

1361

PLANTS

LEVEL BOOK

No. 539 F

X. Sec	Columbia St.	Chalmers to Walnut	1
" "	Chalmers	India to Linwood	5
" "	State	Walnut to Middleborn	12
" "	Guy	160' W of Benson "	16
" "	Eleanor Dr. Exempt		19
" "	"B" St.	43 rd Lemon Grove Blvd.	25
" "	Benson.	Guy to Linwood	38
" "	Chalmers	State. to "	45
" "	10 th	cb's N.L. University Ave.	50
" "	Beryl.	Cass to Dawes New Nater	51
" "	Alley bet. Delaware & Maryland	S. of Madison	57
" "	Sigsbee	Logan to National	61
" "	Alley bet. 23 Teratta	Re sub. 05 L. 11	64
" "	31.	Normal Heights	67
" "	44	Park Villas	71

D. N. 1 Dec 60 Chalmers 114

9-27-29
 J.C. Blais
 Lynn Drebert
 Chuck Turner

X-section Columbia Street - Chalmers
 to Walnut - 75' Wide - 12' cbs - 12.75' / 45'

0 1

B.M. SW B.P. - Chalmers + India

66.07

13.03 79.10

T.P.

1.16 77.94

12.86 90.80

0.00 90.80

+13.03 H.I.
 103.83

B.M. SE B.P. Chalmers + Columbia

6.77 97.06

S.L. Chalmers = 0700

W-edge walk

9.96

cb-existing end return

10.04

93.79

G

10.0

1/4

8.6

1/4

8.4

95.4

1/4

8.0

G

7.5

cb-existing end return

6.92

96.91

E-edge walk

6.59

0.145

F

3.2

100.6

cb

6.1

1/4

6.5

1/4

7.5

96.3

1/4

7.9

cb

9.0

W

9.6

99.2

Plotted 11/23-29
 CBH

π 103.83

0+50

W	6.0	97.8
cb	5.9	
1/4	5.0	
♀	4.0	99.8
1/4	2.7	
cb	2.1	
T.P.		0.20

103.63

+1224

π 115.87

+10	7.3	
E	6.9	109.0
	0+75	
E	1.8	114.0
+3	2.3	
cb	9.5	
1/4	11.4	
♀	13.0	102.5
1/4	13.7	
cb	13.6	
W	11.7	104.1

1+00

W	9.1	106.7
cb	10.8	
1/4	9.3	
♀	8.6	102.8

π 115.87

2

1/4	6.9	
cb	4.5	
+10	+5.6	
E	+5.6	121.4
	1+25	
E	+8.2	124.0
+2	+8.2	
cb	0.1	
1/4	2.2	
♀	4.6	111.2
1/4	5.5	
cb	6.8	
W	5.4	110.4
	1+50	
W	0.3	115.5
cb	1.4	
1/4	2.1	
♀	1.3	114.5
T.P.		0.29

+1316 128.74

1/4	11.7	
cb	9.6	
♀	0.4	128.3

π 128.74

1+75

E +2.2 130.9

cb 5.1

1/4 7.4

φ 9.1 119.6

1/4 9.8

cb 9.2

W 9.2 119.5

2+100

W 5.9 122.8

1/4 7.6

cb 7.0

1/4 7.0

φ 6.4 122.3

1/4 4.4

cb 1.1

E +6.4 135.1

2+25

E +9.0 137.7

cb +3.5

1/4 +1.0

φ 1.7 127.0

1/4 2.3

cb 3.2

W 3.7 125.0

π 128.74

2+50

W 1.0 128.7

cb 1.0

T.P. 0.19 128.55

+13.04 141.59

1/4 12.7

φ 11.2 130.4

1/4 8.3

cb 5.5

E 1.4 140.2

2+75

E 0.3 141.3

cb 2.6

1/4 5.8

φ 7.6 134.0

1/4 9.5

cb 11.4

W 11.7 129.9

3+00 = H.L. Walnut - 80' wide 14' deep 15' high

W 11.9 129.8

cb 9.7

1/4 7.7

φ 5.6 136.0

1/4 3.6

cb 1.2

E +0.5 142.1

3

T 141.59

N e b Walnut

E	+1.0	142.6
cb	1.7	
1/4	3.2	
♀	5.7	135.9
1/4	7.3	
cb	9.1	
W	11.5	130.1

N 1/4 Walnut

W	11.2	130.4
cb	9.4	
1/4	7.6	
♀	5.6	136.0
1/4	3.6	
cb	2.0	
E	+0.2	141.8

♀ Walnut

E	0.3	141.3
cb	2.6	
1/4	4.2	
♀	5.8	135.8
1/4	7.8	
cb	9.0	
W	11.8	130.3

S 1/4 Walnut

W	12.1	129.5
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T 141.59

4

cb	9.8	
1/4	8.4	
♀	6.7	134.9
1/4	4.7	
cb	3.2	
E	1.2	140.4

S e b Walnut

E	1.7	139.9
cb	3.5	
1/4	5.3	
♀	7.1	134.5
1/4	8.9	
cb	10.7	
W	13.1	128.5

S L Walnut

W	14.2	127.4
cb	12.2	
1/4	10.2	
♀	8.2	133.4
1/4	6.5	
cb	4.8	
E	3.1	138.5

B.M. Nail Tree 22' East of SE

Corner Walnut + Columbia on S L Walnut

0.00 141.59

T 141.59

9-28-29
J.C. Bliss

X-section Chalmers-India
40 Linwood - 80' wide 14' cb - 13' 1/4 5

T.P. -12.93 128.66

0.02 128.68

T.P. 13.10 115.58

0.01 115.58

T.P. 13.08 102.50

0.11 102.61

B.M. S.E. B.P. Chalmers & Columbia 5.54 97.07

Correct 97.06

N

G

+5-edge concrete gutter

⊥

+21-edge concrete gutter

G

S Tp cb

S Tp cb

G

+5-edge concrete gutter

⊥

+21

G

N Tp cb

T.P.

N Tp cb

G

+5

1/4

T 102.61 - Previous page

N.L. Columbia = 0 + 00

8.65 93.96

9.36 92.25

9.18

10.0 92.6

9.50

9.79 92.82

8.87 93.74

0 + 25

12.00 90.61

12.75

12.51

12.4 90.2

12.30

12.69

11.87 90.74

13.27 89.34

+ 009

T 89.43

0 + 50

1.96 87.47

2.70

2.45

2.8

PLOTTED 10-21-29
C.B.H.

π 89.43

£	2.5	86.9
1/4	2.6	
+8	2.50	
G	2.75	
STp cb	1.94	87.49
	0.775	
STp cb	5.22	84.21
G	6.10	
25	5.82	
1/4	5.7	
£	5.8	83.6
1/4	6.2	
+8	5.74	
G	5.96	
N T p c b	5.16	84.27
	1.700	
N T p c b	8.46	80.97
G	9.19	
+5	9.00	
1/4	9.1	
£	9.3	80.1
1/4	9.1	
+8	9.03	
G	9.23	
STp cb	8.45	80.98

π 89.43

6

	1425	
STp cb - Drive net	12.25	77.18
G	12.45	
+5	12.20	
1/4	12.2	
£	12.0	77.4
1/4	12.1	
+8	12.15	
G	12.40	
N T p c b	11.57	77.88
T.P		-13.23 76.23 ⁰
	+0.47	
	π 76.62	
	1450	
N T p c b	2.01	74.61
G	2.80	
+5	2.53	
1/4	3.0	
£	2.4	74.8
1/4	2.8	
+8	2.65	
G	2.88	
STp cb	2.08	74.54

76.62

5 Top cb	529	71.33
	610	
+5	585	
1/4	60	
¢	55	71.1
1/4	57	
+8	5.67	
G - Driveway	6.00	70.62

2.00 = F.L. India

Top cb + Paring Flush	857	68.05
1/4	860	
¢	8.62	68.00
1/4	858	
Top cb + Paring Flush	862	68.00

Note 2.5' x 4' Grotting on North cb. Chalmers flush
with India Paring

B.M. S.M. B.P. Chalmers + India	1054	66.08
	<u>Correct</u>	66.07
B.M. S.E. B.P. Chalmers + Columbia		97.27
+ 8.89		

105.96

W cb Columbia - 75' wide 12 cbs 12.75/45

S.L. Top cb	12.14	93.82
G	12.1	
H/Edge gutter	12.46	
cb - Bottom Gutter	12.78	

105.96

7

+5 = edge concrete gutter	12.50	
1/4	12.2	
¢	12.4	93.5
1/4	12.0	
+8 = edge gutter	12.37	
cb = bottom "	12.62	
+3 = edge "	12.42	
N.L. Top cb	11.95	94.01
G	12.1	

w 1/4 Columbia

N	11.7	94.2
+11 = edge gutter	11.73	
cb = bottom "	12.00	
+5 = edge "	11.73	
1/4	11.4	
¢	11.5	94.4
1/4	11.6	
+8 = edge gutter	11.78	
cb = bottom gutter	12.06	
+3 = edge "	11.72	

S	11.3	94.6
¢ Columbia		
S	10.5	95.4
+11 = edge gutter	11.08	
cb = bottom "	11.40	

π 105.96

ST	+5 = edge gutter	11.10	
	1/4	11.1	
	⊕	10.7	95.2
+3	1/4	10.8	
1/4	+8 = edge gutter	11.02	
⊕	cb = bottom "	11.30	
1/4	+3 = edge "	11.00	
+3	N	10.2	95.7
G			
	E 1/4		
N		9.6	96.3
TP	+11 = edge gutter	10.31	
1/4			
⊕	cb = bottom "	10.62	
⊕	+5 = edge "	10.34	
1/4		10.3	
TP	⊕	10.1	95.8
No	1/4	10.5	
W	+8 = edge gutter	10.40	
B	cb = bottom "	10.69	
B	+3 = edge "	10.42	
	S	10.2	95.7
	E cb		
S-TPcb		90.5	96.91
G		9.5	
	+11 = edge gutter	9.27	
G	cb = bottom "	11.07	
1/4	+5 = edge "	9.27	
cb			

π 105.96

8

1/4		10.0	
⊕		10.5	95.4
1/4		9.8	
	+8 = edge gutter	9.66	
	cb = bottom "	9.90	
	+3 = edge "	9.66	
	N.L. Tap cb	8.27	96.99
G		8.9	
	E.L. Columbia = 0+100 = End existing concrete gutter		
	NTpcb	8.98	96.98
G		9.77	
	+5 = edge gutter	9.48	
	1/4	9.3	
⊕		8.9	97.0
1/4		9.3	
	+8 = edge gutter	9.55	
G		9.81	
	STpcb	9.02	96.94
	0+25		
	STpcb	7.55	98.41
G		8.5	
1/4		8.0	
⊕		7.8	98.1
1/4		8.1	
G		8.1	

π 105.96

N Tpcb	7.72	98.24
	0+50	
N-Tpcb	6.47	98.49
G	6.9	
1/4	6.6	
k	6.4	99.5
1/4	6.8	
G	6.9	
STpcb	6.08	99.88
	0+75	
STpcb	4.58	101.38
G	5.5	
1/4	5.3	
k	5.0	100.9
1/4	5.2	
G	5.7	
N Tpcb	5.16	100.80
	1+00	
n Tpcb	3.97	101.99
G	4.5	
1/4	4.0	
k	3.5	102.4
1/4	3.8	
G	4.1	
STpcb	3.11	102.85

 π 105.96

9

	1+25	
STpcb	16.2	104.34
G	2.7	
1/4	2.3	
k	2.2	103.7
1/4	2.6	
G	3.3	
N Tpcb	2.76	103.20
	1+50	
N Tpcb	1.49	104.47
G	2.1	
1/4	1.4	
k	0.7	105.2
1/4	0.9	
G	1.0	
STpcb	0.07	105.89
T.P.		-0.00 105.74
	13.21	
	π 118.95	
	1+25	
STpcb	11.56	107.39
G	12.6	
1/4	12.4	
k	12.3	106.6
1/4	13.0	
G	13.7	

π 118.95

N T _p cb	13.21	105.74	cb
		<small>State is 75' wide 18' cbs 1225 754</small>	S
	2100 = W.L. State - End existing cb & Wall		
n	11.6		
T _p cb	12.05	106.90	S
G	12.1		cb
1/4	11.6		1/4
⊥	10.9	108.0	⊥
1/4	10.6		1/4
G	10.3		cb
T _p cb	10.02	108.93	N
S	7.3		
	W cb State		
S	6.8	112.1	N
cb	8.8		cb
1/4	9.6		+9
⊥	10.2	108.7	+10
1/4	10.8		1/4
cb	10.9		+8
N	10.6	108.3	⊥
	W 1/4 State		
N	10.1	108.8	+5
cb	9.7		1/4
1/4	9.8		T.P.
⊥	9.2	109.7	
1/4	7.6		

π 118.95

10

	6.6		
	3.6	115.3	
⊥ State			
	+0.4	119.3	
	2.1		
	3.6		
	8.8	110.1	
	8.4		
	8.9		
	8.8	110.1	
	E 1/4 State		
	8.2	110.7	
	7.7		
	7.9		
	5.4		
	6.2		
	7.3		
	5.5	112.4	
	3.0		
	0.3		
		-0.37	118.58
	+1310		
	π 131.68		
	11.2		
	8.6	123.1	

T 131.68

E cb State

S	4.2	127.5
cb	7.2	
1/4	10.4	
1/2	14.9	116.8
+5	16.1	
1/4	15.4	
+8	13.8	
+10	20.3	
cb	20.0	
N	20.1	111.5

E.L. State cut 00

N	19.3	112.4
cb	19.6	
+1	19.6	
+4	11.2	
1/4	11.9	
1/2	11.0	120.7
1/4	8.2	
cb	4.0	
S	1.4	130.3

T.P. SE. Cor + b. Chalmers + State

-1.35 130.33

+13.04

T 143.47

T 143.47

0+25

S	7.7	135.7
cb	11.4	132.0
1/4	14.8	
1/2	16.2	127.2
1/4	16.6	
cb	17.5	
+7	19.0	
+8	22.6	
N	25.8	117.6
0+14	28.6	

0+50

0+5 = edge cut	16.8	
N	15.7	127.5
cb	13.3	
1/4	12.8	
1/2	12.3	131.1
1/4	11.3	
cb	8.0	
S	3.5	139.9

W.L. Linwood - 0+81.8 - S.L. + 0+56.8 N.L.

S	40.4	143.8
cb	3.6	
1/4	7.0	
1/2	8.7	134.7
1/4	9.7	

143.37
143.47

cb 11.4
+10 13.0
N 15.7
Out 10 = edge cut 17.3

127.7

10-14-29 X-section State Street Walnut
J.C. Bliss
Lynn Oredert to N.L. Middletown. '75' wide. 12' cbs
Chuck Ranner 12.75' / 145

12

Proctor

B.M. Walnut tree 22' East of S.E. Cor. Columbus + Walnut on S.L. Walnut 141.59

12.41 157.00

-4.58 149.42

+11.65
161.07

N.L. Walnut = 0+00

W 2.7 158.4

cb 3.6

1/4 5.1

E 6.7 154.4

+10 8.0

1/4 11.5

cb 11.6

E 12.2 148.9

0+25

E 7.2 153.9

cb 5.7

1/4 4.6

E 3.4 157.7

1/4 2.2

cb 1.2

W 1.1 160.0

0+50

W 1.5 159.6

cb 2.0

π 161.07

1/4	2.4	
¢	3.0	158.1
1/4	3.6	
cb	4.2	
E	4.7	156.4
	+7.5	
E	5.0	155.1
cb	4.4	
1/4	4.2	
¢	4.6	156.5
1/4	4.0	
cb	4.0	
W	4.0	157.1
	+4.0	
W	7.9	153.2
cb	7.7	
1/4	7.4	
¢	7.3	153.8
1/4	7.0	
cb	7.2	
E	7.0	154.1
	+2.5	
E	10.2	150.9
cb	10.8	
1/4	11.2	

 π 161.07

13

¢	11.0	150.1
1/4	11.4	
cb	11.4	
W	12.0	149.1
T.P.		-13.04 148.03
	+0.05	
	π 148.08	
	+5.0	
W	3.8	144.3
cb	3.2	
1/4	3.0	
¢	2.6	145.5
1/4	2.4	
cb	0.8	
E	+0.3	148.4
	+4.75	
E	2.6	145.5
cb	4.4	
1/4	6.4	
¢	8.4	139.7
1/4	9.4	
cb	10.2	
W	10.2	137.9
	+2.00	
W	18.4	129.7
cb	16.8	

∑ 148.08

1/4	15.6	
£	13.6	134.5
+5	14.0	
+8	12.2	
1/4	10.3	
cb	7.0	
E	4.7	143.4
2+25		
E	6.6	141.5
cb	8.7	
1/4	12.0	
£	16.1	132.0
1/4	20.0	
+5	21.1	
cb	21.6	
W	24.3	123.8
2+50		
W	27.0	121.1
cb	26.4	
+3	24.4	
1/4	22.2	
£	19.0	129.1
1/4	14.6	
cb	10.7	
F	8.4	139.7

∑ 148.08

14

2+75

E	12.7	135.4
T.P.		134.82
		13.26
		12.26
		135.82
+0.16		
	134.98	
	∑ 135.98	
cb	2.9	
1/4	6.0	
£	7.0	126.0
1/4	12.2	
£9	14.5	
cb	16.7	
W	16.6	118.4
3+00 = 5L Chalmers		
W	23.9	111.1
cb	23.0	
1/4	19.5	
£	15.3	119.7
1/4	12.0	
cb	7.7	
E	4.8	130.2
T.P.		12.79
		122.19
+0.03		
	∑ 122.22	
Niki Chalmers = 0.00		
E	9.8	112.4
cb	10.8	
1/4	11.6	

122.22

¢	12.2	110.0
114	13.6	
cb	14.0	
W	15.1	107.1
0+28	0+28	
W	80	114.2
cb	82	
+5	7.3	
+10	9.2	
1/4	12.9	
¢	12.4	109.8
1/4	11.1	
cb	10.4	
E	9.5	112.7
0+49 = N.L. Middletown on E.L. State		
E+7 = N.L. Middletown	9.6	112.6
cb	10.0	
+3	5.1	
1/4	6.1	
+6	3.7	
¢	4.3	117.9
1/4	5.4	
+5	5.4	
+7	3.8	
cb	3.8	

122.22

15

W	2.8	119.4
T.P.		-0.70 121.52
+11.73		
133.25		
0+85		
W	2.3	130.9
cb	4.2	
1/4	5.3	
¢	4.7	128.5
+5	6.9	
+11.5 = N.L. Middletown	6.9	126.3
+107 = N.L. Middletown on E. State		
¢	+3.0	136.3
1/4	+4.5	
cb	+5.0	
W	+6.0	139.3
+16.5 = W.L. State + N.L. Middletown		
	+16.7	150.0
B.M. S.E. Prop. Hub. Chalmers + State		-2.94 130.31
		Correct 130.33

Page 11

10-18-29 X-section Guy St. Canyon West
 J.C. Blas of Benson to E.L. Middleton Addition
 Diebert 5' cbs 10' 1/45 - 50' wide
 Poney

B.M. S.E. Prop Hub State & Chalmers
 +12.96 143.29
 +13.07 156.33
 +13.13 169.24
 +13.21

130.33 N
 143.26 1/4
 156.11 1/4
 168.98 S

+182.19

East edge of Canyon West of Benson = +100

S 6.0 176.2
 cb 5.4 176.9
 1/4 3.6
 S 1.5 180.7
 +13.11 0.35 181.84
 T.P.

+194.95

1/4 13.2
 +5 10.9
 cb 10.1
 N 9.3 185.6
 N
 1/4
 1/4
 cb

+194.95

16

0430
 4.5 190.3
 5.9
 8.0
 8.6 186.3
 9.8
 11.7 183.3
 12.5 182.4

0460

8.1 186.8
 7.2 187.8
 5.8
 4.6 190.3
 2.9
 0.9
 +0.4 195.3

0.31 194.64

+9.88

+204.52

0485
 5.3 199.2
 6.2
 8.7
 9.4 195.1
 10.8
 13.4 191.1

Plotted 10/21-29 - C.B.M.

T 204.52

S	144	190.1
	1+10	
S	11.2	193.3
cb	10.3	194.2
1/4	8.5	
£	6.8	197.7
1/4	5.6	
cb	3.3	
N	2.1	202.4
	1+35	
N	0.1	204.4
cb	1.0	
1/4	3.9	
£	5.2	199.3
1/4	6.4	
cb	8.4	196.1
S	9.7	195.1
	1+60 = Wil Benson	
S	9.1	195.4
cb	7.5	197.0
1/4	5.7	
£	4.7	199.8
1/4	3.3	
cb	0.8	
N	40.2	204.7

T 204.52

17

S.L. Benson = 07.00

N	7.6	196.9
cb	8.8	
1/4	10.3	
£	11.4	193.1
1/4	12.6	
	T.P.	-13.00 191.52
	+0.27	T 191.79
cb	1.3	
S.L.	1.4	190.4
EM	S.E. prop high Guyard Benson	1.36 190.43
	0+25	
S.L.	9.1	182.7
cb	8.8	
£	7.8	
£	6.8	185.0
1/4	5.1	
cb	3.0	
N	3.1	188.7
	0+50	
N	9.6	182.2
cb	11.0	
1/4	13.0	
£	14.3	177.5
1/4	15.5	
cb	46.6	

191.79

S 17.0 174.8
0+87.75 = EL. Midd. Odd - N.L. Guy

S 25.3 166.5

cb 24.5

1/4 22.7

E 21.1 170.7

1/4 19.5

cb 17.8

N 17.4 174.4

Section along E.L. Middletown Odd from

0+87.75 on N.L. Guy to 1+23.54 S.L. Guy

N 17.4 174.4

cb 18.6

1/4 21.0

E 24.0 167.8

1/4 26.5

cb 27.5

S 29.3 162.5

T.P. -12.50 179.29

+0.37 179.66

T.P. -13.22 166.44

+0.09 166.53

T.P. 12.60 153.93

001 153.94

153.94

T.P.

-12.58 141.36

+0.09 141.45

B.M. S.E. Prop. Hub. State & Chalmers

11.06 130.39

Correct 130.33

Page 11

Note

Notes on Linwood - Fremont to Benson

Book 1217 - Page 28

Benson - Linwood to E.L. Middletown Odd - 1217 - 37

Sta	+	T	-	Elev	T		
S.W.B.P. Chalmers	+ India			66.07	137.34		
	12.87				B.M. S.E. Prop. Hub. State & Chalmers	7.06	130.28
T.P.			0.26	78.68		Correct	130.33
	12.90						
T.P.			0.09	91.49			
	13.21	104.70					
B.M. S.E. B.P. Chalmers & Columbia				7.65	97.05	True 97.07	
T.P.				0.37	104.33		
	+13.07	117.40					
T.P.				0.00	117.40		
	+13.11	130.51					
B.M. S.E. Prop. Hub	State & Chalmers			0.21	130.30	True 130.33	
	+13.13	143.43					
T.P.				0.19	143.24		
	1.64	144.88					
B.M. Nail in tree 22'	East. of S.E			3.29	141.59	Correct	
Cor. Walnut & Columbia	on S.E. Walnut				141.59		
	13.02	154.61					
T.P.				0.67	153.94		
	7.71	161.65					
T.P.				12.91	148.74		
	0.35	149.09					
T.P.				12.48	136.61		
	0.73	137.34					

12-2-29
 J.C. Bliss
 Robert
 Connor
 McHugh

X-section Eleanor Drive (Encanto)
 See sketch page 04 Book 1368 for sketch
 also page 24 this book
 50' wide 10' cbs - 30' Roadway

B.M. N.W. Prop Hub 65th v Eleanor 409.57
 13.05

π 422.62
 0700

15' out

N
 +8
 cb
 ‡
 cb
 +5
 S
 S
 +5
 cb
 ‡
 +6
 cb
 N
 Out 15
 Out 15
 N
 cb

Plotted 12-5-29 TGH

17.5
 13.6 409.0
 11.1
 10.8
 10.2 4124
 8.3
 6.9
 6.2 4164
 0+25
 4.0 4186
 5.2
 7.4
 8.9 137
 9.0
 11.9
 15.0 076
 17.4
 0+50
 15.8
 13.5 090
 11.1

+13
 ‡
 cb
 +4
 S
 S
 +5
 cb
 ‡
 +2
 cb
 N
 Out 15
 Out 15
 N
 cb
 +8
 ‡13
 ‡
 cb
 +4
 T.P.

π 422.62

0+75

1400

7.6
 7.5 15.1
 6.2
 4.3
 3.1 19.5
 2.0 20.6
 2.9
 4.3
 4.8 17.8
 4.8
 7.9
 11.2 114
 15.2
 12.6
 8.8 138
 6.1
 4.4
 2.8
 2.8 198
 2.0
 0.7
 0.64 421.98

10.97 432.95

π 43295

S	9.9	23.1
	1+25	
S	6.3	26.7
+8	8.2	
cb	9.4	
ϕ	10.6	22.4
+4	10.6	
+10	13.0	
cb	14.3	
N	16.8	16.2
Out 15	20.0	
	1+50	
Out 15	18.1	
N	14.7	18.3
cb	10.2	
+8	8.0	
ϕ	8.3	24.7
+10	7.1	
cb	5.1	
S	3.6	29.4
	1+75	
S	0.4	32.6
cb	2.6	
+3	2.9	
+8	4.8	

π 43295

20

ϕ	5.3	27.7
+8	5.4	
cb	7.0	
N	11.1	21.9
Out 15	15.4	
	2+00	
Out 15	10.8	
N	8.0	25.0
cb	3.5	
ϕ	2.9	30.1
+6	2.1	
+10	0.4	
T.P.		0.00
		43295
		+906
	π 442.01	
cb	8.6	
S	5.9	36.1
	2+25	
S	3.0	39.0
cb	4.6	
+5	5.6	
+10	8.2	
ϕ	9.0	33.0
cb	10.8	
N	13.8	28.2

Σ 442.01

Out 15

17.6

N

2+54.63 = N.L. Eleanor 25' strip - ^{Sketch} - Page 24

out 15

13.4

E

N

10.9

31.1

S

cb

7.4

0+25

+3

6.4

S

1.2

1.6

1.2

0+50

1.9

2.5

2.3

0+75

6.7

5.8

4.7

1+00

8.6

9.8

11.7

13.8

12.20

Σ 430.34

21

0+00 = Eleanor Now 25' wide

2.1

39.9

2.4

1.2

0.6

41.4

40.8

40.8

40.1

39.7

35.3

37.3

33.2

30.3

12.20

429.81

7+27 West
139 West - 2

see sketch
Page 24

5.0

3.1

Out 15

0.53

430.34

1+25

Out 15	6.1	24.2
Out 12	5.3	
S	4.9	25.4
⊕	2.7	
N	1.3	29.0

1+50

N	5.2	25.1
⊕	6.7	
+4	6.9	
S	9.2	21.1
Out 15	13.3	

1+75

Out 15	17.8	
S	13.6	16.7
⊕	8.5	
+2	8.0	
N	7.4	22.9

2+00

N	5.9	24.4
+5	7.9	
⊕	8.0	
+3	8.0	
S	12.5	17.8
Out 15	17.4	

430.34

2+25

Out 15	17.7	
S	13.3	17.0
+7	10.0	
⊕	9.7	
+5	9.3	

+10

N	6.6	
N	5.6	24.7

2+50

N	5.1	25.2
+10	10.2	
⊕	10.4	
+7	10.6	
S	13.2	17.1

Out 15

Out 15	17.0	
--------	------	--

2+75

Out 15	17.3	13.0
N ⊕	13.4	16.9
+5	10.8	
⊕	10.5	
+4	9.5	
+5	8.0	
N	5.1	25.2

22

430.34

3400

N	6.3	24.0
+5	7.9	
+	11.0	
+8	11.4	
S	13.7	16.6
Out 15	17.7	

2+25

Out 15	19.3	
S	14.9	15.4
+5	12.9	
+	12.7	
+2	12.2	
+7	9.8	
N	8.0	22.3

3+51.67

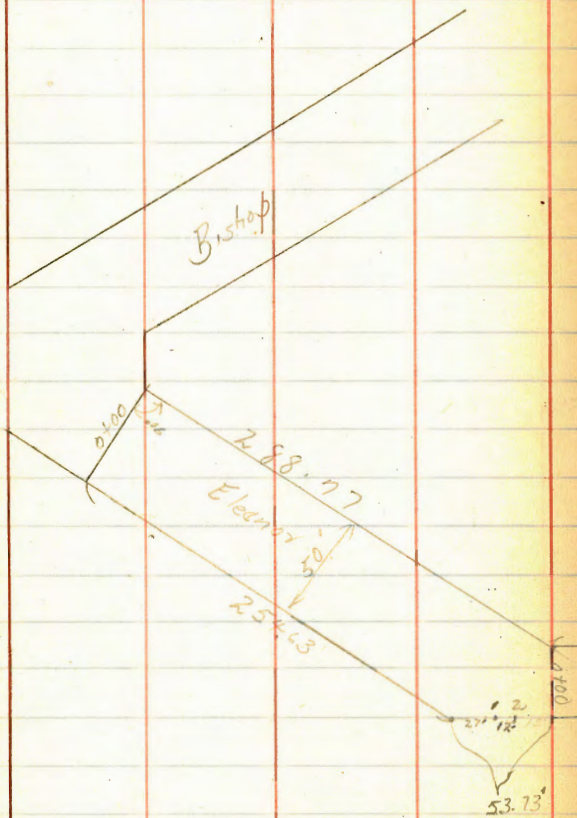
Subdivision Line

N	10.0	20.3
+7	11.5	
+	13.8	
+8	14.1	
S	18.0	14.3
Out 15	20.2	

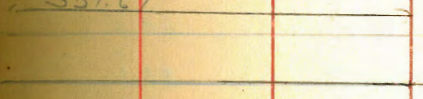
B.M. Top Pipe N. Li. Edmunds Tract + N. Li. Eleanor 9.97 420.37

Correct 420.41

6.574



351.67'



12-2-29 X-section B St. Leman Grove Blvd
 J.C. Bliss to 43rd St. - 50' wide - 5' cbs
 Drebert 10' x 45
 Ranner
 McHugh Stationed same as original x-section - Book 1269 - Page 47

B.M. Mon. Intersection of B St. & St. Leman Grove Blvd 87.13

+13.06

T 100.19

0+00

North-Leman Grove Paving 11.90 88.29

cb - " " 11.85 88.34

1/4 " " " 11.95 88.24

£ " " " 12.13 88.06

+4-South edge Leman Grove Paving 12.21 87.98

1/4 12.4 87.8

cb 12.2 88.0

S-Base cut 12.0 88.2

Tip 9.0 91.2

0+53-Intersection N.H. B St & South edge Leman Grove Paving

S-Top cut 7.6 92.6

Base cut 11.4 88.8

cb 11.7 88.5

+ 12.1 88.1

1/4 11.8 88.4

£ 11.5 88.7

1/4 11.5 88.7

cb 12.1 88.1

N-South edge Leman Grove Paving 11.70 88.49

T 100.19

25

0+75

N 11.1 89.1

cb 11.3 88.9

1/4 10.8 89.4

£ 10.8 89.4

1/4 11.3 88.9

+9 11.9 88.3

cb 11.2 89.0

S-Base cut 11.2 89.0

Top 6.8 93.4

1+00

S-Top cut 6.7 93.5

Base 10.6 89.6

cb 10.7 89.5

1/4 11.3 88.9

1/4 10.6 89.6

£ 10.3 89.9

1/4 9.9 90.3

cb 10.4 89.8

N 9.8 90.4

1+25

N 9.7 90.5

cb 9.5 90.7

1/4 9.8 90.4

+8-Top cut 7.7 92.5

£-Base 9.7 90.5

π 100.19

1/4	9.7	90.5
+9	10.6	89.6
cb	9.9	90.3
S-Base cut	9.8	90.4
Top	5.7	94.5
	1+50	
S-Top cut	4.0	96.2
Base	8.4	91.8
cb	8.4	91.8
H	9.1	91.1
1/4	8.4	91.8
$\frac{1}{2}$ -Base cut	8.2	92.0
+2-Top	7.5	92.7
1/4	8.3	91.9
cb	7.9	92.3
N	8.4	91.8
	1+75	
N-Edge fill	6.0	94.2
cb	5.8	94.4
1/4	6.1	94.1
+9-Top cut	5.3	94.9
$\frac{1}{2}$ -Base	6.4	93.8
1/4	6.6	93.6
+9	7.2	93.0
cb	6.6	93.6

 π 100.19

26

S-Base cut	6.6	93.6
Top	2.6	97.6
	2+00	
S-Top cut	2.9	97.3
Base	4.3	95.9
cb	4.6	95.6
H	5.1	95.1
1/4	4.6	95.6
$\frac{1}{2}$	4.3	95.9
1/4	4.5	95.7
cb	4.3	95.9
N-Edge fill	4.8	95.4
	2+25	
N-Edge fill	3.1	97.2
cb	2.6	97.6
1/4	2.6	97.6
$\frac{1}{2}$	2.2	98.0
1/4	2.3	97.9
+9	2.9	97.3
cb	2.2	98.0
S	2.1	98.1
cut	2.4	97.8

$\pi 100.19$

2450

Out 1	0.6	99.6
S	0.0	100.2
cb	0.0	100.2
+1	0.7	99.5
1/4	0.1	100.1
¢	0.2	100.0
1/4	0.7	99.5
cb	1.2	99.0
N-Edge fill	1.5	98.7

-0.30 99.89

+13.09

 $\pi 112.98$

2475

N-edge fill	12.5	100.4
cb	11.5	101.4
+1	11.4	101.5
¢	11.0	101.9
1/4	10.9	102.0
+9	11.6	101.3
cb	10.7	102.2
S	10.7	102.2
out 1	11.6	101.3

 $\pi 114.98$

3400

Out 1	9.8	103.1
S	8.5	104.4
cb	8.7	104.2
+1	9.4	103.5
1/4	8.7	104.2
¢	8.8	104.1
1/4	9.0	103.9
cb	9.1	103.8
N-edge fill	9.8	103.1

3425

N-edge fill

N-edge fill	8.0	104.9
cb	6.4	106.5
1/4	6.6	106.3
¢	6.4	106.5
1/4	6.4	106.5
+9	6.9	106.0
cb	6.2	106.7
S	6.3	106.6
Out 1	7.5	105.4

3450

Out 1	5.0	107.9
S	4.9	108.0
cb	4.3	108.6
+1	5.1	107.8
1/4	4.5	108.4

27

π 112.98

♀	4.3	108.6
1/4	4.6	108.3
cb-edge fill	6.0	106.9
N	8.5	104.4
3+25		
N	6.8	106.1
cb	6.5	106.4
+5	5.5	107.4
1/4	3.7	109.2
+5-edge fill	2.0	110.9
♀	2.0	110.9
1/4	2.2	110.7
+9	2.9	110.0
cb	2.4	110.5
S-Base cut	2.7	110.8
Top "	1.5	111.4

0.29 112.89

π 125.60

4+20		
S-Top cut	7.1	118.5
Base "	12.3	113.3
cb	12.7	112.9
1/4	13.4	112.2
1/4	12.5	113.1

π 125.66

28

♀-Base cut	12.4	113.2
1/4-Top "	8.5	117.1
1/4	10.2	115.4
cb	11.0	114.6
N	11.3	114.3
4+17		
N	5.6	120.0
cb	5.7	119.9
1/4	4.7	120.9
+9-Top cut	4.2	121.4
♀-Base "	10.6	115.0
1/4	11.0	114.6
+9	11.8	113.8
cb	11.0	114.6
S-Base cut	10.8	114.8
Top "	3.6	122.0

4+50

S-Top cut	1.5	124.1
Base "	8.0	117.6
cb	8.2	117.4
1/4	8.7	117.0
1/4	8.1	117.5
♀-Base cut	8.1	117.5
1/4-Top "	2.0	123.6
1/4	2.5	123.1

T 125.66

cb	3.6	122 0
N	4.1	121 5
5+00		
N	1.6	124 0
cb	1.2	124 4
1/4	0.4	125 2
+9 = Top cut	0.3	125 3
2 = Base "	4.4	121 2
1/4	4.4	121 2
+9	5.1	120 5
cb	4.2	121 4
S-Base Cut	4.3	121 3
Top	41.5	127.1

S -0.59 125.07

+12.39

T 137.46

5+50

S-Top cut	8.3	129 1
Base "	11.9	125 5
cb	12.3	125 1
H	13.2	124 2
1/4	12.3	125 1
2 = Base cut	11.9	125 5
+2 Top "	11.2	126 2
1/4	11.3	126 1

T 137.46

29

cb	11.5	126 0
N	11.7	125 7
6+00		
N	10.5	127 0
cb	10.1	127 4
1/4	9.8	127 6
2	8.9	128 5
1/4	8.9	128 5
+9	9.5	128 0
cb	8.8	128 6
S-Base cut	8.5	129 0
Top	7.3	130 1

6+50

S	5.0	132 5
cb	5.3	132 1
H	5.9	131 5
1/4	5.4	132 0
2 = Edge gill	5.4	132 0
+7 = Toe slope	8.1	129 3
1/4	8.5	128 9
cb	9.1	128 3
N	9.2	128 2

137.46

7+00

N.	8.9	128.5
cb	8.7	128.7
1/4 = Toe Slope	7.6	129.8
1/2 = Edge Gill	1.9	135.5
1/4	2.1	135.3
+9	3.1	135.3
cb	2.2	135.2
S	2.1	135.3

7+25

Out 1	0.8	137.6
S	0.2	137.2
cb	0.2	137.2
1/4	1.0	136.4
1/4	0.3	137.1
1/2 = Edge Gill	0.0	137.4
1/4	5.2	132.2
+V = Toe Slope	6.3	131.1
cb	2.8	129.6
N	8.2	129.2

7+50

N	6.2	131.2
cb	5.6	131.8
+6 = Toe Slope	5.2	132.2
1/4	3.0	134.4

T.P. = East end catch basin

2.95 134.51

30

134.51

+ 12.95

147.46

1/2 = edge gill	7.8	139.6
1/4	8.3	139.1
+9	9.0	138.4
cb	8.2	139.2
N	8.1	139.3
Out 1	9.0	138.4

7+75

Out 1	7.0	140.4
S	6.3	141.1
cb	6.6	140.8
1/4	7.2	140.2
1/4	6.5	140.9
1/2 = edge gill	6.1	141.3
1/4	9.9	137.5
cb	12.9	134.5
N = Toe Slope	13.9	133.5

8+00

N	9.9	137.5
cb	8.4	139.0
1/5 = edge gill	6.3	141.1
1/4	5.8	141.6
1/4	4.9	142.5
1/4	4.8	142.6
+9	5.5	141.9

π 147.46

cb	4.7	142.7
S-Base cut	4.6	142.8
Top "	2.2	145.2
	8+2.5	
S-Top cut	0.9	146.5
Base "	3.2	144.2
cb	3.3	144.1
1/4	4.0	143.4
1/4	3.3	144.1
1/4	3.5	143.9
1/4	3.7	143.7
+5-edge fill	4.0	143.4
cb	5.7	141.7
N	7.2	140.2
	8-5.0	
N	5.2	142.2
cb	3.8	143.6
+5-edge fill	2.0	145.4
1/4	1.9	145.5
1/4	1.4	146.0
1/4	1.6	145.8
+9	2.1	145.3
cb	1.6	145.8
S-Base cut	1.6	145.8
Top "	+3.2	150.6

 π 147.46

31

TIP	0.12	147.34
	+12.67	
	π 160.01	
	8+7.5	
S-Top cut	7.1	152.9
Base "	12.2	147.8
cb	12.2	147.8
1/4	13.0	147.0
1/4	12.3	147.7
1/4	12.0	148.0
1/4	12.6	147.4
cb-edge fill	13.7	146.3
N	15.0	145.0
	8+9.0	
N	15.8	144.2
cb	14.7	145.3
1/4	11.0	149.0
+9-Top cut	10.4	149.6
1/4-Base "	11.1	148.9
1/4	11.2	148.8
+9	11.8	148.2
cb	11.7	148.3
S-Base cut	10.9	149.1
Top "	5.7	154.3

π 160.01

9+10

S-Top cut	3.4	156.6
Base "	9.7	150.3
cb	9.8	150.2
1/4	10.5	149.5
1/4	9.9	150.1
♀ = Base cut	9.5	150.5
1/4 - Top	9.2	150.8
1/4	9.8	150.2
+ S-edge fill	10.0	150.0
cb	12.0	148.0
N	13.8	146.2

9+40

N	10.7	149.3
cb	9.6	150.4
1/4	7.1	152.9
+ 9 = Top cut	6.2	153.8
♀ = Base "	7.8	152.2
1/4	7.8	152.2
+ 9	8.4	151.6
cb	7.9	152.1
S-Base cut	7.9	152.1
Top	2.5	157.5

π 160.01

9+75

S-Top cut	0.4	159.6
Base "	6.1	153.9
cb	6.3	153.7
1/4	6.9	153.1
1/4	6.2	153.8
♀ = Base cut	5.9	154.1
1/4 - Top	4.4	155.6
1/4	5.5	154.5
cb	7.8	152.2
N	9.4	150.6

10+00

N	7.1	152.9
cb	6.1	153.9
1/4	5.3	154.7
♀ = Top cut	4.1	155.9
♀ = Base "	4.7	155.3
1/4	5.0	155.0
1/4	5.6	154.4
cb	4.9	155.1
S-Base cut	4.9	155.1
Top	10.5	160.5

32

T 160.01

10+35

S-Top cut	+3.6	163.6
Base "	3.3	156.7
cb	3.5	156.5
H	4.2	155.8
1/4	3.6	156.4
L=Base cut	3.4	156.6
H=Top "	2.6	157.4
1/4	3.4	156.6
cb	4.1	155.9
N	4.4	155.6

10+75

N	3.8	156.2
cb	3.3	156.7
1/4	2.9	157.1
+9=Top cut	1.4	158.6
L=Base "	2.1	157.9
1/4	2.3	157.7
+9	3.0	157.0
cb	2.3	157.7
S-Base cut	2.2	157.8
Top "	2.9	157.1

T 160.01

10+95

S-Top cut	+3.9	163.9
Base "	1.6	158.4
cb	1.7	158.3
H	2.5	157.5
1/4	1.9	158.1
L=Base cut	1.8	158.2
H=Top "	1.0	159.0
1/4	2.1	157.9
cb	2.3	157.7
N	2.9	157.1

11+20³⁶

N	2.8	157.2
cb	2.2	157.8
1/4	1.8	158.2
+9=Top cut	0.6	159.4
L=Base "	1.1	158.9
1/4	1.7	158.8
cb	1.8	158.2
S-Base cut	1.0	159.0
Top cut	+2.0	162.0
B.M. on E. B. St about 43' East 43rd	5.92	154.09
Correct		154.15

Note: Any change in Northern section of B. St from original x-section is due to dumping of loose dirt by contractor or to movement of equipment over ground.

33

12-3-29 X-section of Breaks on Improvement
 J. C. Bliss Profile not actually covered in x-section
 Drebert pages 25-33 this book - S. St.
 Roney

50 w/c
 5' cbs
 10' 4/4s

π 99.51 34

B.M. Man & B. N. Lomen Grove Rd. 87.13
 +12.44

π 99.57
 +0.90

S-Top bank 6.8 92.8
 Base " 10.1 89.5
 cb 10.2 89.3
 H 11.0 88.5
 1/4 10.2 89.3
 ♀ 9.9 89.6
 1/4 9.6 90.0
 cb 9.7 89.8
 N 10.1 89.4

+1.10

N 9.8 89.7
 cb 9.6 90.0
 1/4 9.1 90.4
 +8=Top cut. 8.7 90.8
 ♀=Base " 9.4 90.1
 1/4 9.6 90.0
 +9 10.4 89.1
 cb 9.8 89.7
 S-Base cut 9.6 90.0
 Top 5.6 94.0

S-Top cut 5.0 94.6
 -Base " 8.8 90.8
 cb 8.9 90.7
 H 9.7 89.8
 1/4 8.8 90.8
 ♀=Base cut 8.8 90.8
 +7=Top " 7.1 92.4
 1/4 8.0 91.6
 cb 8.2 91.3
 N 8.5 91.0

+1.70

N 5.6 94.0
 cb 5.5 94.0
 1/4 5.6 94.0
 +8=Top cut. 4.9 94.6
 ♀=Base " 6.1 93.5
 1/4 6.4 93.1
 +9 7.0 92.6
 cb 6.2 93.3
 S-Base cut 6.3 93.2
 Top 2.0 97.5

T.P. 0.48 99.09
 +12.05 112.14
 0.03 112.11
 +13.02 125.13

T 12513

4+60

S-Top cut	0.5	124.6
Base "	6.5	118.6
cb	6.7	118.4
H	7.5	117.6
1/4	6.7	118.4
L-Base cut	6.5	118.6
H	0.8	124.3
4	1.1	124.0
cb	2.2	122.9
1/4	2.8	122.3
T.P.		0.70 124.43

+11.92

T 136.35

5+40

N	11.0	125.3
cb	10.8	125.5
1/4	10.5	125.8
+9-Top cut	10.3	126.0
L-Base "	11.7	124.6
1/4	11.8	124.5
+9	12.7	123.6
cb	11.9	124.4
S-Base cut	11.6	124.7
Top "	7.5	128.8

T 136.35

35

T.P. East end catch basin	1.82	134.53
	+13.03	

T 147.56

T.P.	0.20	147.36
------	------	--------

+12.65

T 160.01

9+00

S-Top cut	4.2	155.8
Base "	10.4	149.6
cb	10.5	149.5
H	11.2	148.8
1/4	10.6	149.4
L-Base cut	10.5	149.5
+9-Top "	9.9	150.1
1/4	10.5	149.5
+3-edge fill	11.7	149.3
cb	14.0	146.0
N	15.8	144.2
	9+20	
N	12.7	147.3
cb	11.1	148.9
1/4	9.7	150.3
Q	8.6	151.4
1/4	9.0	151.0
+9	9.7	150.3
cb	9.2	150.8

Σ 160.01

S-Base cut	9.0	151.0
Top "	9.4	156.6
9+60		
S-Top cut	1.7	158.3
- Base "	6.7	153.3
cb	6.8	153.2
H	7.4	152.6
1/4	6.8	153.2
E-Base cut	6.5	153.5
H-Top "	6.0	154.0
1/4	7.2	152.8
cb	9.0	151.0
N	10.4	149.6
9+80		
N	8.8	151.2
cb	7.4	152.6
1/4	5.0	155.0
+9=Top cut	3.7	156.3
q=Base "	5.5	154.5
1/4	5.9	154.1
+9	6.6	153.4
cb	5.9	154.1
S-Base cut	5.6	154.4
Top "	10.4	160.4

Σ 160.01

36

10+40

S-Top cut	+1.6	161.6
Base "	3.8	156.2
cb	4.0	156.0
H	4.8	155.2
1/4	4.1	155.9
q=Base cut	3.9	156.1
H-Top "	3.1	156.9
1/4	4.2	155.8
cb	4.9	155.1
N	6.0	154.0
10+40		
N	4.3	155.7
cb	3.9	156.1
1/4	3.3	156.7
+9=Top cut	2.4	157.6
q=Base "	3.1	156.9
1/4	3.4	156.6
+9	4.0	156.0
cb	3.3	156.7
S-Base cut	3.7	156.8
Top "	43.5	163.5

160.01

10460

S-Top cut	+2.9	162.9
Base "	2.4	157.6
cb	2.7	157.3
H	3.3	156.7
1/4	2.7	157.3
E-Base cut	2.5	157.5
H-Top "	1.6	158.4
1/4	2.6	157.4
cb	3.2	156.6
N	3.7	156.3

10480

N	3.7	156.3
cb	3.0	157.0
1/4	2.7	157.3
+9-Top cut	0.7	159.3
E-Base "	1.9	158.1
1/4	2.2	157.8
+9	2.8	157.2
cb	2.1	157.9
S-Base cut	2.0	158.0
Top "	+3.4	163.4

160.01

11400

37

S-Top cut	+3.8	163.8
-Base "	1.6	158.4
cb	1.7	158.3
H	2.5	157.5
1/4	1.2	158.3
E-Base cut	1.7	158.3
H-Top "	1.0	159.0
1/4	2.3	157.7
cb	2.2	157.8
N	3.1	156.9

B.M. Mon & B 43' East of 43rd -5.92 154.07

Correct 154.15

12-16-29 X-section Benson St. 103' North of
 J.C. Bliss Guy to Linwood - 50' wide - 10' cos
 J. Brebert 25/45
 Lanner

S.M. N.E. Prop. Hub Benson & Guy		204.70	W
+12.68	217.38		cb
T.P.		-0.03	1/4
+11.26	228.61		E
	*		1/4
103' North of Guy =	0+00		cb
W		2.0	E
cb		2.7	T.P.
1/4		3.1	
E		2.0	
+2		1.8	
1/4		0.0	E
cb		0.8	cb
E		3.2	+5
	0+15		1/4
E		12.7	E
cb		10.6	1/4
1/4		9.2	cb
E		6.7	W
1/4		6.6	
cb		6.6	W
W		5.9	cb

226.6
225.9
225.5
226.6
226.8
228.6
227.8
225.4
215.9
219.0
219.4
221.9
222.0
222.0
222.7

T 228.61
0+25
7.7
9.1
9.4
10.1
12.3
14.0
18.2
215.74
T
0+50
11.7
9.5
6.4
5.7
3.6
2.1
1.4
0.6
0+75
5.6
7.0
7.7
7.9
9.7

-13.23

38
220.9
219.5
219.2
218.5
216.3
214.6
210.4
215.38
204.0
206.2
209.3
210.0
212.1
213.6
214.3
215.1
210.1
208.7
208.5
207.8
206.0

π 215.74

0+75 (cont)

cb	12.0	203.7	1/4
E	14.6	201.1	cb
	1+03 = N.L. Guy	50' wide 10' cbs 7.5' 1/4s	W
E	18.8	196.9	
cb	15.9	199.8	W
1/4	13.5	202.2	cb
φ	12.4	203.3	1/4
1/4	12.1	203.6	φ
cb	12.0	203.7	1/4
W	11.0	204.7	cb
T.P.		-13.08 202.66	E

+0.34 π 203.00

	N cb Guy		E
w	0.7	202.3	cb
cb	0.9	202.1	1/4
1/4	0.8	202.2	φ
φ	1.6	201.4	1/4
1/4	2.8	200.2	cb
cb	5.0	198.0	W
E	7.8	195.2	

N 1/4 Guy

E	9.1	193.9	W
cb	6.2	196.8	cb
1/4	4.1	198.9	1/4
φ	2.8	200.2	φ

π 203.00

39

	2.3	200.7	
	2.3	200.7	
	2.3	200.7	
φ Guy	3.2	199.8	
	3.5	199.5	
	3.7	199.3	
	4.2	199.8	
	5.1	197.9	
	7.1	195.9	
	10.2	192.8	

S 1/4 Guy

	11.1	191.9	
	8.2	194.8	
	6.1	196.9	
	5.2	197.8	
	4.7	198.3	
	4.3	198.7	
	3.9	199.1	

S cb Guy

	5.1	197.9	
	5.8	197.2	
	6.1	196.9	
	6.1	196.9	
	7.0	196.0	

π 203.00

cb	91	193.9
E	12.1	190.9
B.M. S.E. Hub Guy + Benson	12.57	190.43
S.W. Guy = 0+00		
E	12.6	190.4
cb	9.9	193.1
1/4	7.8	195.2
¢	8.0	195.0
1/4	7.4	195.6
cb	7.9	195.1
W	7.5	195.5
0+25		
W	11.3	191.7
cb	11.1	191.9
1/4	11.2	191.8
¢	11.0	192.0
1/4	11.4	191.6
cb-	12.2	190.8
E = Top cut	12.6	190.4
0+1 = Base cut - House yard	17.9	185.1
0+30		
E	18.1	184.9
+2 = Base cut	17.9	185.1
+3 = Top cut	12.4	190.6
cb	12.7	190.3

π 203.00

40

1/4	11.8	191.2
¢	11.7	191.3
1/4	11.9	191.1
cb	12.1	190.9
W	12.0	191.0
T.P.		-12.85 190.15
+0.09		
π 190.24		
0+50		
W	2.4	187.8
cb	2.6	187.6
1/4	2.0	188.2
¢	1.6	188.6
1/4	1.6	188.6
cb	2.1	188.1
+6 = Top cut	2.4	187.8
+7 = Base	5.4	184.8
E	5.6	184.6
0+75		
E	6.7	183.5
+7	6.6	183.6
cb	6.1	184.1
1/4	5.5	184.7
¢	5.4	184.8
1/4	5.9	184.3

T 190.24

cb 6.2 183.5
W 6.2 184.0

+0.1

W 11.1 179.1
cb 10.7 179.5
1/4 10.0 180.2
q 9.8 180.4
1/4 9.7 180.5
cb 10.4 179.8
+5 8.5 181.7
E 8.4 181.8

Out 5 = floor level House 6.81 183.43

+0.4

E 11.6 178.6
+3 11.4 178.8
+6 10.3 179.9
cb 10.6 179.6
1/4 10.3 179.9
q 10.2 180.0
1/4 10.4 179.8
cb 11.1 179.1
W 11.4 178.8

13.08 177.16

+0.79 T 177.93

T 177.95

41

+0.8 and +2.2 two small eucalyptus trees 9.7' in St. from East Line

+2.5

W 2.4 175.5
cb 1.8 176.1
1/4 1.5 176.4
q 1.4 176.5
1/4 1.7 176.2
cb 2.4 175.5
E 2.0 175.9

+4.34

Out 10' from E.L. Lower concrete step to apartment House 1.96

175.99

+5.1

Out 10' from E.L. Lower concrete step to apartment House 3.40

174.55

B.C. = 1753.88 West Line + 1754.12 E.L.

175.03

E 5.0 172.9
cb 5.7 172.2
1/4 6.6 171.3
+2 5.6 172.3
q 5.5 172.4
1/4 5.5 172.4
cb 5.5 172.4
W 6.0 171.9

π 177.95

42

B.M. Nails in Pole Benson-Linwood 704 170.91
+ 0.17

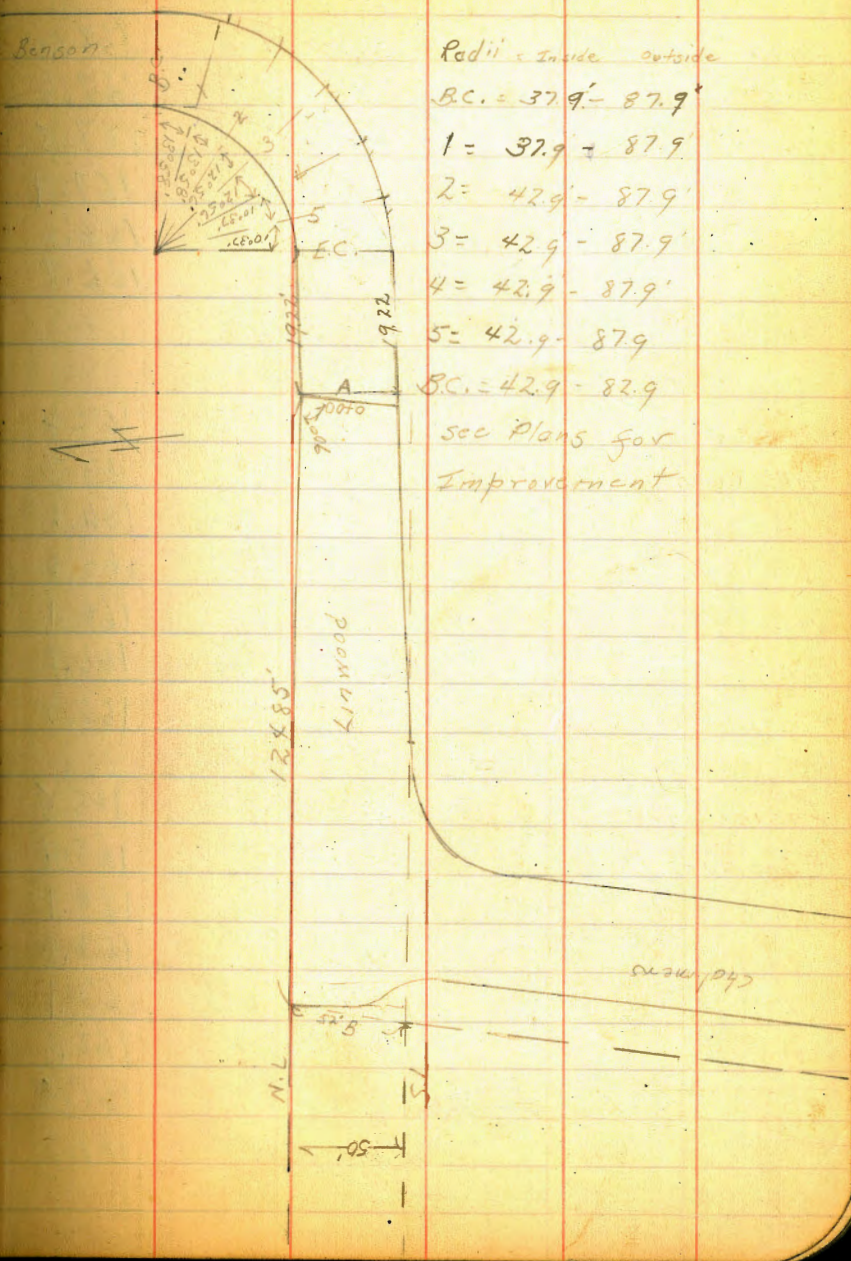
π 171.08

#1 = See sketch

Inside curve	0.1	171.0
+ 1.2 on radial line = W.L. Benson	0.2	170.9
cb	0.0	171.1
1/4	0.3	170.8
1/2	0.3	170.8
3/4	0.8	170.3
cb	1.9	169.2
Outside curve	2.6	168.5
Out 17 Spot on concrete drive to Garage	2.59	168.47

#2

Outside curve	4.0	167.1
+ 10 = cb	2.9	168.2
1/4	2.5	168.6
1/2	2.3	168.8
3/4	2.2	168.9
cb	1.7	169.4
+ 5 = Inside curve	0.6	170.5



Radii - inside outside

BC = 37.9' - 87.9'

1 = 37.9' - 87.9'

2 = 42.9' - 87.9'

3 = 42.9' - 87.9'

4 = 42.9' - 87.9'

5 = 42.9' - 87.9'

BC = 42.9' - 82.9'

see plans for

Improvement

π 17:08

#3

Inside curve	3.1	168.0
+5= curb	3.5	167.6
1/4	3.6	167.5
¢	3.7	167.4
1/4	4.5	166.6
cb	4.4	166.7
+10= Outside curve		

#4

Outside curve	7.7	163.4
+10= curb	7.4	163.7
1/4	6.5	164.6
¢	5.5	165.6
1/4	5.0	166.1
cb	5.0	166.1
+5= Inside curve	4.8	166.3

#5

Inside curve	5.6	165.5
+5= curb	5.7	165.4
1/4	6.2	164.9
¢	7.2	163.9
1/4	8.0	163.1
cb	8.8	162.3
+6.3= N.L. Middle town edge grading	9.6	161.5
+10= Outside curve	9.8	161.3

π 17:08

43

F.C.

Outside curve	12.0	159.1
+5= curb	11.3	159.8
1/4	10.1	161.0
¢	9.4	161.7
1/4	8.1	163.0
cb	7.2	163.9
+5= Inside curve	6.9	164.2

Section A= see sketch

N	10.0	161.1
+5= cb	10.9	160.2
1/4	11.8	159.3
¢	12.5	158.6
1/4	12.9	158.2
cb	14.0	157.1
+5= N.L. Middle town edge grading	14.4	156.7

0+00= see sketch - s-section limwood 50' wide 10' cbs
7 1/2" 1/45

S	16.9	154.2
+8.7= edge improvement	16.0	155.1
cb	15.9	155.2
1/4	15.1	156.0
¢	13.5	157.6
1/4	12.8	158.3
cb	11.9	159.2
N	10.1	161.0

T 171.08

T.P. 12.73 158.35 cb

+032

1/4

T 158.67

¢

0+32 = Intersection N.L. Middletown w/ L. Linwood

1/4

N 0.2 158.5 cb

cb 2.6 156.1 S

1/4 3.4 155.3

¢ 4.2 154.5 S

1/4 6.5 152.2 cb

cb 7.3 151.4 1/4

S 8.7 150.0 ¢

0+50

1/4

S 13.7 145.0 cb

cb 13.2 145.5 N

1/4 10.9 147.8

¢ 7.2 151.5 N

1/4 4.7 154.0 +2

cb 3.8 154.9 cb

N 2.8 155.9 1/4

0+75

¢

N 12.0 146.7 1/4

T.P. 1316 145.51 cb

100

S

T 146.51

44

T 146.51

1.4 145.1

2.8 143.7

4.3 142.2

6.1 140.4

7.1 139.4

8.8 137.7

1400

11.9 134.6

10.3 136.2

9.0 137.5

7.5 139.0

6.4 140.1

4.9 141.6

3.2 143.3

142485

5.5 141.0

6.8 139.7

8.2 138.3

9.5 137.0

11.1 135.4

12.1 134.4

13.2 133.3

15.0 131.5

T 146.51

Section from 1424.85 on N.L. Linwood
to S.W. Cor Linwood & Chalmers. Section B on sketch
S.W. Cor Linwood is 1436.25 on S.L. Linwood

S	18.8	12.77	127.7
cb	16.3		130.2
1/4	14.9		131.6
1/2	12.5		134.0
1/4	10.8		135.7
cb	9.0		137.5
+8	6.9		139.6
N	5.5		141.0

B.M. (S.E.) Hub State & Chalmers 16.15 130.36
N.E. Correct 130.52

12-18-29 X-section Chalmers
g.c. Bliss State to Linwood - width,
Drebert curbs etc noted in Notes
Raney

ETp existing cb State & Chalmers - Page 10 this book	11.82	120.75	108.93
W Tp existing return State & Chalmers	13.84	120.74	106.90
		T 120.75	
SL State -			
W		13.4	107.3
+14 = cb		13.84	106.91
G		13.8	106.9
+16 = W cb Chalmers North of state <small>30' wide 7 1/2" x 4 1/2"</small>		13.3	107.4
1/4		12.7	108.0
1/2		12.6	108.1
1/4		12.4	108.3
cb		12.2	108.5
+6 = Gutter		12.0	108.7
Tp existing cb		11.82	108.93
E		9.7	111.0
SL State + 20 = 5' cb Line State			
E		6.5	114.2
+5		8.5	112.2
+20 = E cb Chalmers North of state		10.3	110.4
1/4		10.8	109.9
1/2		11.1	109.6
1/4		11.6	109.1
cb line Chalmers N of state		12.0	108.7

T 120.75

+30= W.L. Chalmers	12.1	108.6
30' Roadway on State		7/2' Roasters
5/4 State		
W	11.8	109.9
+30= cb	11.5	109.2
1/4	11.2	109.5
¢	9.9	110.8
1/4	8.3	112.4
cb	7.8	112.9
+15	7.1	113.6
E	5.1	115.6
¢ Roadway State		
E	2.6	118.1
+5	4.5	116.2
cb	5.4	115.3
1/4	7.1	113.6
¢	9.4	111.3
+3	10.7	110.0
1/4	11.0	109.7
cb	10.6	110.1
+15	10.6	110.1
W	10.6	110.1

T 120.75

46

N 1/4

	10.4	110.3
	9.9	110.8
	10.6	110.1
	10.1	110.6
	6.2	114.5
	4.3	116.4
	2.9	117.8
	0.20	120.55
	+ 11.48	
T 132.03		
	10.9	121.1
N cb State		123.0
	9.0	123.0
	12.6	119.4
	13.7	118.3
	16.5	115.5
	19.9	112.1
	19.7	112.3
	18.9	113.1
	20.8	111.2
	20.8	111.2
	21.3	110.7

132.03

N cb State + 20 = PC N.E Return

W	20.0	112.0
+16	20.3	111.7
+19	12.4	119.6
cb	13.8	118.2
1/4	13.8	118.2
£	11.7	120.3
1/4	9.6	122.4
cb	7.6	124.4
E	3.0	129.0
N.L. State = 0+00		
E	1.7	130.3
cb	6.2	125.8
1/4	8.5	123.5
£	9.8	122.2
1/4	11.4	120.6
cb	11.9	120.1
+11	11.5	120.5
+15	20.2	111.8
W	20.0	112.0

Note - Chalmers is 53' wide North of state with 3' cbs on West + 20' cbs on East. ^{30' Roadway} This same section was followed across intersection with exception of west property

132.03

0+1948

W = edge grading	6.7	125.3
cb	6.4	125.6
1/4	6.2	125.8
£	5.9	126.1
1/4	4.9	127.1
cb	3.7	128.3
+10	0.0	132.0
E	+2.4	134.4
0+38.95 = PC Curve on West		
E	+6.5	138.5
+10	+2.8	134.8
cb	0.3	131.7
1/4	1.6	130.4
£	2.3	129.7
1/4	2.6	129.4
cb	2.8	129.2
W	3.0	129.0
0+48.95 = PC Return on East		
W	1.6	130.4
cb	1.4	130.6
1/4	1.2	130.8
£	0.7	131.3
1/4	0.0	132.0
cb	+1.0	133.0
+10	+4.3	136.3

47

+15 +6.8 138.8

E +7.6 139.6

Section from 0756.17 E.L. to 0756.21

W.L. - See Plans for Improvement

E +11.0 143.0

+10 +7.9 139.9

cb +4.8 136.8

1/4 +3.6 135.6

¢ +2.8 134.8

1/4 +1.9 133.9

cb +1.2 133.2

+10 +0.5 132.5

+20 0.4 131.6

+25 1.6 130.4

W-SW Cor Linwood & Chalmers 4.4 127.6 127.6

Note - About 83' from S.W. Cor. Linwood &

Chalmers to S.E. Cor. Linwood & Chalmers

B.M. N.E. Hub State & Chalmers -1.70 130.33

Correct 130.33

12-18-29 Location N.W. Cor 10th &

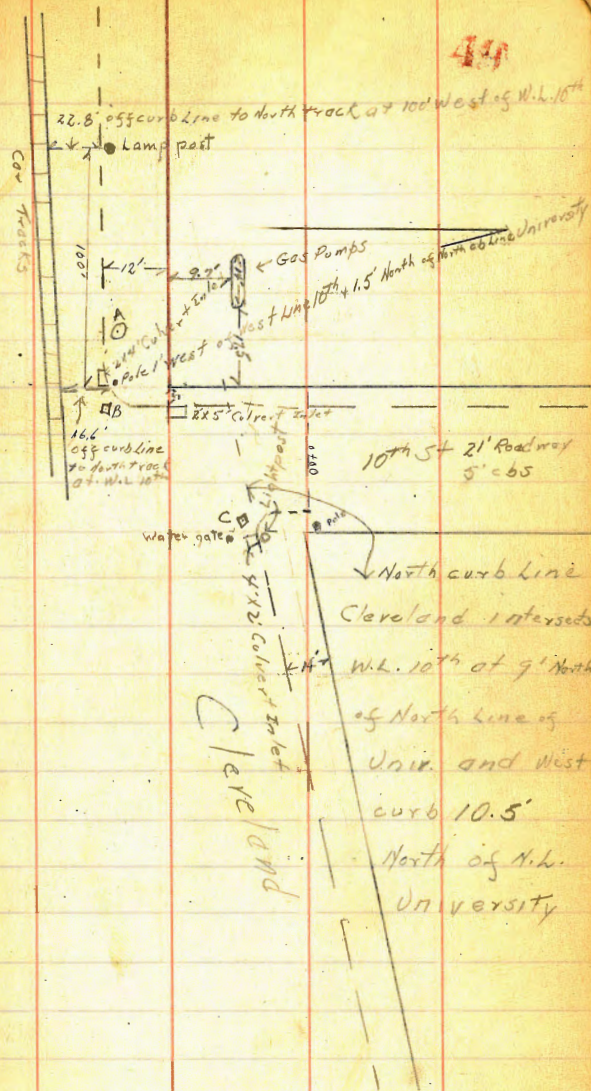
J. C. Bliss
Drebert University
Rauner

A = Telephone M.H. 11' West of West line 10th & 3' North of
North curb line University

B = Clean out M.H. 4' East of W.L. 10th & 1' South
North curb line University

C = Clean out M.H. on East Curb Line 10th & 1'
South North curb line Cleveland

University Ave



X-section 10th St. from North curb
 line University to 4' North of North Line of University
 31' wide 5' cbs 21' Roadway

B.M. S.W. B.P. 10th & University 282.02

+5.88

Σ 287.90

0+00 = North end of N.E. Return 10th & Cleveland

W Top cb 4.85

G 5.35

♀ 4.78

E Top return & paving flush 4.50

0+15 = ♀ Culvert Inlet N.E. Cor 10th & Cleveland

Flowline Inlet 5.73

Paving E.L. 10th 4.53

♀ 10th 4.85

West cb in driveway 5.49

0+33 = N.L. University

W Top cb 5.18

G - Flowline Culvert Inlet 6.54

♀ 4.80

E.L. 10th 4.60

0+44 = N cb Line University

E.L. 10th 4.69

♀ 4.90

W 2.10th Paving & return flush 5.28

Flowline Culvert Inlet 6.19

Σ 287.90

50

Levels along North side University

W.L. 10th = 0+00

Top North track 5.18 287.92

Flowline University Flowline Inlet 6.19 281.71

Top cb 5.28 287.62

0+25

N Top cb 5.22 287.68

G 6.02 281.88

Top North track 5.40 287.50

0+50

Top North track 5.43 281.47

G 5.90 287.0

N Top cb 5.12 282.78

0+75

N Top cb 4.96 287.94

G 5.84 287.06

Top North rail 5.37 281.53

1+00

Top North rail 5.31 287.59

G 5.76 287.14

N Top cb 4.98 287.92

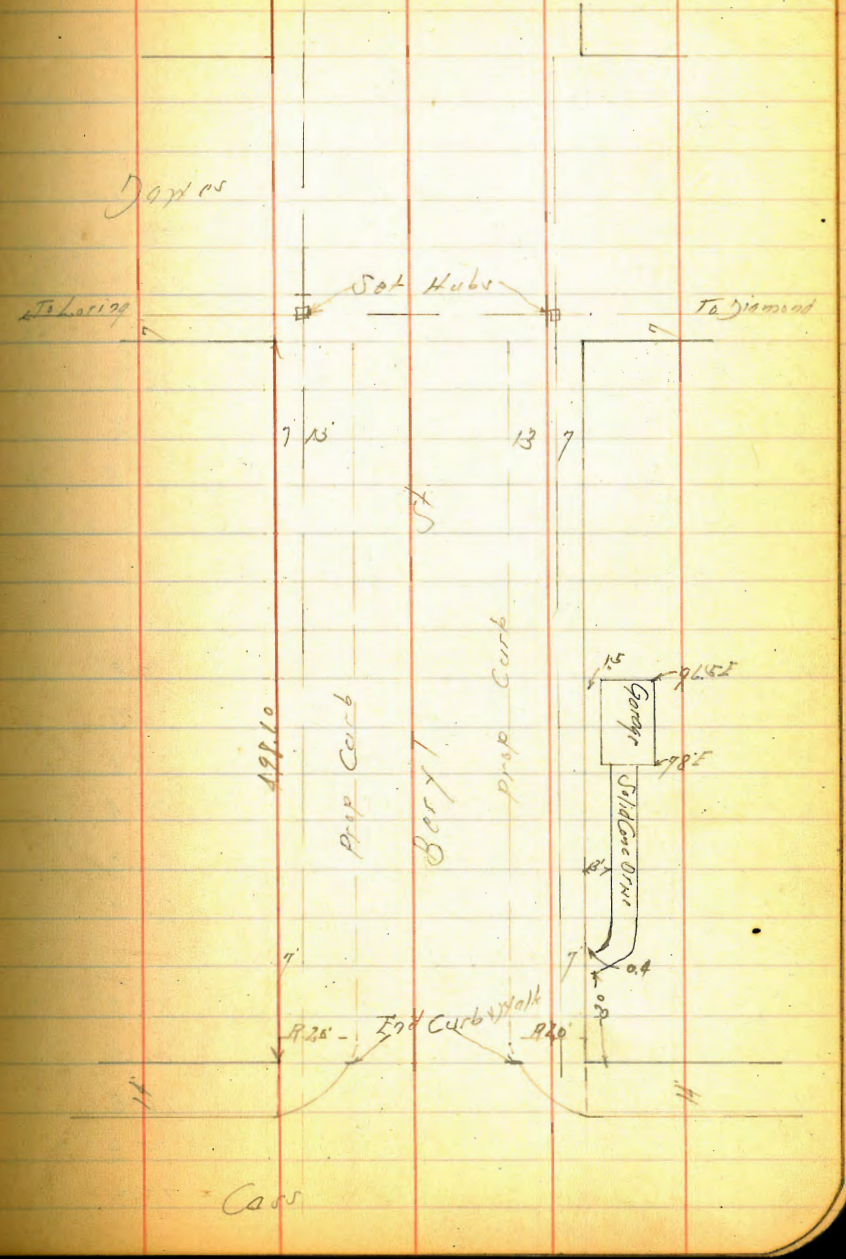
Bary St. Cross Section
 Cars to Jaynes
 old file
 11/20/97

80' wide
 28' Cb
 16' 9"

2-15-30
 Survey
 of Bary St
 51

BM	12.82	79.22	66.40	SW. BT Land & Cars
		East Curb of Cars		
S on Paving		7.71	71.81	
Cb " "		7.06	72.16	
" " "		6.89	72.34	
" " "		6.66	72.56	
" " "		6.49	72.73	
Cb " "		6.32	72.90	
" " "		5.92	73.30	
		E.L. Cars		
" "		4.9	74.3	
+192. End Existing Cb		5.48	73.74	
Gutter on Paving		6.06	72.16	
" " "		6.18	73.04	
" " "		6.32	72.90	
" " "		6.57	72.65	
Gutter " "		6.83	72.39	
Cb +1 = End Existing Cb		6.26	72.96	
S		4.3	72.9	
		10' E of E.L. Cars		
S		6.1	73.1	
Cb		6.1	73.1	
"		6.0	73.2	
"		5.8	73.4	
"		5.5	73.7	

Reduced & Plotted C&H
 Profile 2-18-30



Bony/Sk

7922

Cb	5.1	73.8	
7.6	3.4	75.8	
11	3.0	76.2	
25' F of Fh Coast			
11	3.1	76.1	
Cb	4.0	75.2	36' F
1/4	4.6	74.6	0.45 Conc. 11/4 Foot Solid Drive
2	4.9	74.3	51° 74.12
1/4	5.3	73.9	
Cb	5.6	73.6	
5	5.8	73.4	

50' F

-3 = Solid Conc Drive

	4.55	74.67	
5	5.1	74.1	740
Cb	4.8	74.4	732
1/4	4.6	74.6	747
2	4.1	75.1	752
1/4	3.8	75.4	754
Cb	3.4	75.8	758
11	3.5	76.7	760

75' F

11	1.9	77.3	
Cb	2.7	76.5	
1/4	3.2	76.0	
2	3.3	75.9	
1/4	3.9	75.3	

7922

52

Cb	4.2	75.0	
5	4.7	74.5	
+3 = Solid Conc Drive	4.51	74.66	
100' F			
5	4.4	74.8	746
Cb	3.6	75.6	752
1/4	3.3	75.9	759 117' F 3' 11/4 = 2 Ribbon Drive
2	2.7	76.5	769 1.08 78.14
1/4	2.7	76.5	766
Cb	2.3	76.9	767
11	1.4	77.8	
+0.2 = Conc Walk App'd	1.38	77.84	7787

125' F

11	1.0	78.2	
Cb	1.7	77.5	125' F 2' 11/4 1.2 Conc Walk App'd 0.78
1/4	2.2	77.0	78.44
2	2.3	76.9	
1/4	2.9	76.3	
Cb	3.1	76.1	
5	3.5	75.7	

150' F

5	3.1	76.1	763
Cb	2.7	76.5	767
1/4	2.4	76.8	762
2	1.8	77.4	774
1/4	1.7	77.5	775

Bery 151

79.22

cb		11	781		
N		0.6	784		
	175' E				
N		0.3	789	163' E 0.214 H.L. = 2.19160m drive	
cb		0.8	78.4	0.43 78.79	
1/4		1.3	77.9		
1/2		1.2	78.0		
1/4		1.7	77.5		
cb		1.8	77.4		
S		2.0	77.2		
	200' E				
S		1.3	77.9		
cb		1.4	77.8		
1/4		1.3	77.9		
1/2		0.8	78.4		
1/4		1.1	78.1		
cb		0.7	78.5		
N		0.3	78.9		
TP	1.05	0.75	78.47		
	225' E				
N		7.0	79.5		
cb		7.5	79.0		
1/4		7.9	78.6		
1/2		7.7	78.7		
1/4		8.0	78.5		
cb		8.0	78.5		

86.52

53

		8.1	78.4		
		2.50' E			
		7.7	78.8		
		7.2	79.3		
		7.6	79.3		
		7.0	79.5		
		7.3	79.2		
		6.7	79.8		
		6.3	80.2		
		2.75' E			
		5.8	80.7		
		6.1	80.4		
		6.2	80.3		
		6.7	79.8		
		6.5	80.0		
		6.9	79.6		
		7.3	79.2		
		300' E			
		7.0	79.5		
		6.2	80.3		
		6.5	80.0		
		6.0	80.5		
		6.2	80.3		
		6.6	79.9		
		5.7	81.4		
		325' E			

8152

N	1.5		82.0
Cb	5.2		81.3
1/4	5.7		80.8
1/2	5.6		80.9
1/4	6.1		80.4
Cb	6.1		80.4
S	6.5		80.0

350' F

S	6.1	80.4	80.4
Cb	5.7	81.2	80.8
1/4	5.5	81.2	81.0
1/2	5.0	81.5	81.5
1/4	5.2	81.3	81.3
Cb	4.7	81.8	81.8
N	3.8	82.7	82.7

37.5' F

N	3.5		83.0
Cb	4.1		82.4
1/4	4.8		81.7
1/2	4.6		81.9
1/4	5.0		81.5
Cb	5.0		81.5
S	5.6		80.9

400' F

S	5.3	81.9	81.2
Cb	4.4	82.0	82.1

8652

54

1/4	4.4	82.0	82.1
1/2	4.1	82.5	82.4
1/4	4.0	82.8	82.5
Cb	3.2	83.4	83.3
N	2.7	83.7	83.8

425' F

N	2.4		84.1
Cb	2.9		83.6
1/4	3.7		82.8
1/2	3.6		82.9
1/4	4.0		82.5
Cb	4.0		82.5
S	4.9		81.7

450' F

S	4.7	81.8	81.8
Cb	4.7	82.5	82.8
1/4	3.7	82.9	82.8
1/2	3.2	83.2	83.3
1/4	3.2	83.3	83.3
Cb	2.5	83.7	84.0
N	1.8	84.6	84.7

475' F

N	1.1		85.4
Cb	2.2		84.3
1/4	2.9		83.6
1/2	3.0		83.5

Berry/Dr

81.52

1/4			35		830	cb
cb			36		829	H
S			41		824	
TP	740	90.81	311	83.41	^{DAMES} ^{80% of} ^{20% cb} ^{10% H}	H
						cb
S			85	823	823	1/4
cb			76	834	832	1/2
1/4			76	832	832	1/4
S			71	837	837	cb
1/4			68	841	840	S
cb			61	848	847	
H			51	857	857	S
						cb
						1/4
						1/2
						1/4
						cb
						H
						H
						cb
						1/4
						1/2
						1/4
						cb
						S

498.62 = H.L. DAMES

H cb of DAMES

H 1/4 of DAMES

90.81

55

						6.0
						4.8
						4.3
						4.3
						5.7
						6.3
						6.7
						7.2
						7.6
						8.1
						8.3
						7.8
						7.3
						6.6
						6.1
						5.5
						4.5
						3.7
						5.2
						6.0
						6.4
						7.2
						7.4
						7.5

1/4 DAMES

F cb of DAMES

Beryl St.

90.81

F L of JAMES

v			72	
cb			71	
1/4			68	
1/2			61	
1/4			58	
cb			49	
H			35	
TP	0.30	78.61	12.50	78.31
TP			12.20	66.11

8M DWB

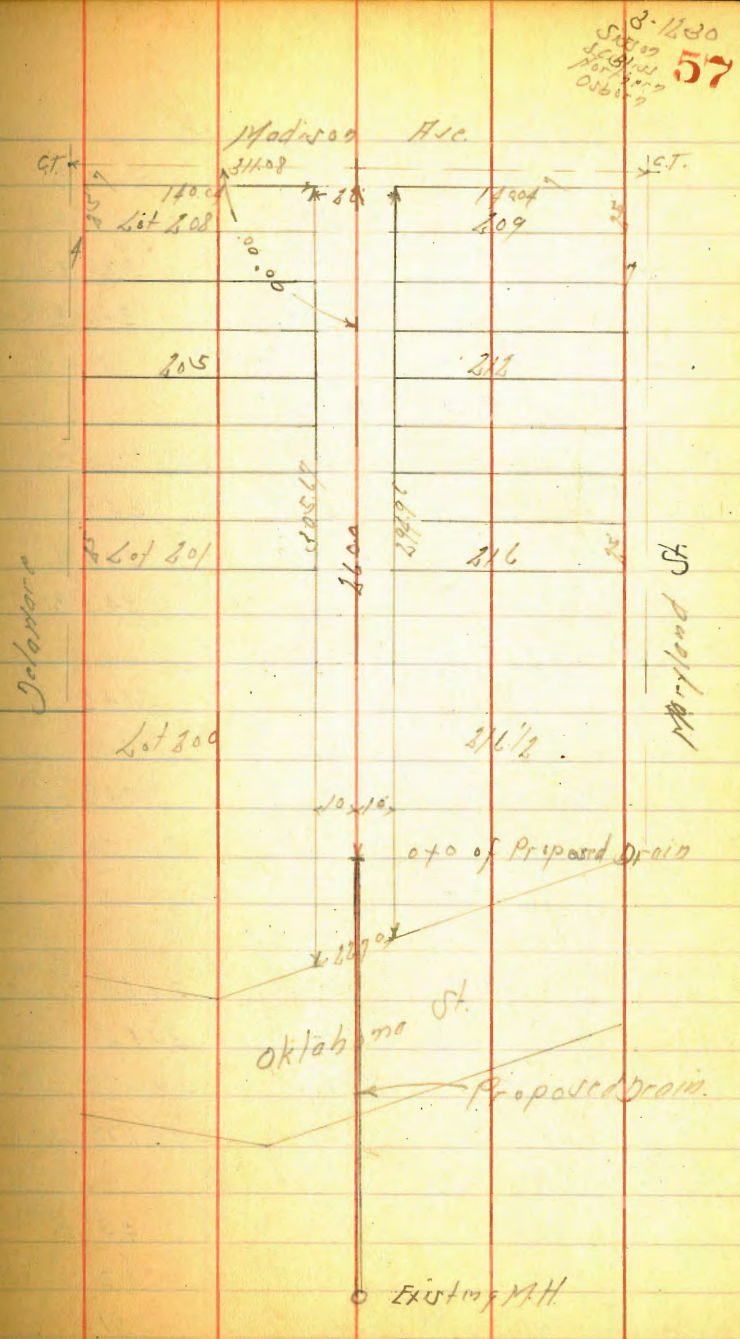
last 100

66.40

56

Cross Section
 Alley between Delaware & Maryland
 South of Madison Ave 20' wide

BM	568	352.66	346.98	SW. BP Madison Maryland
S. cb of Madison				
M on Pavng		785	344.81	
L " "		770	344.96	
F " "		759	344.07	
S.L. Madison				
TP	420	350.08	678	345.88
F on Pavng		427	345.81	
= Top Cbt Ground				
L on Pavng		462	345.46	
M on Pavng		445	345.63	
= Cbt Ground				
25' S of S of S.L. Madison				
M		41	345.6	
L		42	345.0	
F		39	346.2	
56' S of S.L. Madison				
-3.8	M/H of Do Garage	409	345.99	✓
Copt. Floor				
F		44	345.7	73' S of of Do Garage
L		44	345.7	3.5' E of E.L.
M		45	345.6	41°
81' S Plotted - 3-13-30 C.B.H.				
-2.0	M/H of Do Garage	46	345.5	✓
Dirt Floor				
M		46	345.5	
L		47	345.4	
F		46	345.5	
40.7	L Garage Dirt Floor	46	345.5	



3-12-30
 Station
 57

100'S

F		48	3453
L		47	3454
H		48	3453
+1.9 = Sty of Dr Garage		48	3453 ✓
	Dir. Floor		

110'S

-2.5 = 1/2 Garage Conc. Floor		498	34510 ✓
H		50	3451
L		48	3453
F		48	3453

134'S

F		52	3449
L		52	344.9
H		53	344.8
+2 = 1/4 of Dr. Garage		534	344.74
	Con of floor		536

160'S

H		57	344.4
L		56	344.5
+9.6 = Edge Conc. Apron		560	344.48
F 10.9 = 1/2 Garage Conc Floor		530	344.78

179'S

F		61	344.0
L		59	344.2
H = Edge Conc. Apron		627	353.71

+1.0 = 1/4 of Dr Garage Conc Floor

612	343.95
-----	--------

198'S

-1.0 = Sty of Dr Garage		622	343.86
H = Edge Conc. Apron		656	343.42
L		67	343.4
F		68	343.3

209'S = N.H.
2 Alley on Run
716 = 342.88

212'S

F		74	342.7
L		71	343.0
H		71	343.0
+7.0 = 1/2 Garage Conc Floor		715	342.93 ✓

225'S

H		82	341.9
L		78	342.9
F		75	342.6

250'S

F		96	340.5
L		99	340.2
H		103	339.8
TP		1145	338.63

158 340.21

275'S

H		30	337.2
L		28	337.4
F		27	337.5

280'S

340.81

Proposed Drain

1-9-30
59

F		40	3362					
L		3.3	3369	BM	1.78	34876	346.98	
H		8.5	3367			0+0-26.5 of SL Madison & Alley		
	2855							
H		43	3360			10.5 of L	9.0	339.7
L		62	3340			L	9.5	339.2
F		62	3340			10.11 of L	10.0	338.7
	19496 ⁵ : 112. Oklahoma or F						0+18	
F		9.5	3307			10.11	11.9	336.8
L		9.4	3308			L	11.4	337.3
H		8.0	332.2			10.5	13.2	336.5
	291.96 5-22 305.67 on H = 112. Oklahoma or F					TP	2.56	338.62
							12.70	336.06
							0+30	
H		11.7	328.5			10.5	6.0	332.6
L		11.7	328.5			L	6.5	332.1
F		9.5	3307			10.11	4.1	334.5
TP	10.10	34980	0.51	33970			0+17	
BM		284	34696	J.M.B.P. Madison Maryland 346.98		10.11	11.0	327.6
						L	13.0	325.6
						10.5	13.8	324.8
						TP	0.54	326.42
							12.74	325.88
							0+60	
						10.5	9.8	318.6
						L	7.9	318.5
						10.11	5.1	319.3
							0+75	
						10.11	12.6	313.8

See Sketch Page 57

J.M.B.P.
Madison
Maryland

322.42

TP	0.12	313.44	13.10	313.32
♂			2.7	310.7
10'E			2.6	310.8

0.190

10'E			9.8	303.6
♂			10.4	303.0
10'N			7.6	305.8

TP	0.55	300.92	13.07	300.37
----	------	--------	-------	--------

1.105

10'N			4.9	296.0
♂			5.9	295.0
10'E			5.5	295.4

1.115

10'E - Bottom Gulch			12.0	288.9
♂			13.7	287.2
10'N			10.1	290.8

1.120 = 10'N

1.195 = 10'N

1.127

10'N = Bottom of Gulch			14.8	286.1
♂			11.0	289.9
10'E			6.7	293.2

60' wide
10' ebs
10' 443

Sigsbee STA Sec

Logan to National

7-16-30

Muller

J. S. Bliss

Kanagay

N. S. Sigsbee
& National

32.71
0775 S

61

OK
23.94

B.M. B.P.

8.77

32.71

23.94

W. ent. el.

5.61

27.10

00 = S. line Logan Ave

gutter

6.6

26.1

E. ent. el

3.30

29.41

"4

6.1

26.6

gutter parmt

3.30

29.41

⊕

5.7

27.0

"4

3.68

29.03

"4

5.6

27.1

⊕

3.80

28.91

gutter

5.5

27.2

"4

4.03

28.68

E. ent. el.

4.65

28.06

gutter parmt & W. ent. el

4.20

28.51

1+00-S

0+25 S

E. ent. el

5.09

27.62

W. ent. el

4.65

28.06

gutter

5.9

26.8

gutter

5.7

27.0

"4

6.0

26.7

"4

5.3

27.4

⊕

6.0

26.7

⊕

5.0

27.7

"4

6.4

26.3

"4

4.8

27.9

gutter

6.9

25.8

gutter

4.6

28.1

E. ent. el

6.06

26.65

E. ent. el

3.79

28.92

1+25 S

0+50 S

W. ent. el

6.52

26.19

E. ent. el

4.20

28.51

gutter

7.4

25.3

gutter

5.1

27.6

"4

6.8

25.9

"4

5.2

27.5

⊕

6.4

26.3

⊕

5.4

27.3

"4

6.4

26.3

"4

5.8

26.9

gutter

6.3

26.4

gutter

6.0

26.7

E. ent. el

5.57

27.14

W. ent. el

5.17

27.54

Notes Reduced by K.P. Brown
Plotted 7-26-30
C.B.H.

	32.71		
1 + 38 ³⁰ = Alley Return on E. 2. out of Place			
E. line amt el Return + dirt	5.61	27.10	
E. amt el	5.82	26.89	
gutter	6.3	26.4	
N.B. New Alley Return to be constructed 1 + 40 ³⁰ = N. Line Alley			
S. Line	5.5	27.2	
S. el line	6.3	26.4	
"	6.6	26.1	
♀	6.7	26.0	
"	7.0	25.7	
gutter	7.6	25.1	
W. amt. el	6.82	25.89	
W. line amt el. return N.G.	6.60	26.11	
W " E. End Alley Pavmt.	6.87	25.84	
N.B. - New Alley Return to be constructed 1 + 50 ³ = ♀ Alley			
W. 75 on E. End Alley Pavmt.	7.25	25.46	
el	7.3	25.6	
"	7.8	24.9	
"	7.2	25.5	
♀ on Alley	6.9	25.8	
"	6.8	25.9	
el	6.4	26.3	
E	5.9	26.8	
1 + 60 ³ = S. Line Alley			
E. dirt + E. edge 3' amt. walk	5.88	26.83	
+ 5. on E. End Alley curb Return	6.04	26.67	
E. amt. el	6.21	26.50	

N.B. New Alley Ret. to be constructed from E. line to E.W.

	32.71	5.95	24.75
gutter		6.7	26.0
"		7.1	25.6
♀		7.1	25.6
"		7.4	25.3
gutter		8.0	24.7
W. amt. el.		7.20	25.51
+ 2.5' E. edge amt walk		7.09	25.62
W. on Alley Pavmt. + el. ret N.G.		6.92	25.79
N.B. 7.5 of New Alley Return to be constructed			
		2 + 00	
W. amt. el.		7.91	24.80
gutter		8.6	24.1
"		8.2	24.5
♀		7.9	24.8
"		7.8	24.9
gutter		8.0	24.7
E. amt. el.		6.92	25.79
		2 + 25	
E. amt. el.		7.40	25.31
gutter		8.3	24.4
"		8.3	24.4
♀		8.3	24.4
"		8.7	24.0
gutter		9.1	23.6
W. amt. el.		8.35	24.36

32.71

2+50

W. cnt. cl.	8.82	23.89
gutter	9.4	23.3
"	9.2	23.5
⊕	8.8	23.9
"	8.9	23.8
gutter	8.6	24.1
E. cnt. cl.	7.86	24.85

2+75

self-drive gutter	8.89	23.82
"	9.2	23.5
⊕	9.4	23.3
"	9.6	23.1
gutter	9.6	23.1
W. cnt. cl.	9.29	23.42

3+00 60 = N. Lin - National Ave

W. cnt. cl.	9.74	22.97
gutter pavmt.	10.17	22.60
"	9.84	22.87
⊕	9.64	23.07
"	9.49	23.18
gutter	9.47	23.20
E. cnt. cl.	8.75	23.96
chk B.M. B.P. N.W. Sigsbee + Logan	4.36	28.35

Sigsbee St & See

63

366.59

100'N

F	3.5	363.1
S	3.8	362.8
N	3.5	363.1

119'N

N	3.6	363.0
S	3.6	363.0
E	3.3	363.3

++ Conc Mark 118' Nide	3.33	363.26
------------------------	------	--------

TP 5.62 368.93 3.28	3.28	363.31
---------------------	------	--------

150'N

F	5.2	363.7
S	5.5	363.4
N	5.5	363.4

175'N

N	5.5	363.4
S	5.6	363.3
E	5.5	363.4

200'N

F	5.4	363.5
S	5.7	363.2
N	5.4	363.5

225'N

N	5.3	363.6
S	5.3	363.6
F	5.3	363.6

368.93

250'N

F	4.7	364.2
S	4.8	364.1
N	4.7	364.2

275'N

N 84' Front 0.312 Alley	4.8	364.1
S	5.0	363.9
E	4.9	364.0

300'N

F	4.8	364.1
S	4.9	364.0
N 84' Front 0.312 Alley	4.7	364.2

325'N

N " " "	5.0	363.9
S	5.0	363.9
E	5.0	363.9

350'N

F	4.8	364.7
S	4.5	364.4
N Front 0.510 Alley	4.6	364.3

375'N

N Front 0.610 Alley	4.1	364.8
S	4.6	364.9
E	3.6	365.3

400'N

F	4.9	364.0
---	-----	-------

65

368.93

L	Box Cont.	4.9	364.0
H	Fence 0.812 H/lay	4.8	364.1
	425'		
H	Fence at	4.6	364.3
L		4.6	364.3
L		4.7	364.2
	450'		
-4.8	-H End Do Garage	4.25	364.68
L		4.8	364.1
L		4.7	364.2
H	End Concrete	4.3	364.6
H	Fence at 12 H/lay		
	475'		
H		4.8	364.1
L		4.9	364.1
L		5.1	363.8
	500'		
L		5.0	363.9
L		4.6	364.3
H		4.5	364.4
	525'		
H		4.7	364.2
L		4.7	364.2
L		4.6	364.3
TP	3.88 368.18	4.63	364.30
	550'		
L		3.9	364.3

368.18

66

L		3.9	364.3
H		3.6	364.6
	575'		
H		3.9	364.3
L		3.8	364.4
L		3.9	364.3
	592'		
L		3.3	364.9
L		3.5	364.7
H		3.6	364.6
	600'		
H		4.1	364.1
L		4.0	364.2
L		3.2	365.0
	607.2' = 5.2 E/Cajon		
L	Top cb	4.58	363.60
L	Gutter at Parap	4.76	363.42
L	" "	5.21	362.97
H	Gutter " "	4.97	363.21
H	Top cb	4.71	363.47
	627.2' = S cb of E/Cajon Br		
H	07 Par	5.35	362.83
L	" "	5.39	362.79
L	" "	5.36	362.82
BM		4.61	363.57

SM BP.
E/Cajon
Van Dyke
363.56

391.59

391.6

N	45	387.1
S	50	386.6
S	48	386.8
	125 E = H.L. H.V.S. Alley	
S	50	386.6
S	50	386.6
H	47	386.9
	132.5 E = L.H. Alley	
H	46	387.0
S	= Service M.H. on Firm 488	386.71
S	48	386.8
	140 E = E.L. of H.V.S. Alley	
S	48	386.8
S	46	387.0
H	40	387.6
	170 E	
H	42	387.4
S	44	387.2
S	46	387.0
	200 E	
S	44	387.2
S	43	387.3
H	41	387.5
	225 E	
H	39	387.7

391.59

68

S	42	387.4	
S	40	387.6	
	260 E		
S	50	386.6	
S	50	386.6	
H	48	386.8	
	265 E = H.L. Bancroft		
H	Top Cb	5.25	386.34
H	on Paving	5.34	386.25
S	" "	5.61	385.98
S	" "	5.45	386.14
S	Top Cb	5.35	386.24
	H db of Bancroft		
S	on Paving	6.20	385.39
S	" "	6.16	385.43
H	" "	6.10	385.49

North & South Alley Block (3) Normal H.H.
 From E.H. Alley to S.L. Collier
 Between 32nd & Bancroft

391.59

69

391.59 8' Ford 391.6

H.L. of E.H. Alley

47 386.9

46 387.0

41 387.5

50' H of H.L. of E.H. Alley

39 387.7

41 387.5

35 388.1

100' H

33 388.3

38 387.8

37 387.9

125' H

34 388.2

36 388.0

36 388.0

150' H

H Fence 0.510 Alley 2.0 389.6

2.6 389.0

2.2 389.4

200' H

1.9 389.7

2.4 389.2

H Fence 0.210 Alley 2.3 389.3

250' H

H Fence 0.410 Alley 2.0 389.6

1.9 389.7

2.1 389.5

TP 594 396.49 1.04 390.55

300' H

F 6.0 390.5

6.2 390.3

H Fence 0.510 Alley 6.0 390.5

350' H

H Fence 0.910 Alley 6.0 390.5

6.4 390.1

6.2 390.3

400' H

F 5.7 390.8

5.9 390.6

H 5.7 390.8

450' H

H 5.1 391.4

5.2 391.3

F 5.3 391.2

475' H

F 4.5 392.0

5.1 391.4

H 4.6 391.9

500' H

H 4.1 392.4

Plotted 9-17-30 C.B.H.

106' H
 390.90
 1.5' H of H.L.
 Case Floor
 331
 388.28

396.49

L	41	392.4
F	42	392.3

525M

F	46	391.9
L	45	392.0
H	45	392.0

540M

H	45	392.0
L	50	391.5
F	48	391.7

548M

F	52	391.3
L	59	390.6
H	50	391.5

550.6M - 5L Collier

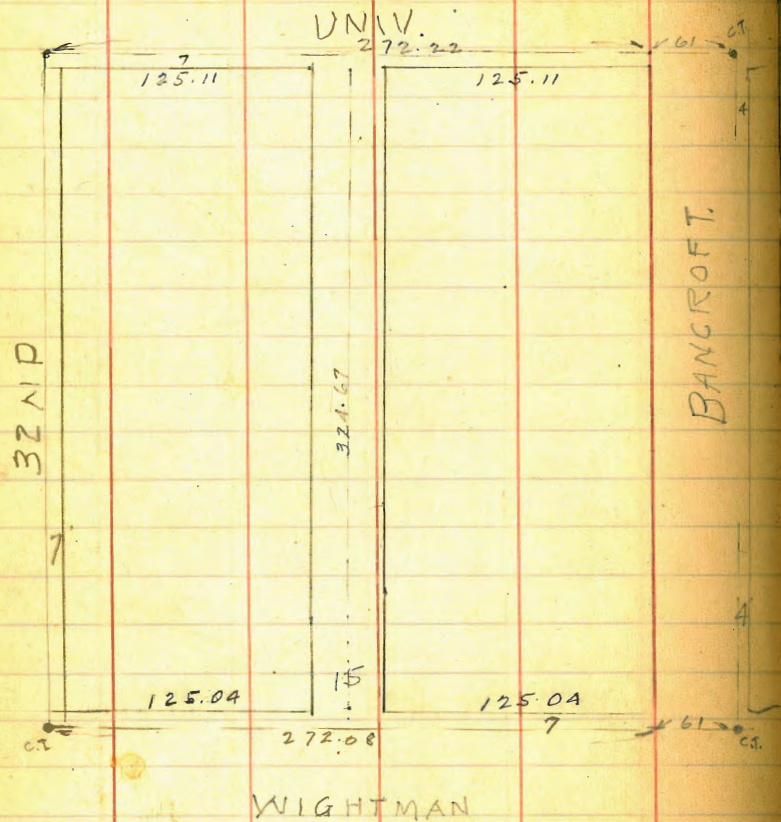
H	Top Cb	585	390.64
H	on Paving	599	390.50
L	" "	629	390.20
F	" "	612	390.37
F	Top Cb	600	390.49

5 ch of Collier

F	on Paving	660	389.89
L	" "	660	389.89
H	" "	651	389.98
BM		558	390.91

 HFBP
 Collier M. 1/2
 390.88

70



2/3/01
London

X sec Alley B1K ~~48~~ ⁴⁴ Park Villas.

71
SW Wightman
= 32nd

B M 475 351.15 346.40

0+10 = N cb Wightman

WL	top cb	5.11	346.04
WL	gut	5.57	345.58
±		5.59	345.56
EL	gut	5.56	345.59
EL	top cb	5.19	345.96

0+00 = NL Wightman

EL	top cb	4.94	346.21
EL	pan	5.16	345.99
±	pan	5.27	345.88
WL	pan	5.18	345.97
WL	cb	4.84	346.31

0+15

WL		4.2	347.0
+3		4.0	347.2
+6		4.3	346.9
±		4.1	347.1
E.L.		3.8	347.4

0+35

EL		4.1	347.1
+4		4.0	347.2
±		3.8	347.4
+2		3.8	347.4
+6		3.9	347.3
WL		4.2	347.0

Plotted by J.R. 2-7-01

351.15

0+60

W.L.	4.0	347.2
+4	3.6	347.6
±	3.7	347.5
+5	4.0	347.2
E.L.	4.1	347.1

0+80

E.L.	3.7	347.5
+5	3.8	347.4
±	3.6	347.6
+5	3.4	347.8
W.L.	3.7	347.5

1+00

W.L.	3.3	347.9
±	3.2	348.0
+4	3.1	348.1
E.L.	3.4	347.8

1+25

E.L.	3.3	347.9
+5	3.0	348.2
±	3.0	348.2
W.L.	3.3	347.9

1+45

351.15

72

W.L.	3.0	348.2	
+4	3.1	348.1	
±	3.0	348.2	
+5	2.7	348.5	
E.L.	3.0	348.2	
T.P. 612	354.24	3.03	348.12
Step 3 rd W at 1+50	5.04	349.20	

1+65

E.L.	5.6	348.6		
+2	5.5	348.7		
±	5.5	348.7		
+2	5.6	348.6		
W.L.	5.6	348.6		
± single garage at 1+66	4.3	W. Conc. floor	5.10	349.14

1+82

W.L.	5.3	348.9
+5	5.6	348.6
±	5.6	348.6
E.L.	5.6	348.6
7'E & Sing garage concrete floor	5.33	348.91
Door at 1+95 2' W.	3.72	350.52

2+00

E.L.	5.1	349.1
+3	5.3	348.9
±	5.2	349.0
+2	5.0	349.2
W.L.	5.0	349.2

354.24

⊕ garage at ^{conc floor} 2+06 1'W	4.77	349.47
⊕ garage at ^{conc floor} 2+17 4.2'W	4.26	349.98
2+25		
WL	4.5	349.7
+3	4.7	349.5
⊕	5.0	349.2
E.L.	5.0	349.2
⊕ garage at 2+28 ^{conc floor} 4.2'W	4.27	349.97
⊕ garage at 2+43 ^{conc floor} 4.2'W	3.78	350.46
2+50		
E.L.	4.8	349.4
+4	4.8	349.4
⊕	4.6	349.6
WL	4.0	350.2
⊕ garage at 2+53 ^{conc floor} 4.2'W	3.75	350.49
2+75		
WL	4.3	349.9
+4	4.5	349.7
⊕	4.8	349.4
+5	4.8	349.4
EL	4.9	349.3
NH on ⊕ at 2+99 (top)	4.82	349.42

73

354.24

3+00		
EL	4.9	349.3
+3	5.4	348.8
⊕	4.9	349.3
+3	5.0	349.2
WL	4.0	350.2
3+12		
WL	4.7	349.5
+4	5.3	348.9
+5	6.1	348.1
⊕	5.8	348.4
+3	6.1	348.1
EL	5.4	348.8
3+20		
EL	6.5	347.7
+3	7.2	347.0
⊕	7.2	347.0
+5	7.2	347.0
+7	6.6	347.6
WL	5.1	349.1
3+24 62		
WL - Ob	6.95	347.29
WL Pav	7.39	346.85
⊕ Pav	8.06	346.18
EL Pav	8.05	346.19
EL Ob	8.05	346.18

Alley Bill 48 Park Villas.

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354.24

3+3867 = Seb Univ.

EL	eb		8.32	345.92
EL	put		8.76	345.48
			8.22	346.02
W.L	put		7.61	346.63
WL	eb		7.11	347.13
T.P.	10.59	356.74	8.09	346.15
B.M			10.35	346.39

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9-22-39

Miller
Wood Run
Blaine

Resub. BIKs. K+L Teralta See Page 64.

Indexed
c.s.K.

RM.	5.67	366.70	361.03
		N. of Orange	
E - 25' gutter		5.82	360.88
E, gutter		5.71	360.99
E ch		5.51	361.19
⊕ pay.		5.79	360.91
W. gutter		5.69	361.02
W ch.		5.32	361.38
+25.		5.65	361.05

0+00 = N. line Orange

W on ch	N. End	5.24	361.46
+0.1	Face of ch. s. end. Stucco wall 0.1' in Alley.		
+0.1	pay. " "	5.36	361.34
⊕	" " "	5.60	361.10
E	" " "	5.39	361.32
E ch	" " "	5.35	361.35

0+0.5

E		4.8	361.9
⊕		5.0	361.7
W		4.7	362.0

0+14 = N. End above wall S. End. Fence 0.1' in Alley.
0+14 - 7.4 W of ⊕ = Elec. Co. Guy wire Dead Man.

0+30

W Fence 0.1 in Alley		3.8	362.9
6.6' W of ⊕ = W. side Elec Pole.			
⊕		4.0	362.7
E		4.1	362.6

366.70

0+50

E		3.5	363.2
⊕		3.7	363.0
W Fence 0.1 in Alley.		3.6	363.1
		0+75	
W Fence 0.1 in Alley.		3.7	363.0
⊕		3.4	363.3
E		3.5	363.2
		1+00	
E		3.3	363.4
⊕		3.3	363.4
W N. End. Fence on W. side of Alley.		3.3	363.4
		1+19	
W		3.1	363.6
⊕		3.1	363.6
E		3.2	363.4
+4	W. End. 18' conc. walk.	3.38	363.32
— T.P. — 5.36 — 368.88 — 3.18 — 363.52 —			
1+53	S. End. conc. apron front of 3 garages on W.		
E		5.3	363.6
⊕		5.5	363.4
W		5.4	363.5
+2.2	= S. E. Cor. apron	5.29	363.69
		1+57	
W - 4.2 = floor.		5.09	363.79

75

36888

1+95 = N. End above garage on W

W-10. N of Garage	5.5	363.4
W-4.2 = floor	5.05	363.83
W-2.2 = apron.	5.23	363.65
	2+00	
-10 W	5.7	363.2
	5.0	363.9
+0.9 = W. edge Elec. Pole		
⊕	5.2	363.7
⊖	5.2	363.7
+1.8 = W. end 36" conc. walk, 5.10	5.10	361.78
	2+25	
-5	5.1	363.8
⊖	5.3	363.6
⊕	5.3	363.6
W	5.2	363.7
+20.	6.0	362.9
+35. Drains. to W.	6.1	362.8
	2+50	
W-10	4.8	364.1
W	4.8	364.1
⊕	5.0	363.9
⊖	4.7	364.2
	2+75	
⊖	4.7	364.2
⊕	4.9	364.0
W.	5.0	363.9

36888

3+00

W Fence on line	4.4	364.3
⊕	4.9	364.0
⊖	4.8	364.1
	3+25	
⊖	4.7	364.2
⊕	4.8	364.1
+7.2 Fence	4.7	364.2
+5	4.8	364.1
3+34 - 6.5 W of ⊕ = W. side Elec. Pole.	3+50	
-5	4.6	364.3
W	4.5	364.4
+0.5 Fence.	4.5	364.4
⊕	4.4	364.5
⊖	4.1	364.8
+5	4.1	364.8
	3+75	
-5	4.3	364.6
⊖	4.0	364.9
⊕	4.2	364.7
+7.0 = Fence	4.0	364.9
W +5.	4.4	364.5
	4+00 = S. End. ex Conc. pav.	
0.25 E. of W. = W. edge pav.	4.62	364.26
⊕	4.77	364.11
⊖ = E. edge pav	4.37	364.51
T.P.	4.92	366.16
orig B.M.	5.13	361.03

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DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

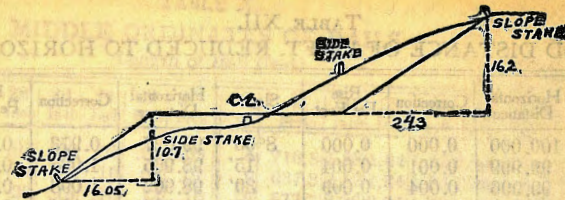
Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body

of table in same row and column gives distance from side stake to slope stake. If ground is not nearly level, the side stake and slope stake, lower stake by this amount if cut, higher if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point and line of sight should cut target.

IMPROVED TABLES
AND
INFORMATION

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given L may be found by dividing tangent (or external), opposite L by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

120
114
230
45

12
85
52
28

84.2
39.1

107
58
49

27°57'
25°52'
210.14
75°03'

42.66
21°14'
25.52'
120.56'

74°03'
47.06
27°57'
1305.8'

97.06
0.29
97.35
13.08
84.27

8521

97.35
9.90
87.45

90.43
1.94
88.49

102.61
12.00
90.61

97.35
9.91
87.44

97.35
9.91
87.44

10.3

405.4

210
80
320

ENGINEERING DEPARTMENT
CITY OF
SAN DIEGO,
CALIFORNIA.