

1398.

College Way Ext.

by Chas. Walker 1899.



ENGINEERING DEPARTMENT,
SAN DIEGO,
CITY OF CALIFORNIA.

1398

MICROFILMED

DEC 23 1964

Our Leather Bound Engineers Note Books are carried in the following rulings:

- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
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- No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.
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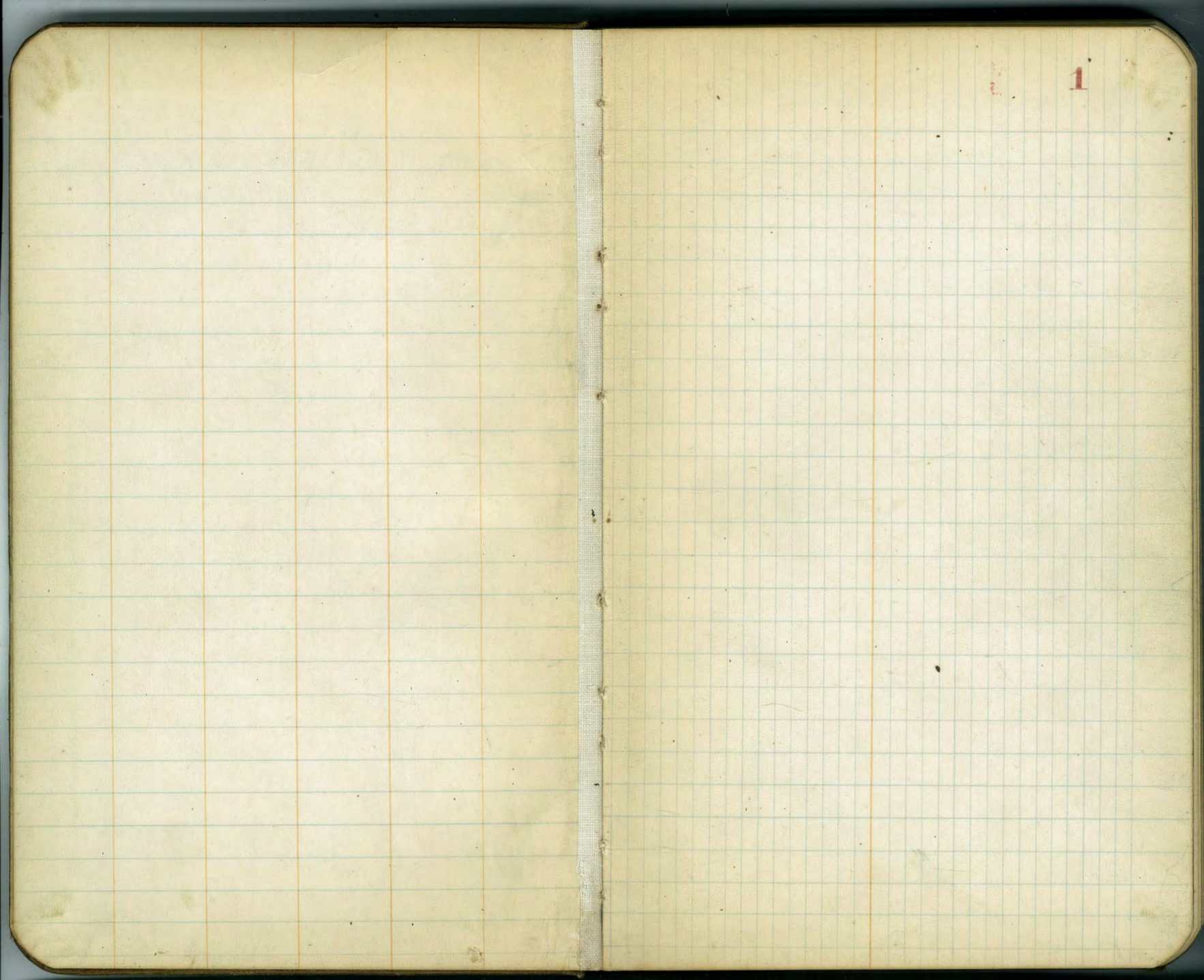
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THE FREDERICK POST CO.
ENGINEERING and DRAFTING SUPPLIES
IRVING PARK STATION
CHICAGO, ILL.

Index

Alignment **COLLEGE WAY EXT.** . 2-18

± Levels College Way Ext. ^{El Cajon Ave.} _{to} Lemon Grove Blvd. 21-26



1

Station	Align.	Def'n.	True Bearing	Curve Data	Magnetic Bearing
+50			5°23.63'		
11+00			4°40.66'		
+50			3°57.69'		
10+00			3°14.78'	$\Delta = 25^{\circ}01'40''$ $R = 2000'$	
+50			2°31.75'	$S.T. = 443.90'$ $L = 873.63'$	
9+00			1°48.78'		
+50			1°05.81'		
8+00			0°22.84'		
+73.40	B.C.		bt.		
7+00					
			773.40'		
6+00					

Station	Align.	Def'n.	True Bearing	Curve Data	Magnetic Bearing
		1259.85'			
17+00					
	+47.93 = E.C.	1230.83'			
16+00		1150.36'			
	+67.81 = P.O.S.T.				
	+50	1107.59'			
15+00		1024.42'			
	+50	941.45'			
14+00		858.48'			
	+50	815.51'			
13+00		732.54'			
	+50	649.57'			
	+17.3 P.I.				
12+00		606.60'			

Station	Align.	Defln.	True Bearing	Curve Data	Magnetic Bearing
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24+00

23+00

1253.85

22+00

21+00

20+00

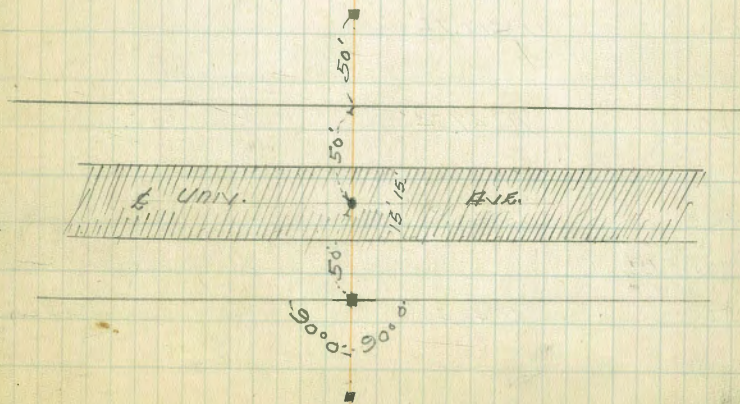
19+00

+22.75 = P.O.T.

18+00

Station	Align.	Defln.	True Bearing	Curve Data	Magnetic Bearing
	+00. ⁰⁴ P.I.			A = 5° 30'	
30+00		1° 30.03'		R = 3000'	
				L _s = 186.17'	
+50		0° 37.06'		ΔT = 93.16'	
+06. ⁸⁸ = B.C.		Rt.			
29+00					
28+00					
		1° 59.85'			
27+00					
26+00					
25+00					
	+68.02 = P.O.T.				

Station	Align.	Defth.	True Bearing	Curve Data	Magnetic Bearing
+50		10°45.56'			
36+00		9°15.14'		$\Delta=55^{\circ}30'$ $R=250.34$	
+50		7°44.72'		$ST=500'$ $L=989.55'$	
35+00		6°14.30'			
+50		4°43.82'			
34+00		3°13.40'			
+50		1°42.98'			
33+00		0°12.56'			
+9395=B.C.		Lt.			
32+00					
+9395					
		200.00'			
+43.05					
31+00					
+9395=E.C.		2°40'			
+50		2°03.0'			



Station	Station	Align.	Def'n	True Bearing	Curve Data	Magnetic Bearing
+50		715.99'				
36+00	+13.60 = E.S.C.		27°45.00'			
	43+00		27°20.28'			
+50	+50		25°49.86'			
35+00	41+00		24°19.44'			
+50	+50		22°49.02'			
34+00	40+00		21°18.60'			
+50	+50		19°48.18'			
33+00	+93.39+00		18°17.76'			
	+50		16°47.34'			
32+00	+93.38+00		15°16.82'			
	+93.25 = P.I.					
+43	+50		13°46.40'			
31+00	+93.37+00		12°15.98'			
+50						

Station	Align	Def'n.	True Bearing	Curve Data	Magnetic Bearing
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49+00

48+00

47+00

715.99'

46+00

45+00

44+00

43+00

Station	#197	Defln.	True Bearing	Curve Data	Magnetic Bearing
55+00		18°10.41'			
	7388-12				
+50		16°34.92'			
54+00		14°59.42'			
+50		13°23.93'			
53+00		11°48.44'		A=28°13'40"	
				R=900'	
+50		10°18.94'		ST. 544.83	
				L=979.04	
52+00		8°37.43'			
+50		7°00.94'			
51+00		5°25.45'			
+50		3°43.76'			
50+00		2°14.47'			
+50		0°38.78'			
	7397-8C	154.			

Station	Align.	Defln.	True Bearing	Curve Data	Magnetic Bearing
61+00					
		609.28'			
60+00					
	+08.63 = E.C.		31°09.85'		
59+00			30°53.33'		
				+00.56 = P.O.B.T	
+50			29°17.84'		
58+00			27°42.35'		
+50			26°07.86'		
57+00			24°32.37'		
+50			22°56.88'		
56+00			21°21.49'		
+50			19°45.90'		

Station	Align.	Defln.	True Bearing	Curve Data	Magnetic Bearing
+50		3°19.46"			
67+00		2°36.49"		$\Delta = 12.45'$ $R = 2000'$	
+50		1°53.52"		$ST = 222.45'$ $L = 445.06'$	
66+00		1°10.55"			
+50		0°27.58"			
+17.9) = B.C.		ST.			
65+00					
64+00					
63+00					
62+00					

Station	Align.	Def'n.	TRUE BEARING	CURVE DATA	MAGNETIC BEARING
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74+00

50'
2.5' 2.5'

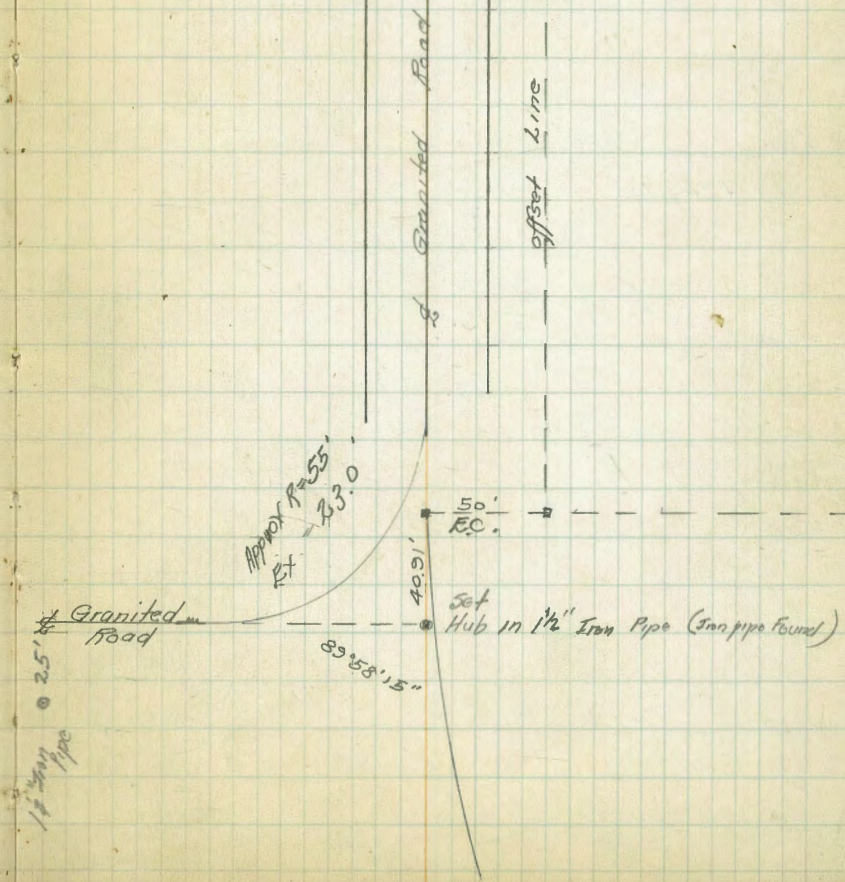
73+00

72+00

1846.76

71+00

70+00

+62.97 = E.C. $6^{\circ}22.50'$ +50 $6^{\circ}11.34'$ 69+00 $5^{\circ}28.37'$ +50 $4^{\circ}45.40'$ 68+00 $4^{\circ}02.43'$ 

Station	Align	Def'n.	TRUE BEARING	CURVE DATA	MAGNETIC BEARING
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25' 25' 25'

80+00

79+00

78+00

1846.76'

77+00

76+00

75+00

Existing Graveled Road to USN Police Station

offset line

25' 25' 25'

Station	Align.	Defln.	true bearing	Curve Data	Magnetic Bearing
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86+00

+70.27

85+00

1846.76'

84+00

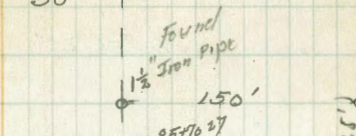
+60.13

83+00

82+00

81+00

50'

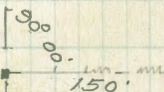


Approx. Radius = 50'

Found 1 1/2" Iron Pipe

Found 1 1/2" Iron Pipe

line



offset

50'

15

U.S. Govt. Line

25'

25'

25'

25'

25'

25'

25'

25'

25'

25'

25'

25'

25'

25'

25'

25'

25'

25'

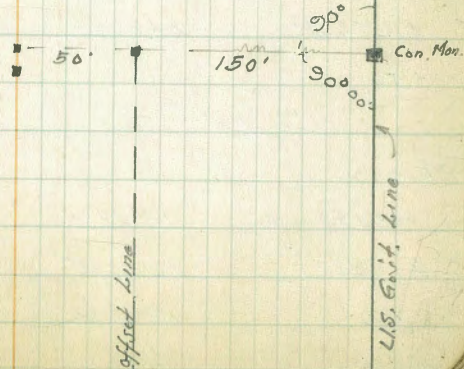
25'

25'

U.S. N. 57410 GROUND.

2 1/2" Galv. Iron Pipe
w/ 1/2" Brass Cap. Slightly deflected
Cap. in top
Marked with
cr. #3 1918

Station	Align.	Def'n.	True Bearing	Curve Data	Magnetic Bearing
750		12°36.74'			
92+00		11°10.80'		$\Delta=36.46'$ $R=1000'$	
+50 +42.06 = P.I.		9°44.86'		$ST=322.33'$ $L=641.70$	
91+00		8°18.92'			
+50		6°52.98'			
90+00		5°27.04'			
+50		4°01.10'			
89+00		2°55.16'			
+54.29 = P.O.S.T.					
+50 +10.31		1°09.22'			
+09.73 = B.C. Lt.					
88+00		1846.76'			
87+00					



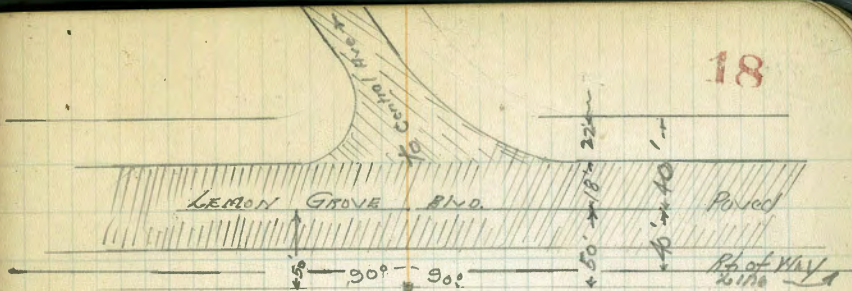
16
Car. Mt. 2 1/2" Pipe
Blast Cap
Hit by track
and off line

To Car. #4 U.S.N.
U.S.N. RADIO GROUNDS

Station	Align.	Defln.	True Bearing	Curve Data	Magnetic Bearing
100+00					
					552°35'E
99+00					
	+55.81 = E.C.	3° 50.0'			
98+00		3° 02.0'		$\Delta = 7^\circ 40'$ $R = 2000'$	
	+50	2° 13.02'		$ST = 134.0'$	
	+22.22 = P.I.			$L = 267.62'$	
97+00		1° 36.05'			Boxing stake
	+50	0° 53.08'			
96+00		0° 10.11'			
	+88.22 = B.C.	LT.			
	+50	136.70'			
95+00					
	+51.43 = E.C.	18° 23.0'			
94+00		16° 54.56'			
	+50	15° 28.62'			
93+00		14° 02.68'			

Completed
6-5-30

Station	Def'n	True Bearing	Curve Data
+69.77	= End line = N 1/2 Line Lemon Grove Blvd.		
+59.77	= E.C.	8° 01'	
+50			$\Delta = 16^{\circ} 02'$ $R = 761.99$
105+00	5° 46'		$L = 212.98$ ST. 107.19
+53.98	= P.I.		
+50	3° 53' 08"		
104+00	3° 00' 16"		
+50	0° 07' 24"		
+46.79	= B.C.	Lt.	
103+00			
	490.95		
102+00			
101+00			



PI Paving stake

Walker
this
aborn
6-6-30

PRELIMINARY LEVELS \pm -
College Way Extension
For location see pages 2-18 this book

Station	Page 2	1.66	466.93	465.27	M.V.B.P. El-City & Gilcher.
0+00				2.5	464.4
+50				4.0	462.9
1+00				4.6	462.3
+50				5.4	461.5
2+00				6.7	460.2
+50				8.6	458.3
3+00				10.9	456.0
T.P.	0.65	454.65	12.93	454.00	
+50				3.1	451.5
4+00				2.7	447.0
+37				11.7	443.0
+50				12.5	442.1
5+00				14.2	440.4
T.P.	0.55	442.36	12.84	441.81	
+25				2.3	440.0
+50				4.4	438.0
6+00				8.7	433.7
+50				10.5	431.8
7+00				11.5	430.8
+50				13.3	429.0
+73.40 = 25' h.t. on Hub				14.31	428.05
8+00				14.6	427.7
+50				14.7	427.7
9+00				14.3	428.1

442.36

9+50	12.2	430.2	
10+00	9.3	433.0	
+37	10.1	432.3	
+38	7.4	435.0	
10+50	7.1	435.2	
11+00	9.1	439.2	
T.P. 1301	459.98	0.39	441.97
+50	10.8	444.2	
12+00	5.1	449.9	
+50	0.7	454.3	
T.P. 1303	466.83	0.18	454.80
+91	9.1	457.7	
13+00	10.4	456.4	
+44	9.7	457.1	
+46	5.4	461.4	
+50	5.1	461.7	
14+00	3.5	463.3	
+50	2.8	464.0	
15+00	3.1	463.7	
+50	5.0	461.8	
16+00	8.5	458.3	
+09	11.4	455.4	
T.P. 040	454.25	12.98	453.85
+47.03 = E.C. on Hub.	1.47	452.78	
17+00	8.5	445.7	
+45	12.9	441.3	

454.25

T.P.	0.25	441.51	12.99	441.26
17+50			1.6	439.9
18+00			11.0	430.5
T.P.	0.76	429.35	12.92	428.59
+29.75 = P.O.T. on Hub.			2.21	427.14
+50			5.8	423.5
19+00			14.8	414.5
T.P.	0.06	416.60	12.81	416.54
+21			12.3	404.3
+25			13.6	403.0
+50			12.8	403.8
+72			10.9	405.7
20+00			12.8	403.8
+50			16.0	400.6
T.P.	1.39	405.08	12.91	403.69
21+00			6.8	398.3
+50			9.3	395.8
22+00			11.6	393.5
+50			15.3	389.8
T.P.	0.64	392.90	12.82	392.26
23+00			5.8	387.1
+50			7.7	385.6
24+00			9.0	383.9
+50			13.2	379.7
T.P.	0.99	381.18	12.71	380.19
+68.02 = P.O.T. on Hub.			3.62	377.56

381.18

22

25+00			7.9	373.3
+50			13.1	368.1
T.P.	0.65	368.94	12.89	368.29
26+00			5.3	363.6
+50			9.5	359.4
27+00			13.0	355.9
T.P.	2.19	358.09	13.04	355.90
+20			5.2	352.9
+50			4.9	353.2
28+00			8.9	349.2
+50			12.1	346.0
T.P.	0.19	345.37	12.91	345.18
29+00			6.6	338.8
+06.88 = B.C. R.H. on Hub.			7.27	338.10
+22			9.9	335.5
+24			14.5	330.9
+50			14.2	331.2
+75			11.6	333.8
30+00			11.3	334.1
+50			11.1	334.3
T.P.	0.84	333.33	12.88	332.49
+70			1.6	331.7
+93.05 = F.C. on Hub.			3.44	329.89
31+00			4.0	329.3
+50			6.7	326.6
+70			7.8	325.5

31+72		10.8	322.5
+78.05 = N.W. edge Riv. ^{up the}		10.86	322.47
+93.05 = L. "		10.73	322.60
32+08.05 = S.W. " "		10.84	322.49
+34		11.2	322.1
T.P. 5.83	326.56	12.60	320.73
chk. SW. B.P. Univ. Ave + City line		7.62	318.94

318.82 = R.P.
0.12 = Error

Correction
on B.P.

7.62	326.44		
T.P. 7.33	327.14	6.63	319.81
32+50		13.0	314.1
+72		12.3	314.2
+80		15.4	311.7
+93.05 = B.C. Lt		14.4	312.7
33+00		14.4	312.7
+17		14.8	312.3
+19		12.6	314.5
+50		12.2	314.9
34+00		12.7	314.4
+50		13.0	314.1
35+00		11.6	315.5
+50		11.2	315.9
+85		9.0	318.1
36+00		2.4	324.7
T.P. 12.41	338.96	0.59	326.55

318.82 = Above B.M.

+25		1.9	337.0
T.P. 12.61	350.49	1.08	337.88
+50		10.8	339.7
37+00		4.8	345.7
+50		3.3	347.2
T.P. 6.49	355.56 344.03	1.42	349.07 337.54
38+00		5.5	350.0
+50		4.6	351.0
39+00		7.0	348.5
+50		16.3	345.2
40+00		12.8	342.7
+50		12.1	343.4
41+00		12.3	343.2
+50		11.6	344.0
42+00		9.5	346.0
42+13 ⁶⁰ E.C. 0.446		8.90	346.66
+50		6.0	349.6
43+00		1.3	354.2
T.P. 6.13	360.52 348.99	1.17	354.39 348.86
+50		7.7	352.8
44+00		9.8	350.7
+50		9.9	350.6
45+00		9.1	351.4
+50		6.6	353.9
+75	Bottom ditch ^{at Right} Angles to line	8.6	351.9
+80		6.4	354.1

348.99
360.52

46+00			5.4	355.1
+ 50			4.7	355.8
47+00			3.0	357.5
TP	11.62	371.42 359.89	0.72	359.80 348.27
+50			10.0	361.4
48+00			5.9	365.5
+50			3.2	368.2
49+00			3.0	368.4
+ 29.52 B.C. Right on Hub			2.03	369.39
+50			2.2	369.2
50+00			5.8	365.6
+ 20			8.2	363.2
+ 25			12.8	358.6
+50			10.1	361.3
+75			6.7	364.7
51+00			4.8	366.6
TP	11.46	379.74 368.21	3.14	368.28 356.75
+50			10.5	369.2
52+00			8.9	371.8
+50			7.6	372.1
53+00			4.9	374.8
+50			2.7	377.0
54+00			1.3	378.4
T.P.	11.65	391.07 379.54	0.32	379.42 367.89
+50			8.5	382.5
58+00			7.4	383.7

379.54
391.07

24

55+50			6.2	384.9
56+00			6.2	384.9
+50			3.6	387.5
+75			+0.8	391.9
T.P. 12.31		402.55 391.02	0.83	390.24 378.71
57+00			11.0	391.6
+50			6.9	395.8
58+00			2.3	400.3
+50			1.0	401.6
59+00			1.9	400.7
+0863 B.C. on Hub			3.12	399.43
+25			5.7	396.9
+63			9.7	392.9
+90			10.2	392.4
60+00			9.2	393.4
+50			3.4	399.2
T.P. 11.91		413.03 400.50	1.43	401.12 389.59
61+00			10.8	402.2
+50			9.2	403.8
62+00			6.8	406.2
+50			4.6	408.4
63+00			2.2	410.8
T.P. 12.98		425.75	0.26	412.77
63+50			12.5	413.2
64+00			7.8	418.8
+50			4.1	421.6

425.75

T.P.	12.15	437.79	0.11	425.64
65+00			12.5	425.3
+1791=BC. 84 on Hub.			11.70	426.09
+50			8.0	429.8
66+00			2.5	435.3
T.P.	11.32	443.18	0.53	437.26
+50			9.2	440.0
67+00			4.3	444.9
T.P.	11.52	460.10	0.60	448.58
+50			10.6	449.5
68+00			6.6	453.5
+50			3.2	456.9
T.P.	12.68	471.97	0.81	459.29
69+00			10.8	461.1
1031' North of BC. on South on Hub in 1 1/2" Iron Pipe Temp.			6.35	465.02
+30			4.7	467.2
+50			4.8	467.1
+62.97 = BC. on Ground. (Hub buried)			4.8	467.1
70+00			4.9	467.0
71+00			4.3	467.6
72+00			4.4	467.5
73+00			4.3	467.6
74+00			4.9	467.0
T.P.	3.37	470.48	4.86	467.11
75+00			4.2	466.3
76+00			5.0	465.5

470.48

25

77+00			5.1	465.4
78+00			4.7	465.8
79+00			4.2	466.3
80+00			3.7	466.8
81+00			3.5	467.0
82+00			3.6	466.9
T.P.	5.92	472.93	3.47	467.01
83+00			4.2	466.3
84+00			6.7	466.2
85+00			6.0	466.9
+75			5.9	467.0
86+00			3.3	469.6
+25			5.7	467.2
+50			3.6	469.3
+70			5.5	467.4
87+00			3.4	469.5
+50			5.3	467.6
+85			3.8	469.1
88+00.73 = BC. 84 on Hub.			5.08	467.85
+50			6.6	466.3
T.P.	11.1	468.21	5.83	467.10
89+00			1.4	466.8
+25			2.2	466.0
+50			5.9	462.3
T.P.	0.67	452.00	12.88	455.33
90+00			4.4	451.6

456.00

90+50			10.7	445.3
+65			14.0	442.0
T.P.	1.00	444.40	12.60	443.40
91+00			4.7	439.7
+25			7.5	436.9
+50			11.9	432.5
92+00			16.5	427.9
T.P.	0.77	432.14	12.03	431.37
+50			7.4	424.7
93+00			11.2	420.9
+30			15.7	416.4
93+50			15.5	416.6
T.P.	1.14	420.47	12.81	419.33
94+00			9.4	411.1
+51.93 = E.C. on Hub.			14.07	406.40
T.P.	0.36	406.76	14.07	406.40
95+00			9.8	403.0
+45			5.8	401.0
+88.32 = B.C. Lt. on Hub.			7.57	399.19
96+00			8.7	398.0
+50			11.7	395.0
T.P.	0.33	394.23	12.86	393.90
97+00			2.7	391.5
+50			7.1	387.1
98+00			11.6	382.6
T.P.	1.05	382.83	12.45	381.78

382.83

Completed 6-6-30

Walker
Bliss
Osborne

26

98+55.84 = E.C. on Hub			5.00	377.83
99+00			7.9	374.9
+50			10.7	372.1
100+00			13.8	369.0
T.P. 0.80	370.94	12.69		370.14
+40			2.4	368.5
+55			5.0	365.9
101+00			7.1	363.8
+50			10.1	360.8
102+00			12.8	358.1
T.P. 1.13	359.51	12.56		358.38
+45			7.6	351.9
+50			10.9	348.6
+60			7.4	352.1
103+00			5.8	353.7
+46.79 = B.C. Lt. on Hub.			6.70	352.81
104+00			11.1	348.4
+25			12.5	347.0
T.P. 2.15	348.73	12.93		346.58
+50			7.1	341.6
+75			4.5	344.2
105+00			3.8	344.9
+38			9.7	339.0
+53.77			10.35	337.38
106+09.77 = on & paving.			10.17	338.56
on % Pav. over culvert			11.20	337.53

Sta. EL.

Topog. College Way Ext. Align-

ment. Page 2 -

Hough-Jain 6/28-1930

27

Sta.	EL.				
105+59	337.38	$\frac{36.7}{21.5L}$	$\frac{35.1}{36.0L}$	$\frac{35.0}{85.0}$	points from Sta Left side
105+00	344.9 51.0 100	$\frac{42.0}{34.0L}$	$\frac{40.0}{51.0L}$	$\frac{40.4}{65.0L}$	
104+50	341.6	$\frac{45.0}{12.0L}$	$\frac{45.0}{71.0L}$	$\frac{40.0}{97.0L}$	
104.0	348.4	$\frac{45.0}{17.0L}$	$\frac{45.0}{23.0L}$	$\frac{50.0}{42.0L}$	$\frac{53.0}{95.0L}$
DC. 103+46	352.8 5.8	$\frac{50.0}{11.0L}$	$\frac{45.0}{32.0L}$	$\frac{45.0}{44.0L}$	$\frac{50.0}{55.0L}$ $\frac{55.0}{68.0L}$ $\frac{60.0}{93.0L}$
103.0	353.7	$\frac{50.0}{21.0L}$	$\frac{50.0}{36.0L}$	$\frac{55.0}{47.0L}$	$\frac{60}{100.0L}$
+50	348.6	$\frac{50.0}{5.0L}$	$\frac{50.0}{25.0L}$	$\frac{60.0}{80.0L}$	$\frac{65.0}{80.0L}$
102	358.1	$\frac{60.0}{18.0L}$	$\frac{65.0}{80.0L}$		
101.	363.8	$\frac{65.0}{30.0L}$	$\frac{70.0}{86.0L}$		
100	369.0	$\frac{70.0}{15.0L}$	$\frac{75.0}{86.0L}$		
99.0	374.9	$\frac{75.0}{3.0L}$	$\frac{80.0}{60.0L}$	$\frac{85.0}{95.0L}$	
98+55 EG	377.8	$\frac{80.0}{18.0L}$	$\frac{85.0}{70.0L}$	$\frac{90.0}{90.0L}$	
98.	382.6	$\frac{85.0}{18.0L}$	$\frac{90.0}{48.0L}$	$\frac{95.0}{75.0L}$	

Sta. El.

97+50-387.1	900	$\frac{95.0}{15.0L}$	$\frac{100.0}{37.0L}$	$\frac{100.0}{68.0L}$	$\frac{105.0}{98.0L}$
97+00-391.5	910	$\frac{95.0}{17.0L}$	$\frac{100.0}{40.0L}$	$\frac{105.0}{63.0L}$	$\frac{110.0}{77.0L}$
96+50-395.0	920	$\frac{100.0}{23.0L}$	$\frac{105.0}{47.0L}$	$\frac{110.0}{67.0L}$	$\frac{115.0}{87.0L}$
95+88.0-399.2	930	$\frac{100.0}{3.0L}$	$\frac{105.0}{25.0L}$	$\frac{110.0}{42.0L}$	$\frac{115.0}{65.0L}$
95	403.0	$\frac{105.0}{8.0L}$	$\frac{110.0}{29.0L}$	$\frac{115.0}{50.0L}$	$\frac{120.0}{71.0L}$
94.	411	$\frac{115.0}{11.0L}$	$\frac{120.0}{26.0L}$	$\frac{125.0}{51.0L}$	$\frac{130.0}{75.0L}$
93	420.9	$\frac{125.0}{17.0L}$	$\frac{130.0}{26.0L}$	$\frac{135.0}{62.0L}$	$\frac{140.0}{90.0L}$
92	427.9	$\frac{130.0}{11.0L}$	$\frac{135.0}{39.0L}$	$\frac{140.0}{56.0L}$	$\frac{145.0}{74.0L}$
+50	371.5	$\frac{135.0}{7.0L}$	$\frac{140.0}{21.0L}$	$\frac{145.0}{47.0L}$	$\frac{150.0}{67.0L}$
91	439.7	$\frac{140.0}{3.0L}$	$\frac{145.0}{21.0L}$	$\frac{150.0}{34.0L}$	$\frac{155.0}{66.0L}$
90.	51.6	$\frac{155.0}{13.0L}$	$\frac{160.0}{45.0L}$	$\frac{165.0}{75.0L}$	$\frac{170.0}{90.0R}$
+50	62.0	$\frac{165.0}{15.0L}$	$\frac{170.0}{130.0L}$		$\frac{175.0}{14.0R}$
89-466.8		$\frac{170.0}{125.0L}$			$\frac{175.0}{40.0R}$

position of Staked line.

R. of E

College Way
Top Knoll
70.0

Sta. El. 35.0 L

88+103 467.85

86. 469.6 70.0 top knoll's
0.0

Sec Page 36 p. 900 Road for ϵ R. side

69 461.1 Wood Pipe. Wire wrapped 8" $\frac{46.00}{22.0 L}$ $\frac{46.50}{31.0 R}$

+50 456.9 Level. $\frac{65.0}{25.0 R}$ $\frac{70.0}{45.0 R}$

68 453.5 $\frac{55.0}{40.0 L}$ $\frac{55.0}{25.0 R}$ $\frac{60.0}{38.0 R}$

+50 449.5 $\frac{55.0}{32.0 L}$ $\frac{50.0}{L 30}$ $\frac{50.0}{25.0 R}$ $\frac{55.0}{70.0 R}$

67 44.9 $\frac{50.0}{31.0 L}$ $\frac{45.0}{L 20}$ $\frac{45.0}{40.0 R}$ $\frac{50.0}{60.0 R}$

+50 440.0 $\frac{45.0}{28.0 L}$ $\frac{50.0}{46.0 L}$ $\frac{40.0}{20.0 R}$ $\frac{45.0}{52.0 R}$ 6-30/30

66 435.3 $\frac{40.0}{32.0 L}$ $\frac{45.0}{47.0 L}$ $\frac{35.0}{3.0 R}$ $\frac{35.0}{12.0 R}$ $\frac{40.0}{43.0 R}$ $\frac{45.0}{60.0 R}$

+50 429.8 $\frac{30.0}{2.0 L}$ $\frac{35.0}{25.0 L}$ $\frac{40.0}{45.0 L}$ $\frac{30.0}{7.0 R}$ $\frac{35.0}{30.0 R}$ $\frac{40.0}{50.0 R}$ $\frac{45.0}{70.0 R}$

65 425.2 $\frac{25.0}{5.0 L}$ $\frac{30.0}{33.0 L}$ $\frac{35.0}{52.0 L}$ $\frac{30.0}{22.0 R}$ $\frac{35.0}{33.0 R}$ $\frac{40.0}{53.0 R}$

+50 421.6 $\frac{25.0}{33.0}$ $\frac{20.0}{20.0 L}$ $\frac{20.0}{5.0 L}$ $\frac{25.0}{12.0 R}$ $\frac{30.0}{30.0 R}$ $\frac{35.0}{47.0 R}$

64 418.8 $\frac{15.0}{38.0 L}$ $\frac{20.0}{21.0 L}$ $\frac{15.0}{10.0 L}$ $\frac{20.0}{4.0 R}$ $\frac{25.0}{20.0 R}$ $\frac{30.0}{39.0 R}$ $\frac{35.0}{54.0 R}$

College Way

Sta. El. ϵ
L \leftarrow \rightarrow R

63+50 - 413.2 $\frac{20.0}{45.0}$ $\frac{15.0}{18.0}$ $\frac{10.0}{4.0}$ $\frac{15.0}{4.0}$ $\frac{20.0}{19.0}$ $\frac{25.0}{35.0}$

63+00 410.8 $\frac{20.0}{26.0}$ $\frac{15.0}{12.0}$ $\frac{10.0}{1.0}$ $\frac{10.0}{7.0}$ $\frac{15.0}{15.0}$ $\frac{20.0}{32.0}$ $\frac{25.0}{50.0}$

62+50 - 408.4 $\frac{20.0}{30.0}$ $\frac{15.0}{16.0}$ $\frac{10.0}{3.0}$ $\frac{10.0}{4.0}$ $\frac{10.0}{11.0}$ $\frac{20.0}{2.0}$ $\frac{25.0}{37.0}$ $\frac{30.0}{54.0}$

62+00 406.2 $\frac{20.0}{30.0}$ $\frac{15.0}{21.0}$ $\frac{10.0}{10.0}$ $\frac{10.0}{3.0}$ $\frac{10.0}{18.0}$ $\frac{20.0}{35.0}$ $\frac{25.0}{55.0}$

+50 405.8 $\frac{15.0}{33.0}$ $\frac{10.0}{21.0}$ $\frac{10.0}{8.0}$ $\frac{10.0}{13.0}$ $\frac{10.0}{21.0}$ $\frac{10.0}{34.0}$ $\frac{10.0}{49.0}$

61+00 403.2 $\frac{45.0}{34.0}$ $\frac{40.0}{22.0}$ $\frac{40.0}{10.0}$ $\frac{40.0}{1.0}$ $\frac{40.0}{21.0}$ $\frac{39.0}{28.0}$ $\frac{40.0}{37.0}$ $\frac{40.0}{65.0}$

+50 399.2 $\frac{40.0}{30.0}$ $\frac{40.0}{18.0}$ $\frac{40.0}{3.0}$ $\frac{39.0}{18.0}$ $\frac{40.0}{24.0}$ $\frac{40.0}{35.0}$ $\frac{40.0}{50.0}$

60+00 393.4 $\frac{40.0}{30.0}$ $\frac{39.0}{7.0}$ $\frac{39.0}{3.0}$ $\frac{39.0}{11.0}$ $\frac{39.0}{17.0}$ $\frac{40.0}{34.0}$ $\frac{40.0}{48.0}$ $\frac{40.0}{60.0}$

+63 392.9 $\frac{40.0}{45.0}$ $\frac{40.0}{33.0}$ $\frac{40.0}{9.0}$ $\frac{40.0}{3.0}$ $\frac{40.0}{5.0}$ $\frac{40.0}{20.0}$ $\frac{40.0}{32.0}$ $\frac{40.0}{46.0}$ $\frac{40.0}{64.0}$

59+00 400.7 $\frac{40.0}{4.0}$ $\frac{40.0}{27.0}$ $\frac{40.0}{16.0}$ $\frac{40.0}{3.0}$ $\frac{40.0}{1.0}$ $\frac{40.0}{4.0}$ $\frac{40.0}{4.0}$ $\frac{40.0}{6.0}$

+50 401.6 $\frac{85.0}{74.0}$ $\frac{85.0}{47.0}$ $\frac{90.0}{20.0}$ $\frac{90.0}{3.0}$ $\frac{40.0}{10.0}$ $\frac{40.0}{25.0}$ $\frac{40.0}{35.0}$ $\frac{40.0}{68.0}$

58.02 400.3 $\frac{85.0}{70.0}$ $\frac{90.0}{51.0}$ $\frac{95.0}{33.0}$ $\frac{100.0}{1.0}$ $\frac{40.0}{14.0}$ $\frac{40.0}{36.0}$ $\frac{40.0}{55.0}$ $\frac{40.0}{76.0}$

+50. 395.8 $\frac{85.0}{20.0}$ $\frac{90.0}{34.0}$ $\frac{95.0}{54.0}$ $\frac{100.0}{74.0}$

57 391.6 $\frac{80.0}{65.0}$ $\frac{80.0}{48.0}$ $\frac{85.0}{29.0}$ $\frac{90.0}{8.0}$ $\frac{95.0}{12.0}$ $\frac{100.0}{30.0}$ $\frac{100.0}{47.0}$ $\frac{100.0}{60.0}$

College Way

Left. → Right.

Sta.	El.								
56+50	387.5	800 750 800 850	700 950 4000 4050	60.0 380.0 300.0 710.0	100.0 270.0 430.0 600.0				
56+00	384.9	385.0 350.0 750 380.0	900 950 400.0 4050	80.0 420.0 300.0 210.0	80.0 170.0 290.0 450.0				
+50	384.9	75.0 25.0 800	900 950 4000 4050	45.0 520.0 20.0	80.0 150.0 220.0 500.0				
55+00	383.7	75.0 800	850 900 950 4000 4050	45.0 150.0	50.0 200.0 340.0 480.0				
+50	382.5	70.0 75.0 800	850 900 950 4000 4050	60.0 500.0 100.0	130.0 280.0 430.0 590.0				
54+00	378.4	70.0 75.0	800 850 900 950 4000 4050	54.0 21.0	60.0 200.0 300.0 440.0 580.0 680.0				
+50	377.0	70.0 700 750	800 850 900 950 4000	67.0 500.0 260.0	70.0 230.0 330.0 450.0 600.0				
53+00	374.8	65.0 650 700	750 800 850 900 950	50.0 200.0 400.0	30.0 180.0 310.0 430.0 560.0 680.0				
+50	372.1	70.0 650 650 800	800 850 900 950	50.0 370.0 300.0 150.0	70.0 270.0 400.0 530.0 680.0				
52	371.8	970.0 650 650 800	850 900	450.0 220.0 160.0 120.0	370.0 800 850 900 120.0 320.0 580.0 750.0				
+50	369.2	70.0 650 650	700 750 800 850	540.0 300.0 200.0	30.0 350.0 640.0 890.0				
51+00	366.6	70.0 65 65.0	700 750	530.0 330.0 120.0	230.0 570.0				
+50	361.3	75.0 700 650 3600 3600	650 700	65.0 40.0 170.0 110.0 50.0	160.0 610.0				
50	365.6	800 750 370.0	3650 600 600 650 700	64.0 430.0 170.0	20.0 170.0 240.0 480.0 980.0				

College Way

29

Sta.	El.								
49+50	369.2	850 730 800 750 700	650 600 550 600 650	490.0 360.0 40.0	190.0 340.0 400.0 500.0 960.0				
49+00	368.4	850 670 800 750 700	650 600 600	390.0 220.0 50.0	200.0 500.0 850.0				
+50	368.2	850 900 750 700	650 600	720.0 440.0 270.0 70.0	200.0 420.0				
48+00	365.5	800 750 700	650 600 650	810.0 590.0 270.0	30.0 350.0 500.0				
+50	361.4	750 700 3650	3600 3550	620.0 400.0 190.0	180.0 680.0				
47+00	357.1	750 700 650 3600	3550 Elev Wash.	800 570.0 350.0 10.0	340.0 720.0				
+50	355.8	750 700 650 3600	3550 510 Wash.	165.0 100.0 650 3600	120.0 410.0				
46+00	355.1	700 650 600 550 500 500 550		102.0 70.0 430.0 20.0 320.0 450.0 70.0					

Sec. Book 1984.

See Page 28

Left. $\frac{L}{R}$ Road -
Right.

6-30-30

Hough
Lane.

30

69+03 Left 470 to N. end Culvert.

69+33 Left 56.0 to S. end Culvert. Flow. El. 464.7

+50 El. 467.1

90 467.0

91 467.6

92 467.5

93 467.6

94 467.0

95 466.3

96 465.5

+50

97 465.4

+50

98 465.2

99

80 466.8

1 467.0

2 466.9

3 466.3

+50

84 466.2

+50

85 466.9

86 469.6

See Page 28

Top Knoll	70.0	69.5
	37.0	50.0
" "	70.0	70.3
	47.0	50.0
		69.8
		50.0

Right
70.0 70.0
70.0 34.0

30' to Pit
34' to Pit
Time 115

70.50
in left.

60.0	65.0
100.0	45.0
60.0	65.0
50.0	20.0
55.0	60.0
74.0	30.0
	65.0
	50.0

66.1
50.0

Flow. S. Road
El. 464.2 Culvert

82+50 = 60.0 65.0
85 17.0

60.0	46.50
72.0	78.0
60.0	65.0
65.0	33.0

apart El. 65.0
177 Pot. Holes
2' Knolls.

60.0	65.0
75.0	36.0
60.0	65.0
76.0	20.0

El. 1170.0
70.0
69.5

60.0	65.0
81.0	73.0
65.0	70.0
95.0	60.0

Top Knoll

Y/1 Key
 El. of
 Dr. 1001
 3-30

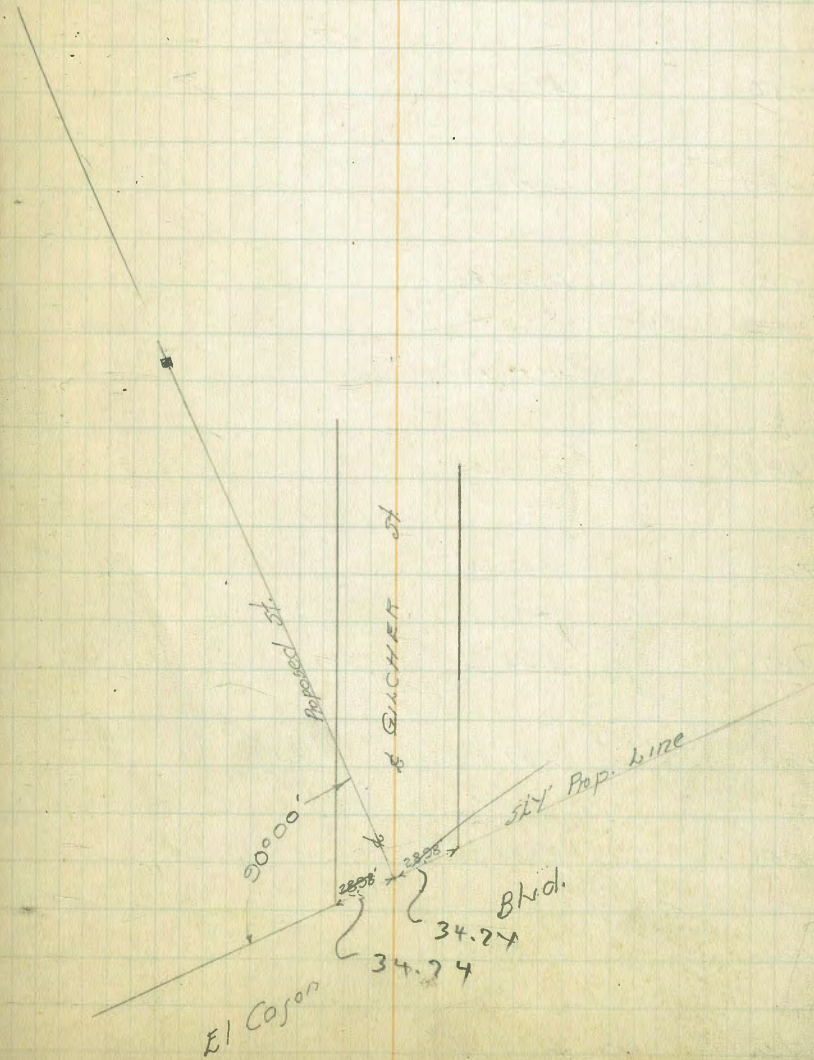
Change in Alignment

College Hwy Extension

From Station 0+00 Page 1 to Station.

Station	Align.	Def'n.	True Setting	Curve Data
5+00		2° 58.37'		
				$\Delta = 39^{\circ} 20'$
+50		3° 01.07'		$R = 1500$
				$ST = 536.10'$
4+00		2° 09.98'		$L = 1029.74$
+50		1° 06.48'		
3+00		0° 09.19'		
+91.98 = B.C.		B.P.		
+50				
2+00				
+50				
1+00				
+50				

0+00 = South line El Cajon Hwy of Gilcher.



Station	Align	Defln.	True Bearing	Curve Data
+50		16°23.20'		
11+00		15°25.91'		
+50		14°28.61'		
10+00		13°31.32'		
+50		12°34.02'		
9+00		11°36.73'		
+50		10°39.43'		
8+00		9°42.14'		
+50		8°44.84'		
7+00		7°47.25'		
+50		6°50.25'		
6+00		5°52.96'		
+50		4°55.66'		

Station	Align.	Defln.	True Bearing	Curve Data
+50		1°53.58'		$\Delta = 33^\circ 14'$ $R = 1000'$
17+00		3°27.64'		$ST = 238.49'$ $L = 580.03'$
+50		2°01.70'		
16+00		0°35.76'		
+79.19 = BC.		Pt.		
+50				
15+00				
		257.47'		
+50				
14+00				
+50				
+21.74 = EC.		13°40.00'		
13+00		13°15.09'		
+50		18°17.80'		
12+00		17°20.50'		

Station #1975 Def'n. True Bearing Curve Data.

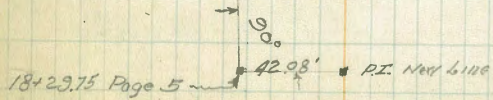
+5922=K.C.	16°37.0'
+50	16°21.10'
21+00	14°55.16'
+50	13°29.22'
20+00	12°03.28'
+50	10°37.34'
19+00	9°11.40'
+7762=K.C.	
+50	7°45.46'
18+00	6°19.52'



old location Page 5 and 6

Proposed new line

Hub



7/5/30
London

Sec. Levels on Alignment P 34

B.M. 1.08 466.35

H65.27

H.W. B.P.
E.C. Stone
College Hill

455.38

0+50

GOR	3.0	463.3
±	3.0	463.3
GOL	4.4	462.0

1+00

GOL	5.0	461.0
±	3.8	462.6
GOR	4.1	462.3

1+50

GOR	4.9	461.5
±	5.7	460.7
GOL	6.1	460.3

2+00

GOL	8.4	458.0
±	7.3	459.1
GOR	7.0	459.4

2+50

GOR	9.4	457.0
±	10.3	456.1
GOL	11.1	455.3

2+91¹⁸ B.C.

GOL	15.7	450.7
±	13.4	453.0
GOR	12.3	454.1

T.P. 1.63 455.38 12.60 453.75

4+00

GOR	10.0	445.4
±	11.7	443.5
25L	11.3	444.1
50L	12.2	443.2
GOL	12.7	442.7

4+13

GOL	13.0	442.4
20L	11.6	443.8
±	13.4	442.0
HOR	11.1	444.3
GOR	11.1	444.3

4+30

GOR	14.2	441.2
±	15.1	440.3
GOL	12.6	442.8

5+00

GOL	9.2	446.2
±	12.6	442.8
80R	17.7	437.7

5+50

GOR	13.4	442.0
±	9.9	445.5
GOL	6.4	449.0

35

6+00	455.38		
GOL		3.0	452.4
±		6.9	448.5
GOR		11.3	444.1

6+50			
GOR		10.1	445.3
±		4.8	450.6
GOL		0.2	455.4
T.P.	3.62	458.24	0.76
			454.62

7+00			
GOL		3.1	455.1
±		7.2	451.0
GOR		12.4	445.8

8+00			
GOR		14.3	433.9
±		10.1	448.1
GOL		7.3	450.9

8+50			
GOL		12.2	446.0
±		14.5	443.7
GOR		16.8	441.4

9+06			
GOR		20.8	437.4
±		19.2	439.0
GOL		16.5	441.7

9+50	458.24		
GOL		12.1	446.1
±		14.4	443.8
GOR		18.0	440.2

10+00			
GOR		15.3	442.9
±		12.0	446.2
GOL		9.3	448.9

10+50			
GOL		3.8	454.4
±		8.0	450.2
GOR		10.7	447.5

11+00			
GOR		8.0	450.2
±		2.5	455.7

T.P.	12.72	468.63	2.33
			455.91
45L		9.9	458.7
GOL		10.7	457.9

11+50			
GOL		8.4	460.2
25L		7.1	461.5
±		11.0	457.6
BOR		11.6	457.0
GOR		15.7	452.9

12+00		46863	
60R	12.3	4563	
30R	10.2	4584	
⊕	7.7	4609	
20L	6.7	4619	
60L	6.4	4622	
12+50			
60L	6.5	4621	
⊕	6.6	4620	
10R	6.6	4620	
30R	9.5	4591	
60R	11.0	4576	
13+00			
60R	8.7	4599	
45R	7.0	4616	
20R	8.3	4609	
⊕	4.6	4640	
60L	5.5	4631	
14+00			
60L	3.4	4652	
⊕	6.1	4625	
45R	7.7	4609	
60R	5.8	4628	

15+00		46863	
60R	6.6	4620	
⊕	7.2	4614	
60L	6.9	4617	
15+50			
60L	13.6	4550	
⊕	13.3	4553	
60R	8.7	4599	
16+00			
60R	11.8	4568	
T.P. 0.15	455.71	13.07	455.56
⊕	9.5	4462	
30L	13.8	4419	
60L	13.9	4418	
16+50			
60L	27.3	4284	
40L	28.1	4276	
⊕	16.9	438.8	
28R	7.7	448.0	
60R	3.1	4526	
17+00			
60R	5.2	4505	
25R	7.4	448.3	
T.P. 0.27	443.07	12.89	442.82
⊕	4.2	4389	
55L	28.0	4151	
60L	25.4	417.7	

18+00 - 443.09
 GOL 26.1 417.0
 £ 12.5 430.6
 5OR 1.6 441.5

18+50
 6OR 7.1 436.0
 T.P. 1.16 431.18 13.07 430.02
 £ 4.3 426.9
 GOL 15.8 415.4

19+00
 6OL 20.6 410.6
 6OL 14.1 417.1
 £ 10.5 420.7
 6OR 3.3 427.9

19+50
 6OR 6.6 424.6
 £ 22.2 409.0
 6OL 34.8 396.4
 T.P. 1.44 419.67 12.95 418.23

20+00
 6OL 20.4 399.3
 £ 3.0 416.7
 6OR 19.1 428.8

21+00 419.67
 6OR 16.9 426.6
 12R 0.5 419.2
 £ 3.6 416.1
 6OL 23.3 396.4

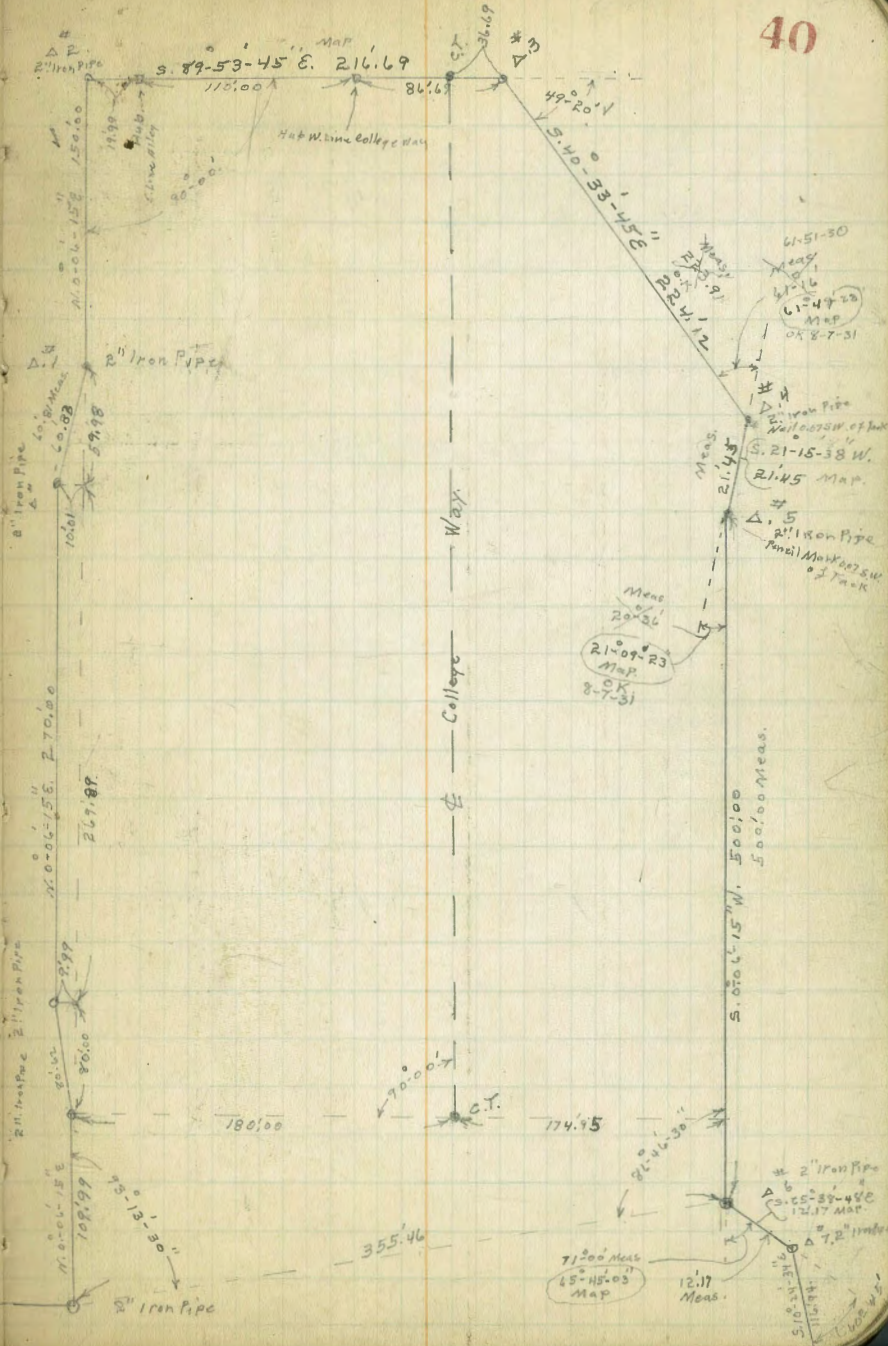
21+59² EC
 6OL 25.1 394.6
 6OL 10.0 409.7
 £ on Hub 14.94 414.73
 6OR 15.2 425.9

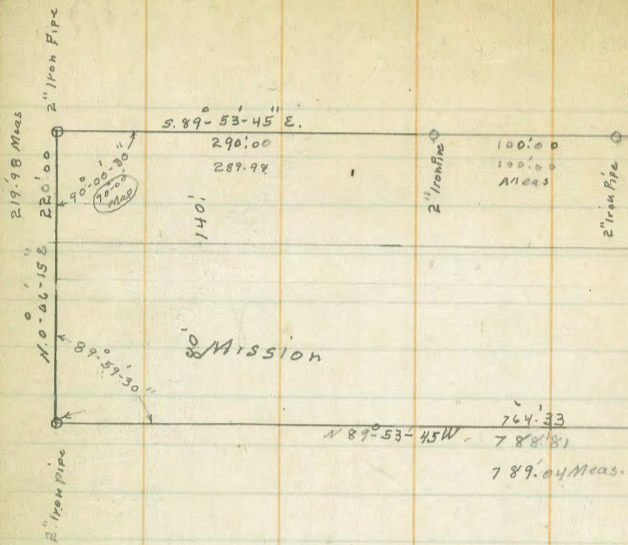
College Park Boundaries

8-1-31

Walker
Walker
Bliss

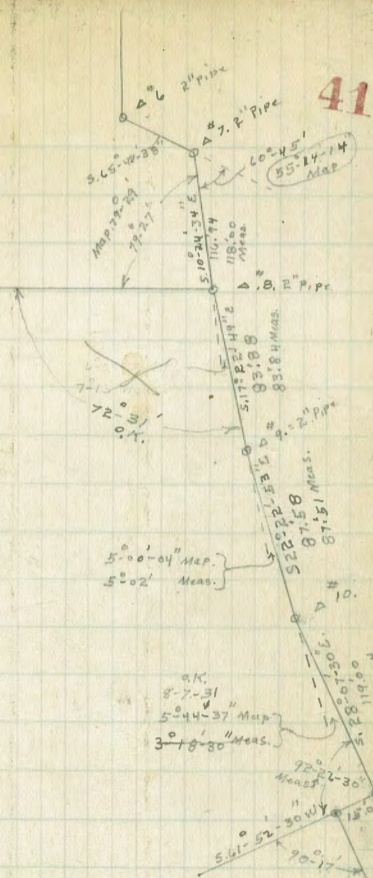
40





Map
89-53-45

219.98
176.43 Meas



11-29-32

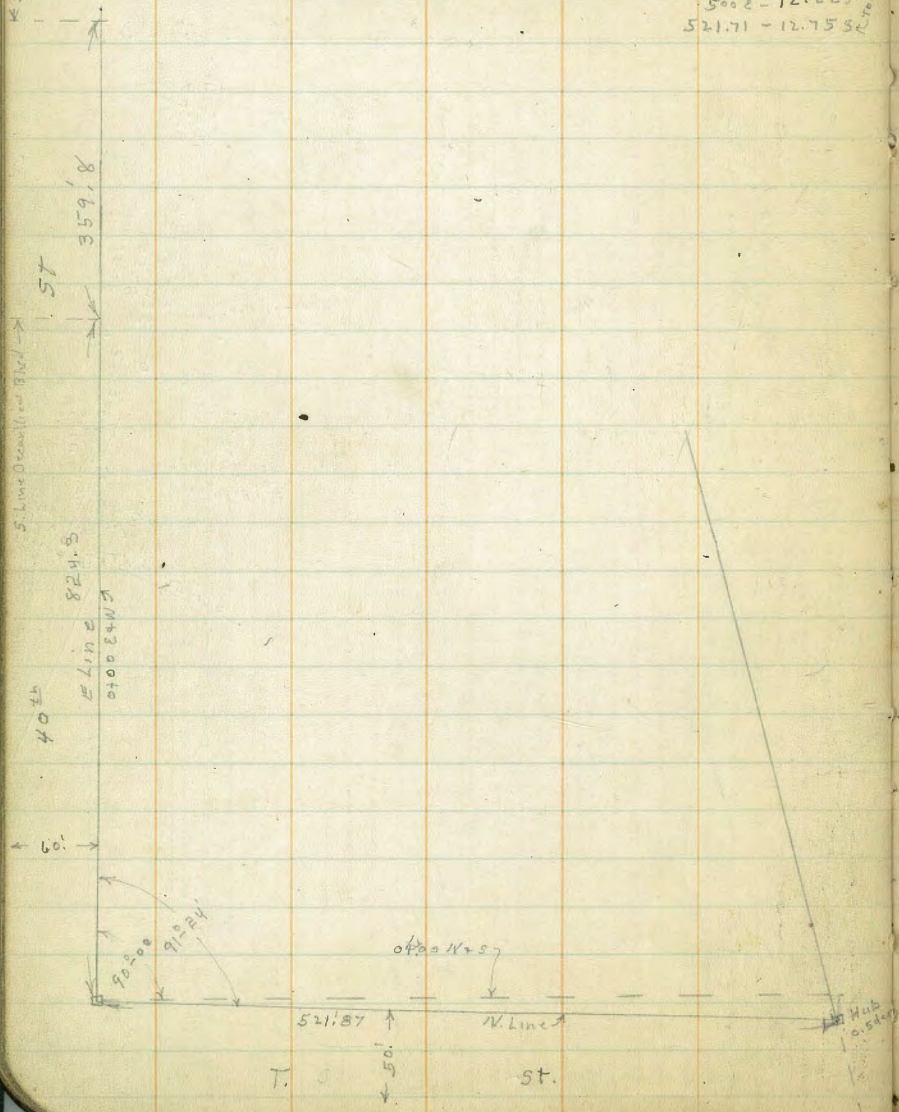
E. Sec. Mt. View - Park.

Miller
Walker
Bliss.

N. Line T 5.4
0+00 N+5
50.2 - 1.22 S
100.2 - 2.44 S
150.2 - 3.67 S
200.2 - 4.89 S
250.2 - 6.11 S
300.2 - 7.33 S
350.2 - 8.55 S
400.2 - 9.77 S
450.2 - 11.00 S
500.2 - 12.22 S
521.71 - 12.75 S

Run N. Line T. st.

← S. Line Frankl. st.



B.M. NW 1/4 CT	2.92	85.10	82.18	40° 4' 00" View.
Set B.M. B.P.			7.84	77.26 N.W. Teak 4 40 th
T.P.	0.83	72.77	13.16	71.94
Set B.M. B.P.			6.01	66.76 N.W. 5 th + 40 th Sts.
T.P.	3.78	63.32	13.23	59.54
Set B.M. B.P.			12.70	50.62 N.W. 7 th + 40 th St.
N.E. Cor 40 th + T. Sts = 00 N + S. + 00 E + W. - E. Line 40 th				
= Base line X sections taken at 90°-00 to Base line				
X 63.32				
00 N + S - 00 E + W			10.2	53.72 N.E. Cor T + 40 th Sts
1.22 S. - 50' E			10.9	52.42 N. Line T. St.
00 N + S - 50' E			10.9	52.42
2.44 S. - 100' E			12.2	51.12 N. Line T. St.
00 N + S - 100' E			12.2	51.12
3.67 S - 150' E			14.3	49.02 N. Line T. St.
00 N + S - 150' E			14.0	49.02
4.90 S. - 180' E			15.5	47.82 N. Line T. St.
00 N + S - 180' E			15.4	47.92
4.99 S - 200' E			17.4	45.92 N. Line T. St.
00 N + S - 200' E			17.3	46.02
5.13 S. - 210' E			18.4	44.92 N. Line T. St.
00 N + S - 210' E			18.4	44.92
5.50 S. - 225' E			18.4	44.92 N. Line T. St.
00 N + S - 225' E			18.4	44.92

6.11 S - 250' E	16.3	47.02	N. Line T. St.
00 N + S - 250' E	16.3	47.02	
6.48 S - 265' E	16.8	46.52	N. Line T. St.
00 N + S - 265' E	15.5	47.92	
25' N. - 265' E	14.8	48.52	
7.33 S. - 300' E	16.2	47.12	N. Line T. St.
00 N + S - 300' E	16.2	47.12	
8.55 S - 350' E	12.4	50.92	N. Line T. St.
00 N + S - 350' E	11.5	51.82	
9.78 S. - 400' E	8.0	55.32	N. Line T. St.
00 N + S - 400' E	8.0	55.32	
10.39 S. - 425' E	5.3	58.02	N. Line T. St.
00 N + S - 425' E	5.3	58.02	
11.00 S. - 450' E	1.6	61.72	N. Line T. St.
00 N + S - 450' E	1.6	61.72	
T.P. 0.58	63.88	0.02	63.30
11.47 S - 470' E	+0.4	64.3	N. Line T. St.
0 + 00 N + S - 470' E	+0.4	64.3	
12.22 S - 500' E	+3.0	66.9	N. Line T. St.
0 + 00 N + S - 500' E	+3.0	66.9	
12.75 S - 521.71 E	+4.0	67.9	N.W. Cor T. + Boundary Sts
0 + 00 N + S - 521.71 E	+4.2	68.1	Traveled Rd. Boundary St.
50' N 510' E	+5.7	69.6	Traveled Rd. Boundary St.
50' N 500' E	+4.2	68.1	
50' N 470' E	+0.8	64.7	
40' N 450' E	1.3	62.6	

63.88

50' N	450' E	2.2	61.7
50' N	420' E	6.0	57.9
50' N	400' E	7.3	56.6
50' N	350' E	11.1	52.8
50' N	300' E	14.8	49.1
50' N	270' E	15.0	48.9
50' N	250' E	16.3	47.6
50' N	225' E	17.3	46.6
50' N	200' E	16.3	47.6
50' N	170' E	15.0	48.9
50' N	150' E	14.1	49.8
50' N	100' E	11.7	52.2
50' N	80' E	10.4	53.5
50' N	50' E	9.1	54.8
50' N	00 E+W	8.8	55.1 E. line = 40'
100' N	00 E+W	6.6	57.3 " " "
100' N	50' E	6.7	57.2
100' N	87' E	8.1	53.8
100' N	100' E	9.7	54.2
100' N	150' E	12.4	51.5
100' N	200' E	15.1	48.8
100' N	225' E	15.4	48.5
100' N	250' E	13.5	50.4
100' N	287' E	12.6	51.3
100' N	300' E	11.5	52.4

63.88

Mt. View Park

44

100' N	350' E	5.9	58.0
100' N	370' E	4.2	59.7
100' N	400' E	2.4	61.5
100' N	450' E	+0.9	64.8
130' N	450' E	+3.4	67.3
100' N	465' E	+3.0	66.9
100' N	490' E	+4.4	68.3
100' N	500' E	+5.7	69.6
150' N	483' E	+6.0	69.9
150' N	476' E	+5.5	69.4
150' N	450' E	+6.4	70.3
150' N	430' E	+7.7	71.6
150' N	400' E	+6.4	70.3
150' N	365' E	+4.0	67.9
150' N	350' E	+1.2	65.1
150' N	315' E	4.6	59.3
150' N	300' E	7.0	56.9
150' N	270' E	9.7	54.2
150' N	250' E	11.4	52.5
150' N	240' E	12.7	51.2
150' N	225' E	13.3	50.6
150' N	200' E	13.1	50.8
150' N	150' E	10.3	53.6
150' N	100' E	6.8	57.1
150' N	87' E	5.1	58.8
150' N	50' E	4.9	-59.0

Traveled Road
Boundary St.
Traveled Rd
Boundary St.

63.88

150'.N	00'E+W	3.6	60.3	8.1 in x 40"
175'.N	00'E+W	3.2	60.7	" " "
200'.N	00'E+W	0.7	63.2	" " "
200'.N	25'.E	1.7	62.2	
183'.N	25'.E	2.2	61.7	
200'.N	50'.E	2.2	61.7	
188'.N	50'.E	2.0	61.9	
200'.N	80'.E	2.5	61.4	
188'.N	80'.E	2.1	61.8	
200'.N	100'.E	4.0	59.9	
192'.N	100'.E	2.0	61.9	
200'.N	120'.E	5.3	58.6	
190'.N	120'.E	4.8	59.1	
200'.N	150'.E	9.3	54.6	
200'.N	200'.E	11.4	52.5	
200'.N	220'.E	10.9	53.0	
200'.N	250'.E	9.1	54.8	
200'.N	275'.E	7.4	56.8	
200'.N	300'.E	4.3	59.6	
200'.N	325'.E	0.0	63.7	
200'.N	350'.E	+6.2	70.1	
200'.N	385'.E	+12.0	75.9	
236'.N	385'.E	+12.0	75.9	
200'.N	400'.E	+14.4	78.3	
236'.N	400'.E	+14.0	77.9	

Mt. View Park

63.88

45

200'.N - 420'.E	+14.7	78.6	
215'.N - 420'.E	+16.2	80.1	
230'.N - 420'.E	+16.0	79.9	
200'.N - 437'.E	+13.3	77.2	
215'.N - 437'.E	+14.8	78.7	
230'.N - 437'.E	+14.3	78.2	
200'.N - 450'.E	+11.5	75.4	
215'.N - 450'.E	+11.7	75.6	
200'.N - 461'.E	+5.3	69.2	
200'.N - 470'.E	+5.4	69.3	Traveled Rd Boundary St.
250'.N - 455'.E	+4.6	68.5	Traveled Rd Boundary St.
250'.N - 448'.E	+4.0	67.9	
250'.N - 437'.E	+11.6	75.5	
250'.N - 430'.E	+13.2	77.1	
250'.N - 420'.E	+12.8	76.7	
250'.N - 400'.E	+11.8	75.7	
250'.N - 365'.E	+7.0	70.9	
250'.N - 350'.E	+4.2	68.1	
250'.N - 330'.E	+1.4	65.3	
250'.N - 300'.E	1.7	62.2	
265'.N - 300'.E	1.7	62.2	
275'.N - 300'.E	2.9	61.0	
285'.N - 300'.E	2.6	61.3	
250'.N 275'.E	4.7	59.2	
250'.N 250'.E	5.8	58.1	
262'.N 250'.E	5.5	58.4	

71.92

350' N	350' E	5.2	66.7
350' N	325' E	4.6	67.3
350' N	300' E	3.9	68.0
338' N	300' E	1.6	70.3
350' N	285' E	2.4	69.5
335' N	285' E	1.7	70.2
350' N	250' E	6.7	65.2
325' N	250' E	6.0	65.9
350' N	215' E	13.3	58.6
350' N	200' E	14.1	57.8
350' N	175' E	15.4	56.5
350' N	150' E	14.8	57.1
350' N	100' E	14.6	57.3
332' N	100' E	14.9	57.0
325' N	100' E	13.5	58.4
365' N	100' E	14.1	57.8
370' N	100' E	12.8	59.1
350' N	85' E	14.2	57.7
360' N	85' E	11.9	60.0
327' N	85' E	14.3	57.6
320' N	85' E	13.2	58.7
350' N	75' E	11.6	60.3
320' N	75' E	12.3	59.6
350' N	50' E	8.2	63.7
335' N	50' E	9.2	62.7

71.92

Mt. View Park

47

350' N	25' E	3.8	68.1	
320' N	25' E	7.6	64.3	
350' N	00 E+W	3.3	68.6	2. Line 40 th St.
375' N	00 E+W	1.2	70.7	" " " "
375' N	25' E	1.6	70.3	
400' N	00 E+W	40.8	72.7	" " " "
400' N	25' E	0.8	71.1	
400' N	50' E	4.1	67.8	
400' N	80' E	9.7	62.2	
400' N	100' E	11.4	60.5	
425' N	100' E	9.3	62.6	
400' N	125' E	13.6	58.3	
425' N	125' E	13.0	58.9	
400' N	150' E	14.4	57.5	
400' N	200' E	14.9	57.0	
400' N	220' E	13.0	58.9	
410' N	220' E	14.3	57.6	
400' N	250' E	12.8	59.1	
400' N	260' E	11.2	60.7	
414' N	260' E	12.2	59.7	
400' N	300' E	9.2	62.7	
413' N	300' E	8.8	63.1	
415' N	300' E	10.2	61.7	
425' N	300' E	10.7	61.2	
425' N	310' E	8.5	63.4	
400' N	310' E	8.6	63.3	

71.92

400'.N	330'.E	6.2	65.7
425'.N	330'.E	6.3	65.6
400'.N	350'.E	5.0	66.9
400'.N	392'.E	5.7	66.2
400'.N	400'.E	7.4	64.5
400'.N	407'.E	7.3	64.6
400'.N	413'.E	5.7	66.2
450'.N	398'.E	5.5	66.4
450'.N	392'.E	7.0	64.9
450'.N	380'.E	3.9	68.0
450'.N	360'.E	3.3	68.6
450'.N	350'.E	4.0	67.3
450'.N	325'.E	8.1	63.8
450'.N	300'.E	9.5	62.4
450'.N	250'.E	12.1	59.8
450'.N	200'.E	12.1	59.8
487'.N	200'.E	13.7	58.2
450'.N	150'.E	12.7	59.2
450'.N	125'.E	11.9	60.0
450'.N	100'.E	9.5	62.4
450'.N	70'.E	7.5	64.4
450'.N	50'.E	4.4	67.5
450'.N	25'.E	1.2	70.7
450'.N	00.E+W	+3.6	75.5
500'.N	00.E+W	+3.0	74.9

Traveled RA
Boundary St

" "

E. Line 40th

" " "

71.92

500'.N	25'.E	0.8	71.1	
500'.N	50'.E	4.4	67.5	
500'.N	100'.E	9.4	62.5	
500'.N	125'.E	10.9	61.0	
500'.N	150'.E	9.9	62.0	
500'.N	165'.E	10.7	61.2	
500'.N	200'.E	9.6	62.3	
525'.N	200'.E	7.3	64.6	
500'.N	250'.E	8.6	63.3	
500'.N	300'.E	8.3	63.6	
515'.N	300'.E	7.0	64.9	
525'.N	300'.E	4.3	67.6	
500'.N	325'.E	6.6	65.3	
500'.N	350'.E	4.4	67.5	
500'.N	344'.E	4.1	67.8	
500'.N	378'.E	6.3	65.6	
510'.N	378'.E	4.7	67.2	
500'.N	383'.E	5.1	66.8	
T.P.	10.27	80.39	1.80	70.12
T.P. BM.	4.82	82.08	3.13	77.26
525'.N	00.E	8.2	73.9	
525'.N	25'.E	12.2	69.9	
540'.N	00.E	18.0	74.1	
550'.N	00.E	19.6	72.5	
575'.N	00.E	11.7	70.4	
575'.N	25'.E	14.1	68.0	

MK View Park

48

Traveled Rd
Boundary StN.W. Teak + 40thE. Line 40th

" " "

" " "

" " "

2nd fl.
garage floor

		82.08		
550' N	25' E	11.5	11.5	70.6
575' N	50' E	14.6	14.6	67.5
550' N	100' E	18.3	18.3	63.8
550' N	125' E	19.4	19.4	62.7
550' N	150' E	14.4	14.4	63.7
550' N	200' E	16.8	16.8	65.3
550' N	250' E	15.3	15.3	66.8
550' N	300' E	13.4	13.4	68.7
550' N	350' E	13.3	13.3	68.8
550' N	375' E	13.2	13.2	68.9
550' N	385' E	13.3	13.3	68.8
571' N	380' E	13.7	13.7	68.45
575' N	333' E	13.1	13.1	69.05
591.5' N	375' E	13.6	13.6	68.5
600' N	375' E	13.0	13.0	69.1
610' N	370' E	8.8	8.8	73.3
610' N	350' E	10.9	10.9	71.2
600' N	350' E	12.6	12.6	69.5
600' N	323.3' E	13.0	13.0	69.1
600' N	290.8' E	12.4	12.4	69.75
425' N	250' E	12.7	12.7	69.4
425' N	240' E	10.6	10.6	71.5
625' N	246' E	11.6	11.6	70.5
625' N	293.9' E	12.3	12.3	69.8
625' N	315' E	11.0	11.0	71.1
625' N	350' E	9.4	9.4	72.7

		82.08		
625' N	366' E	8.3	8.3	73.8
638' N	361' E	5.7	5.7	76.4
650' N	359' E	5.7	5.7	76.4
650' N	350' E	6.6	6.6	75.5
650' N	325' E	8.6	8.6	73.5
650' N	300' E	9.0	9.0	73.1
650' N	288' E	9.4	9.4	72.7
650' N	275' E	11.5	11.5	70.6
650' N	268.9' E	11.5	11.5	70.6
650' N	240.8' E	10.9	10.9	71.2
650' N	235' E	9.9	9.9	72.2
650' N	225' E	13.0	13.0	69.1
600' N	250' E	13.6	13.6	68.5
600' N	200' E	16.4	16.4	65.7
600' N	150' E	17.9	17.9	64.2
600' N	100' E	17.7	17.7	64.4
600' N	50' E	16.6	16.6	65.5
600' N	00' E	12.3	12.3	69.8
625' N	00' E	12.5	12.5	69.6
625' N	25' E	15.4	15.4	66.7
650' N	00' E	13.5	13.5	68.6
650' N	10' E	14.9	14.9	67.2
650' N	50' E	16.0	16.0	66.1
650' N	100' E	16.5	16.5	65.6
650' N	150' E	16.7	16.7	65.4
650' N	200' E	15.0	15.0	67.1

N. edge pav.

S.W. " "

E. Line #40

82.08

675' N	200' E	13.8	68.3
675' N	210' E	9.6	72.5
675' N	216' E	10.2	71.9
675' N	244' E	10.4	71.3
675' N	255' E	10.7	71.4
675' N	275' E	9.4	72.7
675' N	300' E	7.9	74.2
675' N	318' E	7.9	74.2
675' N	325' E	6.1	76.0
675' N	350' E	3.5	78.6
700' N	344' E	3.0	79.1
700' N	320' E	3.5	78.6
700' N	300' E	7.2	74.9
700' N	275' E	8.1	74.0
700' N	250' E	8.9	72.2
700' N	231' E	11.1	71.0
700' N	224' E	9.2	72.9
700' N	219.4 E	9.9	72.2
700' N	191' E	9.5	72.6
700' N	185' E	8.5	73.6
700' N	175' E	14.0	68.1
700' N	150' E	14.9	67.2
706' N	149' E	14.8	67.3
700' N	100' E	14.9	67.2
706' N	50' E	14.8	67.3
700' N	6' E	13.6	68.5

FL outlet 18" cmt.
Pipe Culvert
Crossing Ocean View Blvd

82.08

Mt. View Park

50

700' N	00' E	11.8	70.3
682' N	2' E	14.1	68.0
750' N	00' E	9.9	72.2
750' N	5' E	11.4	70.7
750' N	50' E	12.0	70.1
762' N	50' E	11.3	70.8
750' N	100' E	12.4	69.7
760' N	100' E	8.0	74.1
740' N	125' E	13.3	68.8
750' N	125' E	11.0	71.1
760' N	125' E	7.4	74.7
750' N	136' E	7.1	75.0
750' N	141.5 E	8.0	74.1
750' N	169.6 E	8.3	73.8
750' N	175' E	7.2	74.9
750' N	185' E	11.3	70.8
750' N	200' E	11.6	71.5
738' N	200' E	12.1	70.0
725' N	145' E	14.2	67.9
725' N	161' E	7.7	74.4
725' N	166' E	8.8	73.3
725' N	194.6 E	9.1	73.0
725' N	200' E	8.4	73.7
725' N	208' E	11.8	71.3
750' N	225' E	10.0	72.1
750' N	240' E	8.3	73.8

E. Line 40"
FL outlet cmt.
Pipe Culvert
Crossing 40th St.
E. Line 40th

FL Inlet 18" cmt.
Pipe Culvert
Crossing Ocean View Blvd

s.w. edge pavmt.

N.E. " "

s.w. Edge Pavmt.

N.E. " "

82.04

750' N	250' E	2.8	74.3
750' N	263' E	7.6	74.5
750' N	275' E	5.6	76.5
750' N	300' E	3.3	78.8
750' N	330' E	0.8	81.3
800' N	317' E	+ 3.2	85.3
800' N	300' E	0.3	81.8
800' N	250' E	5.1	77.0
800' N	235' E	6.2	75.9
800' N	225' E	7.9	74.2
800' N	200' E	7.9	74.2
800' N	175' E	9.5	72.6
800' N	150' E	10.1	72.0
800' N	142' E	10.1	72.0
775' N	200' E	10.6	71.5
775' N	175' E	11.2	70.9
775' N	162' E	11.0	71.1
775' N	151' E	6.5	75.6
775' N	144.9 E	7.5	74.6 N.E. edge paymt.
775' N	116.4 E	7.2	74.9 S.W. " "
775' N	113' E	5.9	76.2
775' N	1100' E	7.4	74.7
775' N	75' E	7.4	74.7
765' N	75' E	7.3	74.8
770' N	50' E	7.0	75.1
775' N	50' E	7.0	75.1

82.08

Mt. View Park

51

770' N	25' E	10.3	71.8
775' N	25' E	6.9	75.2
775' N	10' E	9.3	72.8
775' N	00 E	7.3	74.8 E. line 40 th
785' N	00 E	5.3	76.8 " " "
785' N	10' E	5.3	76.8
800' N	126' E	5.4	76.7
800' N	120.3 E	6.5	75.6 N.E. edge paymt.
800' N	91.8 E	6.3	75.8 S.W. " "
800' N	85' E	5.2	76.9
800' N	75' E	5.8	76.3
800' N	50' E	5.9	76.2
800' N	25' E	5.5	76.6
800' N	00' E	4.8	77.3 E. line 40 th
825' N	00' E	4.0	78.1 " " "
825' N	25' E	4.3	77.8
825' N	50' E	4.9	77.2
825' N	54' E	5.3	76.8 S.W. edge paymt.
825' N	82.5 E	5.8	76.3 N.E. " "
825' N	88' E	4.7	77.4
825' N	111' E	8.3	75.8
838.3 N	00' E	3.60	78.48 E. End ent. el Return gutter
838.3 N	00' E	4.15	77.93 S.W. edge paymt.
850' N	00' E	3.75	78.33 on " "
850' N	50' E	4.55	77.53 " " "
850' N	70.4 E	5.01	77.07 N.E. edge "

82.08

850' N	75' E	4.1	78.0
850' N	92' E	7.3	74.8
850' N	100' E	7.7	74.4
850' N	150' E	7.4	74.7
850' N	200' E	6.8	75.3
850' N	250' E	3.3	78.8
850' N	263' E	2.0	80.1
T.P.	10.84	90.89	2.03 80.05
850' N	302' E	4.2	86.7
879' N	292' E	4.7	86.2
890' N	290' E	5.1	85.8
890' N	275' E	6.7	84.2
890' N	250' E	10.7	80.2
900' N	288' E	6.7	84.2
900' N	275' E	9.1	81.8
900' N	250' E	10.9	80.0
900' N	225' E	13.2	77.7
900' N	200' E	13.2	77.7
900' N	150' E	11.6	79.5
900' N	150' E	13.2	77.7
900' N	100' E	12.7	78.2
900' N	75' E	13.5	77.4
900' N	50' E	13.8	77.1
900' N	14' E	12.4	78.5
900' N	00' E	10.7	80.2
875' N	00' E	12.00	78.89

E Line 40th st

" " "

90.89

Mt. View Park

52

875' N	44' E	13.17	77.72	N.E. edge pavmt
875' N	50' E	11.9	79.0	
875' N	60' E	13.5	77.4	
875' N	75' E	14.7	76.2	
880' N	50' E	12.0	78.9	
890.3' N	50' E	13.8	77.1	
890.3' N	25' E	11.5	79.4	
887' N	25' E	12.77	78.12	
890.3' N	00' E	12.12	78.77	Cutter N.E. edge Pavmt.
890.3' N	00' E	11.37	79.52	E. End ch. Return
950' N	00' E	9.1	81.8	E. Line 40 th
950' N	6' E	11.9	79.0	E. End outlet. 24" Cor. Iron Pipe Crossing 40 th St
950' N	6' E	10.9	80.0	
950' N	50' E	10.2	80.7	
950' N	75' E	4.8	82.1	
975' N	75' E	6.7	84.2	
950' N	100' E	8.5	82.4	
950' N	120' E	8.9	82.0	
950' N	125' E	7.6	83.5	
950' N	150' E	7.3	83.6	
950' N	200' E	9.2	81.7	
950' N	225' E	9.6	81.3	
950' N	250' E	8.5	82.4	
950' N	274' E	7.3	83.6	dirt floor garage.
T.P.	11.98	102.01	0.86	90.03

102.01

990' N	263' E	15.1	86.9
990' N	250' E	15.4	86.6
990' N	237' E	15.6	86.4
990' N	225	15.8	86.2
1000' N	262' E	11.6	90.4
1000' N	250' E	11.6	90.4
1000' N	240' E	12.4	89.6
1000' N	235' E	14.3	87.7
1000' N	225' E	14.2	87.8
1000' N	200' E	12.0	90.0
1000' N	175' E	9.3	92.7
1000' N	150' E	8.9	94.1
1000' N	125' E	12.0	90.0
1000' N	100' E	13.7	88.3
1000' N	93' E	14.1	87.9
1000' N	90' E	17.0	85.0
1000' N	65' E	15.9	86.1
1000' N	50' E	17.2	84.8
1000' N	25' E	18.5	83.5
1000' N	00' E	18.8	83.2
105' R	9.21	109.46	1.76
1025' N	00' E	24.8	84.7
1025' N	15' E	23.5	86.0
1025' N	25' E	23.6	85.9
1025' N	50' E	21.5	88.0
1025' N	77' E	22.3	87.2

109.46

Mt. View Park

53

1025' N	80' E	20.3	89.2
1025' N	100' E	17.7	91.8
1025' N	125' E	15.4	94.1
1025' N	150' E	11.1	98.4
1025' N	165' E	10.4	99.1
1025' N	175' E	10.4	98.7
1025' N	200' E	14.6	94.9
1025' N	215' E	17.4	92.1
1025' N	225' E	17.7	91.8
1025' N	254' E	17.4	92.1
1030' N	253' E	17.4	92.1
1050' N	247' E	14.0	95.5
1050' N	225' E	14.0	95.5
1050' N	200' E	9.6	99.9
1050' N	175' E	7.2	102.3
1050' N	150' E	7.5	102.0
1050' N	125' E	13.1	96.4
1050' N	100' E	14.9	94.6
1050' N	70' E	18.8	90.7
1050' N	65' E	20.5	89.0
1050' N	50' E	19.7	89.8
1050' N	25' E	20.4	89.1
1050' N	15' E	20.7	88.8
1050' N	7' E	23.3	86.2
1050' N	00' E	23.6	85.9

cmt floor
garageE. line 40th

109.46

1075' N

00' E	22.2	87.3	E. line 40 th
10' E	23.1	86.4	
17' E	18.6	90.9	
51' E	18.6	90.9	
55' E	16.3	93.2	
75' E	14.8	94.7	
100' E	13.3	96.2	
125' E	10.5	99.0	
150' E	7.0	102.5	
175' E	7.2	102.3	
200' E	8.3	101.2	
225' E	10.6	98.9	
240' E	11.0	98.5	

1100' N

233' E	8.4	101.1	
200' E	8.1	101.4	
175' E	6.7	102.8	
150' E	6.2	103.3	
125' E	7.7	101.8	
100' E	9.8	99.7	
75' E	12.6	96.9	
50' E	13.5	96.0	
45' E	14.7	94.8	
40' E	17.3	92.2	
15' E	16.8	92.7	
00' E	19.9	89.6	E. line 40 th

109.46

1125' N

00' E	17.1	92.4	E. line 40 th
10' E	15.3	94.2	
28' E	15.8	93.7	
31' E	14.0	95.5	
50' E	12.3	97.2	
75' E	10.3	99.2	
100' E	7.4	102.1	
110' E	6.3	103.2	
125' E	5.9	103.6	
150' E	5.6	103.9	
175' E	6.8	102.7	
200' E	7.6	101.9	
225' E	8.0	101.5	

1150' N

220' E	8.0	101.5	
200' E	7.2	102.3	
175' E	5.7	103.8	
150' E	5.6	103.9	
125' E	5.3	104.2	
100' E	6.1	103.4	
75' E	7.3	102.2	
50' E	10.1	99.4	
25' E	11.3	98.2	
18' E	14.5	95.0	
5' E	14.0	95.5	
00' E	14.6	94.9	E. line 40 th

Mt. View Park

54

109.46

1175' N

00' E	11.2	98.3	E. Line 40 th
9' E	9.8	99.7	
15' E	10.3	99.2	
25' E	9.1	100.4	
50' E	6.4	102.9	
75' E	5.1	104.4	
100' E	4.2	105.3	
125' E	5.2	104.3	
150' E	5.9	103.6	
175' E	6.8	102.7	
200' E	7.7	101.8	
212' E	7.4	102.1	
1200' E			
205' E	7.7	101.8	
175' E	7.1	102.4	
150' E	6.2	103.3	
125' E	5.1	104.4	
100' E	4.9	104.6	
75' E	4.5	105.0	
50' E	5.0	104.5	
25' E	6.8	102.7	
6' E	8.2	101.3	
00' E	10.9	98.6	E. Line 40 th

109.46

Mt. View Park

55

1225' N

3' W	11.0	98.5	
00	9.8	99.7	E. Line 40 th
2' E	5.3	104.2	
25' E	5.0	104.5	
50' E	4.6	104.9	
75' E	4.5	105.0	
100' E	4.9	104.6	
125' E	5.9	103.6	
150' E	7.3	102.2	
175' E	8.0	101.5	
197' E	8.0	101.5	
1250' N			
190' E	12.5	97.0	
175' E	12.0	97.5	
150' E	9.4	100.1	
125' E	7.4	102.1	
100' E	5.5	104.0	
75' E	4.1	104.8	
50' E	4.3	105.2	
25' E	4.3	105.2	
2' E	4.0	105.5	
00	8.1	101.4	E. Line 40 th St
3' W	9.3	100.2	

109.46

1275' N

3' W	7.9	101.6	
00	6.3	103.2	E. Line 40 th
2' E	3.1	106.4	
25' E	3.4	106.1	
50' E	4.0	105.5	
75' E	4.5	105.0	
100' E	5.4	104.1	
125' E	7.2	102.3	
150' E	9.9	99.6	
185' E	14.1	95.4	

1300' N

176' E	18.0	91.5	
150' E	11.4	98.1	
135' E	7.2	102.3	
125' E	6.0	103.5	
100' E	5.0	104.5	
75' E	4.4	104.1	
50' E	3.6	105.9	
25' E	3.1	106.4	
2' E	3.7	105.8	
00	7.2	102.3	E. Line 40 th
3' W	7.5	102.0	

1325' N

3' W	9.0	100.5	
00	8.2	101.3	E. Line 40 th
2' E	4.2	105.3	

109.46

Mt. View Park

56

25' E	3.6	105.9	
50' E	3.1	106.4	
75' E	5.2	104.3	
100' E	5.0	104.5	
125' E	6.8	102.7	
150' E	13.8	95.7	
T.P.	1.54	105.69	
173' E	5.31	104.15	
	16.0	89.7	

1350' N

763' E	18.2	87.5	
150' E	14.9	90.8	
125' E	8.1	97.6	
100' E	4.1	101.6	
75' E	2.8	102.9	
50' E	2.1	103.6	
25' E	0.8	104.9	
2' E	2.0	103.7	
00	6.1	99.6	E. Line 40 th
4' W	7.2	98.5	
1358' N	00' E	7.5	98.2 E. Line 40 th
1358' N	2' E	2.8	102.9
1358' N	25' E	1.4	103.9
1355' N	50' E	2.9	102.8
1355' N	75' E	3.8	101.9
1354' N	100' E	4.6	101.1

105.69

1360' N	00' E	7.6	98.1
1360' N	2' E	7.4	98.1
1360' N	25' E	10.3	95.4
1360' N	50' E	13.8	91.9
1360' N	75' E	16.3	89.4
1358' N	100' E	18.2	87.5
1355' N	125' E	19.4	86.3
1353' N	150' E	20.2	85.5
1356' N	162' E	21.4	84.3
1369.4' N	161' E	22.4	83.3

W. End of S. Curb
Franklyn Ave.

1375' N.

161' E	22.2	83.5
150' E	21.8	83.9
125' E	20.4	85.3
100' E	18.7	87.0
75' E	17.0	88.7
50' E	14.1	91.6
25' E	11.3	94.4
00' E	9.1	96.6

E. Line 40'

1400' N

00' E	9.3	96.4
25' E	11.2	94.5
50' E	13.8	91.9
75' E	16.3	89.4
100' E	18.3	87.4
125' E	20.3	85.4

E. Line 40'

105.69

Mt. View Park

57

W. End of N. Curb
Franklyn Ave.

1400' N - 150' E	22.3	83.4
1410' N 50' E	13.1	92.6
1416' N 50' E	14.7	91.0
1410' N 25' E	11.1	94.6
1418' N 25' E	13.5	92.2
1418' N 75' E	12.9	92.8
1418' N 5' E	9.5	96.2
1410' N 5' E	9.5	96.2
1429' N 10' E	14.5	91.2

Fl. Outlet 24" dia
Pipe Culvert
Crossing Holt St.

1425' N

00' E	9.0	96.7
8' E	12.4	93.3
25' E	13.1	92.6
50' E	14.5	91.2
75' E	16.1	89.6
100' E	17.7	88.0
125' E	18.9	86.8
143' E	19.4	86.3

E. Line 40'

1450' N

136' E	16.0	89.7
125' E	16.5	89.2
100' E	16.0	89.7
75' E	15.2	90.5
40' E	14.4	91.3
50' E	12.2	93.5

105.69
1450' N.

25' E		6.8	98.9	
00 E		7.4	98.3	E. line 40"
1437' N	25' E	12.8	92.9	
1441' N	50' E	14.5	91.2	

1475' N

00 E		5.2	100.5	E. line 40"
25' E		4.6	101.1	
50' E		5.8	99.9	
65' E		6.9	98.8	
75' E		9.9	95.8	
100' E		10.9	94.8	
115' E		10.0	95.7	
125' E		8.3	97.4	
130' E				

1485' N	75' E	7.7	98.0	
1490' N	50' E	5.4	100.3	
1466' N	50' E	5.9	99.8	
1492' N	25' E	4.2	101.5	
1492' N	00' E	3.7	102.0	E. line 40"

105.69

1500' N.

MT. View Park

58

00' E		3.3	102.4	E. line 40"
25' E		2.1	103.6	
50' E		2.9	102.8	
75' E		3.6	102.1	
100' E		3.8	101.9	
122' E		3.5	102.2	

T.P. 11.76 115.78 1.67 104.02

1510' N	120' E	12.0	
7510' N	100' E	11.8	104.0
1510' N	75' E	11.4	104.4
1510' N	50' E	11.1	104.7

1525' N

00 E		11.3	104.5	E. line 40"
3' E		9.7	106.1	
25' E		9.7	106.1	
50' E		9.9	105.9	
75' E		10.3	105.5	
100' E		10.0	105.8	
116' E		10.5	105.3	

1550' N

109' E		8.7	107.1
100' E		8.7	107.1
75' E		8.3	107.5
50' E		8.0	107.8
25' E		7.7	108.1

Grades on Tennis Courts

Tennis Courts Mt. View Park

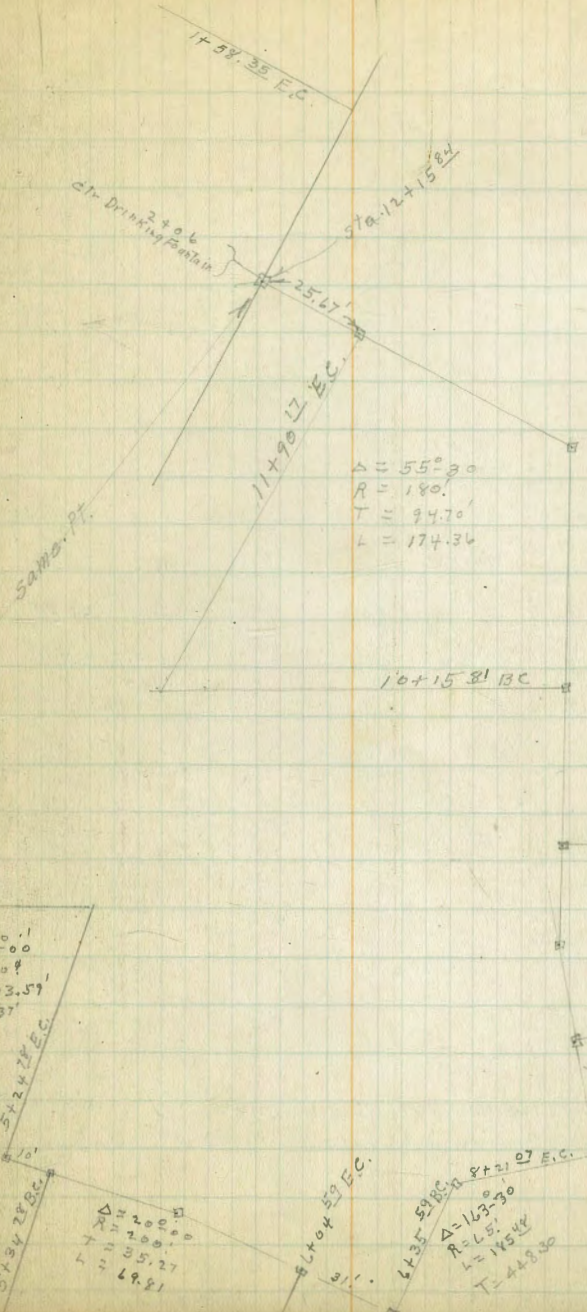
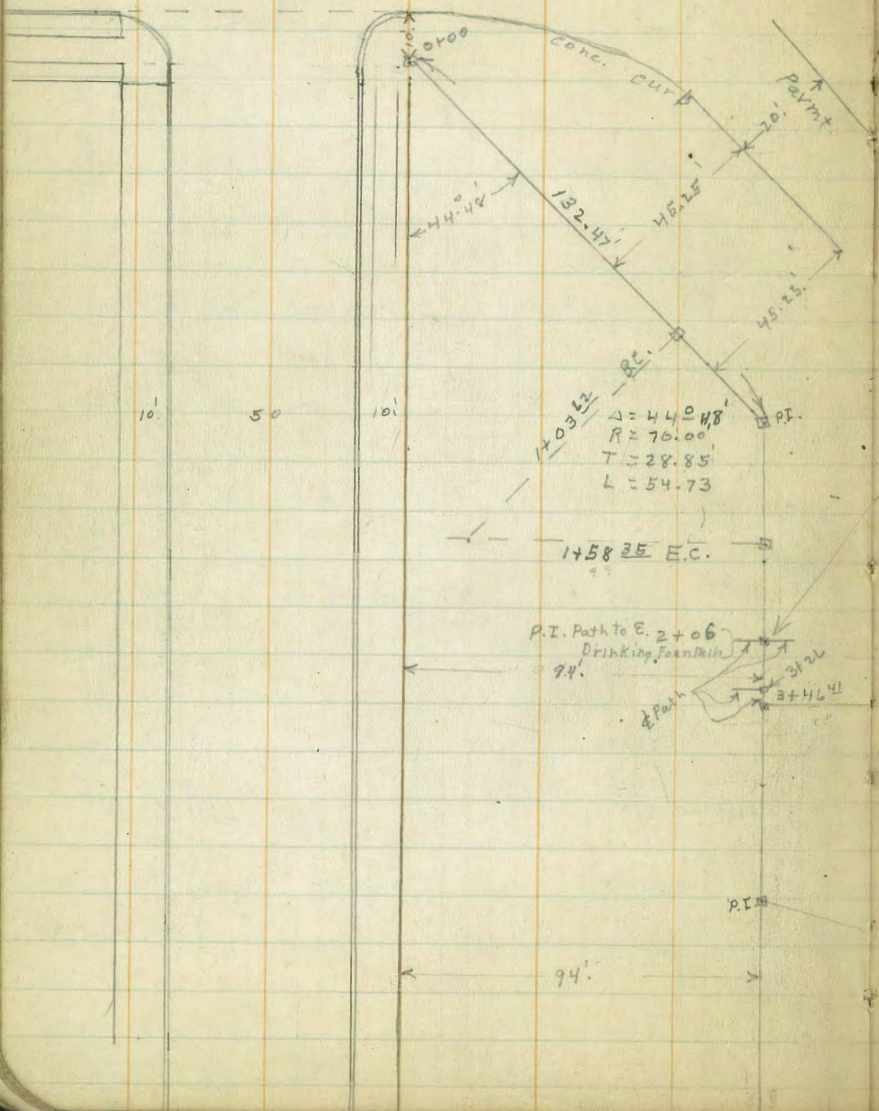
	W. Edge	±	E. Edge	
2+40 N. End	8.5 68.8 +1.00 67.80	8.43 68.87 68.20 C.0.67	9.06 68.24 68.20 C.0.04	9.44 67.86 - B.M. 68.20 F0.34
2+10	culvert 10.92 FL 66.38 EX 47.80 2.00	9.35 67.95 67.95 0.00 V	10.27 67.03 67.95 F0.92 V	10.66 66.64 67.95 F1.31 V
1+80	FL 65.80 culvert to be lowered.	9.87 67.43 67.70 F0.27 V	9.66 67.64 67.70 F0.06 V	11.47 65.83 67.70 F1.87 V
1+50		10.49 66.81 67.45 F0.64 V	10.08 67.22 67.45 F0.23 V	11.80 65.50 67.45 F1.95 V
1+20		9.52 67.78 67.20 C.0.58 V	11.70 65.60 67.20 F1.60 V	12.71 64.59 67.20 F2.61 V
0+90		8.49 68.81 66.95 C.1.86 V	10.67 66.63 66.95 F0.32 V	12.59 64.71 66.95 F2.24 V
0+60		6.18 71.12 66.70 C.4.42 V	9.53 67.77 66.70 C.1.07 V	12.13 65.17 66.70 F1.53 V
0+30		5.88 71.42 66.45 C.4.97 V	9.75 67.55 66.45 C.1.10 V	12.50 64.80 66.45 F1.65 V
0+00 S. End	5.30 72.00 +4.2 67.80	5.17 72.13 66.20 C.5.93 V	9.65 67.65 66.20 C.1.41	12.90 64.40 66.20 F1.80

82.19 B.M. NW. 7. ct. 40 th Ocean View.	77.26 B.M. S.P. W.W. 40 th + Teak Sts.	0.04	0.0	Grade
77.30	68.2	5.17	5.4	68.20
72.13	4.8	1.51	C.0.6	1.52
73.64				68.20
5.08	67.95	84	5.7	67.95
47.5 Red.	5.7	2.60	0.0	1.77
2.20		8.95		47.95
2.20	67.70			67.70
out. 6.5	5.9			5.9
± line 40 th St.	5.9			2.02
20.0'	6.0			67.70
30.0'				67.45
30.0'	67.45			67.45
out. 6.3	6.2			2.27
77.26	0.2			67.45
1.36				67.20
78.62	67.20			6.4
	6.4			5.8
out. 0.6	60.6			2.52
				67.20
	66.95			66.95
out. 0.3	11.7			6.7
	11.4			2.77
	0.3			66.95
				66.70
out. 4.8	11.9			3.02
	7.1			2.02
	4.8			66.70
				66.70
out. 4.8	66.45			66.45
	12.2			7.2
	7.4			3.27
	4.8			66.45
				66.45
	2.52			66.20
	1.52			3.52
	0.20			66.20
	66.20			66.20
out. 1.4	12.4			12.4
	5.0			6.6
	7.4			11.0
				6.8
				1.4
				6.2
				7.4
				9.6
				6.2

6-12-34
Miller
Walker
Bliss

Walk layout Mt. View Park.

Ocean View



Path: A. Alignment.

63

2+06 P.I. Path to E

1+75

1+58³⁵ EC.

chd.
18.19

Def \angle s.
22°-24'

$$\Delta = 44^{\circ}-44'$$

1+40¹⁰

18.19

14°-56'

$$R = 70'$$

$$T = 28.85'$$

1+21⁸⁶

18.19

7°-28'

$$L = 54.73$$

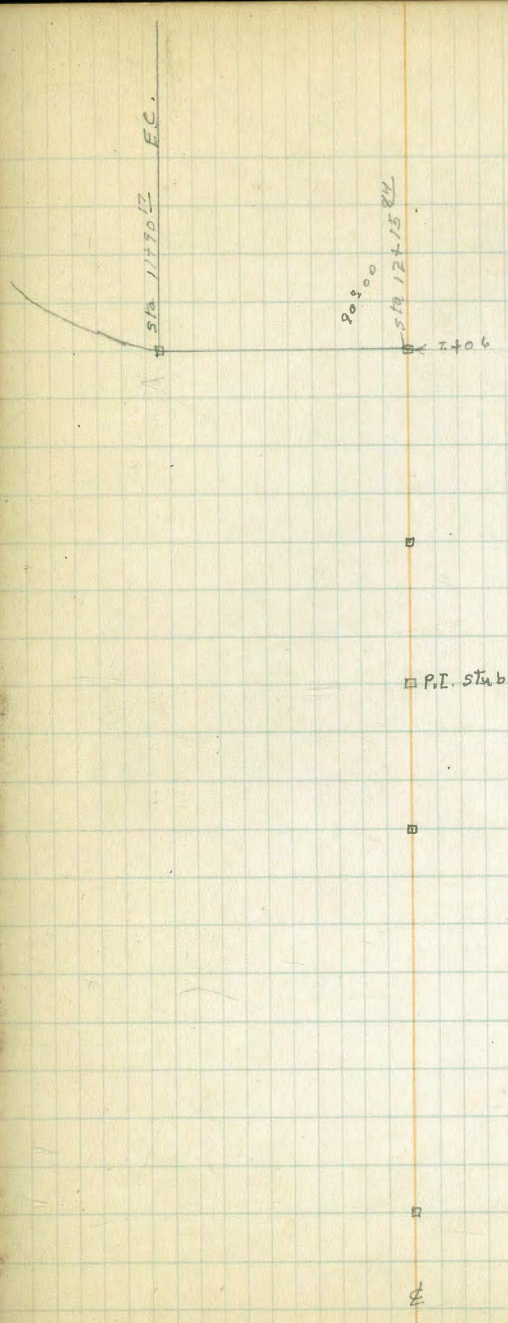
1+03¹² B.C. RT.

0+75

0+50

0+25

0+00 = { 4' on. of S. line Ocean View + E. line 40th
10' curb. Radius S.E. Cor. 40th + Ocean View. Blvd.



5+24 ⁷⁸ EC Def. Ls.
 29.67 36-30

4+95 ⁰⁶ 30-25

"

$$\Delta = 73^{\circ} 00'$$

4+65 ³³ 24-20

$$R = 140'$$

"

$$T = 103.59'$$

4+35 ⁶⁰ 18-15

$$L = 178.37'$$

□ P. I. Stub

"

4+05 ²⁷ 12-10

"

3+76 ¹⁹ 6-05

29.67

3+46 ⁴¹ B.C. Lt.

3+25

3+00

2+75

2+50

2+25

8487⁵⁸ B.C. Rt.

8450

8421⁰⁷ EC

cnd.

30.91

Central 29.

163°-30'

7490¹⁴

"

136°-15'

7459²³

"

109°-00'

7428³²

"

81°-45'

$$A = 163^{\circ}-30'$$

$$R = 65'$$

$$L = 185.48'$$

6497⁴¹

"

54°-30'

6466⁵⁰

30.91

27°-15'

6435⁵⁹ B.C. Lt.6404⁵⁹ EC.

cnd.

23.25

D.F.L.S.

10°-00'

$$A = 20^{\circ}-00'$$

5481²²

"

6°-40'

$$R = 200'$$

$$T = 35.27'$$

5458⁰⁵

23.25

3°-20'

$$L = 69.81'$$

P.I. Hub.

5434⁷⁸ B.C. Rt.

	End.	Defl.	
11+90 ¹⁷ EC	24.90	27°-45'	
11+65 ²⁷		23°-47'	
11+40 ³⁶		19°-50'	
11+15 ⁴⁵		15°-52'	$\Delta = 55-30'$
10+90 ⁵⁴		11°-54'	$R = 180'$ $T = 94.70$
10+65 ⁶³		7°-56'	$L = 174.36$
10+40 ⁷²		3°-58'	
	24.90		
10+15 ⁸¹ B.C.Lt.			
10+00			
9+75			
9+50			
9+21 ⁹⁸ EC			
9+04 ⁵³			$\Delta = 2-00'$ $R = 1000'$ $T = 17.46$
8+87 ⁰⁸ B.C.Rt			$L = 34.90$

66

P.F. Hub

P.F. Hub.

12 + 15^{sq} = 2 + 06 Drinking Fountain

11 + 90^{sq} EC.

E Levels College Ave
El Cajon St

10+34.52 - NW Estelle

7+84.52 E.C.

5+27.68 B.C.R.T.

3+92.52 E.C.

Set & R.W.

1+35.68 B.C.L.T.

0+05.79 = SW El Cajon Ave

0+00 Ld + C.T. in Pav.

Moore
6-28-40
INDEXED
EPB

do of Pipe
Estelle
N.W.
68

250

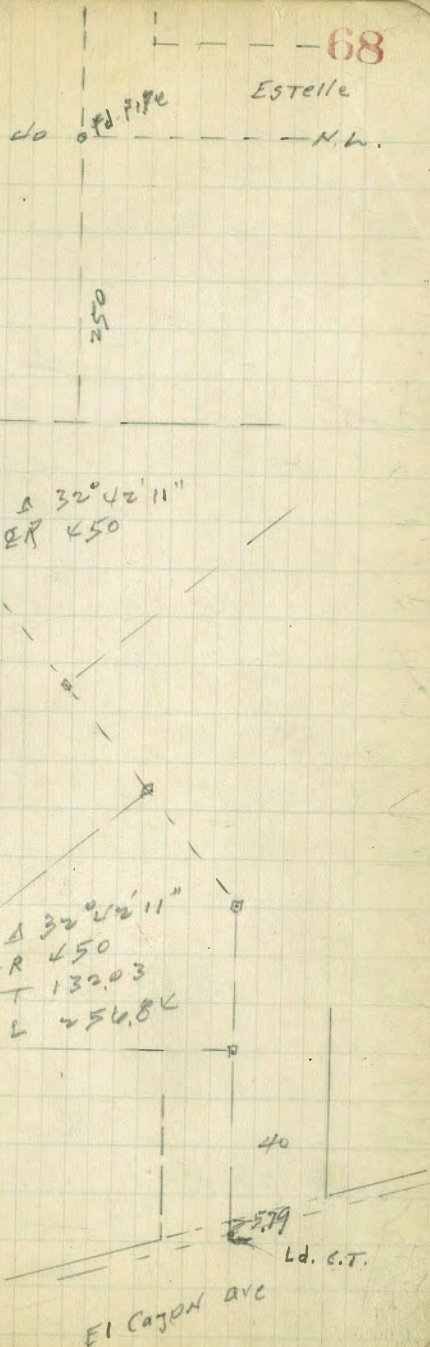
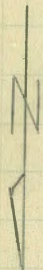
$\Delta 32^{\circ}42'11''$
ER 450

$\Delta 32^{\circ}42'11''$
ER 450
T 132.03
L 256.86

40

El Cajon Ave

Ld. C.T.



LT

2

RT

+50

Contd P 71

493.8
10.5

409.0
53

452.2

19

+50

Y.P. 0.62 454.34 12.92 453.72

454.34 ✓

3

456.0
10.6

+50

458.6

80

459.9

6.7

✓

150

461.5

51

461.8

4.8

1435.08 BC RT.

NINBP 1.37 466.64

465.27 El Canyon College

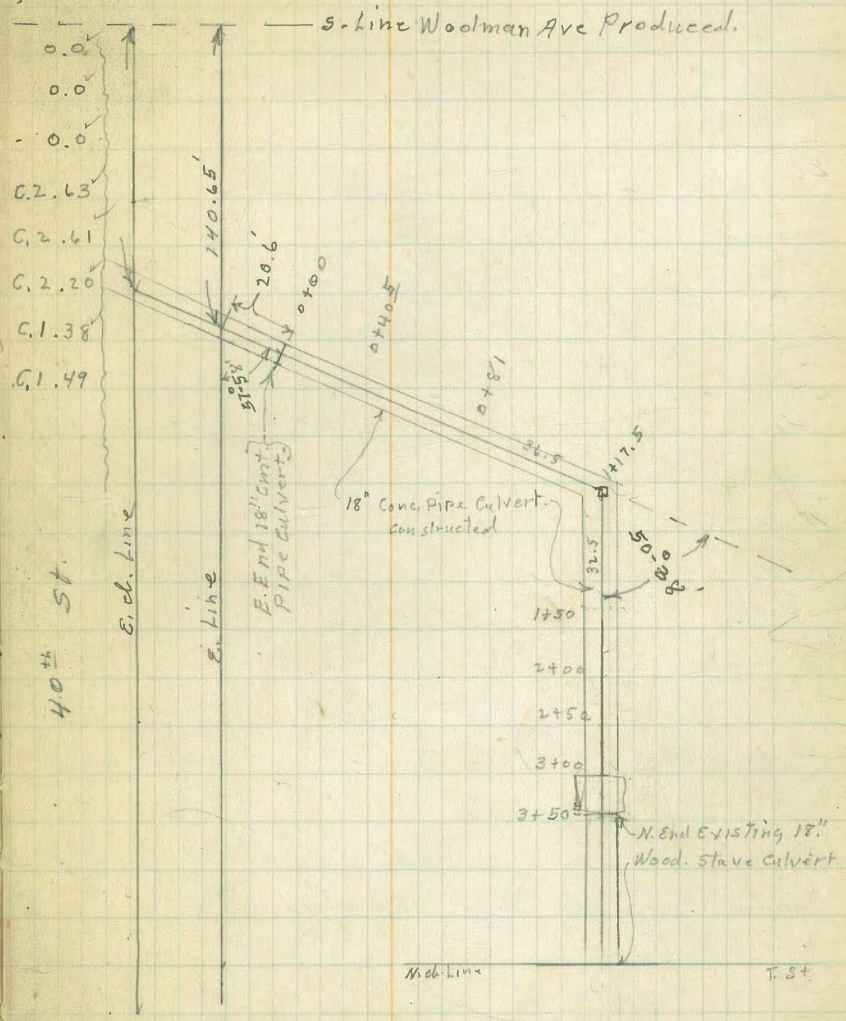
466.64

Culvert Grades.
Mt. View Park

12.37
11.57
13.90

36.5
81
117.5 **70**

BM.	1.86	69.72	67.86	Page 61 Grade Bottom Pipe
0+00	Ex. 18" Pipe Present. F.L.	3.27	66.45	
"	" " " " To Be Lowered Bottom Pipe	4.06	65.66	65.50 √4.22 Rod
0+40 ^E	" "	5.60	64.12	64.15 √5.57 Rod
0+81	" "	6.90	62.82	62.86 √6.92 Rod
1+17 ^S Δ	" "	5.21	64.21	61.58
1+50	" "	6.37	63.35	60.74
2+00	" "	8.07	61.65	59.45
2+50	" "	10.18	59.54	58.16
3+00	" "	11.36	58.36	56.87
3+50 ^E	Ex. 18" wood culvert. Bottom			55.57
"	" " " " " 6 F.L.	13.90	55.82	



LT

E

Rt

71

7

483.1

11.7

+50

482.8

11.5

6

480.8

13.5

+65

480.7

14.1

+50

487.1

17.7

5 + 7.68 BC LT.

487.7

17.1

+20 Prop 18" culv. at 90°

438.9

15.4
50

437.1

17.4

435.4

19.0
55

439.7

16.6

5

454.34

front p 69

454.34 /

ESTC 118
Top cb SW College Ave 6.44 438.93 438.36
+34.54

10

+50

9 Prop. 1.8" C/v. at 90°

+50

T.P. 4.04 445.37 13.03 441.31

8

7+84.54 EC

7+50

LT

E

RT

72

442.8

2.6

440.6

4.8

437.4

8.4

436.7

434.6

433.0

8.7

10.8

12.4

45

55

468.6

6.8

445.37 ✓

441.0

13.3

441.7

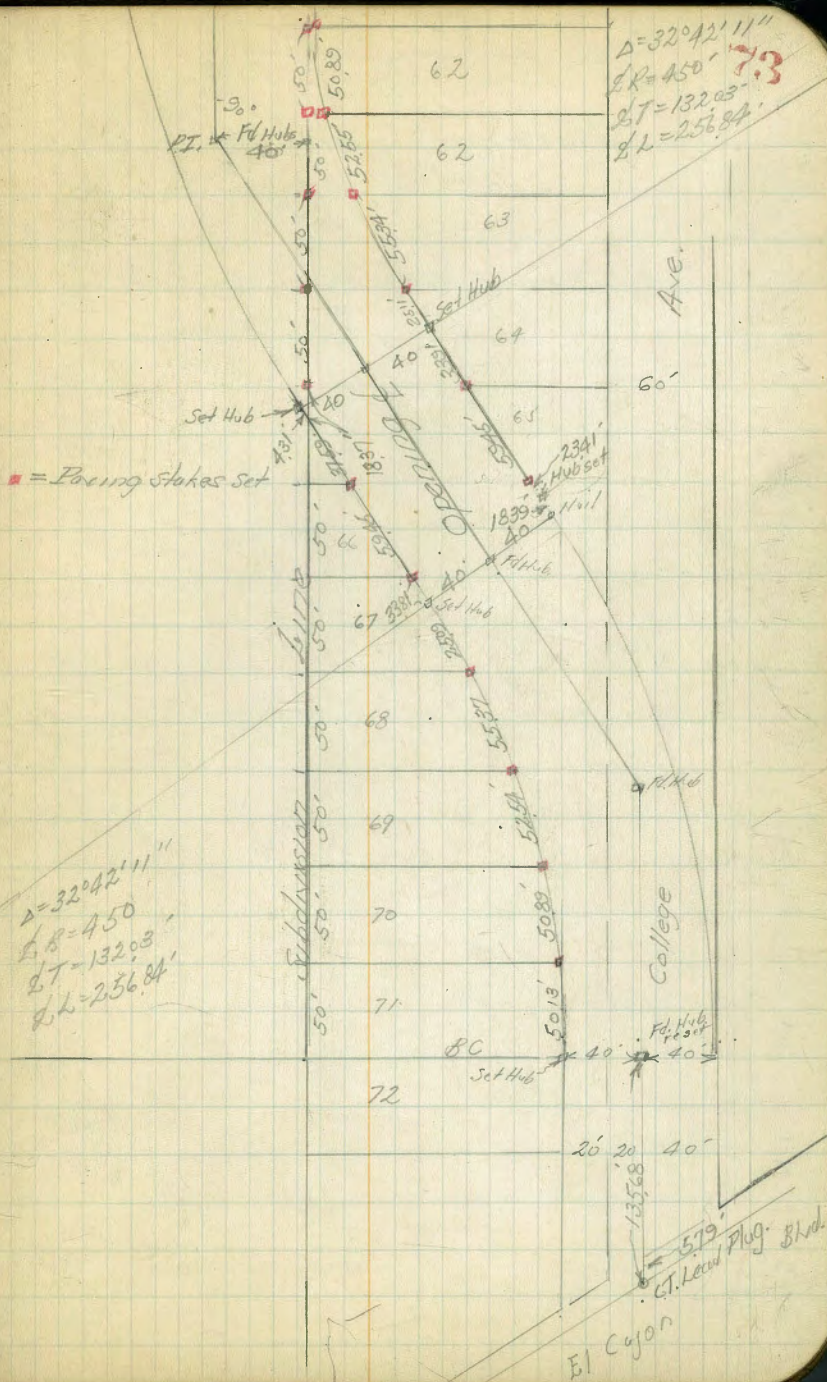
12.5

442.3

12.0

Walker
Bliss
15 July
11-23-40
Station deflection chords.
East line
Location street line as per
OPENING LINE Gilcher Tract
Drawing 5925-L
From B.C. on N line Lot 71, South
See P-68

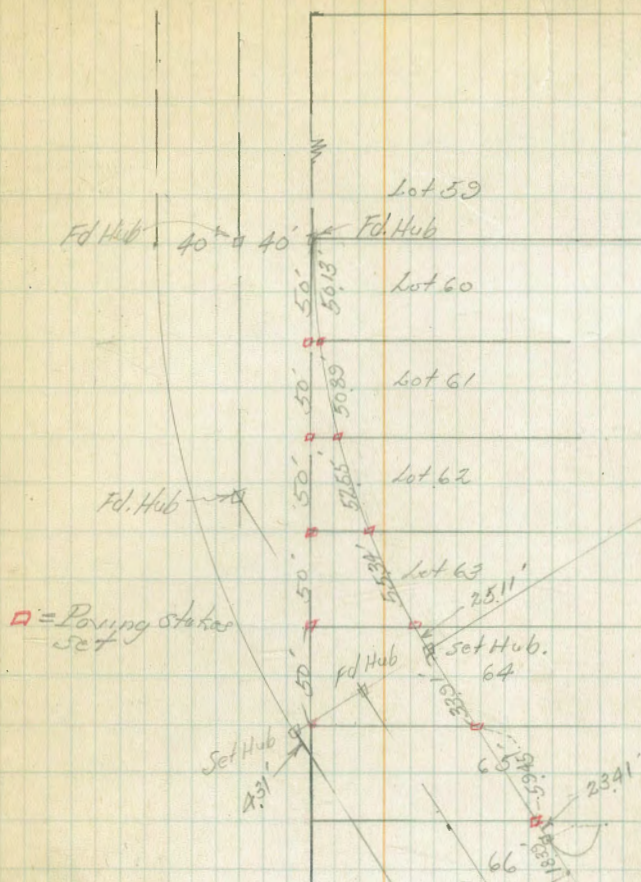
LC, 16°21'05" 25.09'
 Lot 68-69 14°35'48" 55.31'
 Lot 68-69 10°45'46" 52.56'
 Lot 69-70 7°03'29" 50.86'
 Lot 71-70 0+50 13°30'07" 50.09'
 0+00 LC.



Cont. from P. 73
Proposed Opening
As Per Drawing 5925-1

ESTELLE ST.

74



76

June
J. Munday - 5201 - 5-6-7
W. Davis - 11464 - 5-6-7
S. Herman 9865 - 5-6-7
C. Wright 0735 - 5-6-7
C. Deben 14511 - 6-7
a. Kirk. 16205 - 7
J. Coleman - 10875 - 7
G. Markweb - 12615 - 7

Days

7

4

3 1/2

5

7 1/2

5

6

6 1/2

	May	Days
P. Prendy	15603-17-18-19-22	4 ✓
J. Rung	11703-17-18-19-22-23	4 1/2 ✓
D. Hike	13204-17-18-19	2 1/2 ✓
J. Morgan	10598-17-18-22-23	4 ✓
J. Williams	4561-17-18-19-22-23-24-25-26	8 ✓
J. Samuels	10119-17-18-19-22	3 1/2 ✓
L. Montgomery	8561-17-18-19-22	4 ✓
J. Haynes	7448-17-18-19-22	4 ✓
R. Reeves	6976-17-18-19-22-23	4 1/2 ✓
D. Kemp	14897-17-18-19-22-23	5 ✓
J. Rodriguez	14925-17-18-19-22	4 ✓
R. Martin	13177-17-18-19-22	4 ✓
P. Martinez	8439-18-19-22-23-24	5 ✓
T. Royal	8452-18-19-22-23 at bridge	8
J. Surrera	2772-18-19-22-23-24-25	6 ✓
H. Ball	12315-18-19-22-23	4 ✓
H. Hupp	12926-18-19-22-23-26	5 ✓
M. Guirones	11624-18-19-22-23-24-25	6 ✓
H. Goodin	11212-18-19-22-23	4 ✓
J. Moreno	11025-22	1 ✓
H. Blanco	11988-22-23-24	3 ✓
L. Paden	11809-22-23-24-25	4 ✓
P. Ortega	14531-22-23-24-25-26	5 ✓
W. Hanks	12677-22-23-24-25-26	5 ✓
F. Struble	4694-22-23-24-25-26	5 ✓
C. Macias	2943-22-23-24	2 1/2 ✓

78

	May	Days
J. Dyer	15346-22-24-25	2 1/2 ✓
A. Marlow	15660-23 Working at bridge	3 1/2 ✓
A. Heston	11451-22-23-24-25-26	5 ✓
S. Betancor	7831-24-25-26-29-31-1-2-5-6	9 ✓
A. Elias	8515-25-26-29-31-1-2	6 ✓
C. Glason	11418-25-26-29-31	4 ✓
G. Lewis	15286-24-25-26-29	4 ✓
G. Cannon	11662-25	7 ✓
N. Yots	?-26-29-31-1-2-5-6	7 ✓
S. Mahoney	15340-26-27-29-31	4 ✓
J. Malcolm	9123-26-27-29-31-1	5 ✓
J. Moreno	11025-29	1 ✓
M. Orelford	14839-29-31-1-2	3 1/2 ✓
H. Casbeer	11869-31- Bridge	4 ✓
P. Webb	15986-31- Bridge	3 1/2 ✓
H. Peterson	11048-31-1-5-6	4 ✓
M. Arellano	5744-1-2-5-6-7	6 ✓
L. Bellows	12183-1-2-5-6-7	6 ✓
A. Prussdale	11153-1-2-5-6-7	4 ✓
Danny Bolin	8379-1-2	4 ✓
H. Blanco	15778-1-2-5-6	4 ✓
C. Wilson	10594-1-5-5-6	4 1/2 ✓
C. Morales	8592-5-6-7	5 ✓
B. Barrongho	9775-5-6	2 1/2 ✓
D. Rodriguez	4147-5-6-7	6 ✓
P. Charley	8635-5-6-7	6 ✓

L. Mahoney	C# 15340	25-26-27-1-4	✓
G. Markwardt	12615	May-1	1/2 ✓
M. Neacock	9019	" "	1/2 ✓
H. Peterson	11048	May 1-2-3-4	4 ✓
J. Anderson	14897	May 1	1 ✓
C. Dickens	14511	" 1	1 ✓
J. Bellows	12183	" 1-2-3-4-5	5 ✓
H. Dunsdale	11153-B	" 1-2-3-4	4 ✓
C. Gleason	11418	" 1	1 ✓
S. Jacques	9272	" 1	1 ✓
M. Davis	11464	" 2-3-4-5	4 ✓
G. Markwardt	12615	" 2-3-4-5-8	5 ✓
E. Lavin	8165	" 2-3	2 ✓
B. Burroughs	97757 148793	" 2-3-4	2 1/2 ✓
A. Heron	?	" 2-3	1 1/2 ✓
J. Jayden	12458	" 2-3-4	3 1/2 ✓
W. Hayden	6815	" 2-3-4-5	5 ✓
A. Viddl.	8576	" 3-4-5-8	4 ✓
L. Beers	7150	" 3-4-5	2 1/2 ✓
G. Adams	8360	" 3-4-5	2 1/2 ✓
J. Yeargin	5955	" 3	1/2 ✓
J. Munday	5201	" 3-4-5-8-9-10-11	7 ✓
H. Ball	12315	" 3	1 ✓
E. Neal	6537	" 3-4-5	3 ✓
G. Willey	14831	" 3-4-5	2 1/2 ✓

C. Morales	8592	May 4-5-8-9-10	5 ✓
N. Acosta	11005	4-5	2 ✓
J. Learn	10480	4-x-x-x-x-18-19	2 1/2
C. Dickens	14511	4-8-8-9-10-11-12-15	7 1/2
J. Wosten	10940	4	1 ✓
J. McClure	15116	4-5-6-8-9-10	5 1/2 ✓
C. Wright	10735	5-8-9-10-11	5 ✓
P. Chavez	8635	5-8-9-10-11-12	6 ✓
S. Herman	9863	5-6-8-9	3 1/2 ✓
J. ^{Kent} Anderson	14897	8	1 ✓
M. Neacock	9019	8-9-10-11	3 1/2 ✓
C. Gleason	11418	8	1 ✓
L. Janley	5952	8-8-9-10-11	5 ✓
C. Heston	14865	8-9-10	2 1/2 ✓
A. Heron	6006	8-9-10-11-15	10
D. Rosino	10318	8-9-10-11-12	4 1/2 ✓
J. ^{dry} S	12170	8-9-10-11	4 ✓
G. Herrera	12593	8-9-10-11	4 ✓
H. Witten	5210	8-9-10-11-12-15-16-17	7 1/2 ✓
R. Gallegos	15753	9-10-11-12	4 ✓
R. Comacho	3699	9-10-11-12	4 ✓
R. Daniels	6920	9-10-11-12-15-16	6 ✓
H. Ball	12315	10	1 ✓
S. Jacques	9272	10-11-12-15-16	4 1/2 ✓
J. Farbin	9726	10-11-12-15-16	4 1/2 ✓

	Days
✓ C. Mac Gregor - 13412 - 11-12-13-16-17	5 ✓
G. M. Foreman - 1267K - 11-12-18-19-22	3 1/2
M. B. Herrus - 10245 - 11-12 <i>County</i>	6 ✓
H. E. Dowers - 15190 - 11-12-15-18-19	4 ✓
J. J. Coleman - 10875 - 11-12-17-18-19-22-23	7 ✓
C. P. Wooten - 10940 - 12-	1 ✓
P. S. Edward - 14418 - 12-15	2 ✓
H. R. Hise - 14083 - 12-15-16-17-18	5 ✓
C. L. Sharpley - 11773 - 12	2 ✓
E. N. Acosta - 11005 - 15-16-17-18-19	5 ✓
M. C. Blason - 11418 - 15	1 ✓
G. R. Brown - 9841 - 15-16-17-18-19	4 1/2 ✓
E. R. Moreno - 7620 - 15-16-17-18-19-22	5 1/2 ✓
B. For Sprague - 15385 - 15-16-17-18-19	5 ✓
A. H. Hodges - 11571 - 15-16-17-18-19-22-23	8 ✓
J. A. Pedron - 14417 - 15-16-17-18-19	5 ✓
M. G. Razo - 12147 - 16-17-18-19	4 ✓
A. C. Mollenhauer - 2208 - 16-17-18	2 1/2 ✓
L. S. Casillas - 11303 - 16-17	2 ✓
G. O. Darby - 12875 - 16-17-18	2 1/2 ✓
J. A. Casola - 11336 - 16-17-18-19	4 ✓
J. S. Bellows - 12183 - 16-17	2 ✓
H. P. Wooten - 10940 - 18-19-24-25-26	5 ✓
E. G. Cannon - 11662 - 18-19-22-23-24-25-26	7 ✓

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 1/2 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not

IMPROVED TABLES

AND

INFORMATION

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given L may be found by dividing tangent (or external), opposite L by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

82.18
8.71

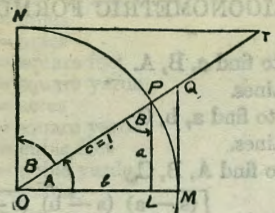
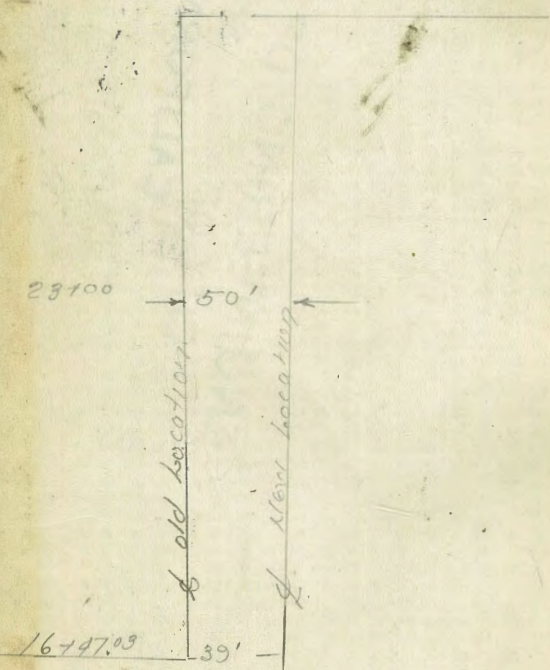


TABLE II
TRIGONOMETRIC FORMULÆ.

$$\begin{aligned} \angle A &= \angle MOP & \angle B &= \angle PON = \angle OPL \\ R &= OB = c = 1 \\ \sin A &= \frac{a}{c} = \frac{a}{1} = a = \cos B = LP \\ \cos A &= \frac{b}{c} = \frac{b}{1} = b = \sin B = OL \\ \tan A &= \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ \\ \cot A &= \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT \\ \sec A &= \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ \\ \csc A &= \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT \\ \text{vers } A &= \frac{LM}{OP} = LM = \text{covers } B \# \\ \text{covers } A &= \frac{OP - LP}{OP} = OP - LP = \text{vers } B \\ \text{exsec } A &= PQ = \text{coexsec } B \\ \text{coexsec } A &= PT = \text{exsec } B \\ \sin \frac{1}{2} A &= \sqrt{\frac{1 - \cos A}{2}} & \cos \frac{1}{2} A &= \sqrt{\frac{1 + \cos A}{2}} \\ \sin 2A &= 2 \sin A \cos A & \cos 2A &= \cos^2 A - \sin^2 A \\ \text{Law of Lines} & \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{C} \\ \text{Law of Cosines} & c^2 = a^2 + b^2 - 2ab \cos C \\ \text{Law of Tangents} & \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)} \end{aligned}$$

723.45
 182.59 from P.T. to Treadle
 40.91
 6962.97
 6912.06
 180 03 30
 70 01 45
 17959.60
 89° 58' 15"
 10.32
 375
 14.07

3 1182° 15' 60"
 1185 25 40'
 121 30 30'



Malcolm
 3061 - Bryan Ave.

10.8
 16.7
 10.65
 21.33
 10.67
 32.00

ENGINEERING DEPARTMENT,
 SAN DIEGO,
 ENGINEERING DEPARTMENT,
 CITY OF CALIFORNIA