

1397

Calhoun Park
ROADS

ROADS

FED. BUREAU OF

NO. 335F

MICROFILMED

Dec 1964

Our Leather Bound Engineers Note Books are carried in the following rulings:

- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
- No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.
- No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.
- No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

We also carry the Note Books listed above, bound in extra strong Fabri-Hide (otherwise the same quality of book), which can be furnished at a somewhat lower price.

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THE FREDERICK POST CO.
ENGINEERING and DRAFTING SUPPLIES
IRVING PARK STATION
CHICAGO, ILL.

X POWDER HOUSE CANYON ROAD
Oct 29-30 By Loudon.
FROM-Florida St. to Pershing Drive 1 to 31

PERSHING DRIVE along pavement 50 to 63

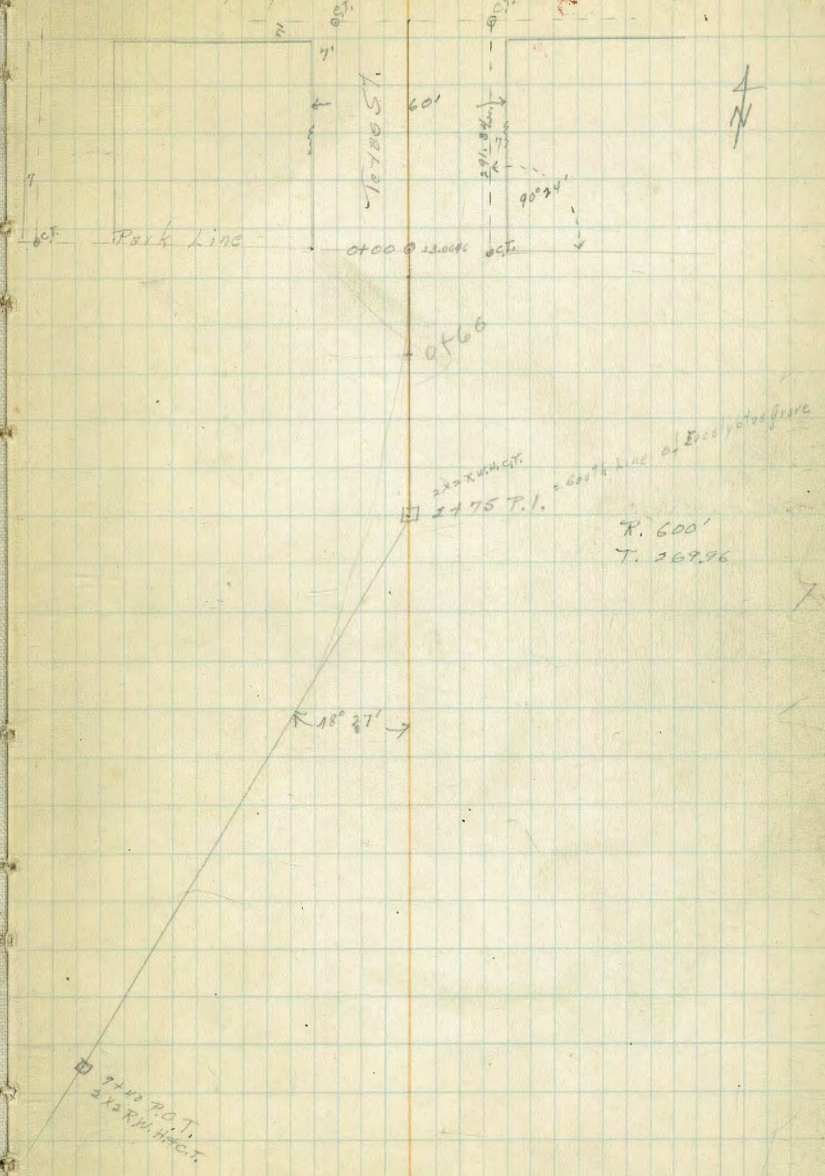
5/16/30
T. Wood
W. Rice
K. Auner.

Powder House Cañon Road
Texas St. Line, From P.I. of Northline
of Balboa Park to Junction with
Powder House Cañon Rd, Florida St. Line @
Sta. 18+55. Length, 24+04.61

540
225

Myrtle Ave

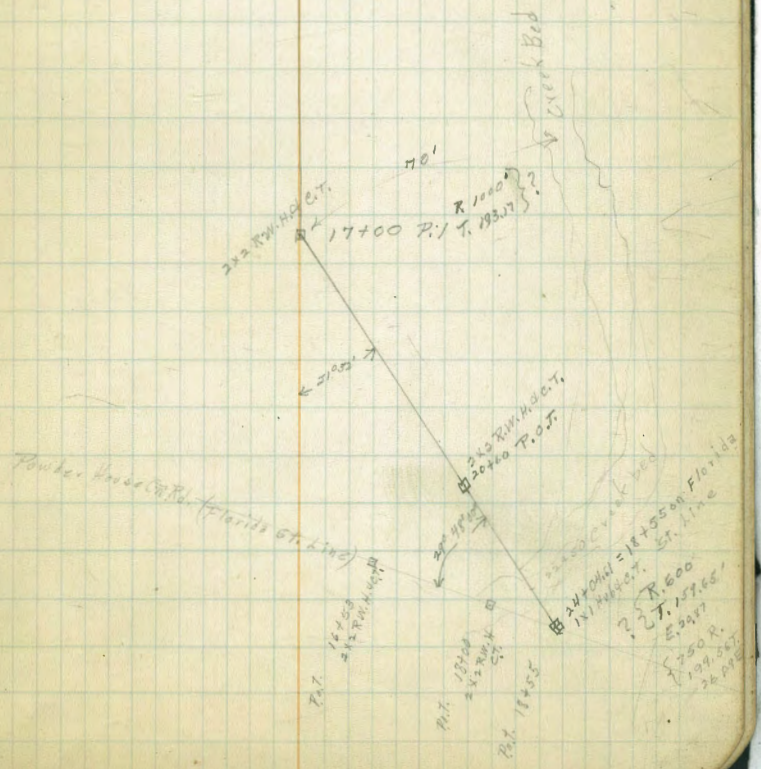
1



2475 P.I.
2475 P.I.

□ 2240 P.O.T.

□ 1240 P.O.T. *Edsel Canyon*
2x2 RW.H.C.T.



X Sec. Powder House Canyon Road.
Alignment - "B" Line Book 1355 P 69 (Sisson)

10/29/30 London.

Intersection Upas & Florida.

NE - NW & SE returns in.

60' wide 10' curbs 40' Railway.

Note.

4

B.M.	2.55	200.54	198.01	Florida & North B.P.S.W.	TP 4.25	203.45	136	199.20
0-140					0+50			
Ecb	4.81	195.75			50L	0.3		203.2
gut	5.71	194.85			30L	4.0		199.5
±	5.96	194.60			15L	5.5		198.0
Wgut	5.64	194.92			±	8.1		195.4
Web	4.82	195.74			15R	10.2		193.3
0-40 = NL Upas					23R	11.0		192.5
Web-2± top cb	5.81				50R	10.3		193.2
gut	6.67	193.89			1+00			
±	6.98	193.58			50R	9.7		193.8
Ecb-2± gut	6.55	194.01			24R	11.1		192.4
top cb	5.70	194.86			15R	9.6		193.9
0-20 = ± Upas					±	7.4		195.9
EL	5.65	194.91			15L	5.8		197.7
cb	6.32	194.24			50L	1.1		202.4
±	7.06	193.50			1+50			
cb	7.40	193.16			50L	2.2		201.3
W.L.	7.60	193.96			15L	6.6		196.9
0+00 = SL Upas					±	8.0		195.5
W.L.	7.18	193.38			15R	9.0		194.5
cb	6.80	193.76			50R	10.9		192.6
±	6.52	194.04						
cb	6.43	194.13						
42± gut	6.39	193.17						
42± top cb	5.58	194.98						

Powder House Canyon.

2 + 00		20345	
50R	10.9	192.6	
15R	10.1	193.4	
⊕	9.2	193.3	
15L	7.8	195.7	
50L	3.5	200.0	
2 + 50			
50L	5.6	197.9	
15L	9.3	194.2	
⊕	10.0	193.5	
15R	11.3	192.2	
45R	15.1	188.4	
50R	14.4	189.1	
3 + 00			
50R	15.5	188.0	
25R	16.2	187.3	
15R	13.6	189.9	
⊕	11.5	192.0	
15L	10.2	193.3	
50L	7.0	196.5	
T.P. 494	198.70	9.69	193.76

3 + 50		198.70		5
50L	3.4	195.3		
20L	5.4	193.3		
15L	6.8	191.9		
⊕	11.8	186.9		
15R	12.1	186.6		
50R	11.8	186.9		
4 + 00				
50R	12.3	186.4		
20R	13.3	185.4		
15R	12.8	185.9		
⊕	12.8	185.9		
15L	13.0	185.7		
25L	11.4	187.3		
50L	3.7	195.0		
4 + 50				
50L	5.4	193.3		
35L	12.9	185.8		
15L	13.4	185.3		
⊕	13.2	185.5		
15R	14.1	184.6		
30R	14.5	184.2		
50R	13.9	184.8		

Powder House Canyon.

5+00	19870		
50R	15.3	183.4	
15R	14.4	184.3	
±	13.6	185.1	
15L	12.2	186.5	
35L	11.7	187.0	
50L	5.5	193.2	

5+50			
50L	7.1	191.6	
30L	10.2	188.5	
15L	11.3	187.4	
±	12.5	186.2	
15R	14.2	184.5	
40R	16.7	182.0	
50R	15.5	183.2	

6+00			
50R channel	18.2	180.5	
45R	16.3	182.4	
35R	16.6	182.1	
32R	18.3	180.4	
30R	17.0	179.7	
15R	15.9	182.8	
±	14.2	184.5	
15L	10.3	188.4	
50L	1.1	197.6	
T.P. 561	197.90	6.41	172.27

6+50	197.90	6
50L	0.1	197.8
28L	7.1	190.8
15L	14.3	183.6
±	15.7	182.2
15R	16.6	181.5
30R	17.4	180.5
50R	15.8	182.1

6+90		
50R	19.2	178.7
43R	17.9	180.0
28R	19.1	178.8
15R	16.9	181.0
±	16.1	181.8
15L	12.6	185.3
50L	2.3	195.6

7+15		
50L	2.2	195.7
15L	8.0	189.9
±	10.3	187.6
15R	12.2	185.7
27R	15.1	182.8
39R	19.5	178.4
45R	18.0	179.9
50R	19.0	178.9

7+50 197.90

50R	18.6	179.3
40R	14.9	183.0
15R	11.1	186.8
£	9.7	188.2
15L	8.3	189.6
40L	6.8	191.1
43L	8.0	189.9
50L	4.7	193.2

7+75

50L	3.7	194.2
15L	9.7	188.2
£	13.0	184.9
15R	13.6	187.3
35R	14.6	183.3
50R	17.9	180.0

8+00

50R	17.5	180.4
15R	13.7	184.8
£	12.1	185.8
15L	11.1	186.8
50L	5.6	192.3
T.P 6.15	191.53	12.52 185.38

191.53

8+50

50L	2.0	189.5
15L	7.9	183.6
£	9.2	182.3
15R	10.9	180.6
30R	13.4	178.1
50R	13.5	178.0

9+00

50R	14.0	177.5
15R	11.9	179.6
£	10.8	180.7
15L	9.0	182.5
50L	3.2	188.3

9+50

50L	2.2	189.3
20L	8.5	183.0
15L	10.5	181.0
£	12.5	179.0
15R	14.0	177.5
50R	15.2	176.3
T.P 6.66	190.25	7.94 183.59

10+00		190.25	
50R	16.9	173.4	
15R	14.3	176.0	
⊕	12.5	177.8	
15L	10.4	179.9	
50L	0.6	189.7	

10+50			
50L	4.6	185.7	
15L	13.1	177.2	
⊕	15.3	175.0	
15R	16.7	173.4	
50R	1.6	173.7	
TP	3.70	181.12	12.83 177.42

11+00			
50R channel	11.0	170.1	
44R	8.2	172.9	
15R	8.8	172.3	
⊕	8.8	172.3	
15L	8.9	172.2	
50L	6.6	174.5	

11+50		181.12	
50L	9.8	171.3	
15L	10.6	170.5	
⊕	9.0	172.1	
10R	9.3	171.9	
15R channel	12.0	169.1	
23R	"	12.0	169.1
25R	10.0	171.1	
50R	9.5	171.6	

11+75			
40R	6.2	174.9	
34R	9.2	171.9	
25R	10.1	171.0	
15R	9.5	171.6	
6R	10.6	170.5	
4R channel	12.5	168.6	
⊕	"	12.3	168.8
4L	"	11.6	169.5
6L	"	10.2	170.9
15L	9.7	171.4	
50L	10.6	170.5	

Powder House Canyon

12+00 181.12

50L	10.4	170.7
38L	10.1	171.0
34L channel	12.4	168.7
15L "	11.7	169.4
±	9.6	171.5
15R	9.5	171.6
20R	7.3	173.8
50R	4.0	177.1
T.P. 0.55	178.38	3.29 177.83

12+50

50R	1.9	176.5
15R	3.7	174.7
±	5.1	173.3
10L	5.8	172.6
15L	8.2	170.2
50L	8.5	169.9

13+00

50L	9.8	168.6
30L	8.8	169.6
15L	6.8	171.6
±	5.7	172.7
15R	4.7	173.7
20R	5.4	173.0
30R	4.0	174.4
50R	3.4	175.0

13+50 178.38

50R	5.7	172.7
30R	5.9	172.5
20R	7.3	171.1
15R	6.5	171.9
7R	7.0	171.4
3R	8.1	170.3
±	8.1	170.3
3L	7.7	170.7
15L	9.2	169.2
21L	10.1	168.3
45L	10.0	168.4
50L	13.4	165.0

14+00

50L	11.8	166.6
47L	12.2	166.2
36L	14.3	164.1
33L	14.4	164.0
31L	12.2	162.2
15L	10.1	168.3
±	9.5	168.9
15R	9.4	169.0
23R	9.4	169.0
33R	8.0	170.4
50R	7.9	170.5

14+50 178.38

50R	9.6	168.8
32R	10.0	168.4
23R	11.1	167.3
15R	11.7	166.7
10R	10.7	167.7
⊕	11.2	167.2
15L	12.1	166.3
25L	13.0	165.4
32L	12.8	165.6
37L	12.0	166.4
40L	13.4	165.0
50L	14.9	163.5

15+00

50L	11.7	166.7
41L	13.6	164.8
28L	14.0	164.4
23L Channel	16.7	161.7
19L "	16.7	161.7
15L	14.1	164.3
⊕	12.6	165.8
15R	12.0	166.4
50R	11.3	167.1
T.P. 8.04	173.52	12.90 165.48

15+25 173.52

50R	7.2	166.3
15R	7.8	165.7
⊕	9.4	164.1
9L	12.4	161.1
15L	12.0	161.5
20L	9.9	163.6
44L	8.0	165.5
50L	6.6	166.9

15+50

50L	4.2	169.3
33L	9.7	163.8
30L	8.9	164.6
15L	9.2	164.3
6L	9.3	164.2
3L	12.7	160.8
⊕	12.9	160.6
1R	12.9	160.6
4R	10.7	162.8
10R	8.5	165.0
15R	8.2	165.3
50R	7.7	165.8

Powder House Canyon.

11

	15+75	173.52
50R	8.3	165.2
15R	9.8	165.7
10R	11.3	162.2
9R	13.5	160.0
4R	12.7	160.8
±	10.8	162.7
15L	9.1	164.4
33L	9.2	164.5
50L	2.1	171.4

	16+00	
50L	0.8	172.7
37L	7.6	165.9
23L	9.5	164.0
15L	8.6	164.9
±	10.1	163.4
8R	11.1	162.4
11R channel	13.9	159.6
15R "	13.7	159.6
20R	10.3	163.2
50R	8.5	165.0

	16+50	173.52
50R	9.8	163.7
40R	10.7	162.8
37R channel	14.7	158.8
29R "	14.1	159.4
25R	11.4	162.1
15R	10.7	162.8
±	9.6	163.9
15L	9.0	164.5
33L	8.8	164.7
50L	1.6	171.9

	17+00	
50L	6.7	166.8
18L	9.0	164.5
15L	9.8	163.7
10L	10.2	163.3
7L	8.7	164.8
±	9.6	163.9
15R	10.2	163.3
39R	11.5	162.0
45R	14.3	159.2
50R	14.3	159.2
T.P.	3.73	167.17 / 10.08
		163.44

17+33¹⁹ B.C. 167.17

50R	6.1	161.1
15R	3.9	163.3
⊕	3.1	164.1
7L	4.2	163.0
15L	4.2	163.0
23L	5.4	161.8
28L	3.0	164.2
50L	0.7	166.5

17+50

50L	1.1	166.1
35L	2.6	164.6
15L	3.7	163.5
5L	5.2	162.0
⊕	5.0	162.2
2R	3.8	163.4
15R	3.5	164.7
50R	5.7	161.5

18+00

50R	6.8	160.4
25R	4.9	162.3
23R	6.1	161.1
15R	6.5	160.7
8R	5.9	161.3
5R	5.0	162.2
⊕	4.7	162.5

18+00 167.17

6L	5.3	161.9
15L	5.0	162.2
40L	2.5	164.7
50L	2.8	164.4

18+50

50L	2.1	165.1
40L	3.2	159.0
35L	4.3	162.9
15L	4.6	162.6
⊕	5.0	162.2
10R	5.8	161.4
15R	7.2	160.0
17R	8.2	159.0
21R	8.0	159.2
23R	6.6	160.6
35R	7.0	160.2
50R	9.5	157.7

18+66²¹ E.C.

50R	9.3	157.9
40R	10.0	157.2
35R	7.7	159.5
15R	5.9	161.3
⊕	5.36	161.81
15L	5.5	161.7
30L	3.8	163.4
50	0.6	166.6

19+00	167.17		
50L	+0.3	167.5	
30L	3.3	163.9	
15L	5.5	161.7	
10L	6.5	160.7	
⊕	6.9	160.3	
15R	6.7	160.5	
29R	8.1	158.1	
33R	10.0	157.2	
39R	10.2	157.0	
44R	8.6	158.6	
50R	8.0	159.2	

19+50			
50R	8.2	159.0	
39R	9.7	157.5	
26R	10.2	157.0	
22R	8.3	158.9	
15R	7.8	159.4	
⊕	7.7	159.5	
15L	5.9	161.3	
50L	1.1	166.1	

20+00	167.17		
50L	2.7	164.5	
15L	7.2	160.0	
⊕	8.0	159.2	
15R	8.3	158.9	
35R	8.9	158.3	
45R	11.6	155.6	
50R	11.3	155.9	

20+50			
50R	10.7	156.5	
40R	11.6	155.6	
15R	9.5	157.7	
⊕	8.9	158.3	
TPS 24	164.50	7.91	159.26
15L	5.4	159.1	
25L	4.7	159.8	
50L	2.8	161.7	

21+00			
50L	2.4	162.1	
36L	4.5	160.0	
15L	5.8	158.7	
⊕	6.6	157.9	
15R	7.7	156.8	
23R	9.0	155.5	
32R	11.4	153.1	
37R	9.9	154.6	
50R	8.7	155.8	

21+50	164.50		
50R	9.6	154.9	
22R	10.2	154.3	
15R	11.4	153.1	
10R chl.	11.8	152.7	
♀	9.8	154.7	
4L	8.1	156.4	
15L	6.6	157.9	
35L	5.1	159.4	
45L	4.9	159.6	
50L	3.9	160.6	

22+00			
50L	3.0	161.5	
35L	3.9	160.6	
27L	6.0	158.5	
15L	9.3	155.2	
10L	10.7	153.8	
♀	11.2	153.3	
15R	11.8	152.7	
20R	13.2	151.3	
30R	10.8	153.7	
40R	10.4	154.1	
50R	10.3	154.2	

22+50	164.50		
50R	11.6	152.9	
40R	12.3	152.2	
35R	14.0	150.5	
30R	13.4	151.1	
25R	11.7	152.8	
15R	11.4	153.1	
♀	9.6	154.9	
15L	4.0	160.5	
28L	2.1	162.4	
24L	1.8	162.7	
40L	0.3	164.2	
50L	11.3	165.8	

23+00			
50L	1.0	163.5	
35L	3.6	160.9	
25L	3.6	160.9	
15L	4.9	159.6	
♀	6.5	158.0	
15R	9.6	154.9	
30R	12.1	152.4	
45R	12.6	151.9	
50R	11.8	152.7	
T.P. 6.44	168.60	2.34	162.16

23+50 168.60

50R	15.2	153.4
30R	14.6	154.0
15R	13.6	155.6
⊕	13.2	155.4
4L	13.0	155.6
15L	11.0	157.6
27L	9.4	159.2
38L	9.2	159.4
50L	6.8	161.8

24+00

50L	5.2	163.4
35L	8.2	160.4
32L	9.5	159.1
23L	9.5	159.1
15L	11.1	157.5
⊕	13.2	155.4
15R	14.3	154.3
32R	16.3	152.3
50R	16.7	151.9

15

24+50 168.60

50R	17.9	150.7
15R	15.1	153.5
⊕	13.2	155.4
15L	11.9	156.7
23L	11.3	157.3
32L	9.0	159.6
50L	5.9	162.7

25+00

50L	6.6	162.0	
27L	10.6	158.0	
15L	12.6	156.0	
⊕	15.2	153.4	
T.P. 198	159.31	11.27	157.33
⊕	5.98	153.33	
15R	6.6	152.7	
50R	10.0	149.3	
⊕ 406	12.08	165.41	153.33

25+50

50R	17.1	148.3
24R	16.5	148.9
15R	14.3	151.1
⊕	12.2	153.2
15L	9.8	155.6
50L	2.9	162.5

26+00 - 165.41

50L	+2.1	167.5
15L	6.5	158.9
£	9.3	156.1
15R	14.9	150.5
40R	18.9	146.5
50R	19.0	146.4

26+50

50R	19.7	145.7	
28R	16.1	149.3	
15R	9.4	156.0	
11R	8.2	157.2	
£	6.3	159.1	
15L	4.4	161.0	
50L	+1.8	167.2	
T.P. 10-36	168.16	7.61	157.80

27+00

50L	0.2	168.0
15L	7.9	160.3
£	10.4	157.8
15R	12.6	156.6
25R	13.9	154.3
38R	23.0	145.2
50R	23.8	144.4

168.16

27+50

50R	24.6	143.6
33R	17.4	150.8
15R	14.1	154.1
£	10.0	158.2
15L	6.8	161.4
33L	3.5	164.7
50L	2.5	165.7

28+00

50L	10.7	157.5
15L	13.5	154.7
£	15.6	153.6
15R	17.0	151.2
25R	19.3	148.9
40R	20.9	147.3
50R	20.0	148.2

28+50

50R	18.2	150.0
15R	14.7	153.5
£	12.6	155.6
15L	8.1	160.1
25L	4.9	163.3
50L	+1.8	170.0

29+00	168.16		
50L		+4.0	172.2
15L		6.2	162.0
♀		11.3	156.9
15R		15.1	153.1
50R		19.4	148.8
T.P. 12.17	190.99	9.34	158.82

29+50			
50R		23.8	147.2
15R		17.7	153.3
♀		14.7	156.3
15L		11.6	159.4
50L		0.8	170.2

30+00			
50L		5.5	165.5
15L		14.2	156.5
♀		16.2	154.5
15R		18.3	152.7
50R		23.1	147.9

30+50			
50R		24.6	146.4
30R		21.6	149.4
15R		20.0	151.0
♀		19.7	152.3
15L		17.0	154.0
50L		11.7	159.3
T.P. 5.35	163.61	12.73	158.26

31+00	163.61		17
50L		7.0	156.6
15L		12.1	151.5
♀		13.7	149.9
15R		15.1	148.5
40R		18.0	145.6
50R		19.5	144.1

31+50			
50R		23.5	140.1
15R		20.2	143.4
♀		19.7	145.9
15L		15.8	147.8
50L		10.3	153.3

32+00			
50L		11.0	152.6
T.P. 0.99	151.55	13.05	159.56
15L		8.3	143.3
♀		10.5	141.1
15R		11.5	140.1
50R		13.6	138.0

32+50			
50R		15.8	136.8
30R		14.1	137.5
15R		13.3	138.3
♀		12.6	139.0
15L		10.1	141.5
35L		4.7	146.9
50L		1.2	150.4

33+00 151.55

50L	3.2	148.4
25L	11.0	140.6
15L	12.2	139.4
☼	13.8	137.8
15R	14.9	136.7
31R	16.4	134.2
50R	16.8	134.2

33+50

50R	16.6	135.0
30R	17.2	134.4
15R	16.0	135.6
☼	15.6	136.0
15L	14.0	137.6
38L	9.9	141.7
50L	5.7	145.9

34+00

50L	7.9	143.7
40L	11.2	139.6
15L	14.1	137.5
☼	15.2	136.4
15R	16.6	135.0
30R	18.4	133.2
35R	17.6	134.0
50R	17.7	133.9

34+50 151.55

50R	19.2	132.4	
30R	18.5	133.1	
25R	19.5	132.1	
15R	17.9	133.7	
☼	17.1	134.5	
15L	15.8	135.8	
30L	13.9	137.7	
50L	8.4	143.2	
T.P. 5.77	144.66	12.66	138.89

35+00

50L	3.1	141.6
33L	8.2	136.5
15L	10.4	134.3
☼	11.9	132.8
15R	12.9	131.8
23R	12.4	132.3
50R	13.3	131.4

35+50

50R	14.0	130.7
15R	13.1	131.6
☼	12.8	131.9
15L	12.0	132.7
25L	10.5	134.2
50L	2.9	141.8

36+00 144.66

50L	2.2	142.5
15L	10.3	134.4
±	11.8	132.9
15R	13.7	130.8
50R	14.1	130.6

36+50

50R	15.2	129.5
35R	15.3	129.4
27R	13.2	131.5
15R	11.9	132.8
±	9.9	134.8
15L	7.8	136.9
50L	3.4	141.3

37+00

50L	4.5	140.2
15L	7.3	137.4
±	9.0	135.7
15R	10.7	134.0
35R	12.6	132.1
50R	15.4	129.3

37+50 144.66

50R	14.2	130.5
30R	11.8	132.9
15R	10.2	134.5
±	9.1	135.6
15L	8.0	136.7
50L	5.6	139.1

38+00

50L	6.6	138.1
15L	9.0	135.7
±	9.89	134.77
15R	10.9	133.8
35R	13.0	131.7
50R	15.4	129.3

38+50

50R	16.6	128.1
30R	14.0	130.7
15R	11.5	133.2
±	10.6	134.1
15L	9.9	134.8
50L	8.5	136.2

39+00

50L	12.9	131.8
35L	10.3	134.4
15L	10.8	133.9
±	11.6	133.1

39+00 144.66

15R	13.0	131.7
40R	16.7	128.0
50R	18.0	126.7
T.P.	3.70	136.67

39+50

50R	10.2	126.5
30R	6.7	130.0
15R	5.6	131.1
+	4.5	132.2
15L	4.0	132.7
30L	4.2	132.5
43L	9.5	127.2
50L	8.4	128.3

40+00

50L	9.2	127.5
45L	11.3	125.4
30L	10.6	126.1
26L	9.1	127.6
15L	9.2	127.5
+	7.6	129.1
15R	11.1	125.6
50R	12.2	124.5

40+50 136.67

50R	11.8	124.9
40R	10.5	126.2
15R	10.9	125.8
+	11.1	125.6
12L	12.0	124.7
15L	10.3	126.4
50L	8.4	128.3

40+75

50L	6.6	130.1
25L	9.7	127.0
15L	10.3	126.4
+	11.1	125.6
7R	12.3	124.4
15R	12.4	124.3
50R	13.6	123.1

41+00

50R	12.2	124.5
15R	10.2	126.5
+	9.7	127.0
15L	8.6	128.1
50L	3.8	132.9
T.P.	6.94	141.97

41+50 141.97

50L	3.4	138.6
15L	8.6	133.4
⊕	10.5	131.5
15R	12.0	130.0
43R	14.9	127.1
50R	16.2	125.8

42+00

50R	17.2	124.8
26R	13.8	128.2
15R	12.2	129.8
⊕	10.6	131.4
15L	9.4	132.6
30L	6.9	135.1
50L	4.3	137.7

42+50

50L	5.6	136.4
15L	10.6	131.4
⊕	12.8	129.2
15R	14.4	127.6
50R	18.1	123.9

43+00 141.97

50R	18.2	123.8
35R	17.3	124.7
15R	15.1	126.9
⊕	13.4	128.6
15L	11.9	130.1
50L	6.5	135.5

43+50

50L	7.7	134.3
15L	11.9	130.1
⊕	14.3	127.7
15R	15.8	126.2
30R	16.4	125.6
50R	19.7	122.3

44+00

50R	24.6	117.4
45R	24.6	117.4
40R	19.5	122.5
15R	17.6	124.4
⊕	15.9	126.1
10L	13.4	128.6
15L	12.4	129.6
32L	10.2	131.8
33L	14.0	128.0
41L	13.7	128.3
45L	8.3	133.7
50L	7.4	134.6

44+15 14197

50L	8.1	1339
25L	11.6	130.4
20L	16.4	125.6
15L	16.8	125.2
⊕	19.2	122.8
15R	19.3	222.7
26R	21.6	120.4
50R	24.5	117.5

44+20

50R	23.9	118.1
26R	19.0	122.0
15R	17.8	124.2
⊕	16.0	126.0
15L	13.4	128.8
50L	8.1	133.9

44+50

50L	10.0	132.0
15L	14.4	127.6
⊕	14.3	125.7
15R	18.7	123.3
30R	20.4	121.6
50R	21.6	120.4

45+00 14197

50R	22.3	119.7
35R	20.7	121.3
15R	19.0	123.0
⊕	17.2	124.8
15L	15.6	126.4
50L	10.4	131.6
T.P. 563	13545	12.15
45+50		129.82

50L	3.4	132.1
15L	8.2	127.3
⊕	10.6	124.9
15R	12.2	123.5
50R	15.6	119.9

46+00

50R	16.5	119.0
25R	13.4	122.1
15R	12.5	123.0
⊕	10.7	124.8
15L	9.0	126.5
50L	4.4	131.1

46+50 135.45

50R	4.8	130.7
15L	9.1	126.4
⊕	10.8	124.7
15R	12.8	122.7
50R	17.3	118.2

47+00

50R	19.0	116.5
35R	15.7	119.8
15R	13.3	122.2
⊕	11.6	123.9
15L	9.9	125.6
50L	6.0	129.5

47+50

50L	6.5	129.0
15L	10.9	124.6
⊕	12.5	123.0
10R	13.2	122.3
15R	14.0	121.5
35R	17.7	117.8
50R	21.6	113.9

135.45

48+00

50R	26.9	108.6
42R	26.3	109.2
35R	18.6	116.9
15R	15.0	120.5
⊕	12.5	123.0
15L	10.7	124.8
30L	7.7	127.8
50L	4.9	130.6

48+50

50L	5.0	130.5
30L	8.7	126.1
22L	9.1	126.4
15L	10.5	125.0
⊕	12.5	123.0
15R	15.2	120.3
30R	18.3	117.2
42R	25.4	110.1
50R	27.3	108.2

49+00	135.45		
50R	29.0	106.5	
45R	29.0	106.5	
42R	26.4	109.1	
30R	24.5	111.0	
15R	20.9	114.6	
⊕	16.0	119.5	
15L	11.9	123.6	
32L	8.3	127.2	
41L	6.7	128.8	
50L	4.8	130.7	

49+50			
50L	4.6	130.9	
15L	12.6	122.9	
TP.	10.35	133.21	12.59
⊕		13.8	117.4
15R		19.9	113.3
25R		21.7	111.5
43R		23.0	110.2
50R		26.3	106.9

50+00			
50R	23.2	110.0	
47R	23.2	110.0	
30R	17.6	115.6	
15R	15.7	117.5	
⊕	14.1	119.1	

15L	133.2/11.8	121.4
31L	9.5	123.7
50L	6.1	127.1
TP 7.19	137.92	248
50+50		
50L	9.9	128.0
35L	12.4	125.5
15L	16.0	121.9
⊕	20.3	117.6
15R	20.7	117.2
31R	22.9	115.0
50R	25.4	112.5

51+00		
50R	26.8	111.1
15R	24.5	113.4
⊕	20.6	117.3
15L	15.8	122.1
45L	7.1	130.8
50L	6.8	131.1

51+24 ¹ B.C		
50L	3.2	134.7
45L	5.8	132.1
37L	6.1	131.8
15L	12.9	125.0
⊕	17.6	120.3
10R	20.8	117.1
15R	23.1	114.8

51+29 ⁰	137.92		
29 R	28.2	109.7	
50 R	28.8	109.1	
51+50			
50 R	29.7	108.2	
35 R	29.3	108.6	
15 R	22.0	115.9	
♀	15.0	122.9	
15 L	10.2	127.7	
35 L	5.1	132.8	
43 L	4.7	133.2	
50 L	0.4	137.5	
52+00			
50 L	4.7	133.2	
47 L	6.0	131.9	
40 L	6.3	131.6	
22 L	10.0	127.9	
15 L	11.7	126.2	
♀	16.9	121.0	
15 R	24.6	113.3	
32 R	30.0	107.9	
50 R	31.6	106.5	

52+50	137.92		
50 R	31.4	106.5	
15 R	31.1	106.8	
8 R	29.8	108.1	
♀	26.8	111.1	
15 L	18.8	119.1	
22 L	15.1	122.8	
50 L	6.9	131.0	
52+75 ⁸⁵ E.C.			
T.P. 1.43	131.23	8.12	129.80
50 L	3.3		127.9
40 L	4.9		126.3
15 L	17.2		113.0
♀	23.8		107.4
15 R	25.6		105.6
50 R	25.7		105.5
53+00			
50 R	26.0		105.2
15 R	26.0		105.2
♀	25.3		105.9
15 L	19.9		111.3
43 L	5.8		125.4
50 L	4.8		126.4

53+50 131.23

50L	7.6	123.6
22L	12.1	119.1
15L	16.2	115.0
♀	23.8	107.4
15R	26.5	104.7
50R	26.3	104.9

54+00

50R	28.3	102.9
40R	28.9	102.3
32R	24.0	107.2
15R	20.5	110.7
♀	17.3	113.9
15L	15.0	116.2
50L	9.4	121.8

54+50

50L	12.5	118.7	
T.P. 3.57	121.70	13.10	118.13
15L	8.0	113.7	
♀	10.5	111.2	
15R	12.7	109.0	
22R	13.2	108.5	
30R	13.9	107.8	
35R	19.8	107.9	
41R	21.7	100.0	
50R	20.0	101.7	

55+00 121.70

50R	16.0	105.7
15R	13.2	108.5
♀	11.4	110.3
15L	9.4	112.3
50L	4.7	117.0

55+50

50L	6.0	115.7
15L	9.7	112.0
♀	11.5	110.2
15R	13.4	108.3
50R	16.4	105.3

56+00

50R	15.3	106.4
15R	13.4	108.3
♀	12.5	109.2
15L	11.4	110.3
50L	8.4	113.3

56+50

T.P. 3.34	118.38	6.66	115.04
50L	5.2	113.2	
37L	7.6	110.8	
30L	7.5	111.9	
15L	9.2	109.2	
♀	11.2	107.2	
15R	12.2	106.2	

56+50 118.38

50R	14.5	103.9
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57+00

50R	15.2	103.2
25R	14.1	104.3
15R	13.5	104.9
⊕	12.5	105.9
15L	9.6	108.8
50L	6.1	112.3

57+50

50L	5.9	112.5
30L	7.9	110.5
15L	10.3	108.1
⊕	12.46	105.92
15R	13.9	104.5
50R	16.8	102.1

58+00

50R	17.6	100.8
15R	15.2	103.2
⊕	13.4	105.0
15L	11.5	106.9
50L	5.8	112.6

58+50 118.38

50L	5.6	112.8
38L	7.5	110.9
25L	11.5	106.9
15L	13.3	104.1
⊕	15.4	103.0
15R	16.3	102.1
50R	18.5	99.9

59+00

50R	18.7	99.7	
25R	17.0	101.4	
15R	15.3	103.1	
⊕	13.8	104.6	
15L	11.7	106.7	
50L	7.4	111.0	
TP 3.90	109.28	13.00	105.38

59+50

50L	+2.2	111.5
15L	3.1	106.2
⊕	4.9	104.4
15R	6.4	102.9
50R	10.7	98.6

60+00		109.28	
50R	12.9	96.4	
24R	11.1	98.2	
15R	8.8	100.5	
±	6.5	102.8	
15L	3.2	106.1	
50L	+4.7	114.0	
60+50			
50L	+6.0	115.3	
15L	3.5	105.8	
±	8.62	100.66	
15R	11.7	97.6	
50R	14.2	95.1	
61+00			
50R	15.3	94.0	
15R	13.6	95.7	
±	11.5	97.8	
15L	7.9	101.4	
30L	2.5	106.8	
50L	+4.0	113.3	

61+50		109.28	
50L	0.4	108.9	
30L	7.0	102.3	
15L	9.5	99.8	
±	12.3	97.0	
15R	14.1	95.2	
50R	17.2	92.1	
T.P. 5.10	102.89	11.49	97.79
62+00			
50R	11.2	91.7	
40R	11.0	91.9	
36R	10.1	92.8	
15R	8.3	94.6	
±	7.1	95.8	
15L	5.4	97.5	
45L toe Parish Dr.	2.4	100.5	
62+50			
40L toe Parish Dr	1.7	101.2	
15L	6.6	96.3	
±	8.4	94.5	
15R	9.6	93.3	
50R	11.6	91.3	

63+00 102.89

50R	12.3	90.6
15R	11.1	91.8
⊕	9.4	93.5
15L	7.1	95.8
40L toe Parsh. Dr.	1.2	101.7

63+50

40L	1.5	101.4
15L	8.0	93.9
⊕	10.3	92.6
15R	11.1	91.8
50R	13.1	89.8

64+00

50R	13.4	89.5
15R	12.5	90.4
⊕	11.4	91.5
15L	9.1	93.8
40L	5.3	97.6

64+50

50L	5.8	97.1
40L	8.4	94.5
15L	10.9	92.0
⊕	12.3	90.6
15R	13.4	89.5
50R	14.2	88.7

65+00 102.89

50R	14.2	88.7
15R	13.2	89.7
⊕	12.1	90.8
15L	10.9	92.0
50L	8.1	94.8

65+50

50L	10.2	92.7
15L	14.0	88.9
⊕	13.6	89.3
15R	15.0	87.9
50R	14.5	88.4
T.P. ^{0.42} Nail Power Pole.	93.35	9.96

65+8988 B.C.

50R	5.8	87.6
30R	5.4	88.0
15R	5.8	87.6
⊕	5.6	87.8
15L	5.1	88.3
47L toe Parsh. Dr.	2.0	91.4

66+00	93.35		
45L	2.4	91.0	
15L	5.3	88.1	
±	5.9	87.5	
15R	5.6	87.8	
30R	5.4	88.0	
50R	5.8	87.6	

66+50			
50R	7.0	86.4	
26R	6.0	87.4	
15R	6.1	87.3	
10R	5.6	87.8	
±	6.0	87.4	
15L	5.1	88.3	
29L	4.0	89.4	
40±	1.9	91.5	

67+00			
50L	3.1	90.3	
30L	4.0	89.4	
15L	4.4	89.0	
±	5.6	87.8	
3R	5.9	87.5	
15R	6.1	87.3	
40R	7.7	85.7	
50R	7.4	86.0	

67+50	93.35		
50R	8.9	84.5	
30R	8.0	85.4	
15R	6.4	87.0	
12R	5.7	87.7	
±	5.8	87.6	
15L	5.7	87.7	
39 ^S L N. Pav. Persh. Dr.	4.81	88.54	

68+00			
16 ^R L N. Pav.	5.94	87.41	
10L	6.0	87.4	
±	6.6	86.8	
15R	6.6	86.8	
22R	6.3	87.1	
30R	8.6	84.8	
50R	9.0	84.4	

68+55 ± Meets N Pav Persh Dr.			
50R	10.2	83.2	
38R	9.7	83.7	
32R	7.7	85.7	
15R	6.6	86.8	
7R	6.5	86.9	
±	6.74	86.61	

68+89⁷³ E.C. 93.35

4	6.88	86.47
6 ^a R	6.91	86.44
15 R	6.8	86.6
26 ^a	7.1	86.3

69+52⁷³

15 R N edge Pan	7.07	86.28
B.M	5.54	87.81

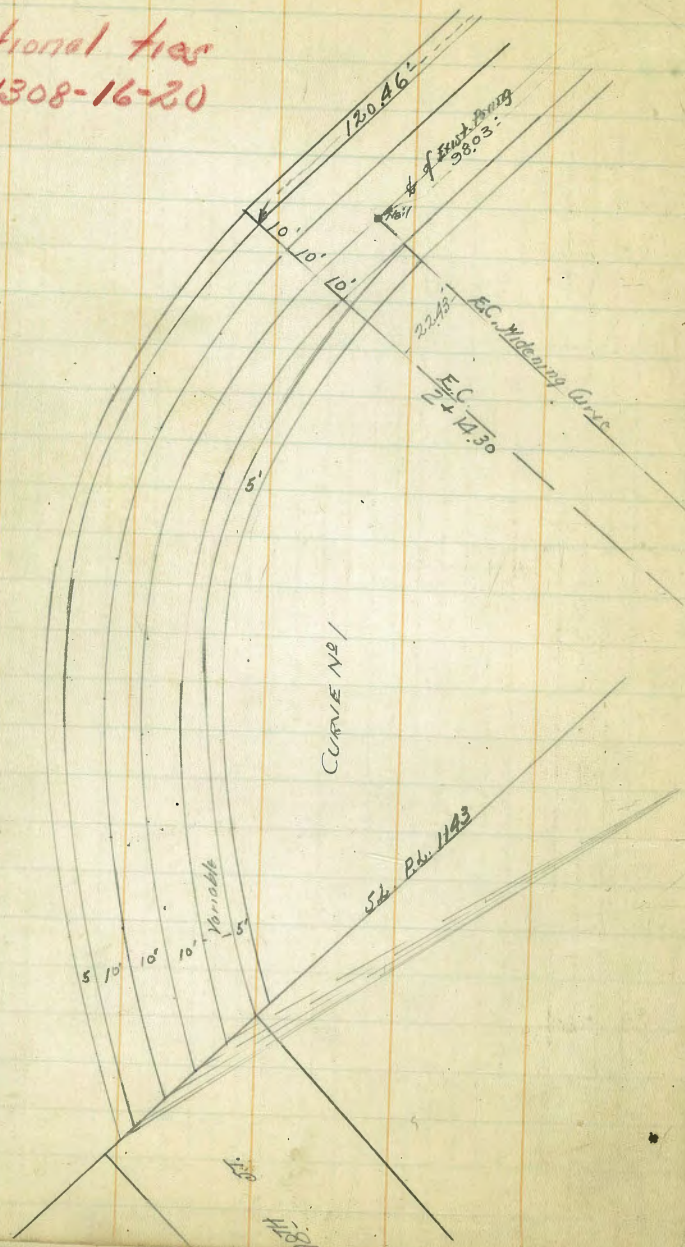
4.6 65.84⁷³ A
87.78 Sisson

60
61
415.3

Miller
Bliss
Debert
12-22-30

Alignment and Construction Notes PERSHING DRIVE

Additional ties
Book 1308-16-20

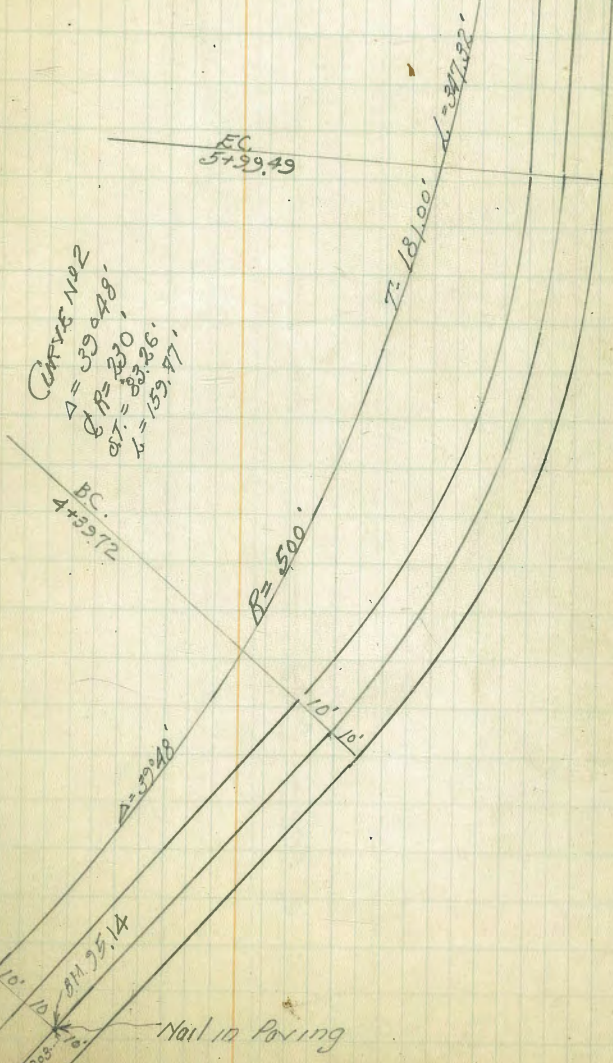


Ⓢ

E.C. Widening Curve

10' 10' 10' Nail in Pav.

32



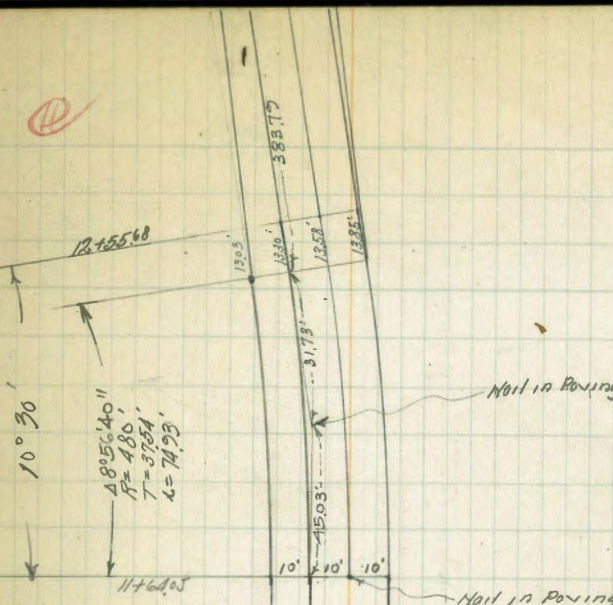
10' 20'

Existing Paving

10' 10' 10'

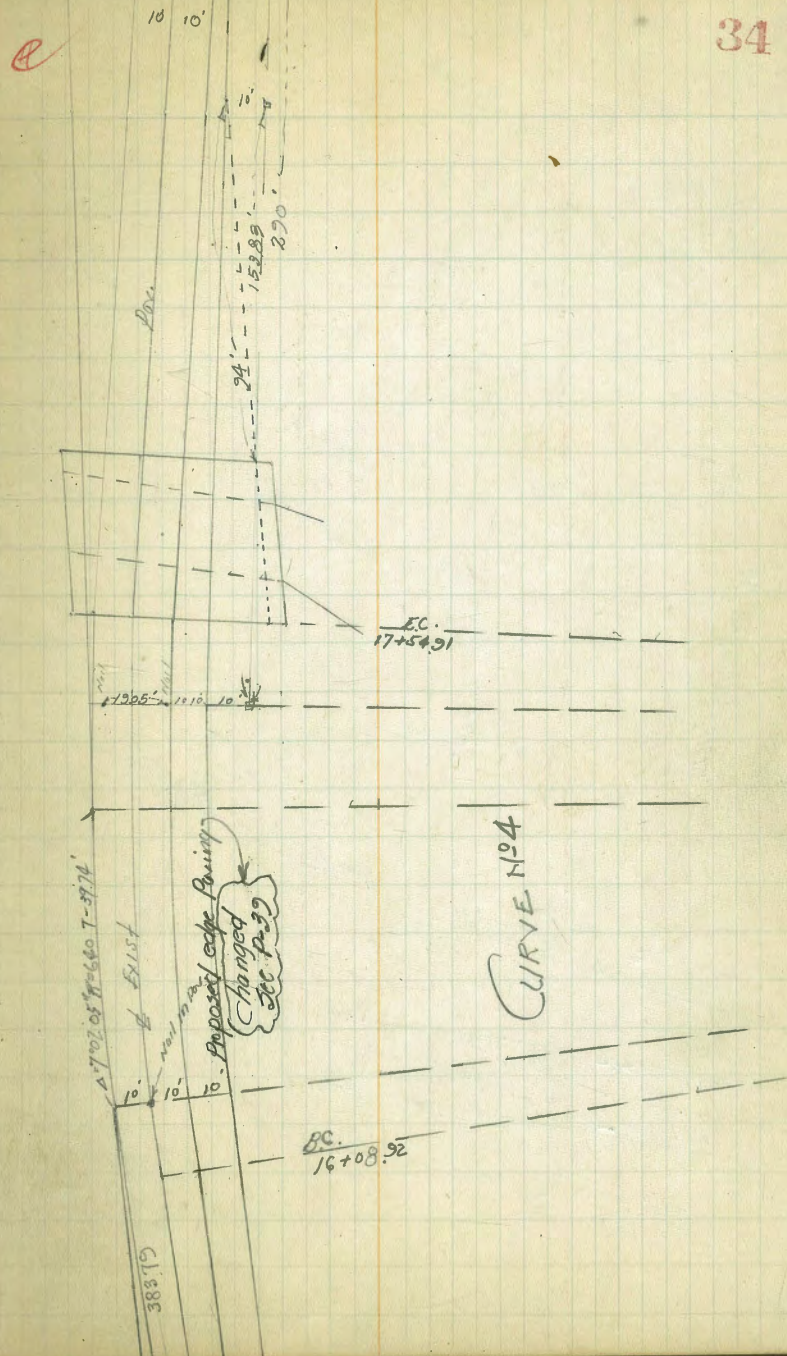
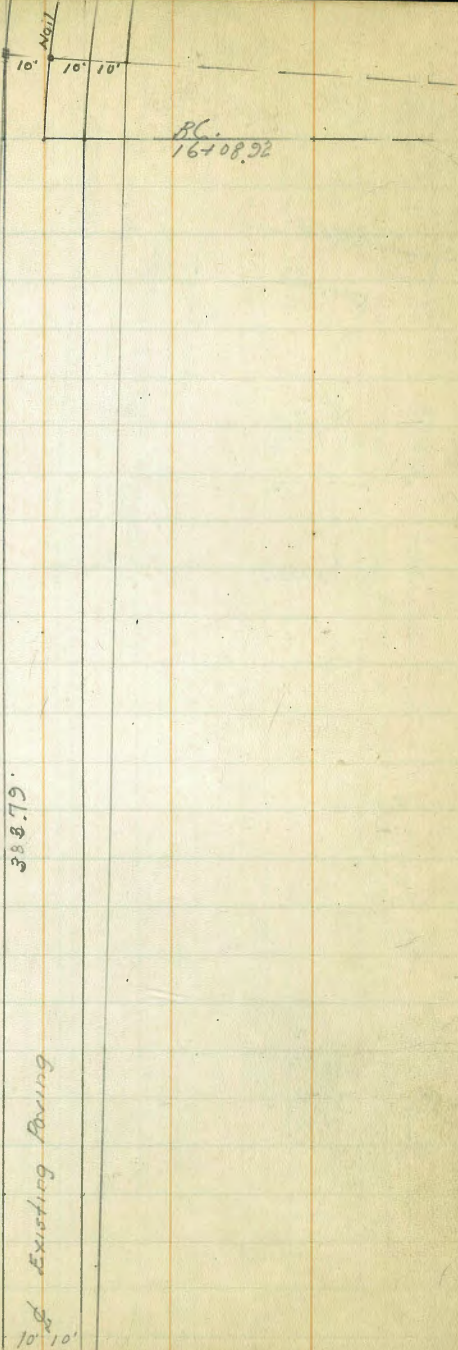
10' 20'

CURVE 123

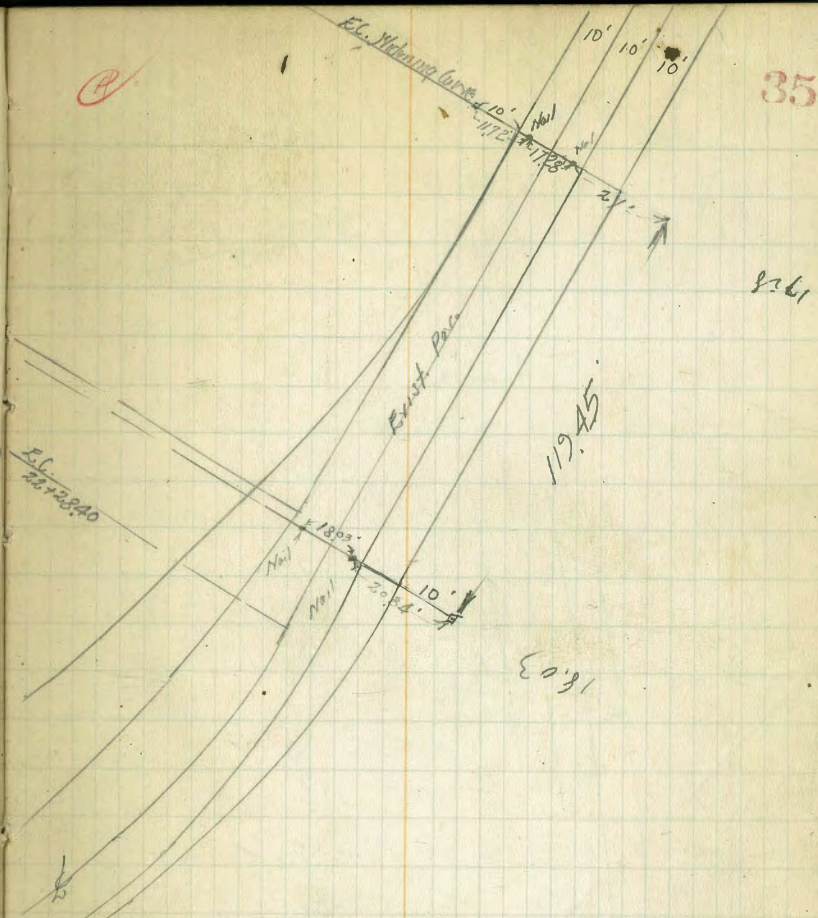
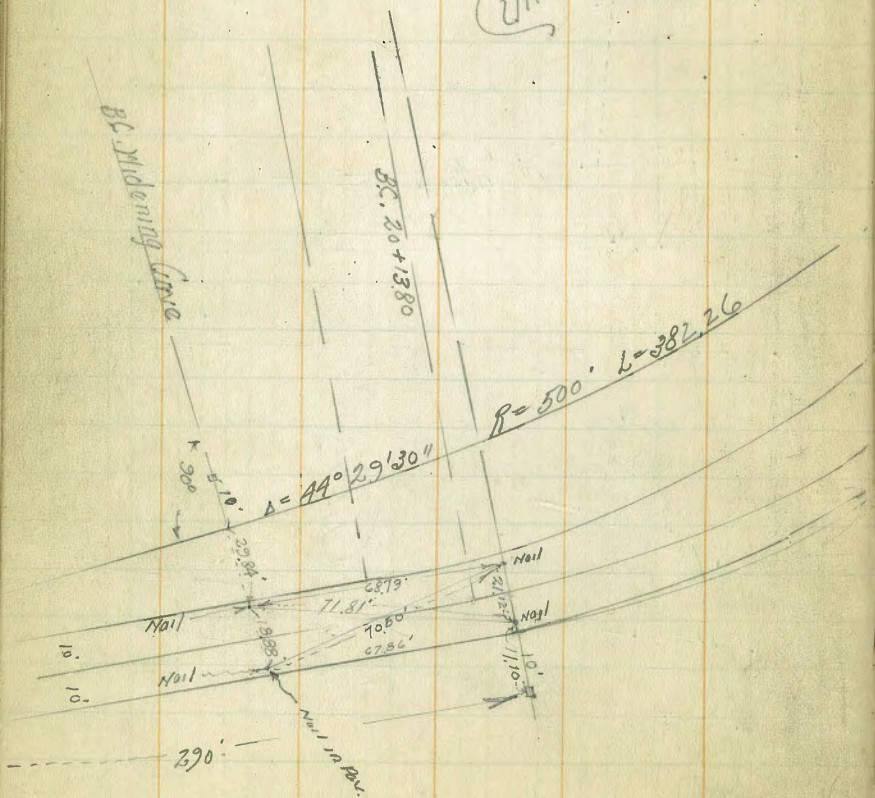


Existing Paving

10' 10' 10'



URVE 105



④

36

EC
34+12.81

BC
28+00.53

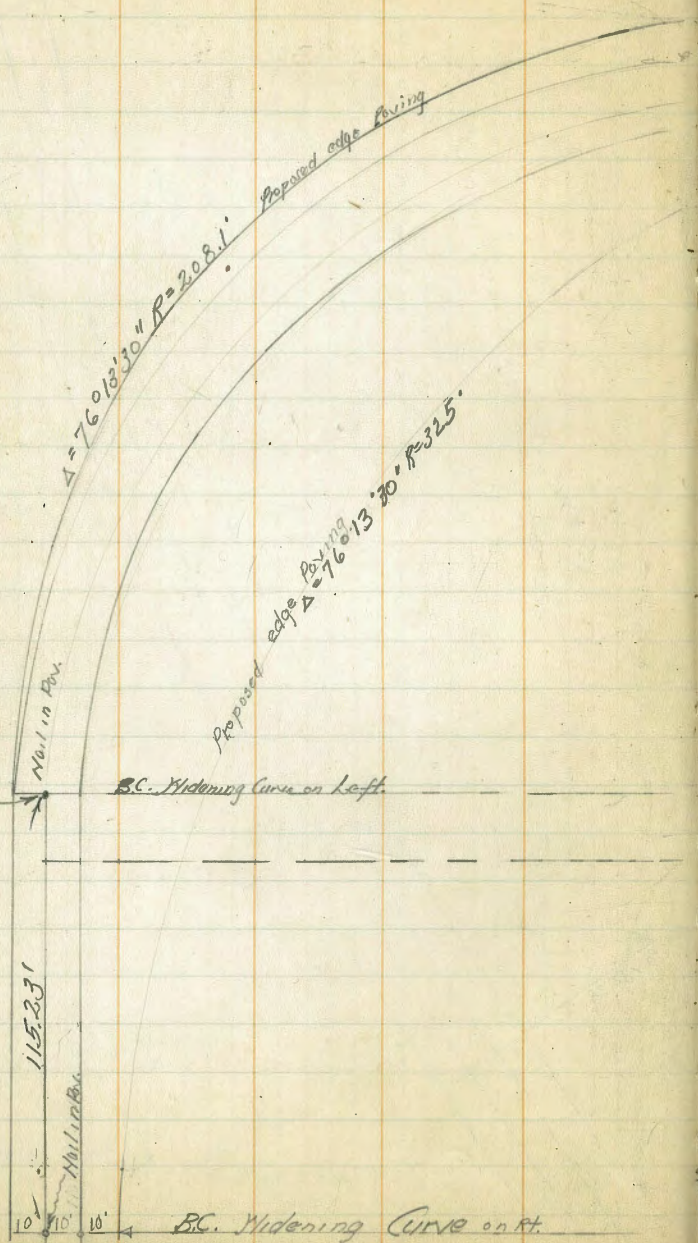
CURVE NO 7

CURVE NO 6

BC
30+84.28

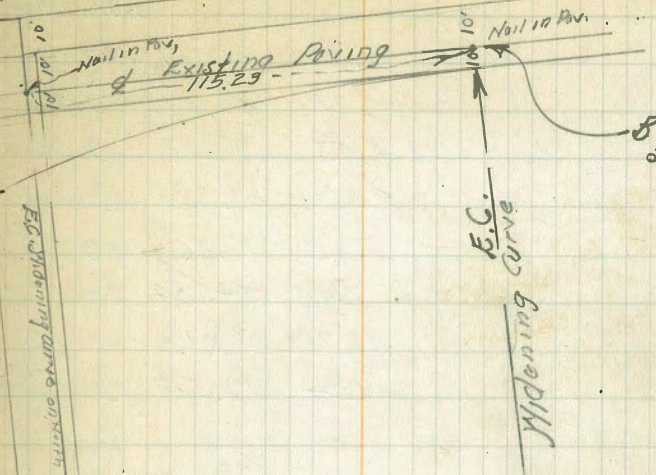
BC
25+09.50

BM. 220.78
See P. 61



115.231
Nail in Pk.
10'

BC. Widening Curve on rt.



E.C. Widening Curve on right

CURVE No 8

BM. 234.33
See P. 63

E.C. Widening Curve
R=325'

Q

Walker
Sigs
Sigs
12-13-80

PERSHING DRIVE BRIDGE

TIES AND GRADES

GRADES are
to the top of
Proleter

Cuts and Fills

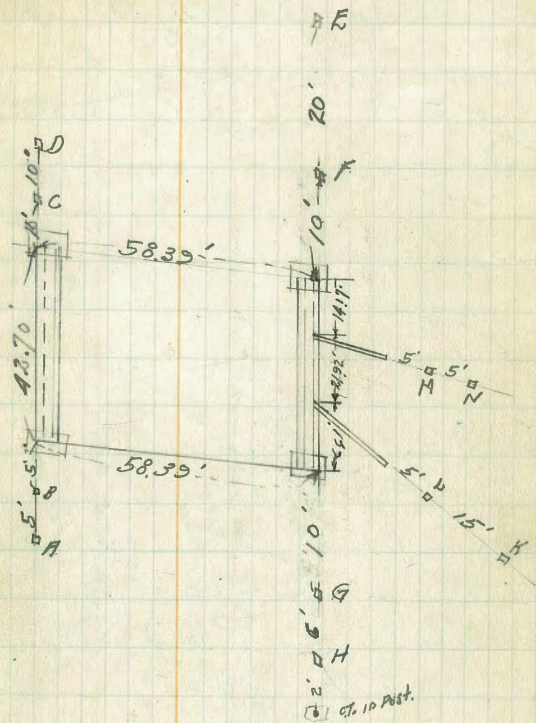
38

Station	X				
A	91.49	5.22	86.27	89.85	-3.58
B		5.22	86.27	89.85	-3.58
C		4.52	86.97	89.85	-2.88
D		4.21	87.28	89.85	-2.57
E		5.23	86.26	89.85	-3.59
F		7.45	84.04	89.85	-5.81
G		12.71	78.78	89.85	-11.07
H		11.94	79.55	89.85	-10.30

WING WALLS

top of
Wing Walls

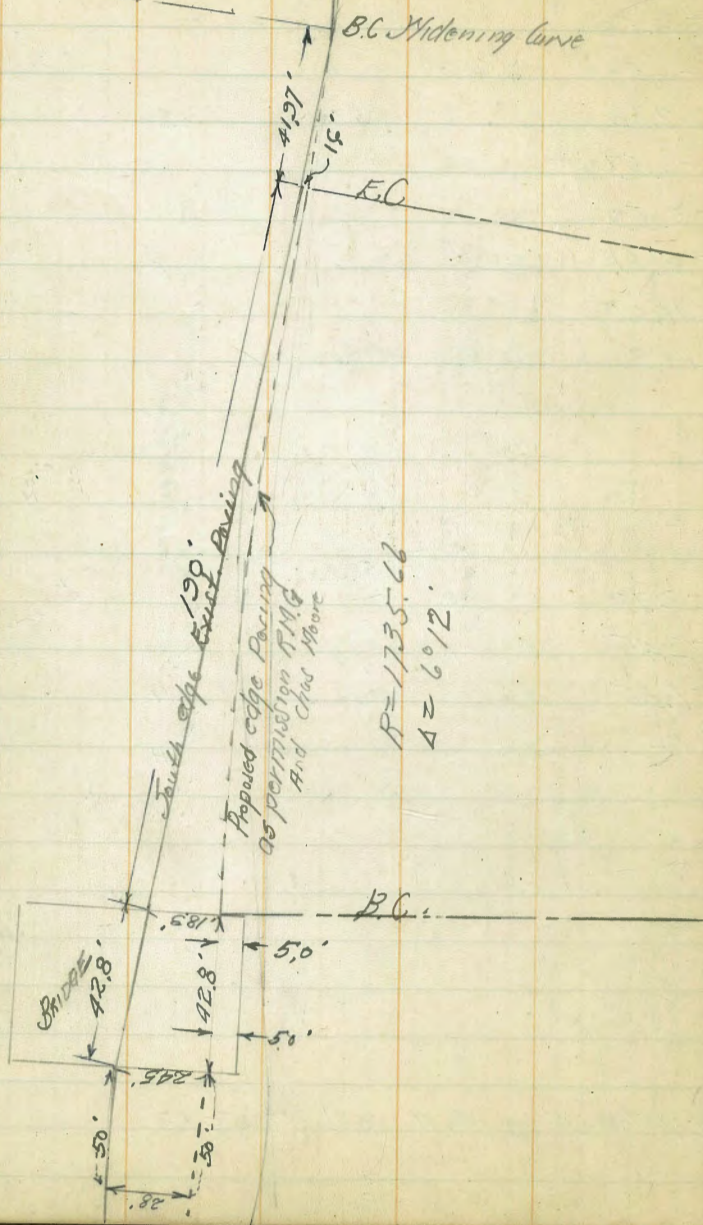
	X				
K	91.49	13.22	78.27	81.00	-2.73
L		12.94	78.55	81.00	-2.45
M		12.34	79.15	81.00	-1.85
N		11.91	79.58	81.00	-1.42
O			81.00	81.00	



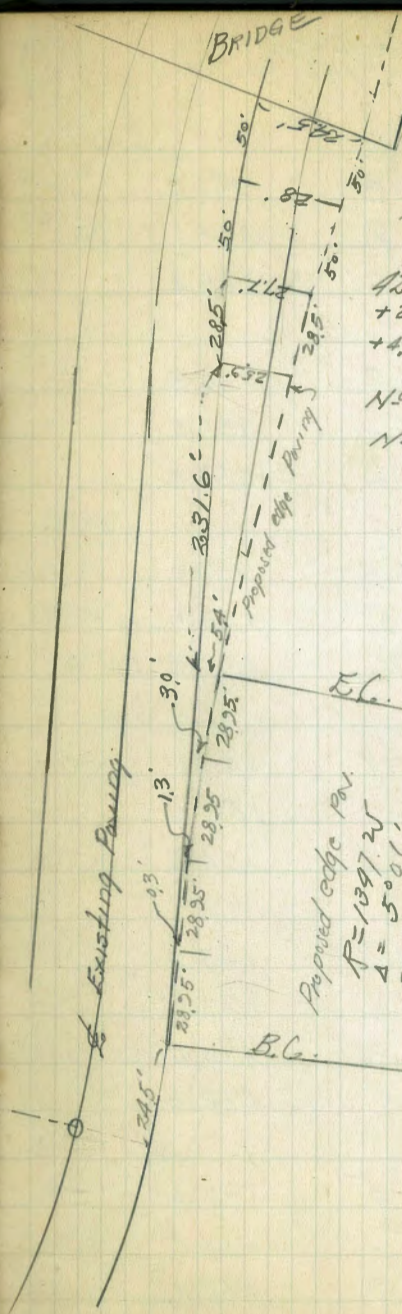
9.21 X
91.49

8228 B.M.

N.Y. top Wing Wall Book 1405-13



$R = 1735.66$
 $\Delta = 60/2$



Proposed edge Par.
 $R = 1397.25$
 $\Delta = 50/2$
 $\Delta T = 60'$

Area bet. South edge exist.
 Facing and edge Proposed Facing.

$42 \times 8 + 190 \times 9.15 + 2.14 \times 42.8 + 2625 \times 50$
 $+ 27.85 \times 50 + 26.8 \times 28.5 + 156.5 \times 231.6$
 $+ 4.2 \times 30 + 2.15 \times 30 + 0.8 \times 24 + 1.15 \times 30$
 No of sq. ft. = 99733
 No of sq. ft. as per plan = 4425.7
 No of Extra sq. ft = 5547.6

181.01

LAUREL ST. EXT
Cont. from p-78

	23+2734-80. ft.		
10' Lt.	19.3	161.7	
£	16.9	164.1	
10' Rt.	15.6	165.4	
	23+50		
10' Rt.	24.2	156.8	
£	26.0	155.0	
10' Lt.	27.2	153.8	
	23+65		
10' Lt.	31.0	150.0	
£	28.9	152.1	
10' Rt.	27.2	153.8	
	23+75		
10' Rt.	25.9	155.1	
£	26.0	155.0	
10' Lt.	26.8	154.2	
	24+00		
10' Lt.	17.1	163.9	
£	13.7	167.3	
10' Rt.	11.0	170.0	
24+85 on £	9.0	172.0	
	24+25		
10' Rt.	2.0	179.0	
£	5.2	175.8	
10' Lt.	8.9	172.1	
	24+50		

181.01

40

10' Lt.	8.1	172.9	
£	3.5	177.5	
10' Rt.	+1.2	182.2	
	24+75		
10' Rt.	+2.7	183.7	
£	1.9	179.1	
10' Lt.	5.9	175.1	
	25+00		
10' Lt.	3.6	177.4	
£	+1.2	182.2	
10' Rt.	+5.4	186.4	
T.P. 12.74	192.29 / 46	179.55	
	25+25		
10' Rt.	3.4	188.9	
£	8.2	184.1	
10' Lt.	12.8	179.5	
	25+50		
10' Lt.	11.5	180.8	
£	8.1	184.2	
10' Rt.	3.5	188.8	
	25+75		
10' Rt.	2.8	189.5	
£	7.7	184.6	
10' Lt.	11.4	180.9	
	26+00		
10' Lt.	11.0	181.3	

192.29

2		7.2	185.0
10' Rt.		2.9	189.4
	26+25		
10' Rt.		0.0	192.3
2		5.0	187.3
10' Lt.		8.8	183.5
	26+50		
10' Lt.		7.7	184.6
2		3.3	189.0
10' Rt.		70.9	193.2
T.P.	12.56 201.83	3.02	189.27
	26+75		26+49
10' Rt.		13.0	188.8
2		16.6	185.2
10' Lt.		19.4	182.4
	27+00		
10' Lt.		23.9	177.9
2		22.1	179.7
10' Rt.		20.3	180.5
	37+15 - Bottom draw		
10' Rt.		26.3	175.5
2		27.8	174.0
10' Lt.		30.9	170.9
	27+25		
10' Lt.		29.2	172.6
2		23.6	178.2

20183

41

10' Rt.		24.6	177.2
	27+37.49 = EC.		
10' Lt.		18.6	183.2
2		17.6	183.2
10' Lt.		19.2	182.6
	27+70		
10' Lt.		5.7	196.1
2		4.0	197.8
10' Rt.		3.8	198.0
	27+80 = B.G. Lt.		
10' Rt.		11.7	203.5
2 on Hub		0.23	201.5
10' Lt.		3.7	198.1
T.P.	1315	214.75	0.23
	28+00		201.60
10' Lt.		15.1	199.6
2		10.7	203.0
10' Rt.		5.1	209.6
	28+25		
10' Rt.		1.3	213.4
2		6.9	207.8
10' Lt.		11.8	203.0
	28+50		
10' Lt.		9.1	205.7
2		4.2	210.5
10' Rt.		10.7	215.4

214.75

28+75		
10' Rt.	+1.0	215.8
L	4.1	210.6
10' Lt.	9.2	205.5

29+00		
10' Lt.	8.3	206.4
L	4.5	210.2
10' Rt.	+1.0	215.8

29+25		
10' Rt.	0.0	214.8
L	4.7	210.1
10' Lt.	8.7	206.0

29+50		
10' Lt.	7.6	207.2
L	3.3	211.4
10' Rt.	+1.7	216.5

29+75		
10' Rt.	+4.5	219.3
L	-0.5	214.2
10' Lt.	4.8	210.0

T.P.	11.22	224.77	1.20	213.55
------	-------	--------	------	--------

30+00		
10' Lt.	13.3	211.5
L	8.7	216.1
10' Rt.	4.1	220.7

30+25

224.77

30+25

10' Rt.	4.0	220.8
L	7.9	216.9
10' Lt.	12.6	211.2

30+50

10' Lt.	12.1	212.7
L	8.0	216.8
10' Rt.	3.9	220.9

30+75

10' Rt.	5.0	219.8
L	10.8	214.0
10' Lt.	13.7	211.1

31+00

10' Lt.	16.3	208.5
L	12.0	212.8
10' Rt.	7.4	217.4

31+25

10' Rt.	9.7	215.1
L	14.4	210.4
10' Lt.	18.8	206.0

31+35

10' Lt.	21.3	202.5
L	17.4	207.4
10' Rt.	14.0	210.8

31+48

10' Rt.	21.7	203.1
L	25.3	199.5

42

224.77

10' Lt.	29.6	195.2
31+75		
10' Lt.	18.1	206.7
↳	15.1	209.7
10' Rt.	10.7	213.1
31+88		
10' Rt.	6.3	218.5
↳	10.7	214.1
10' Lt.	14.1	210.7
32+00		
10' Lt.	15.1	209.7
↳	10.4	214.4
10' Rt.	5.8	218.0
32+50		
10' Rt.	5.1	219.7
↳	10.3	214.5
10' Lt.	14.7	210.1
33+00		
10' Lt.	12.8	212.0
↳	9.0	215.8
10' Rt.	4.0	220.8
33+21.24 = BC. Rt.		
10' Rt.	2.7	222.1
↳ on Hub	6.97	218.8
10' Lt.	11.1	213.7
33+50		

- 224.77

43

10' Lt.	7.1	217.7
↳	2.8	222.0
10' Rt.	11.3	226.1
T.P. 13.00	237.11 0.66	224.77
33+75		
10' Rt.	7.5	229.6
↳	9.8	227.3
10' Lt.	12.7	224.4
34+00		
10' Lt.	6.5	230.6
↳	5.5	231.6
10' Rt.	4.1	223.0
34+25		
10' Rt.	2.0	235.1
↳	2.8	234.3
10' Lt.	3.7	233.4
T.P. 6.51	241.65 1.97	235.14
34+50		
10' Lt.	6.2	235.4
↳	6.0	235.6
10' Rt.	5.7	235.9
34+75		
10' Rt.	5.4	236.2
↳	5.5	236.1
10' Lt.	5.6	236.0

24165
35+00

10' Lt.	5.5	236.1
↳	5.4	236.2
10' Rt.	5.4	236.2

35+12.39 = E.C.

10' Rt.	5.2	236.4
↳ on Hub	5.30	236.3
10' Lt.	5.2	236.4

35+(62.90)[?] = North edge exist. paving.

150' Rt. on Paving.	3.70	237.95
125' " " "	4.62	237.03
100' " " "	5.48	236.17
75' " " "	6.10	235.55
50' " " "	6.39	235.26
25' " " "	6.66	234.99
↳ " " "	6.64	235.01
25' Left " " "	6.38	235.27
50' " " "	5.83	235.82
75' " " "	5.40	236.25
100' " " "	4.82	236.83
125' " " "	4.26	237.39
150' " " "	3.56	238.09

TP 9.77 251.22 0.20 241.45

TP 1.00 248.17 4.05 247.17

chk. on BM. Page 37 13.81 234.36

234.33 = BM.
0.03 = Error

CROSS SECTIONS
 UNDER J.D.F.R.R. BRIDGE
 For Const. of Retaining Wall For EAST
 And West Road from Park Blvd.
 to Pershing Drive

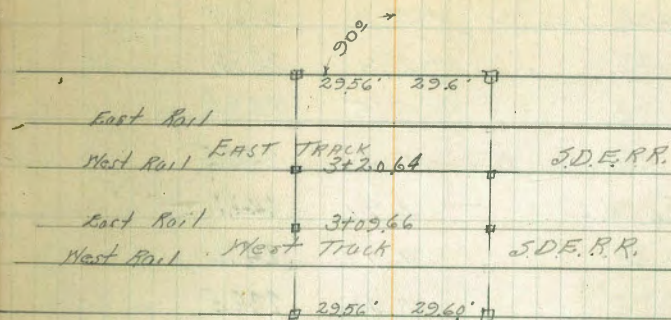
Refer. Conc. Sheet 7
 on Page 8
 Book 1447

3.36 266.97 263.61
 T.P. 3.45 257.66 12.76 254.21

2+90

2' Nat. Ground	2.9	249.8
5' Lt. on Fill	2.0	248.7
10' Lt. " "	10.1	247.6
16' Lt. " "	9.1	248.6
23' Lt.	11.2	246.5
29.6' Lt. " "	9.8	247.9
31' Lt. on Nat. Ground	9.3	248.4
36' Lt. " " "	6.4	251.3
37' Lt. " " "	4.7	253.0
41' Lt. " " "	2.0	255.7
56' Lt. " " "	+4.8	262.5
3+00		
57' Lt. on Natural Ground	+0.9	258.6
51' Lt. " " "	1.9	255.8
41' Lt. " " "	6.8	250.9
36' Lt. " " "	11.7	246.0
32' Lt. on Fill	14.0	243.7
29.6' Lt. on Conc. Pier	12.54	245.2
28' Lt. on Fill	14.9	242.8
23' Lt. " "	16.2	241.5
20' Lt. on North edge Con. Drain	17.2	240.5
17.4' " " Flood Lane " "	20.0	237.7

45



N ←
 257.66
 3+00 Cont.

14.8' Lt. on top South edge Con. Drain	17.0	240.7
9' " on Fill	15.2	247.5
T.P. 0.24	247.93	10.67
	246.99	
3+05		

on & Hub
 3+02.54

2' on Nat. Ground	0.3	247.63
7' Lt. on Fill	5.3	242.63
15.8' Lt. on Con. Drain	8.2	239.7
18.4' Lt. " & Flood Con. Drain	11.0	236.9
21.2' " " top " "	8.8	239.1
25.5' Lt. on Fill	7.2	240.7
29.6' on " "	6.9	241.0
33' Lt. on Nat. Ground	6.2	241.7
40' Lt. " " "	0.3	247.6
50' Lt. " " "	13.8	251.7
57' Lt. " " "	15.3	253.2

3+10

58' Lt. on Natural Ground	+5.9	242.0
48' Lt. " " "	+2.3	245.6
38' Lt. " " "	2.5	245.4
31.6' Lt. " Fill at Con Pier	7.4	240.5
31.6 " " Con. Pier	6.76	241.1
28.6 " " " "	6.76	241.1
28' Lt. " Fill	8.4	239.5
22.3' Lt. on edge Con. Drain	10.0	237.9
19.7 " " " " "	12.7	235.2
17.1 " " edge " "	9.8	238.1
9' Lt. on Fill	6.1	241.8
6 " Nat. Ground.	0.2	247.7

3+15

4 on Fill	0.7	247.7
3' Lt. " "	2.2	245.7
11' Lt. " "	7.1	240.8
14' Lt. on Bottom of Test Hole	10.2	237.7
18' Lt. " "	10.2	237.7
23' Lt. " Con Drain	11.4	236.5
29.6' Lt. " Fill	10.5	237.4
33' Lt. on Nat. Ground	10.1	237.8
42' " " " "	8.1	239.8
48' Lt. " " "	5.9	242.0
56' Lt. " " "	4.0	243.9

3+20

59' Lt. on Nat. Ground	6.7	241.2
------------------------	-----	-------

50' Lt. on Nat. Ground	8.4	239.5
38' Lt. " " "	11.7	36.2
31.6' Lt. on Fill at Pier	14.3	33.6
31.6 " " top " "	10.81	37.1
28.6 " " " "	10.81	37.1
28' Lt. on Fill at Pier	12.4	35.5
24.3' Lt. on top Con. Drain	12.8	35.1
21.7 Lt. on " "	15.4	32.5
18.9' Lt. on " "	12.5	35.4
15' Lt. on Fill	10.7	37.2
13' Lt. " " "	8.8	39.1
6' Lt. " " "	5.9	42.0
4 " " " "	0.8	47.1

3+25

4 on Fill	1.0	47.9
3' Lt. on Fill	3.5	44.4
13' Lt. " " "	10.1	37.8
20.2' Lt. on Con. Drain	13.9	34.0
22.9 " " " "	17.0	30.9
25.6 " " top " "	14.2	33.7
29.6 Lt. on Fill	13.1	34.8
38' Lt. on Nat. Ground	12.4	35.5
45' Lt. " " "	9.6	38.3
48' Lt. " " "	8.2	39.7
60' Lt. " " "	7.6	40.3

247.93

3 + 33.18 = East edge Con pier Section A-A		Book 1447-10	
58' Lt. on Fill	10.6	237.3	
54' Lt. on Natural Ground	12.5	35.4	
48' Lt. " " "	13.0	34.9	
7.P	1.94	237.12	12.75 235.18
45' Lt. on Nat. Ground.	3.2	33.9	
31.6' Lt. at Con. Pier.	4.9	32.6	
31.6' Lt. on Con "	3.98	33.1	
28.6 " " " "	3.98	33.1	
28' Lt. on Fill at Pier.	5.3	31.8	
27.4 Lt. on top Con Drain	5.3	31.8	
24.7 " " Flow " "	7.8	29.3	
22' Lt on top " "	5.0	32.1	
17' Lt. on Fill	2.6	34.5	
17' Lt. on ^{Nat. Ground.} Test Hole	5.2	31.9	
10' Lt. on Nat Ground.	+4.0	41.1	
5' " " " "	+7.1	44.2	
2 " " " "	+9.6	46.7	
3 + 44.5 = End of open Con. Drain			
2 on Natural Ground	+7.6	29.5	
3' Lt. on " "	+5.5	31.6	
10' Lt. " " "	+2.4	34.7	
16' Lt. " " "	2.6	34.5	
24.5' Lt. on top of Con. Drain	8.1	29.0	
27.2 " " Flow " " "	10.9	28.2	
30' Lt. on top " " "	8.2	28.9	

237.12

47

40' Lt. Nat. Ground	9.1	28.0
50' Lt. " "	10.2	26.9
62' Lt. " "	6.0	31.1

Change Alignment"
Continued from Page 75

Station Align. Defn. Δ True Curve Bearing Data

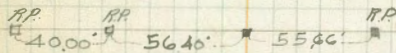
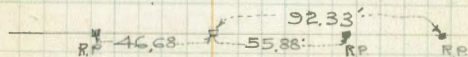
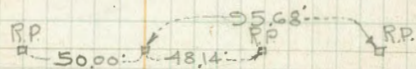
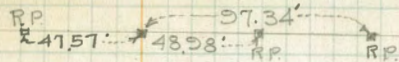
= 11 + 06.94	} EC.		
10 + 84.07	= EC.	3° 00.00'	
+ 75		2° 46.75'	$\Delta = 6° 00'$
+ 50		2° 11.00'	$R = 1200'$
+ 25		1° 35.25'	$L = 125.66'$
10 + 00		0° 59.50'	$ST = 62.89'$
+ 75		0° 23.75'	
9 + 58.41	= BC. Rt.		

115.58'

8 + 42.83	= EC.	3° 00.00'	
+ 25		2° 34.50'	$\Delta = 6° 00'$
8 + 00		1° 58.68'	$R = 1200'$
+ 75		1° 22.86'	$L = 125.66'$
+ 50		0° 47.04'	$ST = 62.89'$
+ 25		0° 11.22'	
+ 17.17	= BC. Lt.		

7 + 00

6 + 00



Walker
BHS
Diebst
Simmermeyer
12-24-70

GRADES and Curve Data

Pershing Drive

Note these stations are along the edge of paving to be constructed

LEFT Station	Left Defln. Δ	Left Grades	RIGHT Station	RIGHT Defln. Δ	RIGHT Grades
			Station of beginning of improvement, this curve is 10 feet	0° 00' 00"	
			①	3° 32' 35"	
			②	7° 05' 10"	
			③	10° 37' 45"	
			④	14° 10' 20"	
			⑤	17° 42' 55"	
			⑥	21° 15' 30"	
			⑦	24° 48' 05"	
			⑧	28° 20' 40"	
			⑨	31° 53' 15"	
				35° 25' 50"	
			⑩	EG. Widening Curve	

BC Widening Curve Curve 10 to 10 feet	Left Defln. Δ	Left Grades	BC Widening Curve Curve 10 to 10 feet	Defln. Δ
①	2° 13' 28"		①	2° 21' 57"
②	4° 26' 56"		②	4° 43' 54"
③	6° 40' 24"		③	7° 05' 51"
④	8° 53' 52"		④	9° 27' 48"
⑤	11° 07' 30"		⑤	11° 49' 45"
⑥	13° 20' 48"		⑥	14° 11' 42"
⑦	15° 34' 16"		⑦	16° 33' 39"
⑧	17° 47' 44"		⑧	18° 55' 36"
⑨	20° 01' 12"		⑨	21° 17' 33"
EG. Widening Curve ⑩	23° 14' 45"		EG. Widening Curve ⑩	23° 39' 30"

50

CURVE NO 2

Left Station	Left Defln. Δ	Left Grades
Station of beginning of widening curve = 0+20	1° 08' 45"	
+40	2° 17' 30"	
+60	3° 26' 18"	
+80	4° 35' 02"	
+100	5° 43' 48"	
+120	6° 52' 33"	
+140	8° 01' 19"	
+160	9° 10' 05"	
+180	10° 18' 50"	
+200	11° 27' 42"	
+220	12° 36' 21"	
+240	13° 45' 07"	
+260	14° 53' 54"	
+280	16° 02' 36"	
+300	17° 11' 24"	
+320	18° 20' 07"	
+340	19° 28' 55"	
+375 = EG	19° 54'	

CURVE NO 8

LEFT Station B.C. Widening Curve = ①	Left Defln. Δ	LEFT Grades	RIGHT Station B.C. Widening Curve = ⑩	Rt. Defln. Δ	Rt. Grades
①	3° 48' 40"		①	2° 32' 27"	
②	7° 27' 20"		②	5° 09' 54"	
③	11° 26' 00"		③	7° 37' 21"	
④	15° 14' 40"		④	10° 09' 48"	
⑤	19° 03' 20"		⑤	12° 42' 15"	
⑥	22° 52' 00"		⑥	15° 14' 42"	
⑦	26° 40' 40"		⑦	17° 47' 09"	
⑧	30° 29' 20"		⑧	20° 19' 36"	
⑨	34° 18' 00"		⑨	22° 52' 03"	
Widening Curve E.C. = ⑩	38° 06' 45"		⑩	25° 24' 30"	
			⑪	27° 56' 57"	
			⑫	30° 29' 24"	
			⑬	33° 01' 51"	
			⑭	35° 34' 18"	
			Widening Curve E.C. = ⑮	38° 06' 45"	

LEVELS on Exist. Pavng
IN Curve NO 2 to determine Grade
For edge Pavng in widening Curve

101.01

52

Dist. from
East Pavng
to Proposed Pav.

			NE. O.M.						
	12.37	80.44	68.07	B- 18th sts.	N		5.04	95.97	24.2'
TR	12.89	93.08	0.25	80.19	S		4.20	96.81	(94.95)
TR	6.71	99.71	0.08	93.00		Part 6 = 1+20			
TR	6.01	101.01	4.71	95.00	N		5.17	95.84	26.6'
	JEG on E.C. Widening Curve No 1				S		4.37	96.64	(94.78)
N		7.09	93.92			Part 7 = 1+40			
S		7.53	93.48		N		5.56	95.45	28.1'
	B.C. Widening Curve No 2				S		4.77	96.24	(94.33)
N		5.93	95.08	10' Elev. in circles = Proposed Pavng on North		Part 8 = 1+60			
S		5.89	95.12	(95.08)	N		5.98	95.03	28.3'
	PART 1 = 0+20				S		5.16	95.85	(93.87)
N		5.68	95.33	10.5'		2+00			
S		5.62	95.38	(95.33)	N		6.33	94.68	27.3'
	Part 2 = 0+40				S		5.57	95.44	(93.56)
N		5.28	95.73	11.6		+20			
S		5.26	95.75	(95.73)	N		6.68	94.33	25.2'
	Part 3 = 0+60				S		5.87	95.14	(93.31)
N		5.28	95.73	13.6		2+40			
S		4.87	96.14	(95.47)	N		6.97	94.04	21.3'
	Part 4 = 0+80				S		6.10	94.91	(93.11)
N		5.15	95.86	16.6'		2+60			
S		4.51	96.50	(95.33)	N		7.13	93.88	17.5'
	Part 5 = 1+00				S		6.40	94.61	(93.24)
N		5.04	95.97	20.5		2+80			
S		4.18	96.83	(95.09)	N		7.16	93.85	14.6'
					S		6.63	94.38	(93.16)

10/01

53

Dist. from Exist.
Paving to Proposed
Paving.

3+00

N	7.20	93.81	12.3
S	6.89	94.12	93.62

+20

6.89

N	7.29	93.72	10.8
---	------	-------	------

S	7.15	93.86	93.64
---	------	-------	-------

3+97.12 = EC.

N	7.48	93.53	10.1
---	------	-------	------

S	7.37	93.64	93.43
---	------	-------	-------

Slope And Grade Stakes
CURVE NO 2

+20
2+00
+80
+60
+40
1+20
1+00
+80
+60
+40
+20
0+00 = BC of Widening Curve
11.46 106.46
π
25.00

LEFT GRADE
edge Prepared Berms

54

93.30 13.2
13.16 5.2
-7.8
15.6 Back of Berm.
93.53 12.9
17.93 7.9
17.1 Back Berm.
93.87 12.6
12.59 9.0
-1.8
10.8 Back Berm.
94.35 12.1
11.1 3.9
-1.2
10.7 Back Berm.
94.73 11.7
11.73 4.6
-1.7
10.2 Back Berm.
95.04 11.4
11.42 7.4
-1.2
10.1 Back Berm.
95.27 11.2
11.19 4.3
-1.2
10.0 Back Berm.
95.41 11.0
11.05 4.0
5' to toe slope
95.46 11.0
10.9 10' Back Preparation
95.38 11.0
10.8 10' Back "
95.22 11.0
11.24 11' Back
95.08 11.0
11.38 10' Back
-1.97

Finish stakes

95.02 = π
95.14 = BM on road
BC Widening Curve NO 2
100.02 = π
106.46
24.41 = E.M. 0+00 to 10' back
95.08 95.22 95.38 95.46 95.41
4.74 4.80 4.84 4.88 4.61
4.83 5.00 4.99 4.78 4.31
4.011 -0.20 -0.35 -0.22 4.825
100.02 = π
106.46

Elev. Grading Near EC. Curve No 1
Locust 94.07 = Prepared top Grading
23.57 = " " Grading
6.95 = 94.07
6.95
105.0201

14732-EC.

120

3 + 00

780

160

2 + 10

2343
13031303
1238
65

5' Back. Barn

2350
1296130
121
9

5' Back. Barn

2350
1296130
121
9

5' Back. Barn

2340
1306131
123
8

5' Back. Barn.

2325
1321132
120
12

5' Back. Barn.

2320
1376133
129
4

9' Back of Barn

2343
659
121
-0.622350
652
121
-0.602350
652
121
-0.812340
662
121
-0.312320
682
121
-0.402320
682
121
+0.37

Finish at 7:45

106.46

LEVELS ON CURVE NO 5
 ON EXISTING PAVING TO DETERMINE
 GRADE FOR EDGE PAVING OF WIDENING CURVE
 ON NORTH SIDE

Station	Offset	Existing Elev.	Prop. Pav. Elev.	Cuts & Fills
BC Widening Curve 27.41				
J	} 20' South 20' from N on to EC.	9.62	87.72	
N		10.08	87.33	
+19.3 - Proposed Pav				
on 10' offset		10.85	86.89 } 86.89	-0.33
Part 1				
S		8.80	88.61	
N		9.57	87.84	
+23 - Proposed Pav				
on 10' offset		10.24	87.17 } 86.95	+0.22
Part 2				
S		7.71	89.70	
N		8.60	88.81	
+27.6 - Proposed Pav.				
on 10' offset		9.31	88.10 } 87.55	+0.55
Part 3				
S		6.13	91.28	
N		7.06	90.35	
+31.2 - Proposed Paving				
on 10' offset		7.84	89.57 } 88.91	+0.66
Part 4				
S		3.44	93.37	
N		4.32	93.09	
+30 - Proposed Pav				
on 10' offset		6.51	90.90 } 91.60	-0.70

56

Elev Stake D on P-38 = $\frac{87.38}{19.13} + 97.41 - X$

Part 5

S		0.16	97.25		
N		1.20	96.20		
+26.4	-Proposed Pav.		94.82	}	-1.48
on 10' offset stake		4.07	93.34		
T.P.	12.79 109.99	0.21	97.20		

Part 6

S		9.80	100.19		
N		10.60	99.39	}	+0.50
+12.9'	-Proposed Pav.		98.59		
on 10' offset stake		11.47	98.52	98.59	-0.07

Part 7

S		7.03	102.96		
N		7.62	102.37		
+12.3'	-Proposed Pav.		102.00	}	+1.05
on 10' offset		9.04	100.95		
					-1.05

Part 8

S		4.69	105.30		
N		4.96	105.03		
+5.8'	to proposed pav.		104.94	}	+0.98
on 10' offset		6.03	103.96		
					-0.98

Part 9

S		2.49	107.50		
N		2.44	107.55		
+1.4'	to proposed Pav.		107.55	}	+0.11
10' offset stake		3.15	106.84		
					-0.71

Cuts & Fills.

9741

T.P. 8.96 103.22 3.15 94.26

Part 10

109.99

T.P. 8.96 115.80 3.15 106.84

Part 10 = EC Widening Curve

S 5.86 109.94

N 5.72 110.08

+ 0.0 on Pos. 110.08

10' offset. 5.91 102.89 } 110.08 - 0.19

chk. on Grating on W 6.03 109.77

Book 1405-16

109.74
0.03 = Error.

58

90.61

S		5.48	85.13
+27.6			84.78
N	2+11.75 = Δ	4.78	85.83
S		5.38	85.23
+28.2			84.82
N	2+25	4.76	85.85
S		5.36	85.25
+28.2			84.86
N	2+50	4.78	85.83
S		5.37	85.24
+28.4			84.92
N	2+75	4.69	85.92
S		5.34	85.27
+27.6			85.05
N	3+00	4.72	85.82
S		5.20	85.41
+25.7			85.28
N	3+16	4.69	85.92
S		5.14	85.47
+24.2			85.40

90.61

60

		3+36	
N		4.54	86.07
S		4.76	85.85
+			85.86
		3159 = BC on Rf.	
N		4.36	86.25
S		4.36	86.25
+18'			86.15
		3845	
N		4.28	86.33
S		4.29	86.32
+14.5			86.20
		4+11	
N		4.22	86.39
S		4.22	86.39
+11.5			86.26
		4+37.5	
N		4.18	86.43
S		4.18	86.43
+8.5			86.37 ✓

Miller
8-15
Robert
8-31

LEVELS For Curve No 8
to determine Grade on Mt. in widening
Curve { Curve in 15 Part see p. 5 }

540 231.20 10.42 225.80
Left BM. on No. 1 B.C. Widening Curve on Lt. 220.78 see p. 37
B.M. Nails in
North end Fence
Post Book 145-28

B.C. Widening Curve on Mt.

Lt. on Pav. 14.13 217.07
Rt. " " 14.14 217.06
+ 10' = Proposed Pav 217.06
on 10' offset stake 14.16 217.04 } - 0.02

Part 1

Lt. 13.16 218.04
Rt. 13.29 217.91
+ 11.4' to Proposed Pav. 217.77
on 10' offset 13.18 218.02 } + 0.25

Part 2

Lt. 12.23 218.97
Rt. 12.59 218.61
+ 15' to Proposed Pav. 218.30
10' offset 10.04 221.16 } + 2.86

Part 3

Lt. 11.12 220.08
Rt. 11.04 219.36
+ 21.10' to Proposed Pav. 218.60'
10' offset 9.01 222.19 } + 3.59

Part 4

Lt. 9.70 221.50
Rt. 10.85 220.35

331.20

62

+ 30' to Proposed Par.	218.94	} + 6.12
10' offset	6.14 225.06	

Part 5

Lt.	8.67	222.53	
Rt.	9.87	221.33	
+ +36.6 to Proposed Par.		219.47	} +4.46
10' offset	7.27	223.93	

Part 6

Lt.	7.68	223.52	
Rt.	8.84	222.36	
+ 40.4' to proposed Par.		220.12	} +5.37
10' offset.	5.71	225.49	

Part 7

Lt.	6.61	224.59	
Rt.	7.80	223.40	
+ 42.3' to proposed Par.		220.94	} +4.41
10' offset	5.85	225.35	

Part 8

Lt.	5.42	225.78	
Rt.	6.62	224.58	
+ 40.9' to proposed Par.		222.20	} +2.38
10' offset	6.02	225.18	

PART 9

Lt.	4.15	227.05	
Rt.	5.28	225.92	
+ 35.5' to proposed Par.		223.90	} +2.02
10' offset	5.28	225.92	

231.20

Part 10

Lt.	2.99	228.21	
Rt.	4.00	227.20	
+28.5 to proposed Piv.		225.75	} +1.81
10' offset	3.64	227.56	

PART 11

Lt.	1.72	229.48	
Rt.	2.59	228.61	
+19.6 to proposed Piv.		227.77	} +0.77
10' offset	2.66	228.54	
T.P.	8.51	238.99	0.72 230.48

Part 12

Lt.	8.41	230.58	
Rt.	8.94	230.05	
+11.1 to proposed Piv.		229.75	} +0.50
10' offset	8.74	230.25	

Part 13

Lt.	7.28	231.71	
Rt.	7.53	231.46	
+5' to proposed Piv.		231.35	} +0.81
10' offset	6.83	232.16	

Part 14

Lt.	6.18	232.81	
Rt.	6.11	232.88	
+12'		232.86	} +0.91
10' offset	5.22	233.77	

~~231.20~~

238.99

63

PART 15 = E.C.

Lt.	1.80	234.19	
Rt.	4.77	234.22	
+00		234.22	} +0.74
10' offset	4.03	234.96	
Left B.M. E.C. this curve in nail & Exact Piv.	4.66	234.33	See p37
chk. Left edge Piv. 48' 22.26	4.62	234.37	
Book 1405-30		234.36	0.01 = Error.

"ALIGNMENT"
LAUREL STREET EXTENSION

See Book 1447-P-69
for final align.

64

Walker
Brooks
Cluett
Nelson
3-21-32

"ALIGNMENT"
LAUREL STREET EXTENSION

Station Align. Defln. Δ True Bearing Curve Data

+33.77=B.C.

5 + 00

$\Delta = 58^{\circ} 30'$

$\frac{L}{R} = 2.00'$

$L = 204.20$

4 + 00

ST = 112.0'

+35.57=B.C. RT.
53.03'
+02.54=E.C.

Alignment Changed
See Page 75

$R = 100'$

$\Delta = 81^{\circ} 30'$

$L = 142.25'$

ST = 86.17'

3 + 00

2 + 00

+60.30=B.C. RT.
75.05'

1 + 00

+85.25=E.C.

$\frac{L}{R} = 63'$

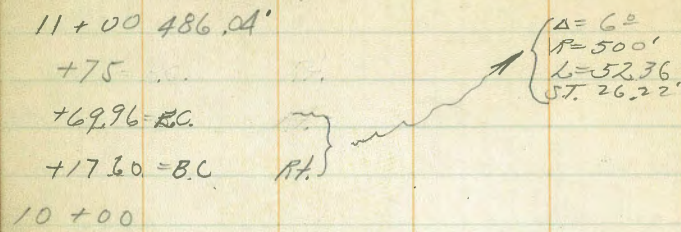
$L = 85.25$

$\Delta = 77^{\circ} 32'$

0 + 00=B.C. Lt.

ST = 50.59'

Station	Align.	Defln.	True Bearing	Curve Data
11+00		486.04'		$\Delta = 62^\circ$ $R = 500'$ $L = 52.36'$ $ST = 26.22'$
+75				
+69.96	B.C.			
+17.60	B.C.			



182.38'

9+00

8+35.22 = B.C.

+2.5

8+00

+75

+69.77 = B.C.

St.

$\Delta = 7^\circ 30'$

$R = 500'$

$L = 65.45'$

$ST = 32.77'$

7+00

6+00

Station	Align.	Deflin. Δ	True Bearing	Curve Data	chords		
					30' L	2	30' R
+75		11° 21.84'		$\Delta = 52.30$	22.49'	25.00'	27.51'
+50		8° 58.60'		$L R = 300'$	"	"	"
+25		6° 35.35'		$L = 274.89'$	"	"	"
16 + 00		4° 12.11'		$ST = 147.94'$	"	"	"
+75		1° 48.87'		"	"	"	"
15 + 56 = B.C.		Lt.			17.10'	19.00'	20.90'

92.00' 24' 25'

297.

+02 = P.O.T.

15 + 00

14 + 00

13 + 00

12 + 00

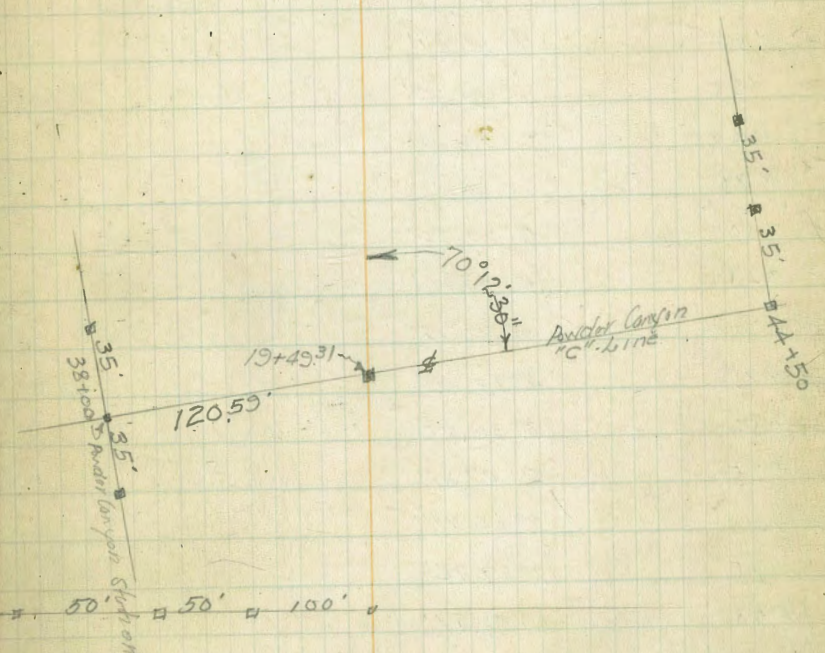
Station	Align.	Defln. Δ	True Bearing	Curve Data
+21.36	=E.C.	18° 30'		
22+00		16° 27.74'		
+75		14° 04.48'		
+50		11° 41.22'		
+25		9° 17.96'		$\Delta = 372.00'$
21+00		6° 54.70'		$2R = 300'$
+75		4° 31.44'		$L = 193.73'$ $\gamma 9^{\circ} 06'$
+50		2° 08.18'		$ST. 100.38'$

+27.63 B.C. Lt.
 — See Page 72 for align. ahead

20+00
 185.11
 +49.31 = Intersection Powder House Canyon "C"-Line B-1355-79

19+00

Station	Align.	Defln. Δ	Chords
+30.89	=E.C.	26° 15'	30' 24' 80'
18+00		23° 18.04'	2778 3087 3336
+75		20° 54.80'	2249 2500 2751
+50		18° 31.56'	" " "
+25		16° 08.32'	" " "
17+00		13° 45.08'	" " "



Station	Align.	Defln. A	True Bearing	Curve Data.
27 + 80	= B.C.	Lt.		
		42.51		
+37.49	= B.C.	11° 45'		
+25		11° 23.52'		
27 + 00		10° 40.55'		
+75		9° 57.58'		
+50		9° 14.61'		
+25		8° 31.64'		
26 + 00		7° 48.67'		
+75		7° 05.70'		
+50		6° 22.73'		
+25		5° 39.76'		
25 + 00		4° 56.79'	$\Delta = 23^{\circ} 30'$	
+75		4° 13.82'	$R = 1000'$	$5^{\circ} 43.76'$
+50		3° 30.85'	$L = 410.15'$	
+25		2° 47.88'	$ST = 208.00'$	
24 + 00		2° 04.91'		
+75		1° 21.94'		
+50		0° 38.97'		
+27.34	= B.C.	Rt.		

Abandoned
see p. 12

23 + 00

105.98

Station Align. Defln. Δ True Curve Bearing Data

+25 0°44.47'

+21.24 = B.C. H.

33 +00

169.49'

32 +00

~~Abandoned~~
See p. 72

+51.75 = F.C. 17°45'

+50 17°39.83'

+25 16°28.22'

31 +00 15°16.61'

+75 14°05.00'

+50 12°53.39'

+25 11°41.78'

30 +00 10°30.17'

+75 9°18.56'

+50 8°06.95'

+25 6°55.34'

29 +00 5°43.73'

+75 4°32.12'

+50 3°20.51'

+25 2°08.9'

28 +00 0°57.29'

$\Delta = 35^{\circ}30'$
 $R = 600$ 9°33'
 $L = 871.55$
J.T. 192.06

Station Align. Defln. Δ True Bearing Curve Data

~~Abandoned~~
see p. 72

+42.90 = North edge exist. Perishing.

20.51'

+12.39 = E.C.

37° 46'

35 + 00

35° 19.02'

$\Delta = 75^\circ 32'$

+75

30° 22.67'

$R = 145'$

+50

25° 26.32'

$L = 191.15'$ $39^\circ 31'$

+25

20° 29.97'

$ST = 112.34$

34 + 00

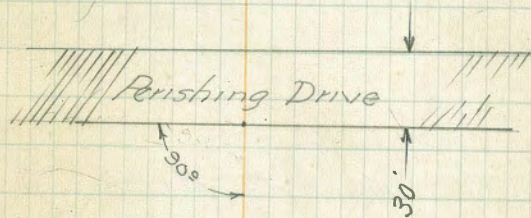
15° 33.62'

+75

10° 37.27'

+50

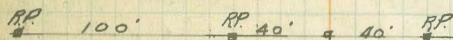
5° 40.92'



Walker
A-32

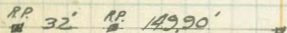
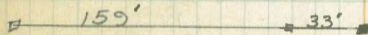
"Change in Alignment"
from Station 20+24.71 to 35+33.08

Station	Align	Defln. Δ	True Bearing	Curve Data	Chords
+50		0°26.6'			159' 154' 150'
23+34.54	=B.C.		RT		



110.86'

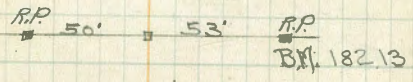
+23.68	=E.C.	19°00'			
22+00		16°44.1'		Δ = 38°	213' 236' 260'
+75		14°20.9'		LR = 300'	224' 250' 274'
+50		11°57.7'		LL = 198.97'	
+25		9°34.5'		LS = 107.30'	
21+00		7°11.3'			
+75		4°48.1'			
+50		2°24.9'			
20+24.71	=B.C.		LT		227' 252' 278'



19+49.31 P. Ho. Canyon - Sta. 19+49.31

18+30.89 = E.C.

Station	Align.	Defln. Δ	True Bearing	Curve Data	chords 30' Lt & Rt
+25		5° 23.84'		$\Delta = 31^\circ$	2399' 2500' 2607'
29+00		4° 22.46'		$R = 700'$	" " "
+75		3° 21.08'		$L = 378.74'$	" " "
+50		2° 19.68'		$ST = 194.12'$	" " "
+25		1° 18.30'			" " "
28+00		0° 16.92'			2399' 2500' 2607'
27+93.11 = BC	LT.				660' 690' 720'
+75					
+50	57.14'				30' Lt & 30' Rt
+35.97 = EC	11° 30'				1129' 1097' 1064'
+25	11° 11.6'				2575' 2500' 2425'
27+00	10° 28.6'				" " "
+75	9° 45.6'				" " "
+50	9° 02.6'				" " "
+25	8° 19.6'				" " "
26+00	7° 36.6'			$\Delta = 23^\circ$	" " "
+75	6° 53.6'			$R = 1000'$	" " "
+50	6° 10.6'			$L = 401.93'$	" " "
+25	5° 27.6'			$ST = 203.45'$	" " "
25+00	4° 44.6'				" " "
+75	4° 01.6'				" " "
+50	3° 18.6'				" " "
+25	2° 35.6'				" " "
24+00	1° 52.6'				" " "
23+75	1° 09.60'				" " "



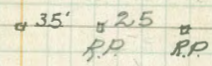
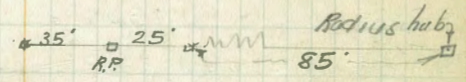
Stations Align. Defln Δ ^{True} Bearing Curve Data

35+33.98 = North edge Exst. Paving.

2.143

Chords
30' Lt. & Rt.

+11.65 = E.C.	36° 17.5'	
35+00	33° 59.17'	$\Delta = 72^{\circ} 35' 11.67'' 1164' 928''$
+75	29° 02.82'	$L.P. = 145' 31.13'' 2497' 1960''$
+50	24° 06.47'	$L.L. = 183.69'$
+25	19° 10.12'	$J.T. = 106.48'$
34+00	14° 13.87'	
+75	9° 17.52'	
+50	4° 21.17'	
33+27.96 = B.C. Pt.		2656 2290 1745
33+00		
+75 156.11'		
+50		
+25		
32+00		
+71.85 = E.C.	15° 30'	2191' 2185' 2286
+50	14° 36.3'	2379' 2500' 2607
+25	13° 34.8'	
31+00	12° 33.5'	
+75	11° 32.1'	
+50	10° 30.8'	
+25	9° 29.4'	
30+00	8° 28'	
+75	7° 26.60'	
29+50	6° 25.22'	



Walker
4-20-32

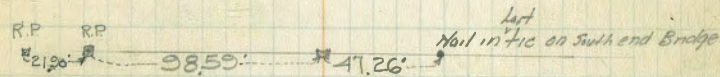
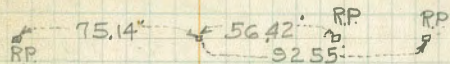
"Change Alignment"
Between Station 1+50.74
And 8+06.21
Defln. True Curvs
Bearing Data

45

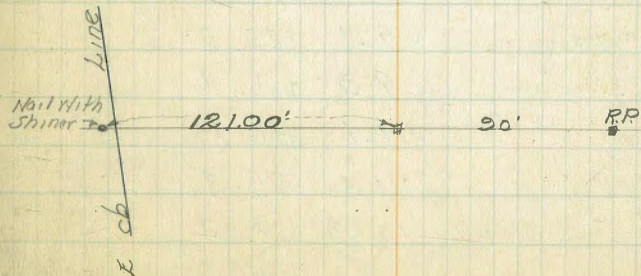
Station Align.

Continued Page 48

Station	Angle	Chords
5+48.55 = E.C.	25° 30.00'	30' Lt. 26.35' 23.54' 20.74'
+25	22° 48.67'	Δ = 51° 00'
5+00	19° 57.87'	LR = 251.58' 28.00' 24.99' 22.00'
+75	17° 07.07'	L = 223.94' " " "
+50 = P.O.C.	14° 16.27' <small>200.60.24</small>	LR = 120.00' " " "
+25	11° 25.47'	" " "
4+00 = P.O.C.	8° 34.67'	" " "
+75	5° 43.87'	" " "
+50	2° 53.07'	" " "
3+24.61 = B.C. Rt.		28.34' 25.82' 22.35'
21.15'		
3+03.46 = E.C.	43° 45.0'	18' Lt. 33.47' 28.37' 23.26'
+75	35° 35.8'	Δ = 87° 30' 29.42' 24.93' 20.44'
+50	28° 26.1'	LR = 100' " " "
+25	21° 16.4'	LR = 152.72' " " "
2+00	14° 06.7'	LR = 95.75' " " "
+75	6° 57.00'	" " "
1+50.74 = B.C. Rt.		29.55' 24.20' 19.81'
0+85.25 = E.C.		



Cross on Steel span 41.60' 120' Cross on top of Con. Pier



March 22-32
Walker

LEVELS
LAUREN ST. EXT.

6

BM. P. 79

	6.96	258.07		251.11
3+35.57=BC. Pt. 58 ³⁰ .			12.6	245.5
+50			11.8	246.3
+75			10.9	247.2
4+00			12.2	245.9
+25			10.2	247.9
+50			8.0	250.1
+68			3.1	255.0
5+00			9.0	249.1
+25			12.0	246.1
+39.77=K.C.			13.2	245.9
+50			12.6	245.5
T.P. 1.06	246.80		12.33	245.74
6+00			7.0	239.8
+50			11.3	235.5
T.P. 1.62	235.87		12.55	234.25
7+00			2.2	233.7
+50			5.0	230.9
+69.77=BC. Pt. 7 ³⁰ .			7.1	228.8
8+35.22=K.C.			9.3	226.6
+50			9.1	226.8
9+00			11.4	224.5
T.P. 3.05	226.29		12.63	223.24
+50			5.2	221.1
10+00			10.0	216.3

226.29

10+17.60 B.C. Rt 6:00	12.2	214.1	
T.P. 4.29 218.00	12.58	213.71	
10+69.9% = E.C. on hub	7.11	210.9	
11+00	9.9	208.1	
T.P. 0.80 205.95	12.85	205.15	
11+50	5.0	200.9	
12+00	12.7	193.2	
+50	20.8	185.1	
+75	32.8	183.1	
(2+15) 10 Lt. of L	35.4	170.5	
13+00	21.3	184.6	
+35	15.6	190.3	
T.P. 0.67 194.05	12.57	193.38	
13+50	3.3	190.8	
14+00	7.0	187.1	
+13	7.6	186.4	
T.P. 0.12 182.16	12.01	182.04	
+50	3.1	179.2	
+75	5.6	176.6	
15+02 = P.U.T. on Hub	8.85	173.3	
+13	11.0	171.2	
T.P. 0.25 169.57	12.84	169.32	
T.P. 0.17 157.09	12.65	156.92	
15+56 = B.C. on Hub	8.58	148.51	
49' Rt.	8.4	148.7	edge ditch.
15+75			
L	13.9	143.1	
44' Rt.	10.6	146.5	edge ditch.

157.09

0.50	144.93	12.66	144.43
	16+00		
L		4.1	140.8
28' Rt. - edge ditch		1.4	143.5
	16+25		
L		6.7	138.2
28' Rt. edge ditch		3.5	141.4
16+37 L edge bridge path		6.4	138.5
+38 L " " "		7.8	137.1
16+50		9.3	135.6
31' Rt. 16+50 - edge ditch		6.4	138.5
16+75		11.9	133.0
17+00		14.1	130.8
+25		15.5	129.4
+50		17.0	127.9
17+75		18.2	126.7
+80 = edge channel		18.2	126.7
+81 = Bottom "		20.5	124.4
18+00 " "		21.5	123.4
+01 top "		20.0	124.9
+25		17.9	127.0
+50		19.0	125.9
+61		20.5	124.4
19+00		17.2	127.7
+25		13.3	131.6
+50		11.3	133.6

19+82		12.0	132.9	
+90		16.1	128.8	
20+16	channel	18.0	126.9	
+25	400 Bank of channel	15.5	129.4	
+50		13.9	131.0	
+75		11.3	133.6	
21+00		6.7	138.2	
+25		0.0		
T.P.	12.02 156.06	0.89	144.04	on Rock.
21+50		2.2		Line change See Cont. below
T.P.	13.09 168.51	0.64	155.42	
21+75		6.8		
22+00		2.5		
	+09.73 = E.C. on hub.	2.06	166.45	
	0.03 144.07		144.04	Above T.P. on Rock.
	on G. hub 38+00 8-1355-78	8.69	135.4	
20+27	63 = B.C. Lt.	14.8	129.2	
+50		13.0	131.0	
+75		10.3	133.7	
21+00		5.8	138.2	
T.P.	12.2 145.26	0.03	144.04	Above Rock.
	G. Hub station 39+50			
chk. on	8M. Book 1355-64	13.13	132.13	
	1303 144.95		131.92 = corrected	
21+25		0.0	145.0	
T.P.	13.13 156.86	1.22	143.73	

21+50				
10' Lt.		5.6		151.2
↳		2.2		154.6
10' Rt.		+2.2		159.0
T.P.	12.50	168.63	0.73	156.13
21+75				
10' Rt.		0.2		168.4
↳		5.0		163.6
10' Lt.		9.5		159.1
22+00				
10' Lt.		4.7		163.9
T.P.	12.87	181.01	0.29	168.34
↳		11.7		169.3
10' Rt.		5.4		175.6
22+21.36 = E.C.				
10' Rt.		6.0		175.0
↳ on Hub		11.12		169.9
10' Lt.		15.9		165.1
22+50				
10' Lt.		14.6		166.4
↳		9.4		171.6
10' Rt.		3.6		177.4
23+00				
10' Rt.		4.5		176.5
↳		8.3		172.7
10' Lt.		13.0		168.0

Cont. on P-40

Walker
3-21-32

"BENCH MARKS"
LAUREL ST. Extension

79

	2.52	295.94		293.42	BM. on top Pine Hub in front Canadian Legion
T.P.	2.92	287.78	11.08	284.86	
T.P.	2.12	277.24	12.66	275.12	
T.P.	0.85	265.15	12.94	264.30	
T.P.	0.94	253.44	12.65	252.50	
T.P.	0.07	251.18	2.33	251.11	on Pine Hub 15' RT. 5+59.77
T.P.	1.12	239.42	12.88	238.30	on 2 Hub
T.P.	4.60	233.40	10.62	228.80	7+69.77-8C
T.P.	0.57	221.38	12.79	220.61	on 2 Hub
T.P.	8.29	218.00	11.67	209.71	10+75 on ST.
T.P.	0.80	205.95	12.85	205.15	

DIRECTIONS FOR USE OF TABLES

86.97
 10.66 +
 9743.7
 1013
 7.30

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 1/2 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body

IMPROVED TABLES

AND

INFORMATION

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given T may be found by dividing tangent (or external), opposite T by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

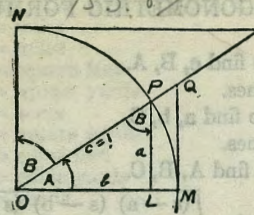


TABLE II
TRIGONOMETRIC FORMULÆ.

$$\angle A = \angle MOP \quad \angle B = \angle PON = \angle OPL$$

$$R = OB = c = 1$$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

$$\sin \frac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \quad \cos \frac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \quad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Lines} \quad \frac{\sin A}{a} = \frac{\sin B}{b} = \frac{\sin C}{c}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$$

140.00
 .383
 136.17
 290.00
 153.83
 1239
 2238
 42.70 ✓
 1172
 1728
 29.00

22
466
333
732

2250 crab bed

126
118
138

237 1/2
28
349

1275
10200
8950

1875

33318
119
344.5

2417
3196
521

13

2417
3196
1310
111
1206



049076

20
23
47
31
4.2

174
26
148

296
73
223

296
225
71

99
78
127

296
53
243

15.00
10.84
4.16

29.6
9.8
20.2

20.00
4.16
15.84

-
-