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ENGINEERING DEPARTMENT,
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CALIFORNIA.

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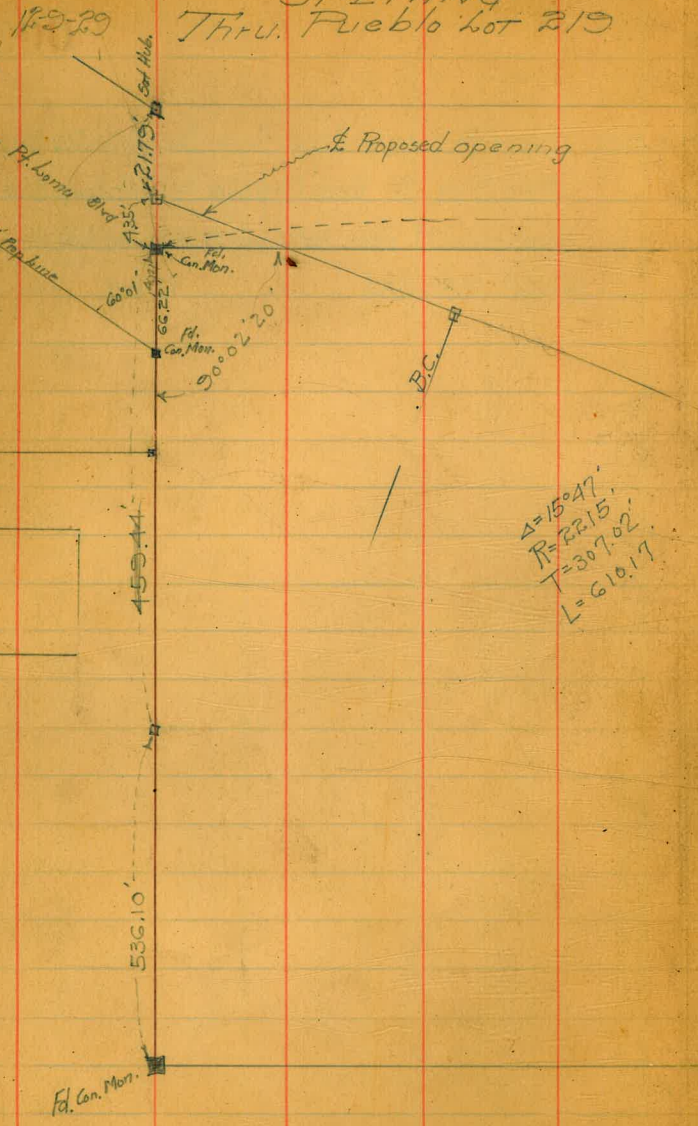
This notebook fully equipped with

0001

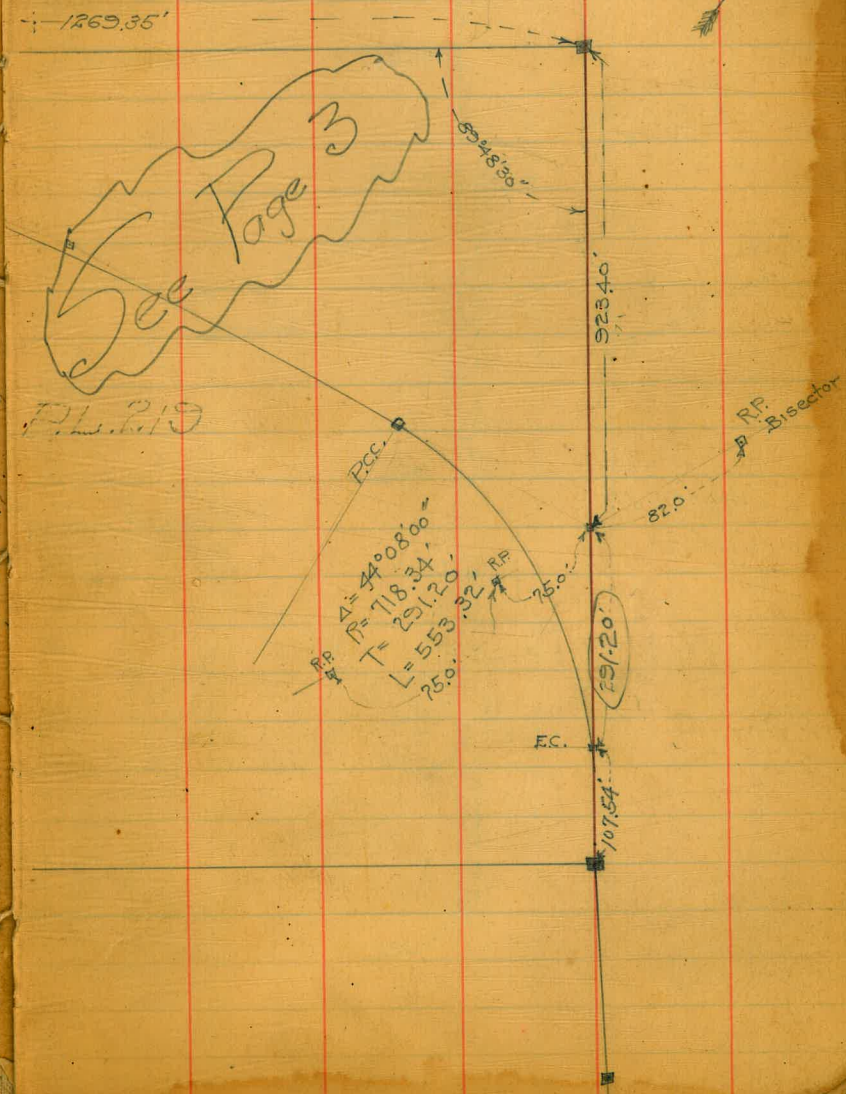
X Sec. West Pt. Loma Blvd. from Bacon to Sea Side 1-64
" " Sea Side St. from Castellar to W. Pt. Loma Blvd. 65-
" " Unnamed St. from W. Pt. Loma Blvd. to Sea Side St. 71-
" " Sunset Cliffs Blvd. " " " " to Bay 73

WEST POINT LIOMA Blvd.
 OPENING
 Thru Pueblo lot 219

Whitkey
 Logkey
 Ma Noon
 Kinnig



$\Delta = 15^{\circ} 47'$
 $R = 2215'$
 $T = 307.02'$
 $L = 610.17'$

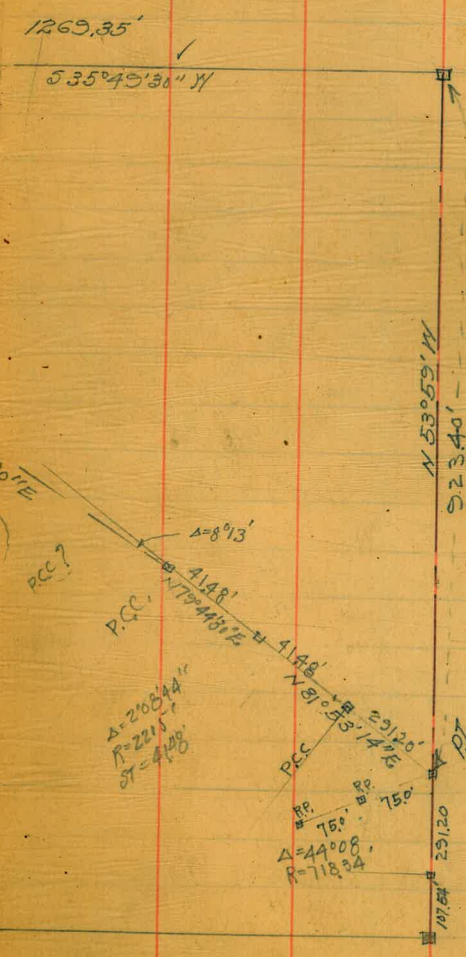
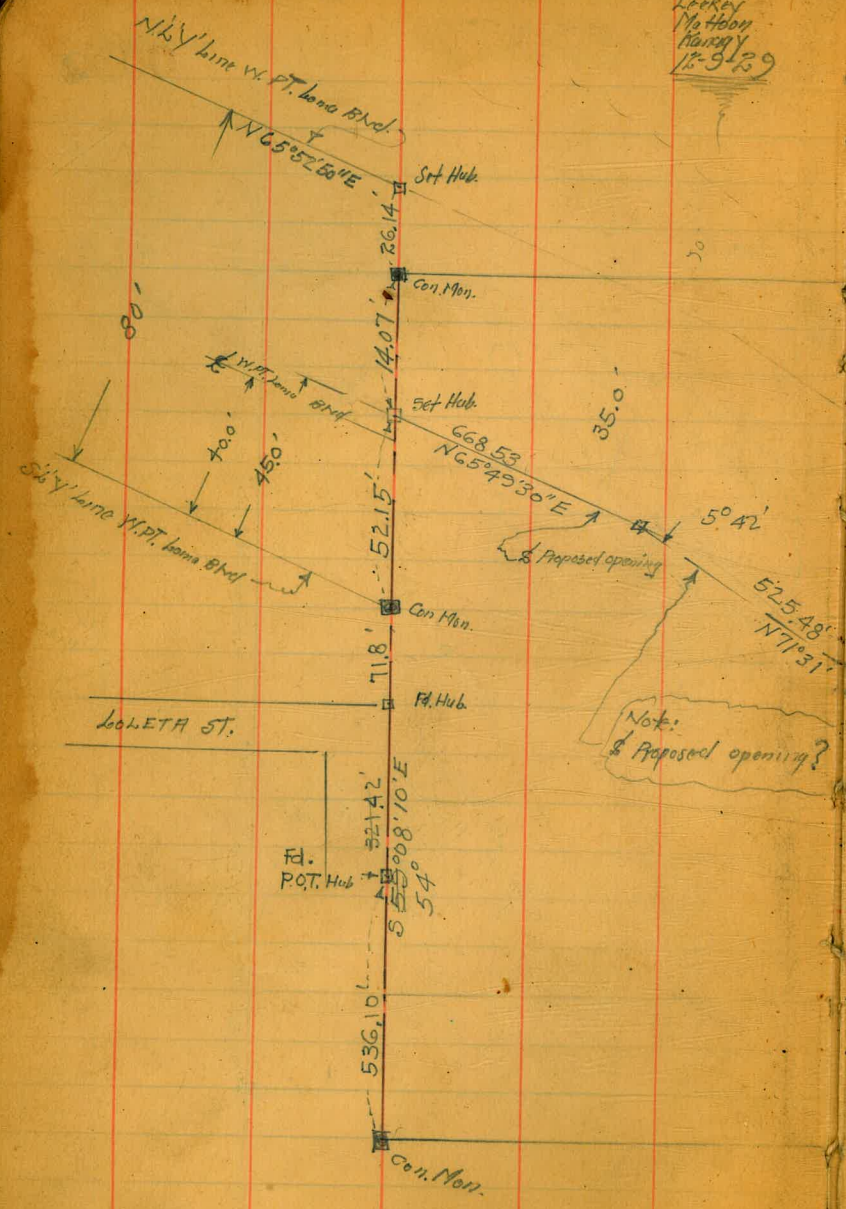


Walker
Lockyer
Matheson
Hanson
12-9-29

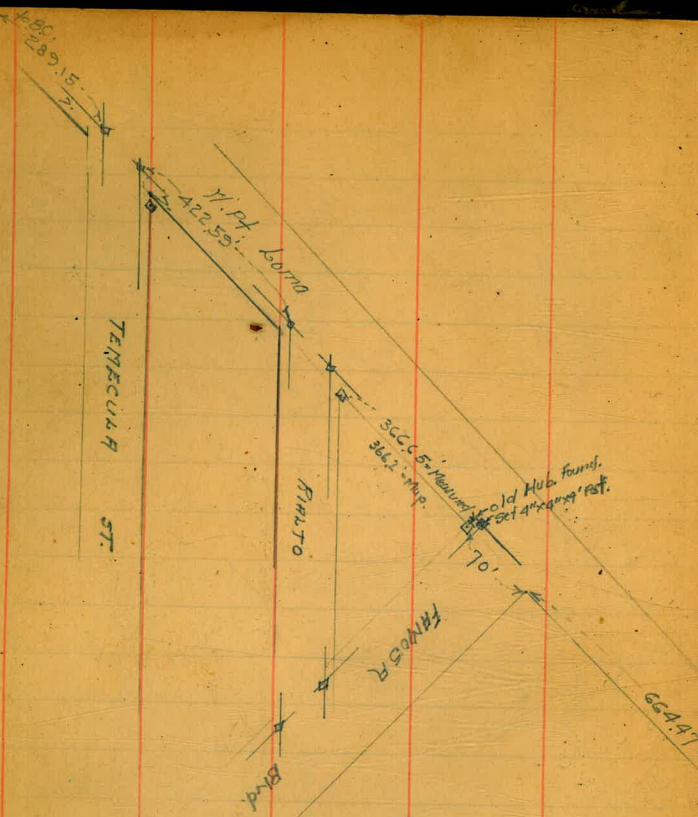
WEST POINT LOMA Blvd.
OPENING
Thru P.L. 219

0003

See Page 4
For Final location



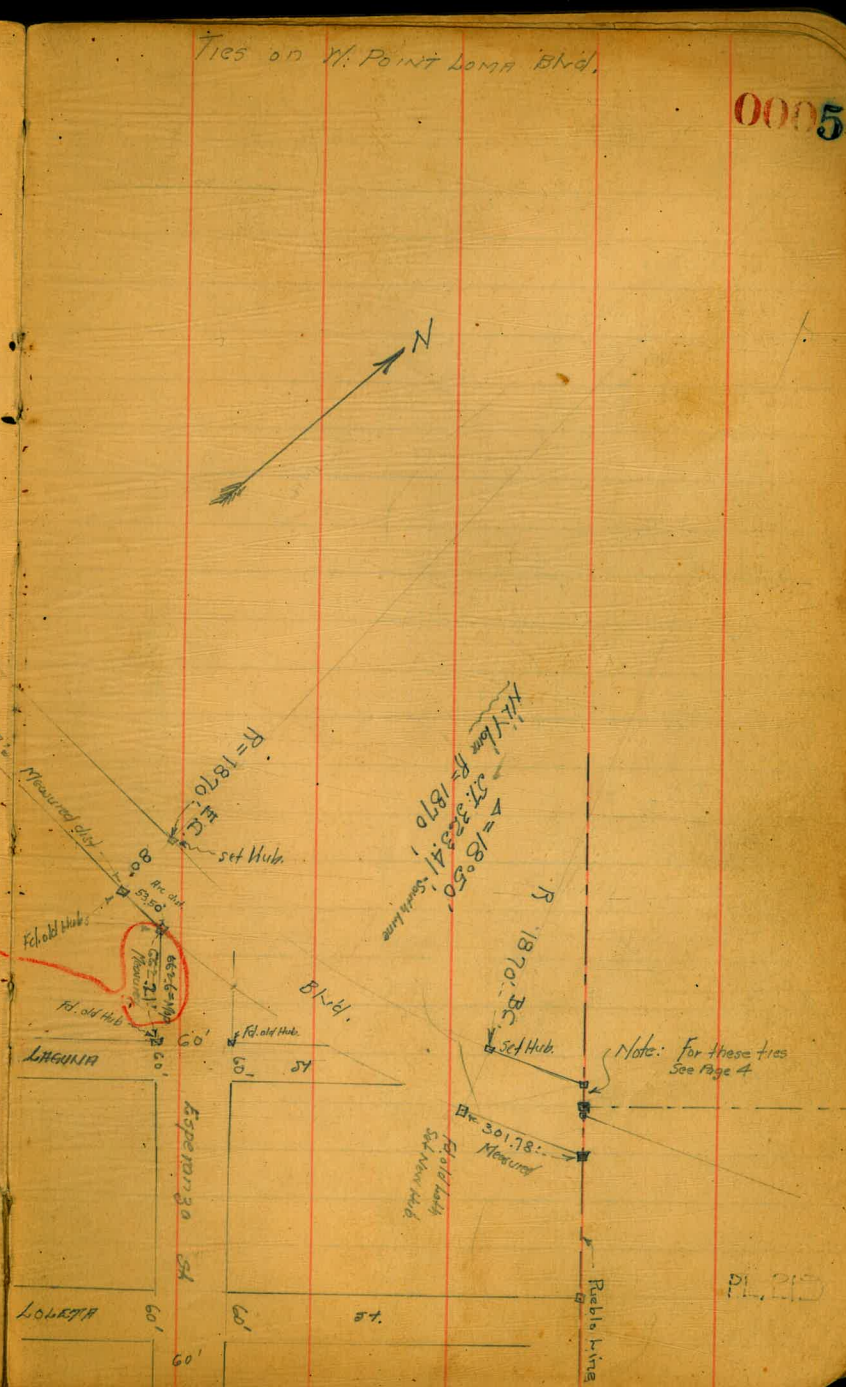
Walker
Loebel
Nelson
12-27-23



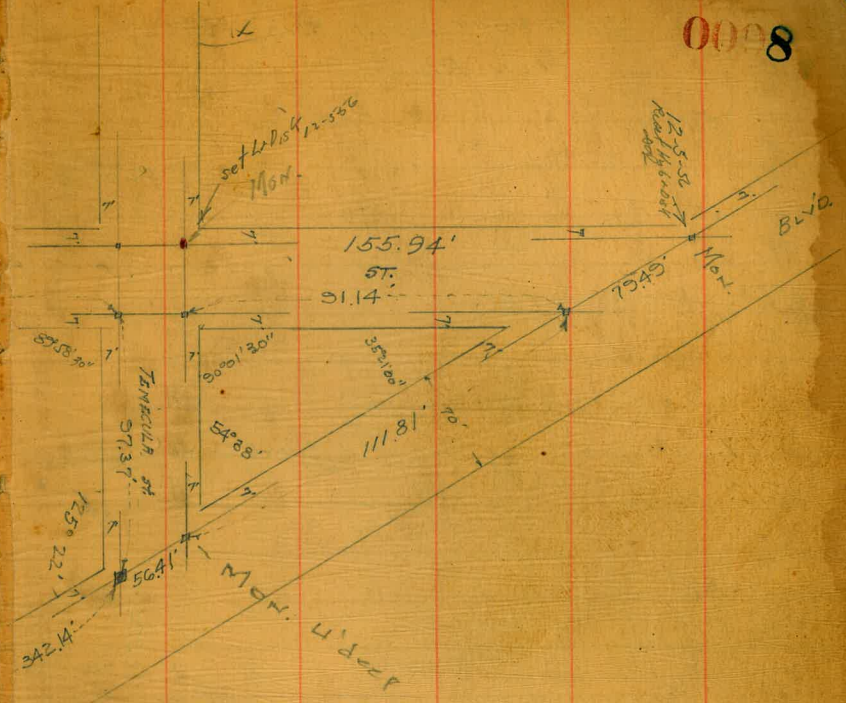
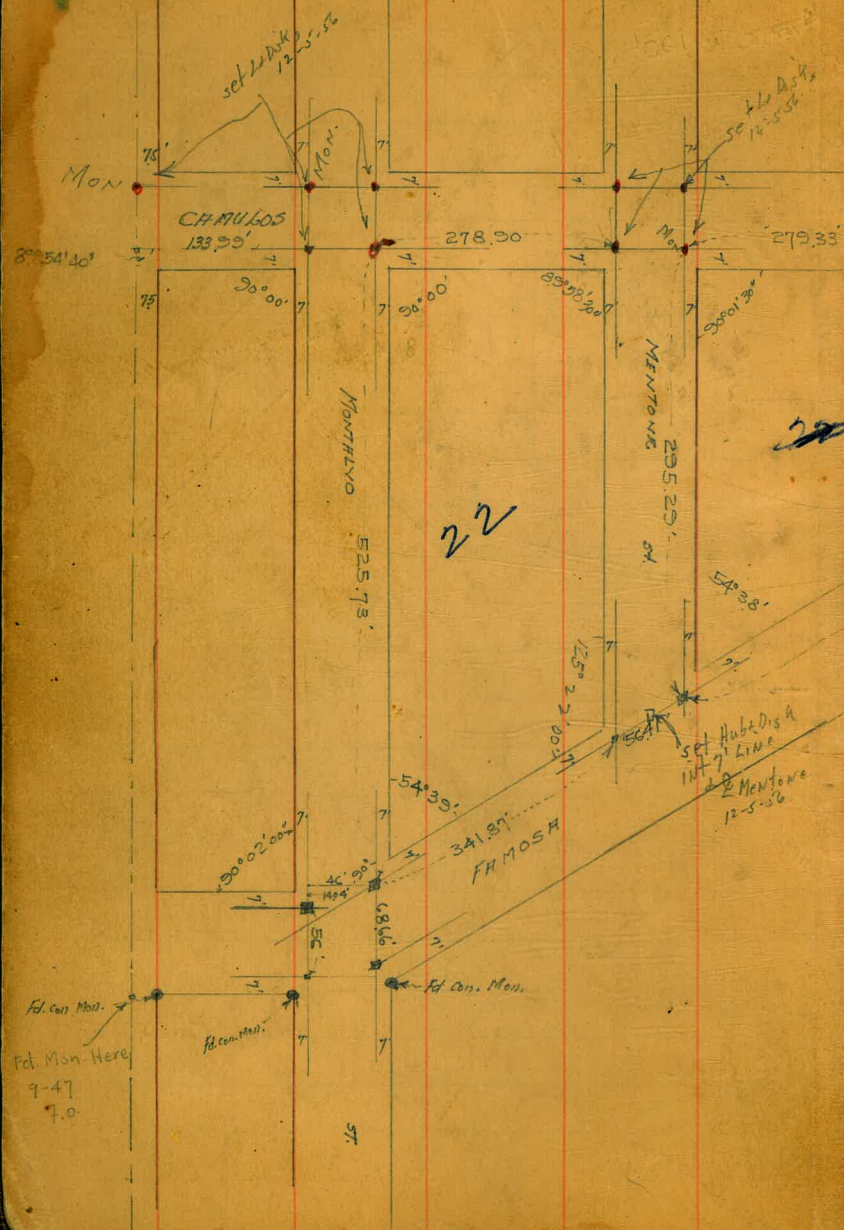
(2626.21)

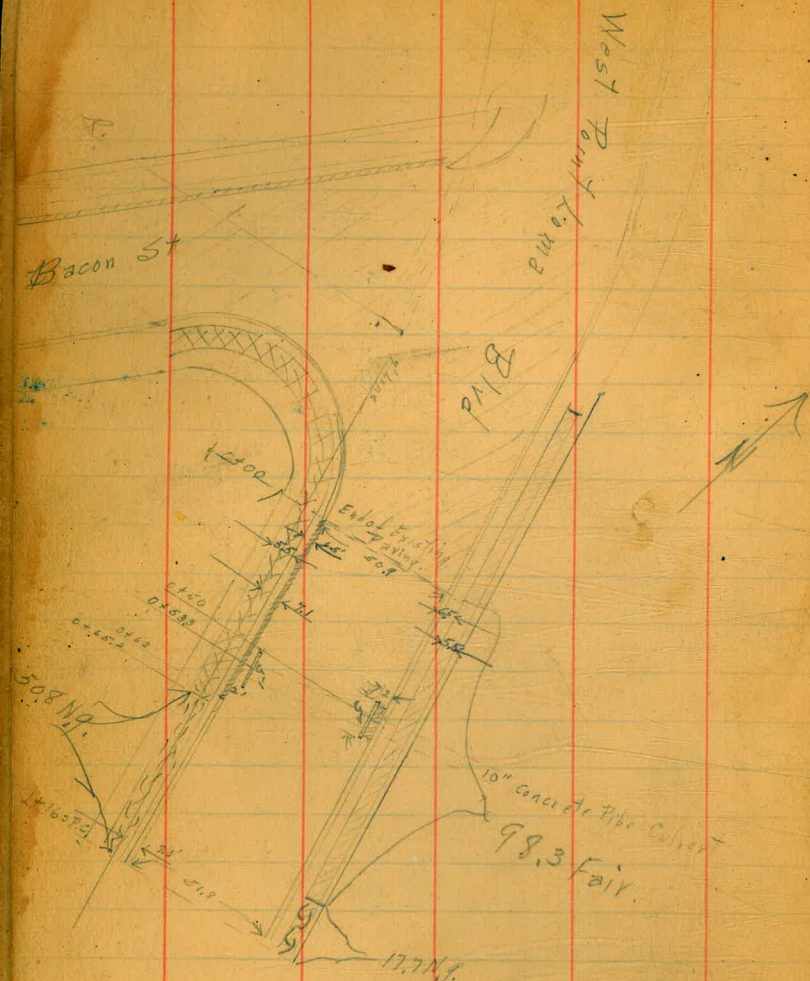
Ties on Y. Point Loma Blvd.

0005



PL 210

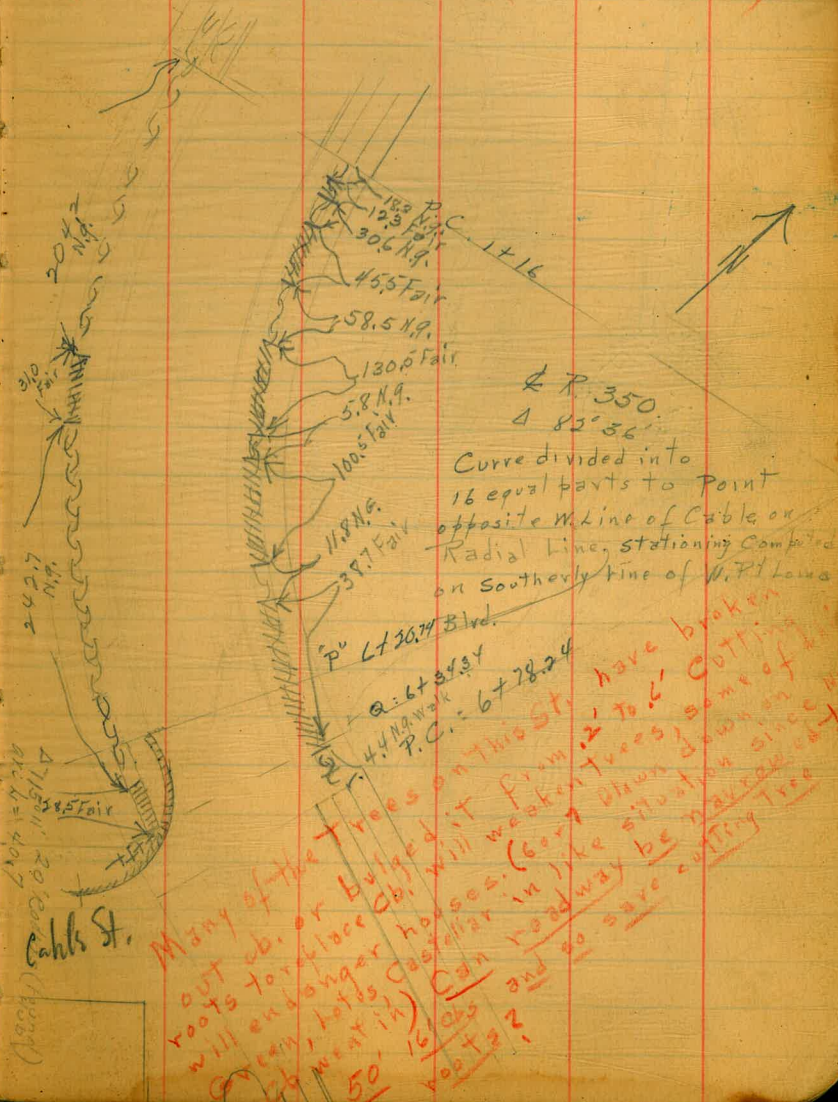




- Symbols
- S.Walk Sand Plastered, but in fair condition. Not recommended to stay in.
 - S.Walk Good - New construction.
 - S.Walk Sand Plastered, Broken N.G.
 - Curb Good - New construction.
 - " N.G. 6\"/>

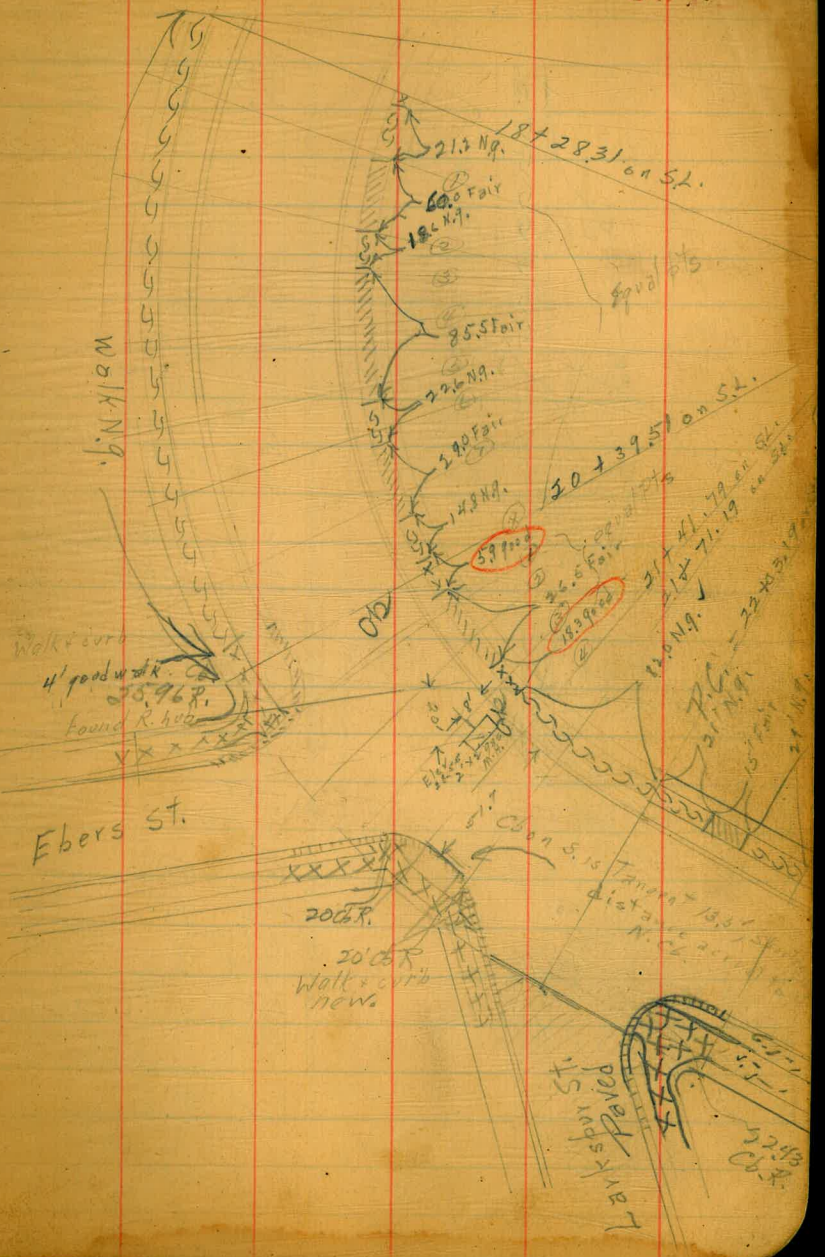
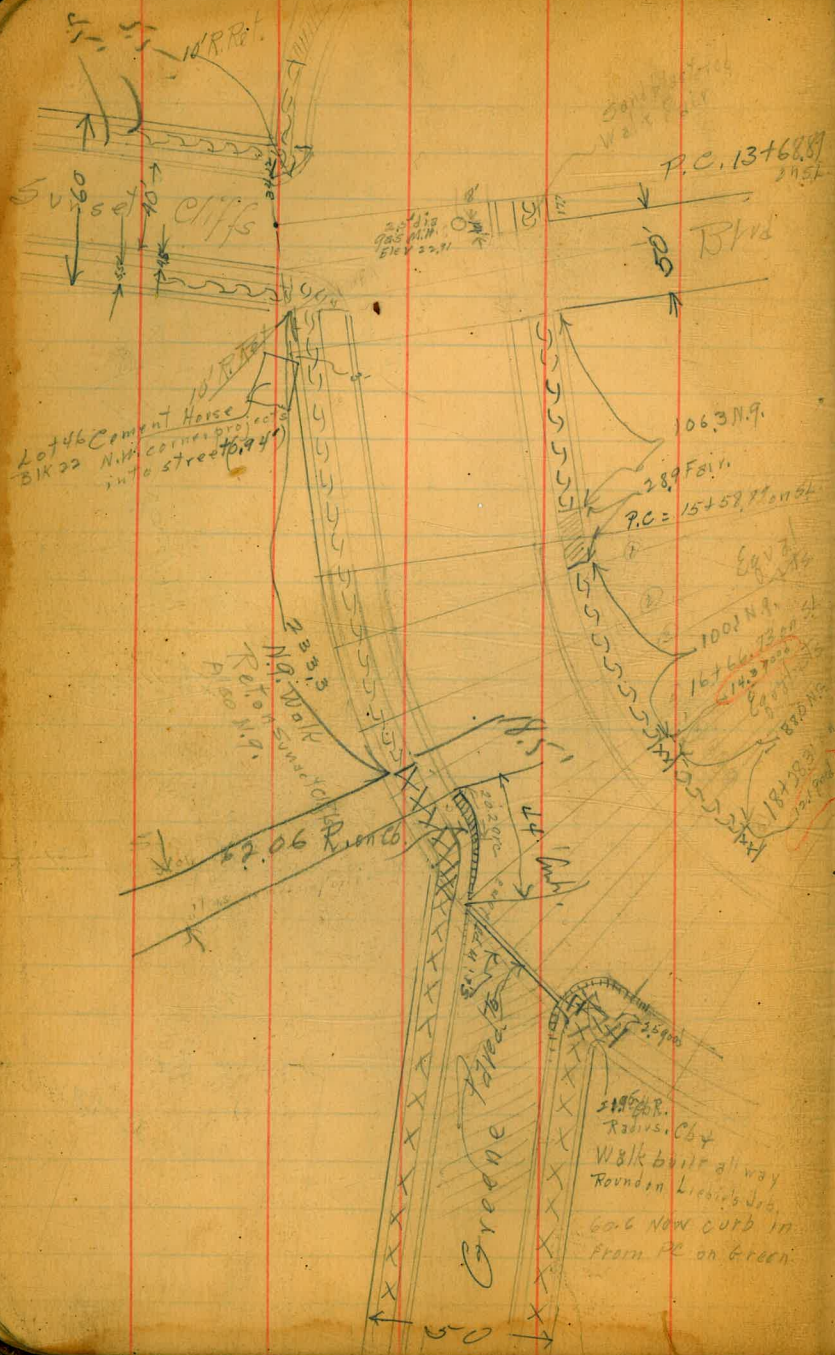
Note: The South Curb is shown in right location: N.Curb 1' too far in St. at intersection of paved section.

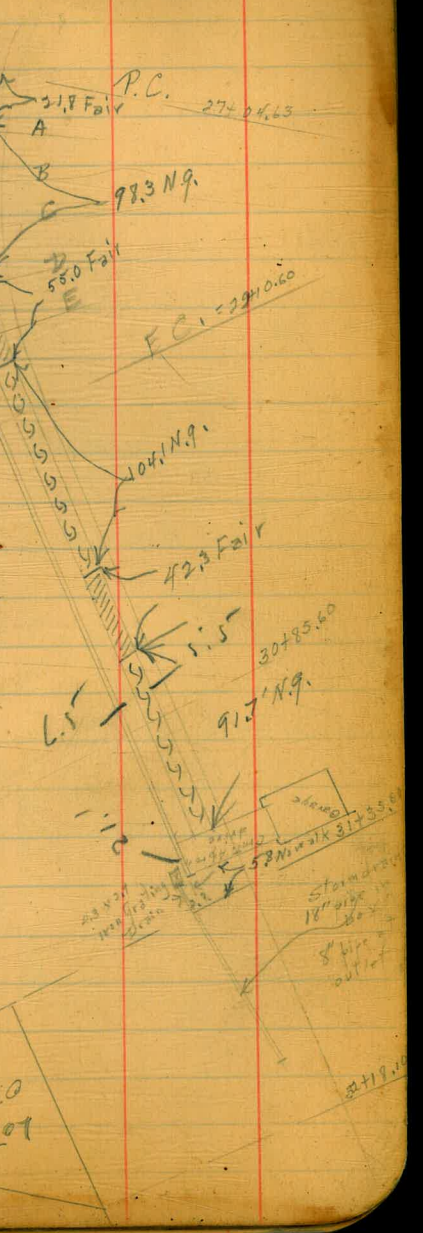
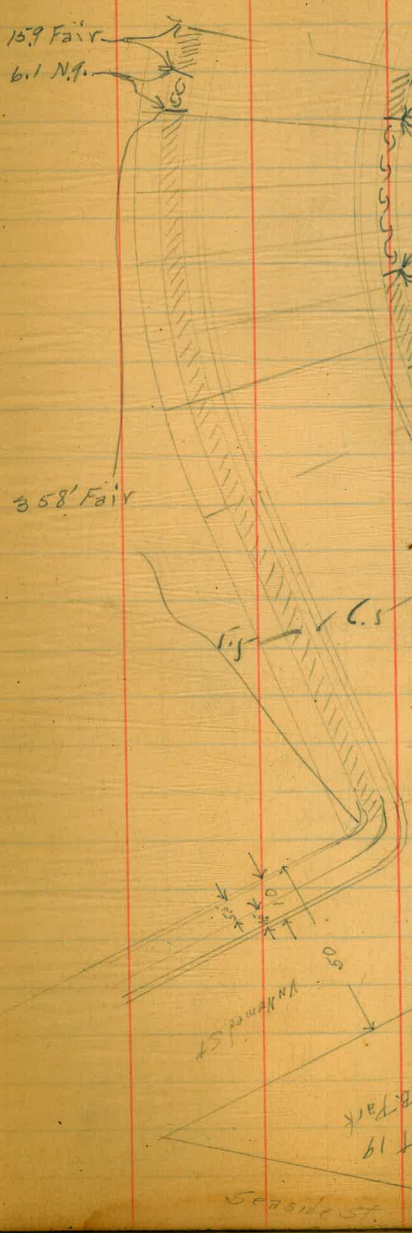
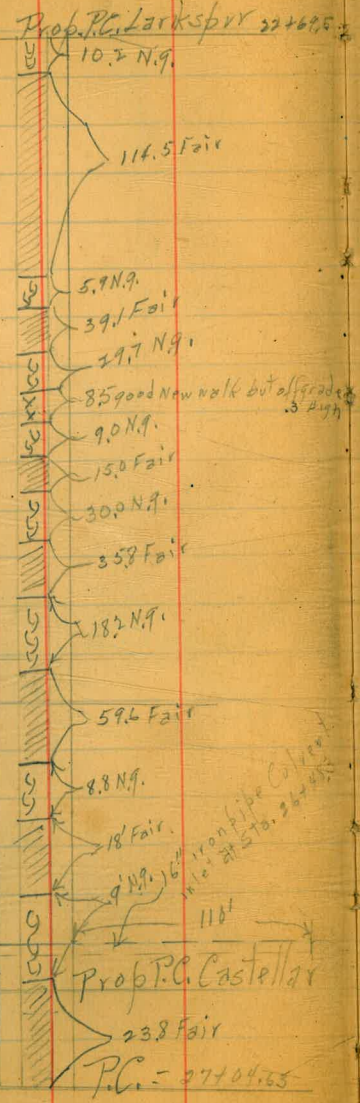
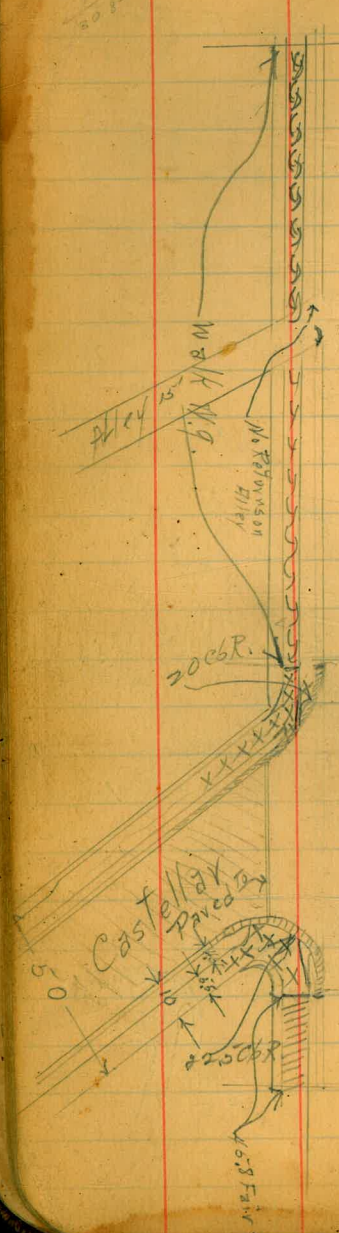
Measurements on Walk show "good" for "N.G." are actual measurements. Taken along 7' line of St. None of the Ck except 0100 to 0103 on S. and returns as shown, is worth trying to save. Trees Located in Notes. (See below)



P. 350
 Δ 83° 56'
 Curve divided into 16 equal parts to Point opposite W. line of Cable on Radial Line, stationing computed on southerly line of N.P. Line

Many of the trees on this St. have broken out ob. or buried roots to place ob. will endanger horses. (60 ft diam trees, some of them green, tops cast in) Can roadway be narrowed to 50' 16' 100' 122'





Flood
Drove
tooney
3-9-30

50' Rd 14' Cb 13' 1/4"

1369

X section W. H. Lane Blvd Bacon to Seaside St

	+	π	-	Elev.	Bacon & Yellow C
N.E.R.R.M.	417	13.67		9.52	
		0-10			
S.L.			6.3	7.4	
+ 0.7 = inside edge Walk			6.58	7.11	
+ 5.8 N.E. Walk			6.64	7.05	
+ 12" Top Cb S.			6.82	6.87	
Print			7.37	6.30	
"			7.06	6.60	
⊕			6.95	6.74	
"			7.16	6.53	
Gut on Print			7.16	6.03	
Top Cb S.			7.13	6.56	
+ 6.5 = Walk			7.06	6.63	
+ 12 = "			7.02	6.67	
N.L.			6.8	6.9	
		0+00 = Edge of Exist. Print.			
N.L.			6.9	6.8	
+ 2 = Walk			7.01	6.68	
+ 7.5 = "			7.11	6.58	
Top Cb N			7.18	6.51 ✓	
Gut N			7.18	6.01	
"			7.26	6.43	
⊕			7.00	6.69	
"			7.15	6.54	

Dittoed 3-27-30

Elev 0015

	+	π	-	Elev
Gut. S.			7.50	6.19
Top Cb S			6.95	6.74 ✓
+ 6.5 Walk			6.78	6.91
+ 12 "			6.68	7.01
S.L.			6.3	7.4
		0+25		
St. on Walk			6.95	7.24
+ 2 "			6.68	7.01
+ 7.5 "			6.82	6.87
Top Cb S.			6.95	6.74
Gut			7.4	6.3
1/4			7.2	6.5
⊕			7.2	6.5
1/4			7.5	6.2
Gut			7.6	6.1
Top Cb			7.09	6.60
+ 6.5 Walk			7.00	6.69
+ 12 "			7.00	6.69
N.L.			6.8	6.9
		0+50		
N.L.			6.8	6.9
+ 2 Walk			6.89	6.80
+ 7.5			6.95	6.74
N Cb Top			7.06	6.63
Gut Cmt Slab over Culvert			7.78	5.91

Note. 0+13 Palm Trees on N side of N.Cb. 1.5' dia 5' N.Cb.

13.69

	+	π	-	Elev
+2	Top of 6" x 8" Cont. Headwall	7.80		5.89 <i>see sketch</i>
1/4		7.4		6.3
1/2		7.0		6.7
3/4		7.1		6.6
GUT		7.4		6.3
Top Cb. S.		6.91		6.78
+ 6.5	Walk	6.79		6.90
+ 12	"	6.65		7.05
S. L.		6.1		7.6

O+50 = proposed location for
culvert storm drain. Levels N at π Angles.

	To W. P. Lams Blvd			
O+00	N. L. W. P. Lams Blvd	6.8		
+50	N of N. L.	8.2		
+92	Edge of filled lot	8.8		
+15	Former tide line	16.5		
+35	Edge of filled lot	13.2		
+00	on filled lot	13.6		
+75	"	14.6		
+85	present tide line	18.6		

O+53.3 = opening Pres Culvert

Top Cb S.	6.90	6.79
flow line inlet	8.80	4.99
Top 6" x 5" Cement Head Wall	6.79	6.90

O+60 = 8" Pine tree on N 3' N of N.Cb.

	+	π	-	Elev
	O+63			
	End of Good 8" Cb on S.	6.89		6.80
	O+65			
	End of Good SW on S.			
	N. Edge	6.71		6.98
	S. "	6.58		7.11
	O+73			
	2.8' dia palm tree 3' So. of S. Cb.			
	O+75			

S. L.	5.8	7.9	
+2	Walk (N.B.)	6.50	7.19
+75	"	6.37	7.32
S Cb Top	6.62	7.07	
Gut	6.9	6.8	
1/4	6.9	6.8	
1/2	7.0	6.7	
3/4	7.0	6.7	
Gut	7.1	6.6	
Top Cb N.	6.89	6.80	
+6.5	walk	6.76	6.93
+12	"	6.68	7.01
N. L.	7.1	6.6	

1+00

N. L.	6.7	6.0	
+7	walk	6.39	7.30
+7.5		6.57	7.13

	+	-	Elev
Top Cb N		6.66	703
Gut		7.0	67
"		6.7	70
⊕		6.7	70
"		6.6	71
Gut		6.6	71
Top Cb S.		6.11	752
+ 6.5 walk		6.08	761
+ 12 "		6.05	764
S.L.		5.6	81
	1+03		
1' dia palm tree & 4' N of N.Cb.			
	1+16 = RC		
S.L.		5.4	83
+ 2 walk		5.70	799
+ 7.5 "		5.75	794
Cb line Cb gone		5.9	78
Gut		6.4	73
"		6.3	74
⊕		6.4	73
"		6.5	72
Gut		6.7	70
Top Cb N		6.40	729
+ 6.5 walk		6.33	736
+ 12 "		6.21	748
N.L.		6.3	74

see page 10 sketch

	+	-	Elev
	13.67		
	1+23		
2.5 dia palm tree & 4' S of S.Cb			
	1+29		
2.0 dia palm tree & 3' N of N.Cb.			
Station A = 148.40 on S.L.			
N.L.		5.7	80
+ 2 } walk		5.45	824
+ 7.0 }		5.44	825
Top Cb N.		5.68	801
Gut.		6.5	72
"		6.1	76
⊕		5.8	79
"		5.7	80
Gut		5.8	79
Top Cb S.		4.99	870
+ 6.5 } walk		4.97	872
+ 12 }		4.95	874
S.L.		4.9	88
Station B - 6'			
2.5 dia palm tree & 3' S of S.Cb.			
Station B = 180.79 on S.L.			
S.L.		4.6	91
+ 2 walk		4.38	931
+ 7.5 "		4.42	927
Top Cb S.		4.36	933
Gut		5.3	84

1369

	+	π	-	Elev
1/4			5.0	87
¢			5.1	86
1/4			5.6	81
Gut.			5.6	81
Top Cb. N.			4.93	876
+ 6.5 } walk			4.2	907
+ 12 }			4.60	909
N.L.			4.8	89

Sta B + 12

2.5 dia palm & 3.5 N. of N. Cb.

Sta C = 213.19 on S.L.

N.L.			4.1	96
+ 2			4.03	966
+ 7.5			4.11	958
Top Cb. N			4.22	947
Gut			5.1	86
1/4			5.0	87
¢			4.4	93
1/4			4.4	93
Gut			4.7	90
Top Cb S			3.92	977
+ 6.5 } walk			3.88	981
+ 12 }			3.92	987
S.L.			3.4	103

1369

0018

	+	π	-	Elev
Sta C + 16				
2.8 dia palm tree & 3.5 S. of S. Cb.				
Sta C + 11				
1.5 dia pine & 4' S. of S. Cb.				
Sta D = 245.58				on S.L.
S.L.			2.6	111
+ 2 } walk			3.30	1039
+ 7.5 }			3.37	1032
Top Cb S.			3.48	1021
Gut			4.1	96
1/4			3.7	100
¢			3.8	99
1/4			4.3	94
Gut			4.8	89
Top Cb N			3.44	1025
+ 6.5			3.41	1028
+ 12			3.37	1032
N.L.			3.5	102

Sta D + 10

2' dia palm & 4' N. of N. Cb.

T.P. 7.5' 17.68 3.52 10.17

Sta E - 8'

Shrub 3.5 S. of S. Cb

Sta E = 277.98 on S.L.

N.L. 6.7 11.0

1768

	+	-	Elev
+2 } walk		6.52	11.16
+7.5 }		6.4	11.04
Top Cb N		6.75	10.93
Gut		7.9	9.8
1/4		7.4	10.3
⊕		6.9	10.8
1/4		6.9	10.8
Gut		7.2	10.5
Cb Line Cb gone		6.6	11.1
+6.5		6.24	11.44
+12		6.37	11.31
S.L.		5.9	11.8

Sta E-2

3.5' dia palm & 4' S of S.Cb

Sta E+4

Large Cactus 3' S of S.Cb.

Sta E+15

Large Cactus 3' S of S.Cb.

Sta E+9

1' dia pine & 4' N of N.Cb.

Sta F = 310.38 on S.L.

3.L.		5.2	12.5
+2 } walk		5.40	12.28
+7.5 }		5.54	12.14

1768

0019

	+	-	Elev
Top Cb S.		5.74	11.94
Gut		6.5	11.2
1/4		5.9	11.8
⊕		6.1	11.6
1/4		6.5	11.2
Gut		7.2	10.5
Top Cb N		5.90	11.78
+6.5		5.85	11.83
+12		5.84	11.84
N.L.		5.9	11.7

Sta F.

Large Cactus 3' S of S.Cb.

Sta F+9

1.3 dia palm & 3.5 N of N.Cb.

Sta F+15

2' dia palm & 3.5 S of S.Cb.

Sta G = 342.77 on S.L.

N.L.		4.7	13.0
+2 } walk		4.86	12.82
+7.5 }		4.97	12.71
Top Cb N		5.15	12.53
Gut		6.4	11.3
1/4		5.6	12.1
⊕		5.2	12.5
1/4		5.2	12.5

17.68

	+	-	Elev
Gut		5.5	12.3
Top Cb S.		4.80	12.88
+ 6.5 } walk		4.63	13.05
+ 12 }		4.49	13.19
SL.		4.4	13.3

Sta G + 9

1.4 dia pine & 3.5 N. of N. Cb.

Sta H = 375.17 on S.L.

SL.		3.5	14.2
+ 2 } walk		3.50	14.18
+ 7.5 }		3.61	14.07
Top Cb S.		3.76	13.92
Gut		4.7	13.0
W		4.3	13.4
E		4.3	13.7
W		4.7	13.0
Gut.		5.6	12.1
Top Cb N		4.34	13.34
+ 6.5 } walk		4.24	13.44
+ 12 }		4.16	13.52
N.L.		3.9	13.8

Sta H + 6

2.5 dia palm & 3.5 S. of Sdb.

Sta H + 7

2' dia palm & 3.5 N. of N. Cb.

17.68

0070

	+	-	Elev
Sta I = 407.56 on S.L.			
N.L.		3.3	14.4
+ 2.5 } walk		3.46	14.22
+ 7.5 }		3.46	14.22
Top Cb N		3.53	14.15
Gut		4.7	13.0
W		4.1	13.6
E		3.6	14.1
W		3.4	14.3
Gut.		3.4	14.3
Top Cb S.		2.76	14.72
+ 6.5 } walk		2.73	14.95
+ 12 }		2.71	15.97
S.L.		2.6	15.1

Sta I + 5

1.3 dia pine & 3' S. of S. Cb.

Sta J = 439.96 on S.L.

SL.		1.7	16.0
+ 2.5 } walk		1.71	15.97
+ 7.5 }		1.83	15.85
Cb Line Cb gone		2.2	15.5
Gut		3.1	14.6
W		2.7	15.0
E		3.8	14.9
W		3.3	14.4

	+	π	-	Elev
Gut			3.9	138
Top Cb N			2.83	1485
+ 6.5 } walk			2.73	1495
+ 12 }			2.65	1503
N.L.			2.6	151

Sta J + 5

1.4 dia palm & 3.5 N of N.Cb.

T.P. on N.Cb. 22.00 1.84 15.84

Sta K = 472.36 on S.L.

N.L.			6.4	156
+ 2 walk			6.48	1552
+ 7.5			6.47	1553
Top Cb N			6.53	1547
Gut			7.3	147
1/4			7.2	148
⊕			6.6	154
1/4			6.4	156
Gut			6.7	153
Top Cb S			5.74	1636
+ 6.5 walk			5.61	1639
+ 12			5.48	1652
S.L.			5.6	164

Sta K + 6

1.4 dia pine & 4' N of N.Cb

Sta K + 7

1' dia pine & 3.5 S. of S.Cb.

	+	π	-	Elev
				22.00
				0021
				Sta L = 504.75 on S.L.
S.L.			5.3	167
+ 2 walk			5.10	1690
+ 7.5			5.21	1679
Top Cb S			5.38	1662
Gut			6.3	157
1/4			6.0	160
⊕			6.0	160
1/4			6.6	154
Gut			7.2	148
Cb N. Broken			6.1	159
+ 6.5 walk			6.02	1598
+ 12			5.94	1606
S.L.			5.9	161

Sta L + 6

1.5 dia palm & 3.5 N. of N.Cb.

Sta M = 537.15 on S.L.

N.L.			5.7	163
+ 2 } walk			5.63	1637
+ 7.5			5.72	1628
Top Cb N			5.68	1632
Gut			6.8	152
1/4			6.0	160
⊕			5.6	164
1/4			5.5	165
Gut			5.8	162

22.00

	+	-	Elev
Top Cb S.		4.92	1708
+ 6.5		4.75	1725
+ 12		4.70	1730
S.L.		5.2	168

Sta M + 3

1' dia Pine @ 35 S of S.Cb.

Sta M + 5

1' dia Pine @ 35 N of N.Cb.

Sta N = 569.54 on S.L.

S.L.		4.6	174
+ 2 } walk		4.36	1764
+ 7.5 } walk		4.37	1763
Cb line Cb gone		4.6	174
Gut		5.5	165
1/4		5.2	168
4		5.3	167
1/4		5.5	165
Gut		6.4	156
Top Cb N		5.47	1653
+ 6.5 } walk		5.42	1658
+ 12 } walk		5.30	1670
N.L.		5.4	166

Sta N

1' dia Palm @ 35 S of S.Cb.

Sta N + 5

1.4 dia Palm @ 4' N of N.Cb.

22.00

4073

Sta O = 601.94 on S.L.

	+	-	Elev
N.L.		5.2	168
+ 2 } walk		4.97	1703
+ 7.5 } walk		5.04	1696
Top Cb N		5.22	1678
Gut		6.0	160
1/4		5.0	170
4		5.0	170
1/4		4.9	171
Gut		5.1	169
Top Cb S.		4.23	1777
+ 6.5 } walk		4.12	1788
+ 12 } walk		4.02	1798
S.L.		4.2	178

Sta O - 5.5

1' dia pine @ 4' S of S.Cb.

Sta O + 4'

1.4 dia pine @ 4' N of N.Cb.

Cb. P.C. ^{R. Ret. on S.} Sta P. = 620.74 on S.L.

S.L.		3.8	182
+ 2		3.83	1817
+ 7.5		3.90	1806
Top Cb S. on P.C. Ret		4.07	1793
Gut		4.8	172
1/4		4.7	173

22.00

	+	-	Elev
£		4.7	17.3
1/4		4.9	17.1
Gut		5.6	16.4
Top Cb N.		5.08	16.92
+ 6.5	} walk	4.92	17.08
+ 12		4.80	17.20
N.L.		5.3	16.7

Sta P + 2

15 dia palm £ 3.5 S of S. Cb.

Sta. Q = W.L. Cable = 6734.34 on S.L.

N.L.		5.0	17.0
+ 2	} walk	4.60	17.40
+ 7.5		4.72	17.28
Top Cb N		4.91	17.09
Gut		5.4	16.6
1/4		4.9	17.1
£		4.4	17.6
1/4		4.5	17.5

Cb line projected

+ 5 = Gutter on Ret

Top Cb on Ret

S.L. on Walk

W.L. Cable + 5.3 Ret crosses St. W. Platform

Top Cb.

Gut on Prmt.

27.00

1023

South of P.C. Ret on Cable

	+	-	Elev
Top Cb		4.04	17.96
prmt		4.46	17.54

Sta Q + 1

1 dia Palm £ 3.5 N. of N. Cb

W.L. Cable + 14.9 = 648.24 on S.L.

S.L. - 10 Prmt		4.00	18.00
S.L. Prmt		4.20	17.80
S.L. + 22' Edge Prmt		4.20	17.80
S.Cb.		4.1	17.9
1/4		4.2	17.8
£		4.3	17.7
1/4		4.9	17.1
Gut		5.38	16.7
Top Cb N		4.78	17.22
+ 6.5	} walk	4.66	17.34
+ 12		4.55	17.45
N.L.		4.9	17.1

W.L. Cable + 14.56 = 657.91 on St.

N.L.		4.8	17.2
+ 2	} walk	4.46	17.54
+ 7.5		4.65	17.35
Top Cb N		4.75	17.25
Gut		5.2	16.8
1/4		4.9	17.1

2200

	+	π	-	Elev
ϕ			4.3	177
1/4			4.0	180
Cb Line			3.9	181
+ 11.5 = Edge Prmt			4.05	1795
S.L.			3.95	1805
+ 10			3.75	1825
W.L. Cable + 24.28 = 667.58 on S.L.				
- 10	prmt		3.58	1842
S.L.	"		3.71	1823
+ 3.0 = edge prmt			3.87	1813
SCb Line			3.8	182
1/4			3.9	181
ϕ			4.2	178
1/4			4.9	171
Gvt			5.2	168
Top Cb N			4.71	1729
+ 6.5 } walk			4.46	1754
+ 12 }			4.34	1766
N.L.			4.5	175
1' diapine # N of N.Cb on above Sta.				
W.L. Cable + 13.9 = 678.24 on S.L.				
N.L.			4.4	176
Cb Line N (Cb + walk out)			4.7	17.3
Gvt			5.1	169
1/4			4.8	17.2

2200

2024

	+	π	-	Elev
ϕ			4.2	178
1/4			3.8	182
Cb Line			3.6	184
+ 11.0 = Edge prmt			3.70	183
S.L. on prmt			3.62	1838
+ 10	"	"	3.50	1850
P.C. + 10.05 = 678.32				
- 10	on PVMT.		3.41	1859
S.L.	"	"	3.47	1853
+ 2.7 Edge Prmt.			3.52	1848
Cb Line			3.5	185
1/4			3.9	181
ϕ			4.2	178
1/4			4.7	173
Gvt			5.0	180
Top Cb N			4.46	1755
+ 6.5			4.23	1777
+ 12			4.05	1795
N.L.			4.2	178
P.C. + 20.16 = 6798.40				
1.5' diapalm 3.5' N of N.Cb				
N.L.			4.2	178
+ 2 } walk			3.93	1807
+ 7.5 }			4.07	1793
Top Cb N			4.33	1767

22.00

	+	π	-	Elev.
Gut			4.9	17.1
1/4			4.6	17.4
⊕			4.2	17.8
1/4			3.8	18.2
S.Cb Line			3.6	18.4
+ 11.5 = Edge Prmt			3.37	18.63
S.L. on "			3.32	18.68
+ 10			3.23	18.77
P.C. + 30.24 = 7 + 08.48				
- 10 on Prmt			3.01	18.99
S.L. " "			3.17	18.83
+ 21. Edge Prmt			3.24	18.76
S.Cb Line			3.6	18.4
1/4			3.7	18.3
⊕			4.1	17.9
1/4			4.5	17.5
Gut			4.8	17.2
Top Cb N			4.15	17.85
+ 6.5			3.92	18.08
+ 12			4.12	17.88
N.L.			4.2	17.8
P.C. + 40.32 = 7 + 18.56				
1' diapine 4' N. of N. Cb.				
N.L.			3.8	18.2
N Cb Top (walk gone).			4.05	17.95

22.00

	+	π	-	Elev.
Gut			4.6	17.4
1/4			4.5	17.5
⊕			4.0	18.0
1/4			3.7	18.3
S.Cb Line			3.5	18.5
+ 12.2 = Edge Prmt			3.13	18.87
S.L. " "			3.05	18.75
+ 10			2.87	19.13
P.C. + 50.4 = 7 + 28.64				
- 10 on Prmt			2.80	19.20
S.L. " "			3.00	19.00
+ 15 Edge "			3.05	18.95
S.Cb Line			3.5	18.5
1/4			3.7	18.3
⊕			4.0	18.0
1/4			4.3	17.7
Gut			4.5	17.5
Top Cb N			3.91	18.09
+ 6.5			3.75	18.25
+ 12			3.50	18.50
N.L.			3.7	18.3
P.C. + 60.18 = 7 + 38.72				
N.L.			3.4	18.6
+ 2 walk			3.45	18.55
+ 7.5			3.61	18.39

2200

	+	π	-	Elev.
Top Cb N			3.83	18.17
Gut			4.4	176
1/4			4.3	177
⊖			3.9	181
1/4			3.6	184
S.Cb Line			3.4	186
+ 12.7 Edgeprmt			2.99	19.01
S.L. on "			2.94	19.06
+ 10			2.76	19.24
			P.C. + 70.56 = 7+48.80	
- 10			2.65	19.35
S.L.			2.89	19.11
+ 0.9 = Edgeprmt			2.15	19.05
S.Cb Line			3.3	187
1/4			3.6	184
⊖			3.8	182
1/4			4.1	179
Gut			4.5	175
Top Cb N			3.66	18.34
+ 6.5			3.51	18.49
+ 12			3.34	18.66
A.L.			3.4	186
			P.C. + 80.67 = intersection of S.L.	
			with Cb on Ret and Lotus = 7+58.99	
N.L.			3.4	186

1' dia Palm 4' No. of Alcobon (Vista)

2200

026

	+	π	-	Elev
+ 2			3.73	18.77
+ 7.5			3.36	18.64
Top Cb N			3.54	18.46
Gut			4.4	176
1/4			3.9	18.1
⊖			3.6	186
1/4			3.5	185
S.Cb Line			3.3	187
+ 13.5 = Edgeprmt			2.92	19.08
S.L.			2.91	19.09
S.L. Top Cb.			2.32	19.68
+ 10 on Ret			2.20	19.80
Gut			2.76	19.24
+ 20 on Ret			2.13	19.87
Gut			2.64	19.36
+ 31 = P.C. of Ret on Lotus				
Top			2.09	19.91
Gut			2.53	19.47
			7+78.30 = Prop P.C. Lotus + W. 7' lines	
S.L.			2.1	19.9
+ 18 on walk			2.26	19.74
+ 7.3 " "			2.33	19.67
+ 13.8 = Cb on Ret			2.45	19.55
Gut			3.2	18.8
1/4			3.3	18.7

	+	22.00	-	Elev
☐			3.4	186
1/4			3.7	183
Gut			4.3	177
Top Cb. N.			3.34	18.66
+ 6.5 walk			3.14	1886
+ 12			3.01	1899
N.L.			2.8	19.2

7492.3

2' dia palm 4' N. of N.Cb.

8+18.3

1' dia pine 4' N. of N.Cb.

Prop. PC + 25 = CB PC. = 7480.8

Top Cb on end of Good 8" Cb 2.48

7487.3

1.4 dia palm 3.5 S. of S.Cb.

8+17.3

1.4 dia pine 4.0 S. of S.Cb.

8+22.32 = P.C.

N.L. 2.8 19.2

+ 2 } walk Zone

+ 7.5 }

Top Cb N 2.88 19.12

Gut 3.8 18.2

1/4 3.1 18.9

☐ 2.9 19.1

	+	22.00	-	Elev
1/4			2.8	19.2
Gut			3.0	19.0
Cb Line Cb gone			2.0	20.0
+ 6.5			1.72	20.08
+ 12			1.80	20.20
S.L.			1.8	20.2
T.P. Post Top 1.98	25.09	1.89	20.11	in front of

Curve Divided into 10 Equal Parts
Sections Taken Radially. Stationing on

S. Property Line

Sec. A = 8+50.75

S.L.	4.6	20.5
+ 2 } walk	4.68	20.41
+ 7.5 }	4.81	20.28
Top Cb 5	4.91	20.17
Gut	5.7	19.4
1/4	5.7	19.4
☐	5.7	19.4
1/4	6.1	19.0
Gut	6.4	18.7
Top Cb 5	5.76	19.33
+ 6.5 } walk	5.52	19.57
+ 12 }	5.40	19.69
N.L.	5.5	19.6

which?

Beginning of
Good Walk on
5.5' wide North.

Sta A - 13

1' dia Palm ☐ 3.5 N. of N.Cb.

25,09

+	T	-	Elev
			Sta A+13
2.4 dia	Pine	4' N of N.Cb.	
			Sta A+14
1.4 dia	Pine	4' S. of S.Cb.	
			Sec B = 8+79.18
N.L.		5.1	200
+2		5.19	1990
+7.5		5.32	1977
Top Cb N.		5.50	1959
Gut		6.1	190
1/4		5.8	193
2		5.4	197
1/4		5.5	196
Gut		5.4	197
Top Cb S.		4.66	2043
+6.5		4.58	2051
+12		4.40	2069
S.L.		4.4	207

Sta B+5

1.7 dia palm 4' N of N.Cb

Sta B+6

1.5 dia palm 4' S. of S.Cb.

Sec. C = 9+07.61

S.L.		3.4	217
+7		4.17	2092

25,09

028

+	T	-	Elev
+7.5		4.23	2086
Top Cb S.		4.50	2059
Gut		5.2	199
1/4		5.2	199
2		5.1	200
1/4		5.6	19.5
Gut		6.0	191
Top Cb N		5.17	1982
+6.5		5.03	2006
+12		4.92	2017
N.L.		4.8	203

Sec. C. - 5

2.3 dia Pine 4' N of N.Cb

Sec. C - 2

1.3 dia Pine 4' S. of S.Cb

Sec D - 2.45' = end of Good

walk on N. 5.5 wide 3' from N.L.

N. edge of walk		4.52	2057
S. " " walk		4.71	2038

Sec. D = 9+36.04

N.L.		4.6	205
Top Cb (walk gone)		4.91	2018
Gut		5.4	197
1/4		5.2	199
2		4.9	202

	+	-	Elev
1/4		5.0	201
Gut		5.2	199
Top Cb S.		4.15	20.94
+ 6.5		4.00	21.1
+ 12		3.98	21.11
S.L.		3.3	21.8

Sec D - 11

1' dia Palm 3.5 S. of S. Cb.

Sec D - 13

1.8' dia Palm 4' N. of N. Cb

Sec D + 13

.9' dia pine 4' N. of N. Cb.

Sec D + 12

.8 dia pine 4' S. of S. Cb.

Sec E = 9 + 64.47

S.L.		3.2	21.9
+ 2 walk		3.67	21.42
+ 7.5		3.79	21.30
Top Cb S.		3.72	21.17
Gut		4.9	20.2
1/4		4.7	20.4
4		4.8	20.3
1/4		5.1	20.0
Gut		5.2	19.9
Top Cb N		4.64	20.45

	+	-	Elev
+ 6.5		4.37	20.72
+ 12		4.39	20.80
N.L.		4.4	20.7

Sec E + 3

2.4' dia Palm 4' N. of N. Cb

Sec E + 4

1.9 dia Palm 4' S. of S. Cb.

Sec E + 12.1 = beginning of Good

walk on N. 5.5 wide 2' from N.L.

N. edge of walk		4.14	20.95
S. edge of walk		4.27	20.82

Sec. F = 9 + 92.90

N.L.		4.1	21.0
+ 2	} walk	4.05	21.04
+ 7.5		4.17	20.92
Top Cb N		4.41	20.68
Gut		4.9	20.2
1/4		4.9	20.2
4		4.6	20.5
1/4		4.7	20.4
Gut		4.6	20.5
Top Cb S.		3.60	21.49
+ 6.5		3.52	21.67
+ 12		3.43	21.66
S.L.		2.8	22.3

25.09

+ π - Elev
Sec F - 4

1.1 dia pine 4' S. of S.Cb.

Sec F + 30 = End of Good

walk on North. 5.5 wide 2' from N.L.

N edge of walk 3.70 21.39

S " " " 3.97 21.12

Sec G = 10 + 21.33

S.L. 3.0 22.1

+ 2 3.21 21.88

+ 7.5 3.28 21.81

Top Cb ~~W~~ 3.50 21.59

Gut 4.3 20.8

1/4 4.4 20.7

♀ 4.3 20.8

1/4 4.7 20.4

Gut 4.5 20.6

Top Cb A 4.09 21.00

+ 6.5 3.97 21.12

+ 12 3.55 21.44

N.L. 3.7 21.4

Sec G - 16'

3.5' dia palm 4' N of N.Cb.

Sec G - 13

1.3' dia palm 4' S. of S.Cb.

Sec G + 11

1.8 dia pine 4' S. of S.Cb.

25.09

+ π - Elev. 030
Sec G + 10.7 = = beginning of

Good Walk on S. 5.5 wide 2' from S.L.

S. edge of walk 3.01 22.08

N " " walk 2.96 22.13

Sec H = 10 + 49.78

N.L. 3.3 21.8

+ 2 3.46 21.63

+ 7.5 3.52 21.47

Top Cb N. 3.72 21.37

Gut 4.6 20.5

1/4 4.3 20.8

♀ 4.1 21.0

1/4 4.1 21.0

Gut 3.9 21.2

Top Cb S. 3.21 21.88

+ 6.5 3.05 22.04

+ 12 2.95 22.14

S.L. 2.6 22.5

Sec H

3' dia Palm 3.5' N of N.Cb.

Sec I = 10 + 78.21

S.L. 2.4 22.7

+ 2 2.63 22.46

+ 7.5 2.70 22.39

Top Cb S 2.91 22.10

2509

	+	π	-	Elev
Gut			3.6	21.5
1/4			3.8	213.
ϕ			3.8	213
1/4			4.0	211
Gut			4.3	208
Top C6 N			3.52	2157
+ 6.5			3.32	2177
+ 12			3.19	2190
A.L.			3.1	220

Sec I - 7

1.7 dia pine 4' S. of S.Cb

Sec I - 8

0.5 dia pine 4' N. of N.Cb.

Sec I + 16

2.7 dia palm 4' N. of N.Cb.

Sec I + 15

2.0 dia palm 4' S. of S.Cb.

T.P. 3.76 27.37 3.46 21.63

Sec J = P.R.C. = 11 + 06.65

N.L.			5.3	221
+ 2			5.27	2212
+ 7.5			5.29	2210
Top C6 N.			5.17	2172
Gut			6.2	212
1/4			6.3	211

2739

	+	π	-	Elev	031
ϕ			6.0	214	
1/4			5.9	215	
Gut			5.7	217	
Top C6 S			5.00	2239	
+ 6.5			4.82	2257	
+ 12			4.73	2266	
S.L.			4.5	229	

Seed + 8

1.1 dia pine 3.5 S. of S.Cb.

Seed + 283 = End of Goodwalk on

South 5.5 wide 2' from S.L.

S. edge of walk 4.51 2288

N. " " " 4.59 2280

Sec A = 11 + 44.67 Curved divided into 6 equal parts to W.L. of Sunset Cliffs Blvd. Sections Taken Radially. Stationing is on Southerly Property Line

S.L.			4.2	232
+ 2			4.45	2294
+ 7.5			4.53	2286
Top C6 S.			4.61	2278
Gut			5.5	219
1/4			5.5	219
ϕ			5.6	218
1/4			6.0	214

27.39

	+	T	-	Elev
Gut			5.9	21.5
Top Cb N			5.35	22.04
+ 6.5			5.7	22.27
+ 12			4.96	22.43
N.L.			5.0	22.4

Sec A-2

1/4 dia palm 4' S. of S. Cb.

Sec A-7

1/4 dia Chinese Camphor Tree 4' N. of N. Cb.

Sec B = 11 + 82.69

N.L.			4.6	22.8
+ 2			4.60	22.79
+ 7.5			4.73	22.66
Top Cb N			4.96	22.43
Gut			5.7	21.7
1/4			5.7	21.7
4			5.3	22.1
1/4			5.1	22.3
Gut			5.3	22.1
Top Cb S.			4.34	23.05
+ 6.5			4.22	23.17
+ 12			4.16	23.23
S.L.			8.7	23.7

Sec B. - 8

0.4 dia Camphor Tree 4' N. of N. Cb

27.39

032

	+	T	-	Elev
Sec B-12				
1' dia pine			3.5 S. of S. Cb.	
Sec B+17				
1' dia palm			3.5 S. of S. Cb.	
Sec B+17				
2.5' dia palm			4' N. of N. Cb.	
Sec C = 12 + 20.71				
5 L.			3.2	24.2
+ 2			3.83	23.56
+ 7.5			3.90	23.49
Top Cb S.			4.02	23.37
Gut			4.9	22.5
1/4			4.9	22.5
4			4.9	22.5
1/4			5.3	22.1
Gut			5.2	22.2
Top Cb N			4.60	22.79
+ 6.5			4.33	23.06
+ 12			4.23	23.16
N.L.			4.4	23.0

Sec C - 4.9 = beginning of

Good walk on N. 5.5' wide 2' from N.L.

N edge of walk			4.22	23.17
5 " " "			4.37	23.02

Sec C + 7

1' dia Pine 3.5 S. of S. Cb.

27.39

	+	-	Elev
	Sec D = 12 + 58.73		
N.L.		4.2	23.2
+ 2		4.13	23.26
+ 7.5		4.14	23.25
Top Cb N		4.29	23.10
Gut		5.1	22.3
1/4		5.1	22.3
⊕		4.6	22.8
1/4		4.6	22.8
Gut		4.6	22.8
Top Cb S.		3.72	23.67
+ 6.5		3.62	23.77
+ 12		3.53	23.86
S.L.		2.8	24.6

Sec D

3' dia palm 4' N. of N. Cb.

Sec D-3

2.8 dia palm 4' S. of S. Cb.

Sec D + 23.3 = end of Good Wood

on N. 5.5 wide 2' from N.L.

Nudge walk		3.92	23.47
S. " "		4.06	23.33

Sec E = 12 + 96.75

S.L.		2.4	25.0
+ 2		3.19	24.20

27.39

033

	+	-	Elev.
+ 7.5		3.29	24.10
Top Cb S.		3.40	23.97
Gut		4.4	23.0
1/4		4.2	23.2
⊕		4.3	23.1
1/4		4.8	22.6
Gut		4.9	22.5
Top Cb N		4.19	23.18
+ 6.5		4.00	23.39
+ 12		3.83	23.56
N.L.		4.0	23.4

Sec F = 13 + 34.77 = W.L. Sunset Cliffs

N.L.		4.1	23.3
+ 2		3.74	23.65
+ 7.5		3.77	23.62
Top Cb N		3.95	23.44
Gut		4.6	22.8
1/4		4.5	22.9
⊕		4.0	23.4
1/4		3.9	23.5
Gut		4.1	23.3
Top Cb S.		3.09	24.30
+ 6.5		2.95	24.44
+ 12		2.82	24.57
S.L.		2.8	24.6

27.39

	+	x	-	Elev
T.P. Top Stand pipe 219		28.75	0.83	26.56
		13 + 45.17 = W.C. of Sunset Cliffs.		
S.L. Top Cb.			4.66	24.29
S.L. Gut			5.2	23.5
Cb Line S			5.4	23.3
1/4			5.1	23.6
⊕			5.3	23.4
1/4			5.7	23.0
Gut			6.2	22.5
Top Cb N.			5.27	23.48
+ 6.5			4.93	23.82
+ 12			5.02	23.73
N.L.			5.2	23.5
		P.C. = 13 + 68.89		
N.L.			5.1	23.6
+ 2			4.90	23.85
+ 7.5			5.04	23.71
Top Cb N			5.19	23.56
Gut			6.0	22.7
1/4			5.6	23.1
⊕			5.1	23.6
1/4			4.9	23.8
S.Cb Line			4.6	24.1
S.L.			4.4	24.3

P.C. + 5

2' dia Palm tree ⊕ 4' N of N.Cb.

28.75

031

	+	x	-	Elev.
		13 + 86.59 = W.L. Sunset to N. + E.Cb. Sunset to S.		
J.L. Top Cb			3.62	25.13
S.L. Gut			4.7	24.0
Cb Line S.			4.6	24.1
1/4			4.7	24.0
⊕			4.9	23.8
1/4			5.5	23.2
Gut			5.8	22.9
Top Cb N.			5.16	23.59
+ 6.5			5.01	23.74
+ 12			4.98	23.77
N.L.			5.2	23.5
		13 + 98.42 = E.L. Sunset to South		
N.L.			5.3	23.4
Cb. Line N			5.6	23.1
1/4			5.4	23.3
⊕			4.9	23.8
1/4			4.6	24.1
Gut S.			4.5	24.2
Top Cb S.			3.63	25.12
S.L. on Walk			3.33	25.42
		+ 14		
		2' dia palm ⊕ 4' S. of S.Cb.		

28.75

+ T - Elev.
 14 + 36.59 = E.L. Sunset to North

B.L.		2.7	25 8
+ 2		3.17	25 58
+ 7.5		3.28	25 47
Top C6 S.		3.38	25 37
Gut		4.3	24 4
1/4		4.4	24 3
⊕		4.7	24 0
1/4		5.2	23 5
Gut		5.6	23 1
Top C6 N		5.13	23 62
+ 6.5		4.93	23 82
+ 12		4.82	23 93
N.L.		5.1	23 6

+ 16
 2' dia Palm E 3.5' S. of S.C6.
 14 + 61.59

N.L.		4.1	23 9
+ 2		4.65	24 10
+ 7.5		4.80	23 95
Top C6 N		4.92	23 83
Gut		5.4	23 3
1/4		5.0	23 7
⊕		4.6	24 1
1/4		4.2	24 5

28.75

0.35

+ T - Elev

Gut		4.1	24 6
Top C6 S.		3.21	25 54
+ 6.5		3.07	25 68
+ 12		2.92	25 83
S.L.		2.50	26 25

14 + 76.59

1.5 dia pine 4' S. of S.C6.
 14 + 86.59

S.L.		2.5	26 2
+ 2		2.81	25 94
+ 7.5		2.70	25 85
Top C6 S.		3.07	25 68
Gut		3.9	24 8
1/4		4.0	24 7
⊕		4.4	24 3
1/4		4.9	23 8
Gut		5.2	23 5
Top C6 N		4.78	23 97
+ 6.5		4.60	24 15
+ 12		4.41	24 34
N.L.		4.6	24 1

15 + 11.59

N.L.		4.3	24 4
+ 2		4.13	24 62
+ 7.5		4.15	24 60

28.75

	+	T	-	Elev
Top cb N			4.52	24 23
Gut			5.0	23 7
114			4.7	24 0
⊕			4.2	24 5
114			3.8	24 9
Gut			3.7	25 0
Top cb S.			3.87	25 88
+ 6.5			2.74	26 01
+ 12			2.66	26 09
S.L.			2.3	26 4.
15+26				
35 dia pine			⊕ 3.5 S. of S. cb.	
15+36.59				
S.L.			2.0	26 7
+ 2			2.41	26 34
+ 7.5			2.47	26 28
Top cb S.			2.72	26 03
Gut			3.5	25 2
114			3.7	25 0
⊕			4.0	24 7
114			4.5	24 2
Gut			4.9	23 8
Top cb N			4.20	24 55
+ 6.5			4.05	24 70

28.75

	+	T	-	Elev	036
+ 12			3.93	24 82	
N.L.			4.2	24 5	
T.P. N. of S. 6.11			31.65	321. - 25.04	12 1/2 of PC in distance
15+58.94 = PC.					
N.L.			6.7	25 0	
+ 2			6.62	25 03	
+ 7.5			6.68	24 97	
Top cb N			6.85	24 80	
Gut			7.3	24 3	
114			7.2	24 4	
⊕			6.8	24 8	
114			6.4	25 2	
Gut.			6.2	25 4	
Top cb S.			5.42	26 23	
+ 6.5			5.27	26 38	
+ 12			5.10	26 55	
S.L.			4.7	26 9	
Sec 1 on Curve = 15+85.88					
S.L.			4.4	27 2	
+ 2			4.17	26 68	
+ 7.5			5.07	26 58	
Top cb S.			5.17	26 48	
Gut			6.2	25 4	
114			6.2	25 4	
⊕			6.3	25 3	

Curve divided into 4 equal parts
 to intersection with Greene St.
 stationing is S.L.

2165

	+	T	-	Elev
114.			6.6	250
Gut			7.3	243
Top Cb N			6.50	2515
+ 6.5			6.31	2534
+ 12			6.13	2552
N.L.			6.0	256
Sec 2 on Curve = 16 + 12.81 on S.L.				
N.L.			5.8	258
+ 2			5.85	2580
+ 7.5			5.96	2569
Top Cb N.			6.14	2551
Gut.			6.9	247
114			6.5	251
6			6.1	255
114			6.0	256
Gut			3.9	257
Top Cb S.			5.09	2656
+ 6.5			4.92	2673
+ 12			4.83	2682
S.L.			3.9	27.7

Sec 2 - 10

2' dia Palm & 4' S. of S. Cb.

Sec 2 - 10

2' dia Palm & 4' N. of N. Cb.

16 + 32.3

Beginning of New Road walk on S. (Put in on Lobbie's job)

31.65

S Edge walk
N. "4.68
4.75

037

	+	T	-	Elev
Sec 3 on Curve =			16 + 39.77	
S.L.			4.3	273
+ 2			4.70	2695
+ 7.5			4.72	2693
Top Cb S.			4.83	2682
Gut			5.7	259
114			6.0	256
6			5.8	258
114			6.4	252
Gut			6.7	249
Top Cb N.			5.91	2564
+ 6.5			5.69	2596
+ 12			5.55	2610
N.L.			5.6	260

Sec 3 - 10

2' dia pine 4' N. of N. Cb.

Sec 3 + 15

1.7 dia palm 4' N. of N. Cb.

Sec 3 + 14

2' dia palm 3.5 S. of S. Cb.

16 + 51.3 = End of New Cb on Lobbie's

Job. Cb is on a radius ^{200'} something over 40'

Top Cb at end 4.80 26.85

31,65

+ T - Elev
 Sec 4 on Curve = 16+66.67 =

intersection of S.L. W. PT Loma & S.L.
 Greene St.

N.L.	5.4	262
+ 2	5.34	2630
+ 75	5.46	2619
Top Cb N.	5.67	2598
Gut	6.5	251
1/4	6.2	254
1/4	5.6	260
1/4	5.6	260
Cb line S.	5.7	259
+ 3.25 = Gut on Ret	5.6	260
Top Cb on Ret	4.75	2690
Cb line 8.7 = walk	4.69	2696
S.L. = "	4.65	2700

Sec 4 + 12

1.4 dia pine 2.5 S of S.Cb. on Return

From intersection of S.L.
 W. PT Loma & S.L. Greene, Curve
 divided into 6 equal parts to
 intersection of S.L. W. PT Loma Blvd
 & Prop. P.C. N. Easterly Line of Greene
 See Sketch.

31,65

+ T - Elev 038
 Sec 1 on Curve in Greene St, intersection
 S.L. Sta 16+93.66

S.L. intersects S.Cb of Greene Here

S.L. on Top of Cb.	4.43	2722
S.L. on Greene St permit	4.90	2675
S.Cb line	5.4	262
1/4	5.4	262
1/4	5.5	261
1/4	6.0	256
Gut	4.1	255
Top Cb N	5.57	2608
+ 6.5	5.31	2634
+ 12	5.16	2649
N.L.	5.2	264

Above Sec + 12

1 dia palm 4' N of N.Cb.

Sec 2 = 17+50.59

X.L.	4.9	267
+ 2	5.09	2656
+ 7.5	5.17	2648
Top Cb N	5.39	2626
Gut	6.0	256
1/4	5.9	257
1/4	5.4	262
1/4	5.0	266

31.65

	+	π	-	Elev
+ 13.2 = edge of Green St prmt	4.58			27 07
S.L.	4.56			27 09
+ 10 on prmt	4.58			27 07
Sec 3 = 17 + 47.52				
S.L. - 10 on prmt	4.25			27 40
S.L. " "	4.30			27 35
+ 1.35 = Edge prmt	4.85			27 30
S.Cb. Line	4.8			26 8
1/4	5.2			26 4
¢	5.4			26 2
1/4	5.8			25 8
GvT	5.9			25 7
Top. Cb. N.	5.12			26 53
+ 6.5	5.01			26 64
+ 12	4.95			26 70
N.L.	4.8			26 8

Sec 3 - 11

1.4 dia pine 4' N of N.Cb.

Sec 4 = 17 + 74.45

N.L.	4.4			27 2
+ 2	4.72			26 93
+ 7.5	4.17			26 78
Top Cb N	5.05			26 60
GvT	5.8			25 8
1/4	5.5			26 1

31.65

089

	+	π	-	Elev
¢	5.1			26 5
1/4	5.1			26 5
S.Cb Line	4.9			26 7
+ 12.9 = edge prmt	4.22			27 43
S.L. on " "	4.20			27 45
+ 10 " "	4.03			27 62
Sec 5 = 18 + 01.38				
- 10 on prmt	4.01			27 64
S.L. " "	4.15			27 50
+ 0.5 edge prmt	4.17			27 48
S.Cb Line	4.8			26 8
1/4	4.9			26 7
¢	4.9			26 7
1/4	5.4			26 2
GvT.	5.5			26 1
Top. Cb. N.	4.82			26 83
+ 6.5	4.64			27 01
+ 12	4.48			27 27
N.L.	4.3			27 3

Sec 5 - 12

1' dia pine 3.5' N of N.Cb.

Sec 5 + 14

1.5' dia palm 4' N of N.Cb.

18 + 09.10 = intersection of
S.L.W. Pt. Lamat Blvd & 23' R.Cb on N. Easterly
side of Greene St

	+	T	-	Elev
SL				
Top Cb			3.80	
Prmt.			4.20	
- 10 on Cb Return				
Top			3.76	
Prmt			4.13	
- 20 on Cb R.				
Top			3.63	
Prmt			4.11	
- 32 = P.C. on Greene				
Top Cb.			3.53	
prmt.			3.96	

Sec 6 = 18+28.35 = intersection
of S.L. W.P.T. from Blvd & P.C. of property
Block # 24 Ocean Beach Park

T.R.	1.65	32.58	3.72	27.93
N.L.			5.2	27.4
+ 7			5.24	27.34
+ 7.5			5.38	27.20
Top Cb N.			5.56	27.02
Gut			6.4	26.6
1/4			6.7	26.4
1/2			5.7	26.9
3/4			5.6	27.0
Gut			5.4	27.2
Top Cb S.			4.90	27.78

	+	T	-	Elev
+ 6.5			4.74	27.84
+ 12			4.65	27.93
SL			4.6	28.0
18+30 = P.C. Return S				
End of New Cb & Walk				
Top Cb.			4.83	27.75
Wedge walk			4.72	27.86
S. " "			4.65	27.93

From Prop P.C. Westerly end of Block 24
To prop P.C. Easterly end of Block 24
Curve is divided into 8 equal parts
Sections taken Radially &
Stationing on S.L.

Sec 1 = 18+54.71

S.L.			3.1	29.5
+ 2			4.31	28.21
+ 7.5			4.32	28.26
Top Cb S.			4.59	27.99
Gut			5.4	27.2
1/4			5.4	27.2
1/2			5.4	27.2
3/4			5.8	26.8
Gut			6.3	26.3
Top Cb N			5.37	27.21
+ 6.5			5.15	27.43

010

10' West of
P.C. 155' 1/2
Palm E. 5' 5" 1/2
Chion S.

	+	-	Elev
+12		5.01	27.57
N.L.		4.7	27.9
Sec 1 - 12			
1' dia pine		4' S. of S.Cb.	
Sec 1 - 14			
0.6' dia pine		4' N. of N.Cb.	
Sec 1 + 12			
2' dia palm		3.5' N. of N.Cb.	
Sec 2 = 18 + 81.11			
N.L.		4.7	27.9
+2		4.71	27.87
+7.5		4.87	27.71
Top Cb N		5.22	27.36
Gut		6.0	26.6
1/4		5.7	26.9
⊕		5.1	27.5
1/4		5.1	27.5
Gut.		5.2	27.4
Top Cb S.		4.25	28.33
+6.5		4.00	28.58
+12		3.94	28.64
S.L.		3.5	29.1

Sec 2 - 15
 2' dia palm 3.5' S. of S.Cb.

	+	-	Elev
Sta 3 = 19 + 07.51			
S.L.		3.3	29.3
+2		3.73	28.85
+7.5		3.74	28.84
Top Cb S.		3.98	28.60
Gut		5.0	27.6
1/4		4.8	27.8
⊕		4.8	27.8
1/4		5.4	27.2
Gut		5.6	27.0
Top Cb N.		4.95	27.73
+6.5		4.60	27.98
+12		4.47	28.11
N.L.		4.5	28.1

Sta 3 - 15'

1' dia pine 3.5' S. of S.Cb.

Sta 3 - 16'

1' dia pine 3.0' N. of N.Cb.

Sec 4 = 19 + 33.91

N.L.		4.2	28.4
+2		4.20	28.38
+7.5		4.34	28.24
Top Cb N		4.50	28.08
Gut		5.4	27.2
1/4		5.0	27.6

3258

	+	-	Elev
Q		4.4	282
1/2		4.5	281
Gut		4.8	278
Top Cb. S.		3.67	28.91
+ 6.5		3.55	29.08
+ 12		3.46	29.12
S.L.		2.5	30.1
Sec 4 - 16			
2' dia palm 4' N. of N. Cb.			
Sec 4 - 15			
2' dia palm 4' S. of S. Cb.			
Sec 5 = 19 + 60.31			
S.L.		2.3	30.3
+ 2		3.26	29.32
+ 7.5		3.28	29.30
Top Cb. S.		3.40	29.18
Gut		4.5	28.1
1/4		4.2	28.4
Q		4.0	28.6
1/4		4.7	27.9
Gut		5.2	27.4
Top Cb. N		4.21	28.37
+ 6.5		4.14	28.44
+ 12		3.91	28.67
N.L.		4.0	28.6

3258

	+	-	Elev
Sec 5 - 14			
1.2 dia pine 3.5' N. of N. Cb.			
Sec 6 = 19 + 86.71			
N.L.		3.7	28.9
4.2		3.72	28.86
+ 7.5		3.84	28.74
Top Cb. N		4.05	28.53
Gut		4.7	27.9
1/4		4.5	28.1
Q		3.8	28.8
1/4		3.8	28.8
Gut		4.2	28.4
Top Cb. S.		3.07	29.49
+ 6.5		2.92	29.66
+ 12		2.90	29.68
S.L.		2.0	30.6
Sec 6 - 14			
1.4 dia palm 3.5' N. of N. Cb.			
Sec 6 - 13			
1.0 dia palm 4' S. of S. Cb.			
Sec 7 = 20 + 13.11			
S.L.		2.3	30.3
+ 2		2.50	30.08
+ 7.5		2.61	29.97
Top Cb. S.		2.75	29.83

012

3258

	+	-	Elev
Gut		3.7	28.9
1/4		3.6	29.0
1/2		3.5	29.1
3/4		4.2	28.4
Gut		4.5	28.1
Top Cb N		3.77	28.81
+ 65		3.59	28.99
+ 12		3.52	29.06
N.L.		3.5	29.1

Sec 7 - 14

1.2 dia pine 3.5 N. of N. Cb.

Sec 7 - 14

1.0 dia pine 3.5 S. of S. Cb.

Sec 8 = Prop. P.C. W. Ebers = 20 + 39.58

N.L.		3.4	29.2
+ 2		3.24	29.34
+ 75		3.33	29.25
Top Cb N		3.55	29.03
Gut		4.0	28.2
1/4		4.0	28.6
1/2		3.3	29.3
3/4		3.3	29.3
Gut		3.3	29.3
+ 0.3 = Top Cb on Ret.		2.41	30.17
+ 65		2.38	30.20

3258

013

	+	-	Elev
+ 12		2.27	30.31
S.L.		2.0	30.6

Sec 8 - 14'

0.8 dia palm 3.5 N. of N. Cb.

Sec 8 - 14'

0.8 dia palm 3.5 S. of S. Cb.

20 + 35.5 = Cb P.C. New Cb Set by

Loebenstein & New W.

Top Cb @ P.C.

N. edge Walk

S. " Walk

From Prof. P.C. (Sec 8) to intersection
 of S.K. W. Pt Loma Blvd & E. Ebers, Curve
 divided into 4 equal parts, Sections
 Taken Radially & Stationing on S.L.

20 + 57.4

S.L. intersects 25.14' Cb Rating.

Top Cb		3.5	30.13	
Prmt.		2.94	29.64	
T.P.	3.77	34.79	1.56	31.02
S.2. W. Pt Loma - 10 on Ret.				
Top Cb		4.65	30.14	
Prmt		5.10	29.69	
- 20 Top Cb on Ret		4.57	30.22	
Prmt		5.00	29.79	

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3479

	+	-	Elev
- 29 = P.C. Cb. on Ebers			
Top Cb.	4.52		3027
Prmt	5.00		2979
Sec 1 = 20465.08			
S.L. - 10 on prmt	4.95		2984
S.L. " "	4.99		2980
+ 0.45 edge of prmt	4.11		2980
S. Cb Line	5.4		294
" "	5.3		295
♀	5.4		294
114	6.0		288
Gut	6.3		285
Top Cb N	5.55		2924
+ 4.5	5.32		2947
+ 12	5.20		2959
N.L.	5.3		295

Sec 1 - 12

1.4 dia pine 4' N. of N. Cb.

Sec 1 + 15

1.7 dia palm 4' N. of N. Cb.

Sec 2 = 20490.65

N.L.	5.1		297
+ 2	5.20		2959
+ 7.5	5.27		2952
Top Cb N.	5.49		2930

3479

	+	-	Elev
Gut		6.0	288
114		5.9	289
♀		5.7	296
114		5.2	296
S. Cb Line		5.2	296
+ 13.35 = Edge of Prmt		4.60	3019
S.L. on " "		4.60	3019
+ 10 " "		4.58	3021
Sec 3 = 21416.22			
- 10 on prmt		4.60	3019
S.L. " "		4.61	3018
+ 0.45 = edge of Prmt		4.64	3014
S. Cb Line		5.1	297
114		5.0	298
♀		5.1	297
114		5.7	291
Gut		5.7	291
Top Cb N.		5.40	2939
+ 6.5		5.17	2960
+ 12		5.10	2969
N.L.		5.2	296

Sec 3 - 11

1.5 dia. pine 4' N. of N. Cb.

012

34.79

	+	-	Elev
	21 + 28.44		
S.L. W.P. Loma intersects E Cb Ebers St			
Top Cb	4.13		30 66
Prmt	4.76		30 03
S.L. - 10 on E Cb Ebers			
Top Cb	4.07		30 72
Prmt	4.68		30 11
S.L. + 9.3 along E Cb line of Ebers: P.C. 30' R.			
Top Cb @ P.C.	4.19		30 60
Sec 4 = intersection of S.L. and			
W.P. Loma Blvd & E.L. of Ebers =			
	21 + 41.73		
N.L.	5.0		29 8
+ 2	5.12		29.67
+ 7.5	5.21		29 58
Top Cb N.	5.03		29 36
Gut	6.3		28 5
1/4	5.8		29 0
6	5.1		29 7
1/4	5.0		29 8
S Cb Line	5.0		29 8
+ 1.55 = Cb Ret Gut	5.0		29 8
Top Cb on Ret	4.21		30 50
S.L. on Walk	4.12		30 67

Sec 4 - 10

1.6 dia palm 3.5 N. of N. Cb.

34.79

045

	+	-	Elev
	21 + 71.23 = intersection of S.L. W.		
	P. Loma Blvd & S.L. Larkspur St.		
S.L. on Walk	4.41		30 38
+ 12.1 = Cb on 30' R. Ret	4.63		30 16
Gut	5.4		29 4
S. Cb Line	5.4		29 4
1/4	5.1		29 7
6	5.1		29 7
1/4	5.8		29 0
Gut	6.0		28 8
Top Cb N.	5.40		29 39
+ 6.3	5.27		29 52
+ 12	5.13		29 66
N.L.	5.1		29 7
Above Sta - 10			
0.8 dia pine 4' N. of N. Cb.			
Sta + 13			
2' dia palm 4' N. of N. Cb.			
Sta - 14			
1.4 dia palm 4' S. of S. Cb.			
Sta + 1.3			
1.4 dia pine 2.5' inside Cb on 30' R. Ret.			
21 + 63 = P.C. 30' R. on Larkspur St			
Top Cb @ P.C.	4.55		30 24

3477

	+	-	Elev
31 + 85.79 S.L. W. Pt Loma Blvd intersects S. Cb. Larkspur			
Top. Cb.		4.50	30 24
Prmt.		5.00	29 79
Above R.I. + 13 along S. Cb. of Larkspur			
P.C. of 20' R.			
Top of Cb		4.62	30 17
P.I. - 10 along S. Cb. of Larkspur			
Top Cb.		4.49	30 30
Prmt.		4.95	29 84
T.P. Top Hyd 425	36.75	2.29	32.50
T.P.	4.40	36.27	4.88
S.M.B.R. for check		6.15	30.12
T.P. Top Hyd 093	33.43		33.50
N.L.			
N.L.		3.9	29 5
12		3.89	29 54
+ 7.5		3.94	29 49
Top. Cb. N		4.20	29 23
Got		4.7	28 7
14		4.5	28 9
2		3.9	29 5
14		3.9	29 5
Cb Line S.		3.9	29 5

22 + 03.59 = P.C.

3343

046

	+	-	Elev
+ 138 = Edge of prmt S.L.		3.48	29 95
+ 10		3.48	29 95
22 + 15.45			
- 10		3.37	30 06
S.L. on prmt		3.50	29 93
S Cb Line		3.8	29 6
14		3.9	29 5
2		4.0	29 4
14		4.6	28 8
Got		4.6	28 8
Cb Line Cb gone		4.3	29 1
+ 6.5		3.99	29 46
+ 12		3.90	29 53
N.L.		3.9	29 5
Above Sta - 5			
19 dia pine 3.5 N of N. Cb			
22 + 27.31			
N.L.		4.0	29 4
+ 2		3.97	29 46
+ 7.5		4.09	29 34
Top Cb N		4.77	29 16
Got		4.8	28 6
14		4.6	28 8
2		4.0	29 4

	+	-	Elev
1/4		3.9	29 5
S. Cb line		4.0	29 4
S.L. on prmt		3.56	29 87
+ 10		3.38	30 05
22 + 39.17			
- 10 on prmt		3.55	29 88
S.L. " "		3.68	29 75
S Cb Line		4.1	29 3
1/4		4.0	29 4
⊕		4.1	29 3
1/4		4.6	28 8
Gut		4.9	28 5
Cb Line Cb gone		4.3	29 1
+ 6.5		4.13	29 30
+ 12		4.02	29 41
N.L.		4.1	29 3
Above Sta - 4			
14 diapalm	4' N. of N. Cb line		
22 + 50.03 = intersection of			
S.L. & Easterly Cb of Larkspur, on Ret.			
N.L. (walk & Cb gone)		4.0	29 4
N Cb line		4.7	28 7
Gut		3.0	28 4
1/4		4.7	28 7
⊕		4.1	29 3

	+	-	Elev
1/4		4.1	29 3
S Cb line		4.2	29 2
S.L. on prmt		3.92	29 51
Top Cb.		3.54	29 89
S.L. + 10 around Ret			
Top Cb		3.48	29 95
on prmt		3.90	29 53
+ 20	" "	3.37	30 06
		3.83	29 60
+ 27 = P.C. Larkspur			
Top Cb.		3.28	30 15
prmt.		3.76	29 67
22 + 69.90 = Prof P.C. Larkspur			
at W. Pt. Loma			
S.L.		3.2	30 2
+ 1.8 walk		3.46	29 96
+ 7.5		3.56	29 87
Cb Top 5		3.62	29 81
Gut		4.1	29 3
1/4		4.2	29 2
⊕		4.2	29 2
1/4		4.7	28 7
Gut		3.0	28 4
Top Cb N		4.40	29 03
+ 6.5		4.13	29 30

	+	-	Elev.
+12		4.13	29.30
N.L.		4.1	29.3
Above Sta - 8			
1' dia pine	4'	N. of N.Cb.	
22+71 = end of Goodwalk put in on Loebie's Job			
S Edge of Walk		3.48	29.95
N " " "		3.57	29.86
22+74 = end of 8' db put in on Loebie's Job			
Top Cb		3.65	29.78
22+94.9			
N.L.		4.2	29.2
+2		4.30	29.13
+7.5		4.40	29.03
Top Cb N		4.55	28.88
Got		5.3	28.1
"		4.8	28.6
"		4.3	29.1
"		4.4	29.0
Got		4.4	29.0
Cb line Cb gone		3.8	29.6
S.L. (walk gone)		3.4	30.0
Sta - 9'			
2' dia palm	4'	N. of N.Cb.	

	+	-	Elev.
1.8 dia palm	3.5	S. of S.Cb.	
23+19.9			
S.L. walk gone		3.7	29.7
S.Cb line		3.9	29.5
Got		4.6	28.8
"		4.3	28.9
"		4.5	28.9
"		5.0	28.4
Got		5.5	27.9
Top Cb N		4.74	28.69
+6.5		4.53	28.90
+12		4.46	28.97
N.L.		4.5	28.9
Sta - 5'			
1' dia pine	3.5	S. of S.Cb.	
Sta - 8'			
1' dia pine	3.5	N. of N.Cb.	
23+44.90			
N.L.		4.8	28.6
+2		4.62	28.81
+7.5		4.65	28.78
Top Cb N		4.77	28.56
Got		5.6	27.8
"		5.7	28.2
"		4.7	28.7

3343

	+	π	-	Elev
1/4			4.7	287
Gut			4.78	286
Top Cb			4.17	29.26
+ 6.5			4.01	29.42
+ 12			3.90	29.53
S.L.			3.7	29.7

Sta - 8

2' dia palm 3.5 N. of N.Cb.

23 + 69.90

S.L.			3.8	29.6
+ 2			4.02	29.41
+ 7.5			4.08	29.35
Cb Line Cb gone			4.46	29.03
Gut			5.0	28.4
1/4			4.9	28.5
⊕			5.0	28.4
1/4			5.5	27.9
Gut			5.8	27.6
Top Cb N			5.05	28.38
+ 6.5			4.88	28.55
+ 12			4.80	28.63
N.L.			4.9	28.5

Sta - 8

1' dia pine 3.5 N. of N.Cb

Sta - 5

1.4' dia pine 3.5 S. of S.Cb.

3343

23 + 90.68 = W.L. Alley. No Returns

	+	π	-	Elev
N.L.			5.4	28.0
+ 2			4.97	28.46
+ 7.5			5.06	28.37
Top Cb N			5.22	28.21
Gut			6.1	27.3
1/4			5.7	27.7
⊕			5.1	28.3
1/4			5.1	28.3
S.Cb line			5.0	28.4
S.L.			4.0	29.4

Sta - 4

1.5' dia palm 3.5 N. of N.Cb.

24 + 12.59 = E.L. Alley

S.L.			4.4	28.8
+ 2			4.26	29.17
+ 7.5			4.39	29.05
Cb Line Cb gone			4.30	29.13
Gut			5.2	28.2
1/4			5.3	28.1
⊕			5.3	28.1
1/4			5.9	27.5
Gut			6.2	27.2
Top Cb N			5.43	28.00

019

	+	T	-	Elev
+ 6.5			5.14	2829
+ 12			5.14	2829
N.L.			5.3	28.1
Sta - 1				
1' diapine 2.5 S. of S. Cb.				
Sta - 2				
1' diapine 3.5 N. of N. Cb.				
2444.90				
N.L.			5.4	280
+ 2			5.24	2819
+ 7.5			5.31	2812
Top Cb N			5.57	27.86
Gut			6.4	270
114			6.0	274
⊕			5.4	280
114			5.5	27.9
Gut			5.4	280
Top Cb S			4.70	28.73
+ 6.5			4.56	28.87
+ 12			4.42	2901
S.L.			4.7	28.7

Sta - 10
 1' diapalm 3.5 S. of S. Cb.
 Sta - 9
 1.5' dia. palm 3.5 N. of N. Cb.

	+	T	-	Elev
				24469.90
S.L.			4.2	292
+ 2			4.52	2891
+ 7.5			4.4	2879
Top Cb S.			4.80	2863
Gut			5.6	278
114			5.6	278
⊕			5.5	27.9
114			6.2	272
Gut			6.5	269
Top Cb N			5.74	2769
+ 6.5			5.41	2802
+ 12			5.42	2801
N.L.			5.7	27.7

Sta - 7
 1' diapine 3.5 N. of N. Cb.
 Sta - 9
 1' diapine 3.5 S. of S. Cb.
 T.P. 5.10 32.19 6.34 27.09
 24494.90
 N.L. 4.5 27.7
 + 2 4.22 27.97
 + 7.5 4.33 27.86
 Top Cb N 4.54 27.65
 Gut 5.2 27.0

32.19

	+	-	Elev
1/4		5.0	27 2
♀		4.5	27 7
1/4		4.5	27 7
Gut		4.3	27 9
Top Cb. S.		3.68	28 51
+ 6.5		3.56	28 63
+ 12		3.41	28 78
S.L.		3.2	29 0
Sta - 9			
2.0 diapalm	4'	N. of N. Cb.	
Sta - 8			
1.2 diapalm	4'	S. of S. Cb.	
25 + 17.90			
S.L.		3.0	29 2
+ 2		3.58	28 61
+ 7.5		3.65	28 54
Top Cb S		3.76	28 43
Gut		4.5	27 7
1/4		4.6	27 6
♀		4.6	27 6
1/4		5.1	27 1
Gut		5.3	26 9
Top Cb N		4.64	27 55
+ 6.5		4.37	27 82
+ 12		4.30	27 89

32.19

	+	-	Elev
N.L.		4.6	27 6
Sta - 9			
1' diapine	30	N. of N. Cb.	
Sta - 8			
1' diapine	35	S. of S. Cb.	
25 + 58.90 = F.P.C. of 20' R. Castellar			
N.L.		4.7	27 5
+ 2		4.62	27 57
+ 7.5		4.75	27 44
Top Cb. N.		4.96	27 23
Gut.		5.6	26 6
1/4		5.2	27 0
♀		4.8	27 4
1/4		4.8	27 4
Gut		4.6	27 6
Top Cb S.F.C.		4.06	28 13
+ 6.5		3.86	28 33
+ 12		3.82	28 37
S.L.		3.4	28 8
25 + 58.71 = intersection of			
S.L. W. Pt. Lomo Blvd & S.L. Castellar			
25 + 63.6 = F.P.C. of 20' R. Return Castellar			
S.L. on Walk		3.70	28 49
+ 8.4 Top Cb @ F.C.		3.75	28 24
Gut		4.7	27 5

051

	+	T	-	Elev
S. Cb Line			4.7	27.5
1/4			4.7	27.5
⊕			4.9	27.3
1/4			5.3	26.9
Gut			5.7	26.5
Top Cb N			5.05	27.14
+ 6.5			4.81	27.38
+ 12			4.71	27.48
N.L.			4.8	27.4

Sta - 3

1.4 diapine 3.5 N. of N. Cb.

2.5474.52 = intersection of S.L.

W. Pt. Loma & S. Cb Castellar

N.L.			5.0	27.2
+ 2			4.76	27.43
+ 7.5			4.88	27.31
NCB Line Cb line			5.1	27.1
Gut			5.7	26.5
1/4			5.3	26.9
⊕			4.8	27.4
1/4			4.6	27.6
SCB Line			4.4	27.8
S.L. on prmt.			4.04	28.15
+ 10 along SCB of Castellar			3.59	28.61
Top Cb			3.24	28.95
Prmt			3.76	28.43

	+	T	-	Elev
			2.5 + 90.12	
- 10 on prmt			3.41	28.78
S.L. " "			3.69	28.51
S. Cb Line			4.2	27.0
1/4			4.7	27.5
⊕			5.0	27.2
1/4			5.4	26.8
Gut			5.7	26.5
Top Cb N			5.08	27.11
+ 6.5			4.84	27.35
+ 12			4.77	27.42
N.L.			4.9	27.3

Sta - 5

2' diapalm & N. of N. Cb.

2.6406.52

N.L.			4.8	27.4
+ 2			4.84	27.35
+ 7.5			4.90	27.29
Top Cb			5.15	27.04
Gut			5.9	26.3
1/4			5.4	26.8
⊕			5.0	27.2
1/4			4.7	27.5
S. Cb.			4.4	27.8
S.L. on prmt			3.50	28.69
+ 10 " "			3.17	29.02

	+	-	Elev
	26+11		
0.7 diapine	3.5	N. of N. Cb.	
	26+22.52		
- 10 on print	3.05		29 14
S.L. " "	3.45		28 74
S. Cb Line	4.6		27 6
1/4	4.7		27 5
⊕	5.0		27 2
1/4	5.6		26 6
Gut	6.2		26 0
Top Cb N	5.37		26 92
+ 6.5	5.09		27 10
+ 12	4.98		27 21
N.L.	5.2		27 0
26+38.52 = intersection of			
S.L. with E. Cb of Castellaron ^{2nd} Return			
N.L.	5.4		26 8
+ 2	5.09		27 10
+ 7.5	5.15		27 04
Top Cb N	5.31		26 87
Gut	6.4		25 8
1/4	5.6		26 6
⊕	4.9		27 3
1/4	4.7		27 5
S. Cb Line	4.4		27 8

	+	-	Elev
S. Lionbrmt	3.59		28 60
S.L. Top Cb.	3.12		29 07
+ 13 around Ret			
Top Cb	2.65		29 54
Print	3.13		29 06
+ 26 = P.C. on Castellaron			
Top Cb	2.22		29 97
Print	2.68		29 51
26+48.3 = inlet of 16" iron pipe			
culvert on N. (intended top on line bet Lots 4 & 48?)			
inlet / lowline	7.13		24 06
Top Cb.	6.29		26 90
N.L.	5.3		26 9
+ 50' N	9.1		23.1
+ 100' N	16.4		15 8
+ 105' N	16.0		16 2
+ 110 outlet of existing pipe	17.4		12 8
+ 111	26.9		5.3
+ 120	29.0		3 2
+ 144 } present tideline	32.7		- 0.5
+ 145	34.0		- 1.8
26+58.02 = Prob'ly P.C. S. Cb 15 0.6 in there			
S.L.	3.0		29 2
+ 19 } end of New Walk	3.53		28 66
+ 7.5 } and Cb set outside	3.59		28 60
Top Cb. 5 @ P.C. of Ret	3.72		28 47

053

1.7 diapine
4' N. of N. Cb on this station

D. L. B.
Please Note

3219

	+	T	-	Elev
Gut			4.6	27.6
114			4.7	27.5
♀			4.8	27.4
114			5.4	26.8
Gut			6.0	26.2
Top Cb N			5.23	26.96
+ 6.5			5.06	27.14
+ 12			4.95	27.24
N.L.			5.2	27.0

Sta + 3

0.7 dia pine 3.5 S of S.Cb
26 + 81.52 S.Cb is 0.7 in st.

N.L.			4.8	27.4
+ 2			4.61	27.58
+ 7.5			4.80	27.39
Top Cb N			4.95	27.24
Gut			5.6	26.6
114			5.2	27.0
♀			4.6	27.6
114			4.6	27.6
Gut			4.6	27.6
Top Cb S.			3.70	28.49
+ 6.5			3.47	28.72
+ 12			3.39	28.80
S.L.			2.7	29.5

3219

051

+ T - Elev

Stat 4

1.7 dia palm 4' N of N.Cb
1.2 " " 4' S of S.Cb.
 $27 + 04.63 = P.C. S.Cb. 0.85 \text{ in st.}$

S.L.			1.5	30.6
+ 2			3.24	28.95
+ 7.5			3.31	28.88
Top Cb S			3.46	28.73
Gut			4.5	27.7
114			4.4	27.8
♀			4.4	27.7
114			4.9	27.3
Gut			5.3	26.9
Top Cb N			4.58	27.61
+ 6.5			4.40	27.79
+ 12			4.30	27.89
N.L.			4.5	27.7

Stat 7

0.6 dia pine 3.0 S of S.Cb.
0.8 " " 3.5 N of N.Cb.
Curved divided into 6 equal parts.
Stations taken Radially & Stationed on S.L.

N.L.			3.6	28.6
------	--	--	-----	------

Sec A = 27 + 38.96

32.19

	+	π	-	Elev
+ 2			3.60	28 59
+ 7.5			3.75	28 44
Top Cb N			3.95	28 24
Gut			4.8	27 4
1/4			4.0	27 8
⊥			4.0	28 2
1/4			4.2	28 0
Gut			4.1	28 1
Top Cb S			3.23	28 96
+ 6.5			2.99	29 20
+ 12			2.90	29 29
S.L.			2.8	29.4

Sta - 1

1.3 dia palm 4' N of N.Cb.
 2.2 " " 4' S of S.Cb.

Sec B = 27 + 73.29 S.Cb 0.7m st.

S.L.			2.5	29 7
+ 2			2.64	29 55
+ 7.5			2.69	29 50
Top Cb S			2.90	29 29
Gut			3.7	28 5
1/4			3.8	28 4
⊥			3.6	28 6
1/4			3.9	28 3
Gut			4.3	27 9

32.19

	+	π	-	Elev	55
Top Cb N			3.40	28 79	
+ 6.5			3.22	28 97	
+ 12			3.09	29 10	
N.L.			3.0	29 09	

Sta - 7

1' dia pine 4' S of S.Cb.

1' dia " 3.5' N of N.Cb.

Sec C = 28 + 0 7.62 Cb sat.

N.L.			2.7	29 5
+ 2			2.63	29 56
+ 7.5			2.83	29 36
Top Cb N			3.04	29 15
Gut			3.9	28 3
1/4			3.5	28 7
⊥			3.1	29 1
1/4			3.4	28 8
Gut			3.5	28 7
Top Cb S			2.45	29 74
+ 6.5			2.25	29 94
+ 12			2.12	29 05
S.L.			2.0	30 2

Sec C - 17

1.4 dia palm 3.5' N of N.Cb.

1.4 " " 3.5' S of S.Cb.

T.p. 500 34.64 2.55 29.64

	+	T	-	Elev
	Sec D = 28 + 41.95 S.Cb 0.4 Top of S.			
S.L.			4.3	303
+ 2			4.23	3041
+ 7.5			4.27	3037
Top Cb S. = 5.4 + 13.6			4.46	3018
Gut.			5.5	291
1/4			5.4	292
⊕			5.1	29.5
1/4			5.7	289
Gut			6.2	284
Top Cb N.			5.31	2933
+ 6.5			5.22	2942
+ 12			5.06	2958
N.L.			4.8	29.8

Sec D

1.6 dia palm 4' N. of N.Cb
 1.0 " " 4' S. of S.Cb.

Sec E = 28 + 76.28 S.Cb 4' 11" Back

N.L.			4.8	298
+ 2			4.83	2981
+ 7.5			5.00	2964
Top Cb N			5.13	2951
Gut			5.9	287
1/4			5.4	292
⊕			4.9	297

	+	T	-	Elev
	56			
1/4			5.2	294
Gut			5.0	296
Top Cb S. = 4.2 m			4.99	3035
+ 6.5			4.07	3051
+ 12			4.00	3064
S.L.			4.0	306

Sec F - 6

0.7 dia pine 3.5 N. of N.Cb.

Sec E - 2

0.7 dia pine 4.0 S. of S.Cb.
29 + 0.7 = 29.7
 29 + 10.60 = E.C.

S.L.			3.98	3066
+ 2			4.00	3064
+ 7.5			4.03	3059
Top Cb S. outline			4.23	3041
Gut			4.8	298
1/4			4.7	299
⊕			4.7	299
1/4			5.3	293
Gut			5.8	288
Top Cb N			5.09	2955
+ 6.5			4.83	2981
+ 12			4.78	2986
N.L.			4.0	301

P.C. - 14
 2' dia palm 4' N. of N.Cb.
 " " " 4' S. of S.Cb.

2464

	+	π	-	Elev
T.P. Wallin Pole	4.66	32.32	6.98	27.68
	29+35.60			
N.L.			2.0	303
+ 2			2.36	2996
+ 7.5			2.46	2986
Top Cb N			2.71	2961
Gut			3.6	287
1/4			3.0	293
1/2			2.4	299
1/4			2.7	296
Gut			2.7	296
Top Cb S.			1.90	3042
+ 6.3			1.76	3036
+ 12			1.65	3067
S.L.			1.5	308

P.C. - 12

1.2 dia palm 4' S. of S.Cb.

1.5 " " 4' N. of N.Cb

29+23

0.8 dia pine 4' N. of N.Cb.

0.4 " acacia 4' S. of S.Cb.

29+46

1' dia palm 4' N. of N.Cb

29+49

1.5 dia palm 3.5 S. of S.Cb.

32.32

57

	+	π	-	Elev
	29+60.6			
S.L.			1.3	310
+ 2			1.83	3049
+ 7.5			1.91	3041
Top Cb S.			2.16	3016
Gut.			3.2	291
1/4			3.0	293
1/2			2.6	297
1/4			3.1	292
Gut			3.7	286
Top Cb N.			2.70	2962
+ 6.5			2.52	2980
+ 12			2.31	3001
N.L.			2.1	302

29+72

0.6 dia pine 3.5 N. of N.Cb.

29+85.6

N.L.			2.4	299
+ 2			2.53	2979
+ 7.5			2.65	2967
Top Cb N			2.83	2945
Gut			3.8	285
1/4			3.3	290

	+	-	Elev
↓		2.8	29.5
1/4		3.1	29.2
Gut		3.4	28.9
Top Cb S		2.38	29.94
+ 6.5		2.09	30.22
+ 12		2.07	30.25
S.L.		1.8	30.5
29 + 97			
2.7 dia palm	4' N. of N.Cb.		
29 + 97			
1.4 dia palm	4' S. of S.Cb.		
30 + 10.6			
S.L.		2.0	30.3
+ 2		2.25	30.07
+ 7.5		2.33	29.99
Top Cb S.		2.59	29.73
Gut		3.0	28.8
1/4		3.4	28.9
↓		3.0	29.3
1/4		3.5	28.8
Gut		4.0	28.3
Top Cb N		3.10	29.22
+ 6.5		2.96	29.36
+ 12		2.81	29.51
N.L.		2.9	29.4

	+	-	Elev
		3.0 + 2.5	
0.6 dia pine	35' S. of S.Cb.		
30 + 35.6			
N.L.		3.4	28.9
+ 2		3.72	29.10
+ 7.5		3.39	28.93
Top Cb N		3.56	28.76
Gut		4.5	27.8
1/4		4.0	28.3
↓		3.4	28.9
1/4		3.7	28.6
Gut		3.9	28.4
Top Cb S.		2.91	29.41
+ 6.5		2.49	29.63
+ 12		2.59	29.73
S.L.		2.3	30.0
30 + 48			
1' dia palm	3.5' S. of S.Cb.		
2' " "	4' N. of N.Cb.		
30 + 60.6			
S.L.		2.7	29.6
+ 2		2.90	29.38
+ 7.5		3.03	29.29
Top Cb S (is 0.2 in st.)		3.79	29.03
Gut		4.3	28.0

	+	T	-	Elev
		?	Street	
S.L.			5.0	273
S.Cb. Line			5.3	270
1/4			5.4	269
⊕			5.6	267
1/4			6.1	262
GUT			6.5	258
To Cb. N.			5.84	2648
+ 6.5			5.69	2663
+ 12			5.54	2678
N.L.			6.0	263
		E. 1/4	? St.	
- 21 = ⊕ Garagon Abrasive			6.06	2626
N.L. on apron drive			6.06	2626
+ 2			6.02	2630
+ 7.5			6.10	2622
Cb. Line (driveway)			6.7	256
1/4			6.6	257
⊕			5.9	264
1/4			5.6	267
S.Cb. Line			5.4	269
S.L.			5.2	271

E 1/4 + 5

4.3' x 2.9' Concrete Box inlet with 3.1' x 1.6'
grating 2.2' out from S.Cb.

	+	T	-	Elev	60
Top Grating ⊕			7.08	2524	
Flow Line Box @ 14" iron pipe drain			8.38	2394	
E.Cb. ? St					
S.L.			4.6	277	
+ 7			4.0	283	
S.Cb. Line			5.0	273	
1/4			5.3	270	
⊕			6.0	263	
1/4			6.6	257	
N.Cb. Line (driveway)			7.0	253	
+ 6.5			6.35	2597	
+ 12			6.34	2598	
N.L.			6.04	2628	
		E.Cb. + 4.7 = End of Cb. Walk on			
North Side.					
Top Cb. at end			6.56	2576	
E.Cb. + 8					
- 30			8.1	242	
N.L.			6.4	259	
Cb.			6.6	257	
1/4			6.3	260	
⊕			5.7	266	
1/4			5.1	272	
Cb			5.0	273	
S.L.			5.0	273	

3232

+ T - Elev
E.L. ? St = 0400

S.L.		5.6	267
Cb.		6.0	263
+ 3		4.6	277
114		5.1	272
♀		5.7	266
114		6.2	261
Cb.		6.5	258
N.L.		6.6	257
+ 20		8.3	240
T.P.	0.44 28.10	4.66	27.66
	0405		
- 40		8.0	201
N.L.		6.4	21.7
Cb.		5.7	230
+ 10		1.9	262
114		2.0	261
♀		1.6	265
114		0.9	272
+ 10		1.2	269
Cb.		3.4	247
S.L.		4.8	233
+ 15		5.3	228
+ 50		0.0	281

2810

+ T - Elev 61
0 + 13

-50		1.9	262
-45		4.7	234
S.L.		6.4	217
S.Cb.		6.1	220
+ 10		1.1	270
114		1.1	270
♀		2.0	261
+ 11		2.5	256
114		3.9	242
N.Cb.		10.8	173
N.L.		11.3	168
+ 40			
T.P.	2.39 20.06	10.43	17.67
	0 + 24		
- 40			
N.L.		12.0	80
Cb.		10.5	9.5
114	0.5		20.6
+ 6	4.7		24.8
♀	5.0		25.1
+ 10	5.3		25.4
114	3.9		24.0
+ 9		2.5	17.5
Cb.		2.3	17.7

20.06

	+	π	-	Elev
S.L.	1.6			21.7
+ 33	16			21.7
+ 35	2.7			22.8
+ 46	4.0			24.1
+ 50	7.7			27.8
- 60	6.7	0 + 31		57.0
- 45	2.0			22.1
- 10	1.0			21.1
S.L.			1.9	18.1
cb			4.8	15.2
+ 5			4.8	15.2
1/4	2.8			22.9
+ 7	4.9			25.0
2	4.3			24.4
+ 7	4.0			24.1
1/4			0.1	19.9
cb.			10.8	9.2
+ 5			13.2	6.8
N.L.			14.4	5.6
+ 50			18.5	1.5
- 50		0 + 36	19.6	0.4
- 27			18.7	1.3
- 10			18.5	1.5
- 3			15.2	4.8
N.L.			14.9	5.1
+ 10			14.4	5.6
cb.			11.8	8.2

20.00

62

	+	π	-	Elev
1/4			0.9	19.1
+ 4	2.9			23.0
2	4.5			24.6
+ 5	4.8			24.9
1/4			0.4	19.6
+ 8			6.7	13.3
cb.			8.0	12.0
+ 13			7.5	12.5
S.L.			2.9	17.1
+ 12			2.3	17.7
+ 30	1.1			21.2
+ 50	0.5			20.5
+ 60	2.1			22.2
- 60		0 + 42	0.9	19.1
- 48 Top of Rubble Wall			4.0	16.0
- 48 bottom " "			6.5	13.5
- 47 Top of Rubble wall			1.2	18.8
+ 1 Bottom " "			2.6	17.4
cb.			9.3	10.7
+ 7			8.7	11.3
+ 7			8.1	11.9
1/4			5.1	14.9
2	3.7			23.8
+ 7	3.2			23.3
1/4			4.8	15.2
cb			14.2	15.8
+ 2			15.5	14.5
N.L.			16.3	13.7
+ 10			20.8	- 0.8
+ 50			20.4	- 0.4

20.06

STB 0+50

	+	-	Elev
S.L. -60		12.0	80
-30 Bottom of Rubble Wall		17.6	24
-30 Top " " "		9.2	108
-20 Bottom of " " "		18.2	18
-20 Top " " "		13.2	68
S.L. Bottom " " "		16.7	33
S.L. Top of End " " "		11.8	82
+7		15.9	4.1
Cb.		12.7	73
+4		10.5	95
114		8.0	120
⊕		2.3	17.7
+2	1.3		21.4
+12		3.7	163
114		8.7	11.1
Cb.		16.5	35
N.L.		17.8	22
+10 Top of Bulkhead		20.6	-06
+10 Bottom " " "		22.2	-22
+50 Top of " " "		21.2	-12
+50 Bottom " " "		23.2	-32
T.P.	2.74	9.88	12.92
			7.14
		0+55	
-50		14.4	-4.5
-10		12.5	-2.6

9.88

	+	-	Elev
N.L.		8.7	12
Cb.		4.7	32
+11		0.9	90
114	4.9		14.8
+10	7.4		17.3
⊕	4.2		14.1
114		3.9	60
Cb.		4.6	53
+7		7.7	2.2
S.L.		7.4	2.5
+40		8.2	1.7
+50		5.7	4.2
+70		8.1	1.8
		0+60	
+70		11.1	-1.2
+50		9.3	06
+30		12.0	-21
S.L.		13.4	-35
+10		12.1	-22
+11		9.2	07
Cb.		8.5	14
114		6.3	3.6
⊕	4.7		14.6
114	1.5		10.4
+7	0.9		108

	+	π	-	Elev.
		9.88		
+ 3			3.0	69
Cb			8.5	1.4
+ 10			9.8	01
N.L.			10.2	- 03
+ 10			12.7	- 28
+ 30			13.6	- 37
+ 50			14.0	- 4.1
	0 + 7.0 = outlet Colvret on N. 6. 4 & Tanker S.			
- 50			14.2	- 43
- 25			14.2	- 43
N.L.			12.2	- 23
+ 10			10.9	- 1.0
Cb			12.4	- 25
	Flowline of N. 9. Colvret on Cb line 11.30			
				- 14
+ 2			8.5	14
114			4.3	56
⊕			1.7	82
+ 4			2.2	77
+ 5			3.8	61
114			7.7	20
+ 8			8.4	1.5
Cb.			9.6	03
+ 3			10.6	- 08
+ 5			15.2	- 53
S.L.			16.7	- 6.8

	+	π	-	Elev.	64
		9.88			
+ 29			15.4	- 5.5	
+ 32			11.0	- 1.1	
+ 40			14.6	- 4.7	
+ 70			14.3	- 4.4	
	+ 83.5 = P.I.				St. with Lamp Bl'd with N. line Sea Side
- 70			15.0	- 5.1	
- 40			15.0	- 5.1	
- 32			11.1	- 1.2	
S.L.			11.1	- 1.2	
Cb.			10.6	- 0.7	
+ 8			13.3	- 3.4	
114			12.9	- 3.0	
⊕			10.7	- 0.8	
114			11.9	- 2.0	
Cb.			12.2	- 2.3	
N.L.			12.8	- 3.0	
+ 20			14.2	- 4.3	
+ 50			14.2	- 4.3	
	+ 85.96 = P.I.				N.L. with Lamp Bl'd with N. line Sea side Diagonal Sec.
- 50			14.2	- 4.3	
N.L.			14.6	- 4.7	
12' Not Sh. on diagonal			14.8	- 4.9	
S.L.			11.1	- 1.2	
T.P.	2.68	3.15	9.41	0.47	Nail in Test

Flood
Barrel
Runway

X Sec From Front to W. Pt. Loma Blvd
3.15
Sea Side St. 50' 10' to 7 1/2' 1/2's

+ - Elev
Sec "A" See Sketch P. 14

W.L.	8.0
Cb.	8.2
1/4	8.3
+	8.2
1/4	8.5
Cb. = edge of slough channel	9.2
E.L.	9.8
+ 11 = edge of slough channel	9.3
+ 50	7.4

"AA" = Section taken N. from P.I. N.L. W. Pt. Loma Blvd
W.L. Seaside R.H. to W. Pt. Loma Blvd

50' N. of P.I. = edge of channel	7.6
50' " " " = channel	10.2
P.I.	9.8
30' S. of P.I.	9.0
60' S. " "	8.4

See B. see sketch

E.L. - 50 = channel	8.4
- 30 = edge "	8.2
E.L.	8.0
Cb	8.1
1/4	8.3
+	8.2
1/4	8.4

Plotted 3-27-30

3.15

+ - Elev

Cb.	8.4
+ 6	8.0
+ 10	4.5
W.L.	4.4

0+00 = Sec. C. see sketch

W.L.	4.4	-12
Cb.	4.6	-15
1/4	7.2	-40
+ 2	8.1	-50
+	8.3	-5.1
1/4	8.3	-5.1
Cb	8.2	-5.0
E.L.	8.2	-5.0
+ 50	8.3	-5.1

0+11

- 50	8.2	-5.0
E.L.	8.1	-5.0
Cb	8.3	-5.1
+ 2	8.4	-5.2
1/4 = edge Tank	4.4	-12
+ 4	4.9	-1.7
+	6.2	-3.0
1/4	8.1	-5.7
Cb	9.4	-6.2
W.L.	9.2	-6.0

65

	+	T	-	Elev
		3.0		
+ 6			6.2	-3.0
+ 8 Top Tank Bank			3.0	-0.2
+ 19 Base of Rubble Wall			0.0	3.2
			0 + 35	
- 1' Base of Rubble Wall			0.5	
W.L. Top Tank			2.8	0.3
+ 1			6.1	-3.0
Cb.			8.9	-5.7
+ 4			8.0	-4.8
+ 5			4.5	-3.3
1/4 Top Tank			5.0	-1.8
+ 3 " "			4.3	-1.1
Φ			6.0	-2.9
+ 5			8.2	-5.0
W			8.4	-5.2
Cb.			8.7	-5.2
E.L.			8.4	-5.2
+ 50			7.9	-4.7
			0 + 35	
- 50			8.0	-4.8
F.L.			8.3	-5.2
Cb.			8.4	-5.2
1/4			8.3	-5.1
+ 2			8.1	-4.9
Φ			6.5	-3.4

	+	T	-	Elev
		3.15		
+ 5 Top Tank			4.1	-1.0
W			4.0	-0.8
+ 3			4.6	-1.4
Cb.			1.7	1.5
W.L. Base of Rubble Wall			1.2	1.9
+ 2			4.1	
+ 10			7.0	
T.P.	997	12.84	0.28	2.87
			0 + 38	
- 15 Top Rubble Wall				
- 13 Bottom " "			1.7	11.1
W.L. Top " "			3.6	9.2
+ 3 Bottom " "			10.6	2.2
Cb.			11.5	1.3
W			11.4	1.4
Φ			13.6	-0.8
W			16.2	-3.4
Cb.			17.5	-4.7
+ 2			17.8	-5.0
E.L.			15.1	-5.3
+ 15			17.7	-4.9
			0 + 49	
- 50			17.6	-4.8
- 15			17.4	-4.6
E.L.			16.4	-3.6

	+	⊗	-	Elev
Cb.			11.9	0.9
1/4			9.3	3.5
R			6.9	5.9
+4 = Cor. Rubble Wall			6.4	3.4
+5 = " " " Top			2.4	10.4
1/4			2.2	10.6
Cb			1.2	11.6
W.L. Bottom Rubble Wall			1.1	11.7
+1 Top	5.8	"		18.6
+10	8.1			20.9
+20	10.2			23.0
		+59		
-20	8.9			21.7
W.L.	8.8			21.6
Cb	6.8			19.6
+4	6.1	Cor. Rubble Wall		18.9
+5	3.2	Bot " "		16.0
1/4	2.5			15.3
⊕	2.0			14.8 ✓
1/4			0.5	12.3
Cb.			4.5	8.3
E.L.			11.7	1.1
+13			17.7	-4.9
+25			17.7	-4.9
+50			18.2	-5.4

	+	⊗	-	Elev
			0+79	
-50			16.4	-3.6
-40			14.1	-1.9
T.P.	11.16	23.36	0.64	12.20
E.L.			9.0	14.4
Cb			4.8	18.5
1/4			3.5	19.8
⊕			0.5	22.9
1/4	1.6			25.0
Cb.	1.9			25.3
W.L.			0.0	23.4
+30			1.2	22.1
T.P.	9.34	32.44	0.26	23.10
		0+91		
-17	EL. Unmarked	+	4.1	28.3
W.L.			4.2	28.2
Cb			3.9	28.5
1/4			4.1	28.3
⊕			4.0	28.4
1/4			4.1	28.3
Cb.			4.3	28.1
E.L.			8.8	23.6
+25			15.5	16.9
+50			35.5	6.9
+75			35.1	-2.7
+90	51.0		37.3	-4.9

32.44

+ T - Elev
104.26 = P.I. Seaside &
Unnamed St. (12.64 Cbs 2.88 W. on diagonal)

- 20		5.9	26.5
E.L.		4.1	28.3
Cb.		3.5	28.9
1/4		3.6	28.8
♀		3.7	28.7
1/4		3.7	28.7
Cb.		3.6	28.8
W.L.		3.7	28.7
B.M. Check	4.78	32.44	4.78 27.66

P.I. + 9

15' dia eucalyptus Tree 4' E of W.L. Seaside
E. Cb. of unnamed St.

W.L.		3.5	28.9
Cb. (on this Sta. 3.5' dia Eucalyptus Tree)		2.9	29.5
1/4		2.8	29.6
♀		3.2	29.2
1/4		3.2	29.2
Cb.		3.3	29.1
E.L.		3.4	29.0
+ 10		3.4	29.0

W. 1/4 of 7 ST

- 10		2.7	29.7
------	--	-----	------

32.44

68

E.L.		2.4	30.0
Cb.		2.2	30.2
1/4		2.2	30.2
♀		2.6	29.8
1/4		2.7	29.7
Cb.		2.2	29.2
W.L.		3.4	29.0

♀ 7 ST

W.L.		2.8	29.6
Cb.		2.8	29.6
1/4		2.8	29.6
♀		2.4	30.0
1/4		1.8	30.6
Cb.		1.6	30.8
E.L.		2.1	30.3
+ 10		2.5	29.9
T.P.	13.06	43.70	0.80 311.60

W. 1/4 7 ST

- 10		13.0	30.7
E.L.		12.9	30.8
Cb.		12.7	31.0
1/4		13.2	30.5
♀		13.4	30.3
1/4		13.4	30.3
Cb.		13.4	30.3
W.L.		13.5	30.2

+ π - Elev
W. 1/2 ? St + 6 on W. 1/2 of Seaside
= intersection of Cb line

Top Cb.	13.34	3136
Gut.	13.5	304
W. Cb ? St		
W. L.	12.1	316
+ 4 Top Cb as is	13.06	31.64
Gut	13.0	307
Cb line	12.9	308
1/4	12.8	30.9
E	12.2	315
W	12.7	310
Cb	12.1	316
E. L.	12.4	31.3
+ 10	12.3	31.4

W. L. ? St = Pl. of 8' Westerly line of 7 St
of Westerly line of Seaside = 0+00

-10	12.4	313
E. L.	11.4	323
Cb.	11.3	324
1/4	11.8	31.9
2	12.0	317
1/4	11.9	318
Gut.	12.1	316
Top Cb P.C.	11.07	3263

+ π - Elev

+5 = Walk	11.00	32.70
W. L. on Walk	10.90	32.80
+2 on this line = W. Cor ? St	10.78	32.72
0+22 = Southerly Line Alley		
W. L. on walk	8.76	34.94
+55	8.89	34.81
Top Cb	9.01	34.69
Gut	10.1	33.6
1/4	10.3	33.4
2	10.2	33.5
W	10.3	33.5
Cb	10.4	33.3
+1	9.5	34.2
E. L.	10.0	33.7
+10	12.2	31.5

0+47

0.8 drapine 3' W. of W. Cb.

0+50

-10	8.6	35.1
E. L.	7.4	36.3
+8	7.2	36.5
Cb.	8.6	35.1
1/4	7.7	36.0
2	7.5	36.2
1/4	7.7	36.0

4370

	+	π	-	Elev
Gut.			7.3	364
Top Cb			6.42	3728
+4.5 on walk			6.20	3750
W.L.			6.17	3753
0 + 75				
W.L. on walk			4.24	3936
+5.0			4.27	3941
Top Cb			4.47	3923
Gut			5.5	382
1/4			5.7	380
Φ			5.4	383
1/4			5.6	381
+5			6.0	377
Cb.			6.7	368
+1			5.4	383
E.L.			5.2	385
1 + 00				
E.L.			3.1	406
Cb.			4.7	390
1/4			4.2	395
Φ			4.0	397
1/4			4.1	396
Gut			4.0	397
Top Cb (walk gone)			3.09	4061
+4.5			3.2	405
W.L.			3.0	407

4370

70

	+	π	-	Elev
1 + 25				
W.L. on walk			1.77	41.93
+5.5			1.86	41.84
Top Cb			1.97	41.73
Gut			2.9	408
1/4			2.7	41.0
Φ			2.8	40.9
1/4			2.6	41.1
Cb			2.8	40.9
E.L.			1.7	42.0
1 + 50				
E.L.			1.7	42.0
Cb			1.7	42.0
1/4			1.6	42.1
Φ			1.5	42.2
1/4			1.5	42.2
Gut			1.4	42.2
Top Cb (walk gone)			0.83	42.87
+6.5			0.6	43.1
W.L.			0.6	43.1
T.P.				
1 + 75 = End of Prmt = 103.75 N. of				
N.L. of Eastellar St. ^{0.11} + 70' N. of				
S.L. of St. to East				
W.L. on dirt			0.5	43.2
W.L. on walk			0.42	43.28

4370

	+	X	-	Elev
+5 = edge of New walk			0.41	43.29
Cb Top = end of New 8" cb			0.45	42.25
Gut on print			0.94	42.76
1/4 " "			0.81	42.89
1/4 " "			0.89	42.81
1/4 " "			1.11	42.59
Gut " "			1.44	42.26
Top Cb = end of New 8" cb			1.00	42.70
+5 = edge of New Walk			0.94	42.76
E.L. " " " "			0.92	42.78
E.L. dirt			0.9	42.8
1+85 Section on New print.				
Top Cb E			0.83	42.87
Gut			1.34	42.36
1/4			0.98	42.72
1/4			0.85	42.85
1/4			0.79	42.91
Gut			0.91	42.79
Top Cb W.			0.43	43.27
T.R	35.7	35.66	11.61	32.09

Sea Side Place
 Sec Unnamed St from
 Seaside To W.P.T. Loma Blvd
 Sketch PH 50' St 10' Cbs 7 1/2 1/5 71

	+	X	-	Elev
from opp. page			35.66	
0+00 = S.L. W.P.T. Loma Blvd				
W.L. on walk			6.66	29.00
+55 " "			6.90	28.76
Top Cb			7.14	28.52
Gut.			8.2	27.4
1/4			8.3	27.3
1/4			8.3	27.4
1/4			8.5	27.1
Cb.			8.1	27.5
E.L.			8.9	26.7
+6			13.5	22.1
+25			14.5	21.1
0+9				
1' dia eucalyptus			8' W. of E.L.	
0+16				
1' dia "			8' W. of E.L.	
0+23				
1' dia "			8' W. of E.L.	
0+25				
-25			14.3	21.3
-7			13.8	21.6
E.L.			8.0	27.6
Cb			7.8	27.8

Plotted 3-27-30

35.66

	+	-	Elev
1/4		8.2	27.4
1/4		7.8	27.8
1/4		7.8	27.8
+ 6.7 = Gut + Cb as is		7.6	28.0
Top Cb	" "	6.37	29.29
Cb		6.4	29.2
+ 3.7 = walk		6.11	29.55
+ 9.2 "		5.90	29.76
W.L.		6.0	29.6

0+37

1.7 dia eucalyptus 7' W of E.L.

0+45

1.7 " " 7' W. of E.L.

0+50

W.L.		5.0	30.6
+ 1.4 = walk 6' wide		5.08	30.58
+ 7.0 "		5.34	30.32
Cb		5.6	30.0
+ 1.5 = Top Cb as is		5.63	30.03
Gut	" "	6.7	29.0
1/4		7.0	28.7
4		7.1	28.6
1/4		7.4	28.2
Cb		7.3	28.3
E.L.		7.1	28.6

35.66

	+	-	Elev
+ 7		8.0	27.7
+ 20		9.5	26.2

0+52

1.7 dia Eucalyptus 6.5 W of E.L.

0+63.76 = P.L. of E.L. 75th

W.L. Seaside St

- 20		7.4	28.2
E.L.		7.0	28.7
Cb		7.1	28.6
1/4		7.0	28.6
4		6.7	29.0
1/4		6.6	29.0
+ 5.6 = Gut. as is		6.3	29.3
Top Cb	" "	5.20	30.46
Cb		5.1	30.6
+ 2.7 = walk		4.89	30.77
+ 8.2 "		4.62	31.04
W.L.		4.3	31.4

Sec Taken on diagonal from

P.L. Seaside 4 75th to P.L. 75th & Alley

W.L.		2.9	32.7
Cb.		4.0	31.7
+ 1.7 Top Cb as is		4.42	31.24
Gut " "		5.2	30.6
1/4		5.7	30.0

72

3566

	+	π	-	Elev
♀			6.1	29.5
W			6.6	29.0
Cb			6.7	29.0
E.L.			7.0	28.7
Section Taken on diagonal from				
P. 1 N. Seaside ♀ E.L. 75' to P. 1. Mt.				
Seaside ♀ N.L. Alley				
E.L.			7.0	28.7
Cb			6.7	29.0
W			6.6	29.0
♀			6.1	29.5
W			5.7	30.0
+ 6.4604 2515			5.2	30.5
Top Cb	" "		4.30	31.36
Cb.			4.0	31.6
P. 1. walk			3.13	32.53
T. P. 6.25	33.91		3.00	27.66
T. P. 6.32	33.77		6.96	26.95
T. P. 3.49	31.95		4.31	27.46
T. P.			5.38	26.57

Top Standpipe
Sunset CliffsFloor
Pierce
KannerX sec Sunset Cliffs Blvd
From W. Pt. Loma Blvd to Bay
50510 Cb 7 1/2 14's Sketch P. 15

73

	+	π	-	Elev
	0.94		27.51	26.59
0+00 = N.L. W. Pt. Loma Blvd.				
W.L.			3.9	23.6
Cb			3.9	23.6
W			4.0	23.5
♀			3.7	23.8
W			3.6	23.9
Cb			3.9	23.6
E.L.			3.8	23.7
0+17				
-10			5.5	22.0
E.L.			5.4	22.1
Cb			5.5	22.0
W			5.7	21.8
♀			6.2	21.3
W			6.2	21.3
Cb			5.8	21.7
W.L.			6.0	21.5
+10			6.3	21.2
Plotted 3-27-30				
0+19				
♀ 1908 Vintage Ford 8' E. of W.L.				
0+45				
-10			8.0	19.5
W.L.			8.3	19.2

Top Standpipe
Sunset Cliffs
W. Pt. Loma

27.51

	+	π	-	Elev
Cb			7.9	19.6
1/4			8.1	19.4
⊕			7.4	20.1
1/4			7.9	19.6
Cb			7.9	19.6
E.L.			7.9	19.6
+10			7.7	19.8
		0+77		
-10			9.7	17.8
E.L.			10.0	17.5
Cb			9.7	17.8
1/4			9.5	18.0
⊕			9.7	17.8
1/4			9.7	17.8
Cb.			10.9	16.6
W.L.			12.0	15.5
+10			12.5	15.0
T.P.	1.57	16.22	12.86	14.65
		1+00		
-10			3.0	13.2
W.L.			3.3	12.9
Cb			3.2	13.0
1/4			2.4	13.8
⊕			3.6	12.6
1/4			3.3	12.9

16.22

	+	π	-	Elev	74
Cb			1.8	14.4	
E.L.			0.7	15.3	
+10			1.1	15.1	
		1+20			
-10			2.4	9.8	
E.L.			6.4	9.8	
Cb			6.1	10.1	
1/4			6.1	10.1	
⊕			5.9	10.3	
1/4			6.0	10.2	
Cb			6.0	10.2	
W.L.			5.3	10.9	
+10			6.2	10.0	
		1+26			
-10			9.0	7.2	
W.L.			7.2	9.0	
Cb			7.3	8.9	
1/4			7.3	8.9	
⊕			8.8	7.4	
1/4			7.0	8.7	
Cb			8.1	8.1	
E.L.			8.0	8.2	
+15			11.3	14.9	
T.P.	0.73	4.41	12.04	3.68	

4.41

+	π	-	Elev
	1 + 38.42		End of Station E.
-50		8.2	-3.8
-25		7.4	-3.0
E.L.		6.7	-2.3
Cb.		6.5	-2.1
14		6.6	-2.2
4		6.8	-2.4
1/4		6.6	-2.2
Cb.		6.6	-2.2
W.L.		6.7	-2.3
+20		6.9	-2.5

1 + 44.24 = End of Station W.

Diagonal Section

W.L. -20 in channel	9.2	-4.8
W.L.	8.2	-3.8
Cb.	7.2	-3.8
14	7.2	-2.8
4	7.6	-3.2
14	6.8	-2.4
Cb.	6.6	-2.2
E.L.	6.7	-2.3
+50	8.2	-3.8

1 + 50 (Below H Tide Line)

-50	10.2	-5.8
E.L.	9.9	-5.5
Cb.	9.6	-5.2

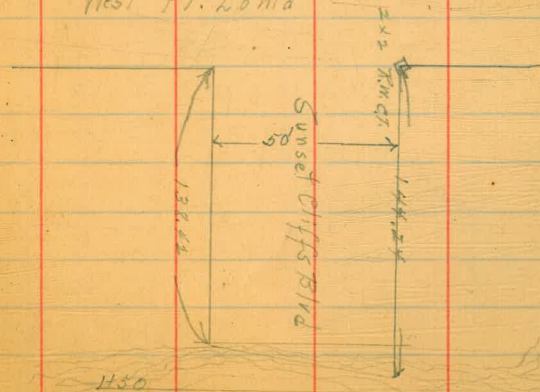
4.41

+	π	-	Elev	75
1/4		7.8	-5.4	
4		7.8	-5.4	
1/4		10.0	-5.6	
Cb.		10.2	-5.8	
W.L.		7.8	-3.4	
+50		10.4	-6.0	
T.P.	12.59	16.76	0.73	3.68
T.P.	12.13	36.80	1.59	14.67
T.P.	4.86	31.43	0.23	26.57
S.H.B.P.			5.80	25.63
				25.62
				10.11

Standpipe
Sunset Cliffs
Vantage of
Sunset Cliffs
Blvd

West Pt. Loma

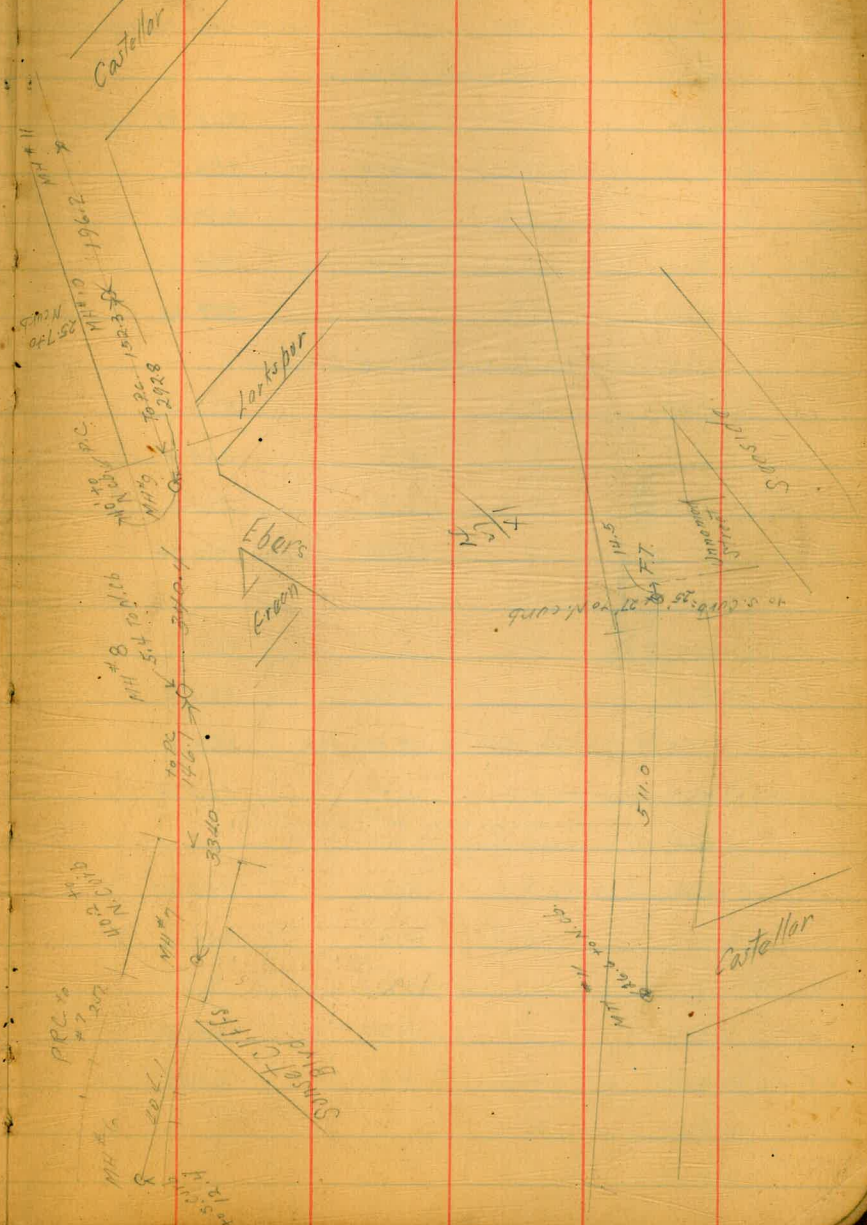
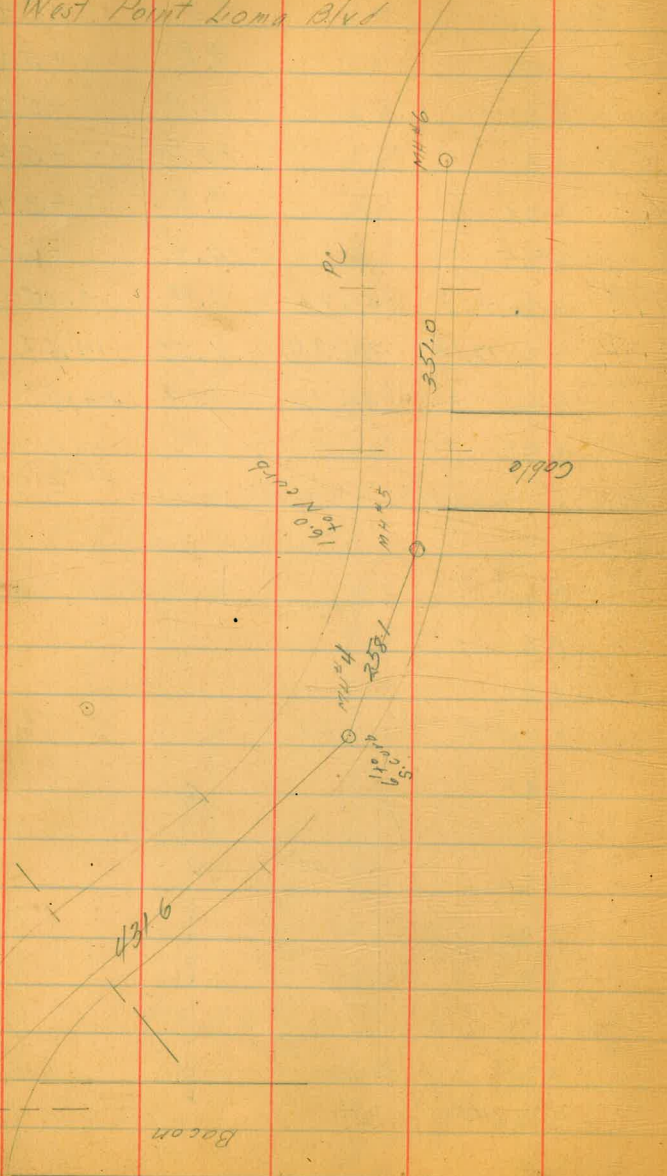
Blvd.



Dearce
Rauwer
4/1/30

Location of Sewer Man Holes on West Point Loma Blvd

E. curb of
Bacon produced
to MH #9 on line of
MH #4, 76
MH #87 to N. curb in Plan. 3114



Parade

X see Alley BIK 14 Tervalta
Orange to Polk bet 40th St + Central

7/19/30

mill
with Hugh
JC BIK
Kangy

B.M.	5.53	369.50	363.97	NW. central + Orange NW. 40 th
B.M.	4.97	369.59	364.62	+ Orange

S. el line Orange

W. on emt. el	5.88	363.71
gutter dirt	6.0	363.6
⊥	5.7	363.9
gutter dirt	5.9	363.6
E. emt. el	5.90	363.69

30 = S. line Orange 14' S. of S. el. line

E. emt. el + dirt	5.64	363.95
⊥	5.6	364.0
W. dirt	5.6	364.0
W. emt. el	5.75	363.84

ck. Garages CBH
7/29/30

10' S

W.	5.3	364.3
⊥	4.9	364.7
E	5.2	364.4
E + 0.5 emt. drive running N + S	5.16	364.43
double garage on W. emt floor 5.6 Back 49' S { End Entrance garage on E. emt. floor 0.5 Back		
E - 0.5 on N + S emt drive	4.82	364.77
E	5.0	364.6
⊥	4.9	364.7
W	5.0	364.6
W + 5.6 floor	5.1	364.5

369.59

91' S double garage on W. emt. floor 5.0 Back

W-5	5.2	364.4
W	5.2	364.4
⊥	5.2	364.4
E	5.4	364.2

94.5' garage on E. dirt floor 5' Back

E-5.0 floor	5.6	364.0
-------------	-----	-------

106.5' garage on E. dirt floor 5' Back

E-5.1 floor	5.7	363.9
-------------	-----	-------

125' S

E	5.9	363.7
⊥	5.3	364.3
W	5.4	364.2

150' S

W	5.7	363.9
⊥	5.6	364.0
E	6.2	363.4

182' S garage on W. emt floor 7' Back

E	6.1	363.5
⊥	5.7	363.9
W	5.5	364.1

W + 7 floor	5.8	363.8
-------------	-----	-------

217' S. garage on W emt floor 7' Back ✓

N-7 floor	6.1	363.5
W	6.0	363.6
⊥	6.2	363.4
E	6.6	363.0

369.59
250.5.

E	6.6	363.0
±	6.4	363.2
+8	6.2	363.4
W	6.8	362.8

From { 224.5 Board Fence on W. 1.8 in Hllay
To, { 275.5 " " " 2.2 " "

280.5 garage on W. ent. floor 6.5 Back ✓

W-6.5 floor	6.5	363.1
W-3.5 ent. apron	6.6	363.0
W	6.7	362.9
±	6.8	362.8
E	6.7	362.9

304.5 N. End double garage on E. ent. floor + Apron 3.1 Back

E-3.1 floor	7.10	362.49
E. on ent. apron	7.17	362.42
E+0.3 W. edge ent. apron	7.17	362.42
±	7.0	362.6
W.	7.1	362.5

322.5 S. End above garage

W	7.6	362.0
±	7.7	361.9
+9.7 W. edge ent. apron	7.25	362.34
E on " "	7.25	362.34
+3 floor	7.17	362.42

T.P 2.51 364.23 7.87 361.72

364.23

Alley BIK 14 Taratta

326.5 N. End double garage on W. dirt floor on W. line 8
W. floor 2.1 362.1

345.5 S. end above garage on W.

E	2.9	361.3
±	2.8	361.4
W dirt	2.4	361.8
W floor	2.07	362.16

368.5 garage on W. ent. floor 0.7 Back

W-0.7	2.65	361.58
W.	2.9	361.3
±	3.3	360.9
E.	3.1	361.1

400.5

E	3.7	360.5
±	3.7	360.5
W	3.7	360.5

418.5 garage on E. ent. floor 1.2 Back

W	3.8	360.4
±	4.0	360.2
+9.4 W. edge ent. apron	3.78	360.45

E	3.76	360.47
E+1.2 floor	3.70	360.53

from 374.5 to 404.5 Board Fence on E. 0.4 in Hllay

from 422.5 to 436.5 chicken House on E. 0.4 in Hllay

452.5 garage on E. ent. floor 1.0 Back

E. floor	4.7	359.5
±	4.8	359.4
W.	4.6	359.6

364.23

465' s. garage on E. end. floor 1.0 Back
 E-1 4.60 359.63
 482' s. garage on E. dirt floor 1.8 Back
 W 5.2 359.0
 E 4.9 359.3
 E floor 5.2 359.0

516' s. garage on E. end. floor 2.0 Back

E-2.0 floor 5.38 358.85
 E 5.4 358.8
 E 5.3 358.9
 W 5.2 359.0

From 489' s. to 513' s. Board Fence on W. 0.6 in Alley

528' s. N. End. double garage on E. end. floor 2.2 Back

W 5.4 358.8
 E 5.5 358.7
 E. on end. apron 5.66 358.57
 E 2.2 floor 5.60 358.63

546' s. S. End above garage

E-2.2 floor 5.50 358.73
 E. on end. apron 5.67 358.56
 E 5.7 358.5
 W. 6.0 358.2

570' s.

W. 6.3 357.9
 E 6.3 358.0
 E 6.2 358.0

364.23

Alley BIK 14 Teralla

574' s. - N. line Polk Av

E. on N. end. end. db 6.29 357.94
 E " " " Pavmt. 6.44 357.79
 E " " " " 6.64 357.59
 W " " " " 6.45 357.78
 W " " " " end. db 6.26 357.91

581' s. - N. db line Polk

N. end. db 6.42 357.81
 W gutter Pavmt 6.85 357.38
 E " " " 6.89 357.34
 E " " " 6.92 357.31
 E end. db. 6.38 357.85

T.P. 6.53 369.67 1.09 363.14

chk original BM. 5.04 364.63 = 864.62

Additional Levels Hilley 8/14 Teratto July 19 45

80

Same Stationing as Original P 77

BM	A1.55	869.17	364.62	
		0+11 = N/4 0.4 Conc Curb on East		
E - 0.1		Top Curb on Wall 4.17	365.00	
		0+49 = S/4 0.4 Conc Curb on East		
E - 0.1		Top Curb on Wall 2.80	365.37	
TP	4.25	268.20	5.22	363.95
		2+15 = 1/2 Do Garage on W		
W - 1.3		1/2 Do Garage Conc Floor 4.40	363.80	
		3+75 = 1/4 Fly Conc Apron For 1/4 Car Garage on W		
W - 0.8		N/4 Fly Conc Apron 6.68	361.52	
		4+10		
W - 0.8		E/4 Fly Conc Apron 6.90	361.30	
W - 5.8		E/4 Garage on Conc 6.52	361.68	
		4+22 = S/4 Fly Conc Apron on W		
W - 0.8		S Fly Conc Apron 6.99	361.21	
TP	3.64	363.82	8.02	360.18
		4+85 = 1/2 Do Garage on E		
E - 1.2		1/2 Do Garage Conc Floor 4.24	359.58	
		5+16 = 1/2 Garage on W		
W - 1.5		1/2 Garage Dirt Floor 4.2	359.60	
		5+74 = N/4 Polk Flc		
W	Top Conc. Cb.	5.84	357.98	For Check

3240
321
34.51
5.96
21.97

75
19

80

DIRECTIONS FOR USE OF TABLES

TABLE No. 1
146
78

Distance of slope stake from side of shoulder
stake for any width roadway. Slope 1% to 1.
If ground is nearly level, the cut or fill at side
stake is located by the double entry method in
left column and top row. The number in body

IMPROVED TABLES
AND
INFORMATION

To find tangent and External for curve of
any other degree, divide by degree of curve and
add correction found in column of corrections.
Degree of curve with a given L may be found
by dividing tangent (or external) opposite L by
given tangent (or external).
The distance from a point on the tangent to
the curve is very nearly the square of the tangent
length divided by twice the radius.

SW. B. P. Wilcox & Ebers 30.06
 107 2nd St. C6 - Tel. Bldg. N.W. Cor. W. P. L. Bldg. & Seaside 27.62

ENGINEERING DEPARTMENT,
 CITY OF SAN DIEGO,
 CALIFORNIA.

3867	4/3837	80.67
52	9.67	10.08
43.87	5.19	
	14.86	
	9.67	
	24.53	
	9.67	5.56
	34.20	2.88
	9.67	
	43.97	2.67

15.38	5.55
12.31	2.03
2.7	
	2.52
	2.58
	7.04
	5.37
	1.67

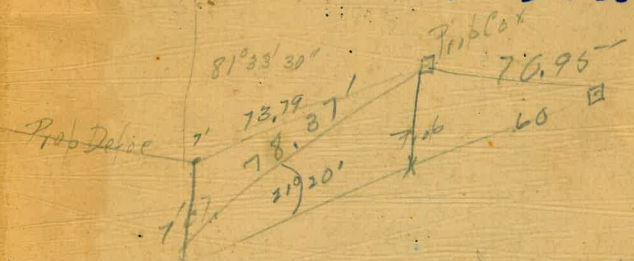
6.8 43
 22 1 3 5
 361

2.67
 2.67
 5.34

107

TANK 18436 - #
 F 7846

H 2-2284



120	71.80
800	325.04
79200	296.34
10560	693.22
1144200.00	
87.120	
260000	
261860	
264000	

135117
 85
 70117