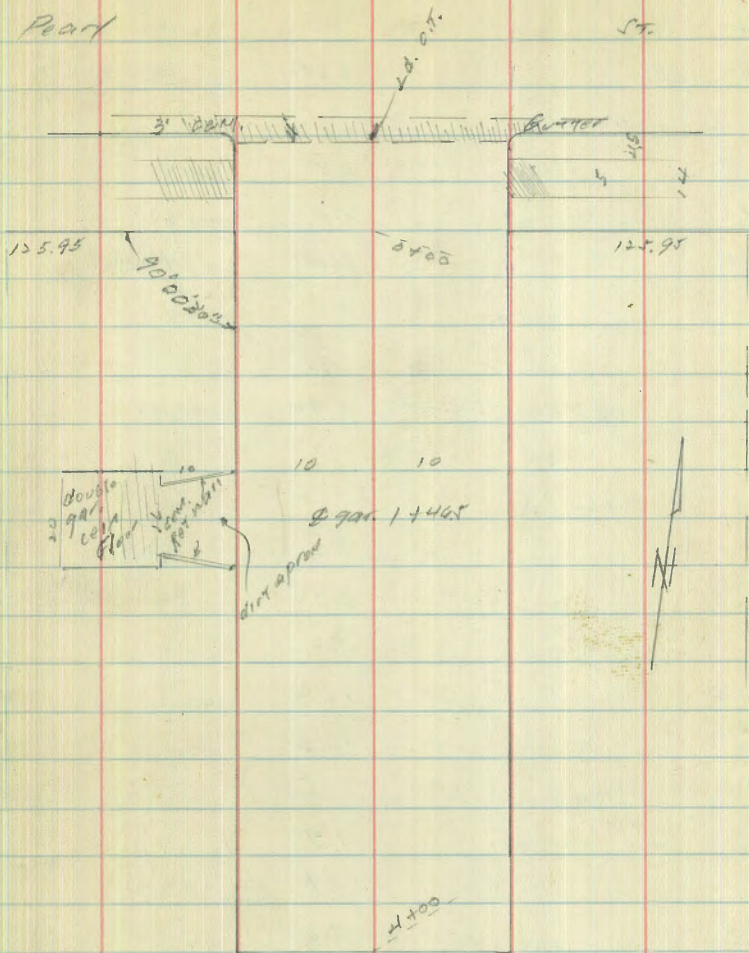
X 200 alley 20' wide
 Bk 14 Center add.
 to La Jolla Park.

Moore
 4-1-28.

Indexed
 C.S.K.

Pearl

S.E.B.P.	4.21	119.38		115.17	Pearl Girard
T.P.	12.86	131.54	0.70	118.68	
S.W.B.P. Pearl & High			4.43	127.11	
T.P.	12.75	143.86	0.43	131.11	



0-17 ^H edge qvt.

W	cem	3.60	140.26
C		2.51	141.38
E		1.54	142.32

0-14 S cb Pearl

E	cb	0.72	142.13	
E	cert. qvt.	1.73	142.13	
C	" " on C.T.	2.75	141.11	B.M.
W	" "	2.83	140.03	
W	cb	2.93	140.93	

0-13 S edge qvt.

W	cem.	3.74	140.12
C	"	2.66	141.20
E	"	1.65	142.21

0-100 S Pearl

E	cb and ground	0.66	143.20
E+7		1.4	142.7
C		2.3	141.6

Overlook Drive

Garage

143.86

W		3.0	140.9
W CB		2.9	141.7
	0+05		
W		2.5	141.4
C		2.0	141.9
W		0.0	142.9
E		0.0	143.9
T.P.	10.72	152.64	1.94
	0+25		141.92
E		8.5	144.1
+8		8.7	143.9
C		9.2	143.2
+2		10.4	142.2
W		10.6	142.0
	0+50		
W		9.9	142.7
C		9.9	142.7
+9		9.6	143.0
+6		8.1	144.5
E		8.1	144.5
	0+60		
E		8.6	144.0
C		9.8	142.8
W		10.5	142.1

152.64

77

W +6	Sim. 99r 10 wide	10.92	141.72	Alt. 41.
	0+80			
W		9.7	142.9	
C		8.4	144.2	
E		7.8	144.8	
	1+00			
E		7.0	145.6	
+7		7.9	144.7	
C		9.0	143.6	
W		9.7	142.9	
+10		10.3	142.3	
	1+15 = Flood condition			
-15		10.4	142.2	
W		10.1	142.5	
+4		9.2	143.4	
C		9.2	143.4	
+5		7.8	144.8	
E		7.0	145.6	
	1+30			
E		8.2	144.4	
C		8.6	144.0	
+5		8.8	143.8	
W		9.8	142.8	
+10		10.4	142.2	
	1+36.5			
W - 5		10.0	142.6	
W		10.0	142.6	

152.64

cent.

W Top 6" Ret wall	8.01	144.63
+1	8.86	143.78
C	8.6	144.0
E	8.1	144.5

1446.5

W - 10. E 16' Gar fl. el.	8.01	144.43
---------------------------	------	--------

1455.5

-5	9.0	143.6
----	-----	-------

W Top 6" wall	8.11	144.53
---------------	------	--------

+1	8.6	144.0
----	-----	-------

C	8.6	144.0
---	-----	-------

+7	8.4	144.4
----	-----	-------

E	7.4	145.2
---	-----	-------

1470.5

E	6.3	146.3
---	-----	-------

+5	7.1	145.3
----	-----	-------

C S.M.H. P.M	7.64	145.0
--------------	------	-------

+5	7.8	144.8
----	-----	-------

W	8.8	143.8
---	-----	-------

+5	9.4	143.2
----	-----	-------

1485

-5	7.0	145.6
----	-----	-------

W	6.7	145.9
---	-----	-------

C	6.7	145.9
---	-----	-------

E	6.3	146.3
---	-----	-------

152.64

78

2400

E	5.4	147.2
---	-----	-------

C	6.5	146.1
---	-----	-------

W	6.2	146.4
---	-----	-------

+5	6.4	146.2
----	-----	-------

2430

-5	4.3	148.3
----	-----	-------

W	4.0	148.6
---	-----	-------

C	5.6	149.0
---	-----	-------

E	4.0	148.6
---	-----	-------

+10	3.8	148.8
-----	-----	-------

2460

E	1.6	151.0
---	-----	-------

C	1.2	151.4
---	-----	-------

+8	1.2	151.3
----	-----	-------

W	2.3	150.3
---	-----	-------

+5	2.7	149.9
----	-----	-------

T.P	11.03	162.81	0.86	151.78
-----	-------	--------	------	--------

3405

-5	9.9	152.9
----	-----	-------

W	9.4	153.4
---	-----	-------

C	9.3	153.5
---	-----	-------

E	8.4	154.6
---	-----	-------

162.81

3 + 05

E	6.5	156.3
c	6.7	156.1
W	7.3	155.5
+5	7.5	155.3

3 + 65

-5	6.3	157.5
W	6.0	156.8
c	4.9	157.9
E	4.3	158.5

4 + 00 = P.L. = H.L. overlook Dr.

E	3.5	159.3
c	4.1	158.7
W	5.1	157.7
+5	5.5	157.3

T.P.	1.87	152.73	11.95	150.84
------	------	--------	-------	--------

NE. top cb	High ave Overlook Dr	8.25	144.48	144.50
------------	-------------------------	------	--------	--------

Please check
to High ave profile

79

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 1/2 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body

from side stake to slope stake. If ground is not amount if cut, elevate it. Add this amount to cut or fill and distance in table. Set up rod at this point and line of sight should cut target.

IMPROVED TABLES AND INFORMATION

TABLE No. 2.

To find tangent and external for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given L may be found by dividing tangent (or external), opposite L by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

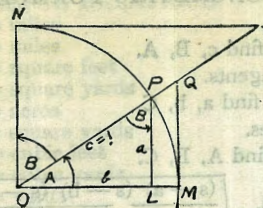


TABLE II
TRIGONOMETRIC FORMULÆ.

$$\angle A = \angle MOP \quad \angle B = \angle PON = \angle OPL$$

$$R = OB = c = 1$$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

$$\sin \frac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \quad \cos \frac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \quad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Sines} \quad \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{c}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$$

477.07 5767.30
 40.20 25
 5727.30
 7.80
 610.00

472.97
 376
 469.21

34
 17
 51

331.49
 4.13
 227.37

17.5
 30.
 12.5
 60.0

92
 72

N 12° 04' 00" W
 N 88° 59' 30" E
 90° 08' 30"

44
 18
 30
 92

31.5
 1.5
 30.48

44
 38
 19
 57

46
 23
 69

46
 24
 72

31.6
 26
 29.0
 14.8
 43.3

44.8
 4.5
 40.0
 20
 60.

39.0
 19.5
 58.5

045
 0414
 11
 0225
 15
 0440
 15
 0455

0486
 0475
 0481

NT,

ENGI. CITY OF SAN DIEGO,
 CALIFORNIA.