

1377

PASTS

LEVEL BOOK

1908

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CITY OF SAN DIEGO,
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This notebook is pp 8 - 6/24/20 1044

Beardsley St. Sullivan to 22nd 1 to
 22nd Beardsley to Crosby 24
 Alley Bk 227 Manassett Schiller's 5-8
 BOWLING GREEN BRANBOR PARK 32-34
 X Sec. Dickens Reservoir to Evergreen 35
 " " Locust Emerson to Charleton 31
 " " Keeler St Highland west 39
 " " 45th St. Market to Hilltop 47
 " " Hilltop 44 to 46 58
 " " "F" (Pearl) 44 to 45 67
 " " "G" (Alma) 44 to 45 71

Walker
Lorkey
McLennan
Kinnery
12-18-29

CROSS SECTION

BEARDSLEY ST. 60' wide 10' cbs
From N.L. Julian^{10' 75'} North to Intersection 22nd St.
Had 22nd St. from above Intersection to Irving Ave.
See Sketch Page 2

NEBR
Julian +
Beardsley

5.53 50.83 44.50

E	5.8	45.0
+2.5 on top Walk	5.88	44.95
+10' = top cb.	6.13	44.70
Gut. on Pav.	6.56	44.27
1/4 " "	6.47	44.36
1/2 " "	6.55	44.28
1/4 " "	6.73	44.10
Gut " "	6.98	43.85
W top cb.	6.48	44.95
+7.5 = top Walk	6.22	44.61
W	6.2	44.6

0+43 = 8" Gauge on W. Brick Floor. 1' in st.

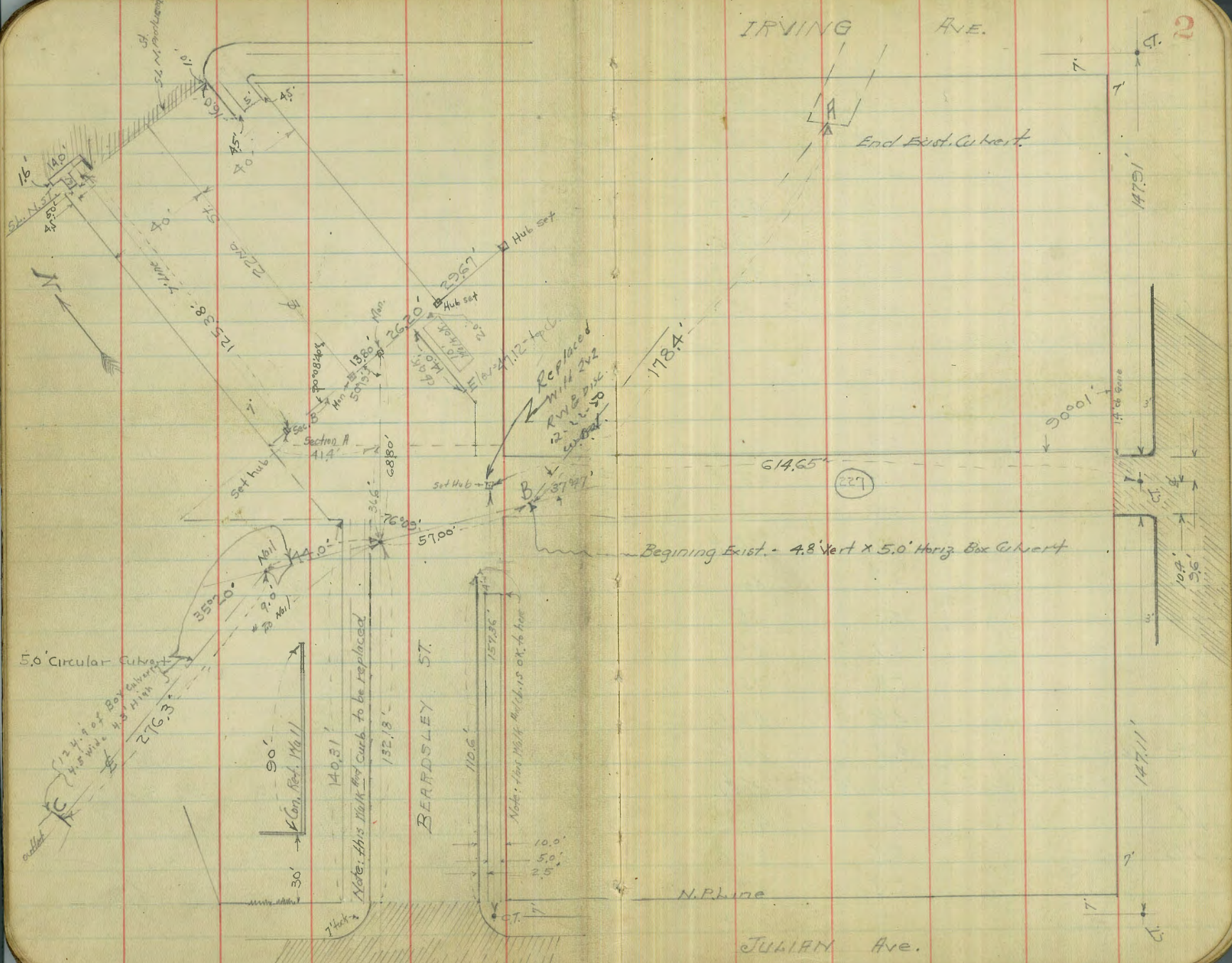
0+50

-20	15.5	35.3
-7 = toe Ret. Wall	15.5	35.3
-7' on top " "	7.8	43.0
W	6.0	44.8
" cb.	6.3	44.5
" Gut.	6.7	44.1
1/4	6.2	44.6
1/2	6.0	44.8
1/4	6.1	44.7
E Gut.	6.4	44.4

Plotted 12/20/29

50.83

E. top cb.	5.55	45.28
+7.5 = top Walk	5.23	45.60
E	5.4	45.4
	1+00	
E	4.8	46.0
+2.5 = top Walk	4.69	46.14
cb.	5.03	45.80
Gut.	5.9	44.9
1/4	5.7	45.1
1/2	5.7	45.1
1/4	6.1	44.7
Gut.	6.6	44.2
cb.	5.5	45.3
+7	5.3	45.5
W	6.5	44.3
+7 = top Ret. Wall	10.0	40.8
+7 = toe " "	16.0	34.8
+20	13.6	36.2
	+9.6	45.87
1+10.6 = End of Exst. Good cb. on E	4.62	46.21
1+06.6 = " " " " Walk " E		cb+7.5
1+20 = End Ret. Wall on W	10.06	40.77 7' Back
1+20 = " " " " toe	12.0	38.8 7' "
	1+40.31 = sb. All of	
-10	9.8	41.0
-2.31 = Projection N.L. 22nd	6.5	44.3
W	5.6	45.2



5.0' Circular Curb

1/2 in. of Box Culvert 4.8' x 5.0' high
Mail
30' x 90'' Con. Box 1411

30'

Note: this 110.6' curb to be replaced

BERDLEY ST.

Beginning Exst. - 4.8' Vert x 5.0' Horiz. Box Culvert

N. Plane

JULIAN AVE.

227

W cb.	5.6	45.2
" Gut.	6.4	44.4
W $\frac{1}{4}$	5.9	44.9
$\frac{1}{2}$	5.4	45.4
E $\frac{1}{4}$	5.6	45.2
Gut.	5.8	45.0
cb.	5.5	45.3
E.	5.0	45.8

Section A

-10'	3.3	41.5
E	5.5	45.3
cb.	5.4	45.4
+10 = Gut.	5.8	45.0
+10 = $\frac{1}{4}$	5.0	45.8
+10 = $\frac{1}{2}$	4.6	46.2
+10 = $\frac{3}{4}$	4.7	46.1
+10 = cb.	5.3	45.5
+10 = W	5.7	45.1
+7	5.8	45.0
+8	4.8	46.0
+244 = W line 3220'	4.7	46.1

Section B = 0+00
= 22nd St. Cross Section 14' cbs 13' fs.

W	4.7	46.1
+13	4.6	46.2
cb.	5.5	45.3
$\frac{1}{2}$	5.0	45.8

Plotted
12/20/29

$\frac{1}{2}$	4.3	46.5
$\frac{1}{4}$	4.1	46.7
Gut	4.2	46.6
cb	3.44	47.39
+9.5' = top Walk	3.22	47.61
E	3.2	47.6
+29.67' = E.L. Beardsley	2.4	48.8
0+50		

E	2.8	48.0
cb.	3.4	47.4
+3	4.2	46.6
$\frac{1}{4}$	4.0	46.8
$\frac{1}{2}$	3.8	47.0
$\frac{3}{4}$	4.3	46.5
cb.	4.7	46.1
+1	4.2	46.6
+12 = top Con. Apron	4.10	46.73
+14 = Garage Floor	3.77	47.06
1+25.38 = Sh. N. St. on West		

W	3.7	47.1
+45 = top Walk	3.69	47.14
cb.	3.84	46.99
Gut. on Pav.	4.33	46.50
$\frac{1}{4}$ " "	3.72	47.11
$\frac{1}{2}$ " "	3.34	47.49
$\frac{3}{4}$ " "	3.35	47.48

cb. on Box.	364	47.19
" + 25 on Box	364	47.19
" + 25" top cb. Return.	287	47.96
1 + 0.8 ⁴ = find exist cb and walk on E 288	47.95	top cb.
1 + 0.84 - " " " " " " " 2.67	48.16	top walk = 47.95

Box Culvert Elevations.

Floer line of A sketch Page 1	16.86	33.97
" " " B " " "	20.29	30.54
" " " C " " "	25.03	25.80
T.P.	4.40	46.43

Not in file
Wed. June
May 227

Walker
Larkin
McHoon
12-19-29

CROSS SECTION 20' Alley Bk. 227
MANASSE and SCHILLER Add.
Bet. Julian Ave. and Irving Ave.
From E.L. Beardsley to Wm. Douglas St.
N.E. B.P. Julian
Beardsley

5.35 50.25 44.90

E.L. BEARDSLEY = 0+00

-10'	4.6	45.6
N	4.7	45.5
6	5.0	45.2
S	5.4	44.8
+5	5.0	45.2

0+12.3

-5 on Rubbish Pile	6.2	44.0
S " " "	6.2	44.0
+1 " Nat. Ground	11.8	38.4
+3 " top culvert Hd Wall	11.8	38.4
6 " " " "	11.9	38.3
N	12.0	38.2
+10	11.3	38.9

0+13

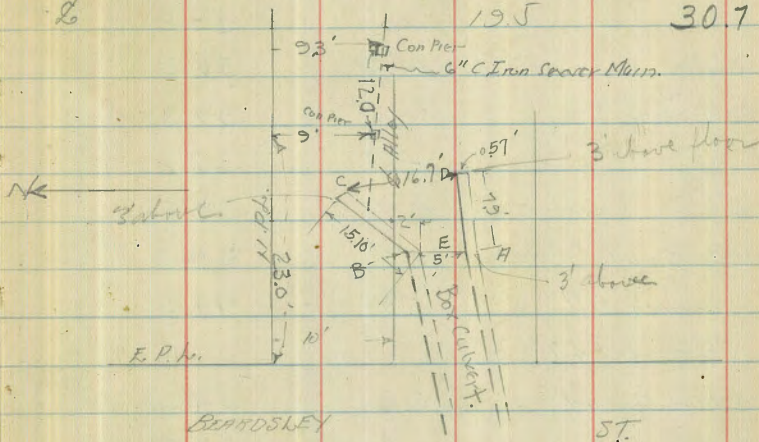
-10	12.0	38.2
N	12.7	37.5
+9 on Hd Wall	12.79	37.46
+9 " top 6" Cast Iron Sewer pipe	13.21	37.04
6 Floor base	19.58	30.67
S on Nat. Ground	11.8	38.4
+1 " Rubbish Pile	6.2	44.0
+10 " " "	6.2	44.0

0+21 = End Wing Walls to Exist. Box Culvert

Plotted 12-20-29-

5025

-5 on Rubbish	6.3	43.9 ⁵
5 " "	6.3	43.9
+2	14.0	36.2
6	19.5	30.7



N	18.3	31.9
+10	15.4	34.8
+20	15.4	34.8

H on top culvert	11.83	38.42
E " " "	11.81	38.44
E " Floor base	19.74	30.51
B " top culvert	11.78	38.47
C " " Hd Wall	17.24	33.01
D " " " "	16.83	33.42

50.25

0+35

-20'	17.1	33.1
-10'	18.2	32.0
-5' - Bottom Ditch But cutverts A and B on Page 2	19.7	30.5
N	17.0	33.2
+9	14.0	36.2
+9.3 on top Pipe ^{2" Sewer}	12.88	37.37
±	14.0	36.2
+6	11.1	39.1
S on Nat. Ground	9.7	40.5
+5" Rubbish Fill	5.9	44.3
0+42		
-5 on Nat. Ground	6.2	44.0
S	6.4	43.8
±	10.3	39.9
N	15.5	34.7
+10	16.6	33.6
+15	17.2	33.0
+18' = Bottom Ditch ^{cutverts} A+B	19.4	30.8
+23	16.4	33.8
0+62		
-25	15.7	34.5
-20	15.7	34.5
N	12.4	37.8
±	6.9	43.3
+24 = Board Fence	6.8	43.4
S+5	6.4	43.8

50.25

0+74

-5	6.9	43.3
S	6.3	43.9
±	5.8	44.4
N	5.8	44.4
+10	6.8	43.4
0+98 = West edge Dble. Garage on South Dirt Floor 0.3' in Alley		
-5	4.6	45.6
N	4.3	45.9
±	3.3	46.9
+97 at Garage	4.1	46.1
1+24 = East edge Above Garage 0.3' in Alley		
S+03	3.6	46.6
±	3.8	46.4
N	3.8	46.4
+5	3.8	46.4
1+47 = ± Garage on South 0.3' in Alley Dirt Floor		
-5'	2.9	47.3
N	3.1	47.1
±	2.8	47.4
+97 = Garage	2.1	48.1
1+52 = West end Garage and shed on S	1.9	48.3
1+72 = ± Garage Comp.	1.4	48.8
1+76 = East end Above Garage	1.4	48.8 0.3' in Alley
T.P.	3.75	52.01
1.99		48.26
2+02 = ± Garage on South Con. Floor. With Con. Apron Approach.		

6

52.01

-0.7 on Garage Floor	3.13	48.88
S Apron	3.13	48.88
+25' = toe (on Apron)	3.32	48.69
ℓ	3.7	48.3
N	4.1	47.9
+5	4.3	47.7
2+50		
-5	5.3	46.7
N	5.6	46.4
ℓ	5.2	46.8
+9 of Fence	5.1	46.9
2+36 = ℓ Board Fence on South 25' wide 5' High 1' in Alley	5.5	46.5
2+68 = ℓ Garage on South 25' Back dirt Floor	5.1	46.9
2+80 = 1/2 end Dble. Garage on N 3' Back dirt Floor	4.7	47.3
2+94 = ℓ Garage on South 26' Back dirt Floor	5.3	46.7
2+98 = 1/2 end Above Dble. Garage on N		
3+00		
S	5.1	46.9
ℓ	4.9	47.1
N	5.0	47.0
3+11 = 1/2 end Dble. Garage on South dirt Floor 4.9' Back	4.5	47.5
3+12 = ℓ Cor. Walk on N of Back 4' wide	4.43	47.58
3+30 = ℓ Garage on N on base Wood Floor	3.0	49.0
3+33 = 1/2 end Above Dble. Garage on South		
T.P. 7.01	55.51	3.51
N	7.3	48.2

55.51

ℓ	8.0	47.5
S	7.9	47.6
+4.3' of Garage	7.9	47.6
3+46 = ℓ Shed on South 18' wide 0.5' in Alley		
3+50		
S+65	6.9	48.6
ℓ	7.2	48.3
N	6.7	48.8
3+75 = ℓ Garage on North dirt Floor on base		
N	6.2	49.3
ℓ	6.6	48.9
S	6.5	49.0
4+00		
S	5.6	49.9
ℓ	6.0	49.5
N	6.1	49.4
4+23 = ℓ Shed on South 26' in Alley 18' wide	5.3	50.2
4+41 = ℓ Dble. Garage on South 0.5' in Alley dirt Floor	5.3	50.2
4+44 = ℓ Garage on N 25' in Alley 12' wide		
4+50		
N	5.3	50.2
ℓ	5.1	50.4
S	5.2	50.3
4+61 = ℓ Dble. Garage on South 0.5' Back dirt Floor	4.9	50.6
4+61 = ℓ Dble. Garage on North dirt Floor	4.7	50.8
4+87 = ℓ Garage on N 0.4' Back dirt Floor		

S+0.6 at Fence	4.6	50.9
L	4.2	51.3
N	4.3	51.2

4+91 = Board Fence on South 0.5' in Alley. 16' wide

5+08 = Shed on South 0.3' in Alley dirt floor

5+25 = Garage on N 13' Back North Entrance dirt floor

5+33 = Board Fence on South 0.1' in Alley.

5+50

N	3.4	52.1
---	-----	------

L	3.1	52.4
---	-----	------

S	3.6	51.9
---	-----	------

5+55 = Garage on N dirt floor 0.4' in Alley

5+55 = " " S 3.3 dirt floor 0.7 Back

5+73 = West End House on North 0.5' in Alley on low Bluffs.

6+00 = W. Gosby St. = East end House on N 0.6' in Alley.

S-0.4' top ch.	2.47	53.04
----------------	------	-------

S-0.4 on Porch	2.52	52.99
----------------	------	-------

L on Rim Sewer MH.	2.66	52.85
--------------------	------	-------

+9.6 = Gut on Pav.	2.44	52.07 53.07
--------------------	------	-------------

T.P. 558	58.44	2.65	52.86
----------	-------	------	-------

Chk. on BM SE. BP. Irving & Gosby St.	3.26	54.48
---------------------------------------	------	-------

5452-BM

0.04 = Error

Cross Section Alley Block 225 S.D. Land + town
 From Jersey to Evans
 Between Irving + Julian

20 ft wide

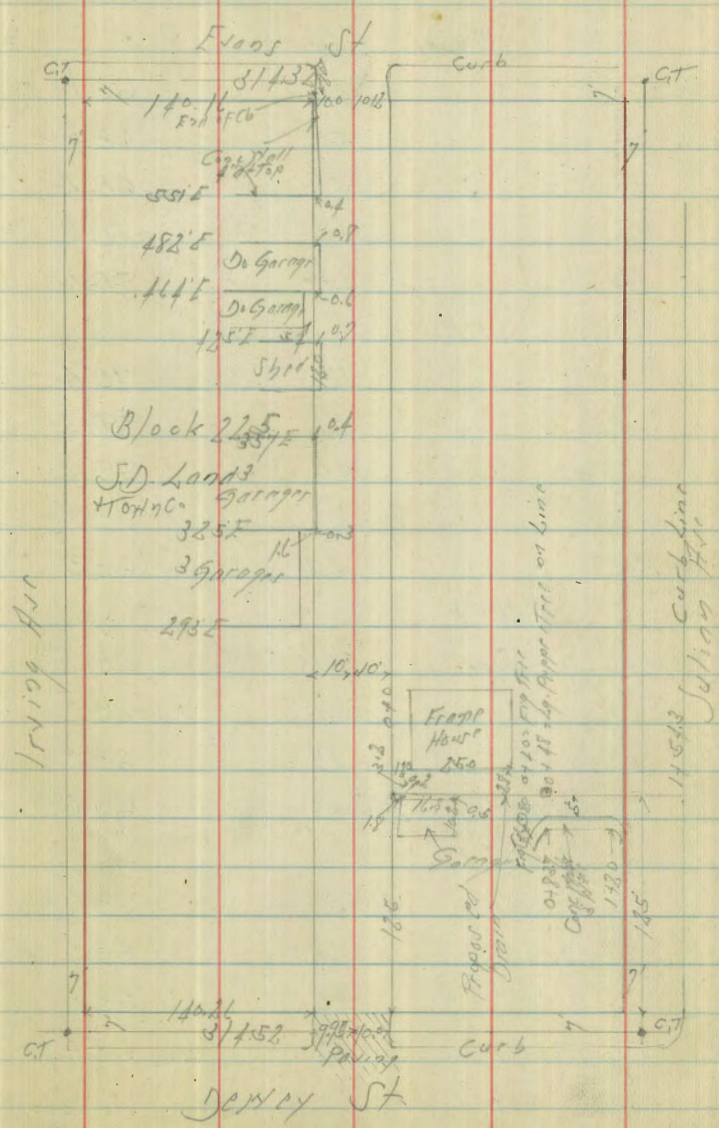
H.W. BP.

Julian + Jersey

BM	11.72	73.66	61.94	
	E. C. of Jersey			
S	on Paving	8.05	65.61	
L	"	7.87	65.79	
H	"	7.66	66.00	
	E. L. of Jersey			
H	on top Cb	6.65	66.01	-
H	" Paving	6.83	66.84	-
L	"	7.32	66.34	-
S	"	7.24	66.42	-
S	" Top Cb	7.15	66.51	-
	S.E. of E.L. Jersey			
S		4.6	69.0	
+2		1.7	68.9	
+6		6.6	67.0	
L		7.0	66.6	
+6		1.2	67.4	
+8		3.7	69.9	
H		2.9	70.7	
	S.E. of E.L. Jersey			
H		2.9	70.7	
+3		3.3	70.3	
+5		5.1	68.5	
L		5.8	67.9	
+6		5.5	67.1	

Plotted 7-26-30 C.B.H.

7-23-30
 S. 11.72
 North 51.9
 Kang 9



7366

+7	44	69.2
5	45	69.1
	15 E of E.L. Driv. Cr.	
5	45	69.1
+4	50	68.6
8	52	68.4
+7	33	70.3
H	32	70.4
	50 F	
H	32	70.4
+3	34	70.2
+5	44	69.2
8	47	68.9
5	43	69.3
	50 F	
-0.7 = H.L. of Do Garage	510	68.56 ✓
Conc Floor		
5	51	68.5
8	48	68.8
H	40	69.6
	68 F	
H	50	68.6
8	55	68.1
5	56	68.0
+0.4 = E.L. of Do Garage	500	68.66 ✓
Conc Floor		
	85 F	
-2.5 = E.L. of Do Garage	18	66.8 ✓
Dir Floor		

7366

10

5	67	67.0
8	69	66.7
H	65	67.1
+2.4 = E.L. of Do Garage	64	66.2 ✓
Dir Floor		
	120 F	
H	81	65.5
8	83	65.3
5	87	65.0
+1.8 = E.L. of Garage Dir Floor	87	65.0 ✓
	133 F	
5	82	65.4
8	82	65.4
H	84	65.2
+2.8 = E.L. of Garage Dir Floor	84	65.2 ✓
TP	368	69.19
	8.15	65.51
	Proposed Drain	See Sketch Page 9
0+0 = S.E. of Alley	41	65.1
+12	48	64.4
+25	50	64.2
+50	50	64.2
{ +83.7	51	64.1
{ 5' W of E.L. of Top Conc Wall	467	64.52
3' Wide		
+10	52	64.0
{ +20	55	63.7
{ 5' W of E.L. of Top Conc Wall	529	63.90
3' Wide		

6919

1440	56	63.6	
+445 = H Edge Walk	680	62.39	
+198 = S Edge Walk	192	62.27	
+543 = Top Ch. N. Ch. of	192	62.27	
Gutter on Top Pav. 179	7.66	61.53	
TP 5547 71.08	3.68	(5.51)	
	170 F of E.L. of Garage	154 F - Conc	
		Walk to House	
-1.0 = 1/2 Garage Dirt Floor	58	65.3	155 F of 1/2 ✓
J	56	65.5	157 = 64.55
1/2	56	65.5	
H	56	65.5	181 F = 2 Do
	200 F		Garage 200 F
			125 F of 1/2 ✓
H	53	65.8	57 = 65.4
1/2	56	65.5	
J	54	65.7	
	235 F		221 F - Conc Walk
J	56	65.5	235 F of 1/2 ✓
1/2	50	66.1	53 F = 65.74
H	48	66.3	
+3 = H.L. of Dr Garage ✓	47	66.4	245 F = 2
	255 F		Dr Garage
			Dirt Floor
			200 F of 1/2 ✓
-3 = E.L. of Dr Garage ✓	45	66.6	61 = 65.0
H	48	66.3	
1/2	50	66.1	
J	45	66.6	
	279 F		

71.08

11

J = 1/2 Dr Garage	49	66.2	
Dirt Floor	47	66.4	
H	47	66.4	
	293 F		
-1.7 = H.L. of 3 Garage	42	66.9	✓
Dirt Floor	42	66.9	
1/2	45	66.6	
J	42	66.9	321 F = 2
			Garage Dirt
			353 F of 1/2 ✓
	325 F		1.0 = 67.1
J	35	67.6	
1/2	34	67.7	
H	34	67.7	
H	34	67.7	
1/2	34	67.7	✓
	257 F		
J = E.L. of 3 Garage	18	69.3	345 F = 2
Dirt Floor	16	69.5	Garage Dirt
			161 F ✓
			on 5.2 ✓
			2.2 = 68.8
TP 1203 8275	0.36	70.72	
	381 F		
-25 = Garage dirt Floor	11.1	71.6	364 F = 2
J	11.1	71.6	Garage Dirt
1/2	11.1	71.6	on 5.2 ✓
H	11.0	71.7	122 70.5
1/2	11.0	71.7	
J	11.0	71.7	✓
	408 F		
-7.7 = E.L. of Dr Garage	10.8	71.9	✓

8375

H		10.0	72.7
S		9.5	73.2
S		8.7	74.0
	435 F		
S		7.3	75.4
S		7.9	74.8
H		7.3	75.4
	437 F		
-5.6 = H/L of De Garage		5.6	77.1 ✓
H		5.8	77.0
S		6.6	76.1 ^{H/L = Garage}
S		6.5	76.2 ^{Dir Floor}
	441 F		6.0 = 76.7 ^{1st Depth}
S		4.5	78.2
S		4.5	78.2
H		4.2	78.5
+5.4 = F.L. of De Garage		1.0	78.7 ✓
	482 F		
H		3.5	79.2
S		3.3	79.4
S		3.2	79.5
	511 F		
S		1.5	81.2
S		1.7	81.0
+9.2 = Garage Dir Floor		1.5	81.2 ✓
TP	666 8803	138	8127

88.03

12

	530 F		
H		5.1	82.9
S		5.7	82.3
S		5.7	82.3
	558 F		
-1.2 = Garage Dir Floor		3.7	84.3 ✓ ^{561 F = 2' of}
S		3.7	84.3 ^{M.H. & 11.1}
S		4.0	84.0 ^{12' Floor}
			3.59 = 84.44
+9.6 = Conc Wall		3.75	84.28 ✓
H		4.2	83.8
	575 F		
H = Top Conc Wall		3.99	84.54 ✓
S		3.4	84.6
S		3.6	85.4
	590 F		
-0.5 = Conc Parch		1.90	86.13 ✓
S		2.2	85.8
S		3.3	84.7
H on Conc Wall		3.25	84.68 ✓
	598 F		
H on Conc Wall		3.30	84.73 ✓
Ground		3.6	84.4
S		4.5	83.5
S		3.9	84.1
S		2.7	85.3
	601.09 = H.L.		

S on Top Cb	536	82.77	
Ground	48	83.2	
S	5.0	83.0	
H Ground	46	83.4	
H - Top Cb	531	82.72	
	W Cb of		
H Top Cb	549	82.54	
S " "	558	82.45	
BIV	599	82.04	W W 8 P Subs. of Fm. 82.01

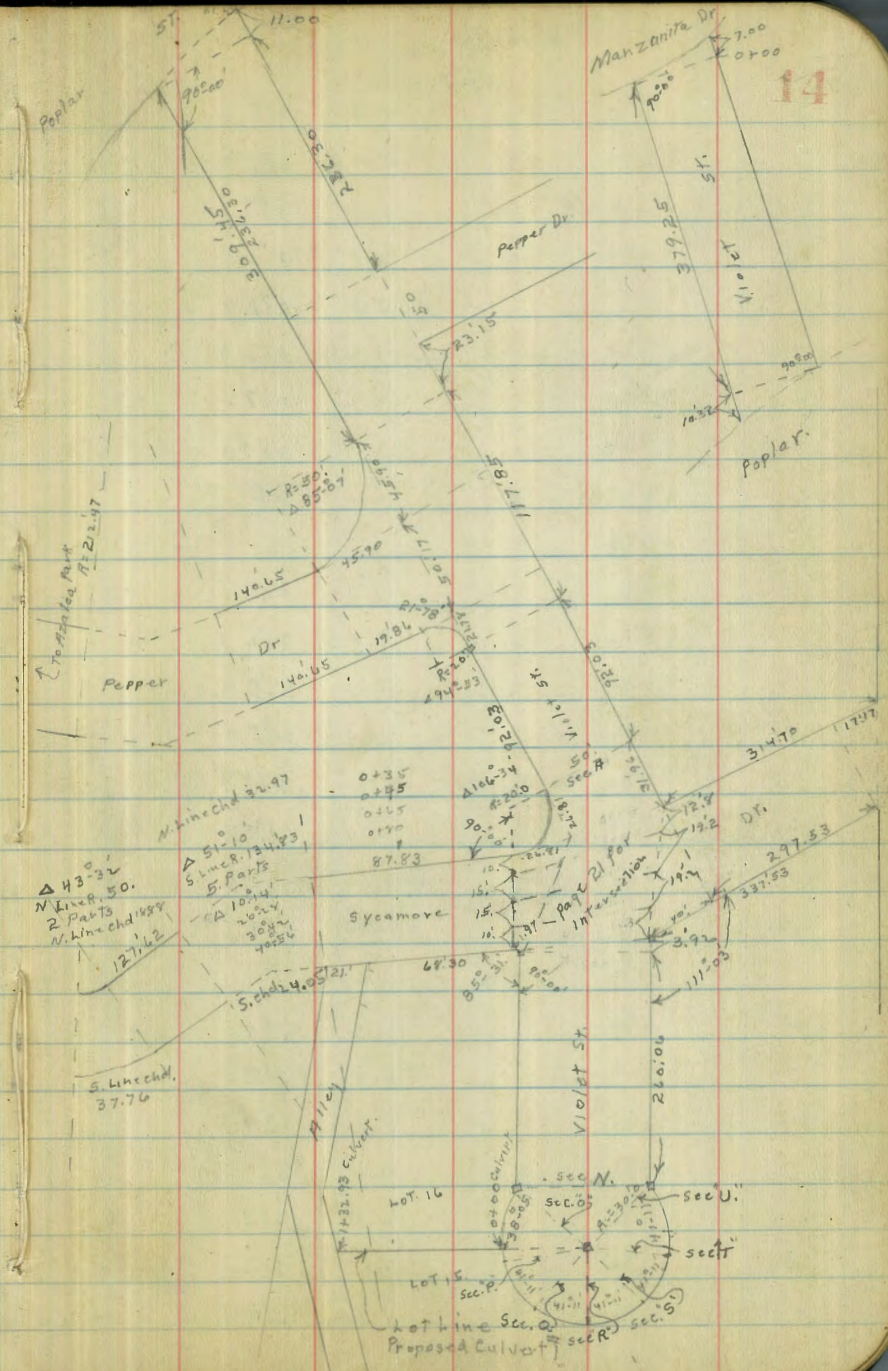
50 wide
10' elev
75' 45"

X sec Violet St - Manzanita to Sand.

Mulla
Samarangaya
Samarangaya
Kahapi

BM. I Pipe	5.72	289.80	284.08
S. Line Manzanita on Curve			
E	1.5	288.3	
cb	1.8	288.0	
1/4	2.3	287.5	
1/2	2.1	287.7	
3/4	2.6	287.2	
+5	3.0	286.8	
cb	3.0	286.8	
W	3.4	286.4	
00 = 90° from SW. Cor.			
W	3.4	286.4	
cb	3.0	286.8	
+3	3.0	286.8	
1/4	2.6	287.2	
1/2	2.1	287.7	
3/4	2.5	287.3	
cb	1.6	288.2	
E	1.4	288.4	
0+50 S			
E	1.9	287.9	
cb	2.3	287.5	
1/4	3.0	286.8	
1/2	2.6	287.2	
3/4	3.1	286.7	
cb	3.0	286.8	
W	3.2	286.6	

Plotted Nov-1-1930



289.80

1+00

w	4.2	285.6
cb	3.9	285.9
"4	3.5	286.3
♀	3.1	286.7
"4	3.8	286.0
+3	3.8	286.0
+5	2.6	287.2
cb	2.4	287.4
E	2.1	287.7
1+50		
E	3.0	286.8
cb	3.5	286.3
"4	4.5	285.3
♀	3.9	285.9
+5	3.9	285.9
"4	4.4	285.4
cb	4.6	285.2
w	4.9	284.9
2+00		
w	5.3	284.5
cb	4.8	285.0
+5	5.1	284.7
"4	4.8	285.0
+3	4.5	285.3
♀	4.5	285.3
"4	4.9	284.9

289.80

Violet st

15

+3	4.7	285.1
+5	3.9	285.9
cb	3.9	285.9
E	3.7	286.1
2+50		
E	4.3	285.5
cb	4.5	285.3
+2	4.5	285.3
+4	5.6	284.2
"4	5.6	284.2
♀	5.0	284.8
+4	5.1	284.7
"4	5.4	284.4
+2	5.6	284.2
+4	5.0	284.8
cb	4.8	285.0
w.	5.0	284.8
3+00		
w	6.1	283.7
cb	6.1	283.7
+5	6.5	283.3
"4	6.4	283.4
♀	5.8	284.0
"4	6.1	283.7
+3	6.2	283.6
+5	5.6	284.2

289.80
3+00 (con)

cl	5.6	284.2
E	5.7	284.1
	3+40	
E	5.7	284.1
cl	6.2	283.6
+1	6.6	283.2
"4	6.6	283.2
♀	6.4	283.4
"4	6.9	282.9
cl	7.2	282.6
W.	7.7	282.1
	3+79 ²⁵	90°00' from N.E. Cor Violet + Poplar
W	8.2	281.6
cl	7.7	282.1
"4	7.3	282.5
♀	6.7	283.1
"4	6.7	283.1
cl	6.5	283.3
E = N. E. Cor. Violet + Poplar	5.7	284.1
	N. Line Poplar on Curve	
E	5.7	284.1
cl	6.4	283.4
"4	6.7	283.1
♀	6.4	283.0
"4	7.2	282.6
cl	7.6	282.2
W	8.4	281.4

289.80
S. Line Poplar on Curve.

Violet St
16

E = S. E. Cor Violet + Poplar	5.5	284.3
cl	5.6	284.2
"4	6.7	283.1
♀	6.6	283.2
"4	6.8	283.0
cl	6.8	283.0
W S. W. Cor. Violet + Poplar	7.1	282.7
	0+00 = 90°00' from S. W. Cor Poplar + Violet	
W S. W. Cor. Violet	7.1	282.7
cl	6.7	283.1
"4	6.8	283.0
♀	6.6	283.2
"4	6.6	283.2
+5	6.3	283.5
cl	5.5	284.3
E.	5.0	284.8
	0+50 S	
E	5.6	284.2
cl	6.0	283.8
"4	6.4	283.4
♀	6.5	283.3
"4	7.1	282.7
cl	7.0	282.8
W	7.3	282.5
	0+62 ♀ Walk to House	
E. on W. end walk	5.44	284.32

289.80 amt. 0+91 S. ϕ Two strips Drive to garage				285.74	Violet St	
E. on W. end emt. strip	5.52	284.28	W	4.6	285.8	17
	1+00		ch	4.4	281.2	
W	7.7	282.1	+2	4.2	281.4	
ch	7.3	282.5	+4	4.5	281.6	
1/4	7.1	282.7	ϕ	3.9	281.3	
ϕ	6.9	282.9	1/4	4.3	281.9	
1/4	6.8	283.0	+3	4.0	281.5	
ch	6.3	283.5	ch	3.9	281.8	
E	5.9	283.9	E	3.6	281.9	
	1+13				282.2	
Gum Tree 10" Diam 9' W. of E. Line			E.	4.1	281.7	
T.P. 289	285.76	6.93	282.87	ch.	4.2	281.6
	1+40 garage on E. emt. floor	2.5 back	+4	4.3	281.5	
E-25 floor	2.5	283.3	1/4	4.7	281.1	
	1+50		ϕ	4.6	281.2	
E	2.6	283.2	1/4	4.9	280.9	
ch	2.5	283.3	+2	5.3	280.5	
1/4	3.4	282.4	ch	4.8	281.0	
ϕ	3.4	282.4	W.	4.6	281.2	
+5	3.4	282.4			4.5 of N. Line ϕ Two strip emt. drive	
1/4	3.8	282.0	W. on emt. strip	4.77	280.99	
+4	3.4	282.4			N. ch line	
ch	3.4	282.4	W	5.0	280.8	
W	3.8	282.0	ch	5.0	280.8	
	1+56.5		1/4	5.2	280.6	
Gum Tree 10" Diam 9' W. of E. Line			ϕ	4.7	281.1	

285.76

'14	4.6	281.2
cl	4.7	281.1
E	4.4	281.4

5' S. of N. cl

8' E. of W. line Pepper Tree 10" Diam.

N. '14

E	4.8	281.0
cl	4.7	281.1
'14	4.5	281.3
♀	4.8	281.0
'14	5.2	280.6
+3	5.4	280.4
cl	5.1	280.7
W.	5.1	280.7

7' S. of N. '14

W of ent. walk

♀

W	4.8	281.0
cl	5.3	280.5
'14	5.6	280.2
♀	4.9	280.9
'14	4.6	281.2
cl	4.8	281.0
E	4.8	281.0

285.74

S. '14

Violet St.

18

E	5.3	280.5
cl	5.2	280.6
'14	4.8	281.0
♀	4.9	280.9
'14	5.3	280.5
+3	5.7	280.1
cl	5.3	280.5
W.	5.4	280.4

1' S. of S. '14

Pepper Tree 8" Diam 8' E. of W. line

S. cl

W	5.4	280.4
cl	5.5	280.3
+4	5.8	280.0
'14	5.5	280.3
♀	5.0	280.8
+4	4.8	281.0
'14	5.2	280.6
cl	5.6	280.2
+2	5.0	280.8
E	4.9	280.9

9400 = S. line Pepper Dr

E	5.1	280.7
cl	4.7	281.1
+3	4.7	281.1
+4	5.7	280.1

285.76
 0+00 = S. Line Pepper Dr (con)

E 14	5.5	280.3
+3	5.0	280.8
±	5.1	280.7
14	5.7	280.1
+3	5.9	279.9
cl	5.5	280.3
W	5.7	280.1

0+23¹⁵ = P.C. 50' Rad. Curve into Pepper Dr on W.

W	6.4	279.4
cl	6.0	279.8
14	5.9	279.9
±	5.5	280.3
14	5.6	280.2
+6	5.8	280.0
cl	5.6	280.2
E	5.2	280.6

T.P.

4.09 282.77 7.08 278.68
 45.90 S = P.I. 50' Rad Curve into
 Pepper Dr. on W. = N. Line

CHK. SW. 1/4 Cor
 Violet & Pepper

E	2.5	280.3
cl	2.8	280.0
+5	3.2	279.6
14	2.9	279.9
±	2.8	280.0
14	3.0	279.8
cl	3.4	279.4
W	4.1	278.7

282.77

Violet St

N. cl. line

19

W	3.8	279.0
cl	3.3	279.5
14	3.0	279.8
±	2.9	280.0
14	3.2	279.6
+3	3.1	279.7
cl	2.5	280.3
E	2.5	280.3

N. 14

E	2.5	280.3
cl	2.3	280.5
+3	2.4	280.4
14	3.1	279.7
14	3.2	279.6
±	2.9	279.9
14	3.1	279.7
cl	3.4	279.4
W	3.6	279.2

±

W	3.7	279.1
cl	3.4	279.4
14	3.2	279.6
±	3.0	279.8
14	3.3	279.5
+3	3.2	279.6
+4	2.4	280.4

282.77

♀ Pepper on W.

E. eb	2.4	280.4
E.	2.5	280.3
6 s. of ♀ Walk on E		
E. on W. end cont. walk	2.54	280.23
S. '14		
E	2.8	280.0
eb	2.6	280.2
+2	2.6	280.2
+3	3.4	279.4
'14	3.3	279.5
♀	3.0	279.8
'14	3.2	279.6
eb	3.6	279.2
W.	4.0	278.8
S. eb line Produced		
W	4.1	278.7
eb	3.5	279.3
'14	3.3	279.5
♀	3.1	279.7
'14	3.4	279.4
+4	3.4	279.4
eb	2.8	280.0
E	3.0	279.8
4' s. of S. eb line		
E	3.0	279.8
eb	3.1	279.7

282.77

Violet St.

20

+5	2.6	280.2
'14	3.2	279.6
♀	3.1	279.7
'14	3.4	279.4
eb	3.4	279.2
W	4.2	278.6
5' s. of S. eb.		
W	3.1	279.7
+3	4.1	278.7
eb	3.6	279.2
'14	3.4	279.4
♀	3.0	279.8
'14	3.3	279.5
+3	3.6	279.2
eb	3.1	279.7
E	3.0	279.8
S. Line Pepper Dr Produced from W. P.E. 20' Rad. Curve		
E	3.1	279.7
eb	3.1	279.7
+4	3.7	279.1
'14	3.3	279.5
♀	3.2	279.6
'14	3.5	279.3
eb	4.0	278.8
+5	3.1	279.7
W.	3.1	279.7

282.77

R1.78 S. of S line = P.C. 20' Rad. Curve into Pepper Dr on W.

W	4.1	278.7
cb	3.6	279.2
+4	4.1	278.7
14	3.9	278.7
4	3.4	279.4
14	3.7	279.1
+3	3.9	278.9
+6	3.4	279.4
cb	3.3	279.5
E	3.2	279.6

0+46⁰¹ S

E	3.8	279.0
cb	4.2	278.6
+2	4.3	278.5
+3	4.8	278.0
14	4.6	278.2
4	4.1	278.7
14	4.5	278.3
+6	4.8	278.0
cb	4.2	278.6
W	4.4	278.4

Plat Page 14.

Sec A 0+92⁰³ S = P.C. 20' R. Curve into Sycamore on W.

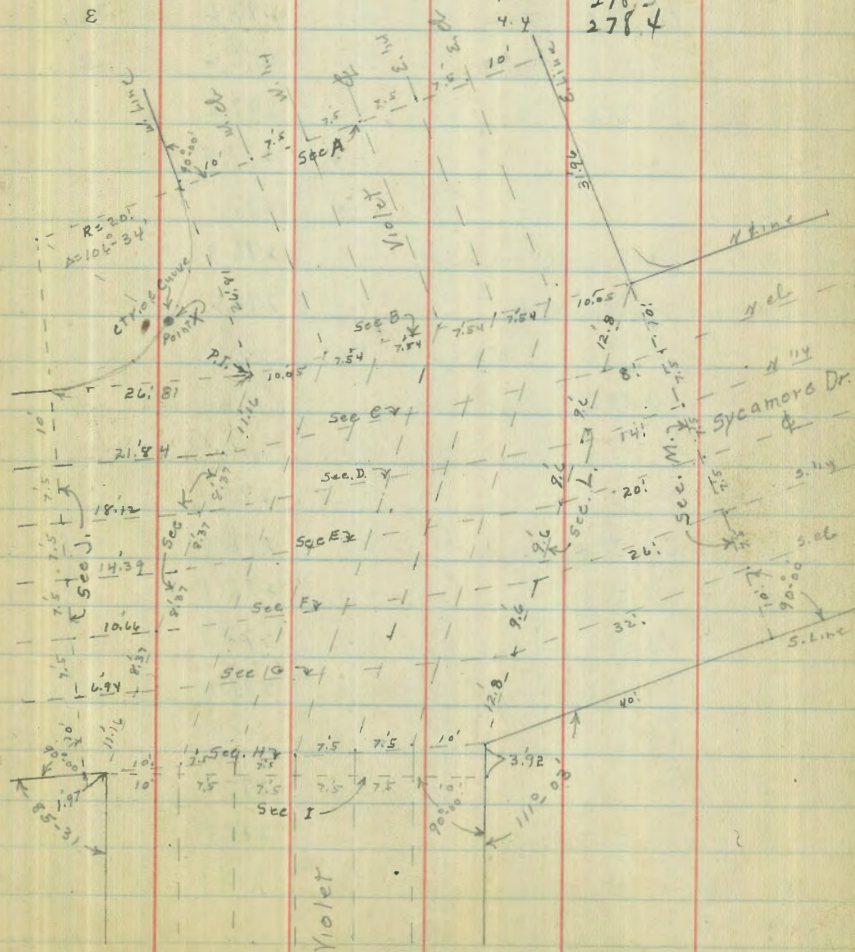
W-5	6.9	275.9
W-1	6.9	275.9
W.	5.7	277.1
+9	5.3	277.5

282.77

Violet St

21

cb	5.7	277.1
14	5.1	277.7
4	4.8	278.0
14	5.5	277.3
+2	5.4	277.4
+4	4.5	278.3
cb	4.5	278.3
E	4.4	278.4



282.77

T.P. 4.21 282.89 4.09 278.68

Ctr. Curve at NW. Cor Violet & Sycamore

at Point X 6.8 276.1

Sec. "B" - N. Line Sycamore

E.-N.E. Cor Violet + Sycamore 5.1 277.8

cl 5.2 277.7

+ 5 5.9 277.0

"4 5.7 277.2

♀ 5.6 277.3

"4 5.4 277.5

cl 5.8 277.1

W. on P.I. 20' Rad Curve on sec K. 6.6 276.3

13.4 W. on N. line Sycamore 6.4 276.5

26.81 " " " " " P.C. at sec J 8.8 274.0

Sec. "C" N. ch. line

at Sec. J. 8.1 274.7

10.9 E. 7.6 275.3

21.84 E at sec K = W 6.9 276.0

cl 6.3 276.6

"4 5.8 277.1

♀ 5.7 277.2

"4 5.8 277.1

cl 5.9 277.0

E at sec. L. 5.6 277.3

8. E. at sec M. 5.2 277.7

282.89

Sec. "D" N. 1/4 of Sycamore

at sec M. 5.8 277.1

14' W =
= E. at Sec. L. 5.8 277.1

cl 5.7 277.2

"4 5.9 277.0

♀ 5.9 277.0

"4 6.2 276.7

cl 6.6 276.3

W. at sec. K. 7.0 275.9

9.06 W 7.5 275.4

18.12 W at Sec. J. 8.1 274.8

Sec. E ♀

at sec. J. 7.9 275.0

7.2 E 7.4 275.5

14.39 E = W Line at sec. K. 7.1 275.8

cl 6.7 276.2

"4 6.4 276.5

♀ 6.1 276.8

"4 6.0 276.9

cl 6.0 276.9

E at sec. L. 6.0 276.9

10' E 5.7 277.2

20' E. at sec. M. 5.6 277.3

Violet St

22

282.89

Sec. "F." S. 1/4 of Sycamore

at Sec. M.	6.0	276.9
13' W	6.3	276.6
26' W. = E. line at Sec. L.	6.6	276.3
cl	6.8	276.1
'14	6.5	276.4
cl	6.4	276.5
'14	6.6	276.3
cl	7.1	275.1
W. line at sec. K.	7.6	275.3

1066 W. at sec. J.

Sec. "G." S. cl. line

at sec. J.	8.1	274.8
6.94 E. = W. line at sec. K.	7.5	275.4
+5	7.8	275.5
cl	7.4	275.5
'14	6.9	276.0
cl	6.6	276.3
'14	7.3	275.6
+4	7.5	275.4
cl	6.5	276.4

E. line at sec. L.

16' E

32' E. at sec. M.

Sec. "H." S. line Sycamore

at sec. M.	6.3	276.6
20' W	6.5	276.4
40' W at sec. L. = S.E. Cor. { Violet & Sycamore	6.95	275.24
+5	6.8	276.1

on H4b

Violet St

282.89

23

cl	7.3	275.6	
'14	7.5	275.4	
cl	6.8	276.1	
'14	7.3	275.6	
cl	7.2	275.7	
W. at S.W. Cor. Violet + Sycamore	7.5	275.4	at sec K
1.97 W. at Sec. J. at 90° from P.C. on W.	7.6	275.3	
0+00 = Sec. I. at 90° from S. W. Cor.			
W at S.W. Cor	7.5	275.4	
cl	7.2	275.7	
'14	7.5	275.4	
cl	6.9	276.0	
'14	7.6	275.3	
cl	7.3	275.6	
E 3.92 S. of S.E. Cor.	7.0	275.9	
0+50 S.			
E	8.2	274.7	
cl	8.7	274.2	
+3	9.1	273.8	
'14	8.5	274.3	
cl	8.1	274.8	
'14	8.4	274.5	
cl	8.2	274.7	
W.	8.5	274.4	

282.89

1700 S. of Sec I

W.	9.1	273.8
cb.	9.2	273.7
"4	9.6	273.3
±	8.9	274.0
"4	9.5	273.4
cb.	9.6	273.3
E.	9.7	273.2

1750 S.

E.	10.5	272.4
cb.	10.3	272.6
+3	10.3	272.6
+5	11.5	271.4
"4	10.2	272.7
±	9.7	273.2
"4	10.5	272.4
cb.	10.2	272.7
W.	10.3	272.6

2400 S.

W.	11.4	271.5
cb.	11.5	271.4
+4	11.7	271.2
"4	11.5	271.4
±	11.2	271.7
"4	12.0	270.9
+5	11.5	271.4
cb.	11.6	271.3
E.	11.9	271.0

282.89

2+37 S. = ± cut drive on E.

Violet ST

24

E. on cut Drive	12.54	270.35
+7.5 = W. End Drive	12.27	270.62
cb.	12.5	270.4
+5	12.6	270.3
"4	12.2	270.7
±	11.7	271.2
"4	12.1	270.8
+3	12.3	270.6
cb.	12.1	270.8
W.	12.5	270.4

T.P. 4.10 274.85 12.14 270.75

2+600 S = Sec. N. Beginning of banjo. Plat. Page 14

W. at Beginning Curve	5.3	269.6
cb.	5.0	269.9
"4	4.3	270.6
±	4.3	270.6
"4	4.5	270.4
cb.	5.2	269.7
+2	4.6	270.3

E. at beginning of Curve 4.7 270.2

Curve Divided into 6 Parts A 41°11'

Sec. "U"

Propine at E. End Sec. N.	4.7	270.2
+10 = cb.	4.7	270.2
+11	5.2	269.7
+20	4.8	270.1
+30 on 30' Radius Hub	4.4	270.21

274.85

See "T"

Property line	5.0	269.9
+10 = cl	4.9	270.0
+14	5.5	269.4
+20	4.9	270.0
+30 = 30' Rad. Hub	4.64	270.21

See "S"

Prop line	5.4	269.5
+10 = cl	5.7	269.2
+20	5.1	269.8
+30 = Radius Hub	4.64	270.21

See "R"

Prop line	6.5	268.4
+10 = cl	5.6	269.3
+20	4.9	270.0
+30 = Radius Hub	4.64	270.21

See "A"

Prop line	6.1	268.8
+10 = cl	5.6	269.3
+20	4.8	270.1
+30 = Radius Hub	4.64	270.21

See "B"

Prop line	6.0	268.9
+10 = cl	5.5	269.4
+20	5.0	269.9
+30 = Rad. Hub	4.64	270.21

274.85

See "O"

Prop line	5.2	269.7
+10 = cl	5.3	269.6
+20	4.7	270.2
+30 = Radius Hub	4.64	270.21

Profile for Culvert 7

On lot line bet. Lots 15 + 16 BIK 26.

Plat Page 14

10' E. of 0+00 = cl. line	5.5	269.4	
0+00 = Property line	5.9	269.0	
0+15	6.6	268.3	
0+30	7.8	267.1	
0+50	11.8	263.1	
T.P. 0.30	262.48	12.67	262.18
0+75	8.0	254.5	
T.P. 0.32	249.99	12.81	249.67
0+95	4.0	246.0	
T.P. 0.09	238.12	11.96	238.03
1+17	2.0	236.1	
1+32 ²³ = E. line Alley	9.8	228.3	
1+40 = ϕ Wash	13.2	224.9	

Violet St

25

50' wide
10' elev.
7.5' 1/4 s.

Sycamore Drive X Sec.
Tuberosc To Shamrock

284.79

1700 W.

26

BM. S.E. Biker.

8.85 284.79

275.94

Violet +
Sycamore.

S.

4.9

279.9

M. line Tuberosc. on Diagonal 52.87

cl.

4.6

280.2

N.

3.5

281.3

1/4

4.5

280.3

cl

3.8

281.0

1/4

4.1

280.7

1/4

4.7

280.1

1/4

4.5

280.3

1/4

4.5

280.3

+ 3

4.6

280.2

1/4

4.4

280.4

+ 4

4.2

280.6

cl

4.7

280.1

cl

4.0

280.8

S. at S.W. Cor.

5.1

279.7

N

3.7

281.1

17.17 W on N = 0 + 100 = 90-00 from S.W. Cor

1750 W.

S at S.W. Cor.

5.1

279.7

N.

4.2

280.6

cl

4.7

280.1

cl.

4.5

280.3

1/4

4.2

280.6

1/4

5.1

279.7

1/4

4.2

280.6

1/4

4.4

280.4

1/4

4.5

280.3

1/4

4.9

279.9

cl

3.8

281.0

cl

5.3

279.5

N

3.4

281.4

S.

5.5

279.3

0 + 50 W

1778⁵⁰ 1/4 cmt. drive on N

N.

3.5

281.3

S.

5.2

279.6

cl

3.8

281.0

cl.

5.4

279.4

1/4

4.2

280.6

1/4

5.3

279.5

1/4

3.8

281.0

1/4

4.8

280.0

1/4

3.9

280.9

1/4

5.0

279.8

cl

3.9

280.9

cl

4.8

280.0

S

4.0

280.8

N. dirt

4.6

280.2

W on cmt. drive

4.34

280.45

Plotted Nov. 3 - 1930

284.79
2+00 W.

N	5.0	279.8
cb	5.1	279.7
1/4	5.4	279.4
±	5.2	279.6
1/4	5.5	279.3
cb	6.0	278.8
S.	6.3	278.5

2+50 W.

S.	7.4	277.4
cb	6.9	277.9
1/4	6.8	278.0
±	6.4	278.4
1/4	7.0	277.8
+3	6.9	277.9
+4	6.3	278.5
cb	6.3	278.5
N	6.1	278.7

2+97⁵⁷ W = W. line Violet produced S. = See M. Page 21

N.	7.0	277.8
cb	7.1	277.7
1/4	7.7	277.1
±	7.5	277.3
1/4	7.9	276.9
cb	7.8	277.0
S.	8.2	276.6

284.79

0+00 = P.T. W. of Violet on N. 1/4 W. of S.W. Cor. = See J. Page 21.

Sycamore Dr.

S.	9.5	275.3
cb	10.0	274.8
1/4	10.1	274.7
±	9.8	275.0
1/4	10.0	274.8
cb	10.1	274.7
N	10.8	274.0
+8	10.3	274.5

0+10 W.

-5	10.4	274.2
N	10.6	274.2
cb	10.6	274.2
1/4	10.5	274.3
±	10.6	274.2
1/4	10.9	273.9
+5	11.8	273.0
cb	11.3	273.5
S	10.4	274.4

T.P. 2.15 275.88 11.06 273.73

0+35 W.

S-10	3.3	272.6
S	4.4	271.5
+8	7.0	268.9
cb	6.4	269.5
1/4	3.5	272.4
+2	3.0	272.9

275.88

0+35 W. (con)

Φ	2.5	273.4
1/4	2.3	273.6
cl	2.2	273.7
+5	2.2	273.7
N.	1.1	274.8
0+45 W.		
N.	0.8	275.1
+6	2.5	273.4
cl	2.3	273.6
1/4	2.7	273.2
Φ	3.1	272.8
+1	3.1	272.8
1/4	7.5	268.4
+5	9.4	266.5
cl	9.5	266.4
S.	6.4	269.5
+10	4.0	271.9
0+65 W.		
S.-20	6.4	269.5
S.	12.4	263.5
cl.	11.6	264.3
1/4	6.7	269.2
+5	3.0	272.9
Φ	3.0	272.9
1/4	2.7	273.2
cl.	2.5	273.4

275.48

Sycamore Dr.

28

+3	2.6	273.3
+5	1.5	274.4
N.	1.2	274.7
0+80 W.		
N.	1.4	274.5
+6	1.6	274.3
+7	2.7	273.2
cl	2.7	273.2
1/4	2.7	273.2
Φ	2.9	273.0
+3	3.0	272.9
1/4	5.1	271.8
cl	9.3	266.6
S.	13.7	262.2
+20	13.1	262.8
0+87 ⁸³ W = P.C. { N. line R = 144.83 } divided 5. Parts Δ 10° 14' N. line hole 2.87 S. line R = 134.83 } S. line hole 24.05		
S-30	15.5	260.4
S-15	17.0	259.9
S.	11.1	264.8
cl.	7.9	268.0
1/4	4.4	271.5
+2	3.4	272.5
Φ	3.0	272.9
1/4	2.8	273.1
cl	2.8	273.1
+2	2.7	273.2
+4	1.7	274.2
N	1.5	274.4

275.88
Sec. 7 $\Delta 10^{\circ}-14'$

N.	1.2	274.7
+ 8	2.0	273.9
cl	3.0	272.9
'4	2.8	273.1
cl	3.0	272.9
'4	3.0	272.9
cl	5.1	270.8
S	8.0	267.9
+ 15	12.0	263.9

Sec. 2 $\Delta 20^{\circ}-28'$

S-10	7.1	268.8
S	5.1	270.8
cl	3.8	272.1
'4	3.3	272.6
cl	3.1	272.8
'4	3.0	272.9
cl	3.0	272.9
+ 4	2.0	273.9
N	2.0	273.9

Sec. 3 $\Delta 30^{\circ}-42'$

X	3.2	272.7
cl	3.4	272.3
+ 3	4.1	271.8
'4	3.3	272.6
+ 4	3.1	272.8
cl	3.4	272.5

275.88

Sycamore Dr

29

'4	3.1	272.8
cl	3.2	272.7
S	3.9	272.0

Sec. 4 $\Delta 40^{\circ}-56'$

S	5.0	270.9
cl	4.6	271.3
'4	4.6	271.3
+ 3	4.7	271.2
cl	4.2	271.7
'4	4.4	271.5
cl	4.6	271.3
+ 2	4.0	271.9
N.	3.8	272.1

0+00 Sec. 5 = E.C. $\Delta 51^{\circ}-10'$

N	4.4	271.5
+ 7	4.6	271.3
cl	5.2	270.7
'4	4.8	271.1
+ 5	4.2	271.7
cl	4.5	271.4
+ 5	4.4	271.1
'4	4.0	271.9
cl	4.3	271.6
S	5.3	270.6

275.88

0+25 W

S	6.1	269.8
cl	5.2	270.7
'14	4.9	270.0
+5	5.4	270.5
±	5.5	270.4
+5	5.2	270.7
'14	5.3	270.6
cl	5.9	270.0
+3	5.2	270.7
N	4.8	271.1

0+50 W.

N	4.9	271.0
+8	5.1	270.8
cl	6.2	269.7
'14	6.0	269.9
+4	5.8	270.1
±	6.0	269.9
'14	6.2	269.7
cl	6.0	269.9
S	6.7	269.2

0+75 W

S	7.0	268.9
cl	6.4	269.5
'14	6.5	269.4
+3	6.8	269.1
±	6.2	269.7

275.88

Sycamore Dr.

30

+4	6.2	269.7
'14	6.6	269.3
+4	7.5	268.4
cl	7.5	268.4
+2	5.7	270.2
N.	5.3	270.6

1+00 W.

N.	7.0	268.9
+7	7.2	268.7
cl	8.3	267.6
'14	7.4	268.5
+3	7.1	268.8
±	7.2	268.7
+5	7.8	268.1
'14	7.4	268.5
cl	7.5	268.4
S	7.8	268.1

5 Line R=100
 1+27⁶² P.C. N. Line R=50 A 4B-32-R Parts S " " 37.76
 N. Line chd 18.88

S	8.45	267.43	on Hub P.C.
cl	8.3	267.6	
'14	8.4	267.5	
±	8.3	267.6	
'14	7.8	268.1	
cl	8.8	267.1	
+3	8.0	267.9	
N	7.2	268.7	

275.88
see 1st curve $\Delta 21^{\circ}46'$

N	7.8	267.1
cl	9.0	266.9
1/4	8.4	267.5
1/2	8.4	267.5
+4	8.8	267.1
1/4	8.7	267.2
+2	8.3	267.6
cl	8.3	267.6
S.	8.8	267.1

see 2, $\Delta 43^{\circ}32' = P.A.C.$ 30' Rad. into Shamrock on S.

S. at P.A.C.	8.9	267.0		
cl.	8.8	267.1		
1/4	9.2	266.7		
1/2	8.5	267.4		
+2	8.4	267.5		
1/4	9.0	266.9		
+5	9.4	266.5		
cl	8.7	267.2		
N.	8.5	267.4		
T.P.	6.57	281.34	1.11	274.77
chk. B.M. Hub S.E. Violet + Sycamore	5.40	275.94		

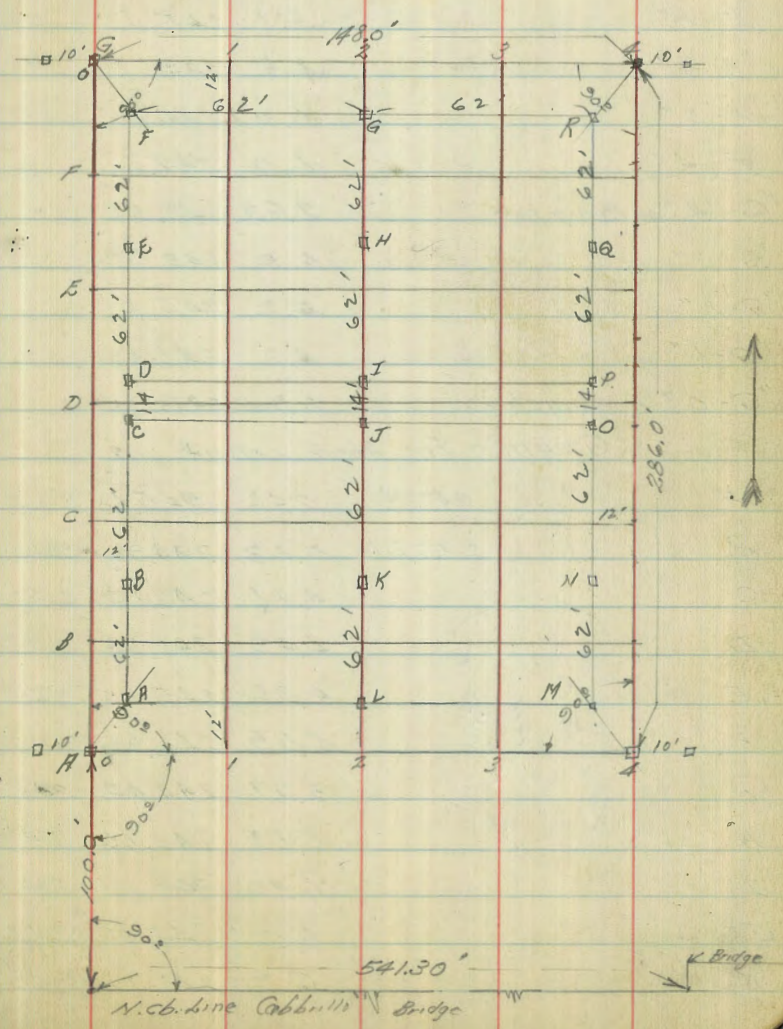
Moore
Walker
Flood
Northern
Morley 12-4-30

CONTOURS
FOR BOWLING GREEN
IN BARBOUR PARK

	2.93	254.86	251.93
T.P.	2.24	250.93	6.17 248.69
Set Temp. P.M.		1.23	249.00
"A-0" on stub		4.82	246.11
"A-1"		7.1	243.8
"A-2"		8.5	242.4
"A-3"		9.0	241.9
"A-4"		9.2	241.7
"B-0"		5.0	245.9
T.P.	4.48	250.21	5.20 245.73
"B-1"		5.9	244.3
"B-2"		7.2	243.0
"B-3"		7.8	242.4
"B-4"		7.9	242.3
"C-4"		7.5	242.7
"C-3"		7.2	243.0
"C-2"		6.8	243.4
"C-1"		5.6	244.6
"C-0"		4.2	246.0
"D-0"		3.9	246.3
"D-1"		5.3	244.9
"D-2"		6.3	243.9
"D-3"		6.6	243.6
"D-4"		6.6	243.6
"E-4"		5.9	244.3

N.H. 20
Level + 6.25

3 nails in wall
2' West of entry
to Bowling Green



250.21

"E-3"	6.0	244.2
"E-2"	6.0	244.2
"E-1"	5.3	244.3
"E-0"	3.9	246.3
"F-0"	3.6	246.6
"F-1"	5.1	245.1
"F-2"	5.5	244.7
"F-3"	6.0	244.2
"F-4"	6.0	244.2
"G-4" on Paving state	7.69	242.58
"G-3"	6.5	243.7
"G-2"	5.2	245.0
"G-1"	4.2	246.0
"G-0" on Paving state	2.90	247.31

GRADAS For Above Layout

A	247.94	246	245.48	243.5	+1.98
B	250.21	5.23	244.98	243.5	+1.48
C		4.11	246.10	243.5	+2.60
D		4.43	245.78	243.5	+2.28
E		4.36	245.85	243.5	+2.35
F		3.55	246.66	243.5	+3.16
G		5.77	244.44	243.5	+0.94
H		5.55	244.66	243.5	+1.16
I		6.40	243.81	243.5	+0.31
J		6.21	244.00	243.5	+0.50
K		6.90	243.31	243.5	-0.19

GRADAS
Changed
see p. 34

250.21

L	7.68	242.53	243.5	-0.97
M	8.55	241.66	243.5	-1.84
N	7.68	242.53	243.5	-0.97
O	6.84	243.37	243.5	-0.13
P	6.36	243.85	243.5	+0.35
Q	6.08	244.13	243.5	+0.63
R	6.77	243.44	243.5	-0.06

250.21
8.55
241.66
6.28
247.94
1.83
246.11

chk. on p. 0

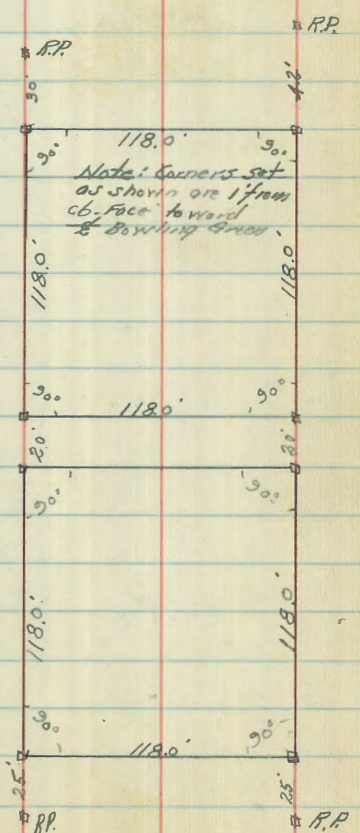
33

BOWLING GREEN

Re-staked

	X		GRADE Below Green		Cuts in fourths	Cuts in Inches
A	249.62	4.13	245.49	243.00	+2.49	+2'-6"
B	249.62	4.63	244.99	243.00	+1.99	2'-0"
C	249.62	3.50	246.12	243.00	+3.12	3'-1 1/2"
D	249.62	3.83	245.79	243.00	+2.79	2'-9 1/2"
E	249.62	3.75	245.87	243.00	+2.87	2'-10 1/2"
F	249.62	2.95	246.67	243.00	+3.67	2'-8"
G	249.62	5.17	244.45	243.00	+1.45	1'-5 1/2"
H	249.62	4.95	244.67	243.00	+1.67	+1'-8"
I	249.62	5.79	243.83	243.00	+0.83	+0'-10"
J	249.62	5.61	244.01	243.00	+1.0	+1'-0"
K	249.62	6.31	243.31	243.00	+0.31	+0'-4"
L	249.62	7.08	242.54	243.00	-0.46	-0'-5 1/2"
M	249.62	8.01	241.61	243.00	-1.39	-1'-4 3/4"
N	249.62	7.08	242.54	243.00	-0.46	-0'-5 1/2"
O	249.62	6.24	243.38	243.00	+0.38	+0'-4 1/2"
P	249.62	5.77	243.85	243.00	+0.85	+0'-10 1/2"
Q	249.62	5.49	244.13	243.00	+1.13	+1'-1 1/2"
R	249.62	6.18	243.44	243.00	+0.44	+0'-5 1/2"

BM. Page 32 = 249.00
0.62 +
249.62 X



Dickens St Cross Section
Roscreaw to Evergreen

70' wide

Ⓟ

21.07

Jan. 2-31
J. J. J.
McHugh
Hartford

35

BM	11.15	21.07	992	SW of M ₁₁ Roscreaw - Dickens		256' W		
		W.L. Roscreaw			N		6.3	14.8
					E		7.3	13.8
S		10.9	10.2		E		7.3	13.8
L		11.6	9.5			275' W		
F		121	9.0		E		6.8	14.3
		27' W of W.L. Roscreaw			L		6.8	14.3
F		112	9.9		N		6.0	15.1
L		110	10.1			300' W = E.L. Locust 70' wide		
N		10.2	10.9		N		5.9	15.2
		50' W of W.L. Roscreaw			L		6.0	15.1
N		101	11.0		F		6.4	14.7
L		107	10.4			L Locust		
F		111	10.0		F		5.7	15.4
		100' W			L		5.1	16.0
F		105	10.6		N		5.3	15.9
L		101	11.0			W.L. Locust		
N		90	12.1		N		4.2	16.9
		150' W			L		4.7	16.4
N		82	12.9		F		5.5	15.6
L		92	11.9			25' W of W.L. Locust		
F		97	11.4		E		4.5	16.6
		200' W			L		4.4	16.7
F		80	13.1		N		3.9	17.2
L		82	12.9			50' W of W.L. Locust		
N		72	13.9		N		3.6	17.5

21.07

36

♂	41	17.0
♀	43	16.8

100 M of *M. locust*

♀	45	16.6
♂	32	17.9
W	25	18.6

150 M

W	26	18.5
♂	32	17.9
♀	41	17.0

200 M

♀	40	17.1
♂	32	17.9
W	25	18.6

250 M

W	20	19.1
♂	27	18.4
♀	35	17.6

275 M

♀	26	18.5
♂	21	19.0
W	14	19.7

300 M = E.L. *F. virginiana*

W	10	20.1
♂	12	19.9
♀	17	19.4

Locust St Cross Section
Emerson to Carleton

70' wide

Q

21.07

Jan 31/37

21.07

J.L. Emerson

H	80	13.1
L	86	12.5
F	90	12.1

25' S of J.L. Emerson

F	88	12.3
L	83	12.8
H	77	13.4

50' S

H	70	14.1
L	79	13.2
F	87	12.4

100' S

F	81	13.0
L	72	13.9
H	67	14.4

150' S

H	55	15.6
L	64	14.7
F	70	14.1

175' S

F	68	14.3
L	60	15.1
H	51	15.5

200' S H.L. Locust

H	55	15.6
L	57	15.4
F	64	14.7

J.L. Locust

F	60	15.1
L	51	16.0
H	42	16.9

25' S of J.L. Locust

H	41	17.0
L	45	16.6
F	47	16.4

50' S of J.L. Locust

F	43	16.8
L	40	17.1
H	35	17.6

100' S

H	24	18.7
L	29	18.2
F	28	18.3

150' S

F	16	19.5
L	11	20.0
H	06	20.5

505 2584 028 20.79

1584

175 J

M	41	21.7
L	49	20.9
F	56	20.2

200 J: H. Carleton

F	52	20.6
L	46	21.2
M	42	21.6
BM	1130	14.54

500 BP
 1000 BP
 1500 BP

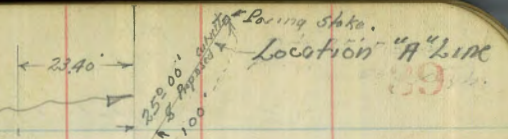
Walker
Bliss
Hornay
3-3-31

ROSS SECTION
KEELER St. 50' wide
From Highland Ave to West Termination

7' cb.
9' 45"

(R)

Location
"B" line



#1. 76.38 72.48
B.M. N.Y. Keeler = See Grade Book 151-73
Highland plug See matter for explanation

Sec. A

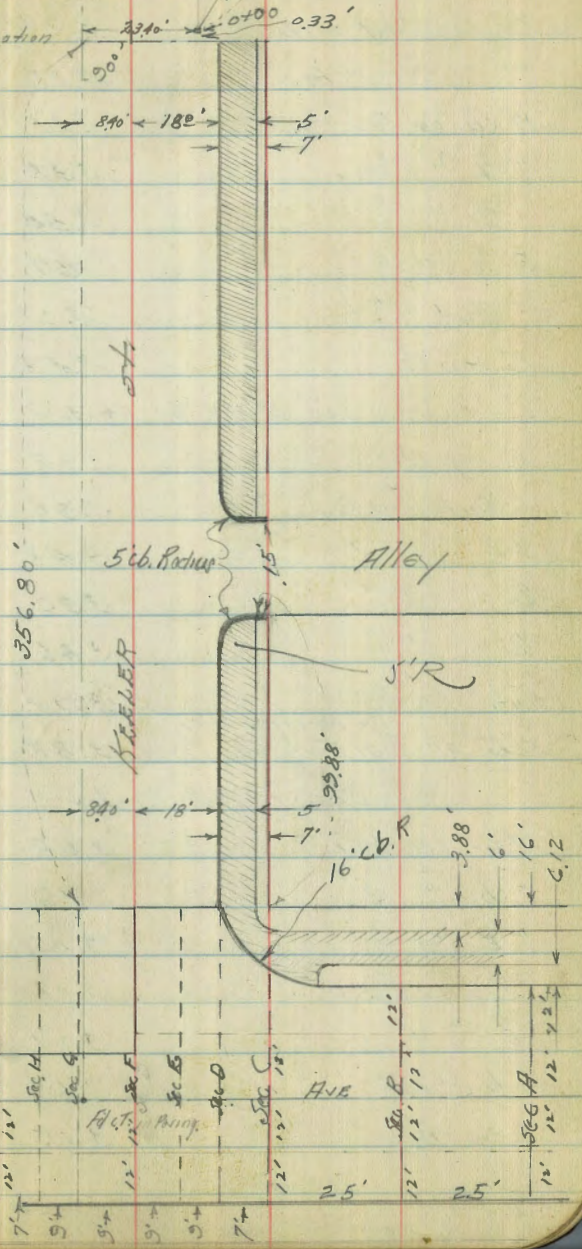
E top cb.	4.80	71.58
E Gut. on Pav.	5.34	71.04
E 1/4 " "	5.00	71.38
L " "	4.80	71.58
M 1/2 " "	4.89	71.49
M Gut " "	5.40	70.98
1/4 top cb.	4.84	71.54

Sec. B

top 1/4 cb.	4.36	72.12
Gut. on Pav.	4.80	71.58
M 1/2 " "	4.92	72.06
L " "	4.23	72.15
E 1/4 " "	4.38	72.00
E Gut " "	4.80	71.58
E top cb.	4.24	72.14

Sec. C - N.Y. Keeler

E top cb.	3.68	72.70
E Gut on Pav.	4.22	72.16
" 1/4 " "	What → 4.89	71.55
L " "	3.73	72.65
M 1/2 " "	3.72	72.66
M cb. on Pav.	4.26	72.12
+ 2.8 at cb Return on Pav.	4.25	72.13
+ 2.8 on " "	3.69	72.69



H.L.
7638

7638

40

Sec. D. = H. cb. Laine Keeler.

M. Highland on cb.	3.70	72.68
" " " Pav.	4.29	72.09
H. cb. on Pav.	4.17	72.21
" $\frac{1}{2}$ " "	3.58	72.80
L " "	3.52	72.84
E $\frac{1}{4}$ " "	3.67	72.71
" Gut. " "	4.07	72.31
E top cb.	3.53	72.85

Sec. E. = N $\frac{1}{2}$ Keeler.

E top cb.	3.35	73.03
E Gut. on Pav.	3.90	72.48
L " "	3.48	72.90
L " "	3.32	73.04
H " "	3.36	73.02
Gut. " "	3.23	72.45
M. h. on Rim Gate Gas Main	3.88	72.50

Sec. F. = L Keeler

M. h. on Pav.	3.63	72.75
" cb. " "	3.70	72.68
" $\frac{1}{2}$ " "	2.15	73.23
L " "	3.07	73.31
$\frac{1}{4}$ " "	3.21	73.17
E Gut. on "	3.69	72.69
" top cb.	3.15	73.23

Sec. G.

E cb.	2.93	73.45
Gut. on Pav.	3.48	72.90
$\frac{1}{4}$ " "	3.05	73.33
L " "	2.93	73.45
+8.9 = Wedge Pav.	3.01	73.37
$\frac{1}{4}$ " "	3.1	73.3
cb.	3.6	72.8
H.	3.9	72.5

Sec. H.

H.	3.7	72.7
cb.	3.5	72.9
+3.1 = Wedge Pav.	2.83	73.55
L on Pav.	2.77	73.61
$\frac{1}{4}$ " "	2.83	73.55
Gut. " "	3.25	73.13
cb.	2.67	73.71

Sec. I.

E cb.	2.98	73.90
Gut.	3.11	73.27
$\frac{1}{4}$	2.67	73.71
L	2.60	73.78
+8.8 = Wedge Pav.	2.67	73.71
$\frac{1}{4}$	2.7	73.7
cb.	3.2	73.2
H.	3.5	72.9

Sec. J. = 25' S.S. Keeler

76.38

M.L.	3.1	73.3
cb.	2.5	73.9
$\frac{1}{4}$	2.1	74.3
+3.2 = Hedge Pav.	2.07	74.31
L on Pav.	2.02	74.36
E $\frac{1}{2}$ " "	2.11	74.27
E Gut. " "	2.45	73.93

Sec 15 = 50' South St. Koeler.

E Gut. on Pav	1.77	74.61
" $\frac{1}{2}$ on Pav.	1.46	74.92
L " "	1.86	75.02
+8.8 on Hedge Pav.	1.41	74.97
$\frac{1}{4}$	1.4	75.0
cb.	2.0	74.4
M.L.	2.3	74.1

M.L. Highland Ave = 0+00

0+25

S	4.0	72.4
cb.	3.8	72.6
$\frac{1}{4}$	4.5	71.9
L	4.4	72.0
$\frac{1}{2}$	4.6	71.8
Gut.	4.9	71.5
cb.	4.27	72.11
N	4.5	71.9

0+50

76.38

41

N	4.7	71.7
cb.	4.68	71.70
Gut.	5.4	71.0
$\frac{1}{4}$	5.0	71.4
L	4.8	71.6
$\frac{1}{2}$	4.6	71.8
cb.	4.2	72.2
S	4.3	72.1

0+75

S	5.0	71.4
cb.	4.6	71.8
$\frac{1}{4}$	5.1	71.3
L	5.2	71.2
$\frac{1}{2}$	5.5	71.9
Gut.	5.5	71.9
cb.	5.16	71.22
N	5.1	71.3

0+94.88 = P.C. 5' Ch. R

0+99.88 = Sta. ^{of face E side} Alley on N

N top ch. at Prop. line	5.37	71.01
Gut.	6.1	70.3
cb. on Ground	6.2	70.2
$\frac{1}{4}$	5.9	70.5
L	5.7	70.7
$\frac{1}{2}$	5.7	70.7
cb.	5.4	71.0

76.38

U	5.2	71.2
1+14.88 = E. face cb. on N.W. Alley	5.50	70.88
+12.88 = E.C. 5' cb. Radius.	5.81	70.57
1+25		
U	5.1	71.3
cb.	5.8	70.6
$\frac{1}{2}$	6.2	70.2
$\frac{1}{2}$	6.0	70.4
$\frac{1}{2}$	6.3	70.1
Gut.	6.7	69.7
cb.	5.89	70.49
N	5.7	70.7
1+50		
N	6.1	70.3
cb.	6.44	69.94
Gut.	7.2	69.2
$\frac{1}{2}$	6.8	69.6
$\frac{1}{2}$	6.5	69.9
$\frac{1}{2}$	6.3	70.1
+2	6.5	69.9
cb.	5.6	70.8
U	5.55	70.9
1+75		
U	5.6	70.8
cb.	6.2	70.2
$\frac{1}{2}$	6.9	69.5

76.38

42

$\frac{1}{2}$	6.9	69.5
$\frac{1}{2}$	7.2	69.2
Gut. in Drive Way	7.69	68.69
+3' = Bit. in	6.86	69.52
N	6.8	69.6
1+80 on N. on cb.	7.07	69.31
1+96.3 " " "	7.51	68.87
3+00		
N	7.3	69.1
cb.	7.68	68.70
Gut.	8.3	68.1
$\frac{1}{2}$	8.0	68.4
$\frac{1}{2}$	7.7	68.7
$\frac{1}{2}$	7.8	68.6
cb.	6.9	69.5
U	6.5	69.9
2+12.15 = Bit. in cb. on N	8.60	67.78
2+25		
U	7.6	68.8
cb.	8.3	68.1
$\frac{1}{2}$	8.9	67.5
$\frac{1}{2}$	9.0	67.4
$\frac{1}{2}$	9.2	67.2
Gut.	9.8	66.6
N-top cb	8.85	67.53
N	8.4	68.0

76,38

2+80 on N = 8th incb.	3.20	67.18
2+40 " " " " "	3.97	66.41
+0.45 " " " " "	10.32	66.06
2+50		
N	10.4	66.0
cb.	10.81	65.57
Gut.	11.5	64.9
$\frac{1}{2}$	11.2	65.2
$\frac{1}{2}$	10.8	65.6
$\frac{1}{2}$	10.3	66.1
cb.	9.7	66.7
S	8.8	67.6
2+60 on N = 8th incb.	11.70	64.68
2+70 " " " " "	12.61	63.77
T.P.	2.04	65.42
	13.00	63.38
2+75		
S	16	63.8
cb.	15	63.9
$\frac{1}{2}$	19	63.5
$\frac{1}{2}$	22	63.2
$\frac{1}{2}$	24	63.0
Gut.	2.2	63.2
top cb.	2.16	63.26
N	1.5	63.9
2+95		
N	4.0	61.4

65,42

43

cb.	4.13	61.29
Gut.	4.2	61.2
$\frac{1}{2}$	4.4	61.0
$\frac{1}{2}$	4.4	61.0
$\frac{1}{2}$	4.1	61.3
cb.	3.9	62.0
S	3.8	62.6
	3+10	
S	3.0	62.4
cb.	4.1	61.3
$\frac{1}{2}$	5.6	59.8
+5	6.1	59.3
$\frac{1}{2}$	5.8	59.6
$\frac{1}{2}$	6.0	59.4
Gut.	5.6	59.8
cb.	5.63	59.79
N	5.4	60.0
	3+25	
N	6.9	58.5
cb.	7.08	58.34
Gut.	7.5	57.9
$\frac{1}{2}$	7.8	57.6
$\frac{1}{2}$	7.2	58.2
+5	5.2	60.2
$\frac{1}{2}$	4.5	60.9
cb.	4.1	61.3
S	2.9	62.5

6542

3+45

S	2.8	62.6
cb.	3.3	62.1
z	2.7	62.7
+2	2.2	63.2
L	8.0	57.4
+2	9.0	56.4
z	9.2	56.2
Aut.	9.10	56.3
cb.	9.10	56.32
N	9.0	56.4

3+56.8 = End cb. on N

N	10.2	55.2
cb.	10.25	55.17
z	9.7	55.7
+5	9.4	56.0
L	8.4	57.0
+4	3.8	61.6
z	3.2	62.2
cb.	4.2	61.2
S	3.9	61.5

3+70

S	5.0	60.4
cb.	6.4	59.0
z	6.0	59.4
+6'	6.8	58.6

K
6542

44

L	8.6	56.8
z	9.6	55.8
cb.	10.3	55.1
N	10.7	54.7

Levels For Proposed Culvert Location "A"

0+00		10.7	54.7	
+22		11.7	53.7	
T.P.	0.88	53.21	12.99	52.43
+35		7.0	46.3	
+65		10.2	43.1	
+75		11.4	41.9	

L

41.92

M

Proposed

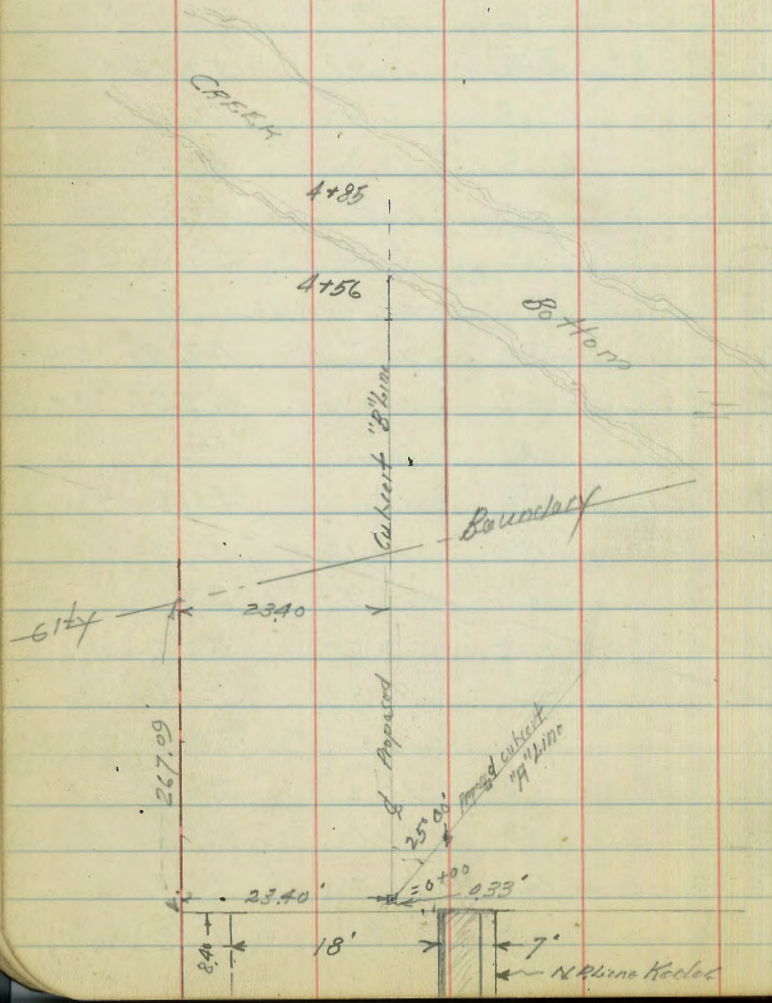
3.85 49.46 38.07

Levels For "Culvert Location B"

0+00		10.7	42.6	54.7
+25		10.8	42.5	54.6
+50		6.2	47.1	
+75		12.2	41.1	
T.P.	0.73	41.92	12.12	41.19
+100		4.9	37.0	
+130		9.5	32.4	
+160		11.8	30.1	
+180		13.8	28.1	
+200		15.2	26.7	
+230		16.1	25.8	
+256 = Brown River Bank		16.5	25.4	
+260		24.7	17.2	

41.92

4768		283	13.6
+85 = RIVER Bed		28.0	13.9
T.P.	13.26	54.45	0.73
T.P.	11.70	65.76	0.39
T.P.	11.15	75.85	1.06
Starting B.M.		3.37	72.48



Market St B.M. Levels

4-9-81
Mills
Lammeyer
Aspen

✓

s. of Market				
B.P. old City Boundary	1.73	141.65		139.92
T.P.	8.39	137.68	12.36	129.29
(B.M.)			1.55	136.13
T.P.	7.42	132.51	12.59	125.09
(B.M.)			9.99	122.52
(B.M.) s. Bottom Belt			2.17	130.34
T.P.	0.83	132.73	0.61	131.90
(B.M.)			0.22	132.51
T.P.	9.98	139.76	2.95	129.78
(B.M.)			4.23	135.53
T.P.	12.88	152.16	0.48	139.28
(B.M.)			8.53	143.63
T.P.	10.18	161.67	0.67	151.49
B.M. B.P.			2.82	152.85
T.P.	0.71	149.66	12.72	148.95
B.M. B.P.			8.61	141.05
T.P.	0.39	138.76	11.29	138.37
T.P.	5.93	135.71	8.98	129.78
B.M. B.P.			8.17	127.54
T.P. B.M. B.P.	4.23	135.02	4.92	130.79
- chK			4.68	130.34
B.M. B.P.			6.26	127.76
T.P.	5.09	127.61	12.50	122.52
B.M. B.P.			2.32	125.39
T.P.	11.59	138.73	0.47	127.14
chK			2.60	136.13

F.H. S.E.
40th ST
F.H. S.E.
Raven St
F.H. S.E.
41st ST
F.H. S.E.
Morrison
F.H. S.E.
42nd ST
F.H. S.E.
Toyne
F.H. S.E.
43rd
F.H. S.E.
Carlos
F.H. S.E. 44
Oncil on N
N.W. 45th
= Oncil
N.E. 44th
F.H. S.E.
chK 43rd
S.E. 43rd
N.E. Toyne
S.E. 42nd
S.W. 42nd
F.H. S.E.
Morrison
N.W. 41st
F.H. S.E.
Raven

138.73

T.P. B.M. B.P.	0.46	128.70	10.49	128.24
T.P.	11.82	140.22	0.30	128.40
chK B.M. B.P.			0.30	139.92 = 139.92

16
N.E. 40th ST
B.M. B.P. s. of Market
old Boundary

139.92 B.M. Boundary + s. of Market

8.34
148.26
6.64
141.58
0.29
141.87
12.54
129.33
- 0.01
129.32
13.19
116.13
7.77
123.90
11.63

122.27 = 122.27 B.M. B.P. N.W. 36th + Market

80' wide
20' els
10' 1/2"

45th ST. X Sec.
Market To Alma

4-9-31
Miller
Summersayer
Osborne.
N.W. 75th St
+ Market

10

169.77
40' N

19.03

B.M. B.P.	10.92	169.77	158.85		W.	9.9	159.9
00 = N. Line Market St.					+6.5 Bonita Pipe Line	13.03	156.74 Top. Pipe ✓
W.		10.7	159.1		ch	10.8	159.0
+7.5 W. Edge N. End. ent. Walk Ret.		10.52	159.25 ✓		"4	10.9	158.9
+12.5 E " " " "		10.55	159.22		±	11.0	158.8
20' N. End. ent. ch		10.65	159.12 ✓		"4	11.3	158.5
gutter N. end. Pavmt		11.30	158.47 ✓		ch	11.3	158.5
"4 " " "		10.92	158.85		E	11.5	158.3
± " " "		10.67	159.10		+10	11.6	158.2
"4 " " "		10.66	159.11				
gutter " " "		10.64	159.09 ✓		-10	11.7	158.1
N. end. ent. ch		10.12	159.65 ✓		E	10.8	159.0
+7.5 W. edge N. End. ent. Walk		10.05	159.72 ✓		ch	10.8	159.0
+12.5 E " " " " "		9.98	159.79		"4	11.2	158.6
E		10.0	159.8		±	11.2	158.6
					"4	10.9	158.9
					ch	10.5	159.3
-10		12.1	157.7		W.	10.8	159.0
E		11.4	158.2				
ch		10.3	159.5				
"4		10.5	159.3		W	10.1	159.7
±		10.7	159.1		ch	9.9	159.9
"4		11.0	158.8		"4	10.6	159.2
ch		11.0	158.8		±	10.8	159.0
+5		10.1	159.7		"4	10.7	159.1
W.		10.5	159.3		ch	11.1	158.7
					E	12.0	157.8
					+10	12.0	157.8

Plotted 5-4-31

4' N

65' N.

100' N.

47

Lot: 26, H.P.

Hill Top

1324.72

664.14

Lot: 27, H.P.

1328.24

Drive

Set L.P.&T 1933

48

(1603.82
W.L. in Mar Park)

1325.45
Men
36.150
Pipe

Lead & Ct.

662.95

Market

39.15

662.95

150' x 40' x 20'

30' x 20'

20' x 30'

Men

1927.47

Men

30.00

10.28 + 63.72

30.00

30.00

50

50

270.96

50

270.96

30

60

270.96

30

60

60

270.96

30

60

270.96

30

60

270.96

30

60

270.96

30

60

57

270.96

30

50

50

270.96

30

60

270.96

30

60

270.96

30

60

270.96

30

60

270.96

30

60

270.96

30

60

270.96

30

60

270.96

30

60

R

Lot: 32, H.P.

Lot: 31, H.P.

459.94

1329.08 ST.

Hub

Hub

Hub

Hub

20' x 20' x 20'

18.70

10.10

625.31

20

20

20

10

10

10

10

10

10

10

10

10

10

10

10

10

47 ft

Fairmont

Ave

Expansion

57

270.96

30

60

270.96

30

60

270.96

30

60

270.96

30

60

270.96

30

60

Set L.P.&T 1933

Lot: 33, H.P.

1323.16

ST.

60'

60'

44'

60'

60'

60'

60'

60'

60'

60'

60'

60'

60'

60'

60'

60'

60'

60'

60'

vacated.

F. ST.

30.00

30.00

30.00

600.00

600.00

600.00

600.00

600.00

600.00

600.00

600.00

600.00

600.00

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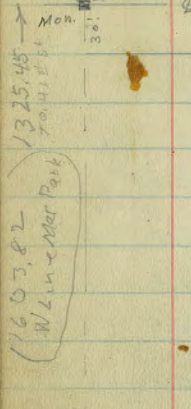
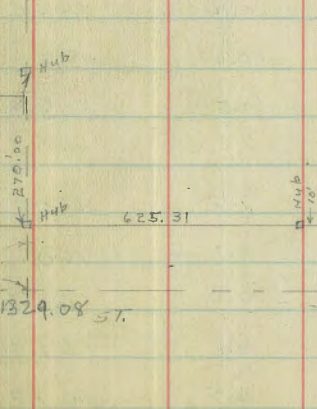
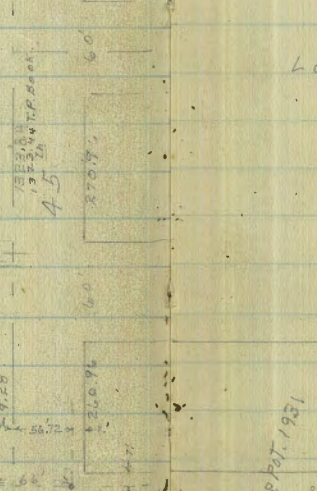
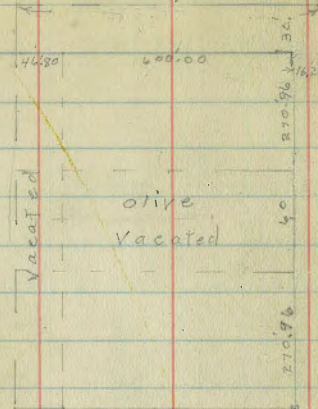
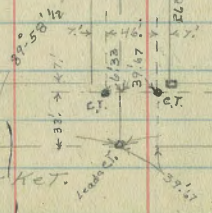
600.00

600.00

1927.47
H.P. Patent
45

Set L.P.&T 1931

Set L.P.&T 1933



	169.77		
	130'N		
-10	11.2	158.6	
E	11.2	158.6	
dr	10.8	159.0	
"4	9.8	160.0	
+	8.8	161.0	
"4	8.4	161.4	
dr	8.3	161.5	
W	9.4	160.4	

	150'N		
W	9.7	160.1	
dr	8.8	161.0	
"4	9.2	160.6	
+	9.6	160.2	
"4	9.9	159.9	
dr	10.2	159.6	
E	10.6	159.2	
+10	10.5	159.3	

	175'N		
-10	9.6	160.2	
E	9.7	160.1	
dr	8.4	161.4	
"4	8.1	161.7	
+	8.5	161.3	
"4	8.7	161.1	
dr	8.4	161.4	
W	8.8	161.0	

	169.77	45' ST
	200'N	19
W	8.4	161.4
dr	6.6	163.2
"4	7.5	162.3
+	8.4	161.4
"4	8.4	161.4
dr	8.4	161.4
+	8.8	161.0
+10	8.9	160.9

	230'N	
E	8.1	161.7
dr	7.8	162.0
"4	7.4	162.0
+	7.5	162.3
"4	7.2	162.6
dr	7.4	162.4
W	7.9	161.9

	240.96N. = S. line Alma St	60' wide 10' plus 10' ins.
W	7.3	162.5
dr	6.9	162.9
"4	7.7	162.1
+	7.7	162.1
"4	7.6	162.2
dr	7.2	162.6
E	7.1	162.7

169.77

S. db

E	6.2	1636
db	7.0	162.8
1/4	7.3	162.5
±	7.3	162.5
1/4	7.5	162.3
db	7.1	162.7
W	7.6	162.2
	5.1/4	
W	7.2	162.6
db	6.8	163.0
1/4	7.1	162.7
±	7.1	162.7
1/4	7.0	162.8
db	6.6	163.2
E	5.7	164.1
	±	
E	6.0	163.8
db	6.3	163.5
1/4	6.8	163.0
±	6.8	163.0
1/4	7.0	162.8
db	6.6	163.2
W	6.9	162.9
	16.1/4	
W	6.7	163.1
db	6.3	163.5

169.77

45th ST

50

1/4	6.6	163.2
±	6.4	163.4
1/4	6.3	163.5
db	6.1	163.7
E	5.7	164.1
	N. db.	
E	5.5	164.3
db	5.8	164.0
1/4	6.0	163.8
±	5.9	163.9
1/4	6.3	163.5
db	6.0	163.8
W	6.2	163.6
	oo = N. line Alma	
W	5.8	164.0
db	5.9	163.9
1/4	5.8	164.0
±	5.7	164.1
1/4	5.5	164.3
db	5.4	164.4
E	5.1	164.3
	15' N	
E	4.8	165.0
db	5.1	164.7
1/4	5.1	164.7
±	4.9	164.9

		169.77	
15' N. (con)			
W. 1/4	5.3	164.5	E
cb	4.9	164.9	cb
W.	5.1	164.7	1/4
40' N			ϕ
W.	5.3	164.5	1/4
cb	4.5	165.3	cb
1/4	4.9	164.9	W
ϕ	4.7	165.1	
1/4	4.8	165.0	W
cb	4.2	165.6	cb
E	3.0	166.8	1/4
65' N			ϕ
E	2.7	167.1	1/4
cb	3.5	166.3	cb
1/4	4.2	165.6	E
ϕ	4.4	165.4	
1/4	4.3	165.5	E
cb	3.8	166.0	cb.
W	5.2	164.6	1/4
100' N.			ϕ
W	4.0	165.8	1/4
cb	2.6	167.2	cb
1/4	3.1	166.7	+12.7 Air Valve on Pipeline
ϕ	3.2	166.6	+12.7 " " " " "
1/4	2.7	167.1	+10.
cb	2.5	167.3	W
E	1.7	168.1	

		169.77	45 th St
130' N.			51
	0.9	168.9	2.7
	1.3	168.5	2.3
	1.6	168.2	
	2.1	167.7	
	2.7	167.1	
	2.9	166.9	
	4.4	165.4	
140' N			
	3.3	166.5	
	2.9	166.9	
	2.5	167.3	
	2.2	167.6	
	1.9	167.9	
	1.8	168.0	
	1.5	168.3	
175' N.			
	1.8	168.0	
	1.2	168.6	
	1.2	168.6	
	1.9	167.9	
	2.6	167.2	
	3.0	166.8	
	0.6	169.2 Top of Valve	
	4.93	164.84 Top of Pipe	
	2.3	166.5	
	3.1	166.7	

169.77

185' N.

W	3.0	166.8
+10	2.4	167.4
cb	3.2	166.6
114	2.7	167.1
⊕	2.3	167.5
114	1.4	168.4
cb	1.6	168.2
E	2.1	167.7

200' N

E	2.6	167.2
cb	2.9	166.9
114	2.9	166.9
⊕	3.1	166.7
114	3.2	166.6
cb	3.5	166.3
+10	2.7	167.1
W.	3.5	166.3

235' N.

W.	4.9	164.9
+10	4.3	165.5
cb	5.1	164.7
114	4.9	164.9
⊕	5.0	164.8
114	4.8	165.0
cb	4.5	165.3
E	3.8	166.0

169.77

270.9' N. = S. Line (Pearl) F. St. { 60' wide
10' el's
10' 114's.

45' ST

52

E.	5.9	163.9
cb	6.3	163.5
114	6.3	163.5
⊕	6.2	163.6
114	6.0	163.8
cb	6.1	163.7
+10	6.0	163.8
W	6.7	163.1

S. d.

W	7.3	162.5
+10	6.5	163.3
cb	6.5	163.3
114	6.4	163.4
⊕	6.3	163.5
114	6.7	163.1
cb	6.8	163.0
E.	6.4	163.4

S. 114

E	6.6	163.2
cb	7.2	162.6
114	6.9	162.9
⊕	6.6	163.2
114	7.1	162.7
cb	6.2	163.6
W.	7.4	162.4
T.R	211	165.20
	6.68	163.09

165.20

E (Pearl) F. ST

W.	2.7	162.5
cl.	2.6	162.6
"4	3.1	162.7
Φ	2.7	162.5
"4	2.8	162.4
cl	2.8	162.4
E	2.3	162.9
N. "4		
E	3.0	162.2
cl	3.2	162.0
"4	3.6	161.6
Φ	3.5	161.7
"4	3.7	161.5
cl	3.0	162.2
W	3.5	161.7
N. cl		
W	3.5	161.7
cl	3.5	161.7
"4	4.0	161.2
Φ	4.1	161.1
"4	4.0	161.2
cl	3.9	161.3
E	3.7	161.5

165.20

0+00 = N. Line (Pearl) F. ST.

45' ST

53

E.	4.2	161.0
cl	4.3	160.9
"4	4.4	160.8
Φ	4.4	160.8
"4	4.3	160.9
cl	3.7	161.5
+10	2.9	162.3
W.	3.5	161.7
40' N		
W	6.0	159.2
+10	5.1	160.1
cl	5.7	159.5
"4	5.8	159.4
Φ	5.8	159.4
"4	5.5	159.7
cl	5.2	160.0
E	5.0	160.2
E+50	3.5	161.7
60' N on E } Culvert Location 70' N on W }		
E-50	3.5	161.7
E	4.8	160.4 ✓
+25	5.6	159.6
+40	5.0	160.2 ✓
+60	6.2	159.0
+80 = W.	7.0	158.2 ✓
+50.	8.0	157.2
+100.	9.3	155.9

165.20
70' N

e		4.7	160.5
cb	+80 12	5.8	159.4
+5	157.7 Fl W 12	5.9	159.3
1/4	.5 N	5.4	159.8
2	1.0 or less 1/4 high	5.0	160.2
1/4		5.6	159.6
cb		6.3	158.9
+13. Top of Pipe Line		8.8	156.4
W		7.0	158.2
+10		7.1	158.1
	100' N		
-10		7.4	157.8
W		6.9	158.3
+10		5.4	159.8
cb		5.8	159.4
1/4		6.2	159.0
2		6.1	159.1
1/4		5.2	160.0
cb		4.8	160.4
e		4.4	160.8
	135' N		
e		2.9	162.3
cb		4.0	161.2
1/4		4.6	160.6
2		5.1	160.1
1/4		5.5	159.7
cb		5.9	160.0

165.20

45 54

54

+10		4.4	160.8
W		5.9	159.3
+10		6.6	158.6
	170' N		
-10		6.0	159.2
W		6.0	159.2
cb		4.5	160.7
1/4		3.6	161.6
2		2.7	162.5
1/4		3.1	162.1
cb		3.0	162.2
e		2.2	163.0
	200' N		
e		1.2	164.0
cb		1.2	164.0
1/4		2.2	163.0
2		3.2	162.0
1/4		3.9	161.3
cb		3.9	161.3
W		5.0	160.2
+10		5.0	160.2
	235' N		
W		4.0	161.2
+10		2.5	162.7
cb		3.0	162.2
1/4		3.1	162.1

165.20

235' N (con)

♀	2.5	162.7
3/4	2.0	163.2
ch	1.5	163.7
ε	0.7	164.5

260' N.

ε	0.6	164.6
ch.	0.0	165.2
1/4	0.1	165.1
♀	0.9	164.3
1/4	2.4	162.8
ch	2.1	163.1
+10	1.6	163.6
W.	2.6	162.6

T.P. 9.32 172.31 2.21 162.99

270' 96' N = S. line Olive. (closed)

W.	9.5	162.8
+10	8.4	163.9
ch	9.3	163.0
1/4	9.3	163.0
♀	8.3	164.0
1/4	7.2	165.1
ch	7.2	165.1
ε	7.6	164.7

30' N. = ♀

ε	6.7	165.6
ch	7.6	164.7

172.31

45th st.

55

1/4	7.9	164.4
♀	8.0	164.3
1/4	8.4	163.9
ch	8.3	164.0
+10	8.0	164.3
W.	8.6	163.7

60' N. of S. line = N. line Olive (closed)

W	7.6	164.7
+10	6.7	165.6
ch	6.6	165.7
1/4	6.4	165.9
♀	5.7	166.6
1/4	5.8	166.5
ch	5.2	167.1
ε	4.3	168.0

25' N.

ε	4.9	167.4
ch	5.5	166.8
1/4	5.6	166.7
♀	5.4	166.7
1/4	4.0	166.3
ch	5.7	166.6
+10	5.3	167.0
W.	6.8	165.5

172.31
50' N

W	6.6	165.7
+10	5.5	166.8
cl	5.8	166.5
"4	5.6	166.7
±	5.1	167.2
"4	5.2	167.1
cl	5.1	167.2
ε	4.1	168.2

75' N

ε	3.8	168.5
cl	4.5	167.8
"4	4.1	168.2
±	4.1	168.2
"4	4.8	167.5
cl	5.6	166.7
+10	5.4	166.9
W.	4.0	166.3

89.5' N.

Bypass Valve 4' E. of W. line 6" Valve cover.	6.5	165.8 Top of cover
13.22 " " " = M.H. Cover. over Valve	6.67	166.64 Top of M.H.
11.58 " " " = Valve stem	8.05	164.26 Top of stem

100' N.

W.	5.7	166.6
cl	4.8	167.5
"4	5.4	166.9
±	5.2	167.1

172.31

45' ST.

56

"4	4.7	167.6
cl	4.4	167.9
ε	2.9	169.4

130' N.

ε	2.3	170.0
cl	3.9	168.4
"4	4.4	167.9
±	4.8	167.5
"4	5.3	167.0
cl	5.3	167.0
+10	4.8	167.5
W.	6.4	165.9

164' N.

W.	7.0	165.3
+5.9 Air Valve	4.22	168.09 Top of Air Valve
+5.9 φ Bonita Pipeline	8.02	164.29 Top of Pipe
+10	5.3	167.0
cl	5.5	166.8
"4	5.0	167.3
±	3.4	168.9
"4	2.2	170.1
cl	2.4	169.9
ε	2.3	170.0

271
164
1.07

172.31
180' N.

E	2.2	170.1
cl	3.2	169.0
1/4	3.7	168.6
1/2	4.4	167.9
3/4	5.5	166.8
cl	5.5	166.8
+10	5.0	166.3
W.	6.9	165.4

200' N

W	7.6	164.7
+10	6.1	166.2
cl	5.6	166.7
1/4	5.0	167.3
1/2	4.2	168.1
3/4	4.2	168.1
cl	2.8	169.5
E	1.7	170.6

220' N

E	2.6	169.7
cl	3.4	168.9
1/4	4.3	168.0
1/2	5.1	167.2
3/4	6.1	166.2
cl	6.3	166.0
+10	6.7	165.6
W.	8.0	164.3

172.31
235' N

W	8.0	164.3
cl	5.0	167.3
1/4	5.7	166.6
1/2	5.2	167.1
3/4	3.7	168.6
cl	2.1	170.2
E	1.1	171.2

255' N.

E	1.5	170.8
cl	3.7	168.6
1/4	4.9	167.4
1/2	5.7	166.6
3/4	6.4	165.9
cl	6.3	166.0
+10	6.6	165.7
W.	7.9	164.4

270.96 N. = S. Line Hill Top Drive

W.	8.3	164.0
+10	7.0	165.3
cl	7.3	165.0
1/4	7.3	165.0
1/2	6.3	166.0
3/4	5.7	166.6
cl	4.4	167.5
E	3.5	168.8

chk B.M. Nails in fence Post

6.44 165.87 = 165.86

W. Line Hill Top
6' E. of lot line

45th St

57

60' wide
10' elevs
10' 1/4

Hilltop Drive X Sec 44th St to 46th St

BM. Nails in post 2.41 168.68

N Line - Hilltop
165.87 6' E. of Pt.

46.8' W. of E. line 44th St = ctr. Lot 33.

S.	1.6	167.1
cl	1.4	167.3
1/4	1.3	167.4
+	2.1	167.7
1/2	2.0	166.7
1/4	1.8	166.9
d	1.4	167.3
+2.5 = wire fence Catholic cemetery	1.1	167.6
N	1.1	167.6

00 = E. Line 44th St

N	3.7	165.0
cl	4.1	164.6
1/4	4.4	164.1
+	4.4	164.3
1/4	5.1	163.6
d	5.3	163.4
S.	6.1	162.6
+5	6.3	162.4

30' E.

-5	7.9	160.8
S	7.4	161.1
cl	7.0	161.7
1/4	6.3	161.4
+	5.9	162.8

Plotted - 5-4-91

168.68

✓

1/4	5.9	162.8
cl	5.5	163.2
N	5.0	163.7
	60' E	
N	6.3	162.4
cl	6.7	162.0
1/4	6.8	161.9
+	7.2	161.5
1/4	7.6	161.1
cl	8.5	160.2
S	10.2	158.5
+10	10.3	158.4
	100' E	
-50	15.6	153.1
-30	13.8	154.9
S	10.9	157.8
cl	8.3	160.4
1/4	7.2	161.5
+	7.2	161.5
1/4	7.3	161.4
cl	7.1	161.6
N	6.6	162.1

58

168.68
145'E

N	6.9	161.8
el	7.4	161.3
"4	7.5	161.2
el	7.7	161.0
"4	7.8	160.9
el	8.3	160.4
S	10.0	158.7
+10	10.0	158.7

190'E

-5	7.2	161.5
S	7.2	161.5
el	7.4	161.3
"4	7.8	160.9
el	7.7	161.0
"4	7.5	161.2
el	7.3	161.4
N	6.9	161.9

210'E

N	6.4	162.3
el	6.4	162.3
"4	7.3	161.4
el	7.5	161.2
"4	7.4	161.3
el	7.3	161.4
S	7.9	160.8
+5	8.0	160.7

168.68
250'E

S	6.6	162.1
el	5.5	163.2
"4	5.4	163.3
+2	6.2	162.5
el	6.2	162.5
"4	6.1	162.6
el	5.1	163.6
N	5.3	163.4

300'E

N	4.5	164.2
el	4.5	164.2
"4	5.5	163.2
el	6.0	162.7
"4	6.0	162.7
el	5.8	162.9
S	6.3	162.4

320'E

S	5.4	163.3
el	5.6	163.1
"4	6.1	162.6
el	6.2	162.5
"4	5.7	163.0
el	5.1	163.6
N	4.5	164.2

Hill Top Dr

59

168.68

345'E

N	5.0	1637
cl	5.6	1631
114	4.2	1625
cl	6.6	1621
114	6.6	1621
cl	6.2	1625
S	6.3	1624

370'E

S	8.4	1603
cl	6.6	1621
114	7.3	1614
cl	7.3	1614
114	7.2	1615
cl	6.7	1620
N	5.8	1629

378'E

3' S. of N. line = S.W. cor. Tool house

5' S. " " = Wire Fence

390'E

2.7 S. of N. line = S.E. cor. Tool House

5' S. of N. line = Wire Fence.

400'E

N	8.3	1604
cl	8.8	1599
114	9.2	1595
cl	9.4	1593
	10.2	

168.68

Hilltop Dr.

60

114	10.4	1583
cl	11.1	1576
S	12.3	1564
+50'	15.6	1531

420'E

-50	14.8	1539
-35	15.4	1533
S	14.5	1542
cl	13.5	1552
114	13.2	1555
cl	11.1	1576
114	10.6	1581
cl	10.2	1585
N	9.2	1595
+5	9.0	1597

445'E

-5	9.8	1589
N	10.2	1587
cl	11.2	1575
114	11.4	1573
cl	11.8	1569
114	12.8	1559
cl	13.1	1556
S	13.6	1551
+30	13.8	1549
+50	13.2	1555

168.68

475' E

-10	11.5	157.2
S	11.8	156.9
cl	11.6	157.1
1/4	11.8	156.9
⊕	11.8	156.9
1/4	11.8	156.9
cl	11.7	157.0
N	10.6	158.1
+20	10.0	158.7

510' N.

-20	9.7	159.0
N.	10.5	158.2
cl	11.6	157.1
1/4	10.8	157.9
⊕	11.1	157.6
1/4	11.0	157.7
cl.	8.2	160.5
S.	8.2	160.5

535' E

S	7.8	160.9
cl.	8.8	159.9
1/4	10.0	158.7
⊕	10.3	158.4
1/4	10.3	158.4
cl.	11.0	157.7
N	9.6	159.1

168.68

Hilltop Dr

61

+20	9.1	159.6
	580' E.	
-20	8.6	160.1
N	8.7	160.0
cl	9.7	159.0
1/4	8.4	160.3
⊕	8.5	160.2
1/4	7.1	161.6
cl	5.6	163.1
S.	4.7	164.0

600' E = W. Line 45' S.

80' wide
20' cl's
10' 1/4's

S	4.7	164.0
cl	5.6	163.1
1/4	6.2	162.5
⊕	7.3	161.4
1/4	7.3	161.4
cl	7.4	161.3
N	8.7	160.0
+50	8.3	159.4

W. cl.

-50	7.0	161.7
-20	7.2	161.5
N.	5.3	163.4
cl.	4.5	164.2
1/4	5.2	163.5
⊕	5.2	163.5

168.68

W. el. con

S. 1/4	4.6	164.1
cl	4.4	164.3
S	3.7	165.0
W. 1/4		
S	3.7	165.0
cl	4.0	164.7
1/4	3.7	165.0
cl	4.1	164.6
1/4	4.4	164.3
cl	3.3	165.4
N	4.1	164.6
+10	5.4	163.3

T.P.	13.31	181.89	0.10	168.58
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cl 45th

N	17.6	164.3
cl	16.6	165.3
1/4	16.7	165.2
cl	16.5	165.4
1/4	16.2	165.7
cl	16.4	165.5
S	15.9	166.0
E. 1/4		
S	15.3	166.6
cl	15.5	166.4
1/4	15.4	166.3
cl	15.8	166.1

181.89

Hilltop Dr.

62

1/4	16.4	165.5
cl	16.1	165.8
1/4	17.0	164.9

E. cl.

N	16.5	165.4
cl	15.6	166.3
1/4	15.3	166.6
cl	15.3	166.6
1/4	15.0	166.9
cl	15.0	166.9
S	14.4	167.5

00 = E. line 45th st.

S	13.1	168.8
cl	13.5	168.4
1/4	13.8	168.1
cl	14.1	167.8
1/4	14.4	167.5
cl	14.6	167.3
N	14.8	167.1

40' E

N	12.4	169.5
cl	12.1	169.8
1/4	11.8	170.1
cl	11.8	170.1
1/4	11.4	170.5
cl	10.8	171.1
S	10.5	171.4

181.89
70'E.

S	8.5	173.4
cl	8.1	173.8
114	9.0	172.9
cl	9.4	172.5
114	9.3	172.6
cl	10.3	171.6
N	10.3	171.6

100'E.

N	9.2	172.7
cl	8.8	173.1
114	8.2	173.7
cl	7.9	174.0
114	7.9	174.0
cl	7.9	174.0
S	8.1	173.8

135'E

S	5.9	176.0
cl	6.2	175.7
114	6.5	175.4
cl	6.2	175.7
114	5.3	176.6
+5	4.8	177.1
cl	5.8	175.1
N	6.8	175.1

181.89
170'E

N	4.7	177.2
cl	5.6	176.3
114	5.7	176.2
cl	5.4	176.5
114	5.5	176.4
cl	4.9	177.0
S	4.6	177.3

200'E.

S	3.5	177.4
cl	4.0	177.9
+3	4.3	177.6
114	4.8	177.1
cl	4.9	177.0
114	5.3	176.6
cl	5.5	176.4
N	5.6	176.3

225'E.

N	5.4	176.5
cl	5.2	176.7
114	4.6	177.3
cl	4.4	177.5
114	4.2	177.7
+7	3.8	178.1
cl	3.0	178.9
S	2.3	179.6

Hilltop Dr

63

181.89

255' E.

S	2.5	179.4
cb	3.0	178.9
"4	4.2	177.7
♀	4.4	177.5
"4	4.9	177.0
cb	5.2	176.7
N	4.8	177.1

285

N	4.7	177.2
cb	4.9	177.0
"4	4.0	177.9
♀	3.4	178.5
"4	3.5	178.4
cb	3.3	178.6
S	3.0	178.9

310' E.

S	2.9	179.0
cb	3.4	178.5
"4	3.5	178.4
♀	3.6	178.3
"4	4.1	177.8
cb	4.6	177.3
N	4.7	177.2

330' E.

N	2.9	179.0
cb	2.4	179.5

181.89

H. Hilltop Dr.

64

"4	3.0	178.9
♀	3.6	178.3
"4	3.6	178.3
cb	3.0	178.9
S	2.6	179.3

350' E.

S	2.2	179.7
cb	2.5	179.4
"4	3.5	178.4
♀	3.6	178.3
"4	3.8	178.1
cb	3.9	178.0
N	4.3	177.6

370' E.

N	2.2	179.7
cb	3.2	178.7
"4	3.6	178.3
♀	3.4	178.5
"4	3.2	178.7
cb	2.1	179.8
S	1.8	180.1

400' E.

S	1.7	180.2
cb	2.3	179.6
"4	3.1	178.8
♀	2.9	179.0

181.89

400'.E. (con)

N	114	2.6	179.3	cl
cl		3.6	178.3	S
N		4.1	177.8	
T.P.	6.70	185.61	2.98	178.91

440'.E

N		7.4	178.0	+3
cl		7.1	178.5	14
114		6.6	179.0	cl
cl		6.3	179.3	14
114		6.3	179.3	cl
cl		5.6	180.0	N
S		5.2	180.4	

460'.E

S		4.6	181.0	N
cl		5.3	180.3	cl
114		6.0	179.6	14
cl		6.0	179.6	cl
114		5.8	179.8	+7
cl		5.4	180.2	cl
N		6.0	179.6	S

4.80'.E

N		7.0	178.6	
cl		6.6	179.0	
114		5.6	180.0	
cl		5.8	179.8	
114		5.7	179.9	

185.61

Hill Top Dr.

65

cl	5.3	180.3
S	4.2	181.4

500'.E

S	3.8	181.8
cl	4.6	181.0
+3	5.3	180.3
14	5.3	180.3
cl	5.5	180.1
14	5.4	180.2
cl	5.8	179.8
N	6.3	179.3

520'.E

N	4.3	181.3
cl	4.2	181.4
114	4.6	181.0
cl	5.0	180.6
114	4.8	180.8
+7	4.8	180.8
cl	3.6	182.0
S	2.9	182.7

185.61

535' E.

S	3.0	182.6
cl	3.8	181.8
+3	4.4	181.2
1/4	4.6	181.0
⊕	4.7	180.9
1/4	4.5	181.1
cl	5.0	180.6
N	5.0	180.6

570' E.

N	4.1	181.5
cl	4.2	181.4
1/4	3.9	181.7
⊕	3.7	181.9
1/4	3.7	181.9
cl	2.6	183.0
S	2.0	183.6

600' E.

S	1.5	184.1
cl	1.9	183.7
1/4	2.4	183.2
⊕	2.7	182.9
1/4	2.6	183.0
cl	2.9	182.7

+5' = E. end. Wire Fence Catholic cemetery.

N	2.7	182.9
---	-----	-------

T.P.	1.20	178.86	7.95	177.44
------	------	--------	------	--------

Chk BM Nails

12.99	165.87
-------	--------

45' Hill Top

Hill Top Dr.

66

60' wide
10' elev
10' 1/2

"F." St (Pearl) x Sec 45th to 44th St.

Φ

170.11

E. line 45th St

37

AM. S. W. BIKG. 7.02 170.11 163.09 F. 45th St

100' E. of E. line 45th

S	2.9	167.2
cl	3.4	166.7
1/4	3.6	166.5
1/2	3.5	166.6
3/4	3.7	166.4
cl	4.3	165.8
N.	5.3	164.8

60' E. of E. line 45th

N	7.5	162.6
cl	7.2	162.9
1/4	6.8	163.3
1/2	6.3	163.8
3/4	6.0	164.1
cl	5.4	164.7
S	4.5	165.6

30' E. of E. line 45th

S	5.5	164.6
cl	5.8	164.3
1/4	5.8	164.3
1/2	6.0	164.1
3/4	6.9	163.2
cl	7.9	162.2
N.	8.2	161.9

Plotted 5-5-31

N
cl
1/4
1/2
cl
S

100' W. line 45th St.

S
cl
1/4
1/2
cl
N.

26' W.

on E Pepper Tree 24" Diam

50' W.

N
cl
1/4
1/2
cl
S

9.0	161.1
8.6	161.5
8.0	162.1
7.1	163.0
6.9	163.2
6.7	163.4
6.3	163.8

7.0	163.1
7.6	162.5
8.0	162.1
7.6	162.5
8.5	161.6
8.4	161.7
8.4	161.7

9.7	160.4
8.9	161.2
8.5	161.6
7.5	162.6
7.4	162.7
7.1	163.0
6.5	163.6

170.11		
75' W		
1' N. of ♀ Pepper Tree	14" Diam.	
86' W		
10' N. of ♀ Pepper Tree	24" Diam.	
100' W		
S	6.7	1634
cl	7.4	1627
1/4	7.9	1622
♀	7.9	1622
1/4	9.1	1610
cl	9.7	1604
N	10.1	1600
150' W		
N.	11.3	1588
cl	10.9	1592
1/4	10.5	1596
♀	9.6	1605
1/4	9.2	1639
cl	8.4	1614
S	7.7	1624
200' W		
S	10.7	1594
cl	11.2	1589
1/4	11.3	1588
♀	11.0	1591
1/4	11.8	1583
cl	12.5	1576
N	12.9	1572

170.11			F. St.
250' W			68
N		14.3	1558
cl		13.6	1565
1/4		13.3	1568
♀		12.9	1572
1/4		13.3	1568
cl		12.9	1572
S.		12.7	1574
T.P.	0.42	157.35	13.18
			156.93
300' W			
S		2.2	1552
cl		2.6	1548
1/4		2.2	1552
♀		2.1	1563
1/4		2.9	1545
cl		3.0	1544
N		3.2	1542
330' W			
N		4.4	1530
cl		4.3	1531
1/4		4.2	1532
♀		3.7	1537
1/4		3.8	1536
cl		3.5	1539
S.		3.3	1541

157.35

370' W.

S	5.9	151.5
cb	6.1	151.3
"4	6.3	151.1
♀	6.4	151.0
"4	7.1	150.3
cb	7.2	150.2
N.	7.2	150.2

400' W.

N	7.5	149.9
cb	8.2	149.2
"4	7.9	149.5
♀	7.3	150.1
"4	7.2	150.2
cb	7.0	150.4
S.	7.2	150.2

425' W.

S	8.9	148.5
cb	9.3	148.1
"4	9.3	148.1
♀	9.2	148.2
"4	9.5	147.9
cb	9.6	147.8
N	9.4	148.0

440' W.

N	9.2	148.2
cb	10.0	147.4

157.35

F. ST.

39

"4	10.5	146.9
♀	9.8	147.6
"4	10.0	147.4
cb	9.9	147.5
S	9.5	147.9

465' W.

S	10.7	146.7
cb	10.7	146.7
"4	10.4	147.0
♀	9.8	147.6
"4	10.7	146.7
cb	10.6	146.8
N.	10.4	147.0

500' W.

N	9.9	147.5
cb	10.8	146.6
"4	11.2	146.2
♀	11.5	145.9
"4	11.6	145.8
cb	11.3	146.1
S	10.8	146.6

520' W.

S	12.0	145.4
cb	11.7	145.7
"4	11.1	146.3
♀	9.8	147.6

157.35

520' W (20th)

N	1/4	9.8	147.6
cl		9.9	147.5
N		9.8	147.6

540' W

N		8.6	148.8
cl		9.0	148.4
1/4		9.5	147.9
1/2		10.0	147.4
1/4		10.5	146.9
cl		10.7	146.7
S		11.4	146.0

565' W

S		12.2	145.2
cl		11.7	145.7
1/4		10.9	146.5
1/2		10.1	147.3
1/4		10.5	146.9
cl		10.2	147.2
N		9.8	147.6

600' W = 2. Line - 44th St.

N		10.0	147.4
cl		9.9	147.5
1/4		9.9	147.5
1/2		10.5	146.9
1/4		10.8	146.6
cl		11.1	146.3
S		12.0	145.4

157.35

*P.S. 2. Bk. Con.	7.07	152.38	12.04	145.31	44 th + F.
chk B.M. B.P.			11.33	141.05	N. 6. 44 th + Market

F. 51.

30

60' wide
10' chs
10' 1/4's.

(Alma) St X Sec. 44th To 45th

G

B.M. B.P. 9.95 168.80 158.85 N.W. 45th
+ Market

100' E. of E. Line 45th

S	2.3	166.5
ch	2.0	166.8
"4	1.8	167.0
±	1.9	166.9
"4	1.9	166.9
ch	1.2	167.6
N.	0.2	168.6

75' E. of E. Line 45th

N	2.3	166.5
ch	2.8	166.0
"4	3.2	165.6
±	3.4	165.4
"4	3.7	165.1
ch	3.4	165.4
S	2.7	166.1

45' E. of E. Line 45th

S	5.4	163.4
ch	4.9	163.9
"4	4.7	164.1
±	4.0	164.8
"4	3.0	165.8
ch	2.3	166.5
N	2.0	166.8

Ⓟ

N	4.2
ch	4.6
"4	4.7
±	5.0
"4	4.8
ch	5.3
S	6.1
S	6.4
ch	6.6
"4	6.2
±	5.8
"4	5.7
ch	5.3
N	4.8

100' W. Line 45th

50' W

N	6.6
ch	6.8
"4	7.0
±	7.2
"4	7.3
ch	7.5
S	7.7

168.80
E. Line 45th

71

168.80

90' W.

S	8.5	160.3
cl	8.4	160.4
"4	8.1	160.7
cl	7.7	161.1
"4	7.6	161.2
cl	7.6	161.2
N	7.6	161.2

105' W.

N	7.7	161.1
cl	7.4	161.4
"4	7.0	161.8
cl	7.2	161.6
"4	8.1	160.7
cl	8.6	160.2
S	8.4	160.4

125' W.

S	9.3	159.5
cl	9.0	159.8
"4	8.7	160.1
cl	8.4	160.4
"4	8.5	160.3
cl	8.5	160.3
N	8.2	160.6

145' W.

N	8.8	160.0
cl	9.0	159.8

168.80

145' W

"14	9.0	159.8
cl	8.3	160.5
"14	8.4	160.7
cl	8.6	160.2
S	9.6	159.2

185' W.

S	10.9	157.9
cl	10.6	158.2
"14	10.6	158.2
cl	9.7	159.1
"14	9.2	159.6
cl	9.3	159.5
N	9.8	159.0

T.P.	1.27	159.20	10.87	157.93
------	------	--------	-------	--------

205' W.

N	1.1	158.1
cl	0.9	158.3
"14	1.0	158.2
cl	1.0	158.2
"14	1.2	158.0
cl	1.2	158.0
S	1.1	158.1

225' W.

S	0.4	158.8
cl	0.6	158.6
"14	1.1	158.1

Alma

72

159.20

225' W. (con)

♀	1.2	158.0
1/4	1.4	157.8
cl	1.1	158.1
N	0.2	159.0

255' W.

N	1.6	157.6
cl	1.8	157.4
1/4	1.8	157.4
♀	1.8	157.4
1/4	1.7	157.5
cl	1.8	157.4
S	2.0	157.2

280' W.

S.	2.1	157.1
cl	1.3	157.9
1/4	0.9	158.3
♀	1.2	158.0
1/4	2.1	157.1
cl	2.2	157.0
N	2.5	156.7

300' W.

N	2.7	156.5
cl	2.7	156.5
1/4	2.7	156.5
♀	2.5	156.7
1/4	2.8	156.4

159.20

Alma

78

cl	3.0	156.2
S	3.2	156.0

325' W

S	3.9	155.3
cl	3.7	155.5
1/4	3.2	156.0
♀	2.4	156.8
1/4	2.2	157.0
cl	2.5	156.7
N.	2.8	156.4

355' W.

N	3.5	155.7
cl	3.9	155.3
1/4	3.9	155.3
♀	3.7	155.5
1/4	4.0	155.2
cl	4.1	155.1
S	4.3	154.9

375' W

S	3.5	155.7
cl	3.0	156.2
1/4	3.1	156.1
♀	3.5	155.7
1/4	4.0	155.2
cl	4.2	155.0
N.	4.2	155.0

159.20

400' W.

N.	4.0	155.2
cl	3.8	155.4
1/4	3.9	155.3
φ	4.0	155.2
1/4	4.4	154.8
cl	4.6	154.6
S	5.0	154.2

440' W.

S	4.0	155.2
cl	3.9	155.3
1/4	4.2	155.0
φ	3.6	155.6
1/4	3.5	155.7
cl	3.6	155.6
N	3.9	155.3

460' W.

N	4.4	154.8
cl	4.1	155.1
1/4	4.2	155.0
φ	4.1	155.1
1/4	4.8	154.4
cl	5.1	154.1
S	5.2	154.0

159.20

Alma

500' W

S.	6.6	152.6
cl	6.5	152.7
1/4	6.2	153.0
φ	5.5	153.7
1/4	5.9	153.3
cl	5.9	153.3
N	6.1	153.1

540' W

N	7.1	152.1
cl	7.0	152.2
1/4	7.1	152.1
φ	7.2	152.0
1/4	7.9	151.3
cl	8.3	150.9
S	8.6	150.6

555' W

S	9.2	150.0
cl	8.7	150.5
1/4	7.8	151.4
φ	7.0	152.2
1/4	7.2	152.0
cl	7.4	151.8
N	7.6	151.6

159.20

580' W.

N	9.0	1502
d	9.3	149.9
'4	9.6	149.6
4	9.5	149.7
'4	10.0	149.2
d	10.3	148.9
S	10.4	148.8

600' W = E. Line 44th St

S	11.5	147.7
d	11.3	147.9
'4	10.8	148.4
4	10.1	149.1
'4	10.2	149.0
d	9.8	149.4
N	9.3	149.9

T.P 1.47 149.15 11.52 147.68

24K B.M. B.P.

8.10 141.05 = 141.05 + Market

N.E. 44th

Survey for proposed STORM DRAIN between
Jackdaw + Reynard way N of Brookes

Levels p 77

5+08.00 = INT. of Ely of Jackdaw St. ^{Cross-}edge sidewalk

4+76.4 outlet 30" Corr iron pipe

4+16.7 Sewer lat.

3+98.00 = A 37°00' RT Stub

3+09.5 Sewer lat.

2+62.5 " "

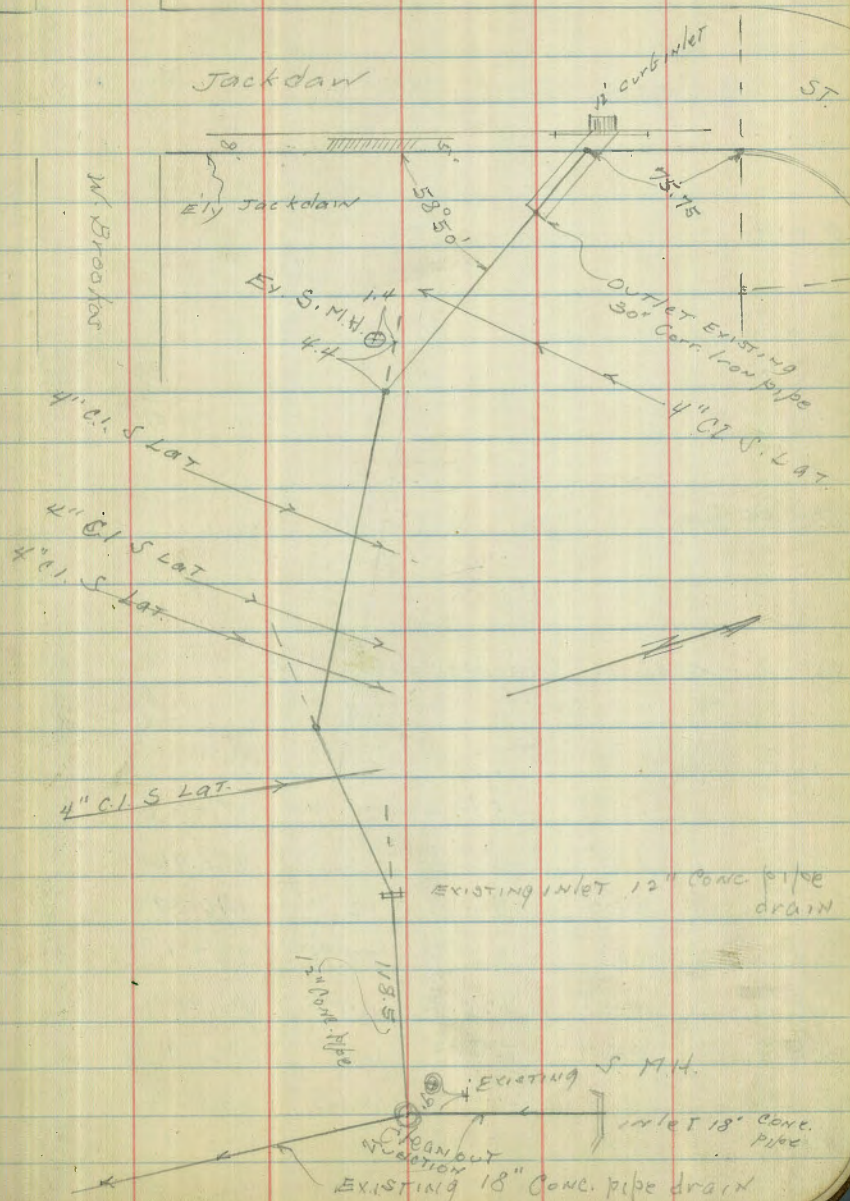
2+31.5 " "

1+70 = A = 10°45' RT. Stub

1+24 Sewer lat.

0+00 = inlet 12" Conc. pipe drain A = 7°15' LT.

JUNCTION BOX of existing drain. Top 13' above ground



Levels for proposed Drain see sketch p 76

0+50

95
174.6

$\frac{13.2}{3}$ wash
170.86

0+40

13.7 bot. wash
170.4

0+15

15.4 " "
168.7

0+05

14.5
169.6

$\frac{14.4}{2}$ bot. wash
167.7

0+00 = inlet 12" Conc. pipe drain Elev.

$\frac{16.2}{2}$
167.44

TP	11.83	184.06	12.92	172.23
TP	1.19	185.15	12.67	183.96
TP	0.44	196.63	12.74	196.19
TP	1.03	208.93	12.95	207.90
TP	0.38	220.85	12.56	220.47
TP	0.24	233.03	12.75	232.79
TP	0.18	245.54	12.65	245.36
NESP	1.02	258.01		256.99

Butter
Goldfinch

184.06

LT.

~~LT.~~

RT.

8

1+50

14.4
176.3

1+30

wash $\frac{15.7}{4}$ 12.4
174.8 178.3

1+24 4' CI S Lot

9.51 Top pipe
181.0

1+10

wash $\frac{16.6}{3}$ 13.9
173.7 176.6

1+00

16.5
173.7

T.P. 12.23 190.49 5.80 178.26

190.49

Note: RT. of 0+75 existing sewer is
0+75 exposed and in danger of washing out8.7 11.7 bot wash
176.4 172.4

0+60

12.5
171.6

184.06

184.06

2+62.5 CI pipe

2+40

2+31.5 4" CI pipe

T.P. 12.90 203.12 0.27 190.22

2+20

2+13

2+00

1+85

1+70 = A

190.49

LT

E

RT

79

12.7
190.4

98 Top pipe
193.31

130
190.1

15.8
7 wash

11.86 Top 4" CI pipe
191.2

203.12
2
101.56

2.0
188.5
5.4
8 wash

6.3 wash
184.2

7.0 wash
183.5

9.3
181.2

10.1
180.4

190.49
3

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1% to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table is same row and column gives distance from side stake to slope stake. If ground is not level, the side stake and slope stake, lower larger by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point and line of sight should cut target.

IMPROVED TABLES AND INFORMATION

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given L may be found by dividing tangent (or external) opposite L by given tangent (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

check to NWAP	Jackdaw brook		226	247.53	247.53
" "	FL Box 4 30" pipe		9.35	240.44	240.00
" "	iron grating		6.63	243.16	
5+16.5	Top cb r/c		5.16	244.63	
5+08.00	EL Jackdaw		5.08	244.71	Top Cen Work
T.P.	11.40	249.79	0.07	238.39	
4+87	Top 30" pipe + ground		4.7	233.76	
T.P.	11.97	238.46	0.88	226.49	
4+70.4	FL outlet 30" Cor. 1.5'		+0.40	227.77	
4+76.4			6.3	221.07	
T.P.	12.09	227.37	0.45	214.78	
4+67	Wash		0.2	215.0	
4+40	Wash		4.8	210.4	
4+16.7	4" CIP pipe		7.45	207.78	Top
4+02	3.3' LT SMH		5.7	210.06	10.17 FL 205.06
3+98.20	Δ		6.97	208.26	
3+90	Wash		9.4	206.0	
3+50	Wash		12.1	203.1	
T.P.	12.65	215.23	0.54	202.58	
3+25			3.1	200.0	Wash
3+09.5	4" CIP pipe		4.72	198.4	
3+00			3.0	200.1	
2+90			9.1	194.0	

203.12

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

52
1040
20
208,00

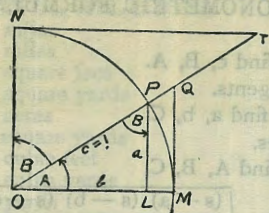


TABLE II
TRIGONOMETRIC FORMULÆ.

$$\begin{aligned} \angle A &= \angle MOP & \angle B &= \angle PON = \angle OPL \\ R &= OB = c = 1 \\ \sin A &= \frac{a}{c} = \frac{a}{1} = a = \cos B = LP \\ \cos A &= \frac{b}{c} = \frac{b}{1} = b = \sin B = OL \\ \tan A &= \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ \\ \cot A &= \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT \\ \sec A &= \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ \\ \csc A &= \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT \\ \text{vers } A &= \frac{LM}{OP} = LM = \text{covers } B \\ \text{covers } A &= \frac{OP - LP}{OP} = OP - LP = \text{vers } B \\ \text{exsec } A &= PQ = \text{coexsec } B \\ \text{coexsec } A &= PT = \text{exsec } B \\ \sin \frac{1}{2} A &= \sqrt{\frac{1 - \cos A}{2}} & \cos \frac{1}{2} A &= \sqrt{\frac{1 + \cos A}{2}} \\ \sin 2A &= 2 \sin A \cos A & \cos 2A &= \cos^2 A - \sin^2 A \\ \text{Law of Sines} & \frac{\sin A}{a} = \frac{\sin B}{b} = \frac{\sin C}{c} \\ \text{Law of Cosines} & c^2 = a^2 + b^2 - 2ab \cos C \\ \text{Law of Tangents} & \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)} \end{aligned}$$

1910 6.94 2460 = 1170

1259
297
134
16.83

2470 1261

ENGINEERING DEPARTMENT,
CITY OF SAN DIEGO,
CALIFORNIA.

86
47
38
32
90
14142
287807
121121
1697057

2671
968
703

40
163
23.7

24967
21107
414

251
271
592

1178
38
958
24166
628
24794-x
521
24253
24794
246
24548

149.2
51.1

177
133.1
1708

Rosecrans & Carleton
SW BP 14.53

218.8
26.5
47.7
95.4

Dickens SW Mon 7'
9.92

143.1
190.6
238.5
256.2

2340

2(1325.96
662.95

12.50
40
35
1825

403.22
845
2414
1272.34
54
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403.22
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