

1369

Murray Cañon

ENGINEERING DEPARTMENT,  
CITY OF SAN DIEGO,  
CALIFORNIA.

MICROFILMED

DEC 23 1964

Our Leather Bound Engineers Note Books are carried in the following rulings:

- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
- No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.
- No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.
- No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

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**THE FREDERICK POST CO.**

*ENGINEERING and DRAFTING SUPPLIES*

IRVING PARK STATION

CHICAGO, ILL.

X-Section New Alignment Murrumbidgee Canyon  
 Road from Sta. 16+96<sup>04</sup> B.C. - Sta.  
 47+18<sup>27</sup> B.C. See F.P. 1335, pg. 40

Sta	+	H.I.	-	Elev.
B.M. Nail on Pole, opp. Sta. 32+35				24.99
	3.26	28.25		
T.P.			3.53	24.72
	11.41	36.13		
T.P.			0.15	35.98
	12.00	47.98		
T.P.			4.34	43.64
	0.46	44.10		
T.P.			3.44	40.66
	6.61	47.27		
T.P.			3.17	44.10
	10.42	54.52	✓	
30-L	16+96 <sup>04</sup> B.C.		7.9	46.6
15-L			8.1	46.4
9-L			9.4	45.1
♠			9.3	45.2
28-R Fence			9.4	45.1
	17+50			
30-R			11.6	42.9
19-R			9.0	45.5
♠			9.2	45.3
9-L			9.4	45.1
19-L			6.6	47.9

Jacq. } Oct. 14<sup>th</sup> 1929.  
 Clare }  
 Morgan }

Sta	+	H.I.	-	Elev.
30-L			4.2	50.3
	18+00			
30-L			2.7	51.8
28-L			3.7	50.8
23-L			5.2	49.3
17-L			6.0	48.5
15-L			7.3	47.2
7-L			9.1	45.4
♠			9.2	45.3
20-R			9.5	45.0
22-R			11.5	43.0
30-R			11.7	42.8
	18+50			
30-R			11.5	43.0
21-R			9.0	45.5
♠			9.1	45.4
3-L			9.1	45.4
10-L			6.1	48.4
20-L			5.6	48.9
30-L			3.8	50.7
	19+00			
30-L			2.3	52.2
21-L			3.5	51.0
♠			8.8	45.7
30-R			9.7	44.8

STA	+	H.I.	-	Elev.	STAB	+	H.I.	-	Elev. <sup>2</sup>
	19+50					21+50			
30-R			9.4	45.1	30-R			11.1	50.1
9-R			8.9	45.6	26-R			9.9	51.3
☐			6.5	48.0	22-R			12.2	49.0
T.P. B.M. Nail on Top of Post in Front of Silo			5.47	49.05	☐			6.4	54.8
	12.12	67.17 ✓			30-L			0.0	61.2
23-L			6.3	54.9	T.P.			0.87	60.30
30-L			5.1	56.1				11.85	72.15 ✓
	20+00								22+00
30-L			3.0	58.2	30-L			8.2	64.0
☐			8.7	52.5	☐			12.5	59.7
10-R			11.5	49.7	30-B			19.4	52.8
15-R			15.0	46.2					22+50
30-R			15.7	45.5	30-R			13.7	58.5
	20+50				25-R			10.8	61.4
30-R			15.8	45.4	☐			8.4	63.8
25-R			15.8	45.4	30-L			5.9	66.3
☐			7.3	53.9					23+00
18-L			3.7	57.5	30-L			+0.4	72.6
30-L			1.7	59.5	☐			4.6	67.6
	21+00				30-R			8.5	63.7
30-L			0.7	60.5					23+50
☐			6.7	54.5	30-R			5.3	66.9
13-B			10.3	50.9	25-R			3.5	68.7
30-B			12.7	48.5	T.P.			0.26	71.89 ✓

STA	+	H.I.	-	Elev.	STA	+	H.I.	-	Elev. <sup>3</sup>
	12.00	84.89			14-L			24.0	85.4
♀			10.7	74.2	30-L			20.8	88.6
30-L			1.9	83.0		25+50			
T.P.			0.12	84.76	30-L			9.2	100.2
	12.42	97.18			15-L			13.0	96.4
	24+00				♀			19.5	89.9
30-L			8.0	89.2	15-R			25.4	84.0
♀			15.6	81.6	30-R			31.0	78.4
13-R			20.0	77.2		25+80			
30-R			26.1	71.1	30-R			36.3	73.1
	24+50				20-R			31.3	78.1
30-R			23.7	73.5	♀			21.6	87.8
15-R			15.6	81.6	10-L			15.5	93.9
♀			10.7	86.5	30-L			6.8	102.6
15-L			6.8	90.4		26+00			
30-L			2.0	95.2	30-L			5.8	103.6
T.P.			0.0	97.18	15-L			12.1	97.3
	12.22	109.40				T.P.		12.77	96.63
	25+00						7.94	104.57	
30-L			10.8	98.6	♀			13.5	91.1
♀			20.6	88.8	15-R			19.7	89.9
30-R			29.1	80.3	30-R			26.0	78.6
	25+25					26+15			
30-R			37.5	72.1	30-R			26.0	78.6
♀			29.5	79.9	15-R			20.0	84.6

STA	+	H.I.	-	Elev.	STA	+	H.I.	-	Elev. <sup>4</sup>
☼			15.3	89.3	15-L			16.0	88.6
15-L			10.0	94.6	30-L			8.0	96.6
30-L			3.5	101.1	T.P. On Fence Post			3.9 <sub>v</sub>	100.65
	26+60					7.59	108.24 <sub>v</sub>		
30-L			20.1	84.5		27+50			
15-L			23.1	81.5	30-L			18.7	89.5
☼			27.6	77.0	15-L			22.0	86.2
15-R			30.1	74.5	☼			28.0	80.2
30-R			34.8	69.8	15-R			31.8	76.4
	27+00				30-R			35.4	72.8
30-R			25.1	79.5		27+85			
15-R			19.1	85.5	30-R			29.9	78.3
☼			14.0	90.6	15-R			23.4	84.8
15-L			9.4	95.2	☼			17.0	91.2
30-L			3.8	100.8	15-L			11.6	96.6
	27+13				30-L			7.2	101.0
30-L			3.6	101.0		28+00			
15-L			8.8	95.8	30-L			5.2	103.0
☼			14.2	90.4	15-L			10.7	97.5
15-R			21.0	83.6	☼			17.2	91.0
30-R			28.4	76.2	15-R			24.4	83.8
	27+31				21-R			28.9	79.3
30-R			32.3	72.3	30-R			32.8	75.4
15-R			26.0	78.6	40-R			39.0	69.2
☼			22.2	82.4					

Sta		+	H.I.	-	Elev.	Sta		+	H.I.	-	Elev <sup>5</sup>
		28+23 ♀ House						29+40			
28-R	N. Wall House, Floor Elev.			39.4	69.0	30-L				3.3	107.8
24-R				38.8	69.4	15-L				12.3	98.8
20-R				31.8	76.4	♀				19.5	91.6
16-R				27.0	81.2	20-R				30.3	80.8
♀				19.4	88.8	25-R				42.3	68.8
12-L				12.0	96.2	30-R				45.1	66.0
30-L				4.2	104.0					1.28	109.82
		28+70						12.46	122.28		
30-L				+ 1.4	109.6					0.87	121.41
15-L				5.4	102.8			13.11	134.52		
♀				12.2	96.0			29+65			
15-R				21.6	86.6	50-L				19.6	114.9
24-R				27.0	81.2	25-L				34.2	100.3
29-R				30.3	77.9	8-L				44.0	90.5
46-R				43.3	64.9	♀				46.9	87.6
		29+00								52.9	81.6
40-R				42.6	65.6	15-R				56.3	78.2
30-R				42.8	65.4	25-R				64.0	70.5
18-R				28.2	80.0			30+00			
♀				18.3	89.9	50-R				68.0	66.5
15-L				9.2	99.0	44-R	Bottom old Conc. Ret Wall			68.0	66.5
				4.00	104.24	✓	Top			59.0	75.5
		6.86 111.10								51.6	82.9
30-L				3.5	107.6	25-R				38.2	96.3

Sta	+	H.I.	-	Elev.	Sta	+	H.I.	-	Elev. <sup>6</sup>
15-L			28.0	106.5	25-L			9.5	125.1
25-L			22.2	112.3	¢			17.7	116.9
37-L			14.5	120.0	25-R			27.7	106.9
50-L			6.0	128.5	50-R	N. Wall Powerhouse		36.6	98.0
	30+50				73-R	N.L. of Mill Plant		42.7	92.4
50-L			1.0	133.5		32+00			
35-L			15.0	119.5	70-R	" "		45.0	89.6
¢			29.8	104.7	50-R			38.8	95.8
10-R			32.2	102.3	25-R			31.8	102.8
25-R			40.4	94.1	¢			25.0	109.6
40-R			47.7	86.8	T.P.			11.41	123.19
60-R	Top Bulkhead		51.6	82.9		0.19	123.38		
✓	Botl. " "		64.0	70.5	25-L			11.0	112.4
	31+00				50-L			8.1	115.3
80-R			55.0	79.5	T.P.			13.16	110.22 x
50-R			39.0	95.5		0.48	110.70 ✓		
25-R			29.9	104.6		32+20			
¢			16.2	118.3	50-L			17.0	93.7
25-L			4.7	129.8	25-L			17.0	93.7
40-L	Bottom Conc. Anchor		+0.2	134.7	10-L			15.9	94.8
50-L	Top " "		+4.2	138.7	¢			10.9	99.8
	T.P.		1.27	133.25	12-R			11.3	99.4
	1.35	134.60 ✓			25-R			16.5	94.2
	31+65				50-R			21.8	88.9
50-L			2.5	132.1	65-R	N.L. Mill Plant		25.3	85.4



Sta	+	H.I.	-	Elev.
	33+00			
55-R	N.L. Mill Plant		19.6	91.1
40-R			24.7	86.0
9-R			6.3	104.4
☿			10.7	100.0
6-L			14.9	95.8
25-L			15.5	95.2
50-L			15.6	95.1
	T.P. 500 pg. 6			110.22x
	8.44	118.66		
	33+50			
50-L			22.7	96.0
25-L			22.4	96.3
☿			22.3	96.4
10-R			13.9	104.8
25-R			22.9	95.8
45-R			21.0	97.7
	34+00			
50-R			21.3	97.4
25-R			21.4	97.3
☿			19.3	99.4
20-L			13.5	105.2
34-L			16.3	102.4
50-L			25.0	93.7
	34+25			

Sta	+	H.I.	-	Elev.
60-L			26.3	92.4
50-L			16.9	101.8
25-L			2.6	116.1
☿			3.9	114.8
25-R			3.6	115.1
50-R			8.5	110.2
	34+50			
50-R			3.3	115.4
25-R			5.9	112.8
☿			10.2	108.5
25-L			9.9	108.8
32-L			4.8	113.9
50-L			15.1	103.6
65-L			27.4	91.3
	35+00			
72-L			28.5	90.2
40-L			4.4	114.3
25-L			15.0	103.7
☿			13.6	105.1
25-R			11.9	106.8
50-R			12.4	106.3
	T.P.		12.10	106.56.
	0.38	106.94		
	35+50			
50-R			7.2	

Sta	+	H.I.	-	Elev.
25-R			7.2	99.7
☿			7.6	99.3
25-L			8.6	98.3
33-L			9.1	97.8
50-L			+ 2.2	109.1
	36+00		.	
50-L			14.0	92.9
25-L			13.1	93.8
☿			13.1	93.8
25-R			13.7	93.2
50-R			13.8	93.1
	T.P.		13.14	93.80
	0.60	94.40		
	36+50			
50-R			5.9	88.5
25-R			5.9	88.5
☿			5.5	88.7
25-L			5.7	88.7
50-L			6.1	88.3
	37+00			
50-L			10.6	83.8
25-L			10.4	84.0
☿			10.4	84.0
25-R			10.6	83.8
50-R			11.2	83.2

Sta	+	H.I.	-	Elev.
	37+77			
50-R			5.0	89.4
28-R			16.9	77.5
☿			16.7	77.7
25-L			17.1	77.3
50-L			16.9	77.5
	37+83			
50-L			17.5	76.9
25-L			11.9	82.5
☿			11.4	83.0
25-R			17.3	77.1
40-R			6.0	87.8
50-R			13.2	81.2
	38+50			
50-R			9.9	84.5
28-R			10.6	83.8
22-R			13.7	80.7
☿			14.2	80.2
25-L			13.0	81.4
50-L			12.4	82.0
	39+00			
50-L			21.2	73.2
25-L			11.8	82.6
5-L			11.7	82.7
☿			7.7	86.7

STA	+	H.I.	-	Elev.	STA	+	H.I.	-	Elev.
25-R			8.5	85.9		41+00			
50-R			9.2	85.2	50-L			33.0	73.8
	39+50				23-L			30.0	76.8
32-R			0.2	94.2	¢			15.9	90.9
25-R			5.7	88.7	25-R			15.7	91.1
¢			6.0	88.4	40-R			14.1	92.7
33-L			22.4	72.0		41+50			
50-L			22.8	71.6	50-R			13.2	93.6
	40+00				25-R			16.0	90.8
50-L			21.0	73.4	6-R			16.7	90.1
35-L			21.6	72.8	¢			22.8	84.0
5-L			4.4	90.0	18-L			31.7	75.1
¢			4.7	89.7	50-L			31.0	75.8
22-R			5.0	89.4		42+00			
30-R			1.0	93.4	50-L			31.9	74.9
	T.P.		0.25	94.15	25-L			32.0	74.8
	12.67	106.82			10-L			31.9	74.9
	40+50				¢			27.0	79.8
35-R			12.7	94.1	9-R			16.3	90.5
25-R			16.5	90.3	30-R			15.7	91.1
¢			17.7	89.1	50-R			1.5	105.3
4-L			17.2	89.6		42+20			
25-L			30.9	75.9	50-R			+1.0	107.8
50-L			32.4	74.4	28-R			10.5	96.3
					26-R			15.5	91.3

Sta	+	H.I.	-	Elev.	Sta	+	H.I.	-	<sup>10</sup> Elev.
9-R			15.6	91.2	12-L			17.2	89.6
ϕ			19.6	87.2	14-L			23.3	83.5
3-L	Top		20.3	86.5	25-L			30.0	76.8
✓	Both		22.8	84.0	50-L			30.6	76.2
13-L	Top		20.3	86.5		43+50			
✓	Both.		25.0	81.8	50-L			30.2	76.6
25-L			31.3	75.5	25-L			29.8	77.0
50-L			31.8	75.0	17-L			26.0	80.8
	42+50				11-L			16.3	90.5
50-L			31.1	75.7	5-L			14.8	92.0
25-L			31.4	75.4	ϕ			12.2	94.6
8-L			24.4	82.4	16-R			12.1	94.7
5-L			17.5	89.3	19-R			8.9	97.9
ϕ			16.8	90.0	37-R			3.9	103.9
5-R			14.3	92.5	50-R			+1.0	107.8
22-R			14.9	91.9		T.P.		2.52	104.30
26-R			11.2	95.6		11.46	115.76		
50-R			+ 2.0	108.8		44+00			
	43+00				50-R			5.2	110.6
50-R			+ 3.6	110.4	35-R			9.7	106.1
21-R			10.8	96.0	21-R			12.3	103.5
18-R			14.9	91.9	14-R			20.0	95.8
2-R			13.6	93.2	ϕ			20.5	95.3
ϕ			14.7	92.1	8-L			20.3	95.5
3-L			16.7	90.1	14-L			31.6	84.2

STA	+	H.I.	-	Elv.	STA	+	H.I.	-	Elv.
30-L			38.7	77.1	☐			19.1	96.7
50-L			39.1	76.7	25-R			14.6	101.2
	44+50				50-R			5.8	110.0
50-L			38.3	77.5	T.P. BM. Spike on Isl. Pole opp. 45+14			6.48	109.28 ✓
40-L			38.4	77.4		11.84	121.12 ✓		
21-L			28.2	87.6		46+00			
13-L			19.9	95.9	50-R			5.5	115.6
☐			20.4	95.4	25-R			17.7	103.4
13-R			19.9	95.9	☐			23.7	97.4
18-R			13.9	101.9	28-L			23.8	97.3
25-R			12.2	103.6	31-L			37.8	83.3
50-R			5.7	110.1	42-L			41.8	79.3
	45+00				50-L			42.0	79.1
50-R			4.1	111.7		46+50			
16-R			12.6	103.2	50-L			41.0	80.1
10-R			20.0	95.8	40-L			40.0	81.1
☐			19.9	95.9	32-L			22.0	99.1
13-L			19.3	96.5	6-L			22.2	98.9
44-L			37.3	78.5	☐			20.0	101.1
50-L			37.4	78.4	25-R			11.2	109.9
	45+50				50-R			0.0	121.1
50-L			37.0	78.8		47+18 <sup>27</sup> Pac.			
40-L			36.7	79.1	50-R			+16.8	137.9
25-L			28.3	87.5	25-R			+3.6	124.7
17-L			19.7	96.1	☐			14.1	107.0

STA	+	H.I.	-	Elv.
10-L			20.8	100.3
33-L			19.6	101.5
37-L			33.8	87.3
50-L			39.5	81.6
T.P.			12.54	108.58
	1.84	110.42		
T.P.			13.16	97.26
	0.53	97.79		
T.P.			8.66	89.13
	2.42	91.55		
T.P.			12.44	79.11
	0.74	79.85		
T.P.			12.13	67.72
	6.19	73.91		
T.P.			11.78	62.13
	0.11	62.24		
T.P.			8.77	53.47
	2.18	55.65		
T.P.			10.00	45.65
	9.55	55.20		
T.P.			6.15	49.05

Check B.M. on Top of Post in Front of Silo  
see pg. 2

49.05  

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0.00

STA	+	H.I.	-	Elv.
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indexed  
c.s.R.

Cross Section of N+S alley inside  
betw. Westbourne & Nautilus S. La Jolla  
east of Neptune Place Bet. Blks B-E-F South La Jolla.

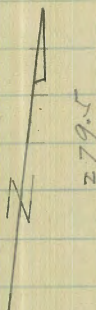
Westbourne

ST.

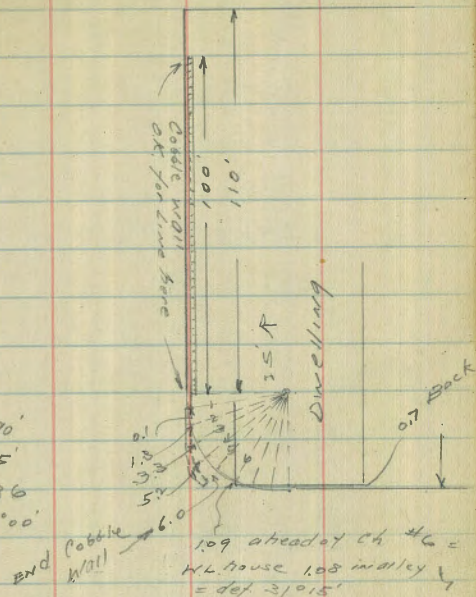
Moore  
Northern  
7/23/51

13

SE.B.P.	1.62	80.63	79.01	10510 Bldg Westbourne
T.P.	0.84	68.42	12.05	67.58
T.P.	0.51	56.19	17.74	55.68
				HI 56.19 = 5
				00 = NL Nautilus ST
E	Top cb		6.21	49.98
E	Facing		6.81	49.38
C	"		7.49	48.70
W	"		7.61	48.58
N	Top cb		7.53	48.66
				+05
W			6.7	49.5
C			6.5	49.7
+3			6.1	50.1
+6			4.2	52.0
E			3.8	52.4
				0+25
E			4.8	51.8
C			5.6	50.6
W			6.3	49.9
+10			8.0	48.2
				0+50
-10			8.0	48.2
W			6.4	49.8
C			5.4	50.8
E			4.5	51.7

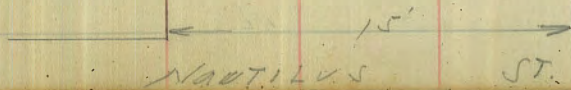


$\Delta = 90'$   
 $R = 25'$   
 $ch = 4.36$   
 $def. = 5.00'$



Note!

100' cobble wall OK for line  
rods at foot of wall = ground elev.  
bottom wall not more than  
05' below ground.



56.19

0+75

E	L.N	52.0
C	5.N	51.0
W	6.5	49.7
+10	8.0	48.2

1+00 = P.C. Curve S.W. along

-10	8.5	47.7
W	7.0	49.2
C	5.9	50.3
E	5.0	51.2

1+25 = P.I. = S.W. along to east

E	5.3	50.9
C	6.5	49.7
W	7.6	48.6
+10	9.1	46.1

1+34.75 = E of alley to east = 19.5 wide

-10	9.5	46.7
W	7.7	48.5
C Top Sewer 1947/1948	6.91	49.28
C Hook here "	10.39	45.80
E	5.8	50.4

1+44.5 = P.I. on N.L. to east

E	5.7	50.5
C	7.0	49.2
W	8.0	48.2
+10	9.4	46.8

56.19

14

1+69.5 = P.C. alley return

-10	9.5	46.7	
W	7.9	48.3	
C	7.0	49.2	
E	ground foot wall	6.5	49.8
E	Top "	4.63	51.56

1+94.5

E	Top wall	5.1	51.1
E	foot "	7.1	49.1
C		7.7	48.5
W		8.5	47.7
+10		10.0	46.2

2+13.2

-15	2. Six garage dirt floor	11.2	45.0	Face South
-10		10.3	45.9	
W		8.7	47.5	
C		8.1	48.1	
E	foot cobble wall	7.5	48.8	
E	Top " "	5.52	50.67	

2+49.5 = 2+19.5' alt

E	Top wall	5.06	50.53
E	foot "	7.6	48.6
C		8.2	48.0
W		9.1	47.1
+10		10.2	46.0



56.19

3+44.5			
-10	11.1	45.1	
W	9.9	46.3	
C	8.9	47.3	
E foot wall	8.3	47.9	
E Top r	6.13	50.06	
2+69.5 = N end cobble wall = old SL ST.			
E Top cobble wall	6.5	49.7	
E foot r r	8.6	47.6	
C	9.2	47.0	
W	10.2	46.0	
T10	11.5	44.7	

2+77.5

-10	11.7	44.5	
W	10.9	45.3	
C	9.7	46.5	
E	8.9	47.3	
2+79.5 = SL Westbourne			
E Top cb	11.14	45.05	
E PAVING	11.73	44.46	
C	14.58	43.61	
W	12.81	43.38	
W cb	12.80	43.39	

56.19

S end cobble wall		See sketch	
	Top wall	2.17	52.02
	foot "	5.3	50.9
25' east of EL of N+S alley = EC alley return =			
N		3.5	52.7 ← d of 19.5
C		3.6	52.6
S		3.1	53.1
50' east of N+S alley			
S		2.3	53.9
C		2.4	53.8
N		2.7	53.5
64' east = 2 double girds on north			
N	18' wide	1.8	54.35
C		1.9	54.3
S		1.8	54.4
100' E of EL of N+S alley			
S		0.4	55.8
S		0.4	55.8
N		0.4	55.8
T.P.	12.70	68.38	0.51
T.P.	12.00	79.58	0.80
check to B.M.			
		0.5-9	78.99
			79.01
			0.02 error OK

15

wide  
of north =  
Top Com  
Foundation of  
house sketch

ON LINE  
CEM FLOOR  
LEVEL

to 704  
Westbourne  
SKBP

Cross Section State St  
From Thorn to Siskiyou

75 N.W.  
335' C.L.  
75 Q.M.

19016

1-12-33  
Map  
Siskiyou  
County  
Oregon  
16

index  
cush

index cush				75 N.W. 335' C.L. 75 Q.M.				
BM	1.80	19016	18836	Thorn State SFBR	F	24	187.8	
BM		2.89	18727	Thorn State	F	37	186.5	0+25
	0+0 S.W. Thorn St			S/4 of Corc Walk		44	185.8	
F	on Corc Walk	2.25	187.91		cb	47	185.5	
+14		3.67	186.19		1/4	51	185.1	
+21.5	S/4 End Ch Rd	4.51	185.65		1/2	52	184.9	
	on Pairing	4.93	185.23		1/2	57	184.5	
	S/4 of End Ch	4.09	186.07		cb	62	184.0	
1/4	on Pairing	4.92	185.24		+8.5	67	183.5	
1/2		4.98	185.18		H	75	182.7	
1/4		5.30	184.86					0+40
cb+1		5.67	184.19		H	86	181.6	
	S/4 End Ch Rd	5.25	184.91		+14	76	182.6	
	S/4 of End Ch	5.18	184.98		cb	69	183.3	
cb+8.5	on Corc Walk	5.31	184.85		1/4	66	183.6	
H		4.37	183.79		1/2	61	184.1	
	0+05 - EC 15' Ch Road				1/4	57	184.5	
H		6.6	183.2		cb	53	184.9	
+14		6.6	184.1		+8.5	51	185.1	
cb		5.6	184.6		F	43	185.9	
1/2		5.4	184.8					0+60
1/2		5.0	185.2		-5	89	181.3	
1/4		4.9	185.3		F	88	181.4	
cb		4.5	185.7		+11	95	180.7	
+8.5		3.6	186.6		cb	102	180.0	

## Stote St

190.16

1/2		70	1832
1/2		69	1833
1/4		74	1828
cb		86	1816
+85		101	1801
H		110	1792
+50		115	1787
H	2.08	179.53	1271
	0.80		17745
-10'		63	1732
H		59	1731
114		55	1740
cb		48	1747
1/4		52	1743
1/2		41	1751
1/4		49	1746
cb		45	1750
+85		41	1751
F		35	1760
+5'		26	1769
	1.40		
-7		51	1744
F		70	1725
+11		110	1685
cb		124	1671
1/4		122	1663

17953

1/2		126	1659
1/4		136	1659
cb		133	1662
+85		127	1668
H		124	1671
+10		129	1666
	1.20		
-15		220	1575
H		213	1582
+14		212	1583
cb		214	1581
1/4		223	1572
1/2		216	1579
1/4		196	1599
cb		169	1626
+85		129	1666
F		79	1716
+6		57	1738
	1.40		
-5		62	1727
F		76	1719
+11		111	1681
cb		153	1642
1/4		181	1609
1/2		220	1575
1/4		256	1539

17

State St.

179.53

Cb	284	1511
+25	295	1500
H	301	1494
+30	308	1487
	1+60	
-25	377	1418
H	355	1440
+11	312	1423
Cb	272	1523
1/2	234	1561
✓ 1/2	203	1592
1/4	175	1620
Cb	152	1643
+25	120	1675
F	81	1709
	1+80	
F	90	1705
+14	129	1666
Cb	158	1637
1/4	191	1604
✓ 1/2	214	1581
1/2	242	1553
Cb	270	1525
+25	299	1496
H	346	1449
+10	386	1411

179.53

18

+30	415	1380
	2+0	
-30	410	1385
H	319	1476
+14	276	1519
Cb	252	1542
1/2	230	1565
✓ 1/2	206	1589
1/4	184	1611
Cb	158	1637
+25	122	1673
F	112	1683
	2+20	
F	110	1685
+2	126	1669
+14	140	1655
Cb	141	1654
1/2	144	1651
✓ 1/2	142	1653
1/4	149	1641
Cb	216	1579
+25	256	1539
H	305	1490
+30	382	1412
	2+40	
-25	350	1465

Stafst.

17953

H	25.0	154.5
+11	16.7	162.8
cb	14.2	165.2
1/4	13.6	165.9
√ 1/2	13.4	166.5
1/2	14.1	165.4
cb	13.9	165.1
+8.5	14.0	165.5
F	8.7	170.8
	2+00	
F	6.4	173.1
+14	8.3	171.2
cb	11.4	163.1
1/4	12.9	166.6
√ 1/2	13.8	165.7
1/4	14.1	165.4
cb	14.4	165.1
+8.5	14.8	164.9
H	17.6	161.9
+1.5	21.5	158.0
	2+67	
-10	16.8	162.7
H	14.8	164.7
+11	13.7	165.8
cb	13.4	166.1
1/4	13.3	166.2

17953

19

√ 1/2	13.3	166.2
1/4	11.7	167.8
cb	9.6	169.9
+8.5	8.4	171.1
F	7.4	172.1
	2+80	
F	7.0	172.5
+14	8.3	171.2
cb	8.5	171.0
1/4	10.1	169.1
√ 1/2	11.6	167.9
1/4	12.3	167.3
cb	12.6	166.9
+8.5	12.4	166.1
H	14.6	164.9
	3+0	
H	14.8	164.7
+11	13.5	166.0
cb	12.9	166.6
1/4	12.5	167.0
√ 1/2	11.9	167.6
1/2	11.2	168.3
cb	9.9	169.6
+8.5	9.1	170.4
F	8.2	171.3

State St. 179.53

TP 2.13 172.49 917 170.36

2+15 = H.L. Sacramento St

F 21 170.4

+11 on Cass Walk 556 166.93

✓ Cb - H End Cb Rd 570 166.79

on Paxiog 632 166.17

" " " 627 166.22

✓ 1/2 " " 633 166.16

" " " 651 165.98

Gutter " " 687 165.62

Cb - H End Cb Rd 619 166.30

BM 617 166.32

19 on Cass Walk 619 166.30

✓ " 88 163.7

H.H.P.  
Sacramento  
St.

Cross Section Sassafras St  
East Line State to 120' E of E Line

W. Dixon  
C. S. K.

8' Wide  
20' Cb  
16' S

18445

1-12-32  
21

17219.81 End

0+0 E. State St

H	21	170.4
+11 = H Edge Walk	2.81	169.68
Cb Top - End Cb Rd	3.03	169.46
Gutter on Paving	3.67	168.82
H	3.11	169.38
H	2.77	169.72
H	2.90	169.79
Gutter	2.82	169.67
Cb - E End Cb Rd	2.22	170.27
+85 = S Edge Walk	2.23	170.26
S	1.8	170.7

0+2

S	0.6	171.9
+11.5	1.1	171.4
Cb	1.5	171.0
H	1.3	171.2
H	1.9	170.6
H	2.1	170.4
Cb	2.3	170.2
+9	1.5	171.0
H	0.8	171.7
TP	1258	18445 0.62
		171.87

0+3

H	5.2	179.2
---	-----	-------

+11.5

Cb

H

✓ S

H

Cb

+85

S

0+10

S

+11.5

Cb

H

✓ S

H

Cb

+85

H

0+30

H

+11.5

Cb

H

✓ S

H

Cb

51

48

45

45

57

75

65

50

54

47

43

42

41

26

47

47

43

27

24

23

27

30

25

40

179.3

179.6

179.9

179.9

178.7

176.9

177.9

179.4

179.0

179.7

180.1

180.2

180.3

180.8

180.7

180.2

180.1

181.7

182.0

182.1

181.7

181.4

180.9

180.4

Sassafras St.

184.45

+8.5		53	179.1
S		16	177.8
TP	4.36	188.79	0.02
	0+50		184.43
S		12.8	176.0
+11.5		10.9	177.9
CB		9.8	179.0
1/4		8.1	180.7
✓ 1/2		6.7	182.1
1/4		5.3	183.5
CB		4.1	184.7
+8.5		3.8	185.0
H		3.3	185.5
	0+75		
H		1.6	187.2
+11.5		2.6	186.2
CB		4.0	184.8
1/4		5.2	183.6
✓ 1/2		7.8	181.0
1/4		10.2	178.5
CB		12.0	176.8
+8.5		13.7	175.1
S		18.2	170.6
+10		22.2	166.6
	1+0		
-1.5		25.9	163.1

188.79

S		19.5	169.3
+11.5		16.6	172.2
CB		13.1	175.2
1/4		12.7	176.1
✓ 1/2		10.7	178.1
1/4		9.0	179.8
CB		6.8	182.0
+8.5		5.2	183.6
H		3.9	184.9
	1+20		
H		4.9	183.9
+11.5		6.9	181.9
CB		8.8	180.0
1/4		11.8	177.0
✓ 1/2		14.3	174.5
1/4		17.0	171.8
CB		19.5	169.3
+8.5		21.3	167.5
S		24.0	164.8
+20		31.0	157.8
BM		1.52	187.27

22

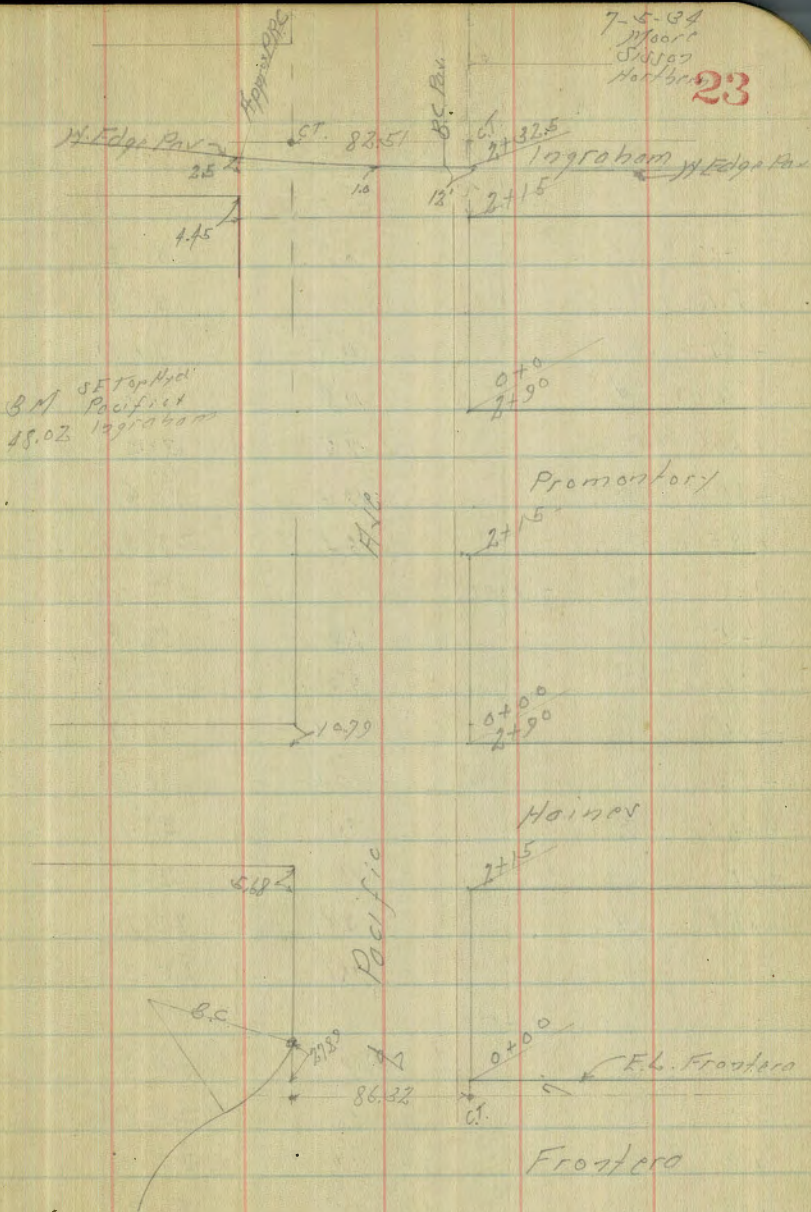
SFBP  
Theront Stale  
18727



Cross Section Pacific Ave  
Frontera St. to Ingraham

Indexed  
c.s.k.

B.M.	11.77	32.96	21.19	N.W. B.P. Pacific & Gresham
	0+0 - 8.5' E Gutter Frontera			
S.L.	on Paving	3.57	29.39	
+20	" "	3.46	29.50	
+30	" "	3.48	29.48	
+43.15	" "	3.67	29.29	
+60	" "	4.07	28.89	
+70	" "	4.33	28.63	
+86.32	" "	4.74	28.22	
+112	= Gutter	5.75	27.21	
+115	= Top Conc. Cb.	5.18	27.78	
	0+0 - 7.5'			
S.L.	Top Curb	2.93	30.03	
	0+02 = Fly Edge Paving			
S.L.		2.1	30.86	
+3.3	= Fly Edge Conc. Walk	2.57	30.39	
+16	= Top Cb.	2.42	30.54	
+17.5	= Gutter on Pav.	2.98	29.98	
+25	on Paving	3.00	29.96	
+43.16	" "	3.20	29.76	
+60	" "	3.63	29.33	
+86.28	" "	4.44	28.52	
+97.0	" " Gutter	4.93	28.03	
+98.5	Top Cb.	4.37	28.59	
+106.2	= N.W. Edge Wall	1.77	28.19	



42.96

TP	11.30	42.89	13.7	31.59
		0+27.89 =	BC. 07 11	
-7			6.7	34.2
S.L.			11.1	31.8
+25			11.8	31.1
+43.08 = $\frac{1}{2}$			11.8	31.1
+60			11.7	31.2
+86.16 = H.L.			12.3	30.6
+95			9.1	33.5
		0+150		
-5			6.8	36.1
S.L.			9.0	33.9
+10			10.6	32.3
+25			10.5	32.4
+43.03 = $\frac{1}{2}$			9.8	33.1
+60			10.0	32.9
+86.06 = H.L.			9.8	33.1
+91			7.6	35.3
		0+75		
S.L.			1.3	38.6
+3			4.8	38.1
+7			7.9	35.0
+25			7.9	35.0
+42.97 = $\frac{1}{2}$			7.5	35.4
+60			7.7	35.2

42.89

24

				+85.95 = H.L.	7.7	35.2
				+90	5.5	37.4
				1+0		
				S.L.	2.1	40.8
				+4	2.2	40.7
				+7	5.1	37.8
				+25	5.0	37.9
				+42.92 = $\frac{1}{2}$	4.7	38.2
				+60	5.1	37.8
				+85.84 = H.L.	5.1	37.8
				+90	3.6	39.3
				TP	11.65	54.30
					0.24	42.65
				1+25		
				S.L.	10.8	43.5
				+4	10.9	43.4
				+7	14.0	40.3
				+25	13.9	40.4
				+42.86 = $\frac{1}{2}$	13.3	41.0
				+60	13.6	40.7
				+85.72	14.0	40.3
				+90	13.0	41.3
				1+50		
				S.L.	7.8	46.5
				+6	8.0	46.3
				+9	11.1	43.2
				+25	10.9	43.4

5430

+42.80	11.0	43.3
+60	11.5	42.8
+82	12.3	42.0
+85.61 = NL	10.8	43.5

1+75

S.L.	5.2	49.1
+5	5.5	48.8
+9	8.4	45.9
+25	8.4	45.9
+42.75 = $\frac{1}{2}$	8.2	46.0
+60	8.8	45.5
+80	9.3	45.0
+85.50 = NL	8.1	46.2

2+0

S.L.	2.9	51.4
+6	3.0	51.3
+10	5.6	48.7
+25	5.7	48.6
+42.69 = $\frac{1}{2}$	5.5	48.8
+60	5.7	48.6
+80	6.1	48.2
+85.38 = NL	5.2	49.0

2+15: NL Hammer to So.

S.L.	1.8	52.5
+7	1.8	52.5
+10	0.9	50.6

5430

+25	3.6	50.7
+42.63 = $\frac{1}{2}$	3.5	50.8
+60	4.0	50.3
+85.27 = NL	3.4	50.9

2+20.68 = NL Hammer to North

S.L.	1.5	52.8
+6	1.4	52.9
+9	3.2	51.1
+25	3.4	50.9
+42.62 = $\frac{1}{2}$	2.9	51.4
+60	3.4	50.9
+85.25 = NL	3.1	51.2
TP 6.34 60.37 0.27		54.03

2+52.15 =  $\frac{1}{2}$  Hammer From S

S.L.	5.3	55.1
+25	5.6	54.8
+42.55 = $\frac{1}{2}$	5.6	54.8
+60	6.7	53.7
+85.10 = NL	6.4	54.0

2+60.68 =  $\frac{1}{2}$  Hammer From N

S.L.	5.1	55.3
+25	5.4	55.0
+42.52 = $\frac{1}{2}$	5.4	55.1
+60	6.3	54.1
+85.05 = NL	6.3	54.1

25

6037

0+0.2+90 = E.L. Hoines Front

S.L.	44	56.0
+25	47	55.7
+42.46 = $\frac{1}{2}$	43	56.1
+60	49	55.5
+84.93 = H.L.	48	55.6

0+10.79 = E.L. Hoines Front

S.L.	43	56.1
+25	43	56.1
+42.44 = $\frac{1}{2}$	42	56.2
+60	44	56.0
+84.89 = H.L.	45	55.9

0+50

S.L.	46	55.8
+25	42	56.2
+42.36 = $\frac{1}{2}$	39	56.5
+60	44	56.0
+84.72 = H.L.	40	56.4

1+0

S.L.	61	54.3
+25	54	55.0
+42.24 = $\frac{1}{2}$	46	55.8
+60	49	55.5
+84.48 = H.L.	43	56.1

6037

1+50

S.L.	8.7	51.7
+25	8.0	52.4
+42.13 = $\frac{1}{2}$	6.9	53.5
+60	6.8	53.6
+84.26 = H.L.	5.9	54.5

2+0

S.L.	11.6	48.8
+25	10.5	49.9
+42.01 = $\frac{1}{2}$	9.6	50.8
+60	9.3	51.1
+84.02 = H.L.	7.7	52.7

2+15 = H.L. Promontory

S.L.	12.4	48.0
+25	11.3	49.1
+41.98 = $\frac{1}{2}$	10.3	50.1
+60	9.8	50.6
+83.96 = H.L.	8.8	51.6

2+52.5 =  $\frac{1}{2}$  Promontory

S.L.	13.3	47.1
+25	12.4	48.0
+41.89 = $\frac{1}{2}$	11.8	48.6
+60	11.3	49.1
+83.79 = H.L.	10.2	50.2

60.37

2+90 = I.L. Promontory 0+0

S.L.	14.0	46.4
+25	13.5	46.9
+41.81	12.7	47.7
+60	12.4	48.0
+83.62 = H.L.	11.5	48.9
TP	3.42	51.21
	12.58	47.79

0+50

S.L.	5.5	45.7
+25	5.0	46.2
+41.70 = $\frac{1}{2}$	4.5	46.7
+60	4.3	46.9
+83.40 = H.L.	3.6	47.6

1+0

S.L.	6.0	45.2
+25	5.8	45.4
+41.58 = $\frac{1}{2}$	5.1	46.1
+60	4.9	46.3
+83.17 = H.L.	4.1	47.1

1+50

S.L.	5.5	45.7
+25	5.7	45.5
+41.47 = $\frac{1}{2}$	5.5	45.7
+60	5.2	46.0
+82.94 = H.L.	3.9	47.3

51.21

2+0

S.L.	4.9	46.3
+25	4.8	46.4
+41.36 = $\frac{1}{2}$	5.4	45.8
+60	5.3	45.9
+82.73 = H.L.	5.3	45.9

2+15 = H.L. Ingraham From S

S.L.	4.9	46.3
+25	4.7	46.5
+41.30 = $\frac{1}{2}$	5.5	45.7
+60	5.3	45.9
+82.60 = H.L.	4.9	46.3

2+32.5 = H. Edge Paving From So

S.L. on Pav.	5.53	45.68
+12 = B.C. of Paving	5.53	45.68
+25	5.5	45.7
+41.27 = $\frac{1}{2}$	5.5	45.7
+60	5.3	45.9
+82.55 = H.L.	5.2	46.0

H. Edge Paving

$\frac{1}{2}$ Pacific on Paving	5.62	45.59
H.L. " " "	5.67	45.74

BM

3.12 48.09

 SET up Hyd  
 Pacific  
 10/10/00  
 48.02

27

 Photo of July 13-1934  
 HFB

Xsec of Sassafras St. 20' curbs  
STATE to 1815

NWBSP 11.45 177.77 166.32 Sassafras  
STATE

00 - 14' = Ely State to North

N Top cb recover 9.65 168.12

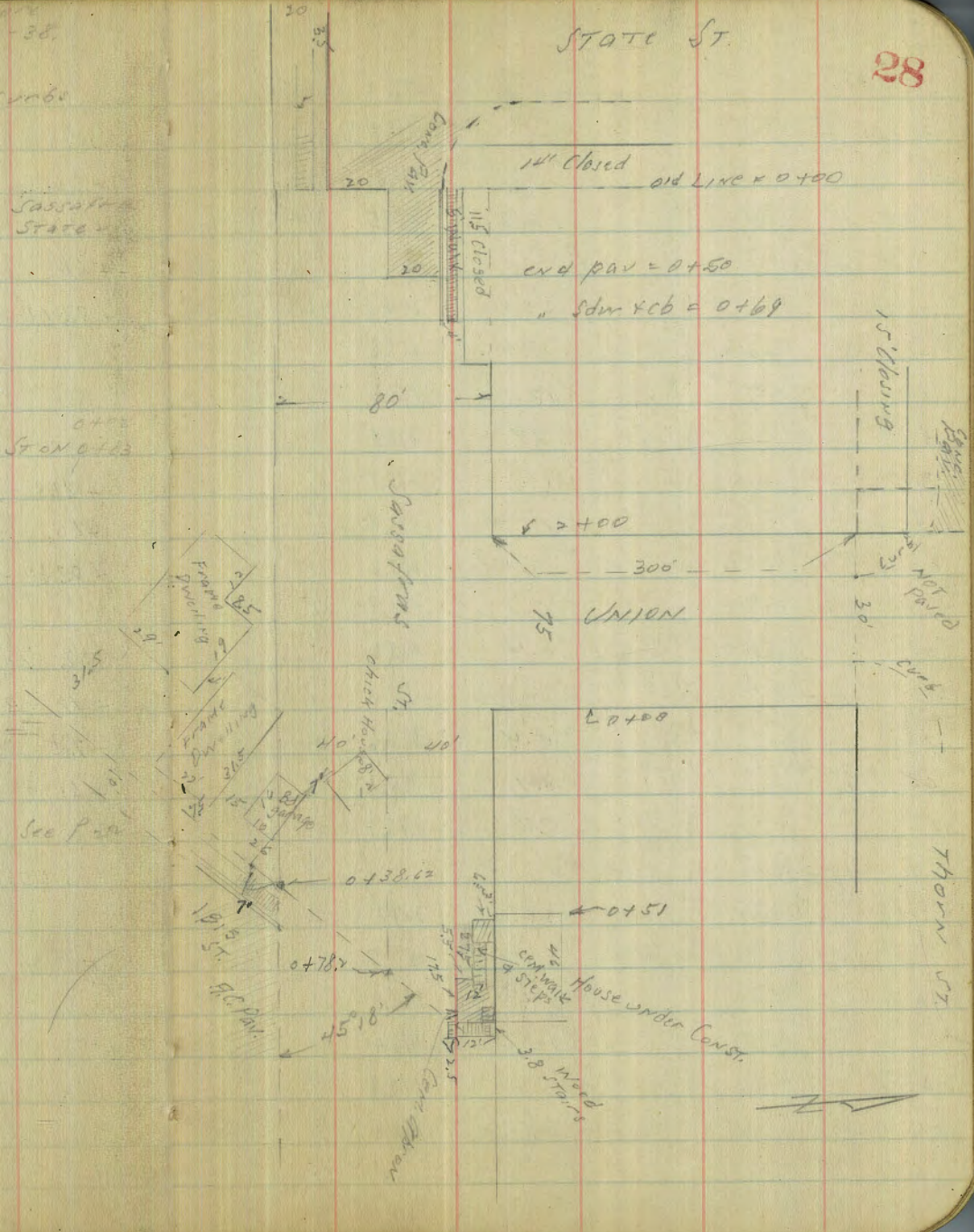
" gut. 10.16 167.61

for 0+00 see p 21 also for 5 1/2' of STON 913

Station	Dist	Elevation
0+00		
N cb	8.07	169.70
gut	8.66	169.11
C Pav	7.90	169.87
0+50		
N cb	3.78	173.99
gut	4.39	173.38
C end pav	4.27	173.50

T.P. 913 186.01 0.89 176.88

Station	Dist	Elevation
0+69 Ely end cb + sdw.		
N cb	11.43	174.58
gut dist	11.9	174.1
C	11.6	174.4
+1	4.6	181.4



186.01

S. cb	8.8	177.2
+10	11.1	174.9
S	14.7	171.3
+10	18.5	167.5
1+00		
-10	22.0	164.0
S	17.4	168.6
cb	12.2	173.8
+19	7.7	178.3
C	10.1	175.9
+10	10.2	175.8
cb	8.4	177.6
N to West	5.1	180.9
N " EAST	0.4	185.6
1+01		
N	0.0	185.6
cb curbs 20' from here to 161.9	3.9	182.1
C	7.7	178.3
1+25		
-10	26.2	159.8
S	22.5	163.5
cb	17.7	168.3
C	12.6	173.4
cb	7.2	178.8
N	3.5	182.5

186.01

1+50		
N	7.2	178.8
+8	9.5	176.5
cb	11.2	174.8
C	16.3	169.7
cb	24.3	161.7
S	29.5	156.5
+22 Top of bank	36.5	149.5
-20 1+75	53.7	132.3
S Top bank	51.6	134.4
cb	36.0	150.9
cb	29.2	156.8
C	22.7	163.3
cb	16.8	169.2
N	12.0	174.0
J.P. Nail Post 0.26	173.36	12.91
		173.10
+00 Wly Union St		
N	7.8	170.6
cb	7.9	165.5
C	14.2	159.2
cb	23.1	150.3
+5	24.1	149.3
S	41.1	132.0
+20	46.1	127.3

29

approx.  
25' bank

173.36

W	cb on Union 222.5		
-15		47.1	126.3
S		47.0	126.4
+14		45.2	128.2
cb		31.2	142.2
+7	Top bank	26.3	147.1
C		21.2	152.2
cb		13.3	160.1
N		8.8	164.6

T.P.	0.52	161.50	123.38	160.98	STUB
------	------	--------	--------	--------	------

E UNION ST

N		2.0	159.5
cb		6.9	154.6
C		13.3	148.2
+6		15.0	146.5
+14		32.1	129.4
cb		34.8	126.7
S		36.1	125.4
+15	under house	36.7	124.8
E cb = 22.5 cb on UNION			
-15		35.4	126.1
S		35.4	126.1
cb		33.4	128.1
+15		32.8	128.7
C		20.5	141.0

161.50

cb		14.0	147.5
N		6.7	154.8

T.P.	ON PIPE	0.35	148.92	1293	148.57
------	---------	------	--------	------	--------

E. L UNION = 0400

N		0.35	148.57
+13		4.4	144.5
cb		9.0	139.9
+13		15.1	133.8
C		23.8	125.1
cb		23.8	125.1
S		28.0	120.9
+15	under house	28.0	120.9

T.P.	0.83	137.14	12.61	136.31
------	------	--------	-------	--------

D + 30

-15		17.5	119.6
S		17.2	119.9
cb		16.8	120.3
C		16.3	120.8
cb		9.0	128.1
+3		5.7	131.4
N		+1.2	138.3

30

N.E. COR  
UNION  
CROSSING



137.14

0+44			
N	2.9	134.2	
+10	7.0	130.1	
cb	7.5	129.6	
+10	9.8	127.3	
C	14.6	122.5	
0+45			
C	14.6	122.5	
+10	9.8	127.3	
cb	7.5	129.6	
+10	7.0	130.1	
N	7.1	130.0	
0+53			
N on cent right	6.87	130.27	
+65 " " "	6.89	130.25	
cb	7.5	129.6	
+14	14.8	122.3	
C	15.2	121.9	
T.P.	2.68	128.60	11.22 125.92

0+78.2 = with 1bis to South Sec. at 90° with

C on stub	7.00	121.60	E Sassafras
cb	5.7	122.9	
+8 W edge cent. apron	6.13	122.47	

128.60

31

N - W edge 9am floor	5.88	122.72	cent. floor level
E edge cent apron	6.02	122.58	17.5 wide
Sta. 0+78.2 on E Sassafras			
Sec. diag. on W/H line of 1Bis to So.			
N	8.0	120.6	
+13	7.4	121.2	
+20 Top cent.	6.07	122.53	
cb	7.5	121.1	
C	7.0	121.6	
cb	7.6	121.0	
S = SW Cor 1bis + Sassafras	8.4	120.2	

Top cb " " " 8.52 120.08

Indexed  
2.5 K.X sec Union  
Sassafras to Thorn37. 75' wide  
22.5 obs

173.45

32

T.P. on Sub 1247 173.45

160.98

P 30

1700

W

+19.7 193.2

cb

+17.4 190.9

C

+14.5 188.0

cb

+12.0 185.5

E

+9.5 183.0

+15

+6.5 180.0

NL Sassafras = 0+100

0+25

-20

21.2 152.3

E

17.0 156.5

cb

10.2 163.3

C

7.0 166.5

cb

2.1 171.4

W

+2.5 176.0

T.P.

13.05 186.42 0.08 173.37

T.P.

12.86 199.05 0.23 186.19

0+50

W

+7.0 180.1

cb

+4.5 178.0

C

+1.0 174.5

cb

3.2 170.3

E Pipe

8.4 165.1

+1.5

10.9 162.6

1+25

-10

14.8 184.3

E

12.8 186.3

cb

9.0 190.1

C

6.3 192.8

cb

4.7 194.4

W

3.3 195.8

0+75

-15

4.8 168.7

E

2.1 171.4

cb

+5.5 179.0

C

+7.3 180.8

cb

+11.4 184.9

W

+14.5 188.0

1+50

W

0.2 198.9

cb

0.7 198.4

C

1.5 197.6

cb

4.0 195.1

E

6.7 192.4

+10

8.3 190.8

199.05  
 T.P. 11.87 210.07 085 198.20

1+75  
 -10 16.0 194.1  
 E 14.8 195.3  
 cb 11.5 198.6  
 C 9.6 200.5  
 cb 9.2 200.9  
 W 9.3 200.8

2+00  
 W 8.1 202.0  
 cb 7.9 202.2  
 C 7.8 202.3  
 cb 8.1 202.0  
 E 11.8 198.3  
 +10 13.4 196.7

2+75  
 E -10 9.7 200.4  
 E 8.7 201.4  
 cb 5.6 204.5  
 C 5.9 204.2  
 cb 6.3 203.8  
 W 7.1 203.0

210.07

33

2+50  
 W 6.5 203.6  
 cb 4.8 205.3  
 C 4.5 205.6  
 cb 3.8 206.3  
 E 5.0 205.1

2+75  
 E 3.3 206.8  
 cb 7.5 207.6  
 C 3.2 206.9  
 cb 3.8 206.3  
 W 5.7 204.4

2+90  
 W 5.3 204.8  
 cb 3.4 206.5  
 C 3.5 206.6  
 cb 3.4 206.7  
 E 2.4 207.7

3+00 SL. Thru to east

E 2.0 208.1  
 cb. CEM. end return 4.18 205.89  
 gut 4.5 205.6  
 C 4.8 205.3  
 cb CEM. " " 5.62 204.45  
 +10 5.2 204.9  
 +12 3.7 206.4  
 W 4.5 205.6

Indexed  
c.s.k

Moore  
11-2-38.

X sec of Alley 15' wide  
Blk 9 Wilshire Pl.

Monroe

Ave 34

NWBP 417 368.83 364.66 <sup>1/2 in</sup> Meade

- 15 = N 16 of Meade

N	par.	4.85	363.98
C	"	4.88	363.95
E	"	4.91	363.92

0+00 = N 16 Meade

E	cb	3.86	364.97
E	par	4.10	364.73
C	"	4.05	364.78 ✓
W	"	3.88	364.95
N	cb	3.43	365.20

0+20

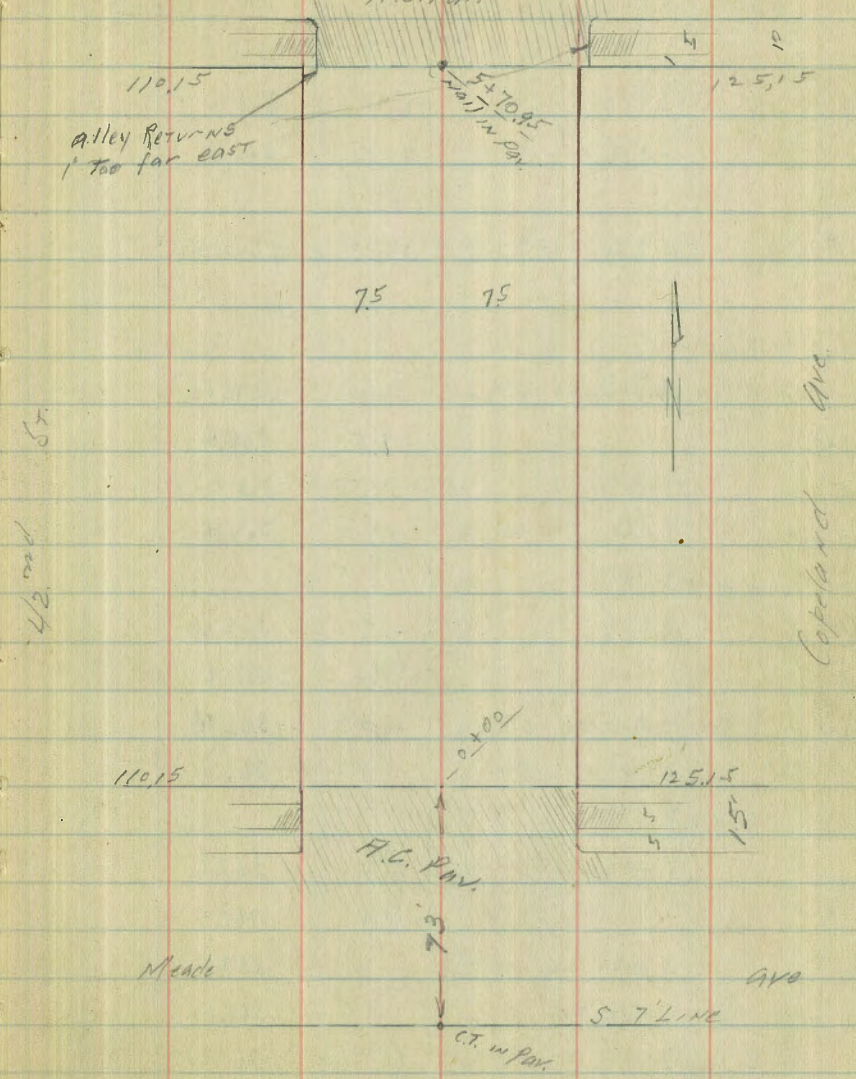
W		2.9	365.9
C		2.5	366.3
E		2.4	366.4

0+50

		2.3	366.5
		2.4	366.4
		2.5	366.3

0+55

E		2.5	366.3
-3	9' wide conc. slab	2.60	366.23



368.83

1+00			
E	2.4	366.4	
C	2.4	366.4	
W	2.5	366.3	
T.P.	5.36	371.87	2.34 366.51

1+15

- 23 Sin gar cem. floor	5.42	366.45	
W	5.5	366.4	
C	5.5	366.4	
E	5.5	366.4	

1+56

E	4.7	367.2	
C	5.0	366.9	
W	Cem apron	4.94	366.98
+4	Sin gar cem.	4.86	367.01

2+07

W	4.3	367.6	
C	4.4	367.5	
E	4.4	367.5	
+2	Cem. apron	4.46	367.41

+4.5 Sin gar cem 4.26 367.61

2+18

W-3 Sin gar cem 4.19 367.68

371.87

2+50

- 4 Sin gar cem.	3.46	368.41	
W	4.2	367.7	
C = S.M.H. P.M.	4.26	367.61	
E	4.3	367.6	

T.P. 361 371.29 4.19 367.68

2+83

W-3 Sin gar dirt 3.4 367.9

3+08

- 12 Sin gar dirt 3.9 367.4

E 3.6 367.7

C 3.3 368.0

W 3.1 368.2

3+50

W 3.3 368.0

C 3.8 367.5

E 3.9 367.4

+10 4.4 366.7

3+70

- 10 5.1 366.2

E 3.9 367.4

C 3.9 367.4

W 3.6 367.7

35

371.29

3+80

- 11 Sin gar. com 2.3 369.0

W 3.0 368.3

3+90

W 3.4 367.9

C 3.9 367.4

E 4.1 367.2

+ 6.5 Sin. gar. dirt 4.9 366.4

4+25

- 5 5.5 365.8

E 4.9 366.4

C 4.6 366.7

W 4.2 367.1

4+50

W 4.9 366.4

C 5.3 366.0

E 5.3 366.0

+ 5 5.5 365.8

4+75

E 5.8 365.5

C 5.9 365.4

W 5.4 365.9

5+04

- 5 Sin. gar. dirt 5.2 366.1

W 5.6 365.9

371.29

36

C 6.1 365.2

E 6.0 365.3

5+30

E 6.0 365.3

C 6.1 365.2

W 5.80 365.49

5+70.95 - SL Meade - ?

W ob. 5.50 365.79

W Pav. 5.89 365.40

C " 6.11 365.18

E " 6.07 365.22

E ob. 5.81 365.48

5+80.95 - S ob line Meade ?

E Pav. 6.72 364.57

C " 6.59 364.70

W " 6.40 364.89

T.P. 1.29 369.33 325 368.04

check to BM. 4.68 364.65 364.66

0.01



973  
834

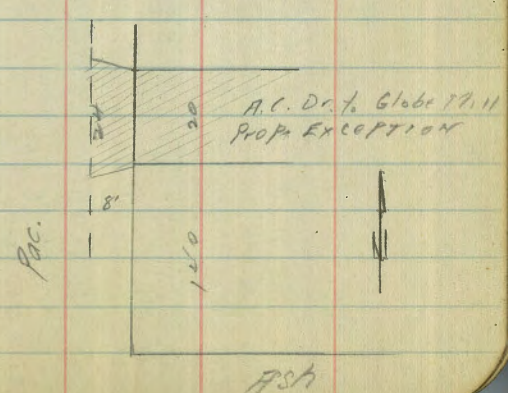
979  
830

NL H + 6

E cb	END TOP cb	5.39	2.85
	0+50		
E		5.6	2.6
cb		5.7	2.5
+2		6.0	2.2
	1+00		
E		4.9	3.3
cb		5.3	2.9
+5		6.1	2.1
T.P.	5.41	8.30 9.79	5.35 2.89 4.38
	1+50		
E		4.6	3.7
cb		5.1	3.2
+5		5.8	2.5
	2+00		
E		4.6	3.7
cb		5.1	3.2
+5		5.6	2.7
	2+50		
E		4.5	3.8
cb		4.2	4.1
+5		5.2	3.1

2+88

E		4.4	3.9
cb		4.5	3.8
+1	PAR. gut	4.83	3.47
	5+00 SL FISH		
E		4.4	3.9
cb		4.6	3.7
+1	PAR. gut	4.80	3.50
	12' E of EL PAC SE Cor Ash - 5' old ash		
	end of { top cb	4.28	4.07
	Prop. RETURN { PAR	4.52	3.78
			to be removed
T.P.	5.31	9.73 4.78	3.88 4.42 5.91
	100' N of NL FISH		
E		5.0	4.7
cb	TOP cb	5.28	4.45
	gut PAR	5.86	3.87





9.73

9.40

140' N of Ash			
E Pav.	4.90	4.83	
cb "	5.40	4.33	
+2	5.7	4.0	
100' N of Ash			
E Pav.	5.0	4.7	
cb "	5.51	4.22	
+2	5.7	4.0	
203 N			
E	4.8	4.9	
cb + Pav. in Drive	5.57	4.16	
T.S. NEBP Pac Beech	4.43	5.30 5.79	
NEBP Pac + Ash	4.13	9.40	5.27
			1.52 0.93
100' N of Beech			
E Hedge Pav. Dr	4.18	5.22	cb
cb	4.77	4.63	E.
150' N			
E	3.9	5.5	
cb	4.1	5.3	
+3	4.6	4.8	
200 N			
E	3.4	6.0	

See P 45  
Mark Correction on or B.M.  
on 197 Top of

cb	3.8	5.6
+3	4.5	4.9
250 N		
E	3.8	5.6
cb	4.2	5.2
+2	4.9	4.5
300 N = 54 Cedar		
E	3.8	5.6
cb	4.4	5.0
+2	4.8	4.6
S cb line Cedar		
E	4.2	5.2
cb	4.6	4.8
NL Cedar = 0+00		
E	3.8	5.6
cb	4.5	4.9
+2	5.1	4.3
0+50		
E	4.3	5.1
cb	4.7	4.7
+3	5.5	3.9
1+00		
E	4.5	4.9
cb	5.2	4.2
+3	5.4	3.8

940

1750				
E		4.9	4.5	
cb		5.1	4.3	
+3		5.7	3.7	
2+0				
E		4.9	4.5	
cb		5.1	4.3	
+3		5.8	3.6	
T.P.	2.90	7.87	4.43	4.97
2+50				
E		3.5	4.4	
cb		3.9	4.0	
+3		4.4	3.5	
3+0				
E		3.8	4.1	
cb		4.1	3.8	
+3		4.6	3.3	
3+50				
E		3.7	4.2	
cb		4.2	3.7	
+3		4.9	3.0	
4+0				
E		3.8	4.1	
cb		4.3	3.6	
+3		4.9	3.0	

7.87

40

4+15				
cb end		4.31	3.56	
4+21 = SL E/M				
E				
cb Top		4.31	3.56	
+3		5.0	2.9	
N.L. E/M = 0+0				
E		3.8	4.1	
cb Top		4.18	3.69	
0+20				
E		3.8	4.1	
cb end		4.06	3.81	
0+50				
E		4.6	3.3	
cb		4.6	3.3	
+3		5.2	2.7	
1+0				
E		3.9	4.0	
cb		4.0	3.9	
+3		4.9	3.0	
T.P.	4.31	8.56	3.62	4.25
1+48.5				
E ground		4.4	4.2	
E sdw		3.87	4.69	

8.56

cb top	4.00	4.56
cb ground	4.5	4.1
+x	5.3	3.3

T.P.	5.66	10.81	3.41	5.15
check to SE BP	Pac. Grape	4.13	6.84	

NK Grape 1010

E	4.3	6.5
cb	4.5	6.3
+3	4.8	6.0

0+50

E	3.6	7.2
cb	4.1	6.7
+4	4.6	6.2

1+0

E	3.4	7.4
cb	3.7	7.1
+3	4.5	6.3

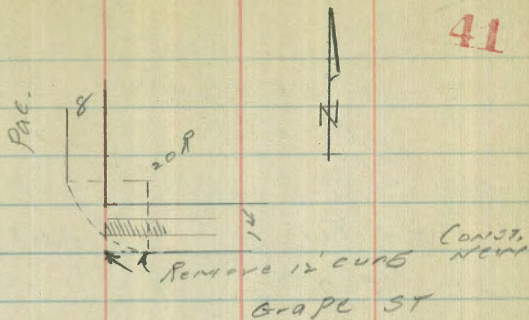
1+50

E	3.0	7.8
cb	3.1	7.7
+3	4.1	6.7

T.P.	4.57	14.00	1.38	9.43
------	------	-------	------	------

T.P.	3.45	13.37	4.08	9.92
------	------	-------	------	------

O.K.  
 4.44  
 4.44 = old  
 BTD  
 NEW BTD 8' E



41

13.37

65' S of SL JUNIPER

E	2.7	10.7
cb	3.4	10.0
+3	4.0	9.4

25' S of JUNIPER

E	2.6	10.8
cb	3.5	9.9
+3	3.9	9.5

6' S of SL J

E	2.8	10.6
cb Top end Ret	3.45	9.92
+2	3.5	9.9

SL JUNIPER

E	2.8	10.6
cb Top Ret	3.38	9.99
9+7 Pac	3.90	9.47

1337

101' N of NK Juniper

E	3.7	9.7
cb top	3.87	9.48
gut Pav	4.47	8.70
150 N		
E	4.3	9.1
cb	4.4	9.2
+3	5.0	8.4
2+0		
E	4.5	8.9
cb	4.5	8.9
+3	5.4	8.0
2+50		
E	5.0	8.4
cb	4.7	8.7
+3	5.5	7.9
3+0		
E	5.0	8.4
cb	5.4	8.0
+3	5.7	7.7
3+50		
E	4.9	8.5
cb	5.2	8.2
+3	6.0	7.4

1337

380 N

E	4.9	8.5
cb end	5.15	8.22
+1	5.7	7.7
400 N		
E	4.9	8.5
cb top	5.30	8.07
429 N		
E	4.5	8.5
cb top	5.54	7.85

T.P. 584 1338 5.93 7.44

479 N of Juniper

E	4.5	8.8
cb	5.6	7.7
528 N		
E	4.8	8.5
cb	5.8	7.5

2.45 10.83

+ 9.01  
19.8419.73  
0.11Harbor B.M. TOP Hyd  
S.E. Pac. Laurel

42

W cb of Pacific 7' wide  
Harasthy to Bean

1470

43

NEBP	470	1470	10.00	PAC Harasthy
	Sky Harasthy = 00			
W		4.7	10.00	
cb		4.74	9.96	
+ 1.0 QUT		5.37	9.33	
0+10				
W		4.7	10.00	
cb end Ret		4.82	9.88	
+1		5.15	9.55	
0+50				
W		4.8	9.9	
cb		4.7	10.0	
+1		5.0	9.7	
1+0				
W		4.4	10.3	
cb		4.5	10.2	
+1		4.8	9.9	
1+50				
W		4.3	10.4	
cb		4.4	10.3	
+1		4.7	10.0	
2+00				
W		4.4	10.3	
cb		4.7	10.0	
+1		4.8	9.9	

	2+50			
W		4.7	10.0	
cb		4.7	10.0	
+1		5.1	9.6	
	3+00 = NL EMO-4			
W		4.7	10.0	
cb		4.9	9.8	
+1		5.2	9.5	
	SL EMO-4 = 00			
W		5.2	9.5	
cb		5.3	9.4	
+1		5.6	9.1	
	0+53 = Nedge Dr. to oil STA			HC. Pav.
W		5.15	9.55	see p 45
cb + QUT		5.90	8.80	
	1+00			
W		5.14	9.56	
cb + QUT Pav.		6.15	8.55	
	1+50 S edge Pav. Dr.			
W Pav		5.47	9.23	
cb + QUT		6.42	8.28	
	2+00			✓
W		6.9	7.8	
cb		6.7	8.0	
	2+50			
W		7.0	7.7	

14.70

cb	6.8	7.9
2+97.8 NL Bean		
w	6.8	7.9
cb	6.6	8.1
+4.5 = Wedge Pav	6.50	8.20

E cb at Pac. Harasby to Bean  
200' S of Harasby

E	4.2	10.5
cb end	4.33	10.37
+1 = gut	4.8	9.9
250' S		
E	4.7	10.5
cb	4.6	10.1
+1	5.2	9.5
300 S ENL Emory		

E	4.1	10.6
cb	4.0	10.7
+v	5.1	9.6

SL Emory = 040

E	4.4	10.3
cb	4.9	9.8
+1	5.2	9.3

0+50

(W) E	4.6	10.1
cb	4.9	9.8
+1	5.5	9.2

14.70

44

1400		
E	4.7	10.0
cb	5.1	9.6
+1	5.8	8.9
1+50		
E	4.8	9.9
cb	5.4	9.3
+1	6.0	8.7

2+00

E	5.1	9.6
cb	5.4	9.3
+1	6.3	8.4

2+50

E	5.6	9.1
cb	5.3	9.4
+1	6.2	8.5

TP	257	1308	6.19	8.51
	2+97.8	NL Bean		

E	3.7	9.4
cb	4.6	8.5
+v	5.0	8.1

SL Bean = 0400

E	4.1	9.0
cb TOP	4.55	8.53

1308

0+06			
E	4.3	8.8	
cb TOP	4.57	8.51	
0+50			
E	4.3	8.8	
cb	4.41	8.67	
1+0			
E	4.4	8.7	
cb	4.38	8.70	
1+50			
E	4.2	8.9	
cb	4.25	8.83	
2+0			
E	3.9	9.2	
cb	4.10	8.98	
2+50			
E	3.9	9.2	
cb	3.93	9.15	
3+0			
E	3.6	9.5	
cb	3.80	9.28	
3+58			
E	3.6	9.3	
cb	3.72	9.36	

check Levels  
Broadway to Fl St.

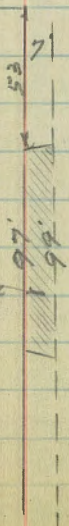
45

NWRP 000 910 4.68 Broadway Pacific  
 TP 554 896 568 300  
 check to Top Hyd BM 330 560  
 SE Cor Fl & Pacific

pac

EMORY

R.C. PAUL PATHE  
 to Oil STA.  
 see p 43



N

8-4-39 X Sec. Balboa Ave  
at. Rose Canyon Bridge

Miller  
Walker  
Bliss

Sections Taken parallel to N & S. Lines of  
Balboa Ave = " " Pavmt. & Bridge

B.M. Mon. 2.42 13.59 11.17

N. Line Balboa  
Sta 18+29.25  
E.P. 1471-P.10

100' N. of N. Line Balboa Ave

Station				
19+85		4.4	9.2	
20+12	W. Bank	5.4	8.2	
20+20	Main channel	11.6	2.0	
20+41	" "	14.5	- 0.9	
20+74	" "	13.2	0.4	
20+80		10.3	3.3	
21+05		9.5	4.1	
21+10		7.2	6.4	
21+33	side channel	11.1	2.5	
21+54		5.2	8.4	
21+75	E. Bank	3.1	10.5	

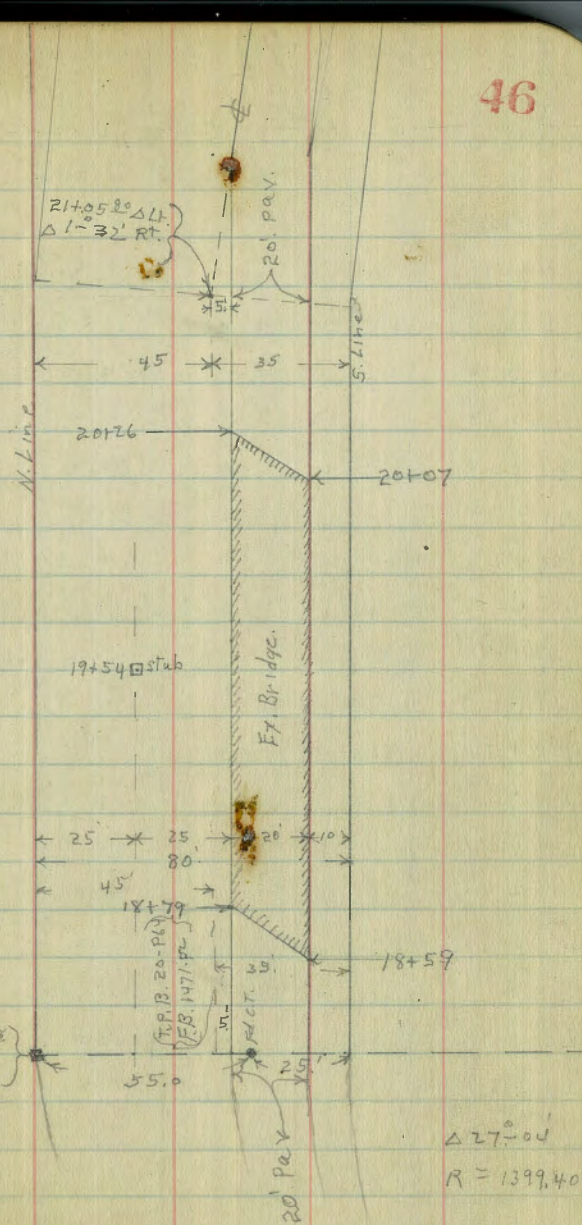
75' N. of N. Line

20+00		5.3	8.3	
20+12	W. Bank	5.5	8.1	
20+18	Main channel	14.0	-0.4	
20+74	" "	13.8	-0.2	
20+85		8.7	4.9	
21+04		5.6	8.0	
21+15	side channel	11.0	2.6	
21+25	" "	11.0	2.6	
21+35		5.2	8.4	
21+60	E. Bank	3.3	10.3	

Indexed  
C.S.K.

46

Fd. Mon. 18+29.25  
E.C. FB 1471-2





13.59

2152

12.27

Balboa Ave

47

T.P. 11.10 - 12.27 - 2.42 - 11.17

50' N of N. Line Balboa Ave

19+60		4.2	8.1	
19+70	W. Bank	4.2	8.1	
20+00	Main channel	13.6	-1.3	
20+70	" "	13.2	-0.9	
20+83		8.3	4.0	
21+00	side	10.4	1.9	S. end
21+13		6.8	5.5	
21+53	E. Bank	2.0	10.3	
	25' N of N. Line Balboa Ave			
19+40		3.2	9.1	
19+57	W. Bank	4.4	7.9	
19+76	Main channel	16.2	1.1	
19+90	" "	13.2	-0.9	
20+61	" "	13.5	-1.2	
21+05	E. Bank	3.0	9.3	
21+30		3.0	9.3	
	N. Line Balboa Ave			
18+29 <sup>38</sup>	E.C.	0.4	11.9	
18+59		1.1	11.2	
18+79		1.1	11.2	
19+35	W. Bank	4.0	8.3	
19+50	Main channel	13.0	-0.7	
19+80	" "	13.7	-1.4	
20+07		13.8	-1.5	

20+26

20+40

20+55 E. Bank

20+70

21+00

T.P.

6.05

17.22

22' S. of N. Line Balboa Ave

18+29<sup>38</sup> E.C.

18+59

18+79

18+84

18+98 W. Bank

19+05

19+20

19+80

19+93

20+07

20+26

20+33

20+36 E. Bank

20+50

20+70

30' S. of N. Line Balboa Ave

18+29<sup>38</sup> E.C.

18+59

18+79

18+84 W. Bank

13.9

14.0

5.1

2.0

2.0

1.10

4.7

4.1

5.4

6.4

8.0

15.0

18.3

19.0

17.0

14.0

14.5

14.3

10.3

7.0

5.3

4.5

3.9

5.4

6.4

-1.6

-1.7

7.2

10.3

10.3

11.17

12.5

13.1

11.8

10.8

9.2

2.2

-1.1

-1.8

0.2

-0.8

-1.3

2.9

6.9

10.2

11.9

12.7

13.3

11.8

10.8

18+85	15.4	1.8
19+05	18.5	-1.3
19+22	18.5	-1.3
19+80	19.0	-1.8
19+93	17.0	0.2
20+07	18.2	-1.0
20+26	18.5	-1.3
20+30	16.5	0.7
20+32 E Bank	8.5	8.7
20+50	7.0	10.2
20+70	5.4	11.8
T.P.	3.83	15.00
50' S. of N. Line Balboa Ave =	6.05	11.17
18+29 <sup>3x</sup> N. edge pav.	1.82	13.18
18+59 " " "	1.56	13.44
18+79 " " NW. Cor Bridge	1.63	13.37
18+80	16.6	-1.6
19+22	16.4	-1.4
20+07	16.6	-1.6
20+19	15.8	-0.8
20+25	8.2	6.8
20+26 NE. Cor Bridge	1.94	13.06
20+30	1.94	13.06
20+50	1.95	13.05
70' S. of N. Line =	1.87	13.13
20+50	1.87	13.13
20+26	1.85	13.15

20+07 S.E. Cor Bridge	1.86	13.14
20+26	9.0	6.0
19+94	9.3	5.7
19+87	15.6	-0.6
19+60	17.0	-2.0
19+10	16.4	-1.6
18+79	16.8	-1.8
18+60	14.2	0.8
18+59 { S. side Pav. S.W. Cor Bridge deck	1.70	13.30
18+29 <sup>2x</sup> E.P. S. Edge pav.	2.04	12.96
76' S. of N. Line		
18+29 <sup>3x</sup>	2.0	13.0
18+54	3.0	12.0
18+55	13.5	1.5
18+59	14.2	0.8
18+79	16.8	-1.8
19+10	16.6	-1.6
19+70	17.0	-2.0
19+85	15.5	-0.5
19+90	8.4	6.6
20+07	5.7	9.3
20+11	5.7	9.3
20+12	2.0	13.0
20+26	2.0	13.0
20+50	2.3	12.7

15.00

80' S. of N. Line = S. Line Balboa Ave

18+29 <sup>38</sup> E.C.	3.7	11.3
18+47	3.0	12.0
18+48	13.6	1.5
18+59	17.0	-2.0
19+10	12.8	-1.8
19+65	16.4	-1.4
19+77	8.4	6.6
20+07	5.7	9.3
20+12	5.0	10.0
20+26	4.8	10.2
20+50	4.6	10.4

8' S. of S. Line Balboa Ave

18+10	5.0	10.0
18+29 <sup>38</sup>	8.0	7.0
18+38	8.0	7.0
18+43	13.5	1.5
18+59	17.0	-2.0
19+10	17.0	-2.0
19+60	16.5	-1.5
19+70	8.6	6.4
20+07	5.8	9.2
20+12	5.0	10.0
20+26	4.8	10.2
20+50	5.0	10.0

15.00  
25' S. of S. Line Balboa Ave

49

17+50	9.2	5.8
18+00	9.0	6.0
18+07	12.4	2.6
18+28	13.6	1.4
18+35	19.0	-4.0
18+60	21.0	-6.0
19+26	17.6	-2.6
19+32	12.3	2.7
19+52	9.3	5.7
19+90	6.0	9.0

T.P. 13.98 18.52 20.46 4.54

50' S. of S. Line Balboa

17+25	9.0	9.5
17+60	8.8	9.7
17+70	12.5	6.0
18+00	13.2	5.3
18+05	15.6	2.9
18+20	18.2	0.3
18+29	19.9	-1.4
18+70	20.7	-2.2
18+99 E. side channel	20.9	-2.4
19+13	15.0	3.5
19+50	12.0	6.5
19+57	9.6	9.9

16.52  
100' s. of s. line Balboa Ave

16+50	2.4	9.1
17+00	2.8	8.7
17+08	13.0	5.5
17+53	14.8	3.7
17+60	19.5	-1.0
17+95	20.8	-2.3
18+25	26.5	-3.0

chk. BM

7.35 11.17

50

18.52

18+65	21.3	-2.8
18+74	15.4	3.1
18+98	9.2	9.3
18+50?	9.2	9.3

150' s. of s. line Balboa Ave

16+00	9.7	8.8
16+45	9.7	8.8
16+67	13.2	5.3
16+96	13.8	4.7
17+00	19.0	-0.5
17+70	21.7	-2.2
18+20	21.3	-2.8
18+24	18.5	0.0
18+30	12.5	6.0
18+50	9.2	9.3
19+00	9.2	9.3

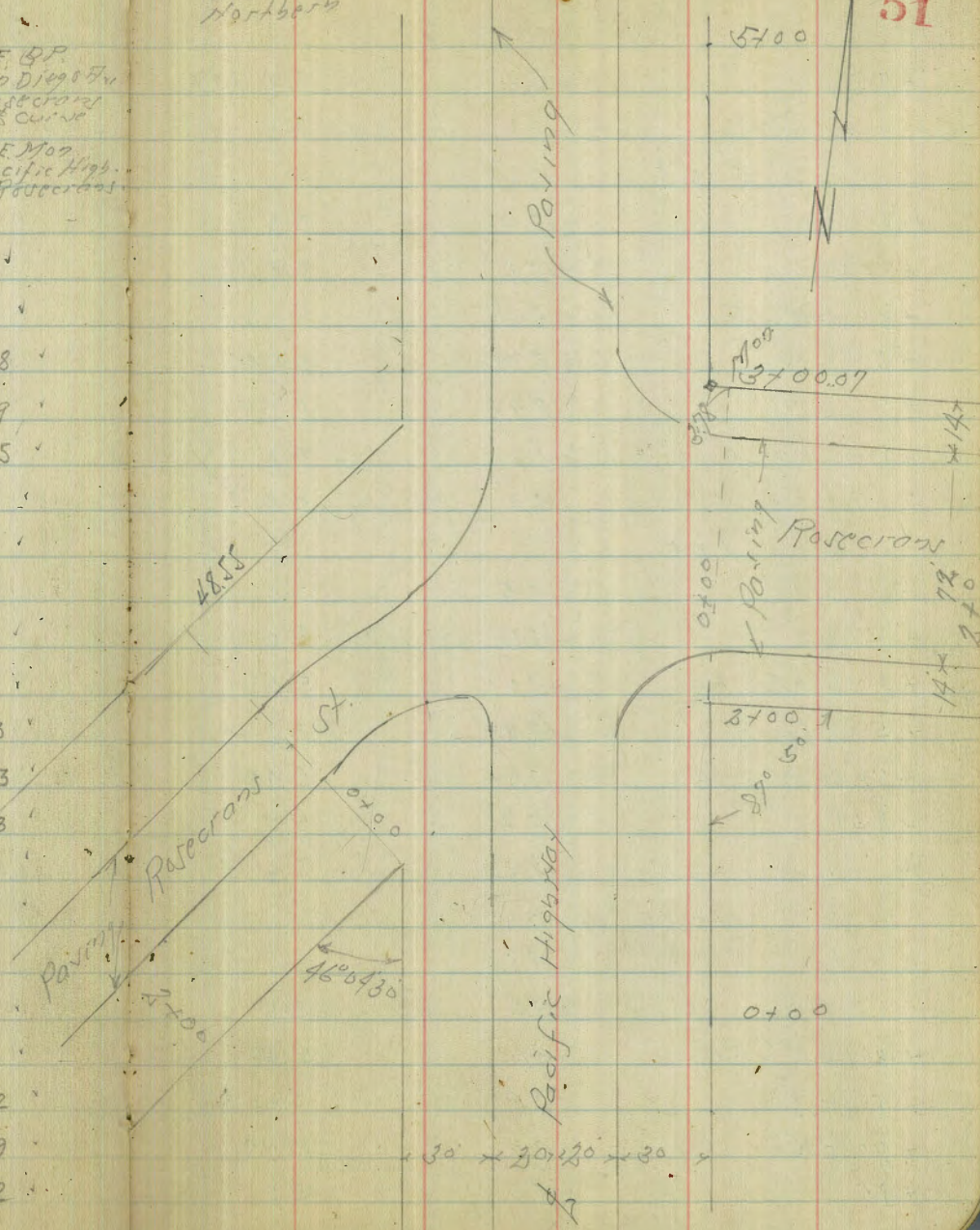
Pacific Highway Cross Section  
 200' So. Rosecrans to 200' N of Rosecrans

Oct 27 39  
 Sisson  
 Northern

Indexed  
 C.S.K.

B.M.	5.63	10.25	4.62	SE BP San Diego Av. Rosecrans & Curve
TP	4.73	8.53	6.75	3.80
		0+0		NE Mo. Pacific High. & Rosecrans
F		3.2	5.3	
+15		3.4	5.1	
+30 = Fly Pav.		2.95	5.58	
+50 = F		2.71	5.79	
+70 = Fly Pav		2.98	5.55	
+85		3.5	5.0	
+100 = F		3.2	5.3	
	0+25			
F		3.1	5.4	
+15		3.3	5.2	
+30 = Fly Pav		3.00	5.53	
+50 = F		2.73	5.83	
+70 Fly "		2.90	5.63	
+85		3.5	5.0	
F		3.4	5.1	
	0+50			
F		3.4	5.1	
+15		3.4	5.1	
+30 = Fly Pav		2.91	5.62	
+50 = F		2.74	5.79	
+70 = Fly Pav.		3.01	5.52	

Notes Reduced Oct 30-39  
 Plotted By C.B. Hough  
 from p 51-59



8.53

+85	3.3	5.2 ✓
W	3.0	5.5 ✓
0+75		
W	3.0	5.5 ✓
+15	3.2	5.3 ✓
+30 = Wly Pav	3.05	5.48 ✓
+50 = <del>z</del>	2.79	5.74 ✓
+70 = Fly "	2.94	5.59 ✓
+85	3.4	5.1 ✓
F	3.5	5.0 ✓
1+0		
F	3.5	5.0 ✓
+15	3.5	5.0 ✓
+30 = Fly Pav	3.00	5.53 ✓
+50 = <del>z</del>	2.82	5.71 ✓
+70 = Wly Pav	3.09	5.44 ✓
+85	3.4	5.1 ✓
W	2.9	5.6 ✓
1+25		
W	2.8	5.7 ✓
+15	3.4	5.1 ✓
+30 = Wly Pav	3.13	5.40 ✓
+50 = <del>z</del>	2.96	5.63 ✓
+70 = Fly Pav	3.09	5.44 ✓
+85	3.5	5.0 ✓

8.53

52

F	3.6	4.9 ✓
1+50		
F	3.3	5.2 ✓
+15	3.5	5.0 ✓
+30 = Fly Pav	3.21	5.32 ✓
+50 = <del>z</del>	3.02	5.51 ✓
+70 = Wly Pav	3.21	5.32 ✓
+85	3.3	5.2 ✓
W	3.2	5.3 ✓
1+75		
W	3.7	4.8 ✓
+15	3.6	4.9 ✓
+30 = Wly Edgt Pav	3.32	5.21 ✓
+50 = <del>z</del>	3.12	5.41 ✓
+70 = Fly " "	3.34	5.19 ✓
+85	3.5	5.0 ✓
F	3.3	5.2 ✓
2+0 = Sk. Pascegras From Fort		
F	3.6	4.9 ✓
+15	3.6	4.9 ✓
+30 = Fly Pav	3.46	5.07 ✓
+50 = <del>z</del>	3.22	5.31 ✓
+70 = Wly Pav	3.42	5.05 ✓
+85	3.6	4.9 ✓
W on Pav.	3.80	4.7 ✓

2+14

W	02 Pav	3.67	4.86 ✓
+15	" "	3.64	4.89 ✓
+30	" "	3.60	4.93 ✓
+50	" "	3.80	5.23 ✓
+70	" "	3.51	5.02 ✓
+85	" "	3.66	4.87 ✓
F	" "	3.66	4.87 ✓

2+32

F	02 Pav	3.77	4.76 ✓
+15	" "	3.82	4.71 ✓
+30	" "	3.63	4.90 ✓
+50	" "	3.40	5.13 ✓
+70	" "	3.66	4.87 ✓
+85	" "	3.67	4.86 ✓
W	" "	3.77	4.76 ✓

2+50

W	02 Pav	4.13	4.40 ✓
+15	" "	3.82	4.71 ✓
+30	" "	3.78	4.75 ✓
+50	" "	3.47	5.06 ✓
+70	" "	3.76	4.77 ✓
+85	" "	3.91	4.62 ✓
F	" "	3.94	4.59 ✓

2+68

F	02 Pav	4.12	4.41 ✓
+15	" "	3.96	4.57 ✓
+30	" "	3.83	4.70 ✓
+50	" "	3.57	4.96 ✓
+70	" "	3.91	4.62 ✓
+85	" "	4.31	4.22 ✓
W	Dirt	4.6	3.9 ✓

2+86

W		5.1	3.4 ✓
+15		4.6	3.9 ✓
+30	Wly Pav	4.01	4.52 ✓
+50		3.67	4.86 ✓
+70	Fly Pav	3.91	4.62 ✓
+85	02 Pav	4.10	4.43 ✓
F	" "	4.18	4.38 ✓

2+0

F		4.2	4.3 ✓
+15		4.2	4.3 ✓
+30	Fly Pav	3.98	4.55 ✓
+50		3.73	4.80 ✓
+70	Wly Pav	4.05	4.48 ✓
+85		4.8	3.7 ✓
W		5.3	3.2 ✓

8.53

3+25

H	5.2	3.3
+15	5.0	3.5
+30 = Wly Pav	4.18	4.35
+50 = <del>X</del>	3.86	4.67
+70 = Fly Pav	4.12	4.41
+85	3.9	4.6
+93	4.0	4.5
F	5.9	2.6

3+50

F	6.0	2.5
+9	6.0	2.5
+15	4.5	4.0
+30 = Fly Pav	4.25	4.28
+50 = <del>X</del>	3.98	4.55
+70 = Wly Pav	4.25	4.28
+85	5.0	3.5
H	5.0	3.5

3+75

H	4.9	3.6
+15	5.1	3.4
+30 = Wly Pav	4.34	4.19
+50 = <del>X</del>	4.12	4.41
+70 = Fly Pav	4.37	4.16
+85	5.2	3.3

8.53

54

+90	6.4	2.1
F	6.5	2.0
	4+0	
F	6.8	1.7
+9	6.8	1.7
+15	4.8	3.7
+30 = Fly Pav	4.51	4.02
+50 = <del>X</del>	4.23	4.30
+70 = Wly "	4.50	4.03
+85	5.2	3.3

H

	4.9	3.6
	4+25	
H	5.4	3.1
+15	5.3	3.2
+30 = Wly Pav	4.67	3.86
+50 = <del>X</del>	4.37	4.16
+70 = Fly "	4.65	3.88
+85	4.5	4.0
+90	6.6	1.9
F	6.8	1.7

4+50

F	6.8	1.7
+8	6.8	1.7
+15	5.2	3.3
+30 = Fly Pav	4.78	3.75



8.53

+50 = <del>Z</del>	4.51	4.02 ✓
+70 = Wly Pav	4.76	3.77 ✓
+85	5.6	2.9 ✓
W	5.8	2.7 ✓

4.75

W	6.0	2.5 ✓
+15	5.8	2.7 ✓
+30 = Wly Pav	4.90	3.63 ✓
+50 = <del>Z</del>	4.68	3.85 ✓
+70 = Fly Pav	4.93	3.60 ✓
+80	4.9	3.6 ✓
+90	6.4	2.1 ✓
F	6.3	2.2 ✓

5.40

F	6.8	1.7 ✓
+10	6.6	1.9 ✓
+20	5.1	3.4 ✓
+30 = Fly Pav	5.04	3.49 ✓
+50 = <del>Z</del>	4.81	3.72 ✓
+70 = Wly Pav	5.02	3.51 ✓
+85	5.8	2.7 ✓
W	6.0	2.5 ✓

Profile of Cross Section  
East Line Pacific Highway to 200 East

Inverted  
1/4"

100 wide  
12' Cb  
18' 1/4

8.53

8.53

0+0 = E.L. Pacific Highway 0 = South

0+25

N	4.0	4.5	✓
Cb = Sly Pav	4.17	4.36	✓
1/4	4.13	4.40	✓
1/2	3.95	4.58	✓
1/4	3.76	4.77	✓
Cb - Sly Pav	3.66	4.87	✓
S	3.6	4.9	✓

S	3.2	5.3	✓
Cb = Sly Pav	3.42	5.11	✓
1/4	3.25	5.28	✓
1/2	3.22	5.31	✓
1/4	3.41	5.12	✓
Cb - Sly Pav	3.70	4.83	✓
N	3.50	5.03	✓

0+25

1+0

S	3.3	5.2	✓
Cb = Sly Pav	3.62	4.91	✓
1/4	3.54	4.99	✓
1/2	3.63	4.90	✓
1/4	3.79	4.74	✓
Cb = Sly Pav	4.08	4.45	✓
N	3.9	4.6	✓

N	3.3	5.2	✓
Cb = Sly Pav	3.57	4.96	✓
1/4	3.32	5.21	✓
1/2	3.06	5.47	✓
1/4	3.14	5.39	✓
Cb = Sly Pav	3.29	5.24	✓
S	3.3	5.2	✓

0+50

1+25

N	3.7	4.8	✓
Cb = Sly Pav	3.88	4.65	✓
1/4	3.54	4.99	✓
1/2	3.38	5.15	✓
1/4	3.86	5.17	✓
Cb = Sly Pav	3.48	5.05	✓
S	3.3	5.2	✓

S	3.2	5.3	✓
Cb = Sly Pav	3.30	5.33	✓
1/4	3.04	5.49	✓
1/2	2.96	5.57	✓
1/4	3.18	5.35	✓
Cb = Sly Pav	3.44	5.09	✓
N	3.3	5.2	✓

8.53

1+50

N	31	5.4	✓
Cb = N/4 Pav	3.24	5.29	✓
1/4	2.98	5.55	✓
1/2	2.84	5.69	✓
1/4	2.90	5.63	✓
Cb = S/4 Pav	3.10	5.43	✓
S	2.9	5.6	✓

1+75

S	2.8	5.7	✓
Cb = S/4 Pav	2.94	5.59	✓
1/4	2.78	5.75	✓
1/2	2.71	5.82	✓
1/4	2.87	5.66	✓
Cb = N/4 Pav	3.14	5.39	✓
N	3.0	5.5	✓

2+0

N	2.9	5.6	✓
Cb = N/4 Pav	3.00	5.53	✓
1/4	2.76	5.77	✓
1/2	2.63	5.90	✓
1/4	2.64	5.89	✓
Cb = S/4 Pav	2.87	5.66	✓
S	2.9	5.6	✓

57

Rosecrans SWly of Pac.

Pacific Rosecrans 5.35 9.15 8.80 N.E. Man.

See R.B. 1449-8

00-48.55 - S.H. Congress to West

W	5.3	3.9 ✓
+15	5.4	3.3
+35 Pav	4.9	4.3 ✓
C "	4.5	4.7 ✓

0+00 = 1+17.58 in 1449-8. <sup>9/80</sup> 150v-17

(B) E	4.2	5.0 ✓
+15	4.6	4.6 ✓
+30 Pav	4.5	4.7 ✓
C "	4.28	4.87 ✓
+16 "	4.53	4.62 ✓
+35	5.1	4.1 ✓
(H) W	4.5	4.7 ✓

0+25

W	5.0	4.2 ✓
+15	4.9	4.3 ✓
+34 Pav	4.35	4.80 ✓
C "	4.12	5.03 ✓
+12 "	4.29	4.66 ✓
+30	4.4	4.8 ✓

Indexed LM

9.15

58

E	3.6	5.6 ✓
	0+50	
E	4.0	5.2 ✓
+20	4.5	4.7 ✓
+30 Pav	4.75	4.70 ✓
C "	4.08	5.07 ✓
+16 "	4.33	4.82 ✓
+35	4.7	4.5 ✓
W	4.8	4.4 ✓

0+75

W	5.0	4.2 ✓
+15	4.7	4.5 ✓
+34 P	4.4	4.8 ✓
C "	4.04	5.11 ✓
+16 "	4.32	4.83 ✓
+30	4.5	4.7 ✓
E	4.2	5.0 ✓

1400

E	4.3	4.9 ✓
+20	4.7	4.5 ✓
+34 P	4.23	4.92 ✓
C "	4.0	5.2 ✓
+17 "	4.34	4.81 ✓
+35	5.1	4.1 ✓
W	5.1	4.1 ✓

9.15

W	1 + 25	5.3	3.9 ✓
+ 15		5.1	4.1 ✓
+ 33	PAV	4.5	4.7 ✓
C	"	4.04	5.11 ✓
+ 14	"	4.10	5.05 ✓
+ 30		4.8	4.4 ✓
E		4.0	5.2 ✓

E	1 + 50	5.1	4.1 ✓
+ 10		4.1	5.1 ✓
+ 20		5.1	4.1 ✓
+ 34	PAV	4.20	4.95 ✓
C	"	4.08	5.07 ✓
+ 18	"	4.58	4.57 ✓
+ 35		5.2	4.0 ✓
W		5.4	3.8 ✓

W	1 + 75	5.2	4.0 ✓
+ 15		5.4	3.8 ✓
+ 32	PAV	4.63	4.52 ✓
C	"	4.12	5.03 ✓
+ 14	"	4.28	4.87 ✓
+ 20		5.2	4.0 ✓
+ 30		5.3	3.9 ✓
+ 40		4.1	5.1 ✓
E		5.0	4.2 ✓

9.15

E	2 + 00	5.1	4.1 ✓
+ 20		5.5	3.7 ✓
+ 33	PAV	4.35	4.80 ✓
C	"	4.12	5.03 ✓
+ 18	"	4.47	4.48 ✓
+ 35		5.4	3.6 ✓
W		5.1	4.1 ✓

pages 51 to 59 Reduced &amp; Plot. 10-30-29 G.B. Hough

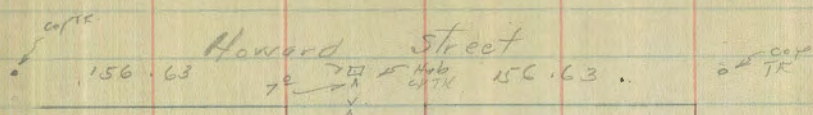
59

Bliss  
Tobell  
9/7/41

Cross Section Alley Block <sup>158</sup> ~~324~~  
Univ. of Ia. <sup>SEBP</sup>  
between 32<sup>nd</sup> & Iowa Polk - Howard <sup>322<sup>nd</sup> Polk</sup>

Indexed  
LM

B.M. 6.92 359.97 353.04 322.6K



Section in North Gutter of Polk

E-25 Topcb	5.30	354.67
" " Gutter	6.02	353.95
E-Line Gutter	5.71	354.26
" " Topcb	5.09	354.88
⊘	5.61	354.36
W Line Gutter	5.54	354.43
" " Topcb	4.82	355.15
WT 25 Topcb	4.64	355.33
" " " Gutter	5.30	354.67

Reduced & Plotted New Profile  
4-8-41 G.B.H.

0+00 N. Line of Polk St

W Topcb	4.72	355.25
Gutter	4.89	355.08
⊘	5.31	354.66
Gutter	5.05	354.92
E Topcb	4.86	355.11

0+10

E-5	4.4	355.6
E	4.8	355.2
+6	5.1	354.9
⊘	4.9	355.1
+4	5.0	355.0
W	4.2	355.8
WT Top concrete walk to W line of alley Walk 2.25 wide	4.04	355.93 ✓

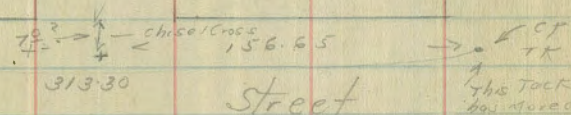
Zong



5 99.99 Tie Pt.

32<sup>nd</sup> St

W line of Iowa Polk



✓  
359.97

359.97

61

0+34

End Walk on West 1<sup>o</sup> Back 3.96 356.01 ✓

T.P. 6.55 363.52 3.00 356.97

0+44 Single Garage on West

1+54 SEnd 4 Car Garage on West

E on concrete floor 0.7 Back 3.61 356.36 ✓

SEnd 2.5 Back Concrete floor 6.22 357.30 ✓

0+50 Telephone Pole on East 0.7 in alley ✓  
<sup>0.9 dia East Edge</sup>

Edge of concrete Apron 0.5 in alley 6.27 357.25 ✓

W-5 4.2 355.8

1+56 Single Garage on East

W 4.1 355.9

Apron 0.3 Back 6.52 357.00 ✓

E 4.3 355.7

Bldg 3.0 Back Floor 3.63 359.89 ✓

E 4.1 355.9

1+90 NEnd 4 Car Garage on West

E+5 4.2 355.8

Edge of Apron 0.5 in alley 6.27 357.25 ✓

0+57 Single Garage on East

N-End 2.5 Back Concrete floor 6.13 357.39 ✓

E Board floor 0.10 in alley 4.10 355.87 ✓

1.5 Dia 1+97 Elec Pole on West W. Edge 0.3 in alley ✓

1+00 Gas 1/4" Pole <sup>W. Edge 1.0 in alley</sup> 1.2 Dia ✓

2+00 Pegin Wood Picket fence on West 0.3 in alley ✓

E-5 3.9 356.1

E-10 6.5 357.0

E 3.8 356.2

E 6.2 357.3

E 3.8 356.2

E 6.1 357.4

W 3.8 356.2

W 6.2 357.3

W+5 3.8 356.2

W+10 6.4 357.1

1+08 Single Garage on West ✓

E Dirt floor 3<sup>o</sup> Back 3.8 356.2

2+02 Telephone Pole on East <sup>0.9 diameter</sup> E. Edge on line ✓

1+50

W-5 3.0 357.0

2+50

W 2.7 357.3

W-10 5.1 358.4

E 3.1 356.9

W 5.6 357.9

E 3.2 356.8

E 5.9 357.6

E+10 3.2 356.8

36352

E	5.8	357.7
E+10	6.0	357.5
+25	6.3	357.2
2468. Single Garage on East		
concrete floor	2 <sup>nd</sup> Back	5.88 357.64 ✓
3100 Gas & Lt Pole on West W Edge 1.9 in alley 1.2 Dia ✓		
E-25	5.7	357.8
E-10	5.4	358.1
E	5.3	358.2
E	4.9	358.6
W	4.7	358.8
W+10	4.9	358.6
3117 on West. NEnd 0.5 in alley ✓ End Picket fence		
3130. Garage on West. Facing South 5.5 W of W line		
W line + 5.5 E of Garage. concrete floor	4.64	358.88 ✓
3150 Telephone Pole on East ✓ E Edge 0.3 East of line. 0.9 Dia		
W-10	4.7	358.8
W	4.7	358.8
E	4.7	358.8
E	4.8	358.7
+10	5.1	358.4
+25	5.2	358.3

36352

62

9100	Gas & Lt Pole on West W Edge 0.5 in alley 1.2 Dia ✓	4.7	358.8
		4.7	358.8
		4.7	358.8
		4.3	359.2
		4.1	359.4
		3.6	359.9
8.18	367.58	4.12	359.40
4120. on line. Redwood lathe fence ✓ Barn Fence on East			
4450. Fence is 0.3 in alley at this point			
		7.4	360.2
		7.4	360.2
		7.5	360.0
		7.7	359.9
		7.5	360.1
4450. Telephone Pole on East E Edge 1.2 in alley 0.8 Dia ✓			
4480 Guy to light Pole on West 1.5 in alley ✓			
5400 Gas & Lt Pole on West. W Edge 0.7 in alley 1.2 Dia ✓ Fence is 0.10 in alley at this point			
		6.8	360.8
		7.0	360.6
		6.9	360.7
		6.7	360.9
		6.7	360.9



367.58

5750

W-15	5.7	361.9
W	5.9	361.7
☿	5.7	361.9
E	5.5	362.1
E+10	5.6	362.0

5755

S. End 5 Car Garage on West  
concrete floors

E-10	4.0	363.6
E	4.9	362.7
☿	5.5	362.1
W on Ground	5.0	362.6
Apron 0.3 m alley	5.00	362.58 ✓
Floor 1.5 Back concrete	4.76	362.82 ✓

5756 Single Garage on East

19' Back. Dirt floor 3.5 364.1

5776 Telephone Pole on East side. East Edge 17" ✓  
0.8 Dia.

5795 North End 5 Car Garage on West ✓

E-5	3.6	364.0
E	4.0	363.6
☿	4.4	363.2
W on Ground	4.2	363.4
Apron 0.2 m alley	4.24	363.34 ✓
Floor 1.6 Back concrete	4.13	363.45 ✓

367.58

63

5799. 9<sup>th</sup> S. line of Howard.

W Top cb 9.9 from ☿	3.97	363.61
Gutter	4.4	363.2
☿	4.3	363.3
E Gutter	3.8	363.8
E Top cb 10' from ☿	3.42	364.16

Section in South Gutter of Howard

E-5 Top cb	3.58	364.00
E-5 Gutter	4.3	363.3
E on Top cb	3.63	363.95
E in Gutter	4.5	363.1
☿	4.8	362.8
W	5.0	362.6
W Top cb	4.26	363.32
W+5 Top cb	4.40	363.18
W+5 in Gutter	5.2	362.4

T.P. 2.15 360.08 9.65 357.93

7.05 353.03

353.04

= 0.07 error

Cross Section 60th St  
Boch Ave to Weaver

BM	12.10	173.81		16.171
TP	12.17	182.30	568	170.13
TP	12.19	194.26	0.23	182.07
TP	12.04	205.79	0.51	193.75
TP	12.30	218.04	0.05	205.74
TP	12.28	230.11	0.21	217.83
TP	11.53	241.07	0.57	229.54
BM			6.60	234.47
TP	11.80	252.26	0.61	240.46
TP	11.91	264.04	0.13	252.13
TP	12.14	275.87	0.31	262.73
BM			1.53	274.34
TP	11.34	286.98	0.23	275.64
BM			4.85	282.13

Indexecl  
LM

Net Height  
Imperial  
Merlin  
Top of  
Merlin  
7000

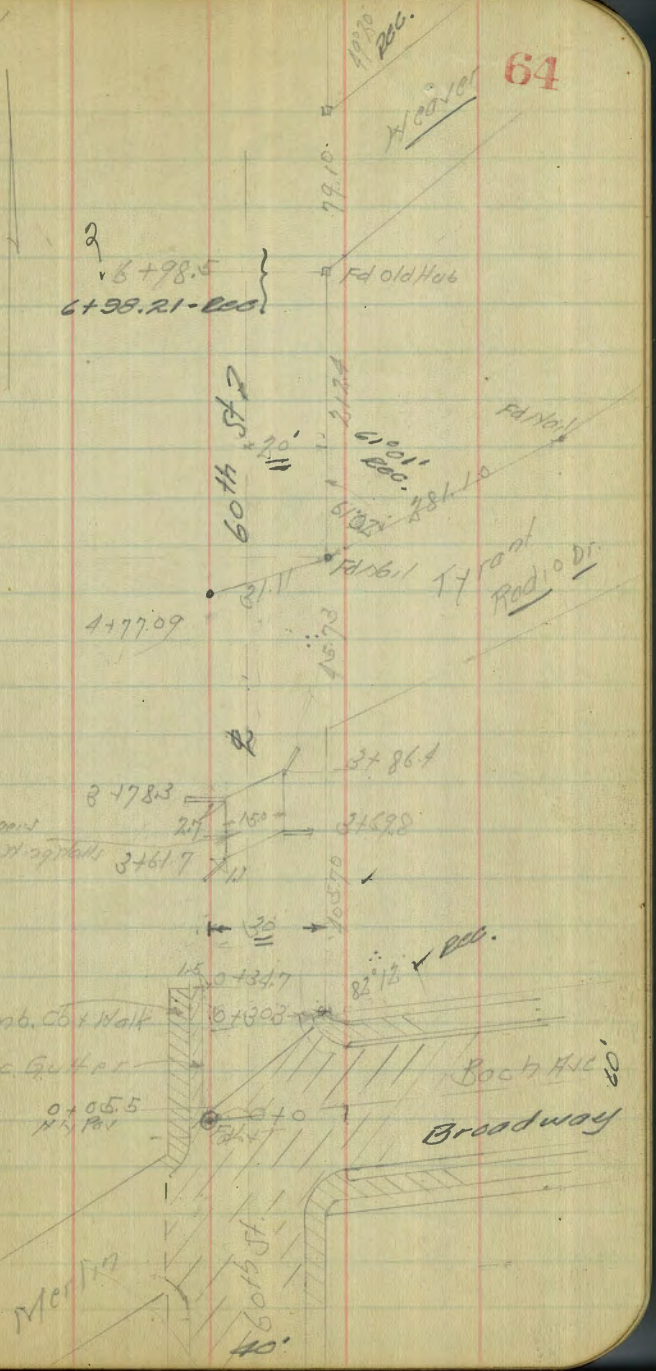
1st 7  
Brooklyn  
with 60th St

1st 7  
Merlin  
with 60th St

5' BP  
Boch Ave

May 12 1941  
Sussor  
North 7th  
H. Wood  
N. H. Albin

12" x 12 Caps  
10-4" x 16" Stairs  
4" Plank Deck + 2" supports  
Pile + Frame  
Trestle



64

Cross Sect 107 60th St  
Back to Weaver  
Brookings

1+0  
TP 0.37 273.16 11.94 272.79  
0+75  
0+50 19' R of L = FH Tol Pole  
0+46  
0+34.7 = 14' Conc Gutter + Conc Ch + Walk  
0+30  
0+0  
BM 2.60 284.70 282.13

Notes Red Plot 5-14-41 C.B.H.

SFBP  
Back to 60th St

L+ = 28      L      R1 = 5      **65**

267.4 5.8 8.5	269.5 5.7 2.0	270.5 3.6 1.3	267.9 5.3 2.0	268.8 4.4 5	<del>269.0</del> 4.3 7	265.5 7.7	273.0 0.2 1.5	274.0 4.8 2.0
273.9 10.8 6.0	274.1 10.6 2.0	273.6 11.1 1.0	272.4 13.3 1.0	<del>272.5</del> 11.6 5	<del>273.3</del> 11.2 8	270.6 19.1	275.6 9.1 1.5	276.7 8.0 2.0
278.1 6.6 3.0	276.7 6.0 2.0	278.6 6.1 1.5	277.7 7.8 2.0	277.9 6.8 3	<del>278.7</del> 6.0 8	277.1 7.6	278.9 5.8 1.5	279.1 5.6 2.0
281.8 2.9 2.0	281.71 3.02 15.5	280.91 2.86 1.5	281.11 3.62 1.5	<del>282.0</del> 4.6 5.0	280.1 4.6 5.0			
281.9 2.8 2.0	281.84 3.89 15.5	281.02 3.71 15.5	281.23 3.50 11.5	<del>282.9</del> 4.1 2.0	280.6 4.1 5	280.6 4.1 5	281.2 4.5 10	280.37 4.36 11.7
282.6 3.1 2.0	282.55 3.18 15.5	281.71 3.03 15.5	<del>281.6</del> 3.27 10	281.46 3.27 5	<del>281.4</del> 3.24 2.0	281.39 3.24 2.0		

2+50

2+25

TP 0.52 250.00 12.26 249.48

2+0

1+95

1+50

TP 0.45 261.74 11.87 261.29

1+25

27216

L+

L

R+

66

240.3

9.7  
35

242.1

7.9  
30

243.3

6.7  
30

243.7

6.3  
30

~~243.7~~  
243.7

6.3  
30

242.4

7.6  
30

245.2

4.8  
30

245.6

4.1  
30

246.7

3.0  
30

242.0

8.0  
35

244.4

5.6  
30

245.6

4.4  
14

249.3

3.7  
30

247.2

2.8  
6

~~247.7~~  
247.9

3.1  
7

243.7

6.5  
13

243.6

1.4  
18

249.0

1.2  
33

249.9

3.0  
30

250.00

244.0

1.7  
35

247.1

1.6  
30

~~249.8~~  
251.2

1.6  
9

251.6

1.1  
10

~~251.7~~  
251.7

1.0  
8

250.2

1.5  
8

248.2

1.5  
13

252.1

2.1  
33

253.3

2.4  
30

247.7

1.4  
35

250.7

1.0  
30

~~255.3~~  
255.3

1.4  
9

255.5

1.2  
6

~~255.9~~  
255.9

1.8  
6

254.0

7.7  
10

256.0

5.7  
14

256.6

5.1  
33

250.1

1.6  
40

258.2

3.5  
20

258.9

2.8  
15

259.4

2.2  
11

~~259.5~~  
260.6

1.1  
10

~~260.1~~  
260.0

1.7  
8

256.6

5.1  
9

262.1

7.4  
14

264.5

7.2  
33

261.74

260.7

1.5  
35

263.9

9.2  
20

265.1

8.1  
13

263.4

9.8  
10

263.9

9.3  
10

~~264.3~~  
264.4

8.8  
5

261.1

12.1  
9

263.0

5.7  
13

267.4

7.8  
30

27216

TP 912 24591 518 236.79

3+698

3+50

3+25

TP 364 24197 1167 238.33

3+10

3+85 = 5/4 18" Steel Pipe

3+75

250.00

236.75 ~~236.8~~ 236.8 228.51 228.7 222A 227.8

5.22 (5) 5.2 13.46 13.2 19.6 14.2  
8.10 9.1 11.3 11.18 20 28.4 35  
100' Pip 100' Pip

218.5 219.2 229.4 232.0 ~~234.4~~ 236.6 237.1 ~~237.0~~ 237.0 234.6 230.7 233.8 233.8

235 22.5 22.8 12.6 10.0 5.2 4.9 5.0 7.4 11.3 8.7 8.7  
30 17 Ground 17.5 13 10 9 13 20 28 35  
S.W. End Plank

227.9 228.9 231.3 231.8 ~~235.7~~ 237.7 237.7 236.0 236.2 237.3

14.1 13.1 10.7 10.2 4.6 4.3 4.3 6.0 5.8 4.7  
35 35 20 17 10 7 7 13 20 30

341.97

232.4 235.0 236.0 ~~237.9~~ 238.6 238.9 ~~239.0~~ 239.0 238.3 240.0 240.4

17.6 15.0 14.0 16.4 11.1 14.0 11.7 18.0 9.6  
35 20 13 10 7 7 13 20 30

238.14

11.26  
10.5 = F.L. 18" Steel Pipe

236.4 239.3 240.5 240.7 ~~240.9~~ 241.0 238.8 243.0 243.2 243.6

13.8 10.7 9.5 9.0 9.0 11.2 7.0 6.8 6.4  
35 20 10 7 7 10 15 20 30

250.00

TP 11.63 257.04 0.550 245.41

BM 2154 243.37

N 2 Nov 96  
60th Radio  
215.39  
Hills

4+77

246.8	246.3	242.5	240.2	239.8	<del>239.8</del> 239.8	238.6	238.4	238.2
10.9 30	7.04 30	3.4 30	5.9 30	6.1 30	6.1 30	7.2 15	7.5 30	7.7 30

4+60

243.3	237.0	<del>237.1</del> 237.2	<del>237.1</del> 237.1	237.5
2.6 38	8.9 20	8.7 10	8.8 10	8.4 25

4+80

234.9	235.3	235.8	236.4	<del>236.4</del> 236.4	233.9	231.1	222.4	221.9
11.0 40	10.6 20	10.1 10	9.5 30	9.5 8	12.0 15	14.8 30	15.5 37	16.0 30

4+0

233.6	233.9	235.8	236.1	<del>235.9</del> 235.8	227.1	225.3	220.6	221.9
12.3 40	12.0 30	10.1 10	9.8 30	10.1 8	18.8 15	20.6 30	25.6 35	24.0 30

3+78.3

227.9	220.3	219.9	219.9	236.7	236.7	<del>236.7</del> 219.7	220.3	224.9
18.0 20	25.5 37	26.0 20	26.0 10	9.2 70	9.2 10	26.3 10	25.6 20	21.0 30

245.91

245.91

6425

TP 11.79 291.41 0.40 279.62

640

TP 12.06 280.02 0.41 267.96

5475

5450

TP 11.69 268.37 0.36 256.68

5425

4194

17.1 RT of 2 - Fly Tail Pk

257.04

4

2

RT

69

284.6 283.2 281.8 280.8 280.6 ~~280.6~~ 280.6 280.4 279.2  
 6.8 8.2 9.6 10.6 10.8 10.8 11.0 12.2  
 30 20 10 7 10 10 20 30

278.8 272.8 276.2 ~~279.8~~ 272.4 271.7 ~~271.4~~ 271.3 272.0 271.8 271.7 270.0  
 1.2 2.2 3.8 7.6 8.2 8.7 8.0 8.2 8.2 10.0  
 30 20 15 10 15 8 10 15 20 30

272.8 271.2 269.6 ~~267.9~~ 265.0 264.3 ~~264.8~~ 265.1 265.0 263.7 262.1  
 4.4 4.2 4.2 3.4 4.1 3.3 3.4 4.7 6.3  
 30 20 14 10 15 8 14 20 30

265.0 263.4 261.4 ~~260.3~~ 259.1 258.5 ~~258.4~~ 258.4 258.7 257.4 256.4  
 3.4 5.0 7.0 9.3 9.9 10.0 9.7 11.0 12.2  
 30 20 15 10 15 9 10 20 30

258.7 257.3 255.9 ~~254.1~~ 251.9 251.8 ~~251.6~~ 251.3 252.0 251.2 249.8  
 4.7 4.0 1.1 5.1 5.2 5.9 5.0 5.8 7.2  
 30 20 14 10 15 10 14 20 30

250.7 249.5 249.1 ~~246.8~~ 245.4 244.3 ~~244.0~~ 243.8 244.6 242.7 240.7  
 6.2 7.5 7.9 11.6 12.7 12.2 12.4 14.2 16.3  
 30 20 15 10 15 8 11 20 30

257.04

8+50

TP 11.41 313.13 1.41 306.72

8+0

7+50

7+0

6+75 13.2 R/0/2 - Fly Tel Polk

TP 11.85 303.13 0.13 291.28

6+50

291.41

Lt

Z

R1

70

301.5 302.0 302.7 302.9 303.1 303.2 303.7 303.7 303.9

11.6 11.1 10.6 10.7 9.9 9.4 9.4 9.2  
30 20 30 10 10 15 30 30

312.13

299.8 300.1 300.6 300.6 300.7 300.7 300.7

3.8 3.0 3.5 2.5 2.4 2.4 2.4  
30 20 30 10 30 30 30

298.7 298.9 299.2 299.1 299.0 298.9 298.6 298.1

4.4 4.2 3.9 4.0 4.2 4.5 5.0  
30 30 30 10 10 30 30

296.6 296.8 295.7 295.4 295.5 294.7 293.1

5.5 6.2 7.4 7.7 7.6 8.4 10.0  
30 30 30 10 10 30 30

293.6 293.4 293.2 292.2 292.1 292.6 291.3 289.9

9.5 9.7 9.9 10.2 11.0 10.5 11.8 13.2  
30 20 15 30 10 8 30 30

303.13

289.7 289.1 287.8 287.1 287.5 287.8 286.8 286.0

1.7 2.2 3.6 4.3 3.6 4.6 5.1  
30 20 30 10 10 30 30

291.41



6076 St.

11+0

TP

8.01 331.53 0.8° 323.52

10+50

10+0

TP

11.97 324.32 0.78 312.35

9+50

BM

2.34 309.79

Nail Pole  
12 ft  
9+23

9+23 1/2 Pt of 2 = Fly Tail Pole.

9+0

312.13

Lt

Z

Pt

71

322.5

323.9

325.4

326.6

327.3  
327.9

329.4

330.3

90  
3076  
2061  
1049  
536  
1021  
2018  
30

331.53

317.9

319.1

320.3

321.3

321.6  
321.8

323.1

324.3

64  
3052  
2040  
1030  
525  
1012  
209  
30

312.9

314.0

314.8

315.7

316.0  
316.3

316.5

317.0

317.5

114  
30103  
2095  
1086  
580  
1078  
1672  
2068  
30

324.32

307.9

309.0

310.1

310.5

310.6  
310.6

311.1

311.6

312.4

57  
3046  
2038  
1026  
525  
1020  
1115  
209  
30

303.9

304.7

305.5

306.1

306.6  
306.6

307.1

307.3

307.9

97  
3084  
2076  
1070  
565  
1060  
1358  
2052  
30

313.13

# Cross Section Alley Block 45

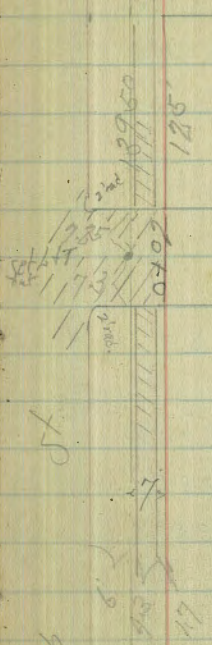
Normal Heights North + South Alley

BM	Elev	Dist	Notes
BM	415	389.95	385.78 S.E.B.P. Adams Cherokim
TP	4.00	388.77	5.16 384.77
TP	8.42	394.87	2.32 386.45
0-12-H.C. Line Modico			
E	on Pav	8.46	386.41
L	"	8.22	386.65
H	"	8.09	386.78
0+0-H.C. Modico			
H	cb Top	7.33	387.54
H	Gutter on Pav	7.45	387.42
L	"	7.65	387.22
E	Gutter	7.76	387.11
E	cb Top	7.67	387.20
0+08			
-10		5.3	389.6
L		5.6	389.3
L		5.9	389.0
H		5.8	389.1
+10		5.5	389.4
0+15			
E-25'	L Do Sprague	6.0	388.9 ✓
0+17			
-10		5.5	389.4
H		5.4	389.5

Red. 8 Plot. 9-4-41 C.B.H.

Indexed LM

FdLHT



Adams

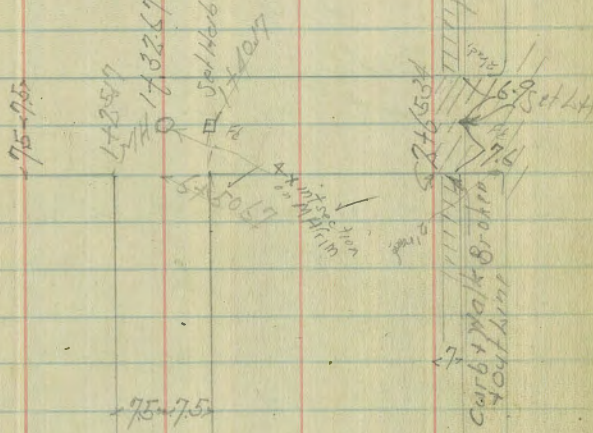
Aug. 30-41 72

Sisson  
North + South  
W. Main

Ave

FdLHT

## Block 43 Normal Hts



75-75

Curb + Walk Brokers  
Gutter line

Cherokee

125

139.73

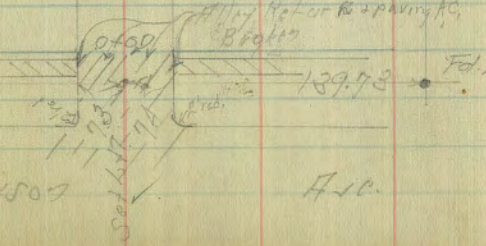
FdLHT

Madison

Ave

139.73

FdLHT



394.87

Z		5.0	389.9
F		5.0	389.9
+1.5 = S.W. Cor Garage		5.3	389.6 ✓
	Dirt Floor & Entrance		
	0+95		
✓ W+0.1 = Wly Power Pole			
TP	4.28	394.01	5.14 389.73
	0+92		
E-32.5 = Garage Conc Floor	4.82		389.19 ✓
	1+0		
-10		4.6	389.4
F		4.4	389.6
Z		4.4	389.6
H		4.5	389.5
✓ +1 = Sly Wire Fence			
+10		4.5	389.5
	1+50		
-10		4.6	389.4
✓ -1 = Wly Wire Fence			
-1 = Sly Picket Fence			
H		4.7	389.3
Z		4.7	389.3
F		4.6	389.4
+2		5.2	388.8
+10		5.4	388.6

394.01

73

		2+0	
		5.3	388.7
		4.6	389.4
		4.7	389.3
✓ +7.1 = Wly Power Pole			
H		4.7	389.3
✓ +0.6 = Wly Picket Fence			
+10		4.7	389.3
	2+04 - Z 7' 2" Ribbon Conc Dr. 0.2 F		
E-0.5 = Wly Dr		4.54	389.47 ✓
E-10 = Dr		4.88	389.13 ✓
	2+02		
W-15 = Garage Conc Floor		4.55	389.46 ✓
	2+28		
-10		4.8	389.2
H		5.0	389.0
Z		5.0	389.0
F		4.9	389.1
+0.9 = S.W. Cor Garage Conc Floor		4.87	389.14 ✓
	South Entrance		
	2+40		
W-12 = Garage Conc Floor		4.45	389.56 ✓
	2+57		
-10		4.8	389.2
F		4.6	389.4

394.01

$\frac{1}{2}$		4.8	389.2
$\frac{1}{2}$		4.7	389.3
+1	S E Cor Garage Conc Floor South Portico	4.47	389.54 ✓
	2+75		
✓	+0.2 = Sky Lath Fence		
TP	4.75	394.00	4.76 389.25
	2+84		
W-15	Garage Conc Floor	4.27	389.73 ✓
	3+0		
-10		4.3	389.7
✓	+0.2 = Sky Lath Fence Sky Wire	4.6	389.4
$\frac{1}{2}$		4.8	389.2
F		4.7	389.3
✓	+0.5 = Sky Board Fence		
	+10	5.3	388.7
	3+33		
W-09	Fly 2 Conc Wall Landing	4.01	389.99
	3+38		
W+0.4	Wire Fence Sky Lath House		
	3+49		
✓	-0.1 = Board Fence		
F		4.8	389.2
$\frac{1}{2}$		5.0	389.0
✓	+6.4 = Fly Pox or Pale Wire Fence		
✓	+7.1 = Fly Lath House		
W		4.7	389.3

394.00

+10		4.5	389.5
		4+0	
-10		5.1	388.9
W		5.0	389.0
✓	+0.1 = Sky Wire Fence Sky Board		
$\frac{1}{2}$		5.1	388.9
✓	+7.2 = Fly Board Fence		
F		5.0	389.0
+10		5.5	388.5
		4+49	
✓	F = Sky Wire Fence		
		4+50	
-10		5.4	388.6
F		5.5	388.5
$\frac{1}{2}$		5.5	388.5
W		5.3	388.7
✓	+0.1 = Fly Board Fence		
		4+51	
✓	W+0.4 = Fly Pox or Pale		
W-0.1	Sky Board Fence		
		4+81	
✓	W-0.2 = Fly Board Fence Sky Lath House		
		4+97	
✓	F-0.2 = Fly Wire Fence		

39400

540

✓ - 2' = 1/2 Sbed + Board Fence

✓ - 0.2 = 1/4 Lat + Hour

W 50 389.0

Z 5.6 388.4

F 5.7 388.3

+10 61 387.9

5434

✓ W - 1.4 = 1/4 Sbed + Board Fence

TP 408 392.24 5.84 388.16

5442

W - 6.0 = 1/2 Do. Garage Cor. Floor 341 388.83 ✓

5450

-10 4.7 387.5

F 4.7 387.5

Z 4.6 387.6

W 4.0 388.2

✓ +0.5 = 1/4 Paper Pole

+10 3.5 388.7

5457

W - 30.1 = 1/2 Garage Cor. Floor 305 389.19 ✓

640

-10 4.0 388.2

✓ - 2.2 = 1/4 Picket Fence

W 4.4 387.8

75

39224

Z

4.8 387.4

F

4.9 387.3

+10

5.4 386.8

6425

-10

5.4 386.8

F

5.0 387.2

Z

5.1 387.1

W

4.8 387.4

+10

4.5 387.7

6448

✓ W = 1/4 Paper Pole

6450.67.84. F + W + H

✓ - 1.0 = 1/4 Picket Fence

W

4.6 387.6

Z

4.8 387.4

F

4.9 387.3

TP

5.50 394.33 3.41 388.83

Cross Section East + West Alley  
Block 43 Normal Heights

394.33 Ft. Ford

394.33

0+66

0-12 = F Cb Line 36" Ht

S on Pavine	6.66	387.67
L " "	6.71	387.62
B " "	6.61	387.72

-10	5.6	388.7
S	5.6	388.7
L	5.5	388.8
H	5.5	388.8

✓ -0.8 = 2 3.5 Cypress Hedge

H Cb Top	6.10	388.23
H Gutter on Pavine	6.25	387.98
L " "	6.29	388.04
S Gutter " "	6.18	388.15
S Cb Top	5.93	388.20

+7.5 = 2 Dr. Garage Concrete Floor 5.40 388.93 ✓  
0+78

0+15

-10	5.2	389.1
S	5.3	389.0
L	5.4	388.9
H	5.4	388.9

H-0.5 = 2 3 Cypress Hedge Wly

1+0

-10	6.6	387.6
H	6.1	388.2
L	6.2	388.1
S	6.3	388.0
+10	6.2	388.1

0+50

H	5.4	388.9
L	5.5	388.8
S	5.6	388.7
+5	5.6	388.7

1+04  
H = Fly 2 3 Cypress Hedge  
H-1.0 = Wly Wire Fence  
1+24

0+52

✓ H = 2 3.5 Cypress Hedge

0+64

✓ S-0.8 = Wly Picket Fence

✓ S = Fly Picket Fence

1+25.17 = W.L. H.C. Alley

S	6.6	387.7
L	6.8	387.5
+6 = Wly Power Pole		
H	7.3	387.0
+10	7.5	386.8

394.33

1740.17 = Elk N + S Hill

-10		7.2	387.0
N		7.3	387.0
L		7.0	387.3
S		7.1	387.2
TP	362	391.53	6.42 387.91

1753

S-1.5 = Nly 2' Hedge

1757

N-1.8 = Fly Wire Fence

1777

-10		5.0	386.5
S		4.8	386.7
L		4.8	386.7
N	= Nly Conc Apron	4.92	386.61
+9'	= Nly 3' Garage Conc Floor	5.07	386.46

2106

-9' = Fly 3' Garage Conc Floor 5.08 386.45

N = Fly Conc Apron 5.12 386.41

L 4.9 386.6

S 4.8 386.7

+10 5.2 386.3

2121

S-1.0 = L + Fly 2' Hedge

S-0.2 = Nly Picket Fence

391.53

2145

-10		5.4	386.1
S		5.4	386.1
L		5.4	386.1
N		5.5	386.0
+10		6.0	385.5

2165.34 = Nly Character

N	ObTop	5.76	385.77
N	Gutter on Pav	5.82	385.71
L	" "	6.06	385.47
S	Gutter " "	6.00	385.53
S	ObTop	5.84	385.69

2177.34 = Nly 2' 1" Character

S	07 Pav	6.50	385.03
L	" "	6.44	385.09
N	" "	6.40	385.13
BM		5.77	385.76

SEBP  
Floor +  
Character  
385.78

78





DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder  
stake far any width roadway, slope 1 1/2 to 1.  
If ground is nearly level, the cut or fill at side  
stake is located by the double entry method in  
left column and top row. The number in both

IMPROVED TABLES  
AND  
INFORMATION

TABLE No. 2.  
To find Tangent and External for curve of  
any other degree, divide by degree of curve and  
add correction found in column of corrections.  
Degree of curve with a given L may be found  
by dividing tangent (or external) by  
given tangent (or external).  
The distance from a point on the tangent to  
the curve is very nearly the square of the tangent  
length divided by twice the radius.

129.40 H.I.  
 - 12.54  
 116.66 ✓ F  
 + 1.84  
 118.50 ✓ H.I.  
 - 13.16  
 105.34 ✓  
 + 0.53  
 105.87 ✓  
 - 8.66  
 97.21 ✓  
 + 2.42  
 99.63 ✓  
 - 12.44  
 87.19 ✓  
 + 0.74  
 87.93 ✓  
 - 12.13  
 75.80 ✓  
 + 6.19  
 81.99  
 - 11.78  
 70.21 ✓  
 + 0.11  
 70.32 ✓  
 - 8.77  
 61.55 ✓  
 + 2.18  
 63.73 ✓  
 - 10.00  
 53.73 ✓  
 + 9.55  
 63.28  
 - 6.15  
 57.13

55.57

24.99 91.10 131.46 ✓  
 + 3.26 14.92 13.16  
 28.25 × 103.52 ✓ 118.30 ✓  
 - 3.53 0.00 + 0.48  
 24.72 × 103.5 ✓ 118.78 ✓  
 + 11.41 + 14.22 ✓  
 36.13 × 115.74 ✓ 118.30 ✓ 20407  
 - 0.15 14.77 + 8.44  
 35.98 × 102.97 ✓ 126.74 ✓ 18459  
 + 12.00 7.94 - 12.10 ✓  
 47.98 × 110.91 ✓ 114.64 ✓  
 - 4.34 - 3.92 + 0.38  
 43.64 × 106.99 ✓ 115.02 ✓ 30  
 0.46 + 7.59 13.14 ✓ 29  
 44.10 × 114.58 ✓ 104.60 ✓ 51  
 - 3.44 - 4.00 92.8 ✓ 29  
 40.66 × 110.58 ✓ 92.8 ✓ 80  
 + 6.61 6.86 104.2 ✓  
 47.27 × 117.44 ✓ 117.6 ✓  
 - 3.17 - 1.28 4.9 ✓  
 50.44 ✓ 116.16 ✓ 2.52 ✓  
 + 10.42 + 12.46 ✓ 11.38 ✓  
 60.86 ✓ 128.62 ✓ 11.46 ✓  
 - 5.47 + 0.87 13.84 ✓  
 55.39 ✓ 129.49 ✓ 6.48 ✓  
 + 12.12 + 13.11 ✓ 36 ✓  
 67.51 ✓ 142.60 ✓ 80 ✓  
 0.87 - 1.27 22 ✓  
 66.64 ✓ 141.33 ✓  
 71.85 ✓ + 1.35 ✓  
 78.49 ✓ 142.68 ✓  
 0.26 - 11.41 ✓  
 78.23 ✓ 131.27 ✓  
 130.00 ✓ + 0.19 ✓  
 91.23 ✓ 131.46 ✓  
 - 0.13 ✓

ENGINEERING DEPARTMENT,  
 CITY OF CALIFORNIA.

20407  
 18459  
 30  
 29  
 51  
 29  
 80  
 1829  
 178  
 2097